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1	Attorney Docket No. 84866		
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3	LOW VOLTAGE PIEZOELECTRIC COMPOSITE FOR TRANSDUCER APPLICATIONS		
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5	STATEMENT OF GOVERNMENT INTEREST		
6	The invention described herein may be manufactured and used		
7	by or for the Government of the United States of America for		
8	governmental purposes without the payment of any royalties		
9	thereon or therefor.		
10			
11	BACKGROUND OF THE INVENTION		
12	(1) Field of the Invention		
13	This invention generally relates to an acoustic transducer's		
14	electromechanical substrate.		
15	More particularly, the invention relates to a piezoelectric		
16	polymer composite substrate enabling an array of transducers		
17	capable of being used with lower voltage than prior art		
18	transducers.		
19	(2) Description of the Prior Art		
20	Several underwater sonar applications exist for high		
21	intensity steered directional acoustic beams. A major drawback		
22	for piezocomposite constructs is the relatively high drive		
23	voltages required to attain significant acoustic intensity per		
24	unit area. This is due to the material's intrinsic broadband		
25	characteristics and the fact that typical designs operate below		

resonance where the impedance phase angle is stable. Phase
stability is required for broadband waveform generation and
reception. The disadvantage of operating off resonance is that
higher voltages are required to produce the equivalent acoustic
intensity.

6 United States Patent Nos. 4,227,111 and 4,412,148 refer to 7 piezoelectric polymer composite substrates that can be used to 8 construct broadband transducers and arrays for sonar 9 applications. The segmentation of the piezoelectric phase and 10 the decoupling characteristics of the backfill polymer enable 11 large transducer apertures operating in a pure thickness mode of 12 vibration.

13 An electrostriction transducer having intermediate 14 electrodes is shown in Sato et al., United States Patent No. 15 4,633,120. The active layer of the transducer is either lead 16 zirconium-titanate or lead magnesium-niobate. This material is 17 incorporated in a polymer slurry which is applied to a substrate 18 such as a Mylar(t) film. A several hundred micron thick active layer is provided. Conductors such as wires are joined directly 19 to contacts positioned between different active layers. 20 The 21 resulting transducer is provided for use in a print head. No provision is made for joining a massive number of co-fired multi-22 23 layered structures in a piezoelectric polymer composite 24 substrate.

It should be understood that the present invention would in
fact enhance the functionality of the above patent by providing
an active substrate consisting of piezoelectric columns within a
polymer composite capable of operating at lower voltages.

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SUMMARY OF THE INVENTION

7 In accordance with one aspect of this invention, there is provided a piezoelectric substrate having three or more odd 8 9 numbers of stacked piezoelectric regions that could bused to 10 construct an array of transducers. Upper and lower contacts are 11 disposed on the end of a stack of piezoelectric regions and 12 intermediate contacts are disposed between the regions. The 13 upper contact is electrically joined by a first trace to a first 14 intermediate contact between the second and third piezoelectric 15 The lower contact is electrically joined by a second regions. 16 trace to a second intermediate contact between the first and 17 second piezoelectric regions. Insulating material is positioned 18 between the first and second trace and the piezoelectric regions. 19 The upper and lower contacts are disposed over the ends of a 20 plurality of piezoelectric stacks or the upper and lower contacts 21 can be segmented for individually addressing the stacks. The 22 insulating material insulates piezoelectric columns from each 23 other.

BRIEF DESCRIPTION OF THE DRAWINGS

2	The appended claims particularly point out and distinctly			
3	claim the subject matter of this invention. The various objects,			
4	advantages and novel features of this invention will be more			
5	fully apparent from a reading of the following detailed			
6	description in conjunction with the accompanying drawings in			
7	which like reference numerals refer to like parts, and in which:			
8	FIG. 1 is a top view of a single piezoelectric ceramic rod;			
9	FIG. 1A is a cross sectional view of the piezoelectric			
10	ceramic rod of FIG. 1 taken along section line A-A;			
11	FIG. 2 is a side view of a single rod;			
12	FIG. 3 is a two dimensional arrangement of rods sharing			
13	common electrodes;			
14	FIG. 4 is a two dimensional arrangement of rods having			
15	independent electrodes that can form an array of transducer			
16	elements; and			
17 [.]	FIG. 5 is a diagram showing layered deposition of the			
18				
	elements used to make this invention.			
19	elements used to make this invention.			
19 20	elements used to make this invention. DESCRIPTION OF THE PREFERRED EMBODIMENT			
20	DESCRIPTION OF THE PREFERRED EMBODIMENT			
20 21	DESCRIPTION OF THE PREFERRED EMBODIMENT FIG. 1 shows the top view of a single co-fired piezoceramic			
20 21 22	DESCRIPTION OF THE PREFERRED EMBODIMENT FIG. 1 shows the top view of a single co-fired piezoceramic pillar 10, in this case a rod of square cross-section. A cross-			

