

AO-A164 562

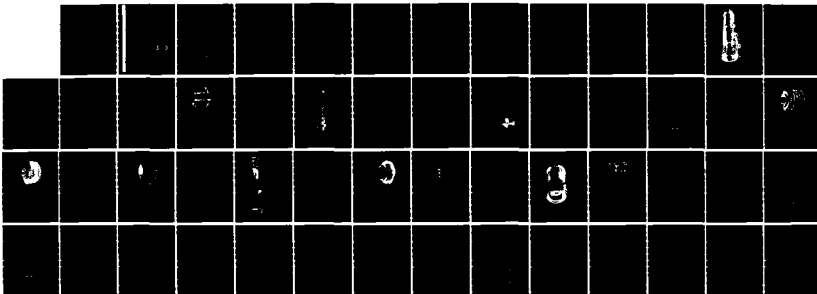
THE GENERAL ELECTRIC F404 - ENGINE OF THE RAAF'S NEW
FIGHTER(U) AERONAUTICAL RESEARCH LABS MELBOURNE
(AUSTRALIA) D FRITH JUL 85 ARL-AERO-PROP-TN-426

1/1

UNCLASSIFIED

F/G 21/5

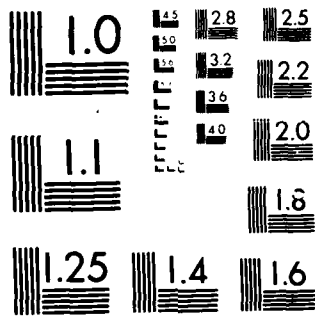
NL



END

FILED

DTL



MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS 1963-A

UNCLASSIFIED

12

ANL-AERO-PROP-TH-426

AR-004-033



DEPARTMENT OF DEFENCE
DEFENCE SCIENCE AND TECHNOLOGY ORGANISATION
AERONAUTICAL RESEARCH LABORATORIES
MELBOURNE, VICTORIA

AD-A164 562

Aero Propulsion Technical Memorandum 426

THE GENERAL ELECTRIC F404 - ENGINE OF THE
RAAF's NEW FIGHTER

by
Denis Frith

DTIC
ELECTE
FEB 24 1986
S D

Approved For Public Release

THE UNITED STATES NATIONAL
TECHNICAL INFORMATION SERVICE
IS AUTHORIZED TO
REPRODUCE AND SELL THIS REPORT

DTIC FILE COPY

(C) COMMONWEALTH OF AUSTRALIA 1985

JULY 1985

UNCLASSIFIED

86 2 21 008

DEPARTMENT OF DEFENCE
DEFENCE SCIENCE AND TECHNOLOGY ORGANISATION
AERONAUTICAL RESEARCH LABORATORIES

AR-004-033

Aero Propulsion Technical Memorandum 426

**THE GENERAL ELECTRIC F404 - ENGINE OF THE
RAAF'S NEW FIGHTER**

by

Denis Frith

SUMMARY

The F404 engine in the F/A-18 is representative of a new generation of military turbofan engines. The features of the engine that govern its performance and contribute to its maintainability are discussed. The intention is to give the non-specialist an appreciation of those factors materially affecting the operation of this type of engine.

Lecture to Melbourne Branch, ROYAL AERONAUTICAL SOCIETY
11 JUNE 1985



(C) COMMONWEALTH OF AUSTRALIA 1985

POSTAL ADDRESS: Director, Aeronautical Research Laboratories,
P.O. Box 4331, Melbourne, Victoria, 3001, Australia.

CONTENTS

	<u>Page No.</u>
INTRODUCTION	1
DEVELOPMENT	2
FEATURES	4
OPERATION	7
CONCLUSION	8
ACKNOWLEDGEMENTS	
FIGURES	
DISTRIBUTION LIST	
DOCUMENT CONTROL DATA	

Accession For	
NTIS CRA&I	<input checked="" type="checkbox"/>
DTIC TAB	<input type="checkbox"/>
Unannounced	<input type="checkbox"/>
Justification	
By	
Distribution/	
Availability Codes	
Dist	Avail and/or Special
A-1	



INTRODUCTION

The new RAAF fighter, the McDonnell Douglas F/A-18 can regularly be seen in the skies over Avalon and will be a common sight around Williamtown and Tindal Air Force Bases well into the 21st Century. This aircraft means different things to different people, even to those in the defence aerospace industry. To the pilot it is a powerful and complex flying machine full of modern gadgetry to be dutifully mastered. To the strategic planner it is a versatile and flexible weapons platform with tremendous potential. The electronics engineer can proclaim that it is a manifestation of the influence of rapidly developing micro computer technology although he will be quick to point out that the hardware is already outdated. The aerodynamicists can point to the influence of the cleanliness of the design on the manoeuvring and range performance of the aircraft. The control man will counter with the importance of the programmable, fly-by-wire control system to operation and behaviour. Materials and structures personnel will emphasise that all this is only possible through judicious choice of advanced materials and structural concepts. The propulsion engineer sees it as symbol of the subtle importance of the engine. After all, the jet engine ushered in the era of the high speed aircraft and effective airliners.

The RAAF F/A-18 Hornets are powered by two General Electric F404-GE-400 augmented turbofan engines, Figure 1. The operation of this engine can be described by referring to Figure 2. The 3-stage fan, driven by the low-pressure turbine, compresses inlet air that subsequently divides into the bypass and core flows. Variable inlet guide vanes schedule the direction of the flow into the fan as a function of rotational speed. The core flow is further compressed for entry to the annular combustor by the compressor, driven by the high-pressure turbine. Variable inlet guide and two rows of stators adjust the flow direction as a function of corrected compressor speed. After expansion through the turbines, the high temperature gas from the combustion process is mixed with the bypass air to form the high speed jet out of the exhaust nozzle. When operating in afterburning mode, the speed of this jet is increased by additional combustion in the afterburner. The exhaust nozzle has variable area to allow afterburning without materially affecting the operation of the core engine. Nozzle area is also varied during non-afterburning operation to obtain optimum performance.

This engine produces over 10,000 lb of thrust in non-afterburning operation while the maximum thrust is in the 16000 lb class. These and other leading figures are listed in Figure 3. For the convenience of those not familiar with the principal characteristics of large, military engines, the values for the Pratt & Whitney TF30, the engine in the F111c, are listed for comparison. In making such a comparison, it should be remembered that the designers of the F404 had the advantage of some fifteen years of advances in the science and technology of engine design over their TF30 counterparts. In addition, they designed against a specification that put greater accent on reliability, durability and maintainability than previously. Figure 3 shows the bald facts. The two engines are comparable in thrust even though the TF30 is 12% longer, 9% greater in diameter, 88% heavier and uses 2% more fuel.

It is natural to wonder how much this affects the operation of an aircraft like the F/A-18. The TF30 could not be fitted into this aircraft because of its size and weight so we can only arrive at a reasonable comparison by considering a hypothetical, scaled-down version of the TF30 for alternative propulsion of the F/A-18. This engine which we may call the TFH30 - the H standing for hypothetical - is presumed to work to the same cycle parameters as the parent engine but reduced in size by 12% to fit the aircraft. Its characteristics are compared with those for the F404 in Figure 4. The most noteworthy point is the reduction in thrust in non-afterburning operation by 20%. The effects of the installation of these hypothetical engines in the F/A-18 are listed in Figure 5. A comparison of this type is based upon a lot of assumptions so I hope that experts will not take issue with the detail:

the intention is to give some indication of how much effect the progress in engine design over the past fifteen years has had on the capability of fighters.

You can see that the range performance of a typical F/A-18 configuration is 6% better with the F404 than with the TFH30. 4% of this is due to the lighter weight of the F404 and 2% because of its better fuel economy, as represented by the sfc, the specific fuel consumption.

The range performance is only part of the story. Fighters are reliant upon their maximum speed to a large extent. A typical configuration of the F/A-18 with F404 would reach a maximum Mach Number about 12% greater than that achievable by the TFH30 powered version when the engines are operating in non-afterburning mode. A lot of this difference in performance is attributable to the difference in power to weight ratio of the two versions. It is shown in Figure 5 that the TFH30 powered version has a 25% lower ratio than the real version.

These figures show the superiority of the F404 over the TFH30 as a propulsor. It is expected that the F404 will also show superior operability, reliability, maintainability and durability over previous engines because of design requirements. An interesting question is what attributes of its design contribute to these qualities. I shall attempt to provide some answers to this question.

DEVELOPMENT

Before doing so it is appropriate to look at the genesis of this engine as it has an important influence on its characteristics. It started out as the YJ101, the General Electric contender for the propulsor for the US Air Force lightweight fighter. Included in the design objectives were stall-free operation, particularly under extreme transient manoeuvres, and afterburner light off and operation throughout the aircraft operating envelope. The performance was optimised for maximum thrust at subsonic altitude combat conditions while a chance was taken in deciding to use three stages in the fan rather than four because of the potential weight and cost advantages. A single-stage, low pressure turbine was selected instead of two stages for similar reasons. The Preliminary Flight Rating Test (PFRT) of December 1973 came after only 1000 hours of running, rather than the more normal 3000 hours, due to the careful definition of the development program. Seven engines were produced for flight testing in 1974 of the YF-17, the fore-runner of the F/A-18. A significant factor in the ensuing 288 flights was the absence of in-flight stalls and blowouts. This test program provided continuously recorded data on engine power usage which yielded, on analysis, information on time at temperature as well as transient throttle movements: information important in establishing life usage of engine components due to low cycle fatigue.

In the period between the YF-17 program and the selection of the F/A-18 as the new US Navy strike fighter, General Electric availed themselves of the opportunity to redesign the engine, to simplify it, to improve reliability and to improve maintainability. An example of what was accomplished is illustrated in Figure 6. 21 fewer parts were employed in the revised C-sump with savings in weight, cost and maintenance complexity. The US Navy then adopted a new approach in setting the requirements for the subsequent full-scale development program. In placing emphasis on operational suitability, reliability and maintainability rather than performance and weight, Figure 7, they included some new elements in the development plan:

- engine power usage definition
- 150 hr. Endurance Test
- Simulated Mission Endurance Test (SMET)
- Accelerated Service Test (AST)
- Failure Modes Effects and Criticality Analysis (FMECA)
- In-flight Engine Condition Monitoring System (IECMS)

The YF-17 flight test program had yielded the first continuously recorded data on engine power usage. The value of this in achieving the desired durability was recognised in formulating the F404 Full Scale Development (FSD) program. The Endurance Test, conducted in the altitude test cell at NAPC, was scheduled to include those regimes important to the F/A-18, including Mach 1.6 operation at 35000 feet, the regime representing maximum severity to engine hot parts. The SMET, based on design mission profiles, was used to demonstrate engine durability and was completed on schedule in July 1980. The AST encompassed 1000 hours of in-flight operation and was intended to prove reliability and maintainability whilst establishing actual mission profiles. The application of FMECA during initial design of the F404 enabled critical problems to be defined and corrected. Reliability features designed into the engine are summarised in Figure 8.

Comprehensive testing of the engine was carried out in sea-level and altitude test cells during this development program. Much of it was devoted to tuning the control system to achieve optimum engine operation and to establishing inlet/engine compatibility. Both steady and dynamic distortion patterns were generated at NAPC, the latter by the Random Frequency Generator, to simulate the flow into the engine under extreme operating conditions. However, fuel pulsing had to be employed to cause the engine to stall under these conditions and recovery was automatic. This work complemented the extensive wind tunnel testing carried out in developing the intake for the F/A-18 to produce little distortion during high angle of attack operation at low speeds while having good pressure recovery during supersonic operation. Inlet/engine compatibility has received a lot of attention following the problems encountered with the F111 in the early 1960s. The subsequent F/A-18 flight trials, beginning November 1978, confirmed that engine operation was stall free over the design manoeuvre envelope. The results of these trials are summarised in Figure 9. Note that an aircraft attitude exceeding 90 degrees was temporarily attained without causing engine stall. The data on afterburner operation confirms expectations for a low bypass engine.

The AST was set back when the aircraft being used crashed at Farnborough in late 1981. However, the program recommenced with another aircraft and it has served to show how the operation of the aircraft, and the engines, can differ appreciably from what was anticipated, with important implications in relation to logistic and durability factors. For example, time at maximum temperature was found to be about 60% more than that used in the original life analyses. Further, afterburner light-ups were up 60% as well. US Navy and Canadian operational experience has tended to confirm these trends. The AST program is now being supported by a Lead the Fleet program (figure 10) in which accelerated field usage is obtained on selected engines that are closely monitored for failure, wear and life usage. This is backed by a factory program for proving the durability of components.

The F/A-18 entered service with the US Navy in early 1981, the CF18 with the Canadian Defence Forces in 1983 and the RAAF are starting pilot training at 20CU about now. The program status is summarised in Figure 10 while that of the F404 is given in Figure 11. These figures were current last September so the engine probably has about 250,000 flight hours up now. The planned production of the F404 is shown in Figure 12. Assembly of engines down at CAC will be at a rate of about 20 per annum.

FEATURES

The F404 has a bypass ratio of 0.34:1. That is, the flow through the bypass duct is 34% of that through the core engine. A high bypass ratio improves the fuel economy, as evidenced by the high ratios of the large civil engines in such aircraft as the Boeing 747, DC10, L1011 and Airbus. Even the TF30 has a ratio of 1.1:1. Thus the bypass ratio of the F404 is low even by military standards. In fact it is often called a leaky turbojet rather than a turbofan. The consequential loss in fuel economy is offset by the rapid response to throttle operation and more reliable afterburner light up that are fundamental characteristics of low bypass engines. Figure 15 notes the expectation of General Electric of the influence of these characteristics on the operational suitability of the engine. There are reasons to

believe that these expectations are justified. These features make the F404 more suitable for fighter aircraft while the TF30 is better suited to strike aircraft where range is of prime importance.

The pressure ratio is another important parameter as it has a significant effect on the performance through its influence on the thermal efficiency. However it is limited by operability and mechanical considerations. The F404 achieves the high pressure ratio of 25:1 in 3 fan stages and 7 compressor stages, shown in Figure 16. In contrast, the TF30 needs 16 stages overall to achieve a pressure ratio of 17:1. That is, the F404 has an average stage temperature rise of 52 C compared to about 30 C for typical military engines of the previous generation. This stage temperature rise is a measure of the amount of energy the compressor blading is able to impart to each unit of flow through the compressor. It is a combination of the aerodynamic design of the blading and of the speed of rotation of the rotors. As an expert in compressor aerodynamics, I found it interesting to note the developments in the aerodynamic design of both fan and compressor of the F404, including such aspects as wide chord blades and the three-dimensional, rather than quasi two-dimensional, design of the fan. Figure 17 brings this point out clearly. However, I would be giving a biased view if I did not comment upon the importance of the materials employed - largely Titanium - and of the advances in mechanical design to the attainment of this high rate of compression. To illustrate, the TF30 has a maximum tip speed of 1488 ft/sec while 1592 ft/sec is attained in the F404. Both the stage temperature rise and the centrifugal stresses are proportional to the tip speed squared!

