

REPORT DOCUMENTATION PAGE				Form Approved OMB No. 0704-0188	
Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing this collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden to Department of Defense, Washington Headquarters Services, Directorate for Information Operations and Reports (0704-0188), 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to any penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number. PLEASE DO NOT RETURN YOUR FORM TO THE ABOVE ADDRESS.					
1. REPORT DATE (DD-MM-YYYY) 30-11-2012		2. REPORT TYPE Research Report		3. DATES COVERED (From - To) 05-01-2011 to 30-11-2012	
4. TITLE AND SUBTITLE Altitude Dependence of Rocket Motor Performance				5a. CONTRACT NUMBER	
				5b. GRANT NUMBER	
				5c. PROGRAM ELEMENT NUMBER	
6. AUTHOR(S) KIMBERLY ALBANESE, MARY MEYERS, KASSANDRA PRUSKO, AND MICHAEL COURTNEY				5d. PROJECT NUMBER	
				5e. TASK NUMBER	
				5f. WORK UNIT NUMBER	
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) DFRL U.S. Air Force Academy 2354 Fairchild Drive USAF Academy, CO 80840				8. PERFORMING ORGANIZATION REPORT NUMBER	
9. SPONSORING / MONITORING AGENCY NAME(S) AND ADDRESS(ES)				10. SPONSOR/MONITOR'S ACRONYM(S)	
				11. SPONSOR/MONITOR'S REPORT NUMBER(S)	
12. DISTRIBUTION / AVAILABILITY STATEMENT Approved for public release; distribution unlimited					
13. SUPPLEMENTARY NOTES					
14. ABSTRACT It is well known that rocket motors produce greater thrust at higher altitudes due to the lower ambient pressure. A simple formula predicts that the thrust increase will be equal to the decrease in ambient pressure times the cross sectional area of the throat of the nozzle. This paper provides experimental tests of predicted increases in impulse based on this simple formula. The experimental method employed 20 trials with each of three solid fuel hobbyist rocket motors: Estes A10-PT, Estes D5- P and Quest D11-0P. Thrust curves were measured with a force plate for ten trials with each motor at two different altitudes corresponding to ambient pressures of 22.80 in Hg and 29.84 in Hg. Resulting impulses and specific impulses were then computed for each trial and the differences in average impulse and specific impulse were then compared with the predictions using the simple model that predicts thrust dependence on ambient pressure. Although thrust increases were measured in each case of reduced ambient pressure, the gains in impulse were not in agreement with predictions of the simple formula in every case.					
15. SUBJECT TERMS Rocket motor, impulse, specific impulse, thrust, altitude, ambient pressure					
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT Same as Report (SAR)	18. NUMBER OF PAGES 8	19a. NAME OF RESPONSIBLE PERSON Michael Courtney
a. REPORT unclassified	b. ABSTRACT unclassified	c. THIS PAGE unclassified			19b. TELEPHONE NUMBER (include area code) 719-333-8113

Altitude Dependence of Rocket Motor Performance

KIMBERLY ALBANESE, MARY MEYERS, KASSANDRA PRUSKO, AND MICHAEL COURTNEY

United States Air Force Academy,¹ 2354 Fairchild Drive, USAF Academy, CO, 80840

Michael.Courtney@usafa.edu

Abstract: It is well known that rocket motors produce greater thrust at higher altitudes due to the lower ambient pressure. A simple formula predicts that the thrust increase will be equal to the decrease in ambient pressure times the cross sectional area of the throat of the nozzle. This paper provides experimental tests of predicted increases in impulse based on this simple formula. The experimental method employed 20 trials with each of three solid fuel hobbyist rocket motors: Estes A10-PT, Estes D5-P and Quest D11-0P. Thrust curves were measured with a force plate for ten trials with each motor at two different altitudes corresponding to ambient pressures of 22.80 in Hg and 29.84 in Hg. Resulting impulses and specific impulses were then computed for each trial and the differences in average impulse and specific impulse were then compared with the predictions using the simple model that predicts thrust dependence on ambient pressure. Although thrust increases were measured in each case of reduced ambient pressure, the gains in impulse were not in agreement with predictions of the simple formula in every case.

