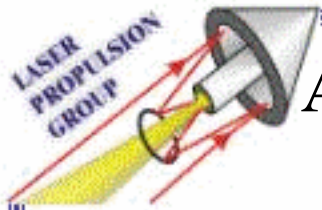


REPORT DOCUMENTATION PAGE				Form Approved OMB No. 0704-0188	
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1. REPORT DATE (DD-MM-YYYY) 20-10-2005		2. REPORT TYPE Briefing Charts		3. DATES COVERED (From - To)	
4. TITLE AND SUBTITLE  Ablation of Liquids for Laser Propulsion with TEA CO <sub>2</sub> Laser (Briefing Charts, PREPRINT)				5a. CONTRACT NUMBER	
				5b. GRANT NUMBER	
				5c. PROGRAM ELEMENT NUMBER	
6. AUTHOR(S) John Sinko, Lisa Kodgis, Simon Porter, Enrique Sterling, Jun Lin and Andrew V. Pakhomov (Dept of Physics, UA Huntsville); C. William Larson and Franklin B. Mead, Jr. (AFRL/PRSP)				5d. PROJECT NUMBER 4847	
				5e. TASK NUMBER 0159	
				5f. WORK UNIT NUMBER	
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES)  Air Force Research Laboratory (AFMC) AFRL/PRSP 10 E. Saturn Blvd. Edwards AFB CA 93524-7680				8. PERFORMING ORGANIZATION REPORT NUMBER  AFRL-PR-ED-VG-2005-395	
9. SPONSORING / MONITORING AGENCY NAME(S) AND ADDRESS(ES)  Air Force Research Laboratory (AFMC) AFRL/PRS 5 Pollux Drive Edwards AFB CA 93524-70448				10. SPONSOR/MONITOR'S ACRONYM(S)	
				11. SPONSOR/MONITOR'S NUMBER(S) AFRL-PR-ED-VG-2005-395	
12. DISTRIBUTION / AVAILABILITY STATEMENT  Approved for public release; distribution unlimited					
13. SUPPLEMENTARY NOTES Presented at the 4 <sup>th</sup> International Symposium on Beamed Energy Propulsion, Nara, Japan, 11-14 Nov 2005.					
14. ABSTRACT Time-resolved force sensing and intensified charge-coupled device (ICCD) imaging techniques were applied to the study of the force generation mechanism for laser ablation of liquids. A Transversely Excited at Atmospheric pressure (TEA) CO <sub>2</sub> laser operated at 10.6 μm, 300 ns pulse width, and 9 J pulse energy was used to ablate liquids contained in various aluminum and glass vessels. Net imparted impulse and coupling coefficient were derived from the force sensor data and relevant results will be presented for various container designs and liquids used. ICCD imaging was used in conjunction with the dynamic force techniques to examine dependencies on absorption depth, irradiance, surface curvature, and container geometry. ICCD imaging was also used to determine whether surface or volume absorption should be preferable for laser propulsion using liquid propellants. Finally, ballistic experiments were conducted in order to verify the dynamic force data and lend additional evidence as to the predominant methods of force generation.					
15. SUBJECT TERMS					
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT	18. NUMBER OF PAGES	19a. NAME OF RESPONSIBLE PERSON
a. REPORT	b. ABSTRACT	c. THIS PAGE			Dr. Franklin B. Mead, Jr.
Unclassified	Unclassified	Unclassified	A	39	19b. TELEPHONE NUMBER (include area code) (661) 275-5929



# Ablation of Liquids for Laser Propulsion with TEA CO<sub>2</sub> Laser (Preprint)

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## Acknowledgements

**ERC, Inc.**

*Edwards AFB, CA 93524-7680, USA*

**Laser Propulsion Group**

*Adam Hendrickson, Casey Kemp, Jonathon Kemper, Jonathan Lassiter, Venkatakrishna Mukundaraj, Christopher Smith,  
and Wesley Swift, Jr.*

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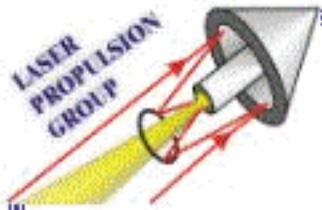
**Gene Nelson**

*UAH Glassblower*

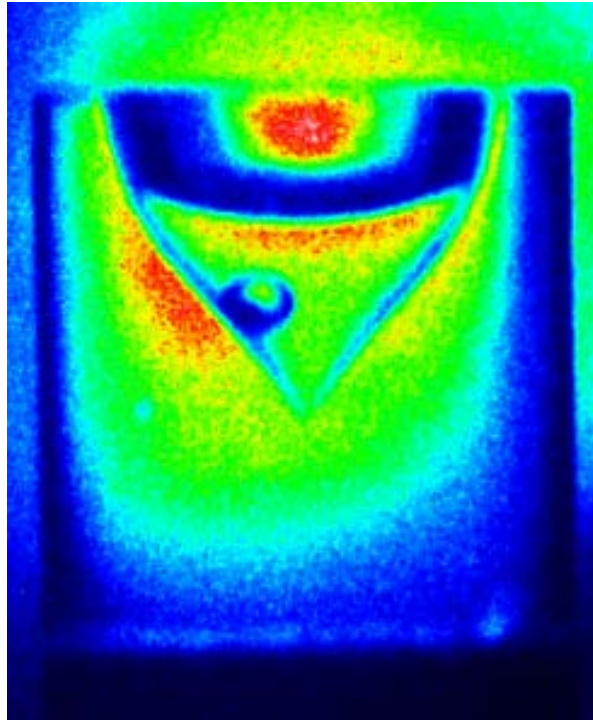
**Scott Anderson**

*Audio Arrangement*

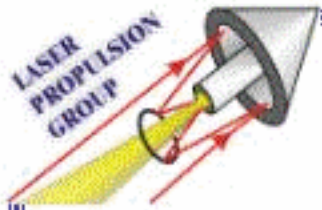




# Outline

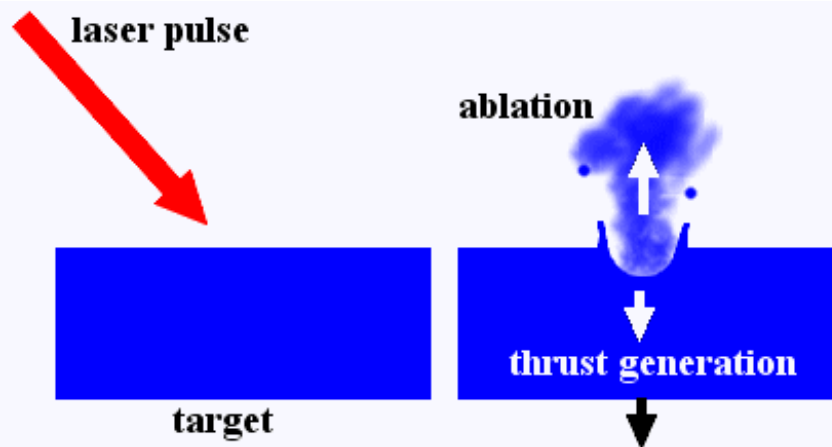


1. Introduction
2. Force
3. ICCD Ballistics
4. ICCD Imaging
5. Results and Discussion
6. Conclusions



# Laser Ablation

- Laser Ablation: removal of material by any physical process under laser irradiation



- Laser Ablation of Liquids
  - $C_m$  up to 350 dyne/W
  - Irradiance:  $10^7$ - $10^8$  W/cm<sup>2</sup>
  - $I_{sp}$  up to 50 s



# Motivation

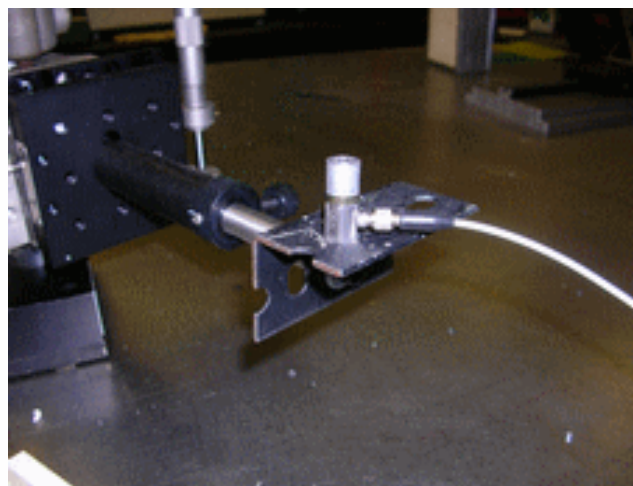
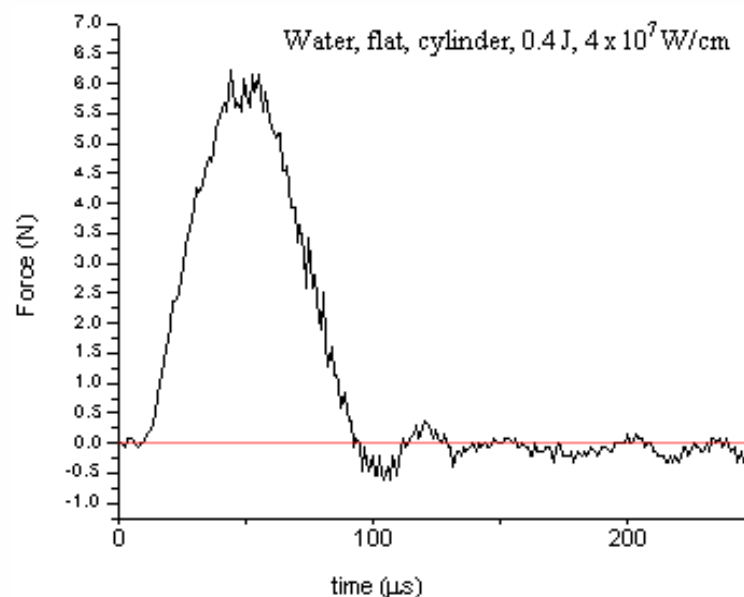
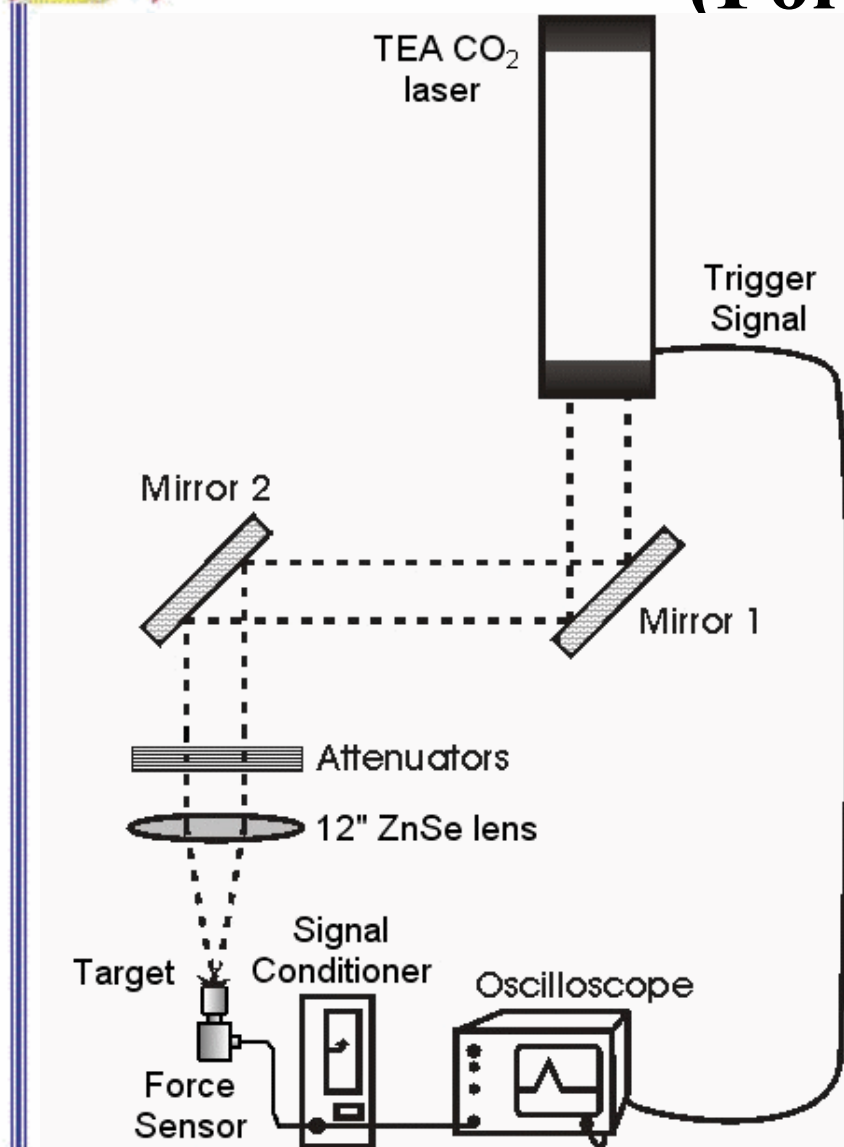
- (1) What is the physical mechanism generating thrust during the laser ablation of a liquid?
  - Plasma formation
  - Vaporization
  - Explosive boiling / Phase explosion
  - Cavity collapse / splashing
- (2) How do the ablation mechanisms for surface and volume-absorbing liquids differ?
- (3) How does  $C_m$  depend on:
  - Container geometry
  - Liquid surface curvature
  - Absorption depth