In the design process, there is generally a requirement to compromise between the operating pressure rise and the stall margin, as illustrated in Figure 18 which depicts the speed characteristic of the fan. The selection of the stage pressure rise to match with other stages has to be a judicious choice between getting the most out of the blading and retaining a reasonable margin between the operating point and the stall line. In view of the high pressure rise per stage, it came as a surprise to find that both the fan and the compressor have good stall margins and so are able to withstand disturbances emanating from in front - the aircraft intake - and behind - pressure pulses from the afterburner - with equanimity, as demonstrated in tests, in flight trials and in operations.

The annular combustor employed is an adaption of the well proven design in the CF6 series of civil engines. Eighteen fuel nozzles supply fuel directly into the forward part of the combustion liner (Figure 19) which contains matching swirlers to facilitate atomization of the fuel. A pattern of inner and outer louvers and dilution holes in the liner causes the cooling air (Figure 20) to mix with the products of combustion.

The other main parameter of the gas turbine performance cycle is the turbine inlet temperature - the temperature of the hot efflux from the combustor. There is a requirement to maximise this value within applicable constraints in order to get high thermal efficiency and specific thrust. The major constraint is the achievement of good durability of the hot end components - nozzle guide vanes, rotor blades, disks and seals. The F404 has a turbine inlet temperature higher than any other operational military engine yet the durability of its hot end components is predicted to far exceed that for earlier engines. This is achieved by a combination of a complex cooling system for these components with the use of advanced materials - powdered super alloys and directionally solidified blading material. The cooling flow through the engine is shown in Figure 21 while Figure 22 illustrates the complexity of the cooling passages in the high pressure turbine blading. Convection, impingement and film cooling is utilised. All the blading in the turbine stages, high pressure and low pressure, stationary and rotating, are cooled, as well as rotors, cooling plates, blade and vane platforms and shrouds. To further illustrate the importance of cooling, some 11% of the air out of the compressor is used to cool the high pressure nozzle guide vanes. Because of the high pressure ratio, this air is rather hot - 520 C - so its cooling effectiveness is more dependent upon quantity than quality!

I expect that a number of you have noted that this engine is quite unusual in that it has only one high pressure turbine stage, Figure 23, and one low pressure stage, Figure 24. As mentioned earlier, this was done to keep the parts count down in order to reduce costs and improve maintainability. In part it caused a reduction in turbine efficiency with its consequential effect on performance. However, it would not have been possible without significant advances in material characterisation, mechanical design, heat transfer and turbine aerodynamics, including boundary layer development. For example, Figure 25 shows the improvement expected by substituting DSR80 for Rene 125 in the high pressure turbine blades. This is equivalent to doubling the life of these blades.

One of the most important developments has been an appreciation of the influence of low cycle fatigue on the life of such engine components as turbine rotor blading, disks and seals. This has led to the development of design methods that enable extended usage to be obtained from such components, despite the severity of their usage. For example, these turbine blades are subject to high centrifugal and, in particular, thermal loads as the engine is cycled through a range of throttle settings. The condition of the blades is inferred by counts accumulated in the aircraft mission computer using an algorithm based on the temperature of the turbine exhaust gas. When the count, called Equivalent Full Thermal Cycles, reaches the prescribed limit the blades are replaced. In the case of the Rene 125 blades, this is equivalent to approximately 1000 hours of average engine operation. However, if mission severity is harsh, the prescribed number of EFTC could come up in appreciably fewer hours. It is expected that the DSR80 directionally solidified blades will have about twice the life of their predecessors.

This example is typical of the twenty odd components of the F404 whose life usage is assessed by counts calculated in the mission computer and monitored by maintenance personnel. However, most of these components have an average life of about 4000 hours which is equivalent to over 10 years of operation. I will comment further on condition monitoring shortly.

Returning to the characteristics of the engine, it is noteworthy that the sfc for non-afterburning operation is similar for the F404 and TF30. The high pressure ratio and turbine inlet temperature of the former off setting the high bypass ratio of the latter. However, the use of single stage turbines have also had their effect. The saving in weight and complexity has been obtained at the cost of a reduced turbine efficiency, with its consequent effect upon the sfc.

Turning now to the afterburner, the low bypass ratio aids light up and modulation of thrust. This is further improved by employing circumferential modulation rather than the more common radial form, which can be unreliable due to the influence of the cold bypass air. The pilot and main spray bars can be seen in Figure 26. The six pilot spray bars are equally spaced and protrude through the afterburner case and liner and extend into the flameholder. The 24 main spray bars are also equally spaced and extend radially through the afterburner case and liner and beyond the flameholder into the turbine exhaust. Fuel is pumped out of the pilot spray bars until the Light Off Detector indicates that combustion has been established when the main spray bars come into play, the number utilised being dependent upon the degree of afterburning called for by the Power Lever Angle. Fuel circulating in the main fuel manifold during non-afterburning operation cools the distributor valves, so reducing the fill time when afterburner operation is initiated.

As noted earlier, the nozzle opens up with the degree of afterburning. This is just one function of the control system which consists of a hydro-mechanical unit for control at powers less than Intermediate Rated Power (IRP), maximum non-afterburning operation. For IRP or afterburning operation, the Electronic Control Unit takes over. These units are mounted on the lower front of the engine. Figure 27 shows the layout as viewed from underneath. In this way the infeasible complexity of a full authority hydro-mechanical system in this type of variable geometry engine is avoided. Sufficient research has been done on Full Authority

Digital Electronic Control (FADEC) systems to indicate that they will be employed on future engines. However, at the time of the F404 development the reliability of electronic control units in the harsh environment on the engine casing was insufficiently proven: the hydro-mechanical unit provides a get-home capability in the event of failure of the ECU.

Some functions carried out by the control system are:

- limitation on corrected fan speed to prevent stall margin erosion
- flow restriction in supersonic flight to maintain intake performance
- fuel dip and variable geometry resetting during rocket firing
- scheduling of nozzle area to limit turbine inlet temperature
- scheduling fuel flow to limit maximum fan speed
- limiting back pressure on core engine during afterburner operation
- limiting maximum and minimum combustor casing pressures
- scheduling fuel flow for engine acceleration and deceleration

The main control operating modes in both dry and afterburning operation are shown in Figure 28. Figure 29 shows the scheduled variation at IRP of exhaust gas temperature (T5) and fan speed (N1) with inlet temperature (T1) to prevent stall margin erosion for T1 less than 440 deg R, to limit compressor maximum pressure at low altitudes between 410 and 530, to limit the turbine inlet temperature between 500 and 650 and to limit actual fan speed between 570 and 620.

To a large extent, the role of material properties and structural design concepts have only been implied in examining the features of this engine. These factors are summarised in Figures 30 and 31 which serve to illustrate the range of materials required to meet the varying, stringent requirements and to highlight some of the structural features.

OPERATION

The driver of a motor car generally expects to be able to ignore the engine of his vehicle. This is also a desirable feature for the fighter pilot. He would like to be able to use the throttle to assist in the manoeuvring of his aircraft without having to bear in mind operability limitations. The F404 is not yet fully proven but there is reason to believe that it meets the requirements listed in Figure 32. It is certainly a very responsive engine and the features built into its control system ensure that it will not have the problems in operation in the high-altitude, cold conditions over Darwin that have characterised the Atar in Mirage. Figure 33 shows the operating mode of the engine at IRP under the 1% extreme conditions at Darwin. Under cold conditions at altitude - Darwin and Panama have the coldest altitude conditions in the world - the corrected fan speed is limited to 104.4% for low Mach Numbers and reduces for the higher speeds. During hot day operation at low level, the limiting factor is turbine inlet temperature for all practical speeds.

This engine is designed for On Condition Maintenance, a concept defined in Figure 34. It is a novel concept for the RAAF. It embraces an In-flight Engine Condition Monitoring (IECMS) - Figure 35 - to provide data to assess the life usage of engine components due to low cycle fatigue, the performance status of the engines and the cause of exceedances of engine parameters. The RAAF have contracted CAC to put into place a Maintenance Data & Service Life Monitoring System (MD&SLMS) to process this monitoring data to provide meaningful information to the maintenance and engineering personnel. ARL are involved in the definition and proving of procedures to be incorporated in this system.

The information extracted in the MD&SLMS from the IECMS data will supplement information on the condition of the engines provided by:

- borescope inspections
- analysis of the debris on chip detectors
- vibration signatures
- spectrometric oil analysis

Figure 36 shows the number of borescope ports available. Most of these are accessible with the engine installed in the aircraft. The location of the chip detectors is shown in Figure 37 while Figure 38 shows the location of vibration accelerometers on the engine for testing in a cell. The one marked ECMS is also on the installed engine and serves to give warning of excessive vibration in flight.

The maintainability of the engine is further facilitated by its modular construction. Figure 39 lists the potential advantages while Figure 40 depicts the six modules. The impact of modular maintenance can be expected to vary from user to user due to the different parameters in the logistic relations.

CONCLUSION

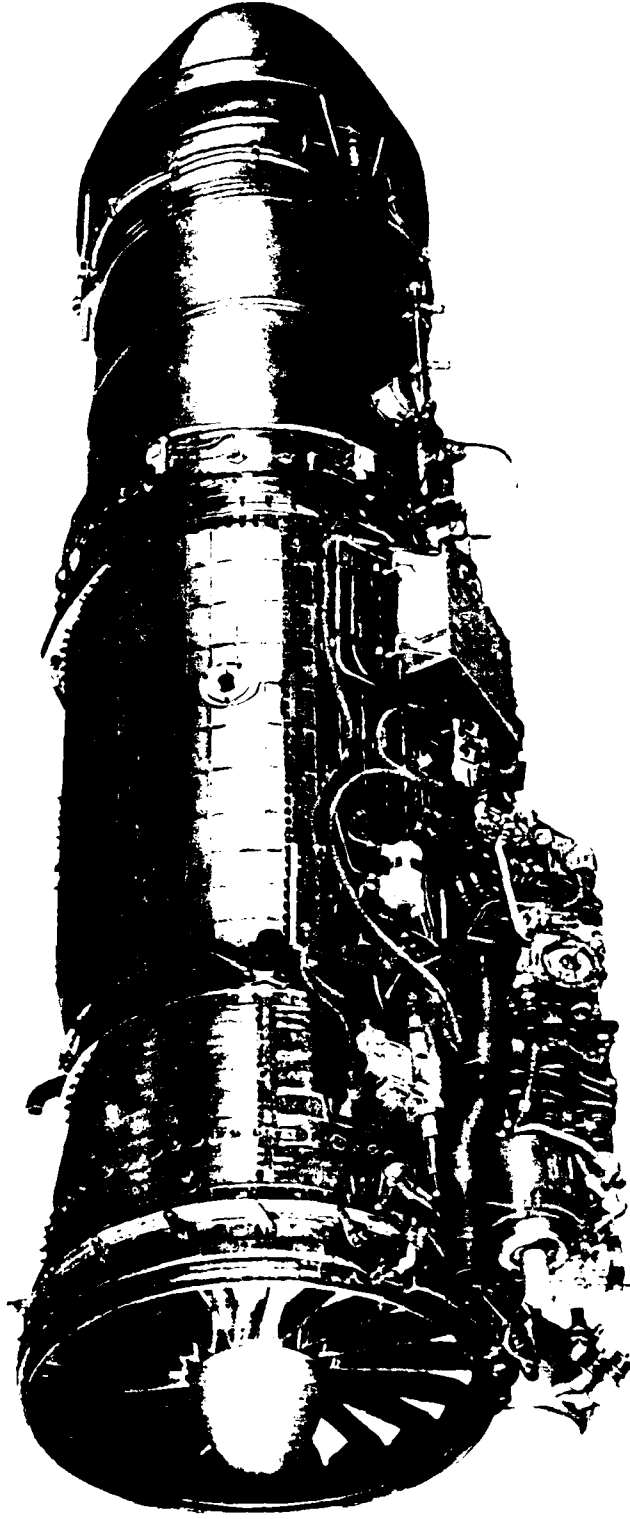
The F404 is a relatively new engine. As it has only about 250,000 hours up, it has a long way to go before it reaches maturity at one million hours. Nevertheless, the tasks being dealt with in the Component Improvement Program seem to indicate that it does not suffer any of the major, fundamental problems that have so inhibited earlier engines. There is good reason to believe that it will set new standards for military engines as regards operability, availability, reliability and maintainability. However, there is no reason to believe that it will be exceptional in that regard. Newer engines are predicted to follow this improved trend.

I will be interested to hear lectures in due course from RAAF and CAC personnel on experience in operating and maintaining this engine. Certainly there is much to be learnt about engine operation and its influence on maintenance from the vast amount of condition monitoring data being acquired through the MD&SLMS. Doubtless there will also be problems but I will be surprised if the overall view is unfavourable.

ACKNOWLEDGEMENTS

Aircraft Engine Business Group, General Electric Company supplied most of the information used in this lecture, which was authorised by the Director, Aeronautical Research Laboratories.

F404-GE-400 Augmented Turbofan Engine



- Thrust 16,000 Lb
- SFC Max A/B 1.85 Lb/Hr/Lb
- SFC IRP 0.81 Lb/Hr/Lb
- Airflow 142 Lb/Sec
- Bypass Ratio 0.34
- Weight 2,180 Lb
- Length 159 in.
- Diameter 35 in.