Keywords: *rocket motor, thrust, impulse, specific impulse, ambient pressure*

Introduction

Performance of rocket motors can be quantified employing metrics based on the measured curve of thrust vs. time (Benson, 2008; Sutton and Biblarz, 2010). The area under the thrust curve is the impulse, and the impulse divided by the fuel mass is the specific impulse. The built up pressures inside the combustion chamber exit through a nozzle designed to increase pressure in the combustion chamber and lead to high velocity gases exiting the nozzle. Thrust is the force that propels the rocket (Benson, 2008). As a rocket is fired, the thrust is measured over the duration of the burn.

Relating the theoretical change of performance to change in ambient pressure requires consideration of the rocket thrust equation,

$$F = \frac{dm}{dt} v + (P_e - P_a) A, \text{ (Equation 1)}$$

where:

F = net rocket engine thrust (N),

dm/dt = mass flow rate of exhaust gas (kg/s),

v = exhaust gas velocity at nozzle exit (m/s),

P_e = exhaust gas pressure at nozzle exit (Pa),

P_a = external ambient pressure (also known as free stream pressure, Pa), and

A = cross-sectional area of nozzle exhaust exit (m²).

¹ Distribution A. Approved for public release. Distribution unlimited. The views expressed in this paper are those of the authors and do not necessarily represent those of the U.S. Air Force Academy, the U.S. Air Force, the Department of Defense, or the U.S. Government.

Altitude Dependence of Rocket Motor Performance

The change in thrust when firing the same rocket motor design at two different ambient pressures, P_h (higher pressure) and P_l (lower pressure) is then

$$\Delta F = (P_h - P_l) A \quad . \quad (\text{Equation 2})$$

Integrating over time gives the change in impulse,

$$\Delta I = \int \Delta F dt = (P_h - P_l) A t_{burn} \quad , \quad (\text{Equation 3})$$

where t_{burn} is the duration of the rocket firing. This paper presents the results of experimentally testing the predictions of equation 3 regarding the expected change in impulse and specific impulse with ambient pressure.

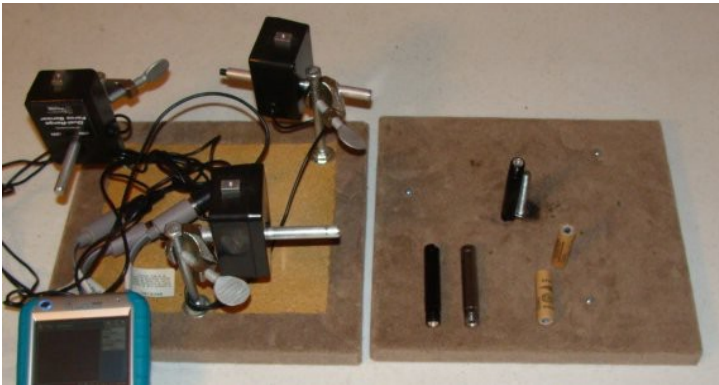


Figure 1: Force plate for measuring rocket engine thrust curves. The rocket motor is attached to the bolt extending out of the plate on the right which is set on top of the three force sensors on the left. (The photo shows one aluminum cased rocket motor attached to the bolt and two other aluminum cased motors in the lower left corner of the plate, as well as two brown paper cased Estes A10-PT rocket motors.)

Method

The experimental method employed 20 trials with each of three solid fuel hobbyist rocket motors: Estes A10-PT, Estes D5-P and Quest D11-0P. Thrust curves were measured with a force plate for ten trials with each motor at two different altitudes corresponding to ambient pressures of 77.878 kPa and 101.04 kPa. The thrust measurement system has been described in detail previously (Courtney and Courtney, 2009). The force plate employs three Vernier “dual-range force sensors” connected to a Vernier LabQuest. The three force sensors are attached to a bottom plate as shown in Figure 1, and a force plate rests on top of them and has a bolt to which the rocket engine is attached for static thrust testing. (The plate is held in place by gravity, there is no adhesive or connectors.) The total thrust is the sum of the three individual force readings. (The force plate is zeroed after the motor is attached.) Each force sensor has a selectable range of either 10N or 50N, so that if the plate was perfectly balanced, the full scale would be either 30N or 150N minus the static load, depending on the sensor setting. However, since the plate is not perfectly balanced, the three force readings are not equal, and the full scale ranges are closer to 20N and 100N for the 10N and 50N sensor settings, respectively. This system design is capable of measuring thrust curves for the full range (1/4A to E) of commonly available hobby rocket engines, as well as many experimental rocket motor designs.

