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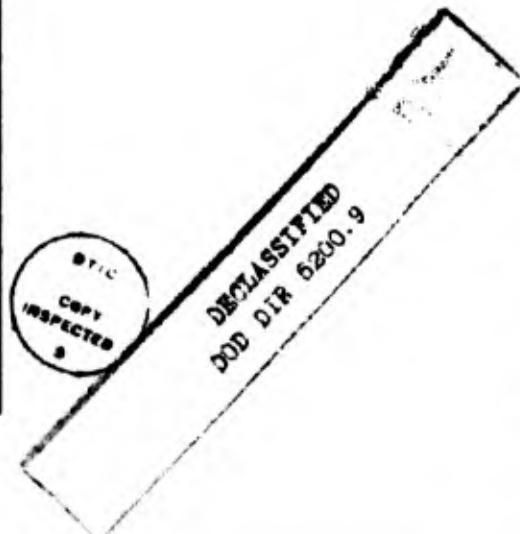
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REPORT NO. 130/43

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BALLISTIC PROPERTIES  
OF AN  
AIR HARDENING STEEL

WATER TOWN

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TITLED AS FOLLOWS:  
"BALLISTIC PROPERTIES OF AN  
AIR HARDENING STEEL",  
BY R. L. REED, WATERTOWN, MASS.

R. L. Reed

January 1936

WATERTOWN ARSENAL  
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Report No. 710/47  
Watertown Arsenal

January 6, 1936

BALLISTIC PROPERTIES  
OF AN  
AIR HARDENING STEEL

UNCLASSIFIED

Purpose

The purpose of this investigation was to determine the ballistic properties of an air hardening armor plate composition proposed for the casting of the experimental tank turret, L-31-23462.

Conclusions

1. The resistance of the castings was in excess of the requirements of Par. O-5 Special Specifications for steel castings, dated July 25, 1935.
2. The ballistic properties of this particular cast steel were slightly less than the requirements for rolled plate of the same thickness.
3. The areas subjected to ballistic test demonstrated toughness and ductility.
4. Good ballistic properties were obtained on castings with a Brinell hardness of 364.

Experimental Procedure

An air hardening steel of the following chemical composition and physical properties was selected for test.

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Chemical Composition

<u>C %</u>	<u>Mn %</u>	<u>P %</u>	<u>S %</u>	<u>Si %</u>
.35/.45	.40/.70	<.02	<.02	.15/.25
<u>Ni %</u>	<u>Cr %</u>	<u>Mo %</u>	<u>Va %</u>	
2.40/2.60	1.10/1.30	.60/.80	.20/.30	

Physical Properties  
(Heat Treated forged bars)

<u>Y.S./.00% Set lb/sc. in.</u>	<u>Tensile Strength lbs/sc. in.</u>	<u>True Breaking Strength lbs/sc. in.</u>
175,000	199,500	271,000
<u>Elongation % in 2 in.</u>	<u>Reduction of Area %</u>	<u>Charpy Tension Impact Ft/lbs</u>
11.4	41.9	323

Four generator covers of this composition were cast from Heat 995 and radiographed, heat treated and subjected to a ballistic test.

Results of Test

1. Radiographic Examination. No pronounced casting defects were revealed by X-Ray examination.

2. Heat Treatment. The castings were heat treated as follows:

Heat 8 hours at  $1150^{\circ}\text{C}$ , transfer to furnace preheated to  $850^{\circ}\text{C}$ , furnace cool. Reheat to  $950^{\circ}\text{C}$  for

5 hours, furnace cool. Reheat to 825°C for 5 hours, furnace cool. Heat 2 hours at 785°C, air quench. Draw 2 hours at 800°F, air cool.

3. Chemical analysis. Chemical analysis of Heat 995 is given below:

C %	Mn %	P %	S %	Si %	Ni %	Cr %	Mo %	Va %
.45	.57	.007	.015	.22	2.55	1.19	.66	.27

4. Brinell Hardness. The Brinell hardness of the heat treated castings is as follows:

<u>Casting No.</u>	<u>Brinell Hardness</u>
1	418
2	364
3	364
4	364

Ballistic Tests. Ballistic tests of each casting are given in detail on Pages 3, 4, 5 and 6.

