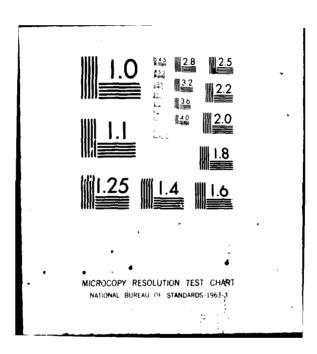
U	NCLASSIF	80 F	M SAND		FAA-A	VP-80-3	DOT-	-FA79WA	-4374 	
) of 2 MD NORS : 5									



Volume II

8 8 8

54

AD A 0 8

of Transportation Federal Aviation

Office of Aviation Policy Washington, D.C. 20590

The Allocation of Runway Slots by Auction

The Airline Management Game and Slot Auction Testing



THIS DOCUMENT IS BEST QUALITY FRACTICABLE. THE COPY FURNISHED TO DDC CONTAINED A SIGNIFICANT NUMBER OF PAGES WHICH DO NOT REPRODUCE LEGIBLY.

FAA-AVP-80-3

April 1980 Final Report

15

M.L. Balinski F.M. Sand

80

Document is available to the U.S. public through the National Technical Information Service, Springfield, Virginia 22161 6 11 01⁹ The contents of this report do not necessarily reflect the official views or policy of the Department of Transportation. This document is disseminated under the sponsorship of the Department of Transportation in the interest of information exchange. The United States Government assumes no liability for its contents or use thereof.

DISCLAIMER NOTICE

THIS DOCUMENT IS BEST QUALITY PRACTICABLE. THE COPY FURNISHED TO DTIC CONTAINED A SIGNIFICANT NUMBER OF PAGES WHICH DO NOT REPRODUCE LEGIBLY.

Technical Report Documentation Page 1. Report / 3. Recipient's Catalog No. 2. Government Accession No. FAA-AVP 80-3-VOL-2 18 G LIHE ALLOCATION OF RUNWAY SLOTS BY AUCTION . Apr The Airline Management Game and Volume II. Slot Auction Testing 8. Performing Organization Report No. F. M./Sand 🛲 M. L./Balinski 9. Performing Organization 10. Work Unit No. (TRAIS) ECON, Inc. Contract of Grant No. 900 State Road DOT-FA79WA-4374 Princeton, NJ 08540 Type Mepori and Period Covered 12. Sponsoring Agency Name and Address Office of Aviation Policy Final B Federal Aviation Administration Department of Transportation Sponsoring Agency Lod Washington, DC 20591 AVP-210 15. Supplementary Notes 17 16. Abstract The allocation of runway slots at the high-density airports by means of an auction is studied. Previous approaches to slot auctions have not allowed for the interdependency of slot values to the air carriers--a single slot for a landing of an aircraft is likely to be of little value without a corresponding slot for a subsequent take-off of that aircraft. A Slot Exchange Auction is designed, its theoretical properties and practical implementation discussed. It is shown to allow the slot market to reach an efficient equilibrium under competitive conditions. The Airline Management Game is used to create a simulation test of the Slot Exchange Auction and its associated continuous market, the slot exchange. 17. Key Words 18. Distribution Statement Slot, exchange, auction, trading, air Document is available to the public through the National Technical Information carriers, allocation, runway, capacity, 22151 market, airport, airline, aircraft, man-Service, Springfield, Virginia agement, game 19. Security Classif, (of this report) 20. Security Classif. (of this page) 21. No. of Poges | 22. Price **Unclassified** Unclassified 176 Form DOT F 1700.7 (8-72) Reproduction of completed page authorized Bm S/C 393807

المراجع والمراجع والمراجع

ACKNOWLEDGEMENTS

The findings of this report have grown out of a joint project between ECON, Inc. and Flight <u>Transportation Associates</u>, supported by the Office of Aviation Policy of the Federal Aviation Administration, in which the following have notably participated: Pradeep Dubey, Antonio Elias, Jai Jaikumar, David Lawson, Robert Simpson, Peter Stevenson, Nawal Taneja and Robert Weber, in addition to the authors.

It is a pleasure to express our appreciation to John Rodgers of the FAA/AVP for his frequent help and continuous interest in this project.

and the state of the second second

Accession	TOT
MITS CAL DEN TAS Lanzanounce Jul ificat	
By	
	Lity Codes Id and/or
Dist 5	pecial 3 4

TABLE OF CONTENTS

anna dhanin 12 si ad badan babbi i a

วิทธิ และ และสาว เหมาะมีความแก้งได้หว่างหนึ่งให้ครั้งหลังได้ที่เหตุมหนึ่ง

.

A DESCRIPTION OF A

H

Cha	oter	Page
	Acknowledgements	ii
	List of Figures	iv
	List of Tables	v
1.	Introduction	1
2.	Testing Concepts and Problems	3
3.	Testing the Slot Exchange Auction	6
	 3.1 Background 3.2 Organization 3.3 The Airline Management Game 3.4 Reference Material on Slot Auction Provided to Participants 	6 8 11 15
4.	Results and Analysis	25
	 4.1 The Slot Exchange Auction Results 4.2 Levels of Service 4.2.1 The System Responses 4.2.2 Service to Small Communities 4.3 The Slot Exchange 	26 30 31 33 34
5.	Comments by the Airlines	40
6.	Conclusion	72
	References	73
	Appendix AData Appendix	74
	Appendix BResults of December 1979 Exercise	160

iii

LIST OF FIGURES

Figure				
3.1	Evaluation of Runway Quota Allocation MechanismsDaily Schedule	9		
3.2	System Route Map	13		
4.1	Aftermarke Form ABuy	35		
4.2	Aftermarket Form BSell	36		

1

the states

and the same any

Anie Water

LIST OF TABLES

Table	Page
3.1 Aircraft Data	75
3.2 Network Data	77
3.3 Airport Data	88
3.4 Initial Schedules	90
3.5 Traffic Data	105
4.1 Net Earnings Before and After Slot Allocations	27
4.2 Slot Prices at End of Iteration 1.1	27
4.3 Slot Prices at End of Iteration 1.2	28
4.4 Slot Prices at End of Iteration 1.3	28
4.5 Potential Slot Revenues	28
4.6 Net Earnings Before Taxes or Slot Payments	29
4.7 Potential Slot Payments After Each Bidding Round	29
4.8 Net Earnings After Slot Payments, After Taxes	29
4.9 Operating StatisticsBase Case	32
4.10 Operating StatisticsPeriod 1	32
4.11 Operating StatisticsPeriod 2	32
4.12 Period 1 Schedules	114
4.13 Period 2 Schedules	130
4.14 Period 1 Traffic Data	142
4.15 Period 2 Traffic Data	151
4.16 Small Communities Average Enplanements/Day	34
4.17 Aftermarket ActionPeriod 1	37
4.18 Aftermarket ActionPeriod 2	38