Altitude Dependence of Rocket Motor Performance

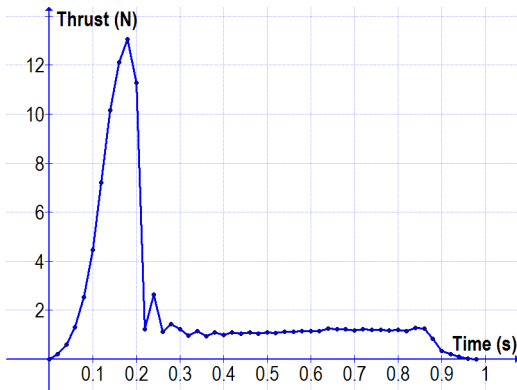


Figure 2: Thrust curve for Estes A10-PT Engine at low altitude (higher ambient pressure).

Figure 2 shows the measured thrust curve for an Estes A10-PT model rocket engine fired at low altitude. The shape of the thrust curve compares favorably with the published curve from the manufacturer. However, our experimental curve has a total impulse of 2.08 N s, compared with the manufacturer's claims of a total impulse of 2.5 N s. After the thrust curve is measured with the force plate, resulting impulses and specific impulses were then computed for each trial and the difference in average impulse and specific impulse were then compared with the predictions using the simple model that predicts thrust dependence on ambient pressure. Fuel masses were computed by weighing each motor before and after firing, with the fuel mass determined as the loss of mass during firing.

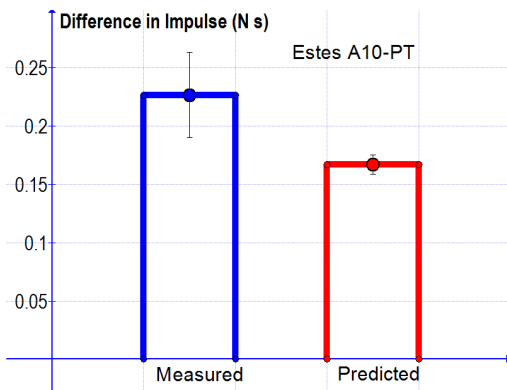


Figure 3: The measured and predicted differences between average impulses of the Estes A10-PT at high and low ambient pressures.

Results

Figure 3 compares the measured and predicted differences in average impulses for the Estes A10-PT at high and low ambient pressures. Equation 3 predicted that the mean impulse would be 0.167 ± 0.008 N s greater at the lower ambient pressure of higher altitude. The uncertainty in the prediction comes from combining uncertainties in the throat area, burn duration, and ambient pressures. However, the mean impulse at high altitude was 2.232 ± 0.029 N s, and the mean impulse at low altitude was 2.006 ± 0.022 N s, where the uncertainty is the standard error of the mean. This is a measured difference of 0.226 ± 0.037 N s. The predicted difference in impulse is in the right ballpark, but outside of the experimental uncertainties.

Altitude Dependence of Rocket Motor Performance

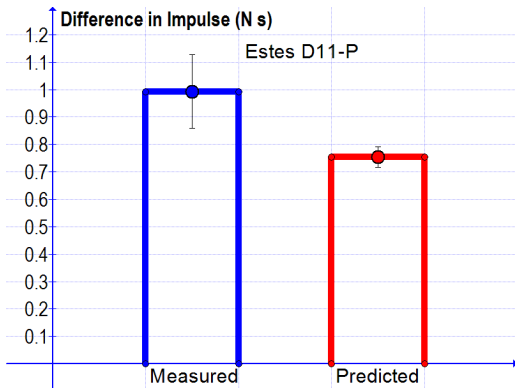


Figure 4: The measured and predicted differences between average impulses of the Estes D11-0P at high and low ambient pressures.