FIG. 1

F404-GE-400 Engine

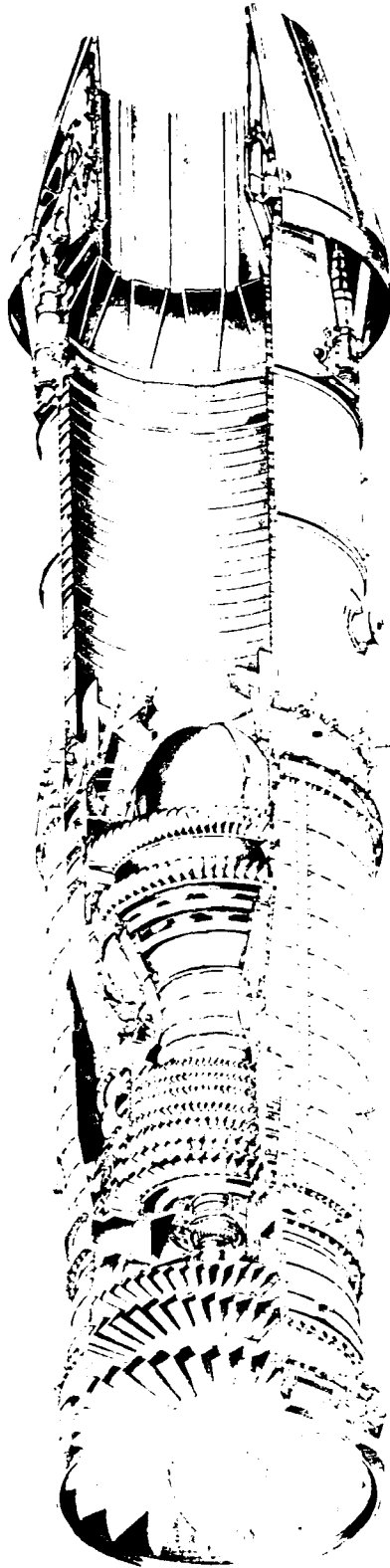


FIG. 2

	F404-GE-400 F404-GE 400	TF30 P 3	
LENGTH, IN.	159	178	(+12%)
DIAMETER, IN.	35	38	(+9%)
WEIGHT, LB.	2180	4100	(+88%)
THRUST/WEIGHT	7.3	4.9	(-67%)
MASS FLOW, LB/SEC.	142	240	(+69%)
BY-PASS RATIO	.34	1.1	
PRESSURE RATIO	25	17	
TURBINE INLET TEMPERATURE, °C	1390	1270	
THRUST, MAX, A/B	16000	20000	(+25%)
" , MAX. NON-A/B	10600	10750	(+1%)
SFC, MAX, A/B, LB/HR/LB.	1.84	1.80	(-2%)
" , MAX. NON-A/B "	0.78	0.80	(+2%)
FAN-STAGES	3	3	
PRESSURE RATIO	4.1	2.0	
SPEED, RPM	13270	9500	
COMPRESSOR-STAGES	7	6 + 7	
PRESSURE RATIO	6.0	8.5	
SPEED, RPM	16810	9500, 14500	

FIG. 3

	F404-GE-400	TFH-30
LENGTH, IN.	159	159
DIAMETER, IN.	35	34 (-3%)
WEIGHT, LB.	2180	2908 (33%)
THRUST/WEIGHT	7.3	5.5
MASS FLOW, LB/SEC.	142	191 (35%)
BY-PASS RATIO	.34	1.1
PRESSURE RATIO	25	17
TURBINE INLET TEMPERATURE, c.	1390	1270
THRUST, MAX. A/B	16000	15900 (-1%)
" , MAX. NON-A/B	10600	8550 (-20%)
SFC, MAX. A/B, LB/HR/LB	1.84	1.80 (-2%)
" , MAX. NON-A/B, "	0.78	.80 (+2%)
FAN-STAGES	3	3
PRESSURE RATIO	4.1	2.0
SPEED, RPM	13270	10640
COMPRESSOR-STAGES	7	6 + 7
PRESSURE RATIO	6.0	8.5
SPEED, RPM	16810	16240

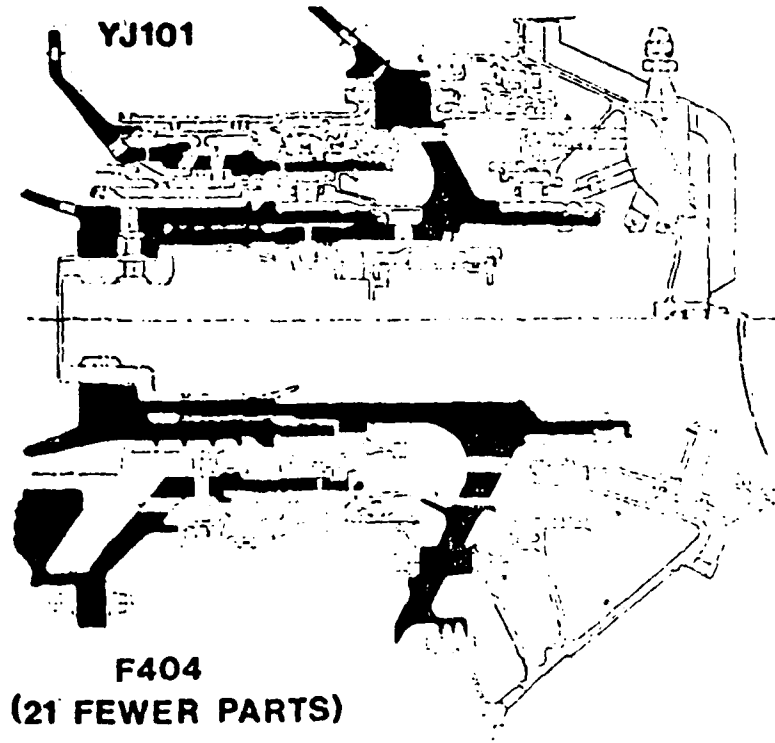
FIG. 4

HYPOTHETICAL PERFORMANCE OF F/A-18 WITH 2 x TFH30

(COMPARISON WITH F/A-18 WITH 2 x F404)

THRUST/WEIGHT	-25%
RANGE PERFORMANCE	-6%
DUE TO ENGINE WEIGHT	-4%
DUE TO SFC	-2%
MAXIMUM MACH NUMBER	-12%

FIG. 5



C-Sump Design Comparison

Design/Development Emphasis

• Operational Suitability Most Important

• Reliability

• Maintainability

• Cost

• Performance

• Weight

FIG. 7

F404-400 Reliability Features

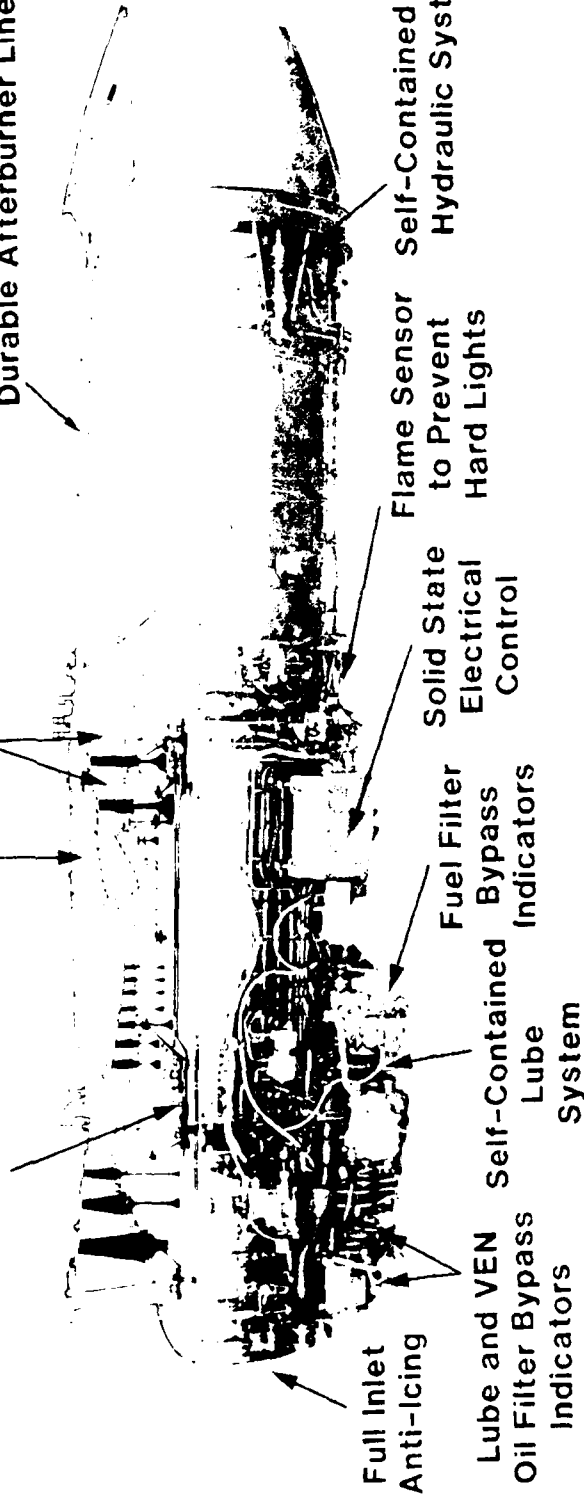
Disciplined Test-and-Fix Program During Development

Durable Machined-Ring Combustor

Advanced Turbine Blade Design

Durable Afterburner Liner

State-of-the-Art Bearings and Seals



Full Inlet Anti-Icing

Lube and VEN Oil Filter Bypass Indicators

Fuel Filter Bypass Indicators

Solid State Electrical Control

Flame Sensor to Prevent Hard Lights

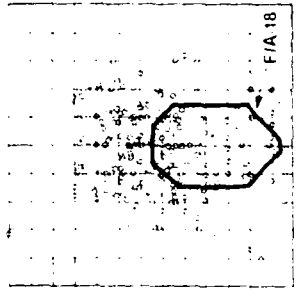
Self-Contained VEN Hydraulic System

- Corrosion Resistance
- Demonstrated Rotor Containment
- All Casings Pressure-Tested
- All Components Fire-Tested
- Overspeed/Overtemperature Protection

FIG. 8

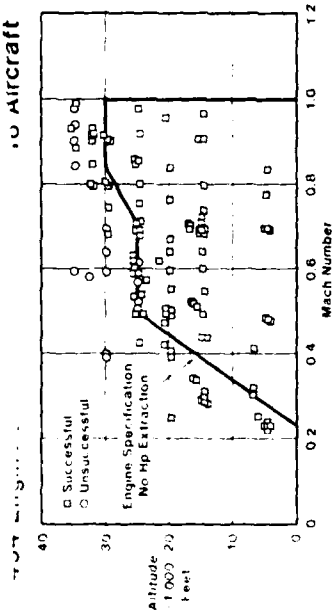
Operation Compatibility

F/A-18 Maneuvering Experience

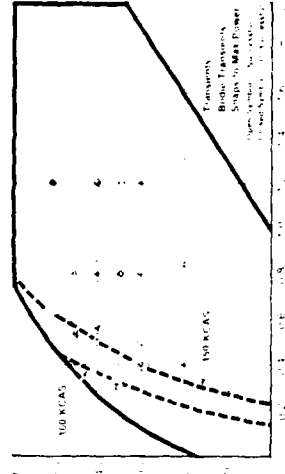


- Mach .15-4
- 35-40,000 Feet
- Aircraft No. 6
- Outstanding Inlet Compatibility

Spooldown Airstarts



F/A-18/F404 Afterburner Operation Flight Test Experience



Successful A/B Lights Throughout Envelope

FIG. 9

Rotor "Lead the Fleet" Plan

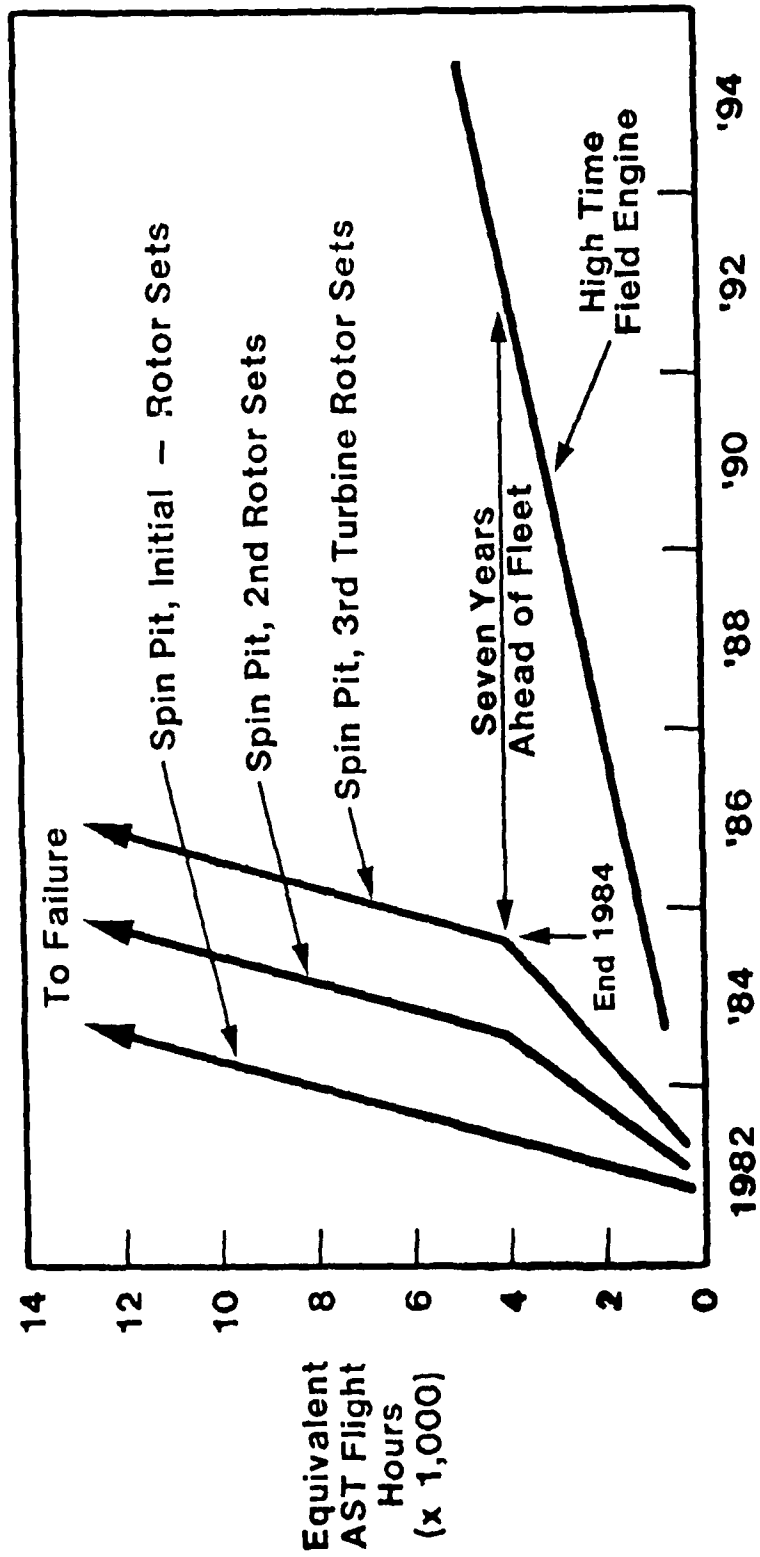


FIG. 10

Program Status

- USN/USMC Operational Sites
 - Lemoore NAS
 - Pt. Mugu NAS
 - China Lake NWC
 - El Toro MCAS
- CAF Operational Site
 - Cold Lake
- Over 170,000 EFH
- Over 600 Production Engines Shipped
- High Time Engine 926 EFH
- Production Fleet Engine Average Age
 - USN — 369 EFH
 - Canada — 179 EFH