#### GENERATOR COVER NO. 1

Actual Thickness - 1/2" - Top of crown

Brinell Hardness 418

Range to plate 100 yards

Bullet-Caliber .30 M1922 A.P. 165 gr. Core 87.5 gr.

Rd	Str	AxS-54 Rev 2	Location	Dia of Hole	Height of bulge	Depth of penetration
No	Vel f/s	Penetration	of Shot	Back	back	
1	1900	Partial	Top of Crown	--	Slight	---
2	1900	"	" "	--	Slight	---
3	1900	Complete	" "	--	---	---
4	1900	"	" "	--	---	---

GENERATOR COVER NO. 2

Actual Thickness - 9/16" - Top of crown

Brinell Hardness - 364

Range to plate 100 yards

Bullet-Caliber .30M 1922 AP 165 gr. Core 87.5 gr.

Rd	Str	AxS-54 Rev 2	Location of Penetration	Dia of Shot	Height Back	Hole of bulge back	Depth of Penetra- tion
No	Vel						
1	1900	Partial	Top of crown		--		.42"
2	"	Partial Pun- ching Started	" " "		1/8"		.5"
3	"	Glanced	rim		--		---
4	"	"	"		Slight		---
5	"	"	"		"		---
6	"	Partial	Top of crown		"		.45"
7	2000	"	" " "		"		.42"
8	2100	"	" " "		"		.5"
9	2200	Partial Pun- ching Started	" " "		"		.41"

GENERATOR COVER NO. 3

Actual Thickness - 9/16" - Top of Crown

Brinell Hardness - 364

Range to plate - 100 yards

Bullet - Caliber .30 M 1922 AP 165 gr. Core 87.5 gr.

Rd No	Vel f/s	AxS-54 Rev. 2	Location of Penetration	Dia of hole back	Height of bulge back	Depth of Penet- tration
			Shot			
1	1900	Partial	Top of crown	---	---	.42"
2	"	"	" " "	---	---	.34"
3	"	"	" " "	---	---	.38"
4	"	Glanced	rim	---	---	---
5	"	Partial	Top of crown	---	Slight	.43"
6	2000	"	" " "	---	"	.46"
7	2100	"	" " "	---	"	.41"
8	2200	"	" " "	---	"	.44"
9	2300	"	" " "	---	"	.5"
10	Service	Partial Punching Started	" "	---	1/16"	.43"
11	Service	"	" " "	---	1/16"	.59"

GENERATOR COVER NO. 4

Actual Thickness - 1/2" - Top of Crown

Brinell Hardness - 364

Range to plate - 100 yards

Bullet - Caliber .30 " 1922 A.P. 165 gr. Core 87.5 gr.

Rd No	Str Vel f/s	AxS-54 Rev. 2 Penetration	Location of Shot	Dia of hole back	Height of bulge back	Depth of Pene- tration
1	1900	Partial	Top of Crown	--	--	.42"
2	"	"	" "	--	--	.46"
3	"	Glanced	Rim	--	--	---
4	"	Yaw C.I.P.	Top of Crown	--	--	---
5	2000	Partial	" "	--	slight	.51"
6	2100	"	" "	--	slight	.48"
7	2200	Complete	" "	--	--	---

### Discussion

The castings made of the air hardening composition demonstrated ductility and toughness when subjected to ballistic tests.

The resistance of the castings was slightly lower than the requirements for rolled plate of the same thickness.

The Brinell Hardness of three of the generator covers, Nos. 2,3, and 4 was 364 and on the other hand these castings had relatively good ballistic properties.

The ballistic properties of Cover No. 1 which had a Brinell hardness of 418 were not superior to covers 2,3, and 4.

An increase in thickness of the casting over the specifications was responsible for high resistance as noted in Covers Nos. 2 and 3.

Photographs of Casting Nos. 2,3, and 4 after ballistic test are shown in Figs. 1, 1A, 2, 2A, 3 and 3A.

### Recommendations

It is recommended that an air hardening steel of the following chemical composition be used in the

manufacture of the experimental tank turret.