Measured and predicted differences in average impulses for the Estes D11-P at high and low ambient pressures are shown in Figure 4. Equation 3 predicted that the mean impulse would be 0.754 ± 0.038 N s greater at the lower ambient pressure of higher altitude. However, the mean impulse at high altitude was 18.308 ± 0.103 N s, and the mean impulse at low altitude was 17.315 ± 0.087 N s. This is a measured difference of 0.993 ± 0.135 N s. The predicted difference in impulse is in the right ballpark, but outside of the experimental uncertainties.

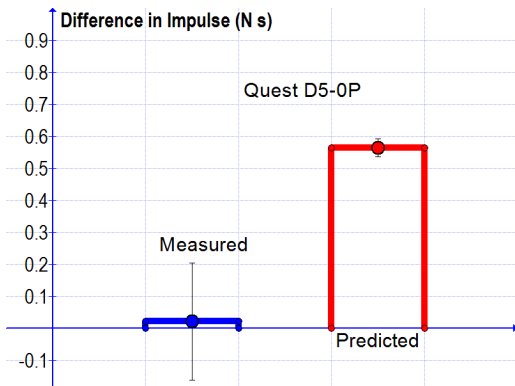


Figure 5: The measured and predicted differences between average impulses of the Quest D5-0P at high and low ambient pressures.

Figure 5 shows measured and predicted differences in average impulses for the Quest D5-0P. Equation 3 predicted that the mean impulse would be 0.564 ± 0.028 N s greater at the lower ambient pressure of higher altitude. However, the mean impulse at high altitude was 19.245 ± 0.106 N s, and the mean impulse at low altitude was 19.226 ± 0.148 N s. This is a measured difference of 0.021 ± 0.182 N s. The measured difference in impulse is much smaller than the predicted difference.

Discussion

In the two cases of the Estes rocket motors, the predictions of Equation 3 were relatively close, though outside the estimated uncertainties. The actual increase in impulse was 20-25% larger than might have been expected based on the simple formula based on the differences in ambient pressures, the cross sectional area of the throat, and the duration of the fuel burn. It may be that the effective area of the pressure differential is slightly bigger than the throat, or it may be that the assumptions that went into equation 3 are not valid. The difference in ambient pressure might effect the mass flow rate or the exhaust velocity (the first term in Equation 1).

Altitude Dependence of Rocket Motor Performance

The discrepancy between the predicted and observed increases in impulse is larger and harder to explain for the Quest D11-0P. This rocket motor does not demonstrate any significant improvement in performance at the lower ambient pressure corresponding to higher altitude. It may be relevant that this rocket motor has a much longer burn time (4.6 seconds), a smaller throat in the nozzle (2.5 mm), and probably a much lower chamber pressure than the other motors. This motor also burns much louder and seems to sputter while burning which suggest a larger deviation from laminar flow.

It is also notable that all of these rocket motors fail to meet their published impulse specifications. The Estes A10-PT advertises an impulse of 2.5 N s, but actually achieves mean impulses of 2.232 ± 0.029 N s and 2.006 ± 0.022 N s, at high altitude and sea level, respectively. The Estes D11-P advertises an impulse of 20.0 N s, but actually achieves mean impulses of 18.308 ± 0.103 N s and 17.315 ± 0.087 N s at high altitude and sea level, respectively. The Quest D5-0P advertises an impulse of 20.0 N s, but actually achieves mean impulses of 19.266 ± 0.148 N s and 19.245 ± 0.106 N at high altitude and sea level, respectively. The present study is not the first to report hobby rocket motors failing to meet their impulse specifications. Measurements reported by a group at the University of Central Arkansas found that Estes rocket motor models A3-4T, A8-3, B4-4, B6-4, C6-5, and D12-3 have measured impulses from 15.4% to 22.8% below the specifications (Penn et al., 2010). A study at the Australian Defense Force Academy found Estes D11-P motor to have an impulse 11.4% below Estes specifications and the C6-0 motor to be 4.45% below Estes' specifications (Carter, 2008), and an earlier study found the Estes A10-PT to be 20% below Estes' impulse specification.

The increase in thrust at higher altitudes is just one factor that will tend to enhance rocket performance in thinner atmospheres. Reduced drag also plays an important role. These two effects combine so that rockets launched at higher altitudes will be expected to fly higher, faster, and farther than rockets launched at sea level. Equation 3 may be a good first approximation to estimating enhanced performance at higher altitudes, but clearly other factors must be considered for accurate predictions.