LIST OF TABLES (Continued)

Table	Page
4.19 Slot Payments in Auction and Aftermarket	38
B.IA Slot Prices at End of Iteration 1	165
B.IB Slot Prices at End of Iteration 2	166
B.2 Potential Slot Revenues	167
B.3 Net Earnings Before Taxes or Slot Payments	167
B.4 Potential Slot Payments After Each Bidding Round	168
B.5 Net Earnings After Slot Payments, Before Taxes	168
B.6 Systemwide Performance of All Five Airlines	169

A COMPANY OF THE OWNER

State of the state

and the second second

Sec. 1

And the second

I. INTRODUCTION

In order to evaluate the viability of the Slot Exchange Auction^{*} and subsequent continuous slot exchange, an interactive computer simulation of actual slot auctions was conducted using the Airline Management Game; participants from the airlines acted as airline executives engaged in bidding and scheduling activities. This Evaluation Exercise held at FAA headquarters in Washington, D.C., February 11-15, 1980 also included a test of the FAA's Administrative Allocation procedure. An earlier version of the same simulation was conducted at M.I.T. in December 1979 by the staff of Flight Transportation Associates (FTA). The scenario included five competing airlines and 17 airports with three of them being capacity-limited. These three airports carried about 66 percent of all the traffic in the initial schedules (base case), and there was a total of 480 flights per day in these schedules. Hourly quotas for the three capacity-limited airports were established by the game administrator based on the airport activity profiles obtained in the base case. They were 13, 12 and 11 for the three airports designated AAA, BBB and CCC respectively in the Evaluation Exercise scenario.

The five teams were assigned FTA staff members and airline participants. They were instructed to maximize short-run airline profits using a fixed fleet of aircraft and fixed fares, but free choice of routes and schedules. The schedules were assumed to operate for six months at a time.

This second volume of the Final Report on runway slot allocation by auction presents an outline of the Airline Management Game, the experimental design, the bidding rules and the results and analysis of the Evaluation Exercise. After the

[&]quot;The terms "Slot Exchange Auction" and "slot exchange," as used in this report refer to the same objects as the earlier names "Trading Post Auction" and "aftermarket."

exercise the airline participants were invited to submit written comments and responses to FAA questions about the two methods of slot allocation and the testing procedure used for evaluating them. Their replies are included in facsimile as Section 5 of this volume.

The airline participants were given a rather large amount of scenario data--operating statistics, cost parameters, initital schedules, system route maps, etc.--and a set of instructions for bidding in each of the two allocation methods. We have not included all of this material here since most of it is covered in the report in a slightly different form, and furthermore this report deals with one of the two methods. We have tried to include all data relevant to the task of interpreting the results of the Evaluation Exercise concerning the Slot Exchange method. The results of the earlier (December) exercise are summarized in Appendix B.

2. TESTING CONCEPTS AND PROBLEMS

This approach is new. There is no mathematical guarantee that the tatonnement process will converge. The circumstantial evidence is very positive, but not completely convincing. The 42 interdependent trading posts of today may well become 142 trading posts tomorrow. Can the airlines cope with this complexity? What are the effects of this complex dependency on the convergence behavior of the repeated Trading Post auction?

These are difficult questions which demand careful study and thorough experimentation.

When should the auctioning process be stopped? It seems highly unlikely that the procedure will of itself reach a point where no party wishes to change a bid-the sheer dimension of the number of trading posts would seem to admit the wish of at least one airline to change its bid at at least one trading post. A <u>sine qua non</u> is that the conditional outcome of any round of auction be a potential final outcome: this to ensure that each airline reveal its true demands to the extent it knows them. The threat must exist that, at any time, the hammer may fall.

The dynamics of the conditional outcomes are complex. After several rounds one may expect that many prices and allocations begin to repeat, with the "action" occurring at the margin. "Chases" may occur, with prices at one or several trading posts driving upwards as participants compete for the marginal slots at those posts. These followed by some, perhaps "too many," airlines dropping out, the demands at the corresponding posts dropping below supply. Because of the indivisible nature of the commodity it may well be necessary to impose, in such cases, a positive trading post price even in the presence of excess supply. This "threshold" price or "entrance fee" would be introduced to prevent cyclic phenomena at trading posts

(caused entirely by the indivisibility of slots): a trading post price might slowly climb in successive rounds, then suddenly drop to \$0 with several bidders dropping at once, then begin climbing again with \$0 being an attractive price to those who had dropped out, etc.

So a stopping rule must be defined. There are several candidates.

1. By <u>convergence</u> of <u>price</u>. If, in two successive rounds of bidding, the 42dimensional trading post prices are sufficiently close to one another, stop. For example, if $p = (p_1, \ldots, p_{42})$ is one set of prices and $p' = (p'_1, \ldots, p'_{42})$ the next set and max_i $p_i - p'_1 \leq \varepsilon$, for ε some positive number defined at the beginning of the auctioning process, then stop.

2. By <u>convergence of allocations</u>. If, in two successive rounds of bidding, the trading post allocations to airlines are sufficiently close to one another, stop. For example, suppose airline i receives a_{ij} slots at trading post j in one round, receives a'_{ij} in the next round, and $\max_{ij} |a_{ij} - a'_{ij}| \leq \delta$, for δ some small positive integer defined at the beginning of the auctioning process, stop.

3. By <u>vote</u>. If, at any round, m% ($m \ge 50$) of the bidders are satisfied with the conditional allocations, then stop.

4. By payment. If, after weak "convergence" by 1, 2 or 3, an airline wishes to change its bid, then it pays a fixed sum for the privilege of so doing.

