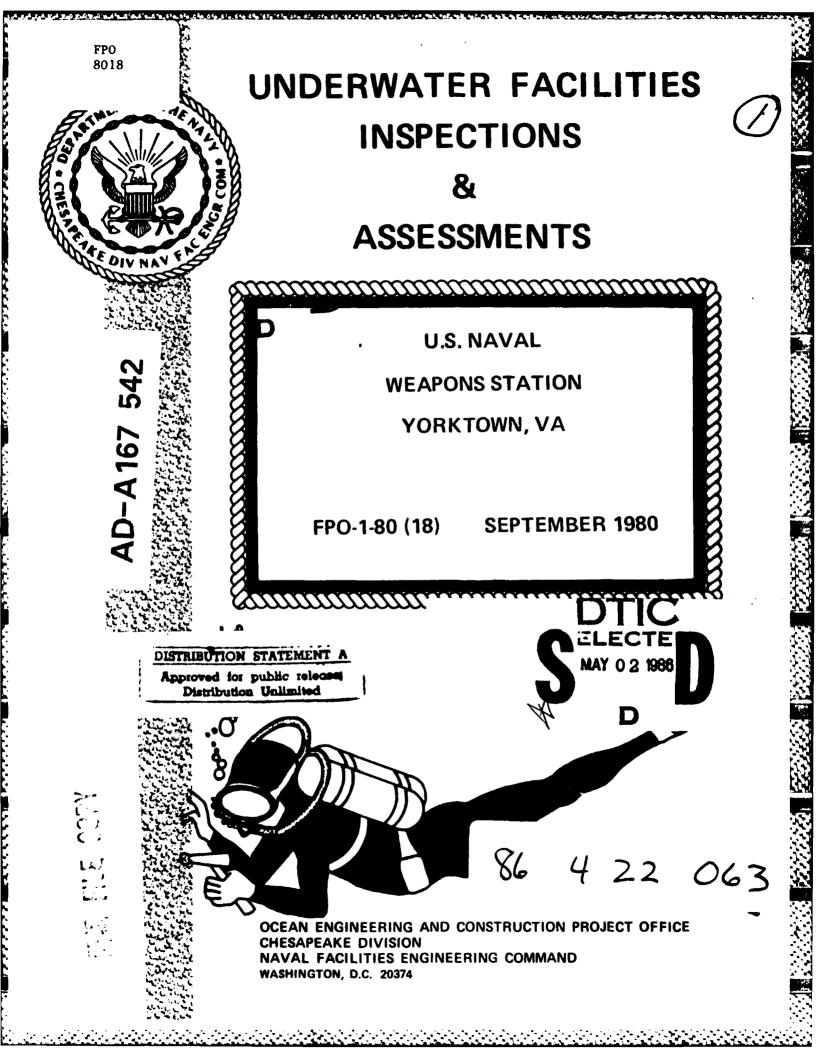
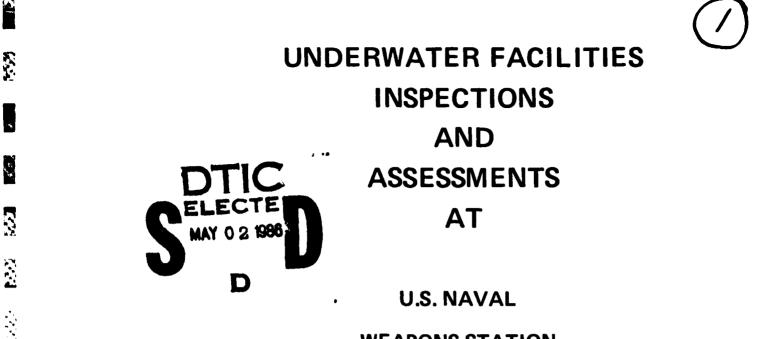


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WEAPONS STATION

YORKTOWN, VA

FPO-1-80 (18) SEPTEMBER 1980

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PERFORMED FOR:

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OCEAN ENGINEERING AND CONSTRUCTION PROJECT OFFICE CHESAPEAKE DIVISION NAVAL FACILITIES ENGINEERING COMMAND WASHINGTON, D.C. 20374

UNDERWATER INSPECTION BY:

UNDERWATER CONSTRUCTION TEAM ONE (UCT-1)

REPORT PREPARED BY:

DOTY ASSOC! ATES INCORPORATED ROCKVILLE, MD 20850

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FOREWORD

The scope of the inspection at the U.S. Naval Weapons Station, Yorktown, Virginia, and the detail to which it was performed and reported was tailored to the conditions at this This report is not intended to be a standard for facility. underwater inspections or reports covering other activities. Attempts are being made, however, toward establishing standards for procedures and reporting formats for underwater inspections and assessment reports. Through these standards, inspections performed by different persons or activities on different facilities under a wide range of conditions, can be effectively compared. It is expected that the inspection and assessment of the Weapons Station, Yorktown berthing facility, like previous operations mandated underwater by the portion of the Specialized Inspection Program, will contribute significantly toward achieving that objective.

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The choice of the level of inspection to be conducted is dictated by an engineering judgement and the quantity of work, constrained both by time and personnel support available. Accordingly at Yorktown, VA, a Level I - General Visual Inspection, was conducted by UCT-1.

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Executive Summary

The objective of the underwater facilities assessments the U.S. Naval Weapons Station, conducted at Yorktown, Virginia, was to provide a generalized structural report and assessment of the principal berthing facility at that activity. That facility is the R3-Fleet Weapons Pier (Wharf) which is the only facility used to load and unload ammunition to and from ships and lighters.

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This report documents the findings of a Level I underwater inspection conducted on 8-15 September 1980 by Underwater Construction Team ONE (UCT-1), with technical guidance and direction by the Ocean Engineering and Construction Project Office (FPO-1), Chesapeake Division, Naval Facilities Engineering Command.

The inspection was limited in scope to a Level I investigation using visual and/or tactile means of examination, providing still photographic documentation where feasible. The inspection objective was to provide a general assessment of the structure's physical condition documenting any mechanical, biological, or corrosion damage, with emphasis on any advanced stages of deterioration.

Because of the huge amount of piles in this structure, over 4600, a random sampling technique was primarily employed to select and inspect about ten percent of the piles, with heavier emphasis on the older sections of the wharf.

ii

Executive Summary (cont'd)

Overall the piles within this facility were rated as being in good condition. In general a greater number of piles within the new section (percentage wise) were rated in good condition with only 3 out of 192 piles rated as fair. The older section of the pier face and approach trestle have some piles which require immediate attention to prevent further deterioration and structural damage, as detailed in the report. These 13 and 20 piles out of 195 were rated fair and poor respectively.

No sections were observed to have advanced structural deterioration or damaqe such that the pier's structural capacity or function should be downgraded. In the southeast corner of the old pier face some structural damage was observed and the old approach trestle has piles, pile caps, and stringers in need of prompt repair to prevent further deterioration, erosion, and loss of structural integrity as described in a previous inspection report by Abiousness Cross and Bradshaw, Inc.

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INTRODUCTION

SECTION 1

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This report is a product of the Underwater Inspection Program conducted by the Ocean Engineering and Construction Project Office (FPO-1), Chesapeake Division, Naval Facilities Engineering Command (NAVFACENGCOM) under NAVFAC's Specialized Inspection Program.

This program provides for underwater inspections of the structural portions of piers, wharfs, bulkheads and other waterfront facilities as needed or required in order to determine the total facility conditions and to report the results of such inspections, so that repairs can be scheduled and completed.

A structural facility assessment is made in those cases where the inspection indicates such need.

1.1 TASK DESCRIPTION

The scope of work required under this portion of the program provides a general structural assessment of the findings, including repairability recommendations of the underwater portions of the Fleet Weapons Pier, Structure R-3, at the Naval Weapons Station, Yorktown Va, as a result of the inspection conducted 8-15 September 1980.

1.2 REPORT CONTENT

In this report the inspection procedures, results of the inspection, recommendations and analysis of the findings are addressed. The principal berthing facility at the Naval Weapons Station is described as to its location, function, construction, and current condition as assessed by this inspection. Recommendations for further inspection and repairs are included. As supplementary information, a brief 1.10.11.11.1

description of the Naval Weapons Station is provided, including its history, mission, existing facilities, hydrographic, and topographic features. SECTION 2

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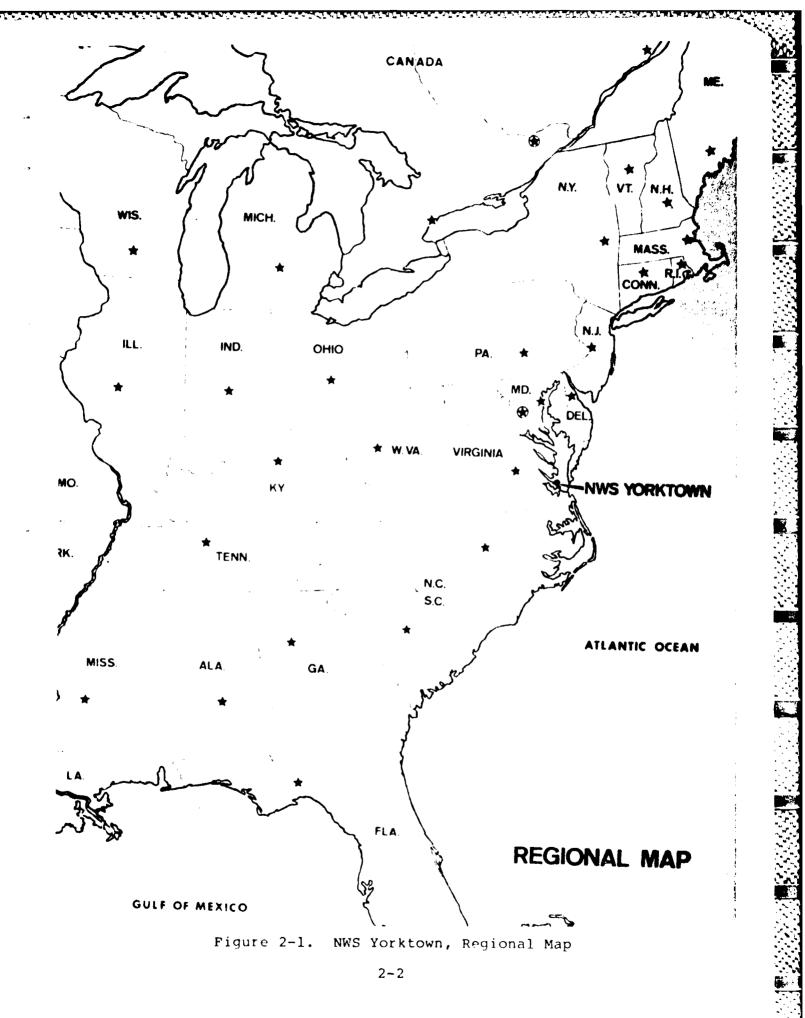
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The purpose of this section is to provide a general description of the Naval Weapons Station, Yorktown, Virginia. Included in this section will be brief discussions of the Naval Weapons Station's location, mission, history, existing facilities, climatological and meterological data and This information is provided to supplement the hydrology. later sections of this report and to support all considerations necessary to accurately assess the structural condition of the waterfront facility inspected in this survey.

2.1 LOCATION OF ACTIVITY

The Naval Weapons Station, Yorktown, Virginia is located in Southeastern Tidewater Virginia as shown in Figure 2-1. The Weapons Station is located on the western shore of the Chesapeake Bay on a peninsula formed by the York and James This historic peninsula contains the renowned triangle Rivers. formed by Williamsburg, Jamestown, and Yorktown. At the peninsula's southern end is Newport News, known for its shipbuilding and port facilities. Adjoining Newport News is the city of Hampton. Established in 1610, Hampton is the oldest English-speaking settlement in continuous existence in America today. Langley Air Force and Fort Eustis are also on this peninsula.

The Naval Weapons Station Yorktown fronts on the York River as can be seen in Figure 2-2. The peninsula may be reached on land via Interstate 64, U.S. Routes 17 and 60, and Virginia Routes 143 and 238. The Weapons Station is approximately 80 highway miles from Richmond, the capital of Virginia, 180 miles from Washington D.C. and approximately 30 miles north of Norfolk, Virginia. The Weapons Station is located near the town of Yorktown. It is bounded on the west by the U.S. Naval





2-3

Supply Center's Cheatham Annex, on the north by the Colonial Parkway and York River, on the east by agriculturally zoned private lands, and by Interstate Highway 64 on the south.

2.2 MISSION AND COMMAND ORGANIZATION OF NAVAL WEAPONS STATION, YORKTOWN

The mission of the Station as assigned by NAVORDINST 5450.17A of 16 January 1969 is: To receive, store, overhaul, test, modify, explosive load and accomplish such other work as necessary for the production, issuance, and maintenance of mines, torpedoes, depth charges, other underwater weapons, bomb type munitions, rockets, guided missiles, and other expendable ordnance, conduct high explosive research and development applying to production, loading, assembly, and test procedures; and to perform other weapons engineering tasks as assigned by NAVSEASYSCOM.

The Station under the command or cognizance of the Commanding Officer is structured to implement its mission with 13 departments, two special assistants, and eight component commands. Detailed functional descriptions may be found in the Station Organizational Manual.

2.3 HISTORY OF THE NAVAL WEAPONS STATION

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In 1917, a search was initiated by the Naval Ordnance Command to locate, on the Atlantic Coast, a site for the establishment of a weapons handling and storage facility. The basic criteria was: (1) a sheltered inland deep waterway, (2) a sparsely populated area sufficient in size to provide quantity-distance separation for explosive materials, and (3) close to the Naval Base at Norfolk.

A site was found on the south bank of the York River about four miles upstream from Yorktown. The U.S. Mine Depot, Yorktown was commissioned on 1 July 1918 to support the laying of mines in the North Sea during World War I. The property, with a history dating from early Colonial times, was obtained by Presidential Proclamation on 7 August 1918. During the twenty years following World War I, the depot received, reclaimed, stored, and issued mines, depth charges, and related materials. During World War II new plants were completed and torpedo overhaul facilities were added. In 1944, an ordnance research and development laboratory was established.