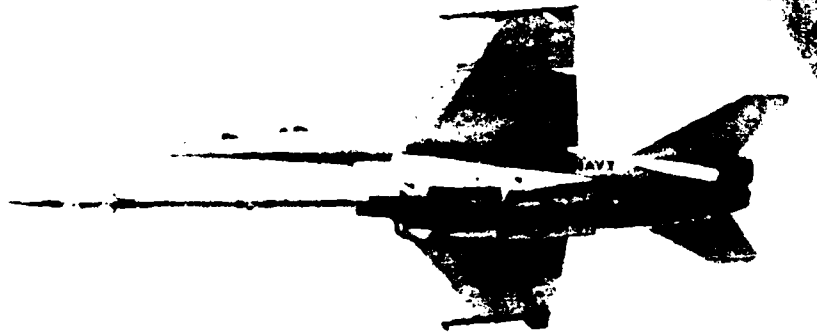


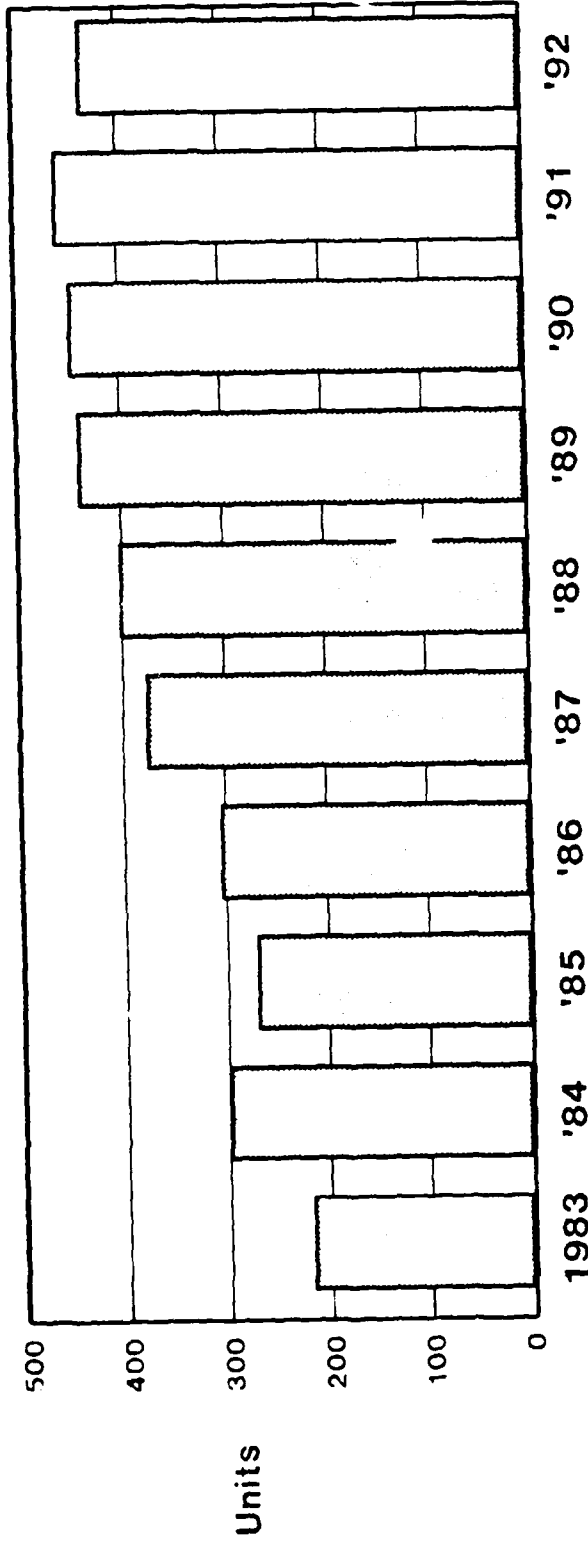
FIG. 11

F404 Status

- **Over 550 Engines Shipped Since December 1979**
 - 96 Percent First Run Acceptance Rate
- **Currently Tooled For 26/Month Rate**
- **Over 160,000 F/A-18 Engine Flight Hours**
- **Reliability . . . Better Than Goal**
 - 281 MTBF Versus 264 Goal At 24,000 Fleet Engine Flight Hours
- **No Trim Verified**
 - Engine Change
 - Module/Component Change

FIG. 12

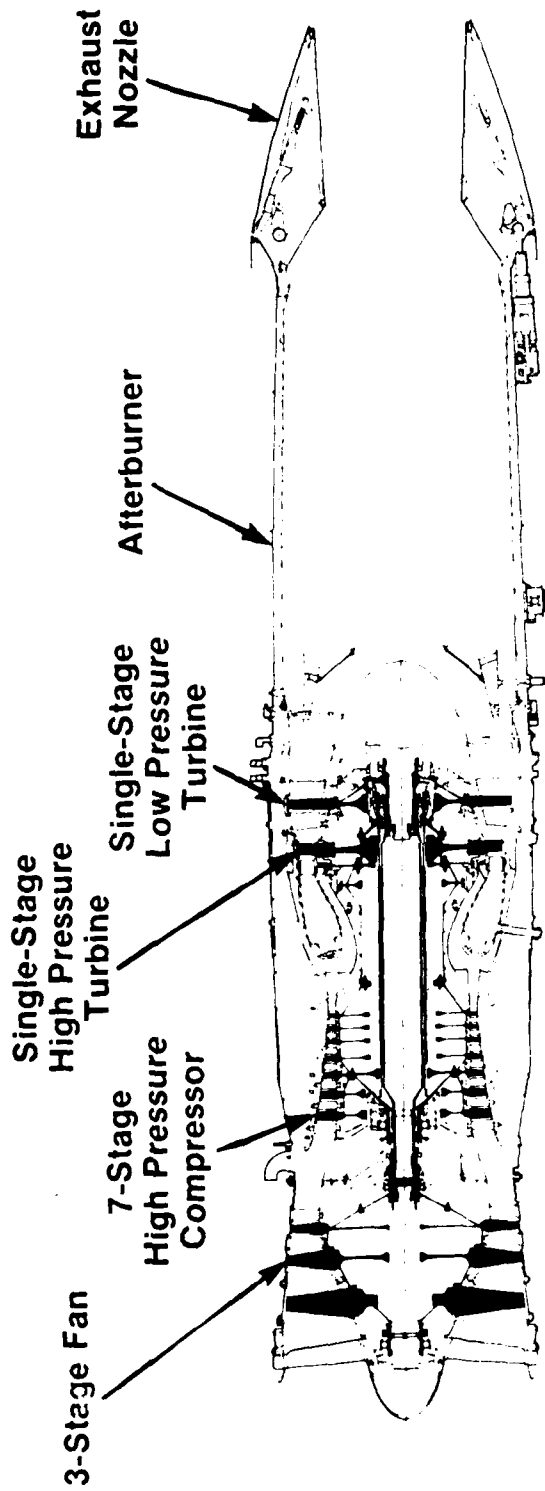
F404 Production Plan



- Performance Margin — Thrust 3%
- SFC 2%
- Weight Margin — 23 Lb
- Production Engine Cost (Constant Dollars)
Reduced By 34% — 1981 To 1984

FIG. 13

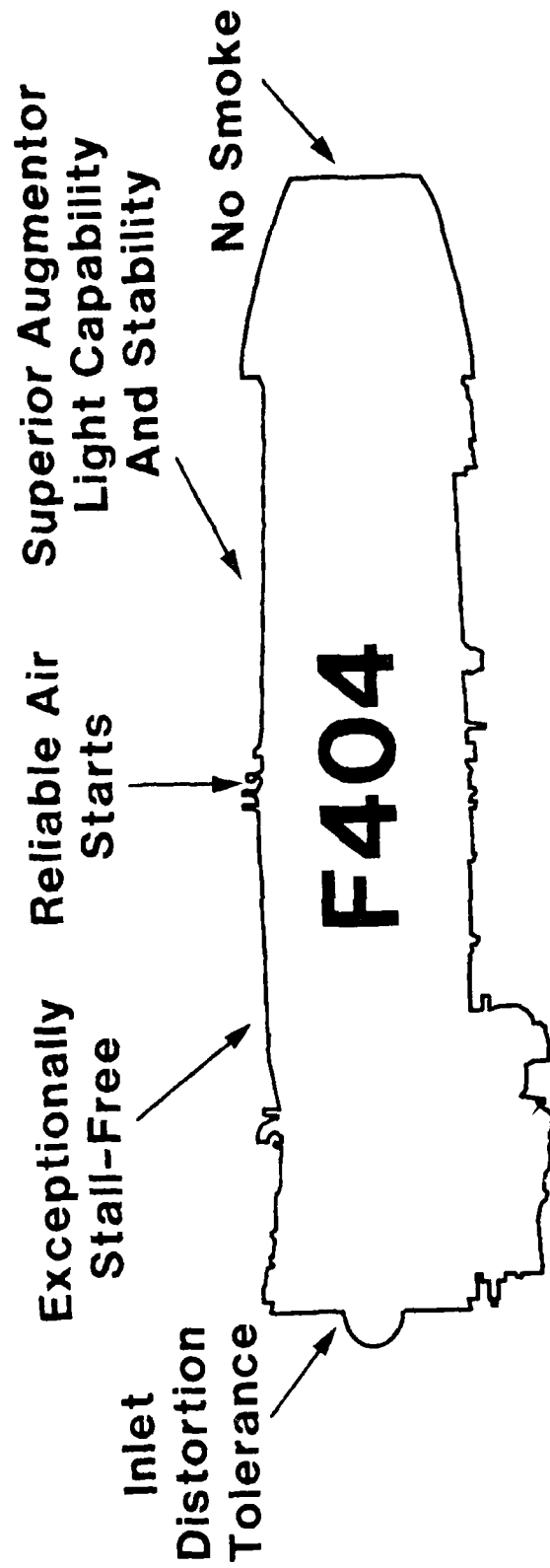
F404-GE-400



- 142 lb/sec Airflow
- 0.34 Bypass Ratio
- 7.5 Thrust/Weight Ratio Class

FIG. 14

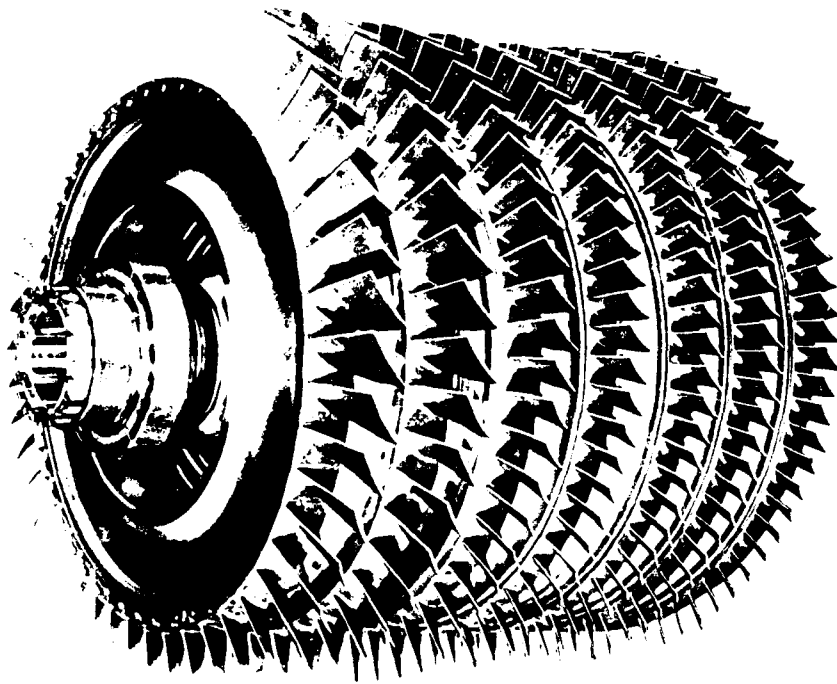
The Fighter Turbofan With Turbojet Characteristics



- **No Throttle Restrictions**
- **<4 Seconds Acceleration (Idle To IRP)**
- **High Thrust Without Afterburner**
- **Supersonic Capability**
- **Low Combat SFC**