5. By <u>price-averaging</u>. If, after several rounds of bidding have taken place, the administrator observes cyclicities in the successive trading-price vector, then the rules of price formation are changed and the conditional trading-price becomes a weighted average of past prices. For example, let p^1 , p^2 ,..., p^{k-1} be the trading post prices of the first k-1 rounds as usually determined, and p^k that of the kth round as usually determined. Then the commissioner announces instead $p^k = \sum_{j=1}^{k} \lambda_j p^j$, with $\sum_{j=1}^{k} \lambda_j = 1$ and $0 \le \lambda_1 \le \lambda_2$... $\le \lambda_k$. 6. By <u>successive shares</u>. Instead of seeking convergence over the entire process, one could seek it by "successive shares." Each round of bidding results in a final but partial allocation. The first round is conducted as usual: conditional trading post prices are found. The top q_1 , with $q_1 < q$, e.g., $q_1 \leq q/10$ of the bidders in a market with quota q are actually awarded the slots at the trading post price. The second round is conducted as usual, but with the quotas reduced to $q - q_1$: conditional trading prices are found and the top q_2 (where $q_1+q_2 < q$) of the bidders in each market are again awarded the slots at the trading post price. And the procedure iterates, with the number of winners per round q_1, q_2, \ldots, q_k defined in advance with $\Sigma q_i = q$ and perhaps decreasing as the rounds proceed. Convergence is assured by construction. The airlines know "where" they are at any point and react accordingly. Uniform trading post prices are lost, but the ultimate allocation should be close to an economic equilibrium.

3. TESTING THE SLOT EXCHANGE AUCTION

3.1 Background

The experimental testing of the Slot Exchange Auction poses a number of difficult problems as pointed out in the previous pages. Foremost among these is the need to have bidding which is related to airline network scheduling in a meaningful way. If the structure of slot interdependence, which we have repeatedly emphasized in this report, is not present in the experiment, the prices attached to slots will have no relationship to the airlines' valuation of slots. Since the real airline scheduling problem is immense and complex, there is a need for a simplified structure in the experiment. The Airline Management Game (AMG), developed and tested by Antonio Elias¹ of M.I.T. and Flight Transportation Associates, is a vehicle for providing a simplified structure of the air transportation network. It is a combination "game" and computer simulation in which the "players" make realistic airline management decisions. These decisions are fed into a computer along with CAB air traffic data, airline operations cost parameters, and air transportation block times and distances. The computer simulation allocates the passenger demand among the competing air carrier services offered by the competing "players," which in practice are teams rather than individuals. It also prints profit and loss, balance sheets, OAG-type schedules, and network and operating statistics for the game. The "players" have a chance to read the computer output, evaluate their performance in the competitive transportation scenario and revise their decisions. After some number of iterations, the results can be regarded as final.

The initial idea for an experiment to evaluate the effects of allocating slots by auction was as follows:

- 1. An air transportation scenario for five competing airlines would be created by Dr. Elias.
- 2. The "players" would be told the hourly quotas at three congested airports and required to bid in a Slot Exchange Auction for runway access slots at those airports. However, many rounds of bidding would be needed (held). A computer program would process the bids to determine slot prices and allocations at the three congested airports.
- 3. The AMG would be played with the slots restrictions imposed on the airlines by the auction results.
- 4. The Slot Exchange Auction and the AMG would be repeated at least once.

In December 1979 a trial exercise of this sort was held at the Flight Transportation Laboratory at M.I.T. It was observed by Harvey Safeer and John Rodgers of the FAA, participants were drawn from the staff of ECON and the FTA, and it was conducted over approximately five days. As a result of this trial exercise it was decided to invite airline participation in early 1980 for a slot allocation evaluation exercise using the AMG and the Slot Exchange Auction. The purposes of this were to expose some representatives of the airline industry to the allocation methodology and obtain their reactions and to evaluate the approach to slot allocation, together with an alternative administrative approach. The December trial exercise involved considerable fine tuning of the AMG and Slot Exchange Auction, and as such can be regarded as a necessary developmental step in creating the procedures, forms, computer software and rules of the game for the evaluation exercise. Neither exercise permitted convergence of the Slot Exchange Auction within the resource constraints available. There was a clearly demonstrated need to have more rounds of bidding to bring the slot market into equilibrium. Results of the trial exercise are presented in summary as Appendix B.

3.2 Organization

In order to evaluate two alternative methods of allocating runway access slots to air carriers at congested airports, the FAA sponsored a week-long evaluation exercise in Washington, D.C. on February 11-15, 1980. A daily schedule for this exercise was provided in advance to participants (Figure 3.1). The heart of the exercise was the Airline Management Game (AMG)--a realistic computer model which permits competing airline teams to schedule their air transportation networks, and learn the performance and financial results through simulation of the resulting traffic flows, costs, revenues, load factors, etc. There were five airline teams: Blue, Gold, Green, Red and White.

With the assistance of the Air Transport Association (ATA), management and professional staff from the airlines were invited to participate in the exercise. Those who accepted the invitation were assigned to the five teams as follows:

AMG Team	Airline	Participant
Blue	Delta Piedmont	W. Jeffrey Rowe Bob McAlpin
Gold	Eastern USAir	Bill Pacelli Jerry Frissora
Green	United Braniff	Ian Bamber Jim Bowers
Red	American American	Brad Jensen Don Roach
White	TWA	R. J. Zablocki

In addition each airline team was assigned a professional staff member of Flight Transportation Associates who served as an experienced user of the AMG software and provided data processing capabilities to his team. Antonio Elias of M.I.T. and the FTA was the Game Administrator.

The major purposes of the evaluation exercise were:

DAY	AM/PM	ACTIVITY
MONDAY FEBRUARY 11	0830-1000 1000-1015 1015-1130 1130-1230 1230-1630 1230-1330 1630-1700	BRIEFINGTHE AIRLINE MANAGEMENT GAME BREAK BRIEFING, THE TRADING POST AUCTION LUNCH PREPARE DESIRED PERIOD 1 FLIGHT SCHEDULES OBSERVERS ONLYBRIEFINGADMINISTRATIVE ALLOCATION BRIEFING ACTIVITIESFEBRUARY 12-15
TUESDAY FEBRUARY 12	0830-1200 1200-1300 1300-1500 1500-1700	TRADING POST AUCTION NO. 1 LUNCH PREPARE FINAL PERIOD 1 FLIGHT SCHEDULES PERIOD 1 SIMULATION
WEDNESDAY FEBRUARY 13	0830-1030 1030-1230 1230-1330 1330-1530 1530-1700	PREPARE DESIRED PERIOD 2 FLIGHT SCHEDULES TRADING POST AUCTION NO. 2 LUNCH PREPARE FINAL PERIOD 2 FLIGHT SCHEDULES BRIEFINGADMINISTRATIVE ALLOCATION (SIMULTANEOUS PERIOD 2 SIMULATION)
THURSDAY February 14	0830-1200 1200-1300 1300-1500 1500-1700	ADMINISTRATIVE ALLOCATION NO. 1 LUNCH PREPARE FINAL PERIOD 1 FLIGHT SCHEDULES PERIOD 1 SIMULATION
FRIDAY FEBRUARY 15	0830-1030 1030-1230 1230-1330 1330-1430 1430-1530 1530-1700	PREPARE DESIRED PERIOD 2 FLIGHT SCHEDULES ADMINISTRATIVE ALLOCATION NO. 2 LUNCH ADMINISTRATIVE ALLOCATION NO. 2 PREPARE FINAL PERIOD 2 SCHEDULES CLOSING FORUM (SIMULTANEOUS PERIOD 2 SIMULATION)