Acknowledgements

This research was supported in part by BTG Research (www.btgresearch.org), by the United States Air Force Academy, and by the Air Force Office of Scientific Research. Ya'el Courtney assisted with the experimental design and with data collection.

References

- High Altitude Launches. Sky Ramp Technology, 2008. Web. 22 October, 2012.
<http://www.g2mil.com/high.htm>
- Benson, Tom. Specific Impulse. 11 July, 2008. Web. 22 October, 2012.
<http://www.grc.nasa.gov/WWW/k-12/airplane/specimp.html>
- Carter, M. G. An investigation into the Combustion and Performance of Small Solid-Propellant Motors. 2008. University of New South Wales at the Australian Defense Force Academy.
- Courtney, Michael, and Amy Courtney. 2009. Measuring thrust and predicting trajectory in model rocketry. Cornell University Library. Popular Physics. arXiv:0903.1555.
- Penn, Kim and William V. Slaton, Measuring Model Rocket Engine Thrust Curves, The Physics Teacher -- December 2010 -- Volume 48, Issue 9, pp. 591.
- Sutton, George P., Biblarz, Oscar. 2010. Rocket Propulsion Elements 8th Ed., John Wiley and Sons, ISBN 0470080248.

Altitude Dependence of Rocket Motor Performance

Appendix: Data

Test	Low Altitude		High Altitude	
	Impulse	Specific Impulse	Impulse	Specific Impulse
	Ns	s	Ns	s
1	2.080	57.605	2.262	62.658
2	2.012	58.113	2.368	68.381
3	1.985	56.679	2.112	60.305
4	1.958	54.674	2.389	66.720
5	2.023	54.837	2.219	60.159
6	1.953	53.387	2.194	59.960
7	2.171	59.166	2.144	58.436
8	1.990	54.822	2.213	60.969
9	1.915	56.918	2.190	65.085
10	1.973	54.790	2.323	64.523
Average	2.006	56.099	2.232	62.519
Std. Dev.	0.069	1.762	0.093	3.305
Uncertainty	0.022	0.557	0.029	1.045

Table A1: Impulse and specific impulse data for each rocket firing of the Estes A10-PT at low and high altitude.

Altitude Dependence of Rocket Motor Performance

	Low Altitude		High Altitude	
	Impulse	Specific Impulse	Impulse	Specific Impulse
Test	Ns	s	Ns	s
1	17.522	72.458	18.810	77.657
2	16.894	70.839	18.420	75.704
3	17.395	71.702	17.870	74.678
4	17.552	72.849	18.250	75.388
5	17.516	71.822	18.020	74.939
6	17.706	72.868	18.500	76.149
7	17.119	70.736	18.660	76.613
8	17.457	72.220	18.150	76.003
9	17.092	70.740	18.090	74.582
10	16.894	70.090	17.860	74.358
Average	17.315	71.632	18.308	75.746
Std. Dev.	0.276	0.932	0.326	1.035
Uncertainty	0.087	0.295	0.103	0.327

Table A2: Impulse and specific impulse data for each rocket firing of the Estes D11-P at low and high altitude.

Altitude Dependence of Rocket Motor Performance

Test	Low Altitude		High Altitude	
	Impulse	Specific Impulse	Impulse	Specific Impulse
	Ns	s	Ns	s
1	19.155	79.601	19.580	80.280
2	19.410	79.814	19.530	81.458
3	19.303	78.738	18.870	78.057
4	19.431	80.944	19.580	79.821
5	19.465	81.285	18.500	77.472
6	19.505	79.277	19.690	81.727
7	18.539	76.976	18.980	78.454
8	19.544	78.996	18.820	77.758
9	18.687	77.246	19.890	80.726
10	19.410	79.049	19.220	79.327
Average	19.245	79.193	19.266	79.508
Std. Dev.	0.334	1.303	0.468	1.608
Uncertainty	0.106	0.412	0.148	0.509

Table A3: Impulse and specific impulse data for each rocket firing of the Quest D50P at low and high altitude.