<u>C %</u>	<u>Mn %</u>	<u>P %</u>	<u>S %</u>	<u>Si %</u>
.35/.45	.40/.70	<.02	<.02	.15/.25

<u>Ni %</u>	<u>Cr %</u>	<u>Mo %</u>	<u>Va %</u>
2.40/2.60	1.10/1.30	.60/.80	.20/.30

Respectfully submitted,

E. L. Reed,  
Research Metallurgist.

References:

- W. A. Report 115/1
- W. A. Report 115/24
- W. A. Report 115/29
- W. A. Report 115/30

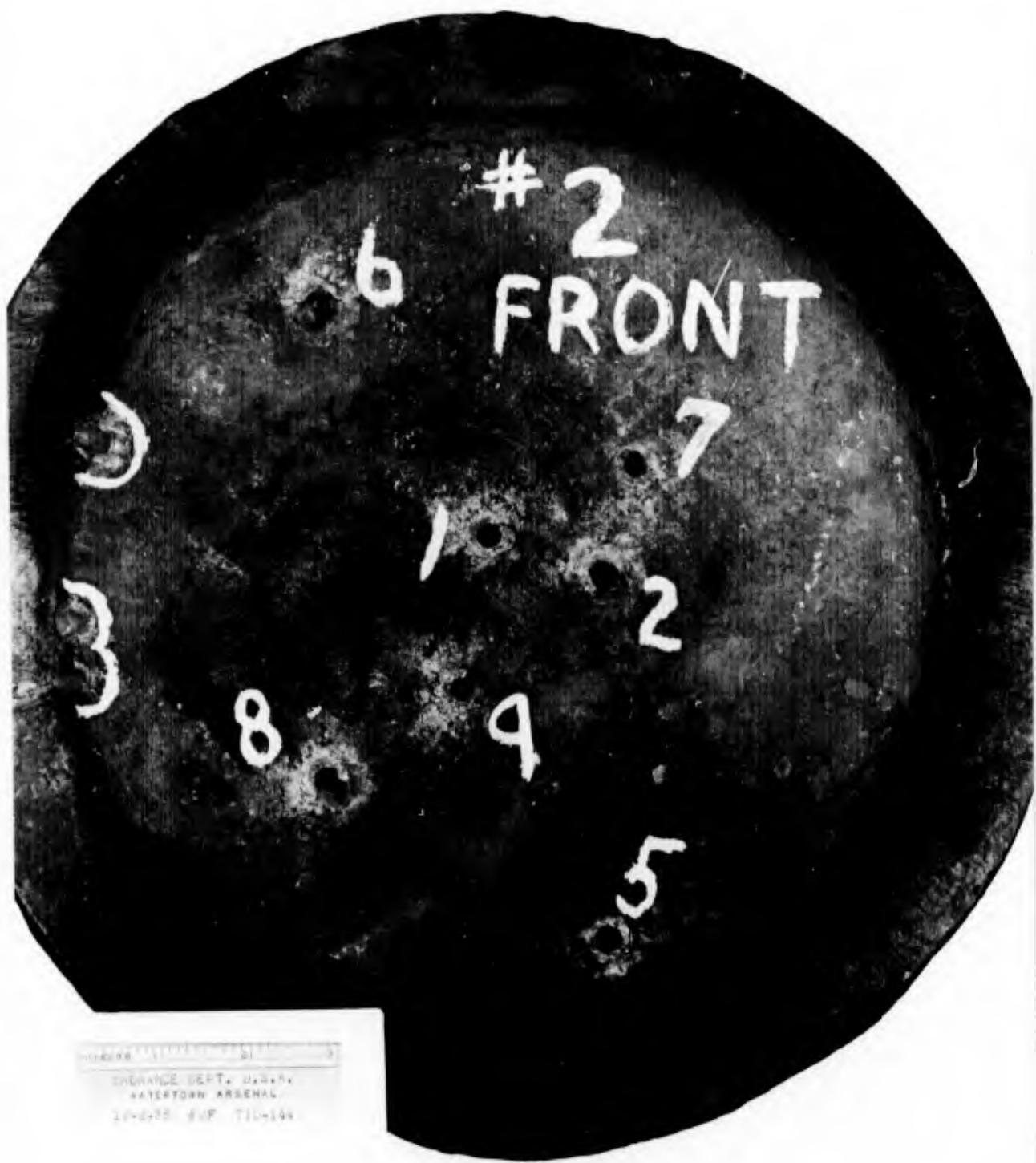


Fig. 1.