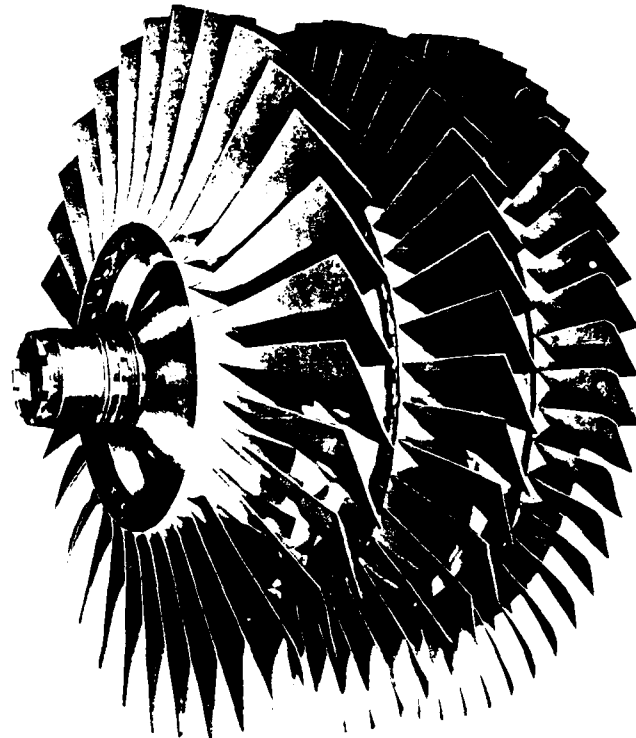
FIG. 15

Compressor



**Inertia Welded
Pressure Ratio 6.3:1**

Fan



Pressure Ratio 4:1

FIG. 17

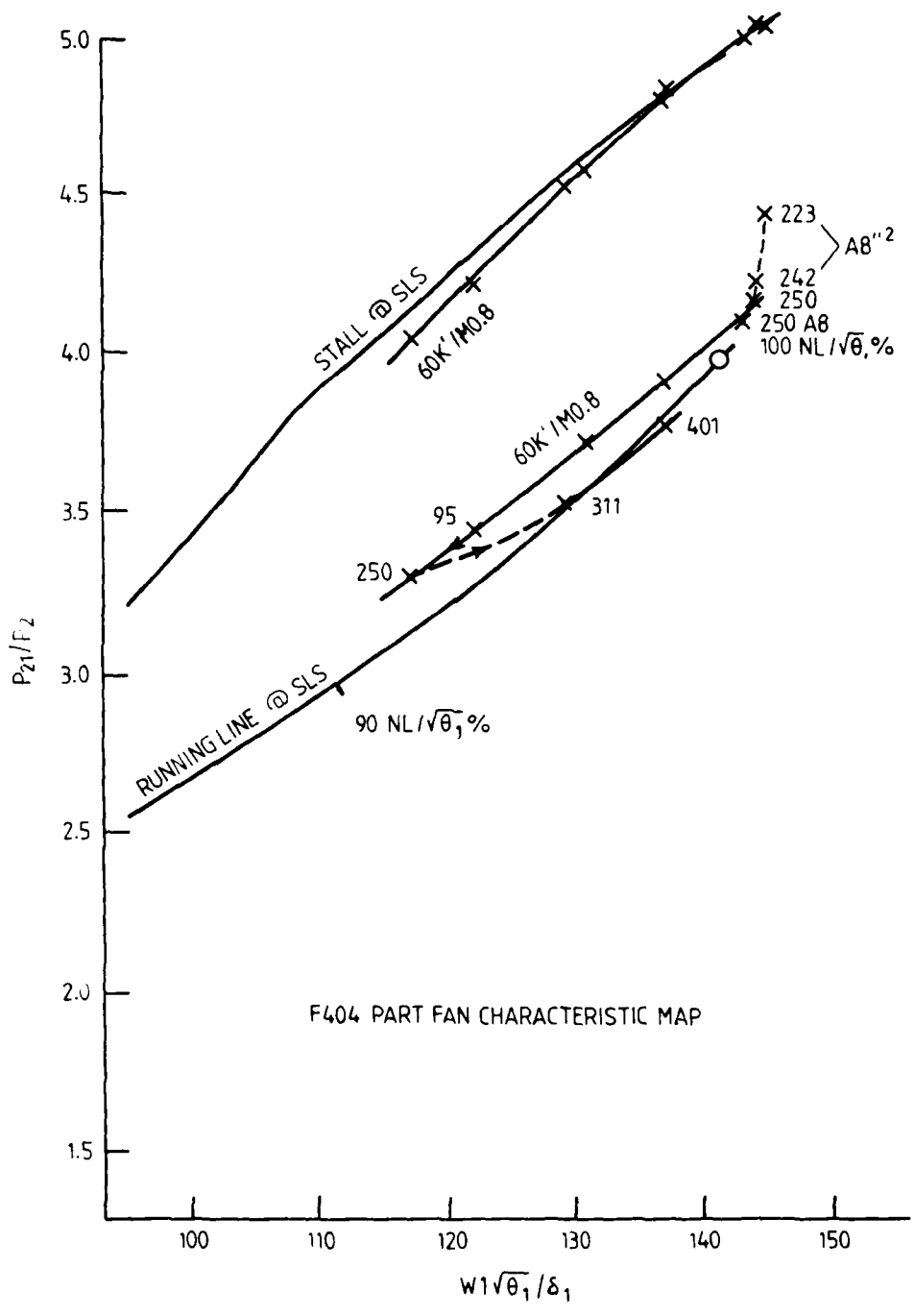
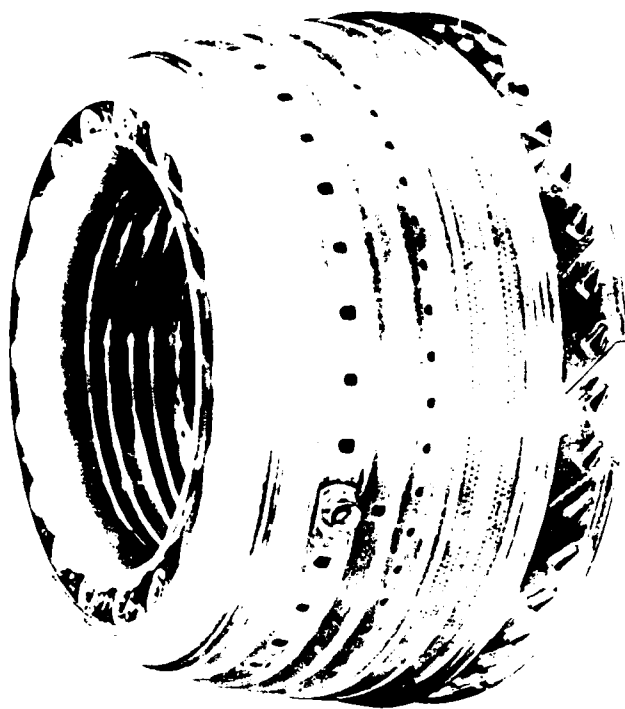


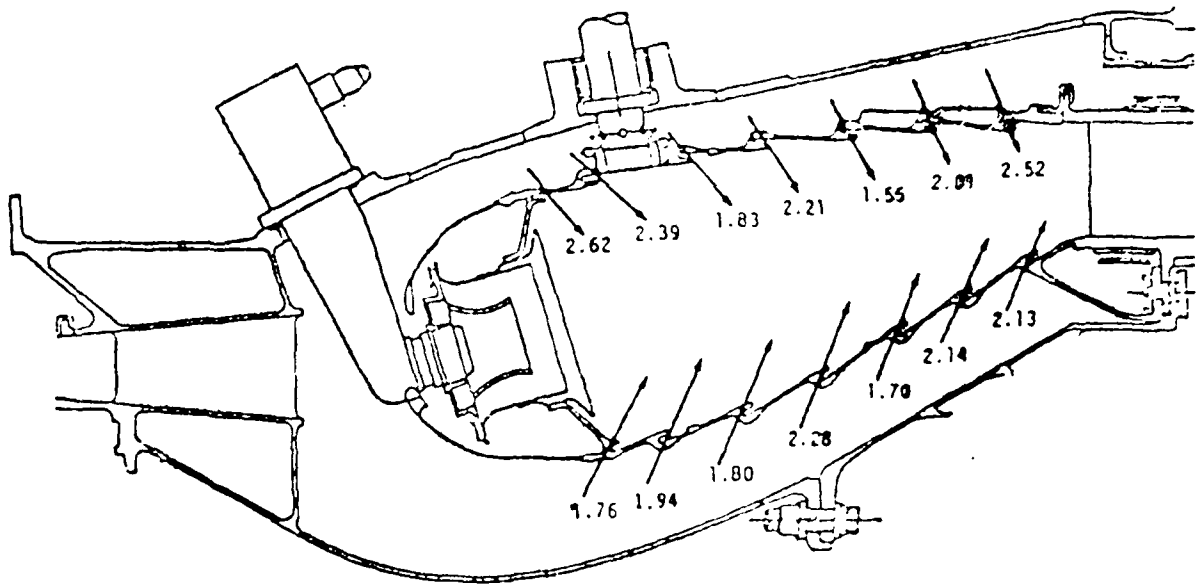
FIG. 18

Combustor



- Machined Ring
- Low Pattern Factor

FIG. 19

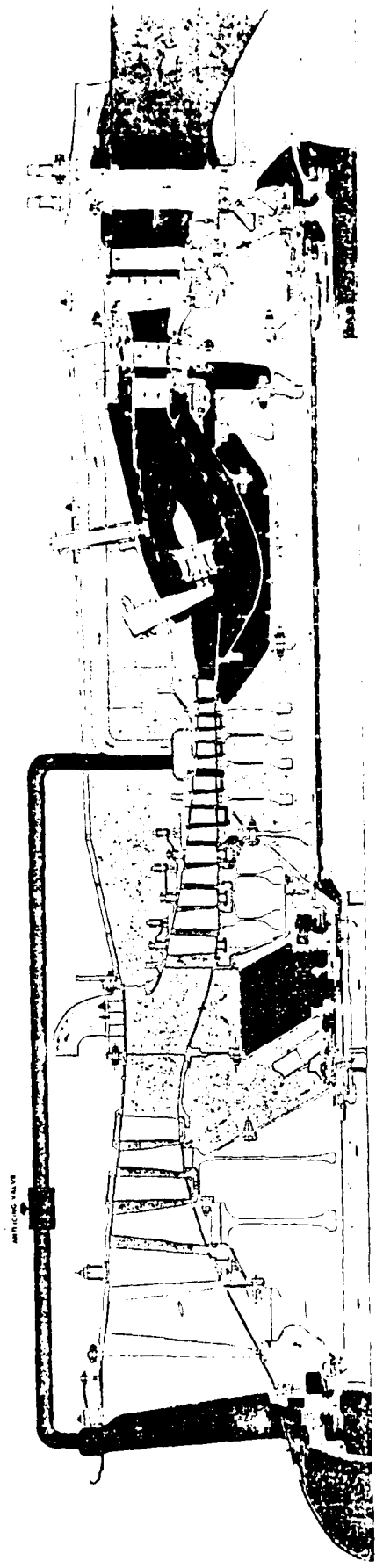


$W_3 = 1M/SEC$

LINER SHELL COOLING FLOWS - $\frac{1}{2}$ Wa 3.0

QT CONFIGURATION

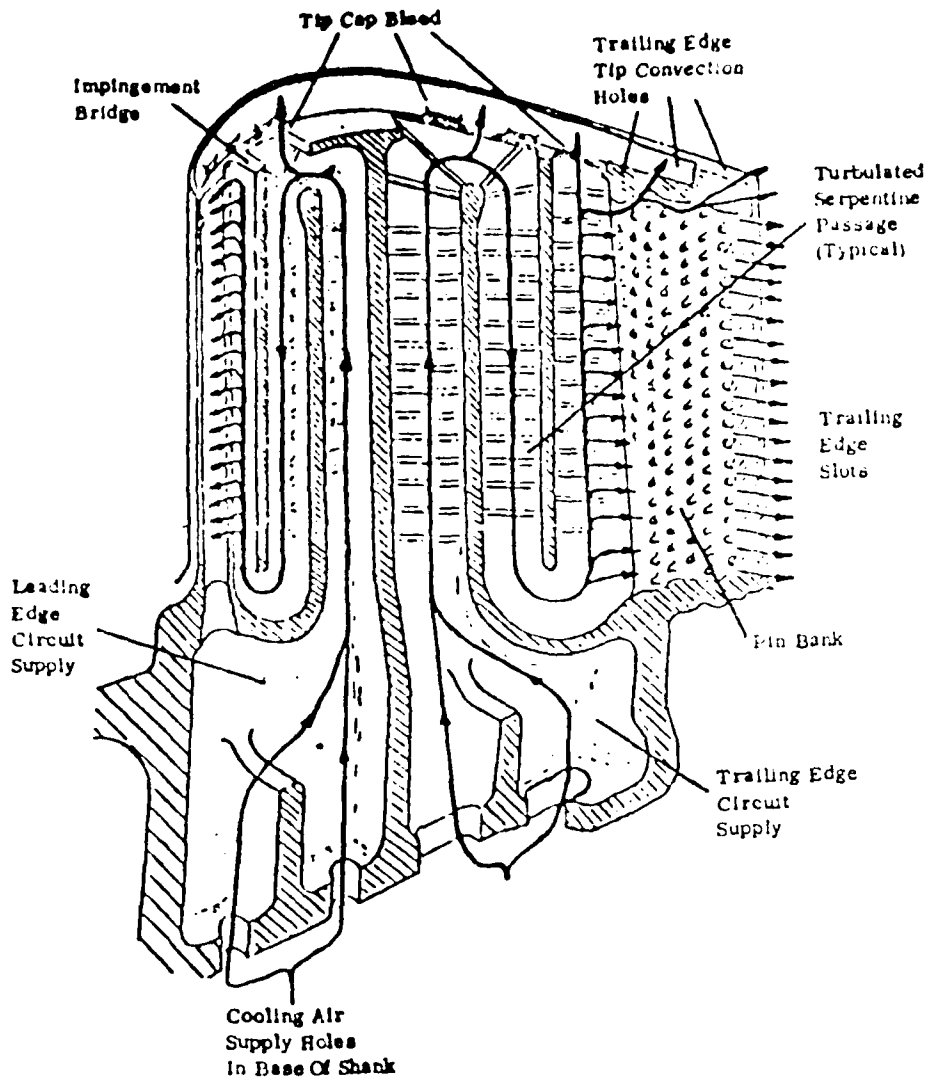
FIG. 20



- AIRBRAFT BLEED AIR
- COMPRESSOR AND EXHAUST GASES
- BALANCE FLOW AIR
- HIGH PRESSURE MAIN AIRFLOW AND HP1 COOLING AIR
- LOW PRESSURE MAIN AIR FLOW BYPASS AIR
- COMPRESSOR HOT AIR COOLING AIR
- VALVE CONTROL COOLING AIR
- HP1 FLOWING AIR
- HP2 FLOWING AIR
- HP3 FLOWING AIR
- HP4 FLOWING AIR
- HP5 FLOWING AIR
- HP6 FLOWING AIR
- HP7 FLOWING AIR
- HP8 FLOWING AIR
- HP9 FLOWING AIR
- HP10 FLOWING AIR
- HP11 FLOWING AIR
- HP12 FLOWING AIR
- HP13 FLOWING AIR
- HP14 FLOWING AIR
- HP15 FLOWING AIR
- HP16 FLOWING AIR
- HP17 FLOWING AIR
- HP18 FLOWING AIR
- HP19 FLOWING AIR
- HP20 FLOWING AIR
- HP21 FLOWING AIR
- HP22 FLOWING AIR
- HP23 FLOWING AIR
- HP24 FLOWING AIR
- HP25 FLOWING AIR
- HP26 FLOWING AIR
- HP27 FLOWING AIR
- HP28 FLOWING AIR
- HP29 FLOWING AIR
- HP30 FLOWING AIR
- HP31 FLOWING AIR
- HP32 FLOWING AIR
- HP33 FLOWING AIR
- HP34 FLOWING AIR
- HP35 FLOWING AIR
- HP36 FLOWING AIR
- HP37 FLOWING AIR
- HP38 FLOWING AIR
- HP39 FLOWING AIR
- HP40 FLOWING AIR
- HP41 FLOWING AIR
- HP42 FLOWING AIR
- HP43 FLOWING AIR
- HP44 FLOWING AIR
- HP45 FLOWING AIR
- HP46 FLOWING AIR
- HP47 FLOWING AIR
- HP48 FLOWING AIR
- HP49 FLOWING AIR
- HP50 FLOWING AIR
- HP51 FLOWING AIR
- HP52 FLOWING AIR
- HP53 FLOWING AIR
- HP54 FLOWING AIR
- HP55 FLOWING AIR
- HP56 FLOWING AIR
- HP57 FLOWING AIR
- HP58 FLOWING AIR
- HP59 FLOWING AIR
- HP60 FLOWING AIR
- HP61 FLOWING AIR
- HP62 FLOWING AIR
- HP63 FLOWING AIR
- HP64 FLOWING AIR
- HP65 FLOWING AIR
- HP66 FLOWING AIR
- HP67 FLOWING AIR
- HP68 FLOWING AIR
- HP69 FLOWING AIR
- HP70 FLOWING AIR
- HP71 FLOWING AIR
- HP72 FLOWING AIR
- HP73 FLOWING AIR
- HP74 FLOWING AIR
- HP75 FLOWING AIR
- HP76 FLOWING AIR
- HP77 FLOWING AIR
- HP78 FLOWING AIR
- HP79 FLOWING AIR
- HP80 FLOWING AIR
- HP81 FLOWING AIR
- HP82 FLOWING AIR
- HP83 FLOWING AIR
- HP84 FLOWING AIR
- HP85 FLOWING AIR
- HP86 FLOWING AIR
- HP87 FLOWING AIR
- HP88 FLOWING AIR
- HP89 FLOWING AIR
- HP90 FLOWING AIR
- HP91 FLOWING AIR
- HP92 FLOWING AIR
- HP93 FLOWING AIR
- HP94 FLOWING AIR
- HP95 FLOWING AIR
- HP96 FLOWING AIR
- HP97 FLOWING AIR
- HP98 FLOWING AIR
- HP99 FLOWING AIR
- HP100 FLOWING AIR