1 the structure has three active piezoelectric ceramic layers 12A, 12B, and 12C with four conductive electrodes 14A, 14B, 14C and 2 14D addressing the three piezoelectric ceramic layers 12A, 12B, 3 4 and 12C. Piezoelectric ceramic layers 12A, 12B, and 12C can be 5 constructed from typical ferroelectric materials such as lead 6 zirconate titanate or lead titanate. A top electrode 14A is positioned on the upper surface of pillar 10. Top electrode 14A 7 8 is in communication with lower intermediate electrode 14C via first trace 16A. A bottom electrode 14D is positioned on the 9 10 bottom surface of pillar 10.

Pillar 10 is polarized so that an electrode having a 11 12 positive polarity is in contact with a positively polarized 13 portion of pillar 10. For example, if top electrode 14A is 14 positive then the top surface of ceramic layer 12A is positively 15 polarized, and the bottom surface of ceramic layer 12A is 16 negatively polarized where it is in contact with top intermediate 17 electrode 14B. The bottom electrode 14D would then have a 18 negative polarity. Ceramic layer 12C bottom surface is 19 negatively polarized where it contacts bottom electrode 14D. 20 Ceramic layer 12C top surface is positively polarized where it 21 contacts lower intermediate electrode 14C because electrode 14C 22 has a positive polarity. Intermediate ceramic layer 12B has a 23 top surface that is negatively polarized and in contact with upper intermediate electrode 14B. Bottom surface of ceramic 24 25 layer 12B is positively polarized and in contact with electrode

14C. Thus, polarized ceramic regions should be in contact with
electrodes having a like polarization.

FIG. 2 provides a side view of pillar 10 showing top 3 4 electrode 14A, trace 16A and bottom electrode 14D. Bottom 5 electrode 14D is in communication with upper intermediate 6 electrode 14B via second trace 16B. An electrical insulator 7 material 18 is used to isolate traces 16A and 16B from the pillar 8 10. Electrical insulation between the traces and the pillar 10 9 prevents leakage of currents across the individual ceramic 10 layers. Thus, top electrode 14A and lower intermediate electrode 11 14C can be associated with one electrical pole, and bottom 12 electrode 14D and upper intermediate electrode 14B can be 13 associated with the other electrical pole. Electrodes 14A, 14B, 14 14C, and 14D and traces 16A and 16B can be made from any 15 electrically conductive material. It is envisioned that top 16 electrode 14A and bottom electrode 14D are formed from continuous 17 depositions of conductive material so that one top electrode or 18 bottom electrode can contact a multiplicity of ceramic layers 12A 19 and 12C, and a multiplicity of traces 16A and 16B respectively 20 forming a multiplicity of co-fired assemblies.

As arranged above, top electrode 14A and upper intermediate electrode 14B are in electrical contact with active ceramic layer 12A. In a passive mode, compression of active ceramic layer 12A results in generation of a differential voltage between electrode 14A and electrode 14B. In an active mode, application of a

differential voltage across ceramic layer 12A results in movement of this layer. In the same manner, active ceramic layer 12B is joined for communication with electrodes 14B and 14C, and active ceramic layer 12C is joined for communication with electrodes 14C and 14D. Because more electrodes are provided, a lower voltage applied between 14A and 14D can give the same displacement of pillar 10.

8 FIG. 3 shows a panel 20 having a plurality of pillars 10 9 arranged over a planar surface. Pillars 10 are supported in 10 panel 20 by insulating material 18. Insulating material 18 can 11 be a dielectric polymer matrix or an elastomeric material. In 12 this embodiment, top and bottom electrodes 14A and 14D are 13 extended over the upper and lower surfaces of the entire panel 14 A plurality of first traces 16A make contact with top 20. 15 electrode 14A, and a plurality of second traces 16B make contact 16 with bottom electrode 14D. As above, each first trace 16A is in 17 contact with one lower intermediate electrode 14C. Each second 18 trace 16B is in contact with one upper intermediate electrode 19 14B. While the panel shown here has two traces 16A and 16B for 20 each pillar 10, it is understood that each trace 16A and 16B can 21 be in communication with multiple electrodes in multiple pillars 22 10. In FIG. 3, pillars 10 are shown arranged in offset rows; 23 however, other patterns of arrangement are possible for efficient 24 utilization of the space.