The U.S. Mine Depot, now designated as a U.S. Naval Weapons Station has continued to support the fleet with more modern and sophisticated weapons including special weapons, guided missiles, rockets, and bombs. The station serves as the central design agency for explosive loading, processing, and documentation for all weapons and weapon component explosive loading.

The Naval Weapons Station Yorktown currently contains 10,522.99 acres (16.44 square miles). This acreage was acquired over a period of 55 years, beginning with the original parcel of 11,433 acres. Subsequent transactions have, by acquisitions and dispositions, reduced the Station area to its present size.

2.4 WATERFRONT FACILITIES

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The Naval Weapons Station fronts on the York River. The York River is formed at the confluence of the Pamunkey and Mattaponi Rivers and extends for approximately 30 miles before emptying into the Chesapeake Bay. The river averages two miles in width but narrows to half a mile at Gloucester, just before emptying into the Chesapeake Bay. The river provides an excellent and well-used commercial and pleasure waterway with a channel averaging 50 feet in depth and rising to 37 feet at its mouth. Most of the tanker and fuel barge traffic (approximately 1,200 ship operations) terminate their voyages downstream of the Weapon Station and the Coleman Memorial

The commercial vessels utilizing the York primarily Bridge. have drafts ranging up to 31 feet. In addition to the commercial river traffic, numerous pleasure craft of all sizes continually sail/motor up and down the river. The largest naval vessels which are currently accommodated at NWS Yorktown are the fast combat support ships (AOEs). Due to the restrictions of the pierside depth, capital ships are limited to designated naval anchorages east of the Coleman Memorial Bridge at Gloucester.

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Support of Fleet requirements for conventional and special ordnance is accomplished by "over-the-pier" off/on loads and by barge deliveries to the explosive anchorages located near the Naval Station, Norfolk. Wharf operations are conducted from the only waterfront facility existing, the Ammunition Wharf.

The NWS Ammo Wharf extends into the York River and is located one and one-half $(1 \ 1/2)$ miles west of the Coleman Memorial Bridge at Yorktown. The wharf is U-shaped, of concrete construction, and has approximately 2240 feet of berthing on the outboard face. The northwestern leg of the wharf has a lift span bridge enabling barges, lighters and service craft to moor on the inboard side of the wharf. Ordnance off/on loading operations are performed by a 25-ton capacity, track mounted, mobile crane or by any of three truck-mounted, 19-ton capacity cranes. A smaller wooden pier, just east of the ammo wharf, is currently used for recreational purposes. An aerial photograph of this facility as attached as Figure 2-3.

A dredging operation was performed on the outboard face area of Pier R3 in September 1980 to a depth of 42 feet below the station low water datum. A post dredging survey completed in October 1980 confirmed the minimum depth to be greater than 42 feet along the outboard wharf face for its entire length.

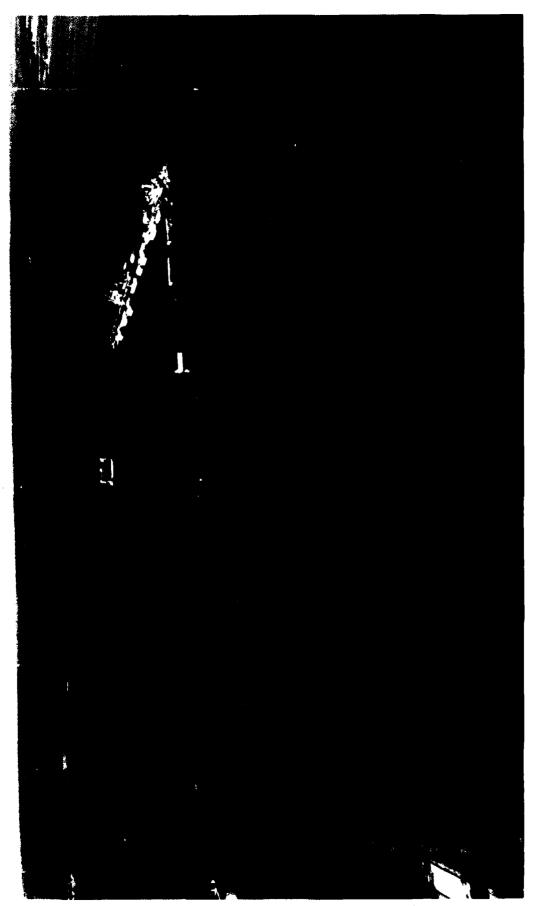


Figure 2-3. NWS Yorktown, Facility R3 Fleet Weapons Pier

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2.5 CLIMATOLOGICAL AND METEOROLOGICAL DATA

The Peninsula weather is generally moderate with average temperatures ranging from $41^{\circ}F$ in January to $79^{\circ}F$ in July. Precipitation is well distributed throughout the year with the heaviest rains occurring during summer and early fall. Snowfall averages nine inches a year and occurs chiefly in December and January.

2.6 TOPOGRAPHY AND HYDROLOGY

NWS Yorktown is located in an area with slightly rolling hills; elevations vary from 5 to 80 feet above sea level with occasional steep slopes occurring at the river banks. The rolling terrain forms natural watershed areas, controlling and channelizing surface drainage. The soil varies from sand to clay with several inches of friable wood and leaf mold in wooded areas. Marshy wetlands occur frequently along the banks of the area's many lakes and tidal inlets.

2.7 TIDES

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The tidal ranges on the York River, measured in reference to Mean Low Water (chart datum) are:

> Mean tide range 2.4 feet Spring tide range 2.9 feet

INSPECTION PROCEDURE

SECTION 3

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3.1 LEVEL OF INSPECTION

From 8 through 15 September 1980, a team of divers and technician/divers from UCT-1 performed a Level I on-site underwater inspection of selected piles at the Fleet Weapons Wharf, Yorktown, Virginia, to provide a general assessment of its physical condition. Visual/tactile observations of a pile's condition at mudline, mid-depth, and splash zone levels were performed. In addition, pile caps and stringers were observed and photographed from a small boat.

3.2 DEFINITION OF LEVEL I INSPECTION

Level I underwater inspections assess the general condition of a structure utilizing visual/tactile inspection techniques. In an open-type structure, this assessment generally consists of a close inspection of all exterior vertical and batter piling (exclusive of fender piles) and some percentage of the interior piling as well as a check for gross structural deterioration on all remaining piles. For bulkhead-type structures, visual/tactile observations of the structure's condition at mudline, mid-depth, and splash zone levels are performed. This level of assessment is designed to give a general condition assessment of the structure and should identify any areas that have been mechanically damaged or are in advanced sites of deterioration. Visual documentation (utilizing underwater television and/or photography) and limited physical measurements must be sufficient for documentation of the findings.

3.3 INSPECTION PROCEDURE

Before each section of the approach trestles and piers were inspected, as built drawings were consulted and bents and pile locations were marked off. For ease of computations and

verification, the structure was divided into sections, each corresponding to an expansion joint, nominally every 30 bents. Each section was then progressively examined by divers and tender/note takers who recorded observed details for future reference and analysis. The diver, starting at a known location, reported the result of each pile inspection upon completion to the tender who verified the bent location and pile number. Direct diver to tender communication permitted simultaneous transmittal of data.

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This coupled with a pneumofathometer, allowed not only the noting of any damage but the exact depth at which it occurred. Divers also noted not only depth, type, and extent of damage but also the pile face on which it occurred.

The inspection plan called for only a selected inspection of the piles in the pier. Both time and cost constraints necessitated this approach because of the huge amount of piles in this wharf structure, approximately 4627. The plan called for a random selection of both bent and pile number to be inspected within a pier section to achieve a 10% sampling of piles within the whole structure. This random selection process was completed before the inspection commenced and the diver and tender/notekeeper proceded together from a known bent/pile to the next bent/pile to be inspected using the as built drawings as guides.

The inspection covered the zone that began at the mudline, went through the submerged, tidal, and splash, zones. In addition, a team in a small boat made a cursory visual inspection of pile caps, stringers, and under deck portions of the wharf structure to verify data from a previous above water inspection report. Photographs were taken above and below water to show representative conditions. Standard underwater photography was not used because of extremely poor visibility,

however with the use of an underwater camera coupled with a clear water box, some successful photography was achieved although this equipment is still under development. All fendering systems, pier utility systems, and expansion joints were not within the scope of from this inspection, and thus excluded.

3.4 INSPECTION EQUIPMENT

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Specialized equipment used during the inspection included: Nikonos underwater camera with strobe, clearwater viewing apparatus, dive lights, folding rule, chipping hammers, calipers, dive knives, Mark 1 surface supplied dive system, pneumofathometer, and a diver/surface communication system. SECTION 4

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FACILITIES INSPECTED

The only waterfront facility in use by the Fleet at the Naval Weapons Station, Yorktown, Virginia, is the Fleet Weapons Pier (Wharf), Facility R-3, which fronts on the York River. This wharf is U-shaped, of concrete construction, and has approximately 2240 feet of berthing space on the outboard face.

4.1 DESCRIPTION

A sketch of the Fleet Weapons Pier R-3 appears below as Figure 4-1

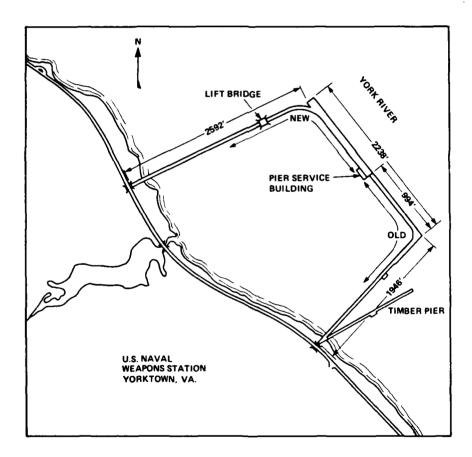


Figure 4-1

The southern approach trestle, Bents 1-163, and southern pier face section to Bent 252 were built in the 1941-1942 era. The approach trestle is 1946 feet long and 24 feet wide, widening to 33 feet in the outer third. This leads to the old pier face which runs from bents 164-252; it is 994 feet long and 42 feet wide. The northern sections consisting of an approach trestle and a wider pier face were constructed in 1964. These join the old southern section to form a U and wharf. The newer wider pier section is 1244 feet long and 93 feet wide. It extends from Bents 245-350 and contains the Pier Service Building. The northern approach trestle, containing a lift bridge is 2592 feet long and 24 feet wide. It consists of bents Tl at the outboard end to T 140 at the land end. Both approach trestles and the wharf frontage include railroad tracks on the deck.

The total wharf length, of the old and new sections joined, is 2238 feet frontage on the York River with depths alongside of 42 feet (October 1980). The wharf has a track mounted 25 ton capacity mobile crane as well as truck mounted 19 ton capacity mobile cranes.

4.2 PRIOR WATERFRONT FACILITY INSPECTION

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A structural inspection was made of the Ammo Wharf, R-3 by Abiousness Cross & Bradshaw, Inc. in April 1978. This structural inspection did not include any of the underwater aspects, nor the buildings, electrical, plumbing, or railway systems on the pier. It consisted of an examination of the pier decking and below the deck above the waterline by boat.

The report is significant in that it reported prior repairs in the original segment of the pier to the pilings, pile caps, and stringers and the fact that these repairs had failed in some areas. It also reported that many of the expansion joints were in various stages of deterioration and

recommended repairs. The stringers supporting the edges and rail beds were reported as cracked in many areas. Pile caps showed moderate deterioration in many locations, including numerous cracks in areas that had been previously patched. The report also stated that some earlier repairs to the piles showed new cracks and surface deterioration.

Similar conditions to those noted above were observed during the September 1980 inspection by UCT-1 and are depicted in the attached photographs.

4.3 OBSERVED INSPECTION CONDITIONS

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As discussed in Section 3.3., piles were randomly selected for inspection. Appendix A contains the pile plans for the entire Fleet Ammunition Wharf, in which inspected piles are designated by blackening the pile. The reader may refer to the pile plan for each section. The plans are labeled by Bent Number and pile number. Appendix В contains the pile inspection data sheet which contains additional data on the piles inspected. Both appendices may be referred to in order to locate the position of bent and piles referred to in the following remarks and photographs. The pile numbering and designation system used followed the same one shown on the as built drawings. Where no system was indicated an arbitrary pile designation system was set up.

4.3.1 Southern Approach Trestle (Right side), 855 Piles, Bents 13-161.

The inspection commenced on 8 September 1980 at the right approach leg. This approach trestle section, built in 1941-42, contains 161 bents and 855 piles, see pages A-3 through A6. A total of 97 piles were inspected in this section for a 12 percent sampling. The inspection commenced at Bent 13 as the lower numbered bents were on land or in the beach approach

This older section, because of prior repairs, contains area. many piles with concrete jackets surrounding the original piles and wooden forms covering the concrete jackets, (see Photograph Overall these wood forms were structurally intact but 4-1).precluded an inspection of the physical or structural integrity of the pile beneath the form which extended to the mudline. In those cases where it was possible to inspect the piling below the wooden form such as Bent 42, pile P-6, where the wood jacket stopped 2 feet above the bottom, concrete aggregate and spalling were observed on all four corners causing rounding of the pile. Similar deterioration was observed in Bent 54, BP-4, and Bent 62, BP-4 where rebar was exposed in both instances. 21 jacketed piles were inspected. In future inspections some of the wooden jackets should be removed from the piles to check conditions of the underlying concrete pile.

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On the piles inspected which did not have wood forms, evidence of spalling, exposed aggregate and cracks were commonplace with hourglassing being present on several piles. (Photos 4-2, 4-3 and 4-4). Photograph 4-3 is an extreme example of loss of cross sectional area at Bent 25, P6. A good deal of the observed erosion was in the splash and tidal zones. Other similar conditions were observed underwater. Moderate marine growth was observed on many piles, in other cases the marine growth was minimal (Photos 4-5 and 4-6).

In addition to the pile inspection conducted by the divers, a visual inspection of the piles, pile caps and stringers was made by small boat. This section of the wharf had been repaired at some unknown time in the past. The revealed numerous of inspection areas cracks, exposed aggregate, exposed rebar both in the original structure and in areas which have been repaired previously. Photos 4-7, 4-8, 4-9, and 4-10 show evidence of conditions observed and is typical along this approach trestle. No serious structural



Southern approach pier, old section

Typical wooden forms over previously repaired piles



Photo 4-2

Southern approach pier bearing pile

exposed reinforcement mesh, failed repair area



Southern approach pier

Bent 25, Pile 6, showing hourglassing, exposed rebar and aggregate.