# Force Experiments



# Experimental Setup (Force Sensors)



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# Piezoelectric Force Sensors

## Small Force Sensor

- **Maximum Force: 9.786 N**
- Linearity:  $< 1\%$
- Sensitivity: 526.6 mV/N
- Discharge time constant:  $> 1.0$  s
- Rise Time: 5  $\mu$ s
- Resolution:  $10^{-4}$  N



PCB-209C01

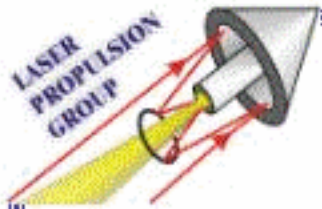
## Large Force Sensor

- **Maximum Force: 444.8 N**
- Linearity:  $< 0.4\%$
- Sensitivity: 11.96 mV/N
- Discharge time constant:  $> 500$  s
- Rise Time: 8  $\mu$ s
- Resolution:  $10^{-3}$  N



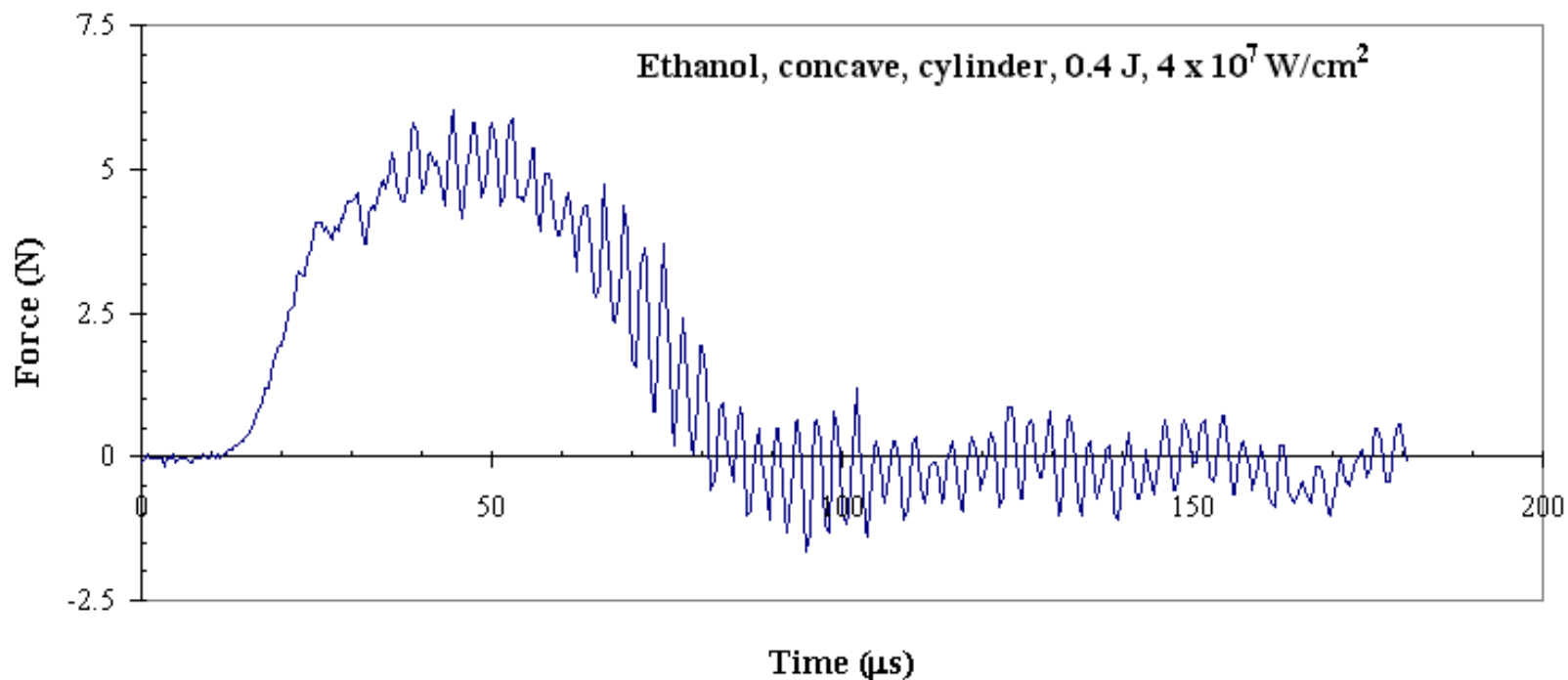
PCB-200B02





# Force-Time Curve

- Measurements are as follows:
  - Single laser shot
  - Force vs. time
  - Large force peak observed (10-90  $\mu\text{s}$ , centered 40-50  $\mu\text{s}$ )



- Integrate to find I, then derive  $C_m$



# Coupling Coefficients and Peak Force

Peak Force (N)		Hexane	Ethanol	Water
Cylinder	Flat	$3.4 \pm 0.4$	$5.2 \pm 0.6$	$4.1 \pm 0.4$
	Concave	$3.1 \pm 0.2$	$6.0 \pm 0.1$	$5.7 \pm 0.5$
Cone	Flat	$3.6 \pm 0.3$	$5 \pm 1$	$4.1 \pm 0.4$
	Concave	$3.7 \pm 0.3$	$5.8 \pm 0.4$	$5.3 \pm 0.4$

$C_m$ (dyne/W)		Hexane	Ethanol	Water
Cylinder	Flat	$22 \pm 3$	$50 \pm 3$	$43 \pm 4$
	Concave	$22 \pm 3$	$56 \pm 4$	$60 \pm 6$
Cone	Flat	$23 \pm 1$	$49 \pm 6$	$47 \pm 5$
	Concave	$24 \pm 3$	$56 \pm 3$	$56 \pm 6$

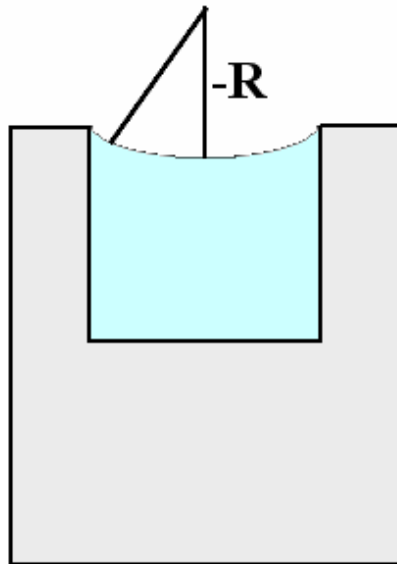
$(1.6 \times 10^7 \text{ W/cm}^2, 0.4 \text{ J, Force Sensor})$



# Surface Curvature

- Radius of Curvature  $R$

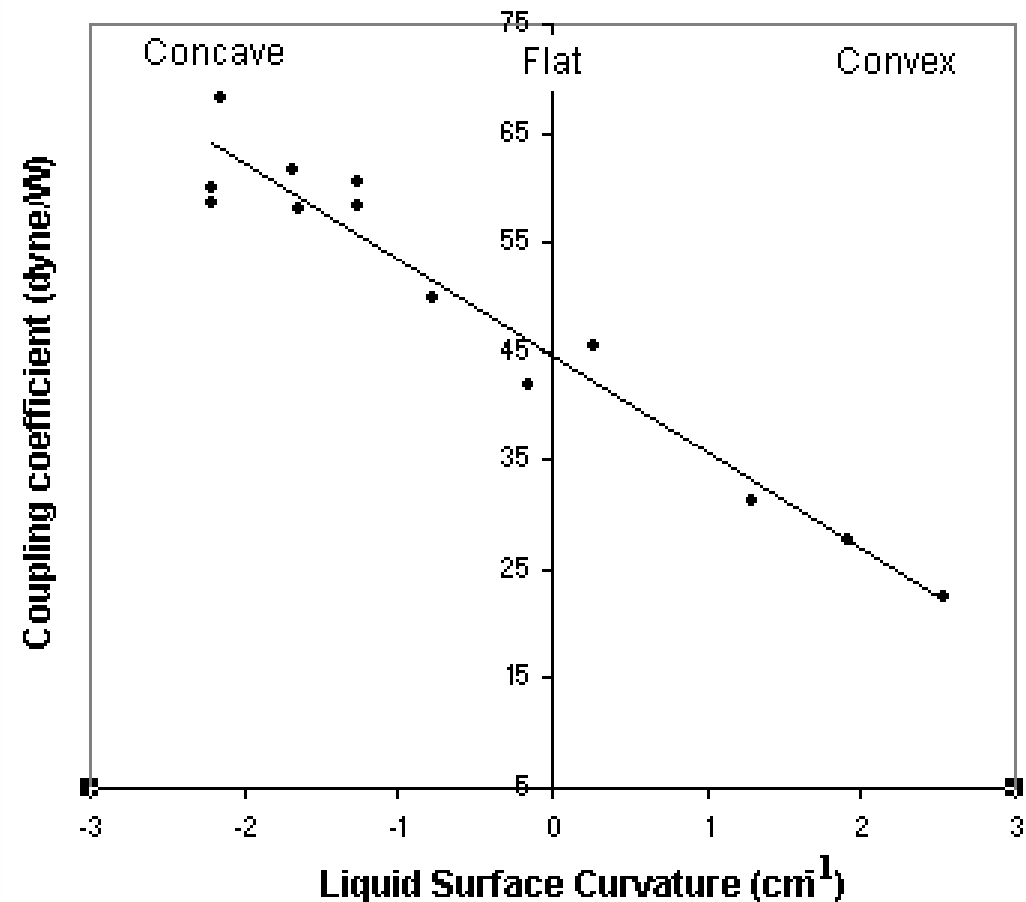
Water, flat, cylinder, 0.4 J,  $2 \times 10^7$  W/cm<sup>2</sup>



