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(15 January 1979)

PTPT REPORT NO. 79-1
AFPEA PROJECT NO. 77-P7-43

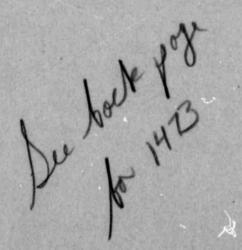
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DO CONTRACTOR OF CONTRACTOR OF

EVALUATION OF AN "ISOPOD"

REUSABLE SHIPPING CONTAINER FOR THE F-16

FIRE CONTROL RADAR SYSTEM COMPONENTS

HQ AFALD/PTP
AIR FORCE PACKAGING EVALUATION AGENCY
Wright-Patterson AFB 0H 45433

January 1979

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ABSTRACT

The evaluation of the Hughes Standard "Isopod" reusable container revealed that this container will adequately protect the F-16 Fire Control Radar System during rough handling situations encountered in shipment. The maximum shock level recorded during the evaluation was 12 Gs. Field test data of a shipment of the actual radar system components are included in this report.

This Agency obtained 18 surplus "Isopod" containers and incorporated the necessary restraining brackets and hardware to reduce the damage potential to the radar components during the loading and unloading sequence. These containers will be available, as government furnished equipment, to the manufacturer of the radar system for shipment of production installs.

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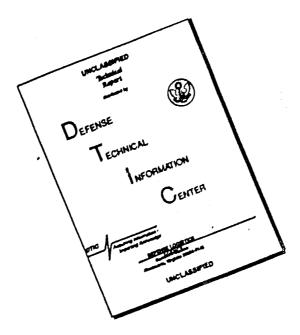
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Acknowledgements

The following AFPEA personnel are acknowledged for their contribution toward the success of this project:

Capt Joseph J. Beradino

James D. Heck

Ronald Vantu

Ernest Vanzant

Robert Rosenkranz

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INTRODUCTION

Beginning in 1976, the Air Force Contract Management Division (AFCMD/PDT) and the Air Force Packaging Evaluation Agency (AFPEA) cooperated in a program to investigate the use of reusable containers for shipping the F-16 Fire Control Radar System components. The use of this container versus the existing wooden crates could result in an estimated cost savings of approximately \$600,000.

This Agency obtained 18 surplus Hughes Standard "Isopod" containers and initated a test program to evaluate this container. Early in the test program it was recognized that a damage potential existed for the radar antenna during the loading and unloading phase. This problem was eliminated by installing a slide/guide mechanism on the bottom shelf of the "Isopod".

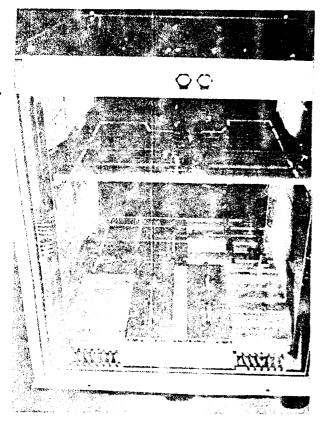
DESCRIPTION OF TEST PACK

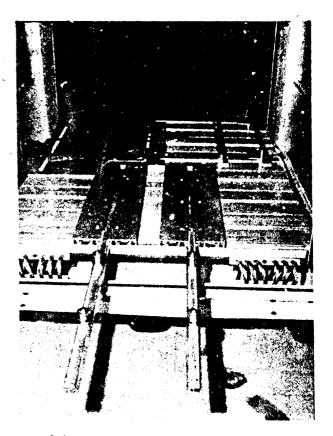
The Hughes Standard "Isopod" aluminum container (P/N K1012750, NSN 8145 00 180 5802) includes a molded plastic pailet which is bolted to the container base and an extruded aluminum shelf assembly which is isolated from the container shell with 8 "Aeroflex" helical shock mounts. Soft vinyl-rubber pads are bonded to the shelf surface and will compress when an item is strapped in place. A desiccant compartment and humidity indicators, with controlled breathing valves, are included with the Standard "Isopod". The two weather sealed access doors are secured with 6 latching devices per door. The container was designed for a load range of 100 to 350 pounds and a shock protection level of 20 Gs. Two models were tested and each was identical in construction except for the height, weight and capacity. The majority of the tests were conducted with the 48 inch high container. A comparison of the two models is shown in Table I.

Mode1	Dimensions	Tare	Cargo
Number		Weight	Capacity
	(Inches)	(Lbs)	(Ft. ³)
K1012750	48 X 40 X 48	210	26.5
K1102234	48 X 40 X 60	263	35.5

Table I. Model Comparison Information

A modified container is shown in figure 1. The slide rail guide assembly is required to prevent damage to the delicate antenna surface when the antenna is placed on the container shelf. A special bracket assembly (right rear), for the transmitter, was used in place of the strap assemblies to secure the item to the lower shelf. The tension on the strap could damage the thin dust cover on the top front surface of the transmitter.