Pile cap shows cracks in section with prior repairs

Pile 5 this bent has similar conditions underwater

Photo 4-4

Southern approach pier

Batter pile, typical, showing bleeding rust, cracks, and spalling



Southern approach pier

Bent 106, pile 7 spalling and exposed aggregate



Photo 4-6

Southern approach pier

Bent 156, pile 8 marine growth, cracks, spalling all faces.



Photo 4-7

Southern approach pier Cracks and bleeding rust in areas of prior repairs along pile caps. Indicative of corroding rebar which will lead to further cracking and then spalling.



Photo 4-8

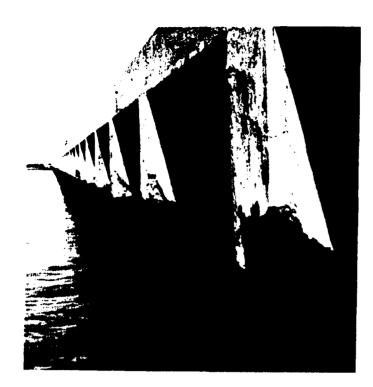
Southern approach pier

Cracks in pile caps and stringers in areas of prior repairs.

D le al

Typical erosion of piles

4-8



Southern approach pier

inboard side cracked cap ends exposed aggregate rebar showing.

Wooden forms visible around piling (previous repair)



Photo 4-10

Southern approach pier

typical cracked stringer

Fishing pier visible in background

failure areas were observed, however it is recommended that repairs be made in those areas where structural integrity would be impaired over time by further deterioration and erosion.

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Of the 97 piles inspected in this section 79 or 81% were rated in good condition. Twelve (12) piles were rated as fair condition, and six (6) piles were rated as poor condition. (See Table 4-1 below)

Table 4-1

Inspection Results, Southern Approach Trestle

<u>Fair Piles (12)</u>					
Bent 42, P6	Bent	83,	P 5		
Bent 46, P5	Bent	89 E	3P7		
Bent 51, BP7	Bent	91 B	3P4		
Bent 62, BP4	Bent	106	BP7		
Bent 64, P4	Bent	139	BP7		
Bent 76, BP4	Bent	156	P8		
Poor Piles (6)					
Bent 25 P5	Bent	62,	BP4		
Bent 25 P6	Bent	66,	P5		
Bent 54 BP4	Bent	76,	P6		
The above piles, locations			_	the	
first scheduled for repair	and mai	ncena	ance.		

4.3.2 Old Wharf Section - (South End) 823 piles, Bents 164-252.

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This pierhead section is of the original construction period in 1941-1942. It is 994 feet long and 42 feet wide. (see page A-6, A-7, A-8) The underwater inspection revealed conditions typically similar to those found in the southern trestle. approach Evidence of spalling, minor cracks. abrasion, exposed aggregate, and corrosion of rebar was seen. No exposed rebar was found in this section and only moderate marine growth was observed. The worse deterioration was Characteristically the most observed in the splash zone. severe deterioration is found in this region of concrete structures.

A total of 98 piles were randomly selected and inspected in this section giving an 11.9 percent sampling size. Clearly the most critical damage was found in 12 outboard batter piles located in the first 12 bents starting from the corner identified on page A-6, as bents 164 through bent 175. Each batter pile has a crack which runs around the perimeter of the The crack is roughly 2 1/2 feet pile across all four faces. down from the pile cap and could have been caused by ship impact damage or overdriving the pile during construction. The fact that the 12 cracked piles are in adjacent bents tends to support the collision damage assessment. Photographs 4-11, 4-12, and 4-13 show examples of these cracks, their apparent penetration across the entire pile, and their location relative to the pile caps. Photo 4-14 shows an adjacent bearing pile with vertical and horizontal cracks.

It was not possible to determine the interior defects caused by these cracks which apparently run through the entire cross section almost perpendicular to the piles length. These cracks were observed by inspection via small boat and no similar cracks were observed in adjacent bearing piles. A more complex inspection and examination of all piles in this area is recommended so that repairs can be initiated.

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Of the 98 piles inspected in this section, 82 were in good condition, 1 was in fair condition and 15 were considered in poor condition (most of these are the batter piles discussed above). See Table 4-2 for a listing of observed damaged piles.

Table 4-2

Inspection Results, Old Wharf Section

<u>Fair Piles (1)</u> Bent 171, BPl				
Poor Piles (15)				
Bent 164,	Pl	Bent	168,	BPl
Bent 178,	P2	Bent	169,	BPl
Bent 178,	BP1	Bent	170,	BPl
Bent 164,	BPl	Bent	171,	BPl
Bent 165,	BPl	Bent	172,	BPl
Bent 166,	BPl	Bent	173,	BPl
Bent 167,	BPl	Bent	174,	BPl
		Bent	175,	BPl



Cracked batter pile.

Outboard corner-old section

Bents 164-175 typical

Photo 4-12

Cracked batter pile.

Typical bents 164-175 outboard corner-old section

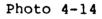


Photo 4-13

Cracked batter pile

Outboard corner-old section

typical bents 164-175



Cracked bearing pile.

Vertical and horizontal crack, bleeding rust, exposed aggregate and spalling

4.3.3 New Wharf Section - (North End), 239 piles Bents 245-350.

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This new section, constructed in the 1964 period, is approximately 1244 feet long and 93 feet wide on the deck; the width of the wharf face at the pier Service Building is 118 feet. See pages A-9 through A-14. Each bent contains at least 22 piles, two of which are batter piles. Blueprints of the wharf revealed that bents 245-252 in this section have the same numbers as bents in the old adjacent section, this numbering was adhered to in both Appendices A and B.

The inspection revealed little damage. The vast majority of piles and the underside areas of the wharf were rated as good. Of 164 piles inspected, 161 were rated as good, and 3 piles were rated as fair. Photograph 4-15 is a worse case example found in this section. The photograph shows a batter pile exhibiting cracks, exposed aggregate and spalling at the waterline. There were no piles rated as poor. Pile caps and stringers all appeared structurally sound and in good condition both by underwater inspection and a visual inspection by boat.

Table 4-3

Inspection Results, New Wharf Section

<u>Fai</u>	r Pil	es
Bent	245,	P22
Bent	304,	P22
Bent	314,	P13



Photo 4-15

Northern wharf section (new). Worse case bearing pile showing cracks, exposed aggregate.

4.3.4 Northern Approach Trestle (Left Side), 558 piles, Bents Tl-Tl40.

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The newer northern approach trestle, contains railroad tracks, a lift bridge, and a curved section at the wharf side connecting to the wide newer section of the wharf face. Many of the shoreside approach bents are on dry land. The trestle has a length of approximately 2592 feet and is 24 feet wide throughout. See pages A-15 through A-20. The two left bridge piers contain 30 piles each encased in a large rectangular concrete footing. These were inspected by divers for deterioration, scouring, or any abnormalities and were found to be in good condition. Each bent consists of 4 piles, the two outboard piles are batter piles while the interior piles are bearing piles. Certain bents have a double set of piles with legs forming an A frame or inverted vee. These are shown on the bent and pile plans, Appendix A.

Inspection of piles in this section revealed no defects, all appeared in good condition. Twenty eight piles were inspected for a 5 percent sample. Bents 127-140 were not inspected as they were in mud, sand, or dry land.

4.4 SUMMARY OF INSPECTION RESULTS

A summary of the inspection efforts in terms of the numbers of piles in the various wharf sections, and the percentage inspected, is shown in Table 4-4. While the pre-inspection objective was to achieve an overall sampling of 10 percent, on-site conditions dictated a heavier sampling in the two older sections, with a concurrent reduction in sampling the newer sections. This was necessary due to time, cost, manpower and scheduling constraints.

	Ta	ble 4-4		
Inspection	Summary,	Sampling	Level,	Percent

Section	Bents	Piles	No. Inspected	% Inspection
Right side approach Trestle (SE)	1 - 163	855	97	11.3
Right side old wharf (South)	164 - 252*	823	98	11.9
Left side new wharf (North)	245*- 350	2391	164	6.8
Left side approach pier (NW)	T1 - T126	558	28	5.0
TOTALS		4627	387	8.3

*both old and new sections have bents numbered 245-252

The conditions of the piles inspected as a result of the underwater inspection is shown below in Table 4-5. It is noted that over 90 percent of piles inspected were rated as good.

Table 4-5

Pile Condition Summary (Pile Condition - Inspected Piles Only)

	EX	GOOD	FAIR *	POOR	TOTAL	REMARKS
Rt side approach T.		79	12	6	97	Repair as indicated.
Rt side old wharf		82	1	15	98	(12 Batter piles
[[cracked)
Left side New wharf		161	3		164	
Left side approach T.		28			28	
Totals		350	16	21	387	

*Repair is warranted

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Of the piles inspected, those rated in the poor category were all in the older two sections. The majority of the poor piles were concentrated in the southern outboard face of the old pier section where the twelve batter piles were found cracked.

4.5 RECOMMENDATIONS

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The inspection results, based on the sampling of piles within the Weapons Wharf, revealed that the wharf in general is in good condition. While this rating presents a favorable picture of the facility on the whole, it must be pointed out that deterioration and degradation of piles within the structure as noted indicate the need for near term repair and maintenance.

It is recommended that batter piles within the older wharf face from bent 164 to bent 175 be repaired. Each of these piles exhibit cracks transversely across each pile face at the location from 2-3 feet below the pile cap. The cracks appear to penetrate the total cross section of the pile. These piles are listed in Table 4-2.

Repairs are also recommended for those piles identified as in poor condition within the right approach trestle. These are identified in Table 4-1, and on the pile plans in Appendix A, and the pile inspection sheets of Appendix B. Those piles with minor defects similarly identified should also be considered for repair, as should the pile caps and stringers in this section.

If repairs to this facility are omitted or delayed over the near term, pile conditions will deteriorate further. delays would the Extended create need for additional the extent inspections to determine of the progressive deterioration. Such inspections would be outside the scope of NAVFAC's specialized inspection program.

4.6 Repair Methods and Schemes.

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This section is provided to recommend actions which could be taken to alleviate problems found during the inspection. There are numerous repair techniques and products on the market today, the methods mentioned here are not all inclusive.

Repair of cracks, spalling, and general disintegration of concrete piles, pile caps, and stringers as described within the previous sections should be of great concern to the station. These forms of deterioration are of varying size, shape, and degree exposing underlying concrete aggragate, and rebar. Cracks provide entrance to airborne water and water vapor whose presence will give rise to the corrosion of the embedded rebar which will cause spalling and further disintegration of the concrete.

There are several repair schemes that address these problems. Epoxy cement is typically used to repair cracks. Above water it can be readily applied by hand, and can also be pressurized to fill hard to reach voids and cracks. This type of bonding agent provides high strength and durability in the marine environment.

Repair of spalled or disintegrated concrete is usually handled the same way. Two methods commonly used are mortar patching and pneumatically applied concrete. After proper cleaning of the surface and rebar either method can be used. Mortar patching is easily accomplished when an epoxy is used. This allows ease in applying overhead, vertical, or horizontal surfaces. Pneumatically applied concrete or mortar (also called gunite or shotcrete) is used in applications where deterioration is relatively shallow. It also can be used with ease in applying overhead.