F4C4 AIRFLOW

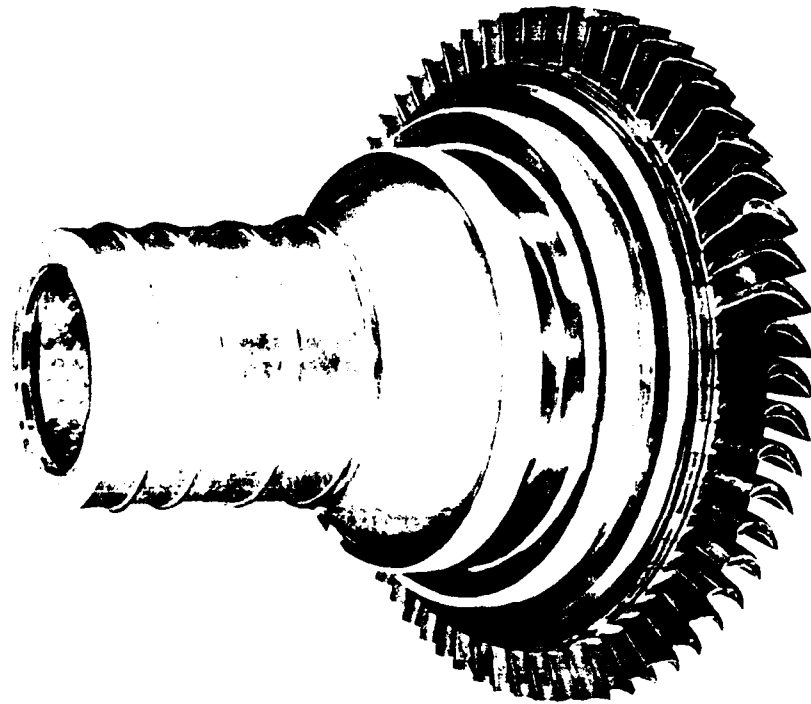
FIG. 21



Cutaway Schematic of HPT Blade Cooling System

FIG. 22

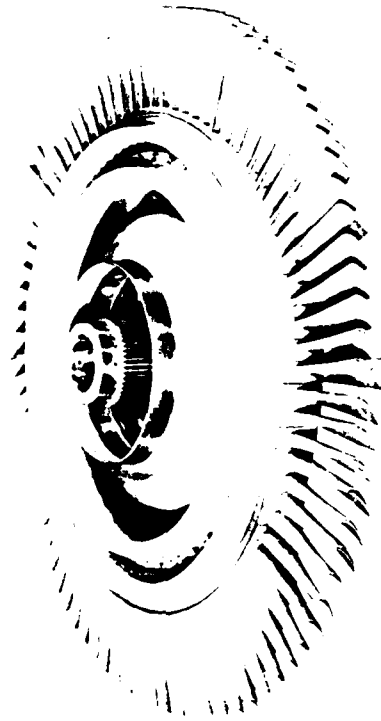
High Pressure Turbine



- Single Stage

FIG. 23

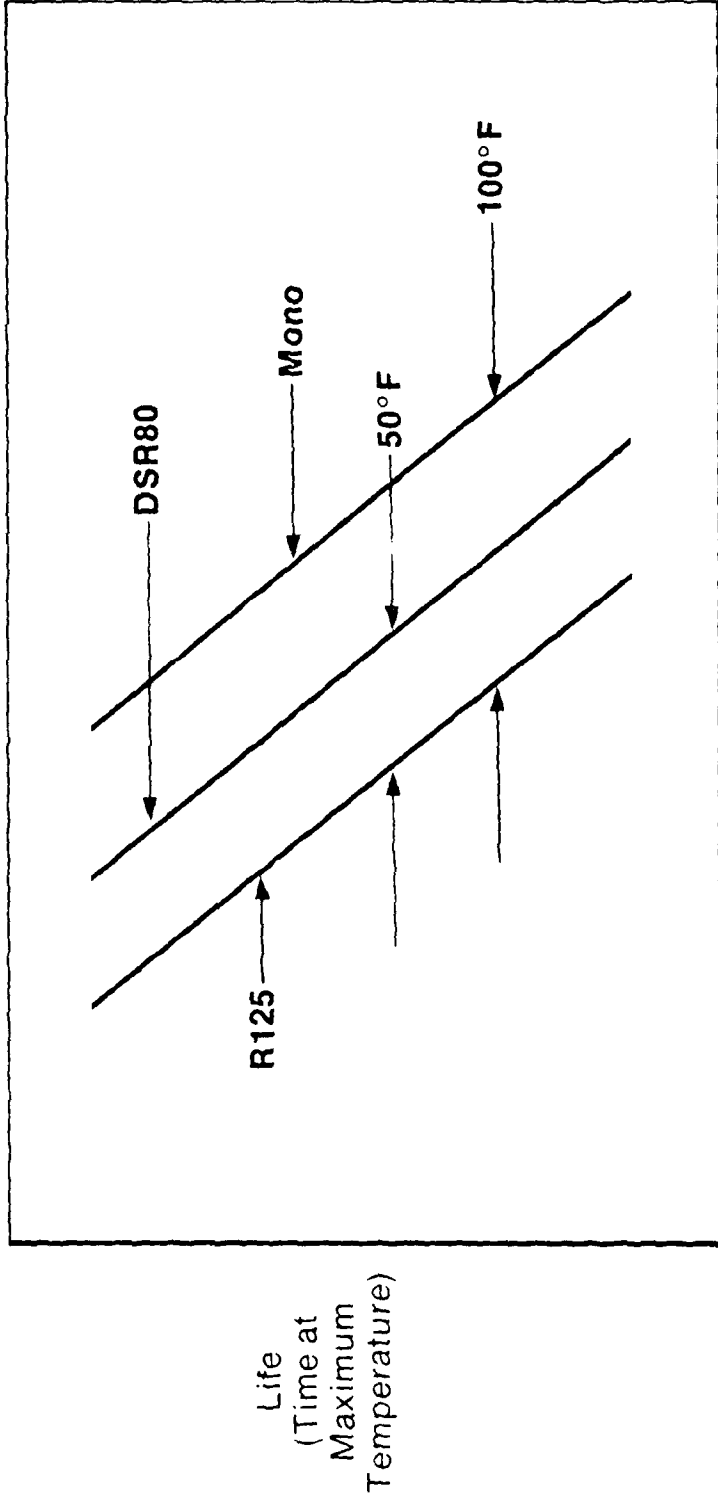
Low Pressure Turbine



- **Single Stage**

FIG. 24

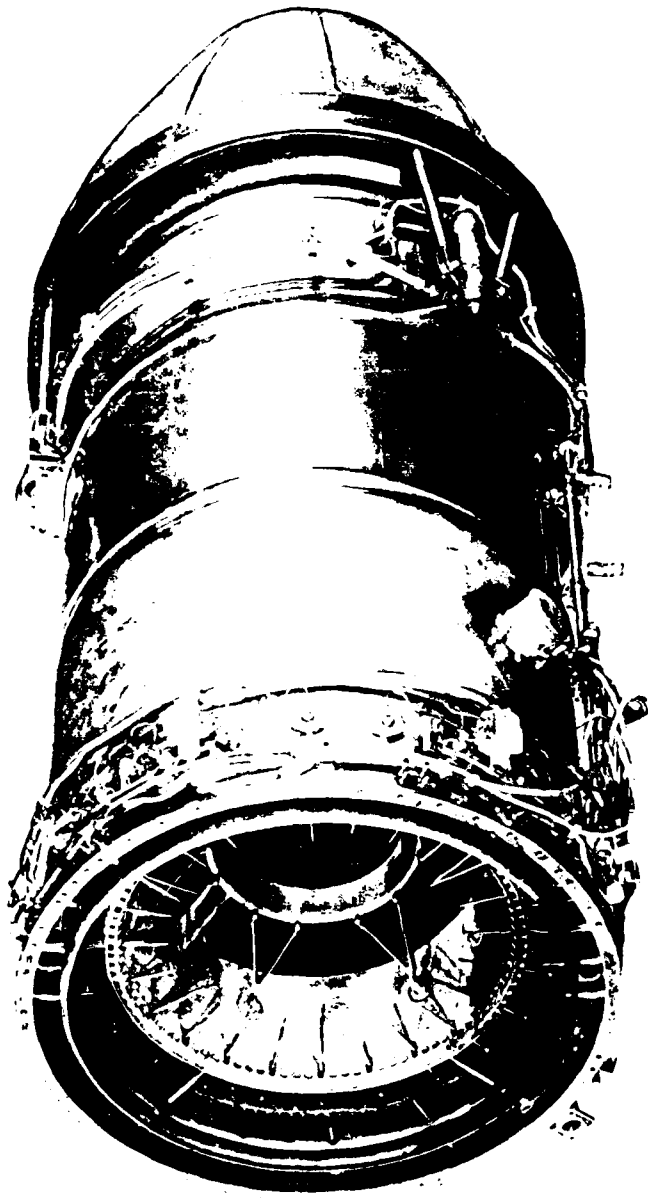
Typical Life/Temperature Characteristic



**Hot Section Life is Sustained by Advancing
Material Technology**

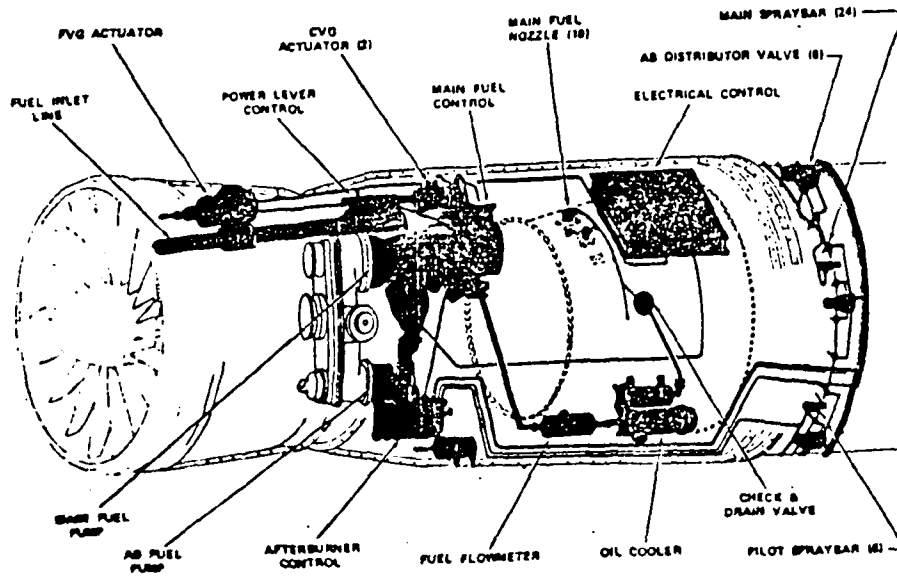
FIG. 25

Afterburner



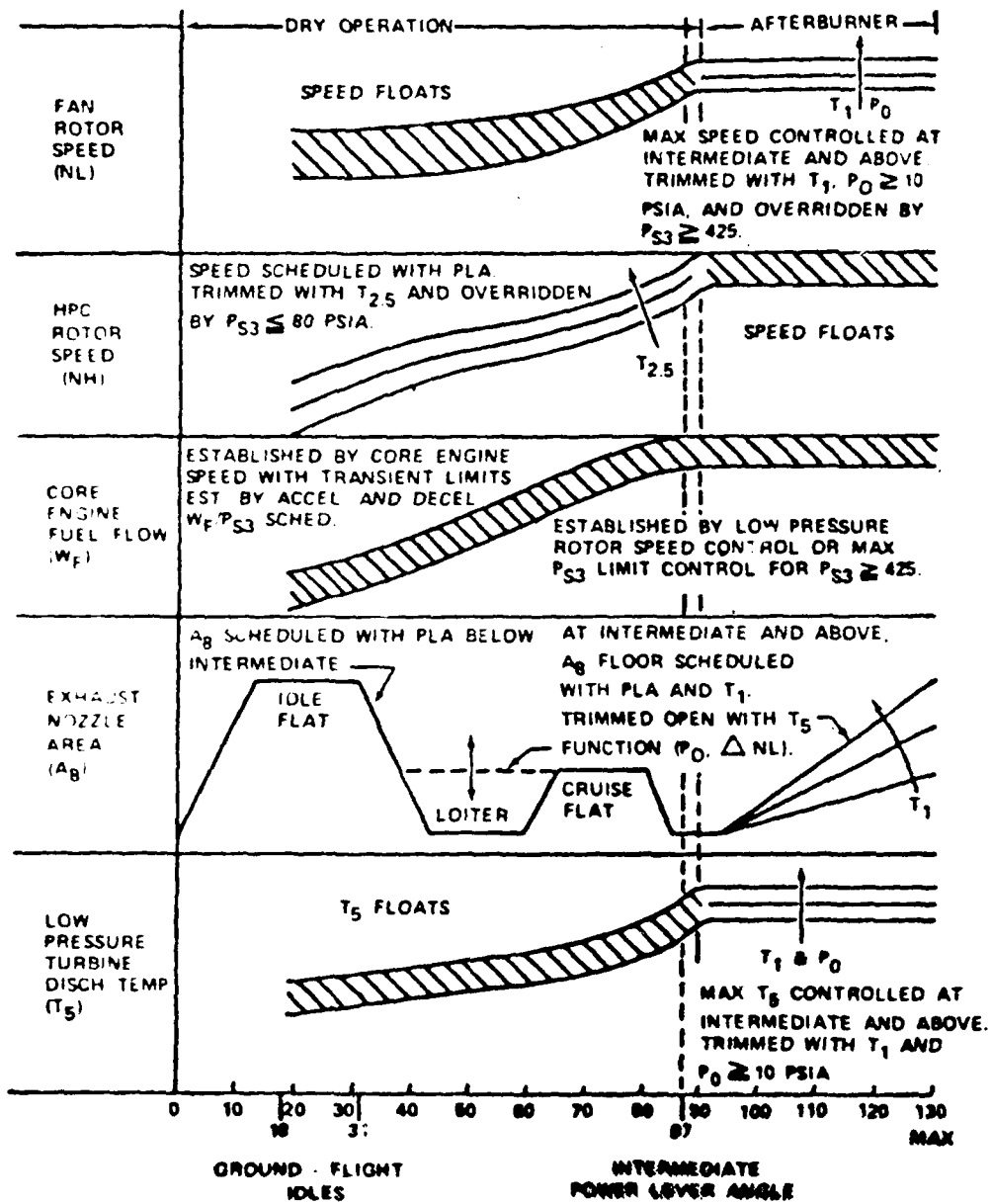
- 2-Stage Mixed Flow
- Soft Light-Off

FIG. 26



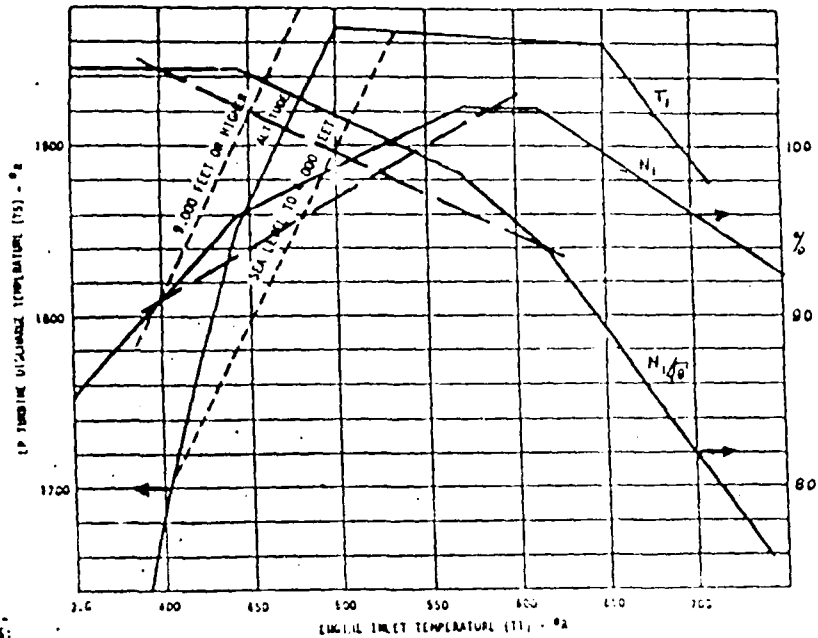
FUEL SYSTEM COMPONENTS

FIG. 27



CONTROL OPERATING MODES

FIG. 28



NOTES:

- (1) Between 4,000 and 9,000 feet (Pressure Altitude), 15 is determined by linear interpolation between dash lines up to the solid line.
- (2) Exact values at any condition T₁ can be obtained from the specification computer.
- (3) Turbine discharge temperature is reset as a function of core engine fuel flow.