- Curvature  $\kappa$  (cm<sup>-1</sup>)

$$\kappa \equiv \frac{1}{R}$$

- $C_m$  directly dependent on  $\kappa$





# Imaging Experiments



# ICCD Imaging

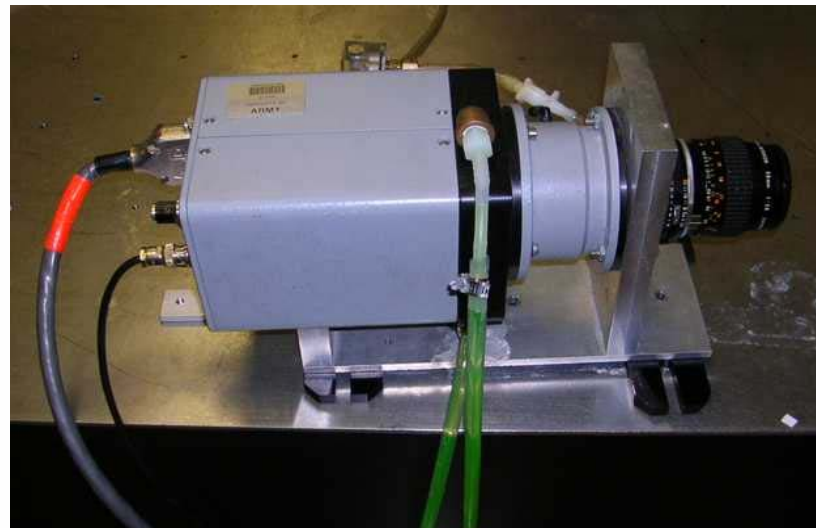
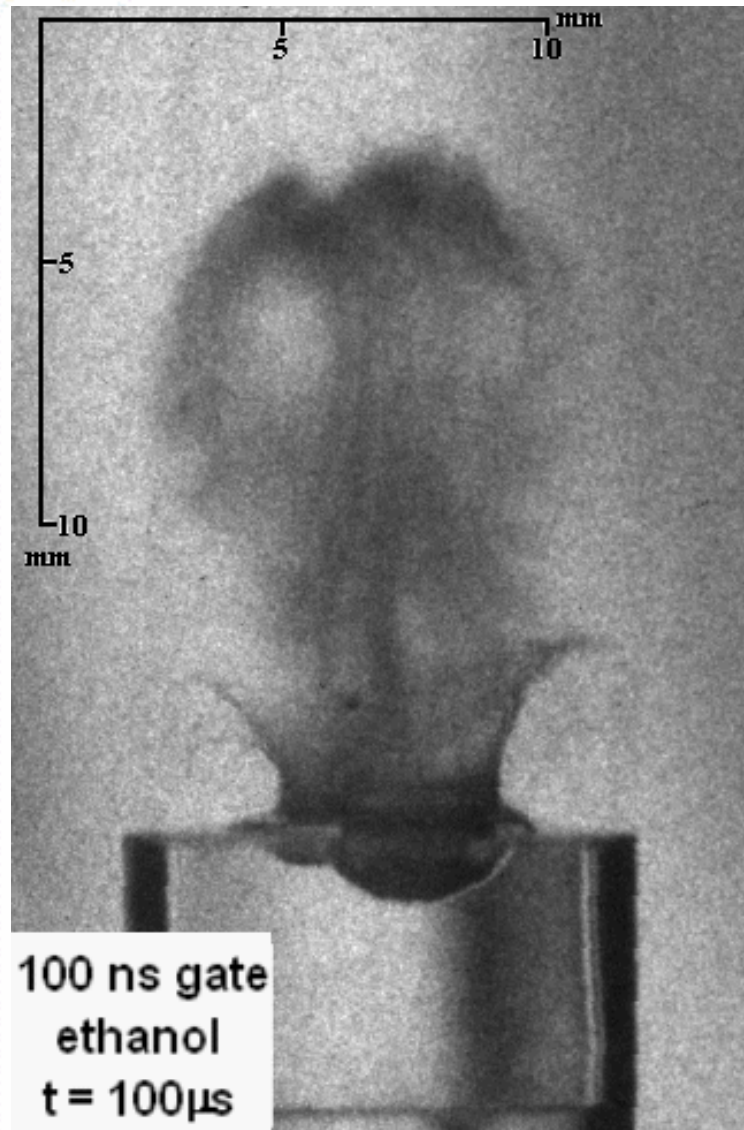
## Information on:

Initial plume velocities

Cavity growth rates

Characteristic physical processes

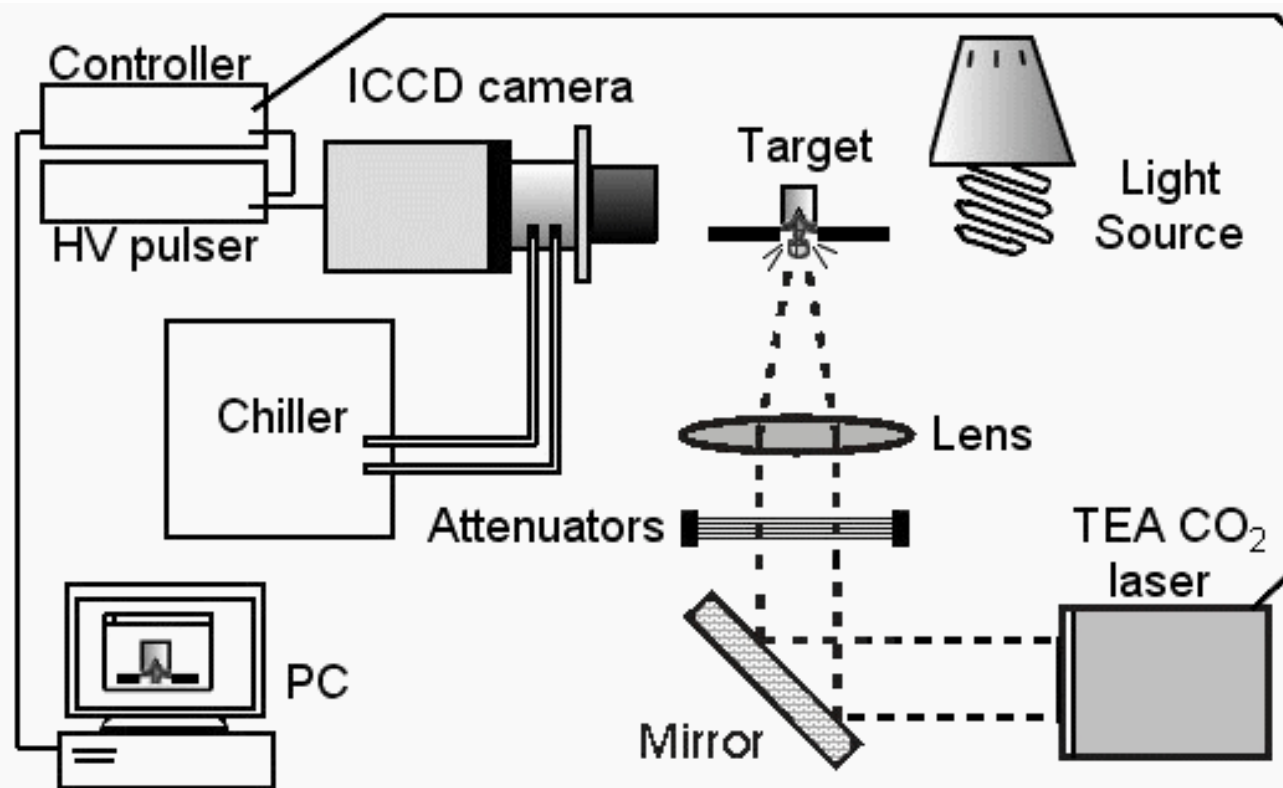
Timeline of processes





# ICCD Ballistics Setup

- Gated CCD technique
- Single laser shot per image
- Highly repeatable
- Composite sequences
- 382 x 574 pixel images
- >5 ns gate width (exposure)
- 5 ns - 83 ms delay







# Coupling Coefficients, dyne/W

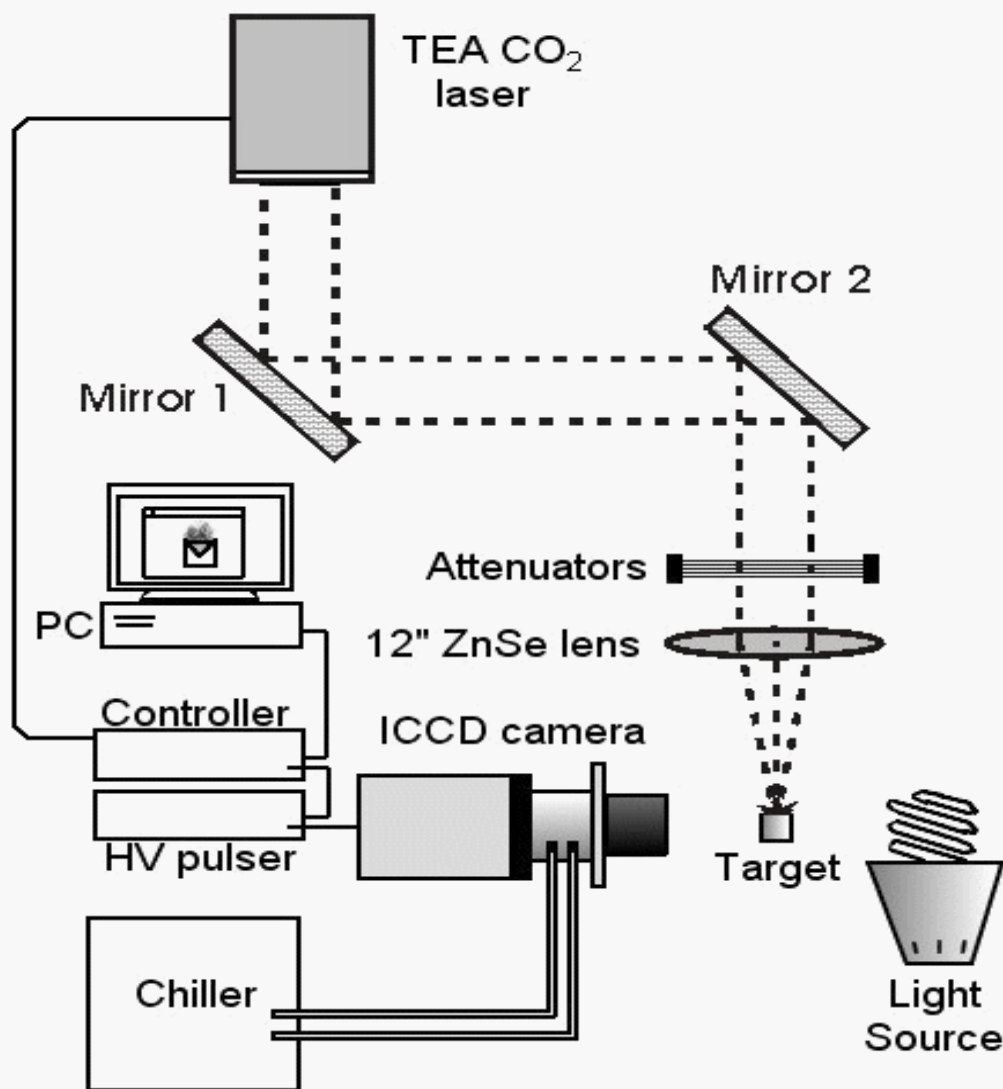
(Water, 3 mm<sup>2</sup> spot size)