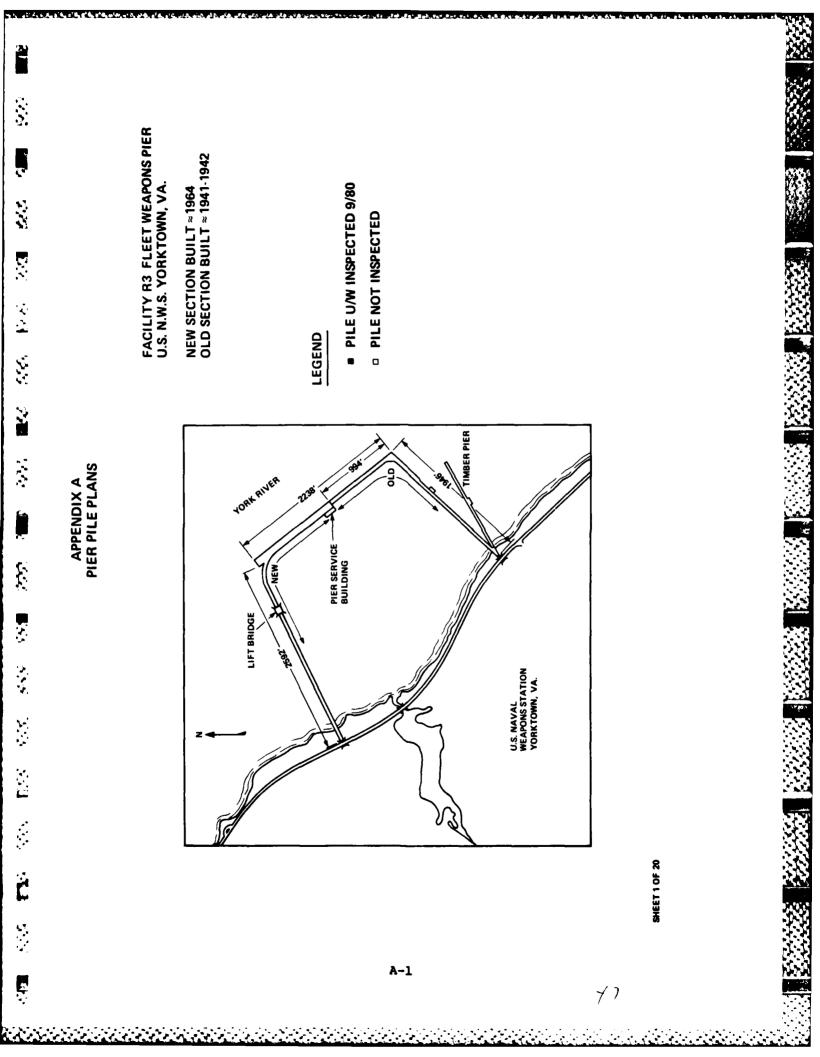
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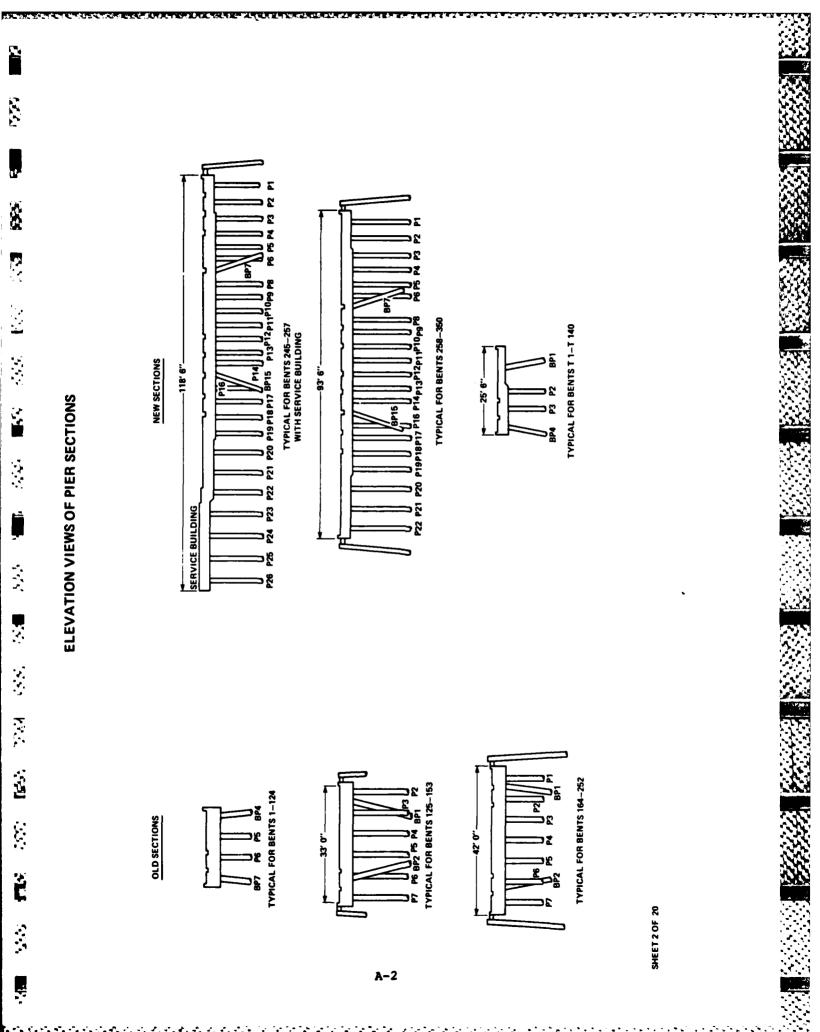
The principal technologies for repair of severely damaged concrete piles (rated poor) is to jacket the pile with reinforced concrete. This is particularly useful where damage is found underwater.

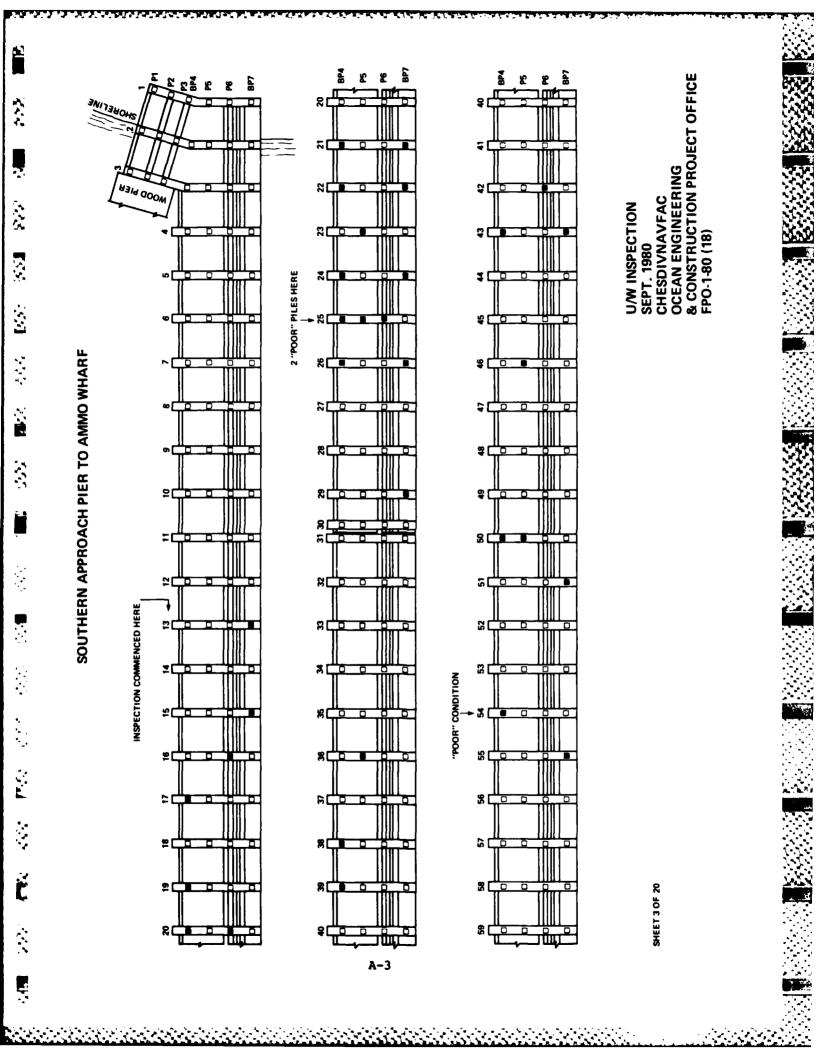
4.7 Estimated Repair Costs

Repair costs associated with the aforementioned repair techniques are order of magnitude estimates only and vary somewhat geographically. These costs are tabularized for ready reference and comparison.

	Description	Fixed Cost*	Unit <u>Cost</u>	Unit Installed
Α.	Repair of concrete pile by placing new reinforcing and form- work around the out- side of the pile and filling the space between the pile and the form with concrete	Included in unit installed cost	\$70/LF to \$110/LF for forms and concrete; \$10-\$15/LF	Symons Z-Bead Fiberglass jackets - manufacturer's installed cost
в.	Mortar patching of spalled concrete piles	Included in unit installed cost	\$13/sq. ft.	Sikastix Epoxy Gels
c.	Filling cracks in concrete piles with epoxy grout	Included in unit installed cost	\$900.00/ crack	Concrete Injectomatic Systems
D.	Covering damaged concrete with pneu- matically projected concrete (shotcrete and gunite)	Included in unit installed cost	\$10/sq. ft.	Per square foot of concrete-in- place
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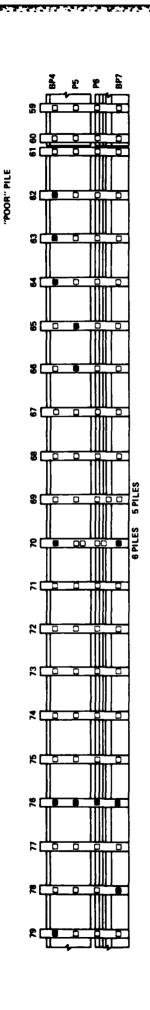


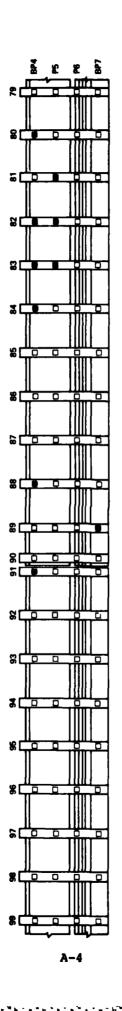


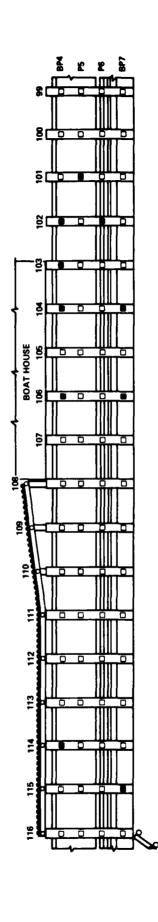












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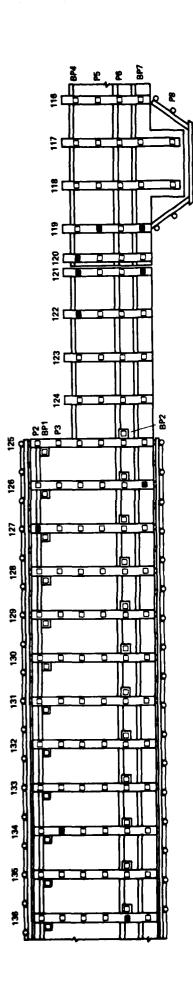
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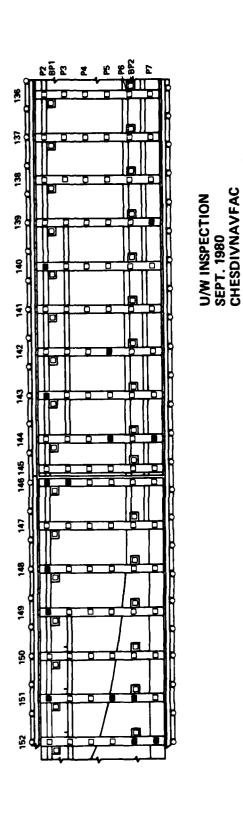
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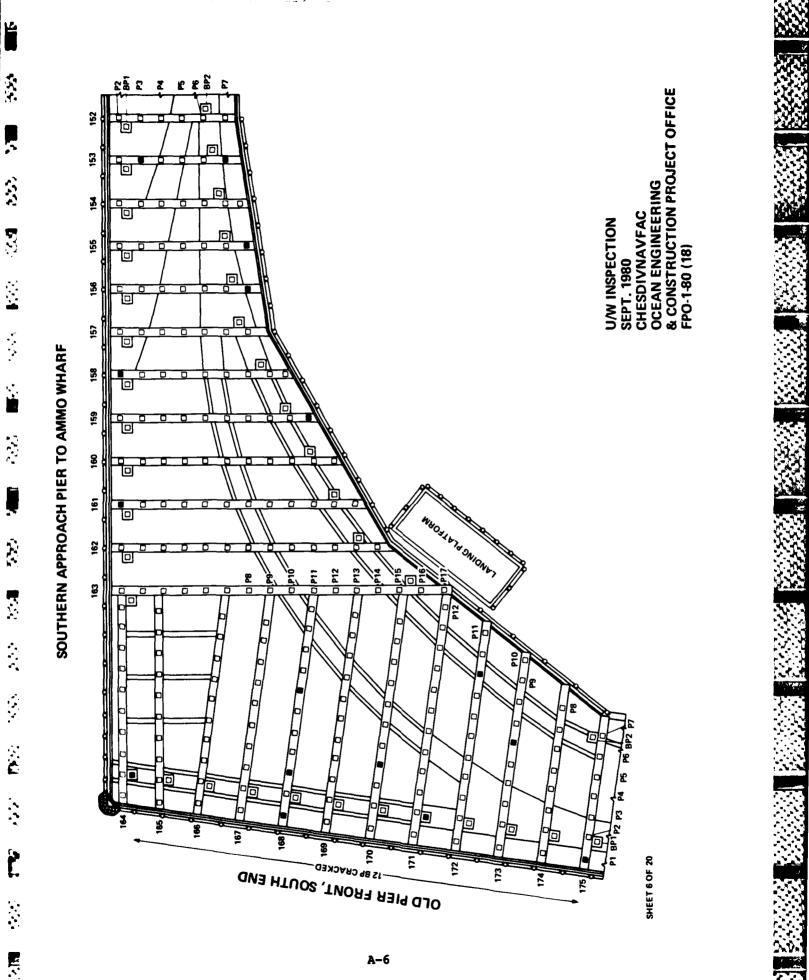


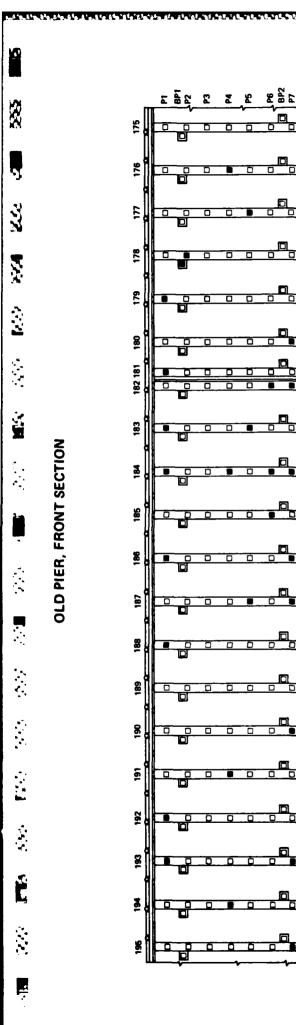


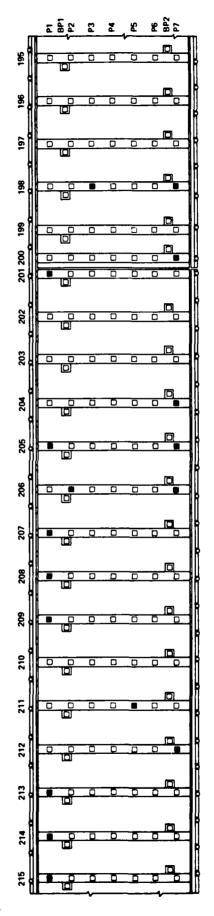


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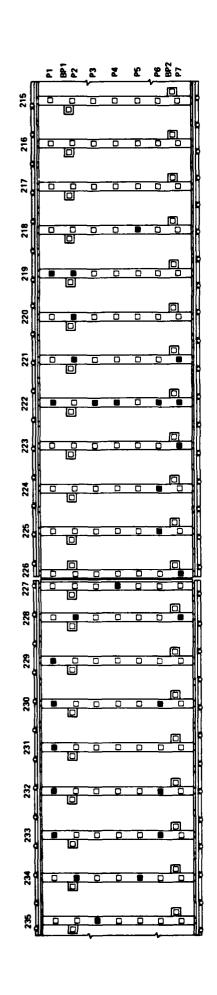
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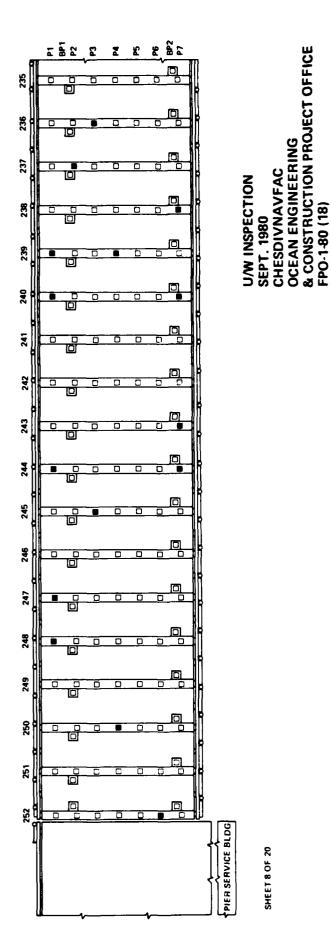
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SHEET 12 OF 20