FIG. 29

F404 Structures

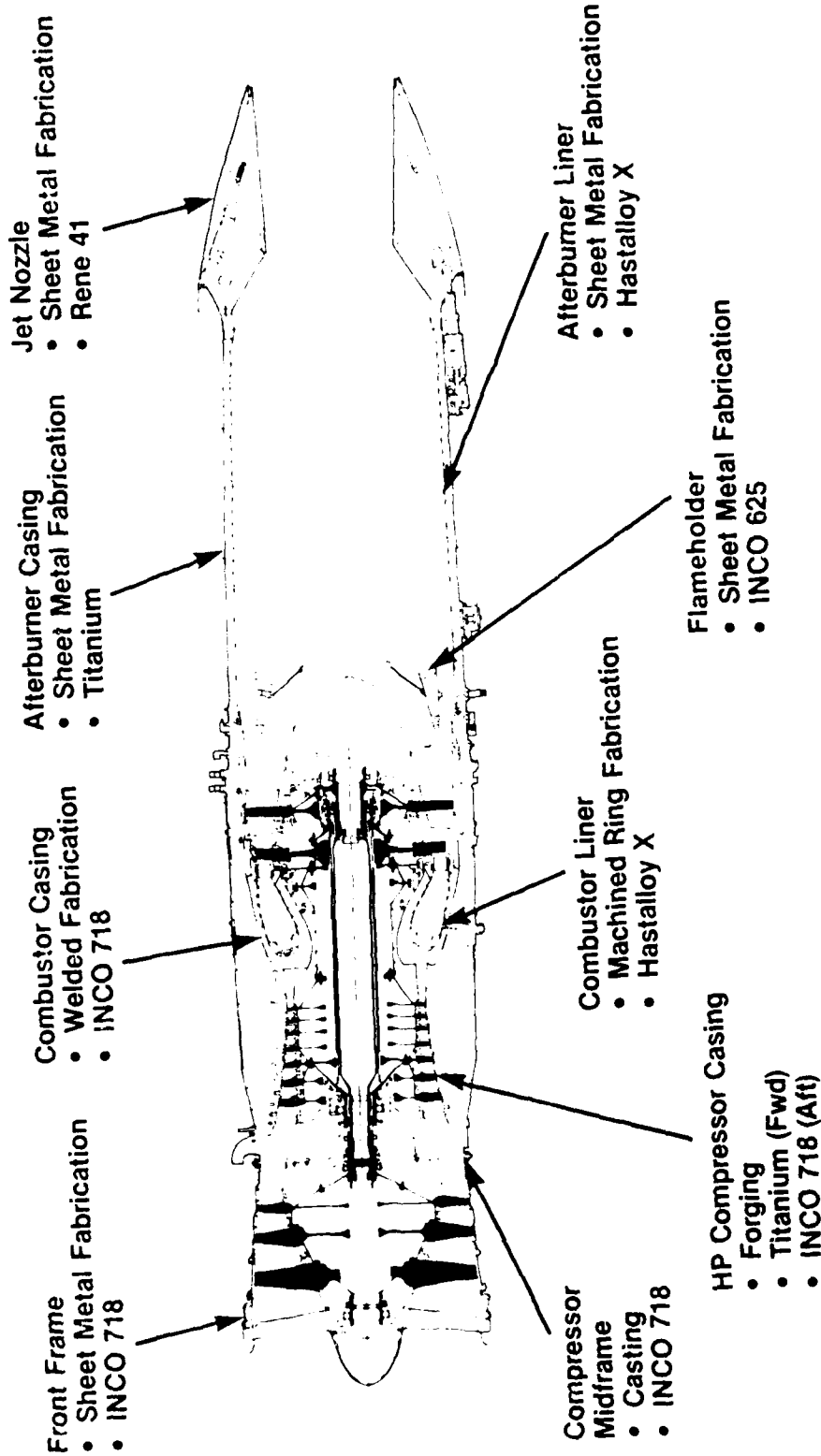


FIG. 30

F404 Turbomachinery

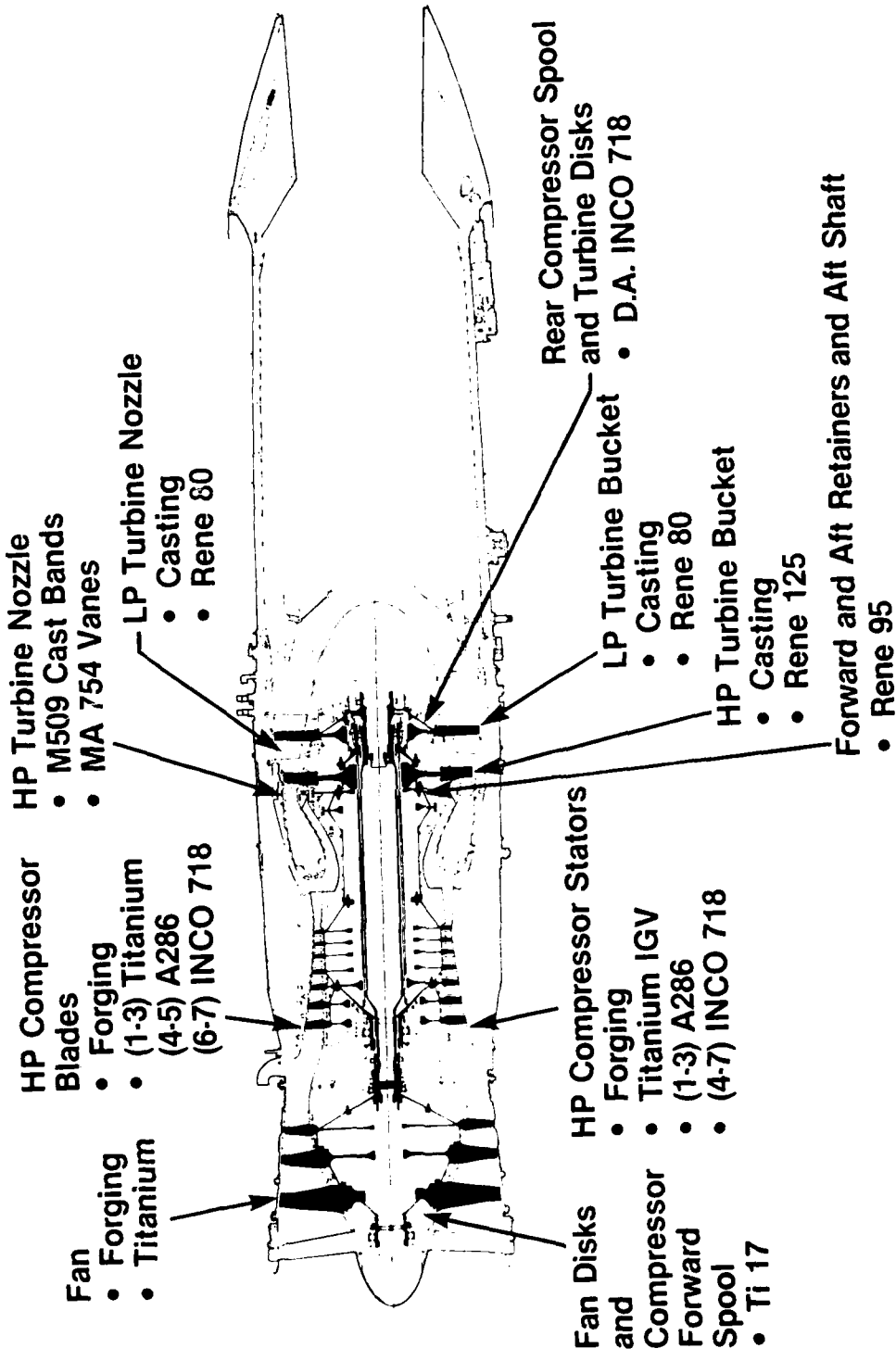


FIG. 31

Excellent Operability

- **A Turbofan with Turbojet Characteristics**
 - **High Combat Thrust without Lighting the Afterburner**
 - Saves Fuel — Longer Mission Capability
 - **Stall-Free Operation Throughout Flight Envelope**
 - Rocket/Gun Firings
 - Extreme Aircraft Maneuvers
 - Outstanding Inlet Compatibility
 - **Unrestricted Throttle Movements Throughout Flight Envelope**
 - **Rapid Acceleration/Deceleration**

A Fighter Pilot's Engine

FIG. 32

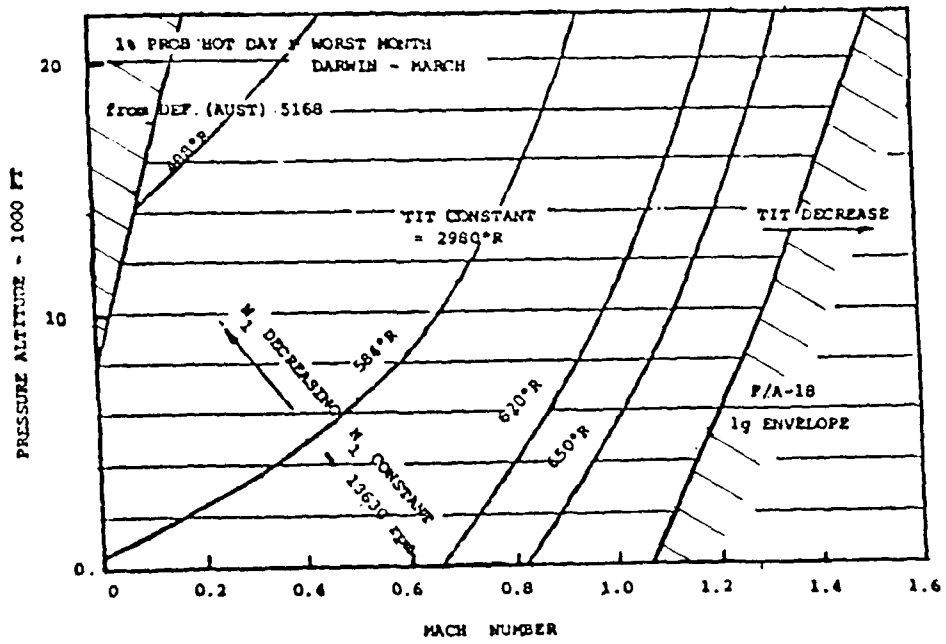
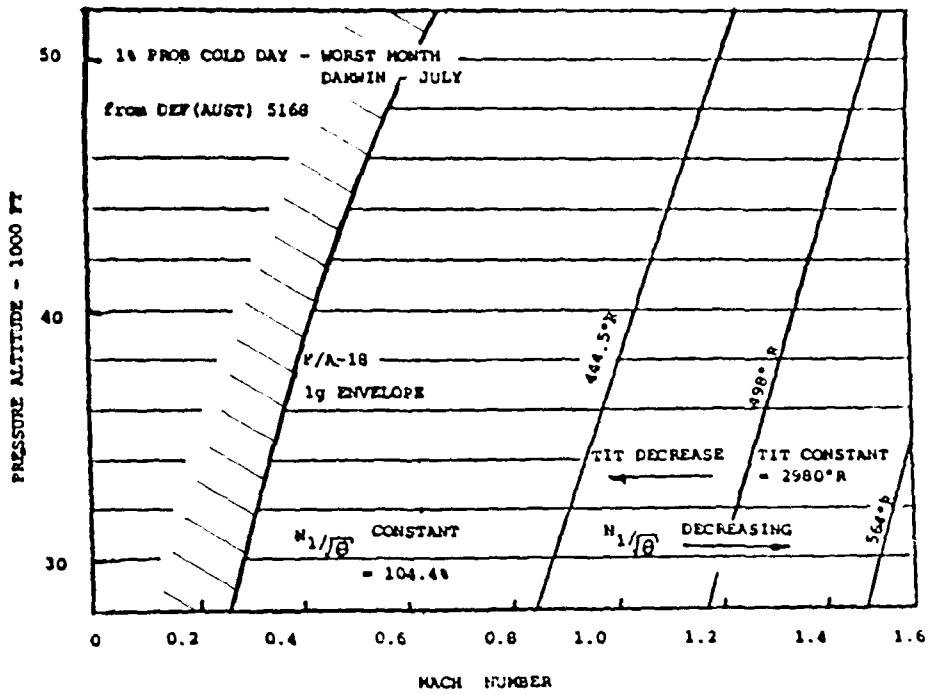


FIG. 33

“On-Condition” — Definition

“On-Condition” is directed at a specific unit (e.g., engine S/N XXX) in order to determine the “health” of that unit. The philosophy of On-Condition is to allow the life of a unit to be determined by the condition of the unit in comparison with a pre-determined standard, instead of some arbitrary hour limitation. It is “before-the-fact” maintenance.