1 An alternative embodiment of the invention is shown in FIG. Panel 20' has a top electrode 22A and a bottom electrode 22B 2 4. associated with each pillar 10. As above, top electrode 22A is 3 joined to a first trace 16A which electrically connects top 4 electrode 22A with one lower intermediate electrode 14C. Bottom 5 6 electrode 22B is electrically joined to upper intermediate 7 electrode 14B via second trace 16B. This arrangement allows 8 independent addressing of the pillars 10. In view of these two 9 embodiments any number of groups of pillars can be independently 10 addressed.

Panels 20 and 20' can be manufactured by the fused deposition of ceramics (FDC) method as shown in FIG. 5. Utilizing this method hundreds of columns can be generated in two orthogonal directions. The example shown above is a composite with 1-3 connectivity (rods in two directions), but the method could also be used to fashion a composite with 2-2 connectivity (plates in one direction).

18 The FDC method utilizes a numerically controlled multi-19 nozzle 30 head in communication with reservoirs 32A, 32B, 32C and 20 32D of various thixotropic materials of interest as shown in FIG. 21 4. Nozzle 30 can precisely dispense these materials over a two-22 dimensional grid 34. Materials can include green ceramic, 23 metallic compounds, and other polymers. The build-up over 24 multiple layers is accomplished by lowering the two-dimensional 25 grid 34 and depositing layer 36 upon layer 36 to create a

multiple layer pre-form 38. This pre-form 38 will typically
include the piezoceramic layers 12A, 12B and 12C; the
intermediate electrodes 14B and 14C; insulating material 18 and
the traces 16A and 16B for a plurality of pillars 10.

Once deposition of the pre-form 38 is complete the pre-form 5 6 38 is subjected to a low temperature burn out to remove the plasticizer in the sprayed material. Pre-form 38 is then fired 7 to sinter the ceramic particles. The pre-form 38 may be back-8 filled with a polymer to hold the pillars together while 9 10 mechanically decoupling the piezoceramic pillars 10 from each 11 other. This can be the same insulating material as insulating 12 material 18 or a different insulating material. The top and 13 bottom electrodes 14A and 14D can the be applied to the outside 14 of the finished composite substrate. The pillars 10 are 15 polarized by a number of methods dependent upon the piezoelectric 16 material utilized.

17 An alternative approach, quasi-multi-layering, involves 18 applying conductive stripes around the pillars. This is similar 19 to conventional striped ceramic cylinders. The realization of 20 this method would be complicated and perhaps not as cost 21 effective as the disclosed method. Additionally, the field 22 impressed on the surface doesn't couple completely to the 23 internal volume of the active material.

In view of the above detailed description, it is anticipated
that the invention herein will have far reaching applications
other than those described herein.

This invention has been disclosed in terms of certain embodiments. It will be apparent that many modifications can be made to the disclosed apparatus without departing from the invention. Therefore, it is the intent of the appended claims to cover all such variations and modifications as come within the true spirit and scope of this invention.

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3 LOW VOLTAGE PIEZOELECTRIC COMPOSITE FOR TRANSDUCER APPLICATIONS

ABSTRACT OF THE DISCLOSURE

6 A piezoelectric ceramic polymer composite is provided with 7 piezoelectric ceramic pillars having intermediate electrodes. 8 These intermediate electrodes reduce the voltage necessary to 9 achieve a given polarizing electric field within the 10 piezoelectric ceramic pillars. Upper and lower electrodes are 11 provided on the surfaces of the composite substrate. These electrodes are electrically joined to the intermediate electrodes 12 13 by insulated electrical traces. The piezoelectric ceramic phase 14 geometry may include either 1-3 (rods) or 2-2 (bars) 15 connectivity. The number of electrode pairs is limited only by 16 the fabrication process. The lateral distribution of these 17 piezoelectric pillars is decoupled using a polymer backfill 18 material. Upper and lower electrodes can be partitioned to form 19 an array of transducer elements.

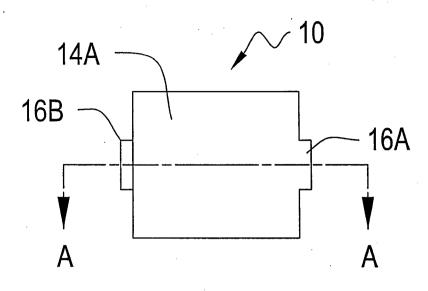


FIG. 1