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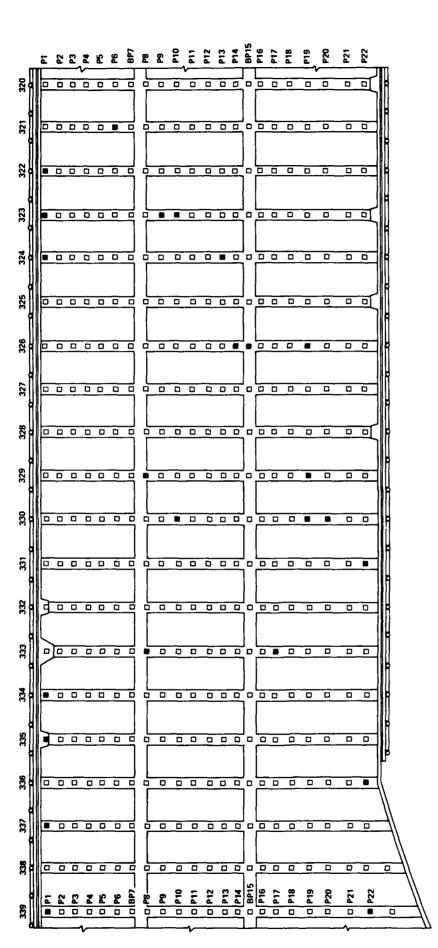
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U/W INSPECTION SEPT. 1980 CHESDIVNAVFAC OCEAN ENGINEERING & CONSTRUCTION PROJECT OFFICE FPO-1-80 (18)

SHEET 13 OF 20

NEW PIER, FRONT SECTION, NORTH END

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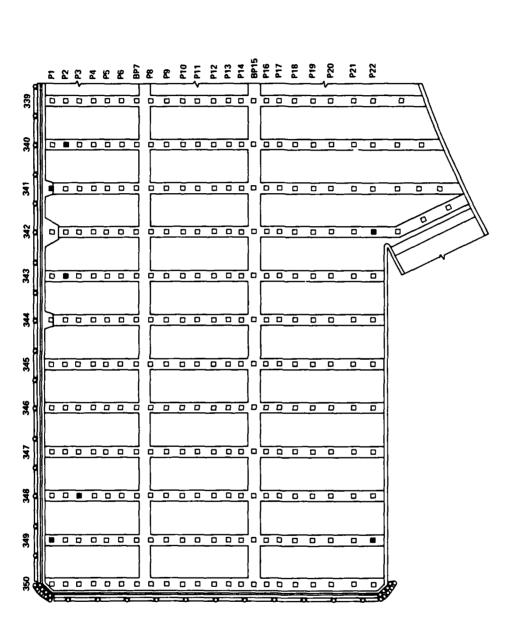
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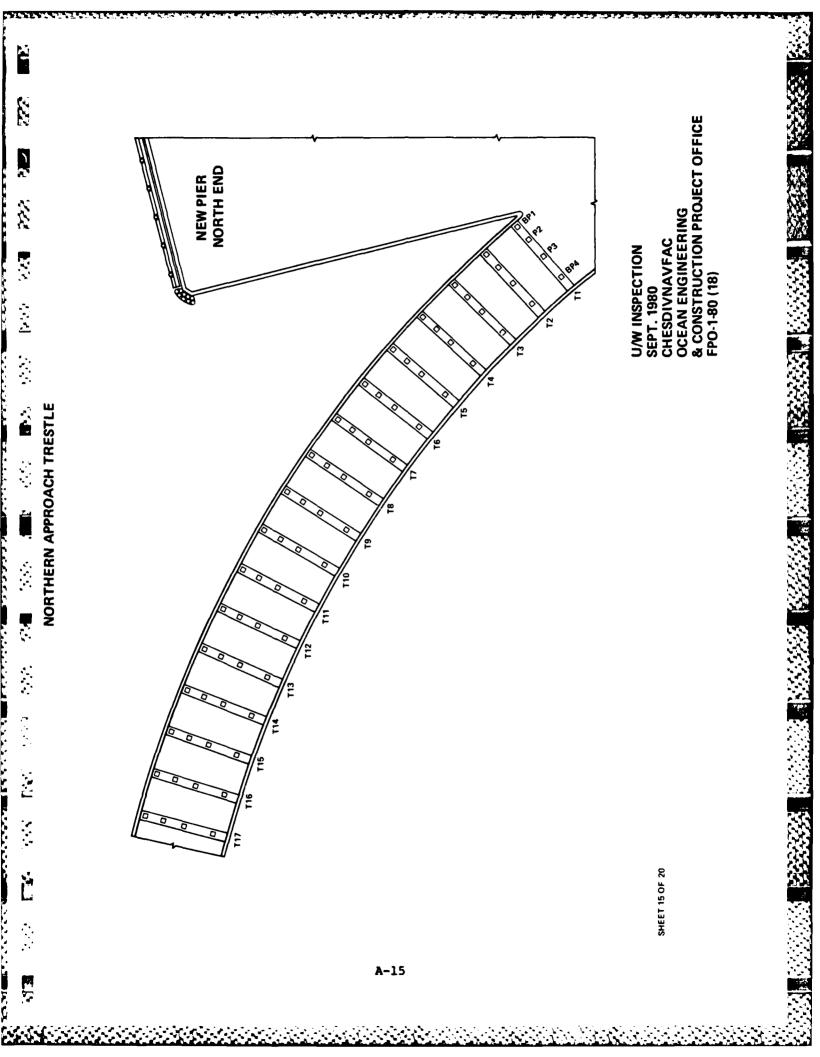
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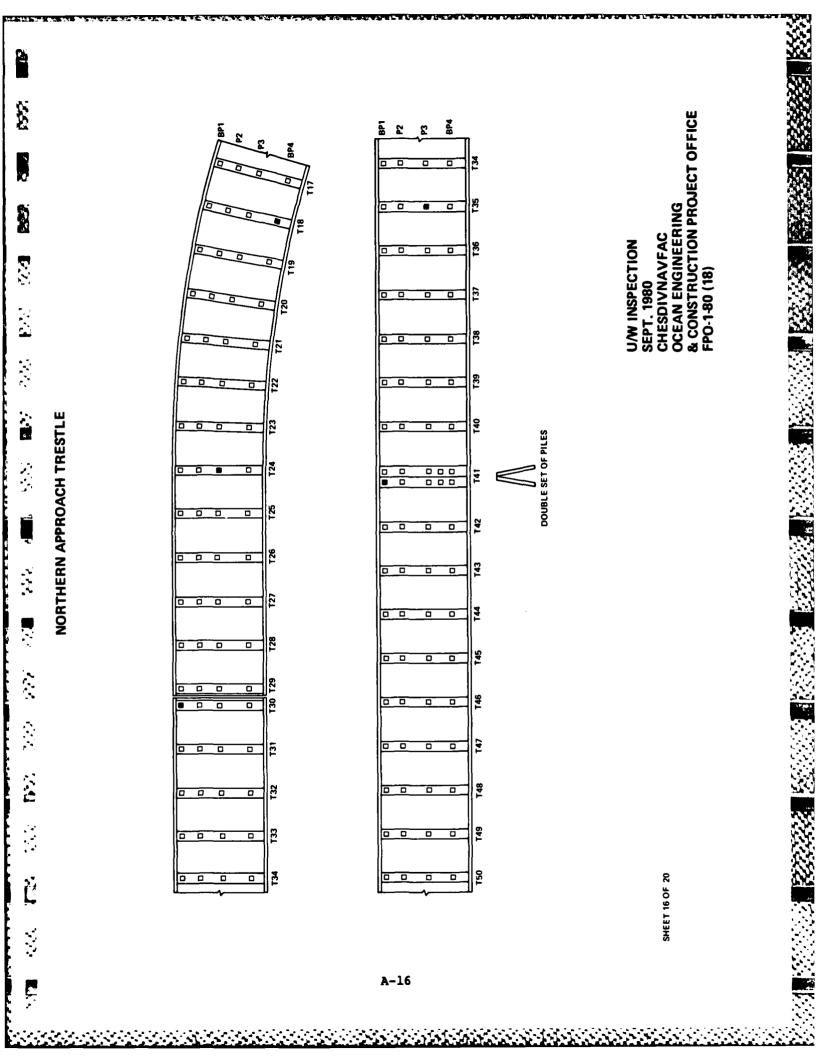
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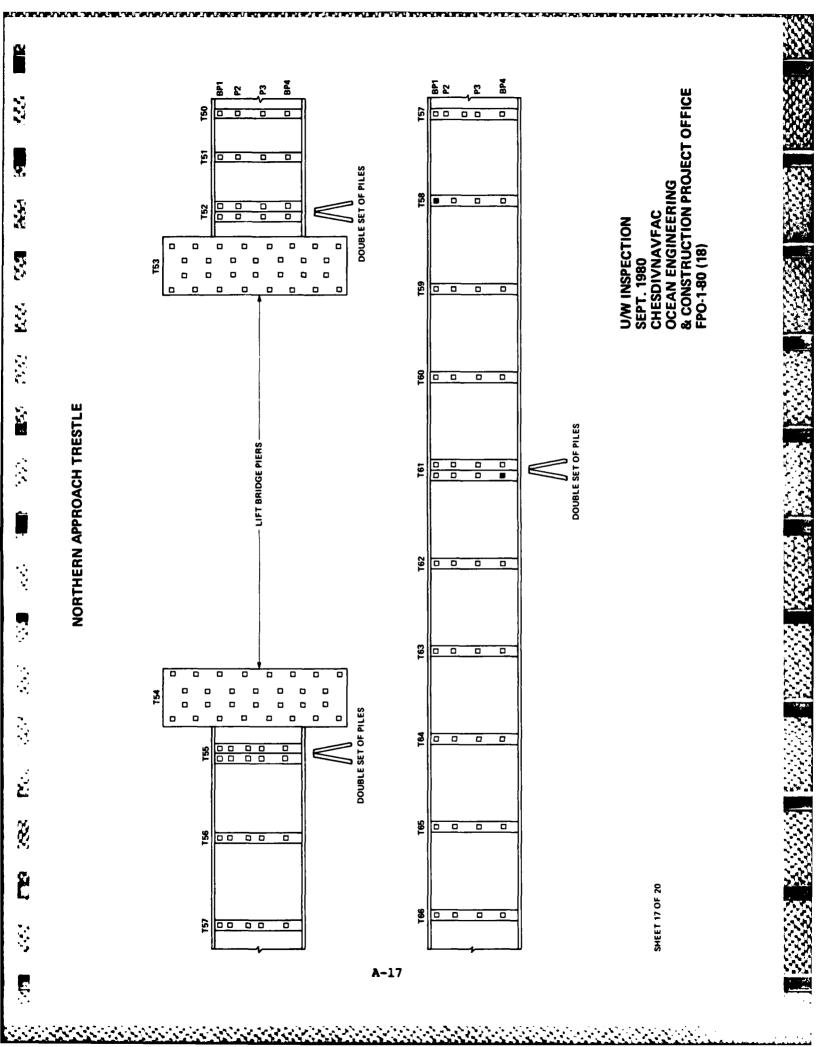