FIGURE 3.1 EVALUATION OF RUNWAY QUOTA ALLOCATION MECHANISMS--DAILY SCHEDULE (AS REVISED FEBRUARY 7, 1980).

- 1. To test the feasibility of two slot allocation mechanisms in a fairly realistic airline scheduling environment:
 - A. The Slot Exchange Auction

and the state of the

- B. The FAA Administrative Allocation
- 2. To obtain comments from the airlines on their reactions to the two allocation methods
- 3. To obtain rough estimates of the economic and air service effects of slot rationing.

The two different allocation methods were evaluated by using them to allocate slots within the context of the Airline Management Game. The first on the timetable was the Slot Exchange Auction; slots were auctioned off to the competing airline teams as described in Volume I. Two days were allowed for this part of the evaluation exercise. The second method on the evaluation timetable was the Administrative Allocation, a nonprice method developed by Ken Geisinger at the FAA. It will not be described in this report. The Slot Exchange Auction was administered in the evaluation exercise by Francis Sand. Before the application of the slot allocation method, the airline teams developed their preferred schedules without consideration of slot restrictions (quotas). After examining airport activity profiles for this base case, the game and auction administrators set hourly quotas for three of the 17 airports in the scenario. The Slot Exchange Auction followed; airline teams had to bid for their slots. They were allowed to reschedule their airlines following the auction to maximize profits in the restricted game. Only those slots which they had acquired at the auction could be utilized. A similar approach was followed in relation to the Administrative Allocation. The same starting schedules and quotas were used as for the auction; accordingly it was not necessary to repeat the initial step of unrestricted scheduling.

3.3 The Airline Management Game

The Airline Management Game placed a team of players in the role of airline management responsible for airline scheduling and market, fleet and financial planning. The Game Administrator created a scenario for one or more competitive airlines by providing historical and forecast information on schedules, traffic, revenue, costs and airline finances, and a set of rules and objectives for the players. Each airline team developed period schedules, having determined appropriate route development, marketing strategies and fleet plans. The results of team decisions were then simulated in a computerized model which estimated the traffic and revenues and consequently the financial results for each airline.

During this exercise the objective of each airline team was to schedule its flights so as to maximize its short-run profits with a fixed fleet of aircraft. Market strategies open to individual airlines consisted of changes in schedules and routes. Schedules had to be feasible in terms of fleet size and slot allocations. No route authority was required because complete deregulation was assumed.

The heart of the game is a computerized traffic allocation process which determines the through and connecting passenger traffic on each segment of each flight. It is based on the complete services offered in all markets and is sensitive to:

- Differences in fares^{*}
- Differences in departure time
- Differences in flight times, including the added inconvenience of connections
- Effects of high load factors on certain flight segments.

Not used in the evaluation exercise. Fares differed by trip length, but not by discretion of the airline team.

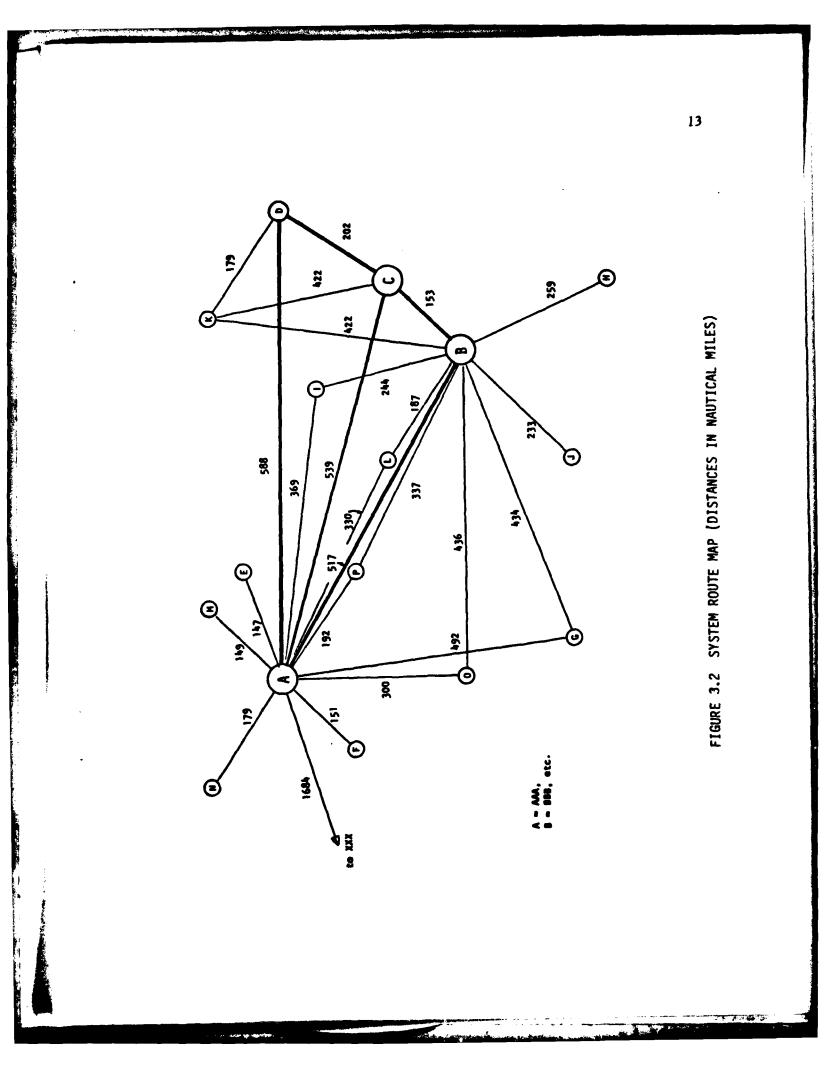
The scenario for the evaluation exercise comprised 17 airports grouped in four major classes according to the market and traffic characteristics:

- 1. There were four major hubs: Alpha (AAA), Bravo (BBB), Charlie (CCC) and Delta (DDD). About half of the total network activity was made up of the traffic between these four major airports. Of these, the first three (AAA, BBB and CCC) were capacity restricted and the participants had to compete for slots at these airports.
- 2. There were six intermediate airports: Echo (EEE), Foxtrot (FFF), Golf (GGG), Hotel (HHH), India (III) and Juliet (JJJ). There was considerable activity between the four major airports and these six, as well as between these six airports.
- 3. The third group was comprised of six minor airports. There was significant traffic between these airports and the previous ten, but no traffic among these minor airports.
- 4. The fourth group was a single airport: X-ray (XXX). This was a special long-haul case, and there was traffic only between XXX and AAA, and XXX and BBB. There was no traffic between XXX and any other airport.

A system route map (Figure 3.2) was provided to the players.

Individual airline teams did not know exactly what the demand was in any of these markets; however, they had the existing traffic data. The game model allowed some stimulation or contraction of demand due to improvement or decrease in the level of service offered (including the case where the market is not served at all).

There were five airlines competing in this network: Blue (BL), Gold (GL), Green (GR), Red (RD) and White (WT). Each of these airlines had, during the past, a traditional pattern of service, which is reflected in the given initial schedule. Under deregulation they were free to serve any market, subject to the limitations of their available equipment. For purposes of this exercise, fares for all airlines were limited to a simple tariff of \$23.40 plus 10 cents per nautical mile (8.68 cents per statute mile).



The participants' fleets included three types of aircraft: DC9, 727 and 707. The technical and economic characteristics of each of these aircraft are summarized in Table 3.1.^{*} The composition of each participant's fleet was fixed as follows:

- 1. Blue: ten 727s and six 707s
- 2. Gold: eight 727s and six DC9s
- 3. Green: nine 727s and six DC9s
- 4. Red: four 727s and three DC9s
- 5. White: six DC9s.

and the second

- Nr. .--28

It was not necessary for a team to use all of its aircraft; however, airlines incurred some daily ownership costs for all the aircraft owned, whether they flew them or not. Table 3.2 shows the distance in nautical miles between each possible pair of airports in the system, as well as the block time required to fly that particular link. This block time includes the flight time, and the average air and ground maneuvering times, including average ATC delays. The minimum gate time for a flight's intermediate stop was 20 minutes. The minimum gate time to turn around an aircraft at the end of a flight and make it ready to start a new flight was 45 minutes.

Teams could declare on-line connections. Note that the simulated passengers only took advantage of published connections (i.e., they did not generate their own connections). Table 3.3 shows the data on each airport, including the minimum connect time (the same for all airlines) at each airport.

Interline connections were not allowed.

Tables 3.1 through 3.5 are presented in the Data Appendix because they are too voluminous to include in the body of the report.

Each simulation iteration simulated a six-month period of operations. Therefore, the participants were required to maximize their short-term objectives, e.g., before-tax profit.

Tables 3.4 and 3.5 contain initial schedules for each airline and associated base period traffic data and economic performance of each airline. Separate material was provided to individual airline teams on the profitability of individual flights during the base period.

3.4 Reference Material on Slot Auction Provided to Participants

The following pages contain the instructions on bidding in the Slot Exchange Auction. They are reproduced here exactly as given to the five airline teams prior to commencement of the exercise.

Slot Auction Description and Instructions

1. Introduction

You are taking part in an experiment to determine the effects of runway slot auctions on airline scheduling and profitability. The FAA imposes hourly quotas on landings and takeoffs at the high density airports. At certain peak hours of the day, the airlines wish to schedule more flights at these airports than there are slots available under the FAA rules. In the experiment, we will simulate the slot restrictions, and an allocation of restricted slots will be made by means of an <u>auction</u>. A slot price will have to be paid for slots at peak hours at congested airports. The purpose of charging a price for such slots is to resolve, in an economically efficient way, the question of which airlines obtain slots when there is an insufficient supply of slots.

You will be asked to prepare bids for slots after you have completed a first cut at desired schedules without slot restrictions. The method of bidding and the determination of slot prices and allocations will be explained in detail below. After you have submitted bids for all the slots (at all quota-airports) that "interest" you, a computer program will determine an allocation and a single price for slots at each peak hour at each congested airport. The price may be nominal--this happens if the number of slots requested in all the bids for one airport at one peak hour is less than the FAA quota. The auction results are not necessarily final. You may study them and prepare new bids if you wish,

providing the auctioneer has not closed the auction market. On the first round of bidding you can be assured of another chance to bid; therefore, you will get a chance on the second round to correct "mistakes" in bidding which may arise due to unfamiliarity with this type of auction.

2. The Auction Procedure (Trading Post Method)

To introduce the concept of the auction we ask you to imagine that there are a number of trading posts at which slots are offered for sale--one for each peak hour at each congested airport. All these trading posts will be open simultaneously. Airlines wishing to buy one or more slots at particular trading posts prepare bids (offers to pay a specified amount of money) for these slots as follows:

	<u>Airline A</u> Trading Post "i"	Bid (\$/opr)	1	Numbe 2 100	3	4 70	5 0
This	means that airline A is of	ffering to pay \$15	50 for	one	slot,	*	
\$100	for each of the second and	d third slots and	\$70 1	for a	fourt	:h	
slot	at trading post "i," at a	specific hour at	a spe	ecific	: airp	ort.	
If av	warded one to four slots, i	it will pay the ar	nound	ed pr	rice v	hich	
wi11	not exceed the bids. Supp	oose a <u>slot</u> price	of \$9	95 is			
annou	unced. Then airline A will	l be awarded 3 slo	ots at	\$95-	the		
fourt	th slot, for which only \$70) was bid, is not	award	ied to	A .		

^{*} A slot is defined as a right to conduct one runway operation within a 60-minute period at a designated airport every day for six months. Pricing is expressed in dollars per operation. The actual payment for slots awarded will be price times 182.