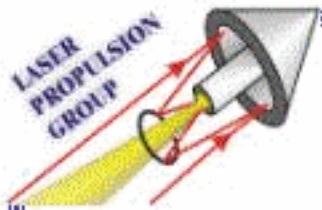
Energy (J)	Irradiance (W/cm <sup>2</sup> )	Small Force Sensor	Large Force Sensor	Ballistics
0.4	4 x 10 <sup>7</sup>	110 ± 14	-	98 ± 9
1.2	1 x 10 <sup>8</sup>	44 ± 24	53 ± 21	37 ± 5
3.6	5 x 10 <sup>8</sup>	-	14 ± 3	14 ± 2

$$C_m = \frac{I}{E_{\text{pulse}}} = \frac{m}{E_{\text{pulse}}} \sqrt{2 g h_{\text{max}}}$$

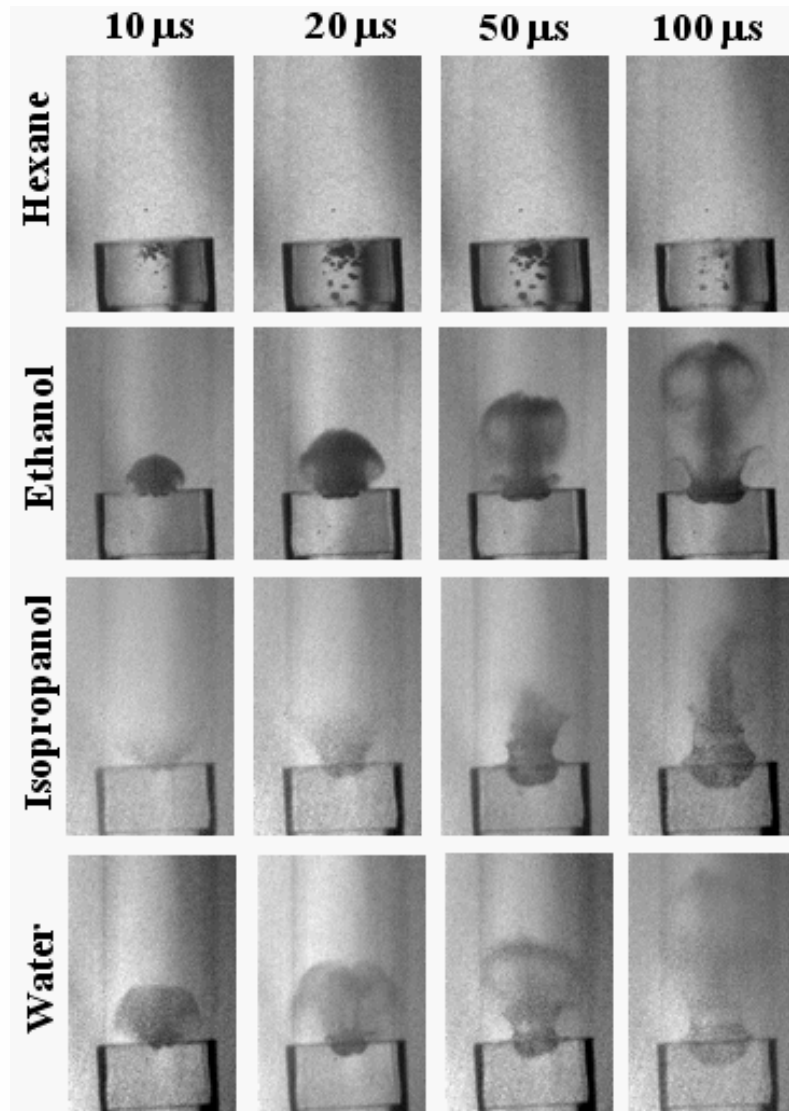


# Imaging Setup





# ICCD Images



## Volume-absorbing

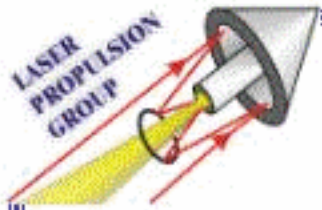
(hexane)

- No observed plume
- No cavity formation
- Boiling

## Surface-absorbing

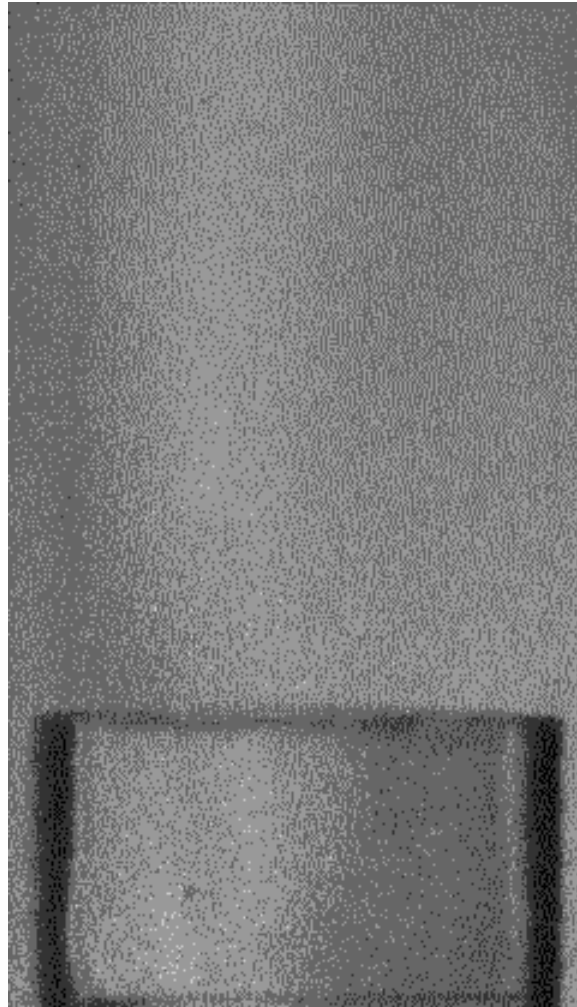
(ethanol, isopropanol, water)

- Vapor plume
- Cavity formation



# Surface Absorption

Ethanol, 0.4 J,  $4 \times 10^7$  W/cm<sup>2</sup>

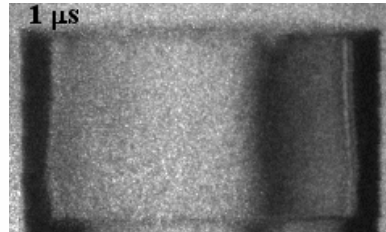




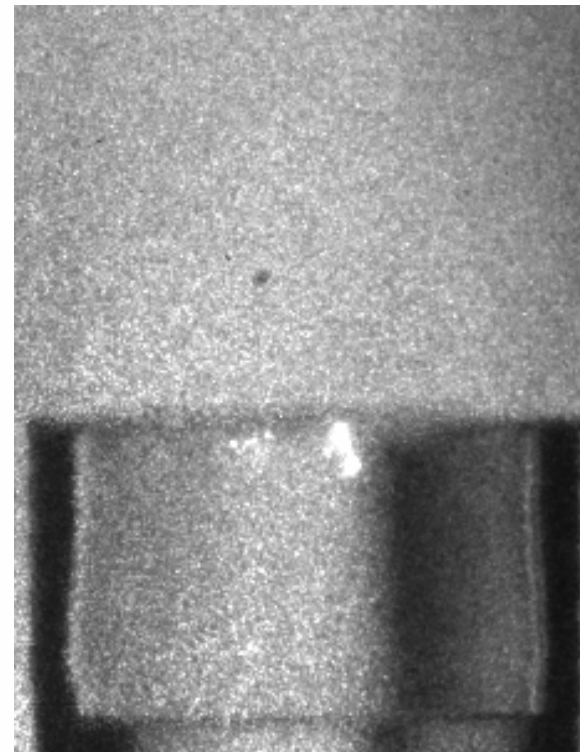
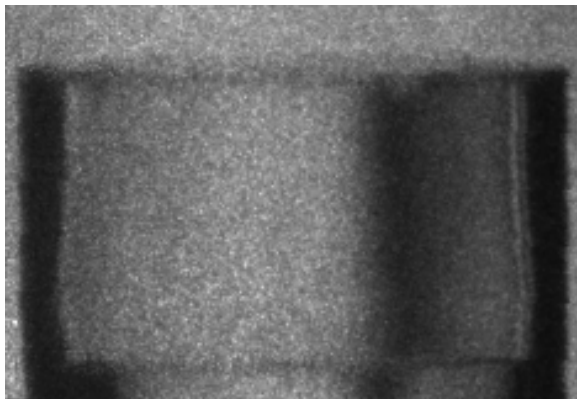
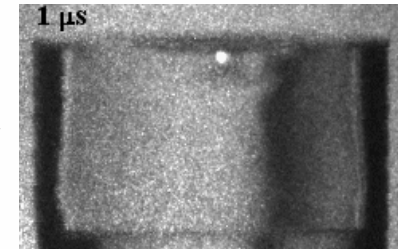


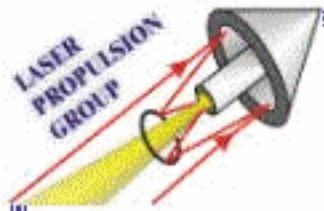
# Volume Absorption (Hexane)

- 0.4 J
- $4 \times 10^7 \text{ W/cm}^2$
- No plasma
- No cavity
- No plume
- Boiling