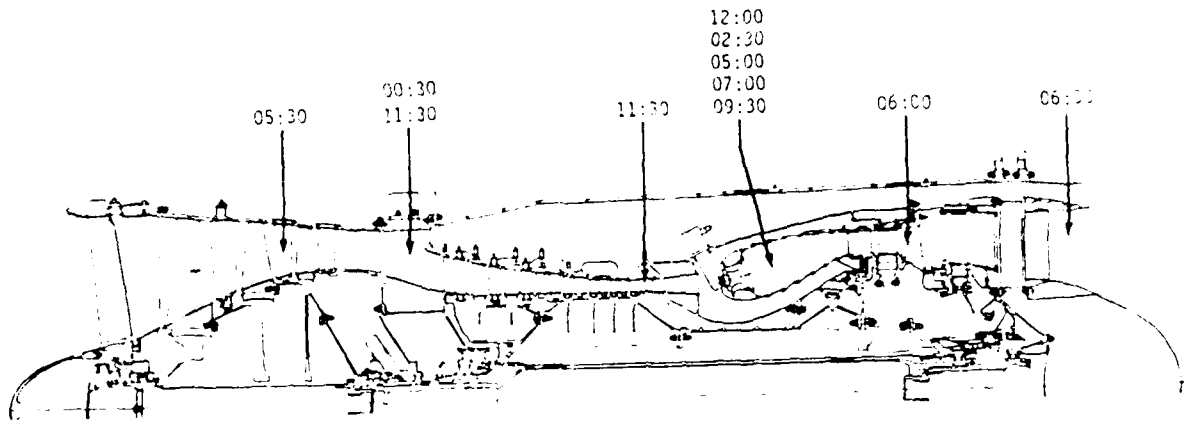
I E C M S
IN-FLIGHT ENGINE CONDITION MONITORING SYSTEM
RECORDS FOR POST-FLIGHT ANALYSIS

- LIFE USAGE INDICATORS
- MALFUNCTION INDICATORS
- PRE-POST EVENT RECORD
- PERFORMANCE TREND RECORD

+

- FLIGHT INCIDENT RECORD

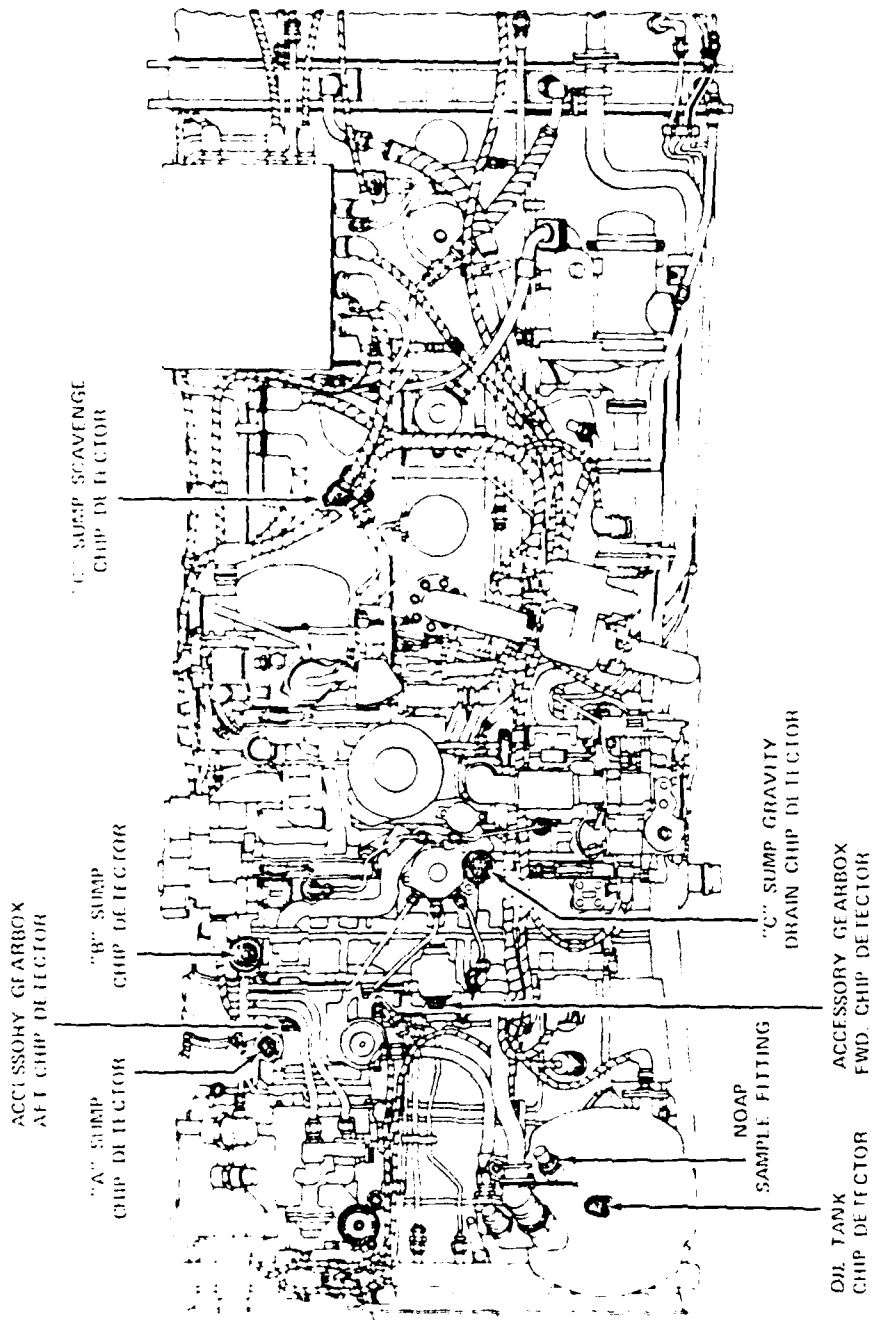
FIG. 35



CLOCK POSITIONS,
AFT LOOKING FORWARD

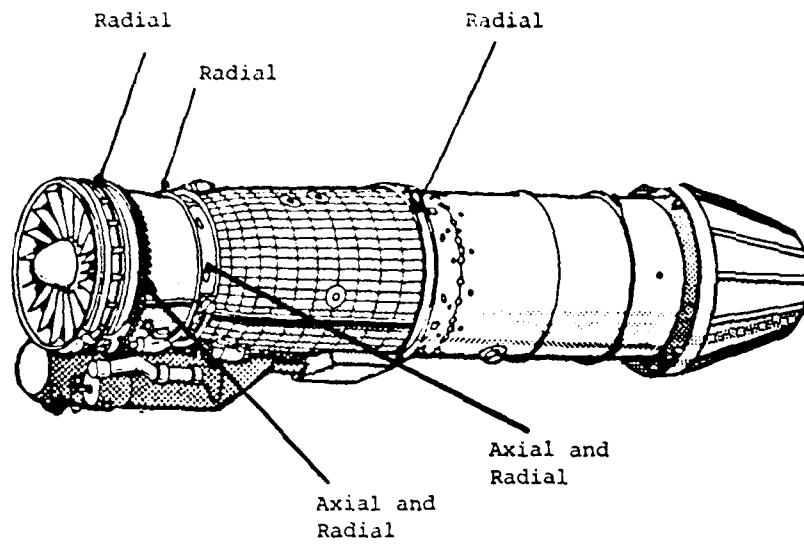
BORESCOPE PORT LOCATION

FIG. 26



CHIP DETECTOR LOCATIONS

FIG. 37



NOTE : ECMS and a
Mount-ring accelerometer
are on the starboard
side.

F - 404 ENGINE : ACCELEROMETER LOCATIONS (ARL TEST)

FIG. 38

Advantages Of Modular Program

- **Improved Aircraft Readiness Rate**
 - Reduced Shop Turnaround Time
 - No Aircraft "Open Hole" During Module Repair Cycle
- **Reduced Spare Engine Requirements**
 - Module Procurement Substitutes For Engine Procurement
 - Reduced Engine Pipelines
- **Ratio Of Modules Optimized**
 - Module Levels Procured Can Conform To Reliability Achieved For Each Module (MTBR)

F404 Engine Modules

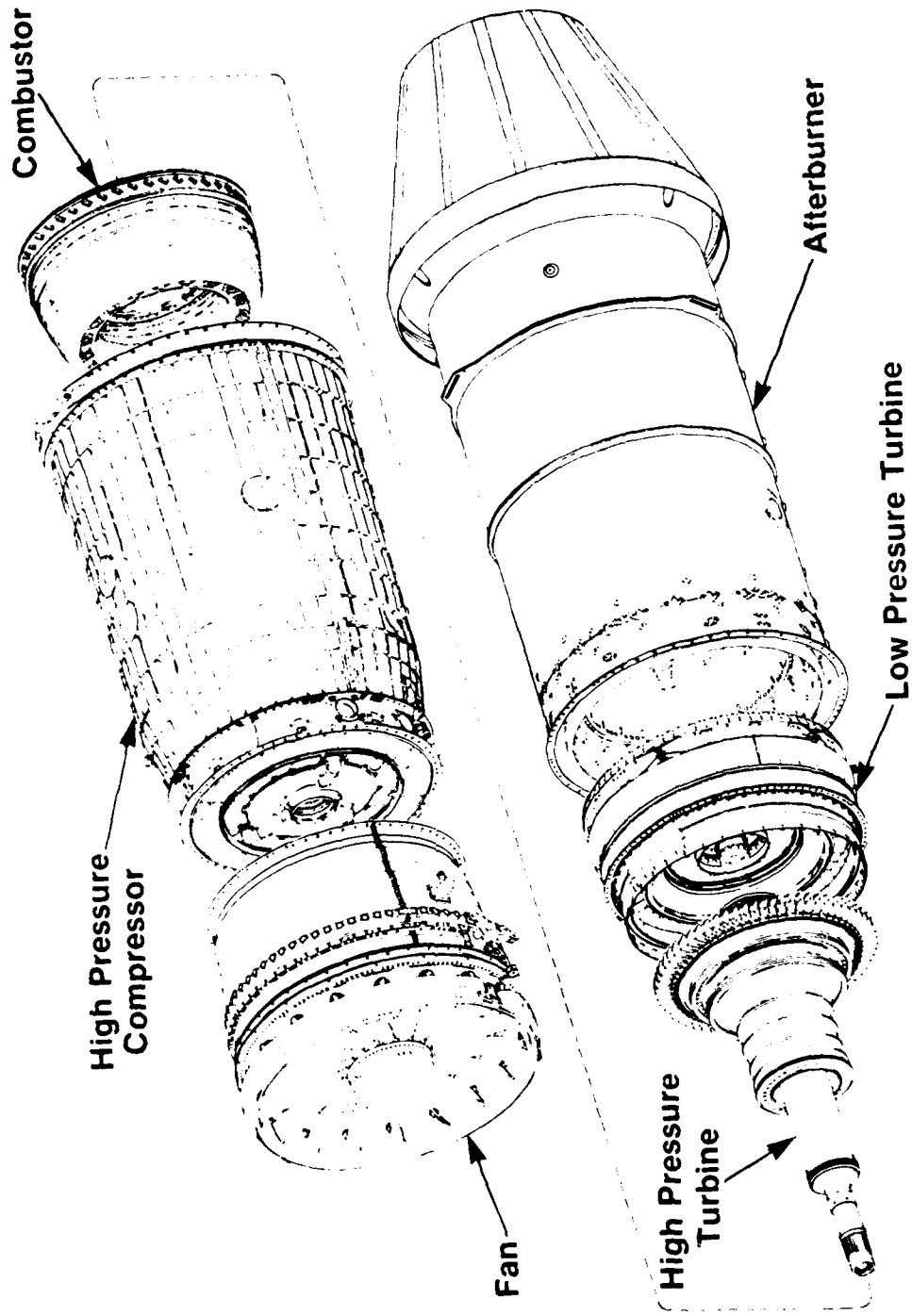


FIG. 40

DISTRIBUTION LIST

AUSTRALIA

DEPARTMENT OF DEFENCE

Defence Central

Chief Defence Scientist)
Deputy Chief Defence Scientist)
Superintendent, Science and Program) 1 copy
Administration)
Controller, External Relations,)
Projects & Analytical Studies)
Defence Science Adviser (UK) (Doc Data sheet only)
Counsellor, Defence Science (USA) (Doc Data sheet only)
Defence Science Representative (Bangkok)
Defence Central Library
Document Exchange Centre, DISB (18 copies)
Joint Intelligence Organisation
Librarian H Block, Victoria Barracks, Melbourne

Aeronautical Research Laboratories

Director
Library
Superintendent - Aero Propulsion
Divisional File - Aero Propulsion
Author: D. Frith

Materials Research Laboratories

Director/Library

Defence Research Centre

Library

Navy Office

Navy Scientific Adviser
RAN Aircraft Maintenance and Flight Trials Unit
Directorate of Naval Aircraft Engineering
Directorate of Naval Aviation Policy
Superintendent, Aircraft Maintenance and Repair

Army Office

Scientific Adviser - Army
Engineering Development Establishment, Library
Royal Military College Library

Air Force Office

Air Force Scientific Adviser
Aircraft Research and Development Unit
Scientific Flight Group
Library
Technical Division Library
Director General Tactical Fighter Project Office
Director General Aircraft Engineering - Air Force
Director General Operational Requirements - Air Force
HQ Operational Command (SMAINTSO)
HQ RAAF Base Williamtown (3 copies)
HQ Support Command (SLENGO)
RAAF Academy, Point Cook

Central Studies Establishment

Information Centre

Government Aircraft Factories

Manager
Library

DEPARTMENT OF AVIATION

Library
Flight Standards Division

INDUSTRY

Trans-Australia Airlines, Library
Qantas Airways Limited
Ansett Airlines of Australia, Library
Commonwealth Aircraft Corporation, Library
Hawker de Havilland Aust. Pty Ltd, Bankstown, Library
Rolls Royce of Australia Pty Ltd, Mr C.G.A. Bailey

UNIVERSITIES AND COLLEGES

Adelaide	Barr Smith Library Professor of Mechanical Engineering
Flinders	Library
La Trobe	Library
Melbourne	Engineering Library
Monash	Hargrave Library
Newcastle	Library
Sydney	Engineering Library

NSW

Physical Sciences Library
Professor R.A.A. Bryant
Mechanical Engineering

Queensland

Library

Tasmania

Engineering Library

Western Australia

Library
Associate Professor, J.A. Cole,
Mechanical Engineering

RMIT

Library

SPARES (10 copies)
TOTAL (90 copies)

DOCUMENT CONTROL DATA

1 a. AH No AR-004-033	1 b. Establishment No ARL-AERO-PROP-TM-423	2. Document Date JULY 1985	3. Task No AIR 82/46
4. Title THE GENERAL ELECTRIC F404 - ENGINE OF THE RAAF'S NEW FIGHTER		5. Security a. document: UNCLASSIFIED	6. No Pages 9
		b. title c. abstract: U U	7. No Refs -
8. Author(s) D.A. FRITH		9. Downgrading Instructions -	
10. Corporate Author and Address Aeronautical Research Laboratories P.O. Box 4331, Melbourne, Vic 3000		11. Authority (as appropriate) a. Sponsor b. Security c. Downgrading d. Approval	
12. Secondary Distribution (of this document) Approved for Public Release			
Overseas enquirers outside stated limitations should be referred through ASDIS, Defence Information Services Branch, Department of Defence, Campbell Park, CANBERRA ACT 2601			
13 a. This document may be ANNOUNCED in catalogues and awareness services available to ... No limitations			
13 b. Citation for other purposes (ie casual announcement) may be (select) unrestricted (or) as for 13 a.			
14. Descriptors Turbofan engines F404-GE-400 engine F/A-18 aircraft		15. COSATI Group 21050	
16. Abstract The F404 engine in the F/A-18 is representative of a new generation of military turbofan engines. The features of the engine that govern its performance and contribute to its maintainability are discussed. The intention is to give the non-specialist an appreciation of those factors materially affecting the operation of this type of engine.			

This page is to be used to record information which is required by the Establishment for its own use but which will not be added to the DISTIS data base unless specifically requested.

16. Abstract (Contd)		
17. Imprint Aeronautical Research Laboratories, Melbourne.		
18. Document Series and Number Aero Propulsion Technical Memorandum 426	19. Cost Code 47 1865	20. Type of Report and Period Covered
21. Computer Programs Used		
22. Establishment File Ref(s)		

END

FILMED

4-86

DTIC