(a) Modified Shelf Assembly

(b) Antenna Rails Extended

Figure 1. Modified Standard Isopod

TEST INSTRUMENT, TION AND EQUIPMENT-

The following instrumentation and equipment were employed during this evaluation:

Instrumentation:

- 1. Oscilloscope, 4 channel storage, Tektronix Model 564-B
- 2. Accelerometer, tri-axial, Endevco Model 2233E
- 3. Amplifier (3 ea.), Endevco Model 2614C
- 4. Power Supply, Endevco Model 2622C
- 5. Transportation Environment Recorder, Bolt-Beranek and Newman, Models 711 and 714

iquipment:

- 1. Vibration Test Machine, (mechanical) L.A.B. Corp., Type 5000-96B
- 2. Vibration Fest Machine, (mechanical) L.A.B. Corp., Model 41012

- 3. Low-Temperature Test Chamber, Tenny Engineering, Inc.
- 4. Environmental Rain Chamber, Harshaw Chemical Company
- 5. Chain Hoist, electrical

TEST PROCEDURES AND RESULTS

All of the tests, except as noted, were conducted in accordance with Federal Test Method Standard 101B. Tri-axial and single accelerometers were secured to the simulated models of the radar components and to the shelf sections of the isolation system. One phase of the testing included the installation of a tri-axial accelerometer at the center of gravity of the simulated computer component. Figure 2 shows the locations of the simulated components.



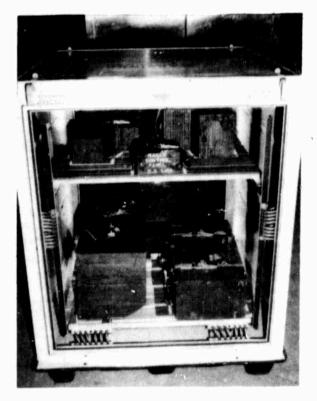


Figure 2. Simulated Models of the Radar Components

The location of each item was carefully selected to provide the proper center of balance for the test pack.

Repetitive Vibration Test - Method 5019

During the initial vibration test the lower angle brackets, which support the lower shelf assembly, fractured and prevented the completion of the tests. The Hughes Company was contacted and informed of this failure. They were aware of the problem and informed this Agency that the later models of the Standard "Isopod" included the redesigned shelf angle brackets which were later supplied to this agency for the replacement

of the defective brackets. The 18 surplus "Isopods" were inspected and the lower shelf angle brackets were replaced as required.

To insure that the redesigned bracket would support the test load, a 4 hour repetitive vibration test was substituted for the standard 2 hour test.

After the antenna and transmitter restraining devices were installed an additional 2 hour vibration test was performed to determine if the mounting integrity could be maintained. The vibration data for each of the two test models are presented in Table II.

Test Pack Model Number	Antenna & Transmitter Mounts		Frequency	Response Acceleration (Peak to Peak)
	with	without	HZ	G
K1012750	Х	-	4.8	5.0
K112234	_	Х	4.2	4.2

Table II. Repetitive Vibration Test Data

Resonant Frequency and Transmissibility

To insure that the Aeroflex helical shock isolators would not weaken or become distorted, a one hour vibration test was substituted for the normal 15 minute test. The test pack was rigidly secured to the vibration table and vibrated at the resonant frequency of the test pack. Both light and heavy load data is included in Table III.

Model Number	Test Load Weight	.Resonant Frequency	Acceleration - G (Peak to Peak)		Transmissibility Factor
	(Lbs)	нг	Table	Test Load	
K1012750	107	. 14	2	9.5	4.75
	263	7.5	2	5.0	2.50

Table III. Resonant Frequency & Transmissibility Data

Pendulum Impact Test - Method 5012

The maximum peak acceleration recorded on the four impacted surfaces of each test pack was 10.2 Gs.

Edgewise Rotational Drop Test - Method 5008

Each test pack was subjected to method 5008 tests with the exception of paragraph 6.1. The greatest attainable height was substituted for the recommended 36 inch height. An unstable condition existed above the heights listed in Table IV.

del	Drop Height	Impact Edge	Peak Acceler	ration - G
[Mode]	(In)		Ambient	-40°F
K1012750	30	2-3	11.0	12.2
27	30	4-3	12.0	10.6
01	24	5-3	9.0	9.2
K	24	6-3	10.0	8.0
34	20	2-3	9.7	_
22	20	4-3	8.4	_
K1102234	20	5-3	9.4	-
KI	20	6-3	10.0	-

Table IV. Drop Test Data

Additional edgewise drop test data was obtained for the light (107 lbs.) load. This data is shown in Table V.

Model No.	D rop Height	Impact Edge	Acc	celera	ation	- G	Duration
Mo	(In)		Х	Y	Z	R	msec
50	30	2-3	17	4	10	20.1	35
27	30	4-3	4	4	18	18.9	50
010	24	5-3	12	8	20	24.7	40
K Z	24	6-3	10	10	15	20.6	50

Table V. Additional Drop Test Data (107 lb load)

Wind Driven Rain Test, MIL-STD-810C, Method 506.1

The 48 inch high test pack was exposed to a two hour, 40 MPH, wind driven rain test. The inspection revealed that no water or condensation was present inside the container.