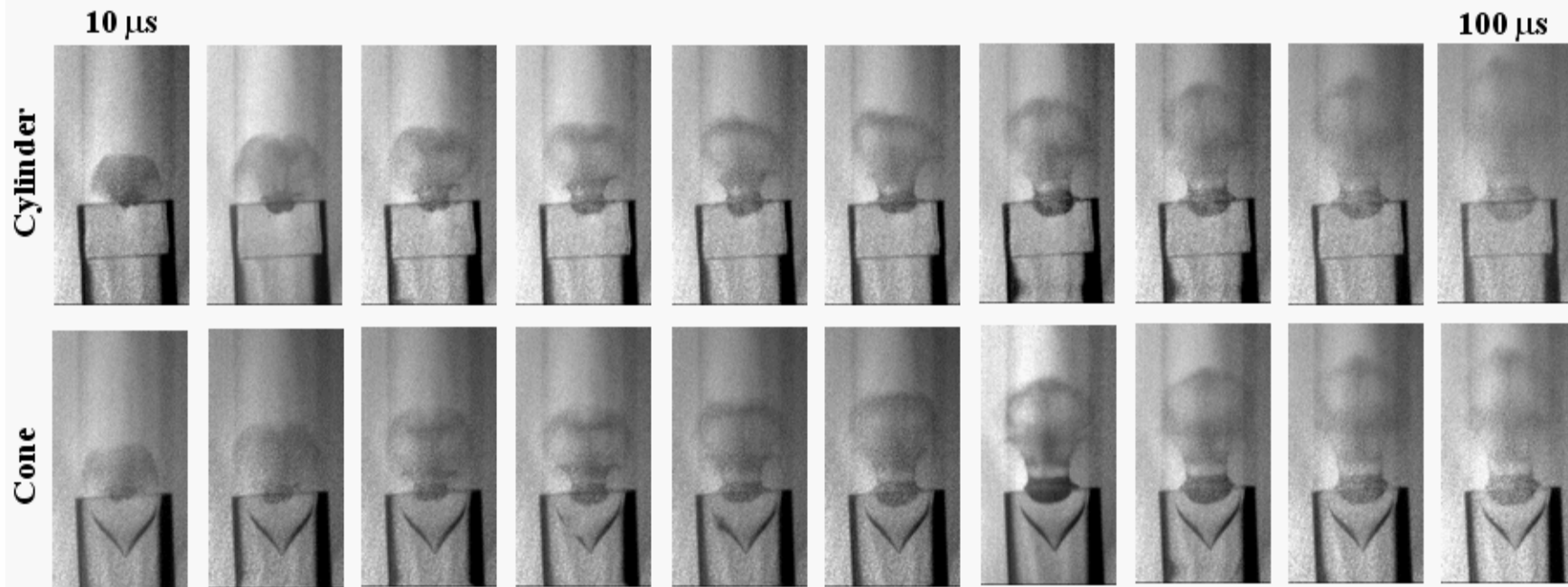
- 1.1 J
- $1 \times 10^8 \text{ W/cm}^2$
- Plasma
- Surface cavity
- Vapor plume



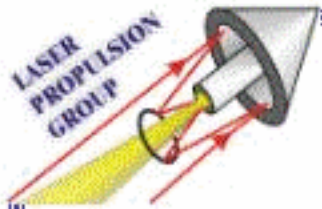


# Containers: Cylinder vs. Cone

- Water, 10-100  $\mu\text{s}$
- Virtually no difference observed

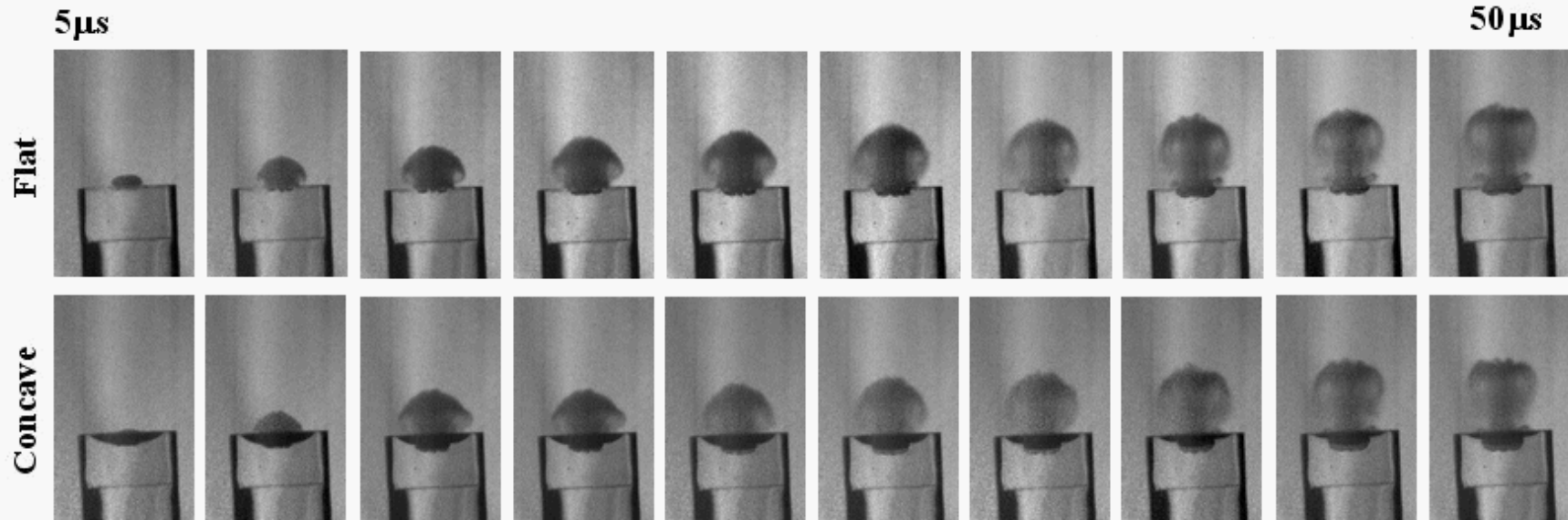






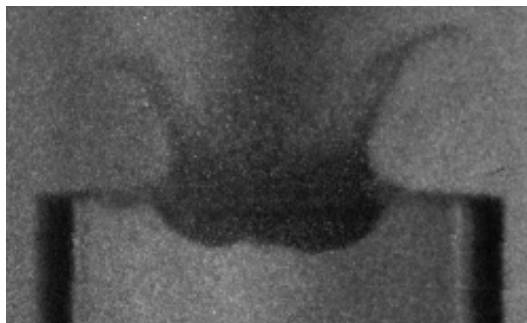
# Surfaces: Flat vs. Concave

- Ethanol, 5-50  $\mu\text{s}$ :

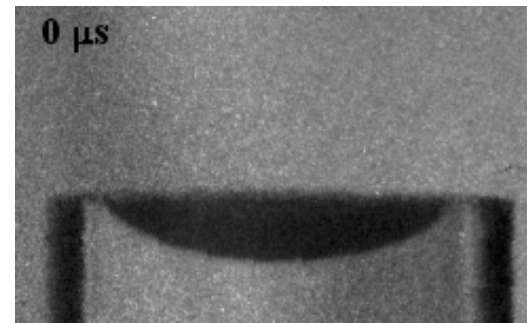


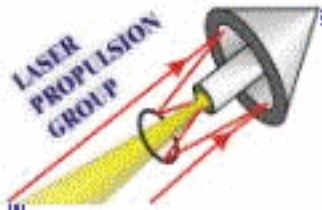
Effect of Initial Curvature (100  $\mu\text{s}$ )

Flat:



Concave:



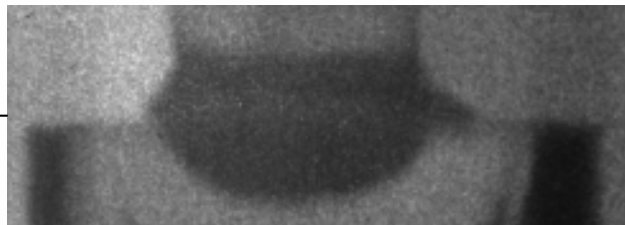
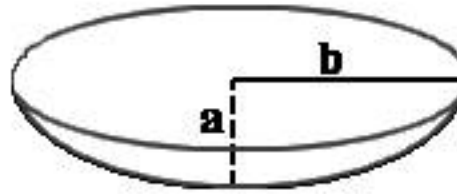


# Analysis of Mass Loss and Cavity Growth

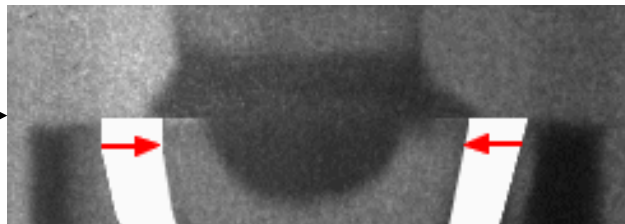


Model as oblate spheroid

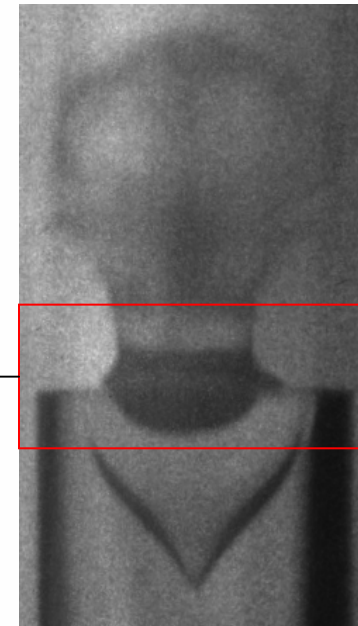
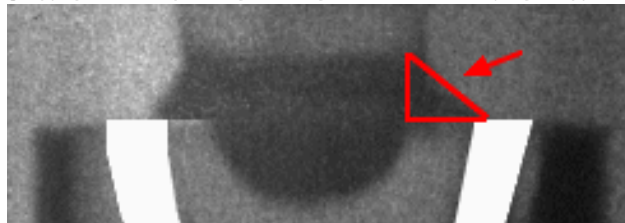
$$\left( V = \frac{2}{3} \pi a b^2 \right)$$



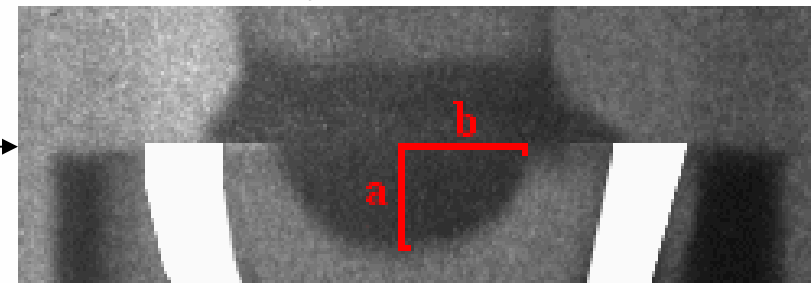
Correction for distortion



Subtraction of rim volume



Cavity measurement





# Liquid Mass Loss

- All data using cylinder, flat surface, 0.4 J,  $7 \times 10^7$  W/cm<sup>2</sup>
- Increased cavity growth during initial 100  $\mu$ s
- ICCD imaging: Mass (mg) removed during initial 100  $\mu$ s
- Scientific Balance: Total mass (mg) removed in entire process