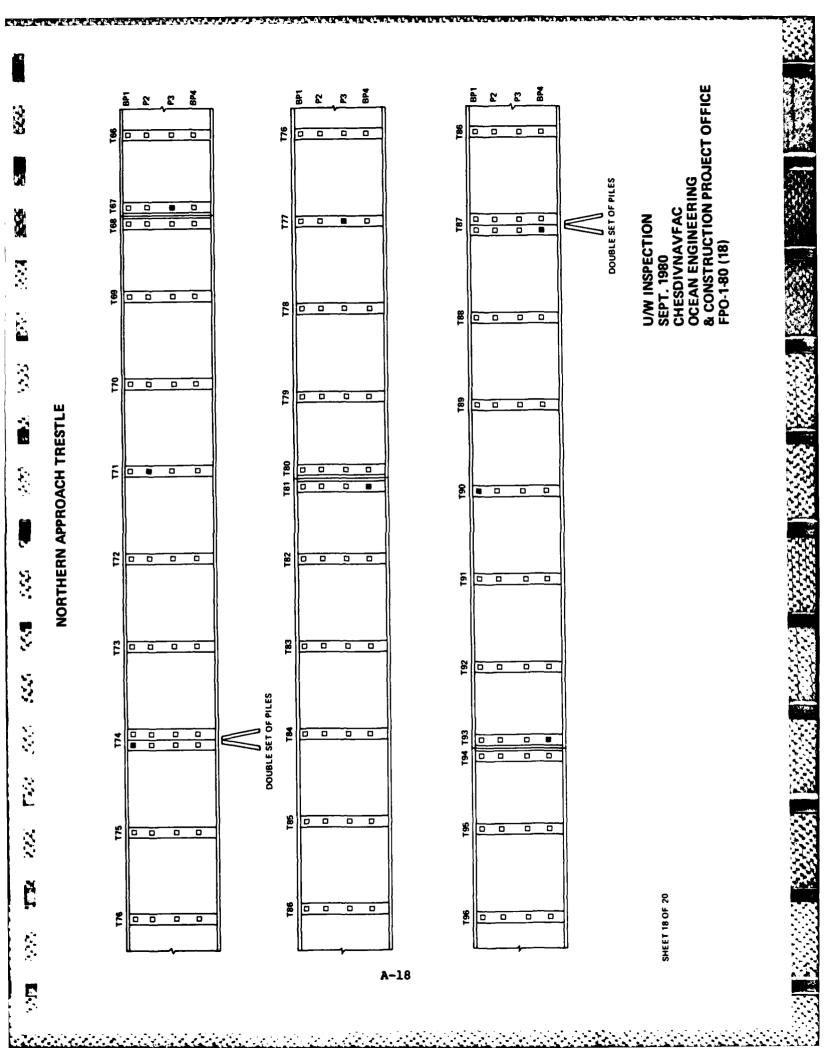
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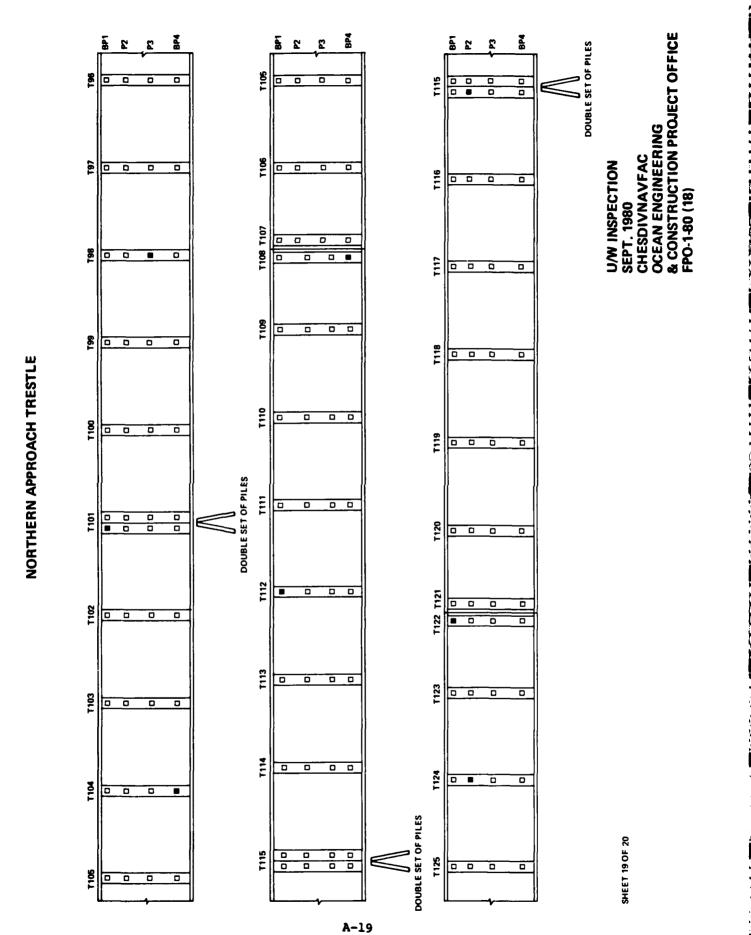
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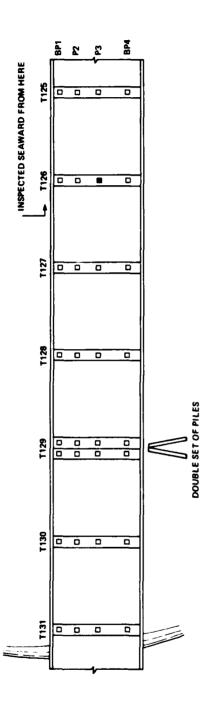
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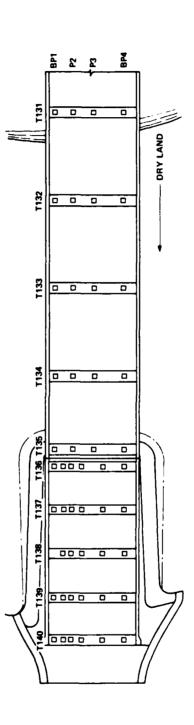
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-		TIME OF DAY: 2022	777 : XVC	Z TIDE:			PTH 0!	DAMA	GE FRO	DEPTH OF DAMAGE FROM DATUM =	1 = GAI	GAUGE DEPTH	1	TIDE]-	
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	61	824									,				5	eroch form in fing Shap
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1156	22	824													× °	extends to much live

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	FAC PILE TINE	NAME/ 3 MATE	FAC NAME/NO. Fleef Wous Pre- PILE MATERIAL: WOOD STEEL STEEL	wor NOC	woon woon	STEEL	22- 2-3 PILE TYPE: BEARING BA EEL CONCRETE OTHER CONCRETE VOTHER CAUGE D	Z PII	2-3 PILE TYPE: CONCRETE TOTIER	C. 2-3 PILE TYPE: BEARIN	GAUGE DEPTH		TIDE	SHEET WATER DEPTH: /2
BENT	T PILE NO	iz	E G		CONDITION F P	N	TYPE	PE DAMAGE	AGE FUNC	DEPTH DAMAGE		ENSTONS	OF DAMAGE	COMENTS
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64	P-4			×						4				word forms extracts 1' BWL 20%0 het & Loss . hour -
کئ	2-2			×			•						· · · · ·	Wood forms appear to be
66	2-0				×					,11-56			Face 182	would extends 5' u/w ; Den age foces 1 7 2 ; Seve Soul (into ; no ar possed re
20	P-4	-A		×						cé				Would extende to 6' Dorth Dange 2' elore hudline
oŁ	1-28	2		×										wood extends to 51 Dept.
76	BP-4			×										Wand entanels to S' Dopth spections a rud was for
76	P-5			×	~									would extend to 5' 1914
76	P-6				×									5 pelling Face 3 (mullis)
76	<i>E-</i> 78	N.		×										would form astends to 6

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to Cop; Bleeding Rust No wood form on pile form present Pile all ern ettends 5 ¢ d' Spelling Fares ሪ ĥ 6 オリ Spalling FI & F2 ¢ spalling Face 18 2-12 1 - Simons woul for extends No word form C wood form mate way pain No spelling iloundins of Spelling 1=1 Sing COMMENTS no word No voud 2\$3(hood ti/a a/n ź 1.2" 2 "- 3 " 1.2 / DIMENSIONS OF PAMAGE PENETR -/4 -/4 3 Sheet 2 of WIDTH 2 4 HGT Spleik 3 me DAMAGE 2-3' JWG PEPT'H (gauge) 4 AW'L 'n ÷. S FUNC TYPE DAMAGE B10) D'e HD31: FACNAME/NO: 1000000 S PILE CONDITION ρ. × \succ Ŀ × \times ኦ \succ \succ \succ ပ × \succ × \succ × × ы IN 2 82.4 BP-4 BP4 21 102 1-4 12-75 BPA 32.4 15-9 K-d P-4 Sid でん 5-5 BP4 PILE 0N 101 79 BENT NO 10 43 78 80 28 6 83 с, С 6 6 G G M 10-19' 88 4 1027 20 285 Q ,ť/ 4 15

	COMMENTS	Crack 1' 4/n to Pile Cap FA, couch F2	W/ - Pile cap . Spellin	Core F1/4. 0						
a 66 450 h 00 Sheet <u>3</u> of <u>3</u>	DIMENSIONS OF DAMAGE HCT WIDTH PENETR									
s 1	EUNC DEPTH DIM FUNC DAMAGE HGT (sauge)									
s Proc	TYPE DAMAGE MECH BIO FU									
FACNAME/NOT HUPNE	PILE CONDITION	×								
	BENT PILE NI I NO NO E	102 12-6			· · · · · ·					

Sheet of 2 Sheet britter and the sheet of 2 Sheet britter Sheet britter Sheet britter	COMPENTS	No cracks or spalling		NO CONCRS/NO Spelling	Exposed Assage	F-2 Spaling, Cracket Corr Stains . F-4 Aggragete		Correct F1/2 Spalling				
RECORDER (S) : _	DIMENSIONS OF DAMAGE HGT WIDTH PENETR				d" 1″	width uf 2"		,, l ,, l				
A DATA SHEET	DEPTH DIMER DANAGE HGT (gauge)				ю, е,	F-2 4"		Splush 12" 30-00- 8"				
NSPECTI NSPECTI S): <u>SW</u> S): <u>SW</u>	NGE FUNC					AWL		3 %				
U/W 1 DATE: 2522 DIVER(Ver 2-3 PILE T EL CONCRETE DAMAGE	TYPE DAM											
LOCATION: York 5 tak of a DATE: FAC NAME/NO. FLEEF WOOD STEEL	CONDITION F P S					×	 					
FAC NAME/NO. FLEEF W/S	NI <u>FILE</u>	*	×	×	×		×	×	$\boldsymbol{\lambda}$	×	×	
	BENT PILE	103 P-4	104 24	104 P-1	106 24	106 P-7	114 24	115 P-7	119 P.S	2-28 511	120 P-4	
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2	COMMENTS	win. with of express agen	Hairline Contr. Exposed Aggri, Rush Stains along	Exposed aggragate on	· · ·					
2	DAMAGE PENETR									
<mark>- 2</mark> of	DIMENSIONS OF HGT WIDTH		hait		 					
Sheet 2	D LYEN		3							
è	DEPTH DAMGE (gauge)	Splith	Splish	Splash						
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: ⟨<\al \al \al \al \al \al \al \al \al \al	SHEET SWYDER RECORDER(S): W.F. Casey BATTER FENDER SHEET WATER DEPTH: SAUGE DEPTH - TIDE	CONTENTS	exposed agg. (2 7' depth (Nud) At Mudline in F13 2 No exposed Reber; 5% bas	· · · · ·	No worsed aggragate Well	0	F2 Verticul Crick (Longe) Spatting in Spiech gone 3 Verticul criets , Rust Sting	Little Aggragate Scient in Splash gene.				Sravel an Batter	
	JRDER(S): FENDER	F DAMAGE PENETP					12						
	ON DATA SHEET 3/DV JNYDER RECORDER (S BEARING BATTER FENDER [TUM - GAUGE DEPTH - TIDE	DIMENSIONS OF				•	* '						
	G C BA1	├ ──- └ ──					<u>6</u> '-10						
	R	DEPTH DAMAGE (gauge)	,t										
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	и/ <u>10 Sep</u> /niv Z-3 Pill] concrete H of dama	TYPE DAMAGE											
	Kien Ke DATE:/ STEEL	S MECH											
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č	LOCATION: <u>Yer</u> FAC NAME/NO. <u>F</u> PILE MATERIAL: TIME OF DAY: <u>O</u>	III											
hug I V Carton V	LOCAT FAC N PILE TIME	r PILE NO	F-7	P-2	P-3	Ple	827	P.2	P-5	P-2	5-9	1-18	
		BENT 130	126	/27	134	136	139	071	142	143	144	144	
	and a state of the s					18,	151	22	21	20,	5	161	

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SHELT SHELT SHELT SHELT <u>ob ~ 5 for</u> RECORDER(S): <u>w</u> ob ~ 5 for RECORDER(S): <u>w</u> MATTER FENDER SHE JOGE DEPTH - TIDE	F DAMAGE PENETR				z-la z-l4	" " " " "				74 74 = = = =	-/4 -/4	
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12, 3) (F2, 3) ~(L) F-1 C wh to correction the Deap Soulding the Sea presadas ! ant the P Creck around F4 \$ 1 (Com) Spalling; Corr Pust Present Spalling Fift (32.5 4 F) F3/4 Noresion (Hiron) Eringde -F-1/2 Spalling Trenser Mirior Gouge - creek Creek (river) - No F3/4 Creek No rust 3 corner - spelling Orack Criefes in splach going Spelling 12-1; composed a E-2, 3 comor exposed Creek . Cort 4 4 - Faces حداباعم (conter) E1/2 Conver T L COMMENTS Né Scouring AAB Abresien Spelling, (F1 + 2; 3) 73,501293 لاسناكمم creeks معنديم 14 21 レーム F2 / 1-3 n 4 v 11 П 4 ちち ĩ ù こ 人村 PENETR DIMENSIONS OF DAMAGE -/y 2 5 af. 74 2 .Ter /4 ۲ : 4 4 42 42 ん 1274 3 1-44 witte 1" Ce Face Sheet 2 of WIDTH Waft 73-1' ت و Tawit 14° 14 3 32 ¥ 0:0 <u>_</u>4 N 3. ٩ 13" : 8 4 1 ŝ 124 ų, 4 HGT 6 Splest Splash Jowe To Cap **クゴイゴ** كعمامح DAMAGE AWL Spleal 3005 Splech splesh 3526 3000 3000 (gauge) Spiech 30000 To Cap reve Splest Barc كملمح JWL کهیا مخ DEPTH 1.44 AWL 205 **>** 1 Ĵ FUNC m TYPE DAMAGE Ř BIO ι Die . NECH Wars. _ Ś CONDITION \succ \mathbf{v} FACNAME/NO: 4 \succ × \succ FILE × \succ × \succ υ × × $\boldsymbol{\times}$ × × × ь: Ľ Z 2-4 ف له P-8 94 1-18 11-d P-9 PILE 2-2 F-7 5 M 2-2 Ч. Ч 37 22 4 164 150 161 24 173 20/1/08 021 172 BENT 155 23 159 21/168 156 22/168 153 Ľ 2231 r,7 31 1303 5 \mathcal{Z} 5 ัก ה

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i ,	PILE NO	P_	P-4	5-9	P.2	<i>вр-1</i>	1-d	P-7	<i>D1</i>							
	BENT NO	175	176	177	178	178	671	nat	181		,					
		<u> </u>		1,3/							· · ·		<u> </u>	.		
2		28,	10	15		- 2	27	, <i>t</i> /	1410							
		$\sim 10^{-1}$									1.15		•			