The bidding rules are as follows:

1. Airlines prepare their bids privately.

- Airlines bid for as many slots as they wish at <u>all trading</u> post <u>simultaneously</u>.
- 3. When the auctioneer closes the auction at any time after the first round of bidding, the airlines must accept and pay for the slots awarded them. Slot prices will never exceed bids for slots actually awarded, and frequently will be substantially lower. The payment schedule for slots awarded may be spread out, interest-free, over the six months of slot utilization.
- 4. If more than one bid is made at the slot price, but the quota is such that not all bids at that price or higher can be awarded, then a random allocation is used to determine which among the airlines bidding the slot price are awarded slots.
- 5. At the end of each round of bidding, the slot prices and allocations are computed and all airlines are informed of the results. If this is not the last round, they may study the computer results and make any changes they wish in their bids, subject to the rules.
- There is no need to resubmit unchanged bids as these are stored in computer memory. Only those bids which are to be

changed in any way need be submitted, and <u>these must be</u> <u>submitted in full</u>. Thus, if the bid was originally:

Airline A, Round 1Slot NumberTrading Post "i"Bid (\$/opr.)150100700and the \$ amount for the second slot is to be increased to\$125 and this is the only change, the resubmission should be:

		Slot	Number				
Airline A, Round 2		1	2	3	4	5	
Trading Post "i"	Bid (\$/opr.)	150	125	100	70	0	

7. After completion of two or more rounds of bidding, the auctioneer may determine when to close the auction. Once the auction has been closed, no further bidding for slots will be accepted. The auction will be closed if the players vote <u>unanimously</u> to discontinue bidding, or if the auctioneer determines that the slot allocation has "settled down" sufficiently.

3. Explanation of Price Determination

The bids prepared by airlines (See Figure 1; for slots at each trading post represent, in effect, the individual demand schedules of the airlines. When all the airlines have bid, the bids are aggregated into market demand curves for slots at each trading post (See Figure 2). The FAA hourly quota causes the supply of slots to be restricted, so that a supply curve for slots is generated with zero price for slots under the quota, and a very high price* for

*effectively infinite

slots above the quota. Supply and demand are in balance if the ²⁰ price is set at the intersection of the supply and demand curves (See Figure 3). The solution technique is displayed in Figure 3 for the same example presented in Figure 1 and we see that the slot price in this example is \$65. Because these curves are step functions, and the quantity of slots muct be an integer, there is a slight ambiguity about the intersection which is resolved by taking the midpoint of the range of slot prices around the balance point of supply and demand. In other cases, the ambiguity may result in two or more <u>marginal</u> slots for which the same amount was bid having to be allocated <u>randomly</u> to airlines. For example, if A and D, had both bid \$80 for their third and fourth slots respectively, only one of these slots could have been awarded; which one would be decided by the "toss of a coin".

Ordinarily, when supply is in excess, the absence of demand pressure will allow the slot price to be zero. However, a minimum price will be announced and charged for all allocated slots. Whenever there is excess demand, however, a positive price is necessary in order to eliminate some of the demand. The price is chosen so that all airlines which bid above that price are awarded slots, all who bid below are not. In a subsequent round of bidding, the disappointed airlines have a chance to bid higher, so as to try to capture desired slots. This causes the slot price to go up so that there will be a new allocation of slots at the next round. Some airlines may find they have lost slots which were previously

FIGURE 1. SUMMARY OF ALL AIRLINE BIDS FOR ONE TRADING POST (UNITS = \$ PER OPERATION)

1		SLOTS	(QUOTA =	11 PER H	OUR)		1
AIRLINE	<u> </u>	22	3	4	5	6	ALLOCATION
А	100*	90*	50	0			2
B	150*	150*	150*	100*	50	0	4
C	100*	D					1
D	110*	100*	9 0*	80*	0		4
E	49	49					0

***INDICATES SUCCESSFUL BID**

FIGURE 2. FORMATION OF PRICE, SLOT ALLOCATION AT A TRADING POST

and the second

AL LINE AND

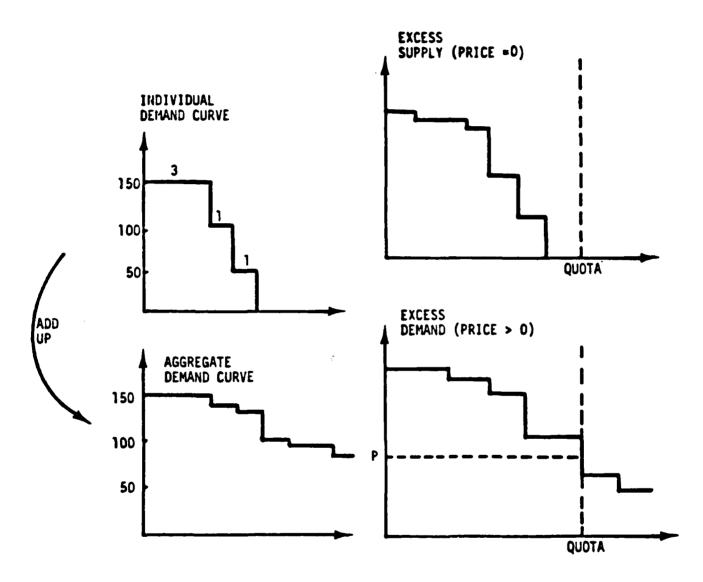
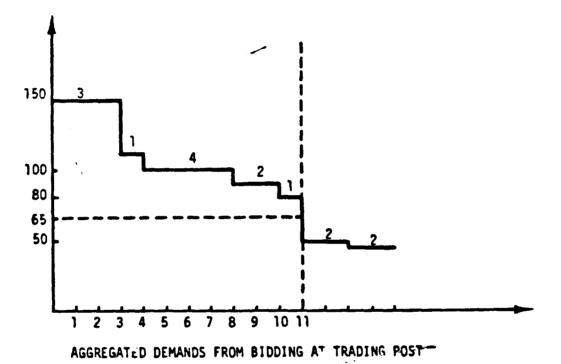


FIGURE 3. AGGREGATED DEMANDS FROM ALL AIRLINE BIDDING AT ONE TRADING POST

15 m 18

1



won. In addition to bidding higher amounts to recapture these lost ²⁴ slots, the airlines should consider "sliding" to an adjacent market. Eventually the process converges to a competitive equalibrium. In practice the auctioneer must determine when the bidding has "settled down" sufficiently and announce a cut-off, as described in the Rule No. 7 above. If the available auction time runs out with the allocation still fluctuating, then it will be necessary to halt the simulated auction. In reality, it will be desirable to resume bidding the next day in any future implementation of the slot auction.