## Mass Loss (mg)

Liquid	Hexane	Ethanol	Isopropanol	Water
0-100 $\mu$ s	0	$2 \pm 1$	$1 \pm 1$	$1 \pm 1$
Total Process	$4 \pm 1$	$51 \pm 6$	$51 \pm 2$	$51 \pm 5$
Ratio	0 %	4 %	2 %	2 %



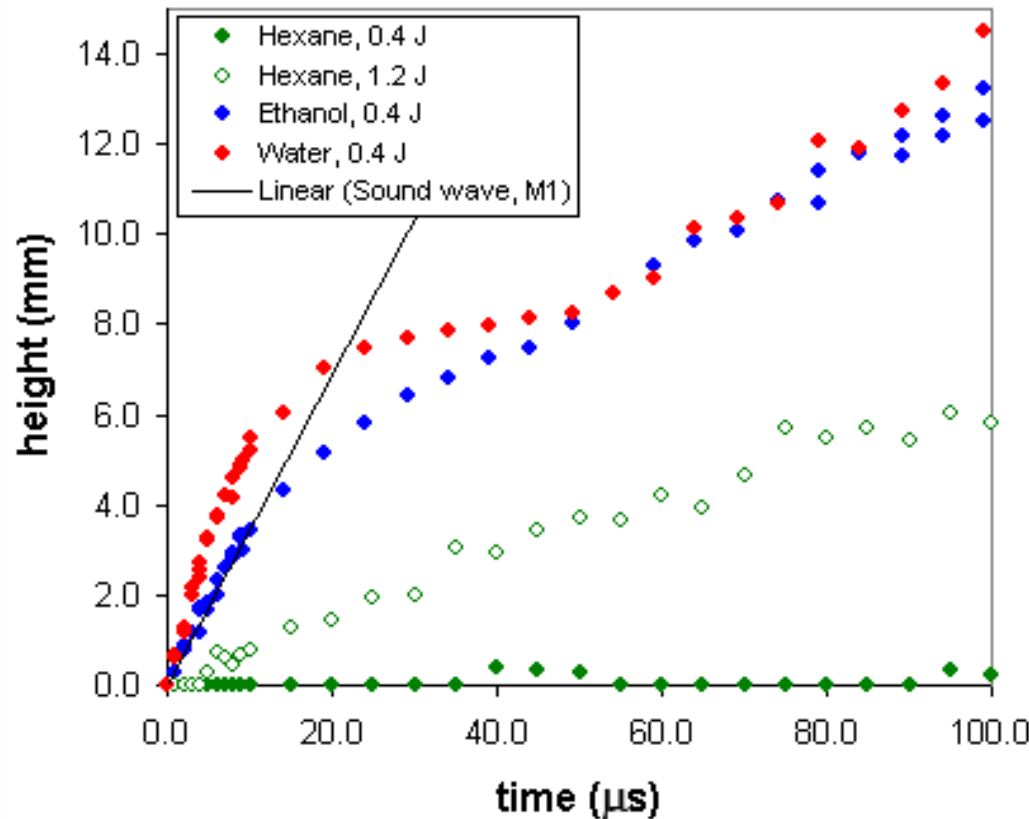
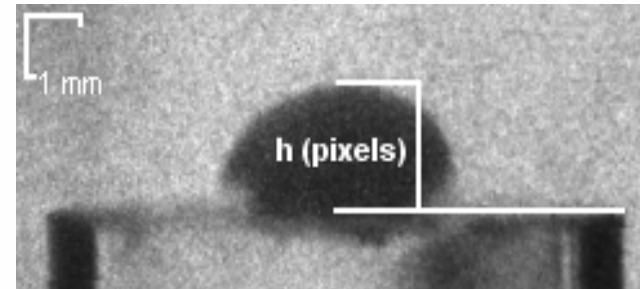
# Analysis of Initial Velocities



Center plume front height  $h$

$\Delta h$  paired with known  $\Delta t$

$$\lim_{t \rightarrow 0} \frac{\Delta h}{\Delta t} = v_0$$



Surface absorbing liquids  
transonic – supersonic  
initial velocities observed

Volume absorbing liquids:  
subsonic to transonic  
velocities observed



# Specific Impulse and Internal Efficiency

$$I_{sp} \equiv \frac{I}{W} \approx \frac{u_e}{g}$$

( $1.6 \times 10^7$  W/cm<sup>2</sup>, 0.4 J)

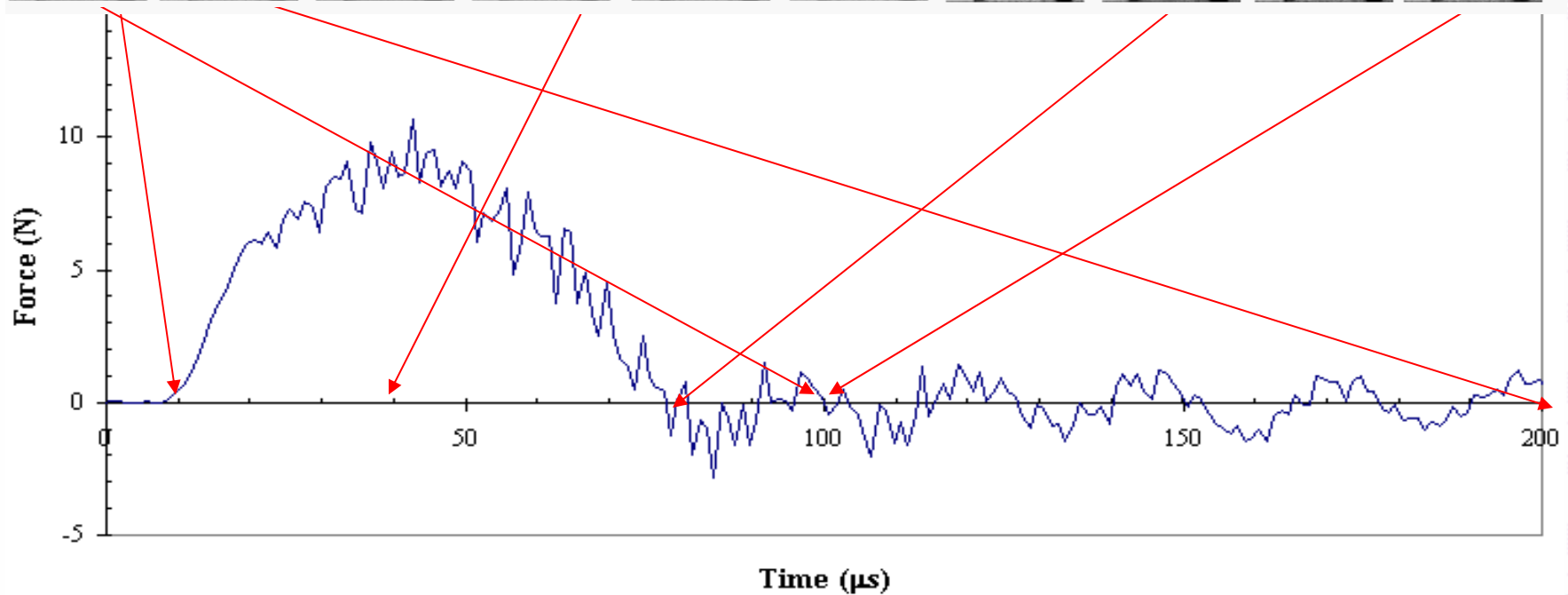
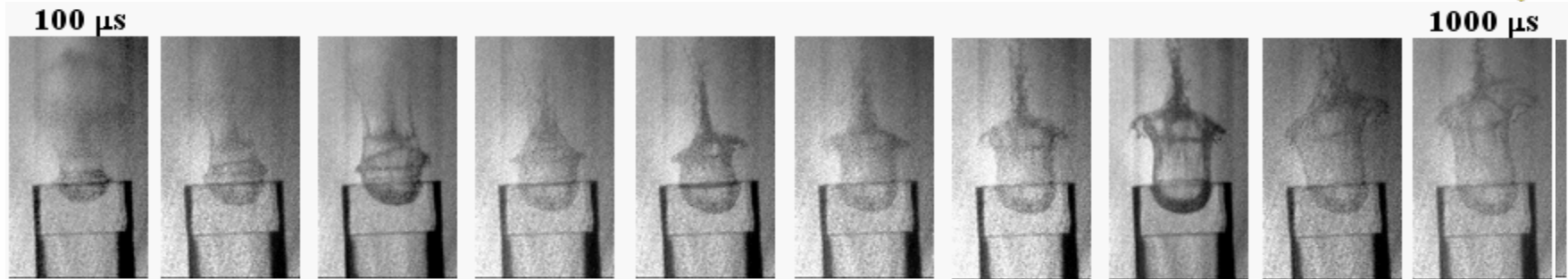
Specific Impulse (s)	Hexane	Ethanol	Water
from $v_0/g$	-	$42 \pm 1$	$84 \pm 3$
1 <sup>st</sup> 100 $\mu$ s	-	$10 \pm 5$	$20 \pm 10$
Total process	$2.3 \pm 0.6$	$0.40 \pm 0.05$	$0.34 \pm 0.05$

Internal Efficiency (%)	Hexane	Ethanol	Water
from $v_0/g$	-	$10.3 \pm 0.7$	$18 \pm 2$
1 <sup>st</sup> 100 $\mu$ s	-	$3 \pm 1$	$4 \pm 2$
Total process	$0.24 \pm 0.08$	$0.10 \pm 0.01$	$0.07 \pm 0.01$





# Force Data with ICCD Imaging



(Water, cylinder, concave, 0.4 J,  $4 \times 10^7 \text{ W/cm}^2$ )





# Conclusions



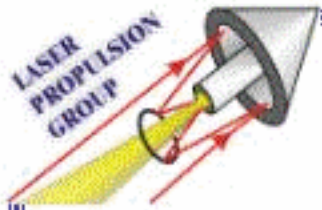
# Conclusions

- 1) A series of experiments with time-resolved force sensors and ICCD imaging were conducted on liquids.
- 2) 2 major physical ablation processes are observed: vaporization and splashing. In some cases plasma formation was also achieved.
- 3) The major source of thrust generation in the laser ablation of liquids is vaporization.
- 4) ICCD imaging shows vaporization occurs from 0 to 100  $\mu\text{s}$  after the laser pulse. Splashing is initiated after about 100  $\mu\text{s}$ .
- 5) Force generation occurs during the vaporization regime.
- 6) The peak force was observed  $\sim 40\text{-}50$   $\mu\text{s}$  after the laser pulse.
- 7) Ballistics experiments corroborate the impulse measurements with force sensors.
- 8) Surface absorbing liquids show higher  $C_m$  ( $\sim 50\text{-}150$  dyne/W) than volume absorbing liquids ( $\sim 10\text{-}50$  dyne/W).