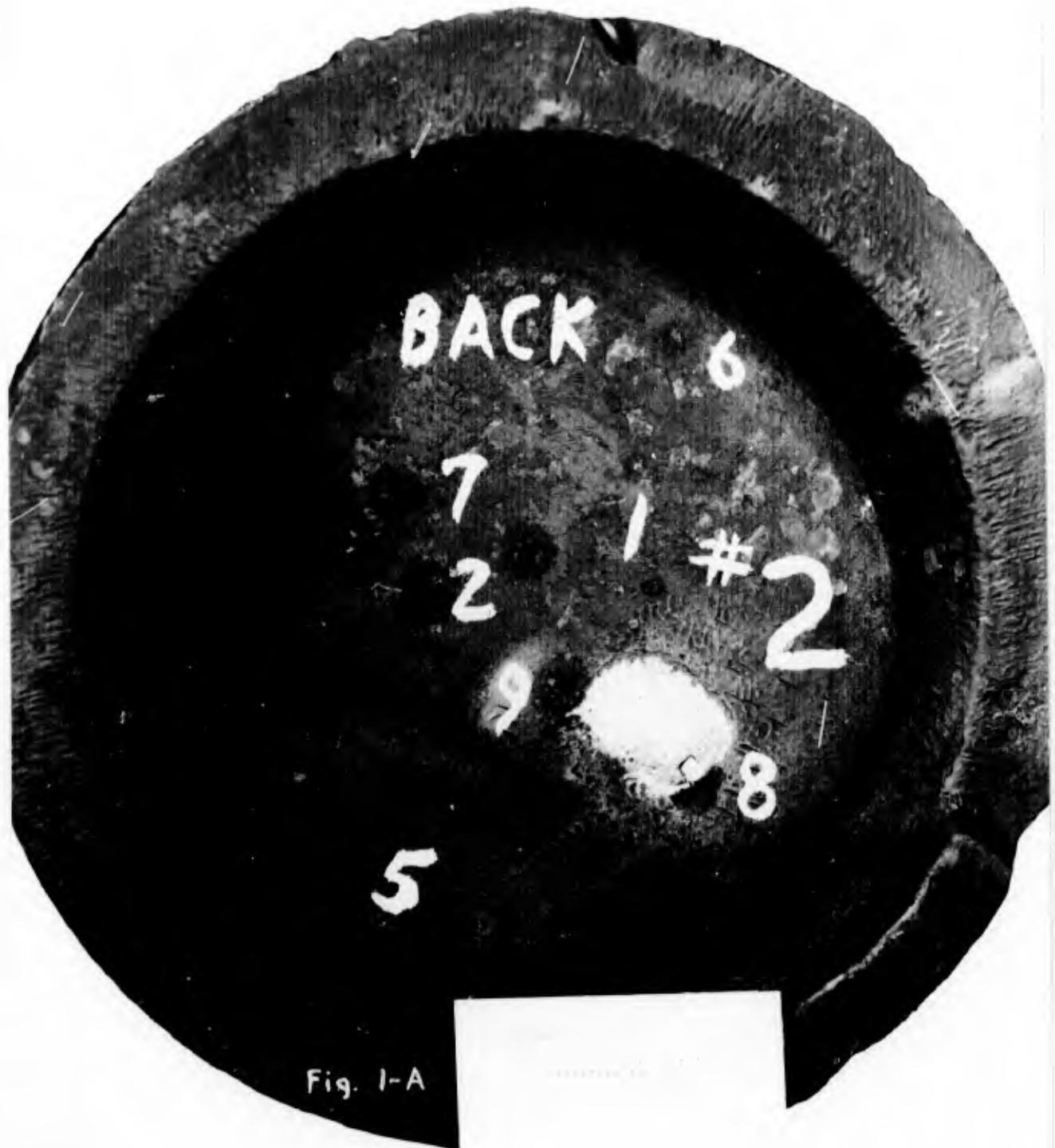


Fig. I-A



Fig. 2.



Fig. 2-A.



Fig. 3-



Fig. 3A