4. <u>Scheduling Flights After Slot Allocations To Airlines.</u>

Following the slot auction, each airline will have received a printout containing detailed information on the slots awarded to itself, and payments required over 6 months operations for those slots. It will be the responsibility of each airline to make sure that flights scheduled subsequently are compatible with the slot allocation at capacity restricted airports. An airline awarded five slots at 9:00 a.m. at airport AAA is therefore expected to schedule <u>no more than</u> 5 runway operations at that airport from 9:00 a.m. to 9:59 a.m. The game administrator will also check the schedules for slot feasibility and inform airlines of any violation.

4. RESULTS AND ANALYSIS

The exercise was conducted in five offices, one for each airline team, and a control center for the game administrators on the ninth floor of the FAA building at 800 Independence Avenue. The airline schedulers, the game administrators and the members of the FAA's Office of Aviation Policy who were involved all put in long hours. A large amount of learning of game procedures and sifting through scenario airline data was required of the airline schedulers. Considering this and the time pressures, the evaluation exercise was conducted reasonably close to the daily schedule and with a number of useful results.

First, the exercise showed that it was possible to operate profitably in the simulated slot-restricted environment, allowing for the new cost element when the slots were priced. Secondly, the results indicated that the airline teams were able to prepare bids and acquire a usable set of slots through the Slot Exchange Auction. Thirdly, the results showed that some of the teams were able to make even better profits within the restricted environment than they did in the base case; other teams gave up some profits to slot payments. The improvement of airline profitability in the face of increased costs due to slot pricing shows a learning effect.

Procedurally, the Slot Exchange Auction was found to work satisfactorily within the time constraints of the exercise. Due to these constraints, there was only a partial test of the equilibrium concept, and indeed many more rounds of bidding would seem to be required. The slot awards demonstrated remarkable convergence, but price convergence remains to be shown. In the previous section some alternative methods of guaranteeing termination were discussed.

4.1 The Slot Exchange Auction Results

Because of the large amount of data generated by the slot allocation evaluation, this section will necessarily be selective in presenting the results. The complete body of the airline management game output and auction evaluation output will be made available on request. Table 4.1 presents the "bottom line" for each phase of the evaluation: the net earnings (after tax) of the five airline teams. In the case of the second and third lines of Table 4.1 these figures are also net of slot payments resulting from the auctions. The "industry" as a whole proved able to generate as much profit after suitable learning with an auction for slots (line 3) as it did without the auction (line 1); indeed, without any restrictions as to slot utilization. Individual teams either improved their profitability (Blue and Red) or managed to avoid serious losses (Gold, Green and White), again after suitable learning. The large loss generated by the Blue team in Period 1 is anomalous and was corrected in Period 2; it was caused by an excessively simplistic market strategy on the part of the Blue team, leading to severe drop in load factors.

The quotas were set by the game administrator and auctioneer as being:

Airport	Α	В	С
Quota	13	12	11

at the end of the base period. Tables 4.2 through 4.11 summarize the financial and performance results of the evaluation exercise. Starting with Tables 4.2 through 4.4 we find that slot prices within the first period Slot Exchange auction tend strongly upwards at the most favored peak hours, particularly at airport C which had the smallest quota. The exceptionally high slot prices at 0800 and 1600 hours at airport A (implying slot payments of respectively \$141,232 and \$128,674 per season by <u>each</u> airline scheduling arrivals or departures at those hours) are indicative of overbidding in the first period auction. This was corrected in the

AIRLINE						
CASE	BLUE	GOLD	GREEN	RED	WHITE	ALL
1. BASE	-0.220	3.817	3.845	1.109	4.018	12.56
2. PERIOD 1AUCTION**	-7 .9 67	3.098	1.634	0.485	3.183	0.43
3. PERIOD 2AUCTION**	1.349	3.254	3,445	1.426	3.691	13.16
4. PERIOD 1ADMINISTRATIVE	2.020	4.282	3.849	1.656	3.892	15.69

Ř.

TABLE 4.2 SLOT PRICES AT END OF ITERATION 1.1 (DOLLARS PER OPERATION)							
		AIRPORT					
HOUR	A	В	C				
0600 0700 0800 0900 1000 1100 1200 1300 1400 1500 1600 1700 1800 1900 2000 2100 2200	0 100 200 8 8 54 79 200 29 200 104 129 4 1 0 0	0 7 0 7 8 125 8 0 38 1 4 25 125 0 0 0	0 7 8 50 100 38 4 8 100 100 100 4 54 58 8 7 0 0				

TABLE 4.3 SLOT PRICES AT END OF ITERATION 1.2 (BOLLARS PER OPERATION)							
	AIRPORT						
HOUR	A	8	C				
0500	0	0	0				
0700	202		8				
0800 0900	560 101	0	101				
1000	30	12	151				
1100	78	13	ö				
1200	251	201	Ō				
1300	311	51	51				
1400	101	0	251				
1500		0 76 201					
1600							
1700 1800	180 0 403 201 51 210						
1900		201	18				
2000	Ĭŏ	ö	51				
2100	j õ j	Õ	0				
2200	0	0	0				

TABLE 4.4 SLOT PRICES AT END OF ITERATION 1.3 (DOLLARS PER OPERATION)					
AIRPORT					
HDUR	A	8	C		
0600	0	0	0		
0700	276	4	0		
0800	776	1 1	58		
0900	209	į 1	209		
1000	51	0	485		
1100	0	0	0		
1200	301	301	0		
1300	351	204	209		
3400	197	0	429		
1500	0	201	501		
1600	707	5	0		
1700	201	0	510		
1800	0	351	458		
1900	(ŏ	155	51		
2000	Ō	0	ŏ		
2100	Ō	Ō	1 õ		
2200	ŏ	i õ	e e		

TABLE 4.5 POTENTIAL SLOT REVENUES (NILLIONS OF DOLLARS PER MALF-YEAR SEASON)						
		AI	RPORT			
ITERATION AND ROUND	A	8	C	ALL		
1.1	2.709	0,760	1.093	4.562		
1.2	5.809	1.332	2.909	10.050		
1.3	7.261	2.671	5.826	15.758		
2.1	1.051	0.646	1.269	2.966		
2.2	0.582	0.535	1.922	3.039		
2.3	2.432	0.937	3.934	7.303		