## Conclusions (continued)

- 9)  $C_m$  is dependent on surface geometry for surface absorbing liquids.  
Changing geometry does not affect  $C_m$  for volume absorbing liquids.
- 10)  $C_m$  is dependent on container geometry for volume absorbing liquids.  
Changing container geometry does not affect  $C_m$  for surface absorbing liquids.
- 11) The majority of mass loss occurs due to splashing (>95%) rather than vaporization (<5%).
- 12) Momentum coupling was observed to be about 3 times more sensitive to changes in the surface curvature for surface absorbing liquids than to changes in the container geometry for volume absorbing liquids.  
This is additional evidence in favor of a dominant vaporization mechanism.



# THANK YOU



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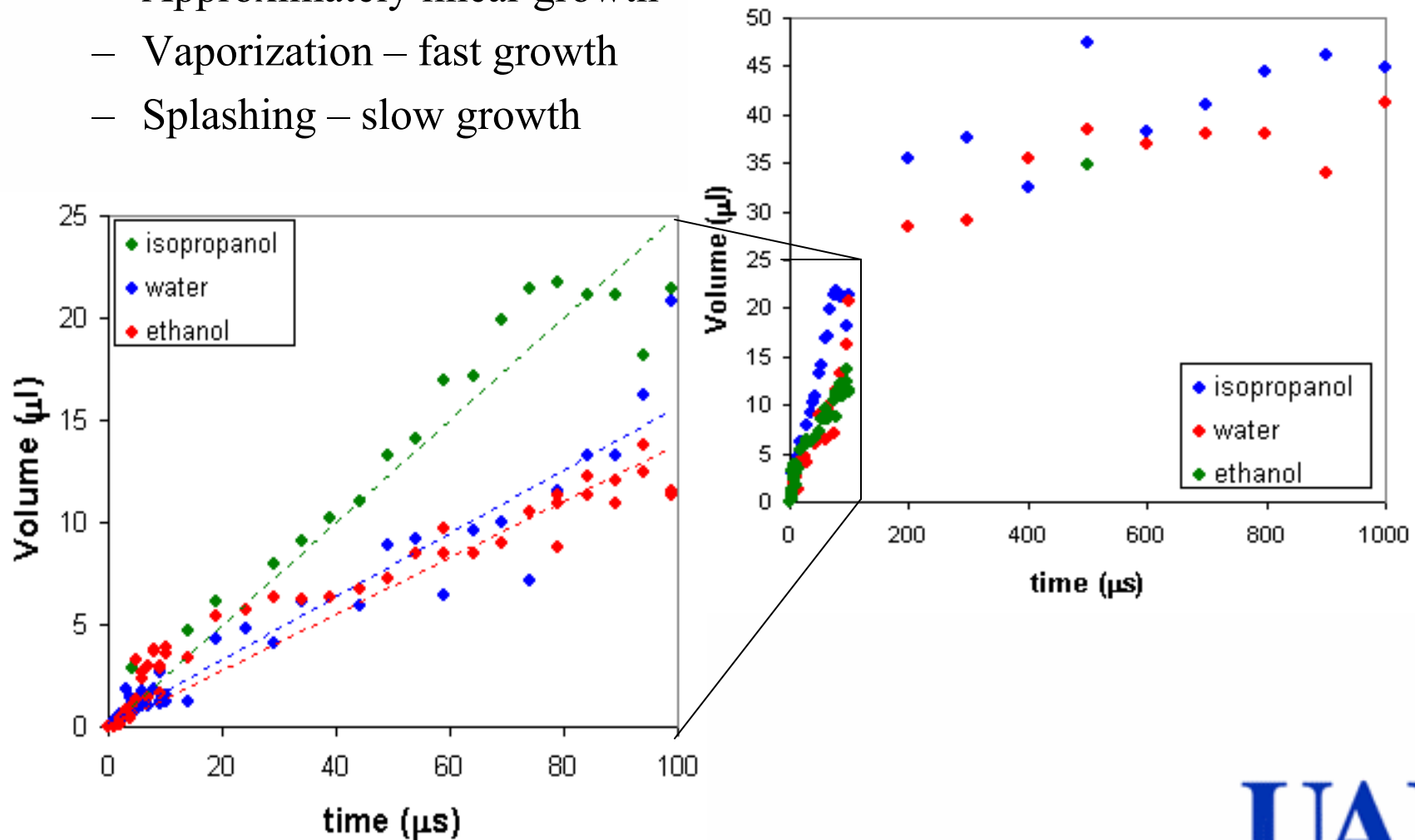
**UAH**  
The University of Alabama in Huntsville





# Cavity Growth

- 2 Regimes:
  - Approximately linear growth
  - Vaporization – fast growth
  - Splashing – slow growth







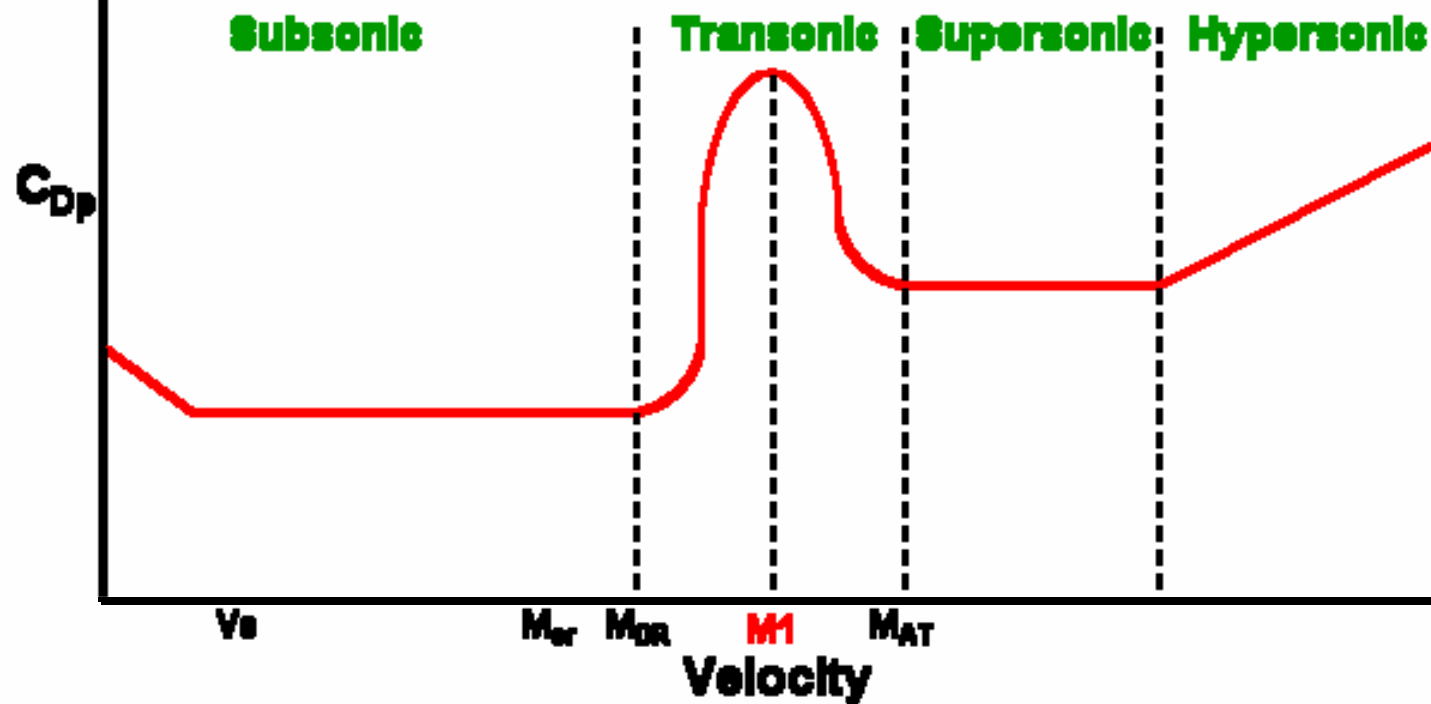
# Challenges of Using Piezoelectric Force Sensors

- Measurements in an accelerating frame
  - Distortion\*
  - Solution: Sensor at rest
- Rise time limits detection speed
  - Plasma processes  $\sim 1 \mu\text{s}$
  - Liquid vaporization  $\sim 100 \mu\text{s}$
  - Cavity Collapse  $\sim 1 \text{ ms}$
  - Liquid splashing  $\sim 10 \text{ ms}$
  - (Force sensors:  $5 \mu\text{s}$  rise time)
- Natural frequencies
  - Solution: Fourier analysis