Sheet of 3	CO:RENTS		Exposed Age F1 & d Spelling F1 & Below Age	5-7 Cry 1 -4							Wonley form Extends To S	
	F DAMAGE PENETR		The eft	3 - 11		i 						
SHEET SHEET TANCAT RECORDER (S SATTER FENDER (S UGE DEPTH - TIDE	DIMENSIONS OF HGT WIDTH			, <i>4</i> "								
A SHEET S TANCAT S TANCAT S TANCAT	DIME		4 Z Z Z Z	5" 6"								
	DEPTH DAMAGE (gauge)		3presh Zore	splesh								
DEPTH OF DAMAGE FROM DATA SHEET	DAMAGE BIO FUNC											
	TYPE D NECH B											
The factor of th	CONDITION F P S											
rent sources sources sources sources sources sources the sources of the sources sources the sources so		X	X	X	×		~			7		
LOCATION: Verpors Si Weapors Si Fac NAME/NO. Fleet W PILE NATERIAL: WOOD TIME OF DAY: 1345 TIDE:	PILE E G				~	У	×-	\times	*	<u> </u>	*	
LOCATION: Yere Fac NAME/NO. E PILE NATERIAL: TIME OF DAY:	IN	. 0					1					
LOCA FAC PILE TIME	T PILE NO	2 26	L-0-	1-1	3 25	1-0-1	404	2-6	201	5-6	1-2	
	BENT 110	162	781	, 133	, 133	104	18, 184	, 124	, 184	185	96/	
n na serie de la companya de la comp		1343	<i></i>	ିକ୍ଷ ଜନ୍ମନାନ) D	22	2 	<i>e</i> :		10	50	

	COMMENTS				les form extracts to selow sur face			der form trikends h Below Surfree							
	AGE ETR				Kone Kone			hond brond							
	S OF DAMAGE TH FENETR														
	DEMENSIONS O HGT WIDTH														
	DAMAGE H (gauge)														
	FUNC														
	MECH BIO														
	s														
	F	×	×	×	×		×		×	×	×	X	×	×	
	E		~	~	~	X		×	×						
	NO NO	ť-	کر	t-d	/-	7	p-4	1-d	1-0	Z-	P-4	t-d	ß	Ľ-	r
` -	NO N	186 P-	187 0-	d tal	1-9 BB1	190 P-7	-d 151	192 P.	193 P	193 2	194 P.	195 P.	6 P-3	198 P-7	ז 0 ייי ג
	ă ⁴	31 ,//	16' 12	,×,	26' 1E	5, 12	18, 19	24' 19		300	12' 19	14/	14' 195	15, 19	10,01

>	COMMENTS				Exposed aggragate facet									
	F PAMAGE PENETR				14									
	DIMENSIONS OF HGT WIDTH				6 1									
	DIME				4				 		.	 		
3	DEPTH DAMAGE (gauge)													
	FUNC													
	DAMAGE BIO											 		
	TYPF. MECH													
	NON S											 		
	CONDITION F P											 		
	FILE C	$\boldsymbol{\lambda}$	×	$\boldsymbol{\lambda}$	×	×	×	$\boldsymbol{\lambda}$	$\boldsymbol{\lambda}$	×		 		
	E N N				· · ·							 		
,	PILE NO	1-d	L-d	12	t-d	2-2	t-d	P_/	1-4	1-0				
	BENT NO	201	204	205	205	206	206	207	208	209		 		
•		24'	/2/	,4	,6	21'	,2	28,	24	28,		 		

R(S):of	COMMENTS	The pile Capit I' u/W	00		Erpused of Corner 3 \$4							
	PENETR											
	SE											
TA SHEET	DIME											
	DEPTH DANAGE (saure)											
	GE FLNC											
X33 X75 X14 Hind U/W Lotte: U/W Lotte: Sechive Lotte: Concrete STEEL CONCRETE	TYPE DAMAGE								} 			
хт: 5 АТЕ: <u>/55</u> е 2,е. 2 Е. П соно ветно от	TYI NECH											
2 733 2 4 1 1 1 1 2 4 1 1 1 1 2 1 2 1 2 1 2 1	CONDITION F P S											
Ris ans St teet W wood [wood [COND E COND	×	×	×	×	×	×	×	×	×	×	
Weepous Weepous : <u>Yurkfer</u> /NO. <u>Fleet</u> ERIAL: WO	E G				_~							
LOCATION: York for (13) 55 Him Incations Station 100 Incations Station (100 Incations Station Vieles) FAC NAME/NO. FLEET WOOD STEEL TIME OF DAY. 093001100 Incot	PILE NI NO	P-7	P_5	P-1	1-4	P-1	P-5	P-1	P-2	P-2	P-2	
	BENT P	212	117	2/3	214 1	215	218 4	219	219	220	172	
		2		11	23	22	2	20	<i>.</i> 6	<u></u>	,Ц	

1											14				<u> </u>	λ. L
	COMMENTS	Erposed aggragate		Expressed agg corner F3/4 Expressed agg corner F2/3							Exposed aggragate F19		Especial aggragate ALL &		Expased and F3 \$ 4	
4	F DAMAGE PENETR															
ct Z of	DEMENSIONS OF HGT WIDTH															
Sheet	DIME															
Ì	DEPTH DAMAGE (gauge)	Splash		JMB							/-		, /-		,/-	
³	FUNC															
J L	DAMAGE BIO															
	TYPE MECH															•
	N S															
	CONDITION F P															
	PILE CO	×	×	×	×	×	$\boldsymbol{\times}$	×	×	×	×	×	×	\times	×	
	NI E				}											•
	PILE N NO	t-d	t-d	p-6	70	P-3:	61	t-d	7-01	Pd	t-d	5-4	2-d	t-d	1-0	ļ
	BENT NO	122	222	222	222	222	222	223	224	225	226	t22	822	228	522	
L /	· · · · · · · · · · · · · · · · · · ·	<i>'el</i>	8.0	12,	3	<u>)</u>	51	13,	13,	12,		<u>13,</u>	, Lt	12	26	,

D	COMMENTS					alt E3 f 4								absangate F3/4	aggragate F-4	
		R				Etpesad a								pusati	Exposeda	
4	OF DAMAGE	PENETR														
1 <u>3</u> of	DIMENSIONS 0	WIDTH														
Sheet 3	DIMEN	HGT													 	
ð	DEPTH	DAMAGE (gauge)				Splesh								Splesh	Splest	<u></u>
2-3	3E	FUNC														
or R	PE DAMAGE															
A)	ТҮРЕ	HECH														
snavi :	CONDITION	P S														
FACNAME/NO:	PILE COND	с С	X	×	X	X	λ	×	X	X	X	×	×	×	×	×
FAC	Id IN	<u>ы</u>														
		0N N	1-d	P-6	P-1	P-I	P-6	1-d	P-6	P-2	P-5	P-3	P-3	P-2	t-d	1-2
		0 N	230	230	231	232	232	233	233	234	234	235	236	237	238	239
:	6		<i>b</i> <i>b</i> <i>b</i>	<u>'</u>	21	22	12,	23	~ =	Ĩ		,4	16	20		5147 239

	COMMENTS					Spalling corror F3/4	Exposed agragate F 2/3								
	DAMAGE PENETR														
	DEMENSIONS OF HGT WIDTH														
	D EMEN HGT														
	DEPTH DAMAGE (gauge)					,7	Splash Zone								
	FUNC														
	DAMAGE BIO														
	TYPE NECH														
	S N														
	CONDITION F P												 	 	
	PILE COI	×	×	×	×	×	×								
	PILE NI NJ	P-4	<u>p-</u>	t-d	1-4		t-d								
ŀ	BENT NO	239	240	240	243	244	244	-						<u> </u>	
L	- <u>-</u>	12	21'	13,	12,21	16,51	12,2	<u></u>	1	1	L	k	J	J	L

				2/3				
8		1		LL L				

or A Start	CONDUTS					zone larks good	o res	ate Erposed	gone OK	aggragate	Joue OK	
Accorner (S):	SIONS OF DAMAGE WIDTH PENETR					Spiesh	flisher Batter 1	6° 1 " Faces 1	Splesh	4" 12" Expresed	ysords	
INSPECTION DATA SHELT INSPECTION DATA SHELT (S) : EPCN DV MARYIN TYPE: BEARING DEATTER TYPE: BEARING DEATTER TYPE: BEARING DEATTER	FUNC DAMAGE HGT WIDT (gauge)						No the piles (7)	splest .		Splesh 2"		
ulter and a concrete	TYPE DAMAGE						man for princip					
LOCATION: Yee pour Station Meepour Station LOCATION: Yee to way Ve DATE: FAC NAME/NO. Fleet Mous Free PILE NATERIAL: WOOD STEEL TIME OF DAY: U30 TIDE. DEPTI	NO E G F PILE CONDITION	P-3 X	P-1 X	P.1	P-4 X	P.6 X	End of Och Segin	P-22	۲-1 ۲-2	PS	P-26 X	
	BENT	15' 245	21' 247	21' 240	14, 250	// 252		14' 245	22' 24	146, 246	17, 246	

agginge Fidel zon side 1 \$2 Exposed agg Splail zone OK 1' Above -2' Below wite Splark gone OK Splerk gove UK Splanl rose OK Splerk gove OK Splark you OK 3, had gove OK Splash zone OK Splesh zone OK Splesh yone OK tore is exposed FACE 344 in COMMENTS 1-1-1 DIMENSIONS OF DAMAGE PENETR Sheet 2 of 4 WIDTH °М HGT * 1 ٢ DAMAGE (gauge) DEPTH Í FUNC FACNAME/NO: LEPONS Die R-3 TYPE DAMAGE BIO MECH S PILE CONDITION **P**-<u>|</u>14 $\overline{\times}$ \succ 0 イ $\mathbf{\mathbf{x}}$ \succ × \succ \succ \succ \succ \succ \times \succ × <u>ا</u>بنا IN 5-28 2-9 P-4 PILE 14, 252 P-25 10' 254 P-24 13' 254 P-21 1-0 10' 253 P-16 51-0 252 247 P-12)-d 251 P-3 252 P-13 5 1 246 ŝ 252 253 253 249 BENT NO [**Z**] 1,01 : 20, 13' 29.45 ,7; 0000 à .61 0 29 5 $\widetilde{\mathcal{S}}$

X225222 Minor Spalling F132 -05 \$1-0 Splerk yourok Hay . 7-10 \$ P-11 ; Splash pile Dehuer Spland gove OR 1/2/201 Sean @ waterlive Spleak gove OK Splach zone OK Exposor aggrosote Splash Zone OK Splash zone OK シントの F192 6 AWL. Splash gove OR Fy C 15 & Cut offs Expose al Age COMMENTS Ertre DIMENSIONS OF DAMAGE PENETR 1w | \$ 44 44 Sheet 3 of 4 HIDIM ej. 1,04 3 [*] ne" m, HGT DEPTH DAMAGE (gauge) Ì e FUNC *2*-3 TYPE DAMAGE BIO FACNAME/NO: Wows Pier MECH \times . 1995 - 20 S PILE CONDITION р. 184 \times υ \succ × \succ メ ト × × \succ × × メ $\boldsymbol{\times}$ \times ш IN Ĺ 259 P-4 15 264 P-6 PILE P-3 257 P-6 258 P-4 22-9 222 2-9 122 262 P-14 262 P-18 263 P-3 260 P-21 262 P-9 261 12-10 263 P-1 0N N 256 BENT NO , <u>i</u>, 1 2915 **`**5) ۍ ۳ 0 0 0 4

2 splesh your ok Splash zone OK Splesh zare ok Splesh gove OK Splest your OK Splash gone ok Splash gave OK Splesh gove OK Splash your OK くらいのとう Splesh your ok Splash gave OK min. Spilling in Ŀ COMMENTS しつべゃく DIMENSIONS OF DAMAGE PENETR Sheet 4 of 4 HIDIM HGT DEPTH DANAGE (gauge) Ð FUNC FACKAME/NO: WOND Pier R. 3 TYPE DAMAGE **BI0** MECH \succ S PILE CONDITION Ч FACKAME/NO: ပြ \succ × × × \succ \times \succ × \succ X \succ X ш IN 54 P-20 PrS 265 P-22 10' 267 P-20 270 P-17 PILE 267 P-19 268 P-10 200 268 12-2 267 P-5 265 P-1 268 12-3 269 P-6 265 BENT NO -5,94,5 22 .16 **Ce** Ũ 5 2

sheet 1 of 3		SHEET WATER DEPTH:	COMMENTS	Splush gove Looks OK	splash yone OK Miror spelling F-3	ł	Splash gone Looks goord	Exposent Agg. F-3 (Minur)	splest your OK	Splushyone ok	splash zone læks good	splesh gone ok	splash gave OK	
ن د. هه	ORDER(S):	FENDER	F DAMAGE PENETR			-/4 2								
	SHEET SNYDER RECORDER(S):	BEARING SATTER FENDER	DIMENSIONS OF HGT WIDTH			44	۰							
		IG SATTER GAUGE DEPTH	DIM			4"								
· Î	H3/DV	BEARIN R	DEPTH DAMAGE (gauge)		BWL	spiest		Splush						
	Hetow UN INSPECTION	2.2. 2.3 PILE TYPE: BEAR L CONCRETE VOTHER	JE FUNC											
	n'n Red DI VI	Z-3 PILE TYPE: CONCRETE TOTH	E DAMAGE BIO											
	V АТЕ: <u>155</u>		TYPE			, 1								
	Station	ster	P S			-								
	town S		CONDITION											
	571	FAC NAME/NO. <i>JELEEL V</i> PILE NATERIAL: WOOD TIME OF DAY: <u>1415</u> TIDE:	PILE E 6	×	×	\checkmark	×	\times	×	×	·×	×	×	
Ċ	LOCATION: Yer	FAC NAME/NO.Z PILE NATERIAL: TINE OF DAY:14	E NI	2	6	7	~	5	0	6	m	4	æ	
E	LOC	FAC PIL TIM	BENT PILE	270 P-22	272 P-9	12-0 ZFZ	273 P-3	273 P-S	273 2-20	274 P-9	276 P-3	276 P.14	276 P-18	
			<u>д</u>	7 2	8	10' 2	21, 2	10, 5	, 1 , 1	10, 2	345	6 8	aí cí	

able an FI 27 spalling corner F3 \$ 4 Agagagate exposed F-A Exposed Ang F-3/4 @ Exposed ASS Corner F3/4. Slight spalling in Jolesh zone or Splash zone OK Spleet gover OK Splash zone or Splash gone OK Spleich zone OK Splash gone OK Splash zone OK splish gove old Spleshgone OK D COMMENTS pmare DEMENSIONS OF DAMAGE PENETR -/4 Sheet 2 of 3 WIDTH 4 4 2 10,2 HGT Splesh DAMAGE (gauge) JONE -6' DEPTH Ù FUNC FACNAME/NO: 12/2 12/2 12-3 TYPE DAMAGE BIO NECH • . S PILE CONDITION 4 <u>ب</u> $\boldsymbol{\succ}$ \succ υ \succ $\mathbf{\lambda}$ × × \succ $\boldsymbol{\times}$ \succ \succ × \succ \succ \succ ĿЛ IN P-4 p-22 7-20 11 284 8-21 PILE P-4 22-2 522 01-2 tt2 550 12-19 15' 2e4 p-2 282 P-1 2-0 232 277 P-1 281 P-13 1-d 02 11/ 202 1 279 275 278 1 282 BENT 53 ,22. 13, à 300 , 30, 25 ,02 .32 á . M ,0