Field Tests

Two separate field tests were conducted with the Standard "Isopod". The first shipment was made September 1977 with the simulated models of the radar components and the second shipment of the actual radar components occurred in September 1978.

Shipment 1: Truck transportation was used for this shipment from Baltimore, Maryland to Fort Worth, Texas. A Transportation Environment Recorder (TER) was used to monitor the test load environment. The non-resultant TER will only record the individual shock inputs from three mutually perpendicular accelerometers and; therefore, the unknown resultant value will be slightly higher. This data is presented in Table VI.

Shock Level	Nu	Elapsed		
Range	Shoo	ks Reco	orded	Time
(Gs)	X	Y	Z	(Days)
2.5 - 5.0	18	7	*	7.2

* Accelerometer inoperative
Temperature range: 50 - 100°F (80 - 90° for 2.2 days)
Humidity range: 30-60% (50-60% for 2.4 days)

Table VI. Field Test Data, Shipment 1

Shipment 2: Field test number 2 consisted of two containers with the actual radar components as shown in figure 3. For security reasons the Low Power RF component is not shown. The Transportation Environment Recorder is shown on the right side of the antenna. The radar systems were shipped from Baltimore MD via commercial air, to Fort Worth TX. The two "Isopods" were later transferred to a military aircraft





Figure 3. F-16 Radar Components

for the final flight to Europe. One system, instrumented with the TER, was delivered to Belgium and the second system, instrumented with "Impact-O-Graph" indicaters was delivered to the Netherlands. The TER data is listed in Table VII. The resultant type TER records individual shock inputs in three mutually perpendicular axes (X, Y, Z) and immediately computes and records the resultant value of the X, Y and Z components.

Shock Level	Numb	er of Shocks	Recorded	Resultant	Elapsed
Range	X	Y	Z		Time
(Gs)	Sides	Front-Back	Top-Bot.		(Days)
2.5 - 5.0	. 1	0	. 7	33	23

Table VII. Field Test Data, Shipment 2

The larger number of shocks recorded as resultants are due to shock and vibration inputs whose individual X, Y & Z components are below the recorders "threshold" setting of 2.5 G and, therefore, not recorded in the X, Y & Z channels. However, when these low level components are combined, the resultant value is above the 2.5 G "threshold" and, therefore, is recorded.

The two "Impact-O-Graph" shock indicators used in monitoring the shipment to the Netherlands were not activated which indicated that the "Isopod" isolation system did not receive a shock input above 15 Gs. The two indicators (15 & 25 G) were calibrated in the laboratory prior to installation in the "Isopod".

The low shock level values experienced during these tests were expected since the rough handling tests produced a maximum of 12 Gs.

DISCUSSION

The test load positions and the condition of the Aeroflex shock isolators were monitored during all phases of the rough handling tests. No damage occurred to either the test load, the container or the shock mounts. Some separation (1/16 to 1/8 inch) occurred between the strands of cable which formed the helical coils of the lower shock mounts. This separation appeared to be a normal characteristic of the coil and did not affect the performance of the isolation system.

The inspection of the surplus containers which were not tested revealed that the welded joint, which frames the access door openings, had small cracks on some of the corners. Since this type of fracture did not occur on any of the test models it is suspected that they were caused by improper latching of the door locking mechanism. If the door is not properly inserted into the framed opening and the locking mechanism strikes the outer edge, the forces generated by the lever arm could shear the pin on the lock or force the frame to separate if continued abuse occurred. This crack would not be serious unless it propagated beyond the door seal. If so, water could enter the container. Rewelding was required to correct this problem which existed on only one of the 18 "Isopods".

The inspection also revealed that one of the containers was punctured with a fork lift truck. This hole was repaired by welding.

Additional details of the rough handling tests are provided in AFPEA Interim Reports no. T-77-34 and 78-8.

CONCLUSIONS

- 1. The Standard "Isopod" will provide adequate protection for the F-16 Fire Control Radar System which has a fragility rating of 25 Gs.
- 2. The Aeroflex helical shock mounts are not effected by rough handling tests including drop tests at -40° F.
- 3. The antenna rail/guide assembly and the transmitter attachment bracket assembly is adequate for securing these items to the "Isopod" shelf assembly.

RECOMMENDATIONS

- 1. The contractor responsible for the packaging of the F-16 Fire Control Radar System should be required to use the modified surplus "Isopods" for the production installs. Three of the 18 "Isopods" are in the possession of the Air Force Plant Representative Office (AFPRO) at the packaging site and the remaining 15 containers are available immediately upon request. The estimated value of these modified GFE containers is approximately \$50,000. The use of these reusable containers in place of the wooden crates now used by the contractor would result in estimated cost savings of \$600,000 for the factory install shipping program.
- 2. The four corners of each access door frame should be reinforced on all future models of this container to prevent cracks in the weld of the corner joint.

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