# Drag vs. Velocity

## Coefficient of Parasite Drag Vs. Velocity

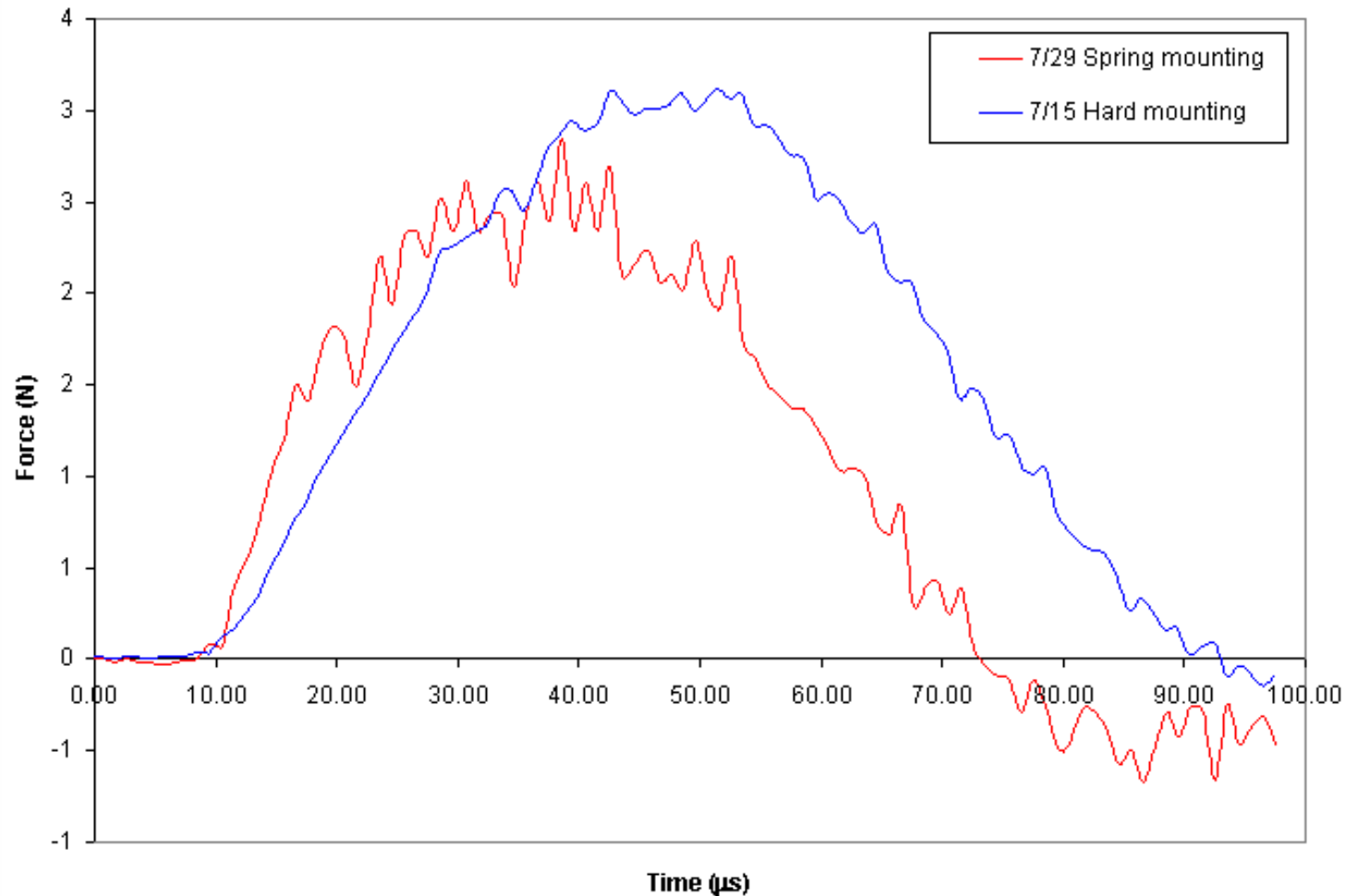




# Force Sensor Distortion

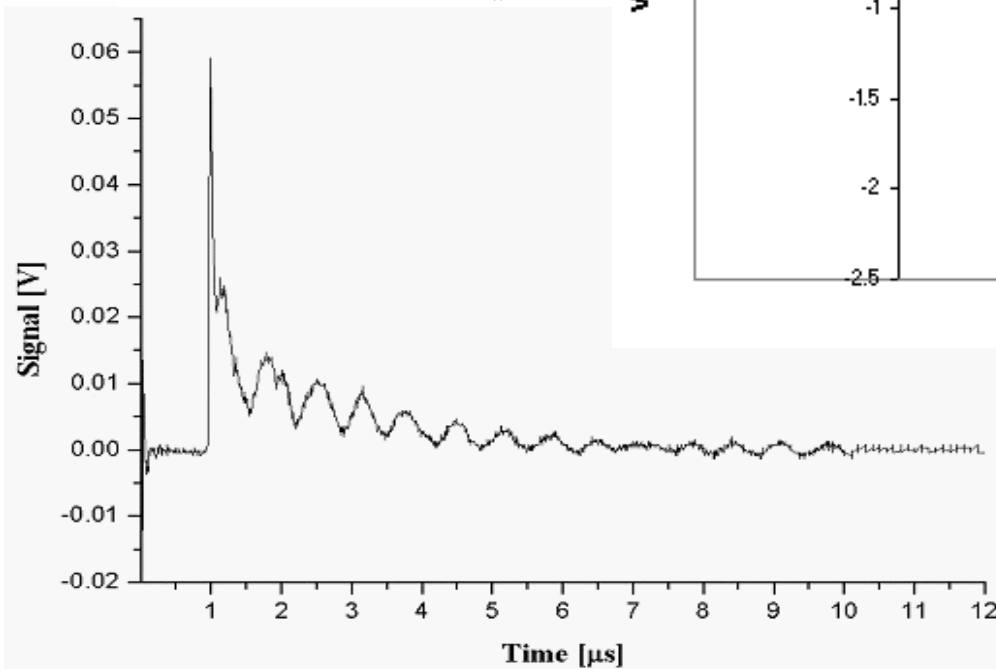
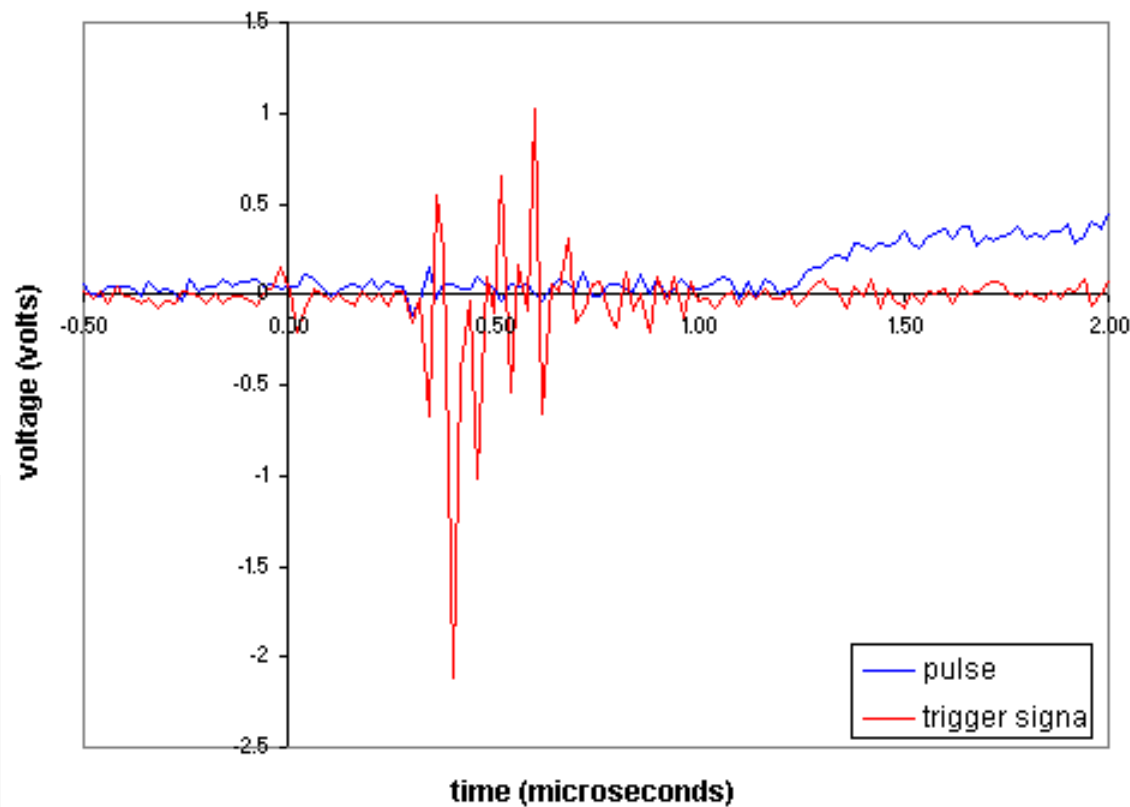
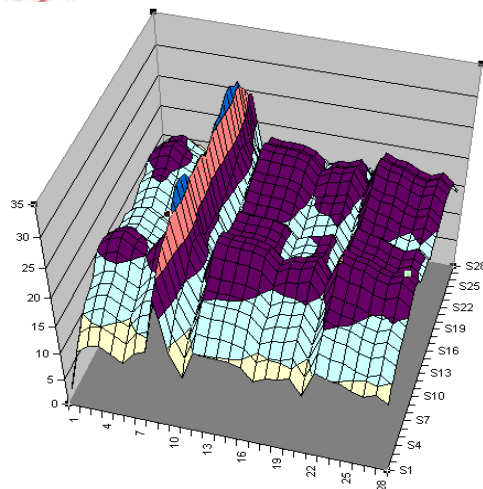
- Spring mounted vs. Hard mounted sensor

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# Laser Properties





# Liquids

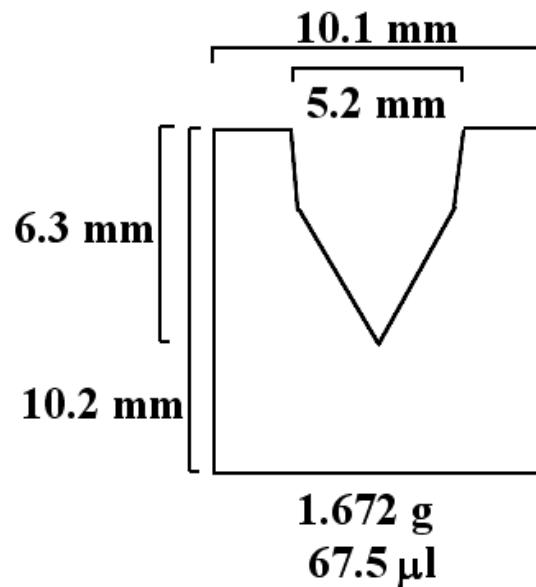
	Hexane	Ethanol	Isopropanol	Acetone	Water
Chemical Formula	$C_6H_{14}$	$C_2H_5OH$	$C_3H_7OH$	$C_3H_6O$	$H_2O$
Absorption Coefficient ( $cm^{-1}$ )	$\sim 0$	17	67	$\sim 100$	$\sim 3300$
Absorption Depth ( $\mu m$ )	large	574	149	78	3
Density (g/ml)	0.66	0.79	0.785	0.790	1.0
Molecular Weight (g/mol)	86.18	46.07	60.10	58.08	18.02
Enthalpy of Vaporization (kJ/mol)	28.85	38.6	39.85	29.1	43.99
Surface Tension (dyne/cm)	18	22.3	21.7	23.7	73.05
Viscosity (mPa-s)	0.3	1.07	2	0.306	1.002



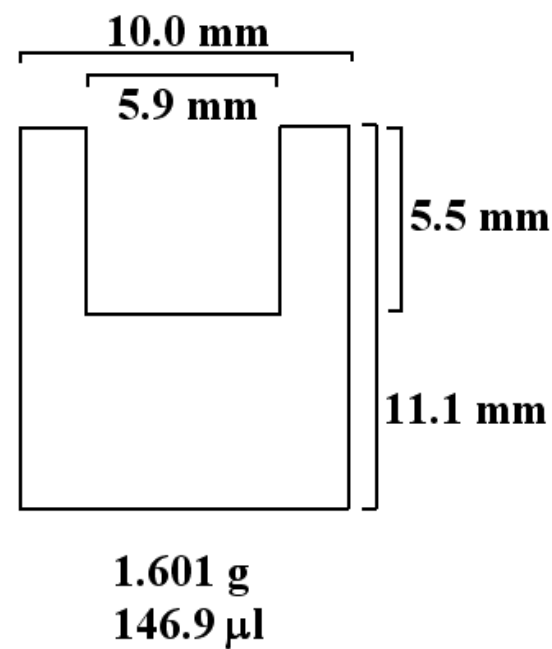


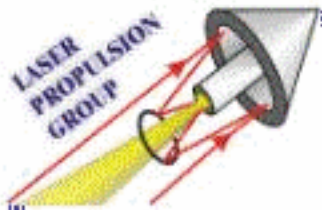
# Quartz Target Containers

Cone



Cylinder





# Surface Distortion