COMMENTS	Splesh gove OK	minor exposed agg	Splash great	Splech zone or	Splash your OK	Splash zone OK	Minur Exposed Ang	Pile Repaired above Nh	Splash Zone OK	Splash Zone OK	Splesh zone OK	Splesh zone OU	splash your UK
OF PAMAGE													
DIMENSIONS C HGT WIDTH												- 	
DEPTH DAMAGE (gauge)							AwL						
DAMAGE BIO FUNC													
TYPE DAW													
TION P S													
PILE CONDITION E G F P	X	X	×	×	Х	×	×	×	×	X	X	×	×
IN				\									
PILE NO	P-3	P-S	1-1	£1-21	p.21	12	2-21	12-22	1-1	1-0	P-10	12-12	6-4
BENT NO	285	286	227	tç2	122 062.	9a2	289	682	0 52	161	291	152	252

			Ľ		22.44					•	Ì,				<u>ب</u>	
		Werpous Station Durch Local Durch Van D	A SINOI	Vers	ting s	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	DATE:	••	r/\\ D1VE	T/W_INSPECTION		DV Peu	111 ewel	La FCO	DV Zeweldercorner(s):	Sheet _ of _2
		FAC NAME/NO. <u>F</u>	AME/N	FAC NAME/NO. FLEET WONS PTER	won [225	7 C	steel Concrete	PILE	PILE TYPE:	e e		EATTEI		BEARTING STATTER FENDER SHEET	SHEET WAJER DEPTH:
		TIME 0	DF DA	OF DAY: 1200 TIDE.	C TID	וור		TH OF	DAMAG	E FROT	DEPTH OF DAMAGE FROM DATES =		GAUGE DEPTH	H - TIDE	DE	
	BENT 140	PILE NO		PILE E G		COXDITION F P	S	TYPE MECH	DAMAGE BIO	FUNC	DEPTH DAYAGE (gauge)	<u> </u>	DIMENSIONS HGT VIDT	IONS OF	DAMAGE PENETR	COMMENTS
,12	243	p-3		×												some exposed assagate ou all A - Faces
ý	293	12.5		×	~											Splesh gover ok
Ġ	243	P-15		×												Splesh gone OK
ó	293	12-14		\mathbf{x}												Splesh your OR
22	294	1-0		*												Splash zone OK
101	294	20		<u>×</u>												Splash zone CK
6	254	P-22		×												Splash goe ok
,¢/	2%	7-4		×												Splash gone OK
۲,	596	P215		$\boldsymbol{\times}$												Spleshzon OK
œ	297	P-/4		×												Splash zone OK

STU	you ok	me OK	one OK	gaver Old	Jone OK	gave CK	gave OR	Jone of	gate expes	ling concertif	zna ole	gone OF	
COMMENTS	Splash ?	zolash zon	Splesh Jo	3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	Spharts	2 years	Splash Jave OK	E ysope	Jone age	miner spal) salas l'	splead '	
PENETR													•
DIMENSIONS OF HGT WIDTH													
DEPTH DAMAGE (gauge)													
DATAGE BIO FUNC													
TYPE DAY													
s													
LILE CONDITION	×	×	×	×	×	$\boldsymbol{\lambda}$	×	X	×	$\overline{\lambda}$	×	×	
II E													
PILE NO	P.IS	P-22	1-9	P-5	p-20	07-Cl	P-21	22-21	P-3	t-d	H11	72-22	
BENT NO	292	258	552	299	259	300	300	300	301	301	301	301	

ç <u>859</u> 200 200 - 830 110 Sheet / of 2	9]	COMMENTS		Spallow		Corr. Stains - No Gracks on F-3	Retar exposed corner					Rest stains & small crack	
	- RECORDER (S) : .	F DAMAGE PENETR		r a			* 1 ²						
	TER PTH	DIMENSIONS OF HGT WIDTH		1 "			12"				;		
	A SHFFT WALES GUGE D	<u> </u>		/*/			* 1						
	A Model and a sheet U/W INSPECTION DATA SHEET Value DATE: ISCATE: ISCATOR (S): Called Diver(S): CM3/OV WALES Steel CONCRETE STEEL CONCRETE DEPTH OF DAMAGE FROM DATUM - GAUGE DEPTH	DEPTH DAMAGE (Rauge)		-15'		Splesh	,t-					splash 300c	
	DEPTH OF DAMAGE FROM DA	ICE FUNC											
	U IIScotbin Z-3 FII CONCRETE TH OF DAMA	TYPE DAMAGE									- 		
	hàu L date: L date: L dette Depti	S MECH			<u> </u>				· 				
1000 1000 1000	we station burn, Va DATE et Nous Pier Wood STEEL	CONDITION F P					X						
		PILE CC	×	×	λ	X		×	×	×	×	×	
Ĉ	Mer Location: <u>Yer</u> Fac name/no. <u>F</u> File naterial: Time of day: <u>L</u>	L.	0				~		0				
	LOCA FAC FILE TIME	BENT PILE	303 P-10	304 P-1	304 P-4	304 P-15	304 P-22	305 p-d	306 P-20	307 P-1	307 P-15	308 P-15	
	an a		m CC	r az	4, 30	ъ С	12,	8, 3	6, 3	24' 30	<i>с</i> , 3с	,t	

÷.,

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	COMMENTS					Spalling	Ø	Minor Spelling	Brithan Spalling					
4	PENETR					-/r 1								
t 2 of	DEMENSIONS OF HGT WIDTH					2"								
Sheet	D LME HGT					3"				-				
Ì	DEPTII DAMGE (gauge)					Splesh 30- e Mudlive		Splash 30~ C	Splitch	> •				
3 Fier K-3	TYPE DAMAGE MECH BIO FUNC													
FACNAME/NO: 1000	PILE CONDITION	×	×	×	×	×	X	X	X					
1	PILE NI E	1-d	2-15	222	P-3	P-20	P-21	P-22	P-10			 		
-	BENT P NO	309 F	309 2	309 2	310 P	310 2	310 6	311 1	3/3 12					
	<u></u>	26	<i>`</i> o	3	20	/2	,2,	, м	1125		• _ • • _ • • _ • •	· • • • • • •	• • • • • •	

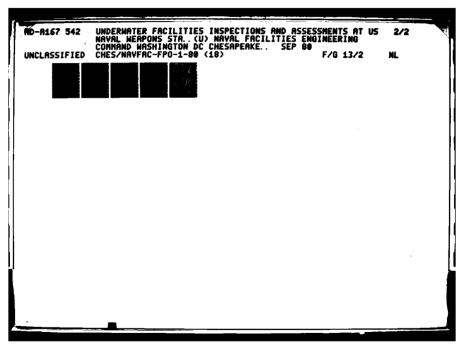
1.01.2

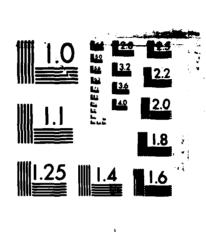
RECORDER (S) : 2 Cas ey	COMENTS		Splesh gove Looks gover cornor Face 192 Churk Missing	0	Splest gove apr	Splash, zone or	Splash zone CK	Splark zone OK	splesh gone OK. Vertical crack, no rust stain(F3)	Hery Marine Growth	Splosh gove oll	
	F DAMAGE PENETI		2''									
H H	DIMENSIONS OF HGT WIDTH		4"						-14		 	
VTA SHEET	DIME		64						m			
A U/N INSPECTION DATA SHEET DATE://See DIVER(S): U/N INSPECTION DATA SHEET DEPTH OF DAMAGE FROM DATUM = GAUGE DEPTH	DEPTH DAMAGE (gauge)		٦,						а́			
U/N INSPECTION U/N IN	AGE FUNC											
. ∵∎ U/1 <u>Z-3</u> PILI CONCRETE H OF DAMA	TYPE DAMAGE											
	S MECH											
	CONDITION F P											
LOCATION: Nerpons 5 LOCATION: Verpons 5 FAC NAME/NO. FLENUL 1 PILE NATERIAL: WOOD P TIME OF DAY: 1230 TIDE.	PILE CON	$\mathbf{\lambda}$	×	×	X	×	×	×	\times	×	×	
LOCATION: Weepons LOCATION: Weepons FAC NAME/NO. Fleet PILE MATERIAL: WOO TIME OF DAY: 1230 TI	NI E	i 										
LOCATION FAC NAME FILE NAT	PILE NO	P-1	P.13	P-19	P-22	22-9	P-3	P-4	P-22	p-3	2-4 4-7	
	BENT 140	314	314	314	314	315	316	319	319	320 /	320	
		30	Ъ,	6	12/	1	,a,	151	13'	je je	۲٦'	

COMMENTS	exposed ago just bolow	vary clear	crossel agragate, shall holes on 1=3. Spiash	Iluston F-3 but no creeks; splash gave tooks ok	Splesh zone OK	expressed aggragate w/	Splesh your looks at	Looks gare in splesh gave	Spliesh gave ok	Spiesh zave OK	Splash zone Ch	Splash give OK	Splush gone OK	50 405 6 Jan UK
F DAMAGE PENETR	: #		14			-14								
DEMENSIONS OF HGT WIDTH	æ,		licross face											
DEMEN	é"		``											
DEPTH DAMACE (gauge)	BUVL		7104	, B-		1JML								
GE FUNC									, ,					
TYPE DAMAGE CH BIO F														
TYI MECH														
CONDITION F P S														
PILE CON	×	×	×	×	×	×	×.	×	×	×	×	×	×	>
E b														
PILE NO	P-22	P-6	1-d	P-1	P-9	P-10	1-2	p-13	P-14	P-15	P-19	P-4	2-8	61-51
BENT NO	320	321	322	323	323	323	324	324	326	326	326	329	329	329
	7	<i>`0'</i>	25	251	e'	210	25	334	a,	7	`ω	<u>`0</u>	6	<i>`</i> ภ

Sheetof	CONNENTS	Splesh gave Looks good	Splash zave Locks Seul F-1 expessed asserbate No rust visible	وندون ع	Splesh gove ok	Splash gene OK	splest zave looks good.	F134 (conver) crack- Little Rustinsible	splash zure ok	Minor spalling F-1	Sphersh zone cul	
Stender (S) :	PENETR		= 72					מל				
ON DATA SHIET ON DATA SHIET 3/DV Zeywolds recorder(s BEARING BATTER TENDER	DIMENSIONS OF		6" Dia					" "				
AUGE DE	DIMENHGT							¢*				
Image: Second Structure U/N INSPECTION DATA SHEFT DATE: 250 DATE:	DEPTH DAMAGE (gauge)		5,					6		Spiesh 30000		
LHigh U/W INSPECTI DATE: 2500 NIVER(S): 5W Low Steel CONCRETE OTHER DEPTH OF DAMAGE FROM DA	FUNC											
U/W P I VE T I LE NCRETE	E DAMAGE BIO											
√ MTE: /25 6/6. 72-3 11 □ CONC DEPTH OF	TYPE											
L L L	P S											
1 - 1000 51	CONDITION	×		×	·		~	· · · · · · · · · · · · · · · · · · ·				
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LOCATION: Yerk FAC NAME/NO. E FILE NATERIAL: TIME OF DAY: []	IN	0	6	0	8		N			2		
LOCA FAC FILE TINE	BENT PILE	330 P-10	330 P-19	330 P-20	331 P22	333 P-4	333 P.17	334 2-1	335 2-1	336 P.22	337 P.1	
•	<u> </u>	<u>in</u> 0	6	9, 33	10, 3	o, m	к, Э	26 431 33		<u>, 1</u>) 6 1 1 1 1 1 1 1	

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Ļ		18,	<u>``</u>	6	21	, e'	18,	25	32,	16,		L	k	d	<u>L</u>





MICROCOPY RESOLUTION TEST CHART NATIONAL BURFALL OF STANDARCE 1993 A

Station U/W INSPECTION DATA SHEET for Val DATE: 115 CPDIVER(S): CM3/DV WALES RECORDER(S): EACN MARYNAK Approach Treste (Let side) Let Wow Pior X-3 PILE TYPE: BEARING SATTER FENDER SHEET WATER DEPTH: 2-4 WOOD STEEL CONCRETE OTHER MALES ENDER SHEET WATER DEPTH: 2-4 TIDE: DEPTH OF DAMAGE FROM DATUM - GAUGE DEPTH - TIDE	DIMENSIONS OF DAMAGE HGT WIDTH PENETR COMMENTS			2" 1" Chip (concrete) corner Face -2 \$3							
SHEET	DIMEN			2"							
U/W INSPECTION DATA SHEET U/W INSPECTION DATA SHEET $LF \neq 5, cd \in $) $LF \neq 5, cd \in $) TLE TYPE: BEARING \Box BA TLE O THER \Box MAGE FROM DATUM = GAUGE D	DEPTH DAMAGE (gauge)							r 			
U/W INSPECTION U/W IN	FUNC										
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COMMENTS			Corver 142										
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DIMENSIONS OF			1"F-1 1"F2										
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