		PERIOD	
AIRLINE	BASE*	1	2
BLUE	-0.22	-2.11	3.00
GOLD	3.82	10.14	7.23
GREEN	3.64	7.25	7.66
RED	1.11	2.48	3.17
WHITE	4.02	9.07	8.20
ALL	12.57	26.84	29.26

TABLE 4.7 POTENTIAL SLOT PAYMENTS AFTER EACH BIDDING ROUND (MILLIONS OF DOLLARS PER HALF-YEAR)								
			PERIOD A	ND ROUND				
AIRLINE	1.1	1.2	1.3	2.1	2.2	2.3		
BLUE	1.843	3.574	5.971	0.921	0.641	1.778		
GOLD	0.158	2.079	3.047	0.843	0.959	2.410		
GREEN	1.823	2.135	3.617	0.395	0.725	2.034		
RED	0.034	0.889	1.019	0.371	0.318	0.185		
WHITE	0.703	1.372	2.104	0.436	0.397	0.886		
ALL	4.561	10.049	15.758	2.966	3.040	7.303		

TABLE 4.8 NET EARNINGS AFTER SLOT PAYMENTS, AFTER TAXES (MILLIONS OF DOLLARS PER HALF-YEAR)						
		PERIOD				
AIRLINE	BASE	1	2			
BLUE	-0.220	-7.967	1.349			
GOLD	3.817	3.098	3.254			
GREEN	3.845	1.634	3.445			
RED	1.109	0.485	1.426			
WHITE	4.018	3.182	3.691			
ALL	12.569	0.432	13.165			

second period auction as can be seen by referring to Table 4.5. Total slot payments at the end of Round 3 of the bidding in the first period amounted to nearly \$16 million per season, which exceeded net earnings (\$12.5 million) of all five airline teams in the base period (Table 4.6). The airline teams were nevertheless able to increase net earnings in Period 1 so that, even with the high cost of slots, they managed to break even (Table 4.8).^{*}

There were significant reductions in slot prices and improvement in profitability during Period 2. The aggregate level of slot payments was less than half the Period 1 level after three rounds of bidding. Net earnings before taxes were up sharply and the final Period 2 profitability was actually better with slot pricing than it had been without slot pricing in the base period (Table 4.8). A learning effect on the part of the team players is clearly in evidence and explains this strange result. It is therefore very important to allow for airline learning in planning to <u>implement</u> a slot auction. The Slot Exchange auction is specifically designed to allow learning about slot market effects to take place without imposing real costs on the airline industry. More than three rounds of bidding would probably be required in implementation of the Slot Exchange auction to complete the information exchange between airlines that occurs through observing slot prices and slot allocation sequentially.

4.2 Levels of Service

In reviewing the results of the evaluation exercise, it is necessary to recall that the five teams had complete freedom to determine which markets they would

As previously mentioned, the Blue team suffered severe losses in Period 1.

serve subject to the constraints of thier given equipment. Due to time pressures, not all of the participants were able to take full advantage of this freedom. Nevertheless, we do see considerable improvement over the initial schedules which were prepared by Flight Transportation Associates in Period 1. Further progress is in evidence in the Period 2 results. Undoubtedly, the fact that the airline participants were professional schedulers contributed to the improved airline schedules. That this improvement occurred in the face of slot restrictions which were not applied in the initial scheduling makes the result more striking.

4.2.1 The System Responses

The operating statistics for the base period and Period 1 and Period 2 are presented in Tables 4.9 through 4.11. The OAG schedules, as printed on the computer by the Airline Management software, are presented in Table 4.12^{*} (Period 1) and Table 4.13 (Period 2). Traffic data are also generated by they AMG software; these are shown in Table 4.14 (Period 1) and Table 4.15 (Period 2).

The operating statistics (Tables 4.9 through 4.11) show considerable stability. While average load factors actually improved in Period 2 for three of the airline teams and were hardly changed for the other two, there is an overall appearance of very little change in airline operating statistics if one compares Period 2 (Table 4.11) with the base period (Table 4.9). The difficulties encountered in Period 1, such as Blue's 10.8 percent drop in load factor, can all be attributed to learning. The main conclusion which we draw from the evaluation exercise is that the airlines can perform "business as usual" in the face of slot pricing and can maintain their profitability. Caution is required in extending this conclusion to the real air transportation system; in allowing the players complete freedom of choice

"On account of their large bulk, Tables 4.12 through 4.15 are presented in the Data Appendix.

	TABLE 4.9 OPI	ERATING STA	OPERATING STATISTICSBASE CASE	E CASE		
	BLUE	GOLD	GREEN	RED	WHITE	ALL
SEAT-MILES (x 10 ⁶)	1,407.7	887.0	1,090.1	378.8	309.7	4,073.2
RPM (x 10 ⁶)	781.6	558.0	651.7	180.0	215.5	2,386.8
ENPLANEMENTS (x 10 ⁶)	1.665	1.200	1.278	0.500	0.493	5.137
AVG. EQUIPMENT UTILIZATION (HRS/DAY)	10:08	9:07	10:08	8:08	9:41	9:36
AVG. STAGE LENGTH (MILES)	453	401	454	355	370	420
AVG. LOAD FACTOR	0.555	0.629	0.598	0.475	0.696	0.586
	TABLE 4.10 OP	ERATING ST	OPERATING STATISTICSPERIOD 1	8100 1		
	BLUE	COLD	GREEN	RED	WHITE	ALL
SEAT-MILES (x 10 ⁶)	1,521.8	900.2	963.1	412.4	309.7	4,107.1
RPM (x 10 ⁶)	752.5	582.5	561.9	183.8	215.0	2,295.8
ENPLANEMENTS (x 10 ⁶)	1.383	1.202	1.172	0.490	0.510	4.757
AVG. EQUIPMENT UTILIZATION (HRS/DAY)	10:19	60:6	8:51	8:17	9:41	9:21
AVG. STAGE LENGTH (MILES)	572	426	477	369	370	461
AVG. LOAD FACTOR	0.495	0.647	0.583	0.446	0.69\$	0.559
	TABLE 4.11 OP	ERATING ST	OPERATING STATISTICSPERIOD 2	100 2		
	BLUE	GULD	GREEN	RED	WHITE	ALL
SEAT-MILES (x 10 ⁶)	1,309.1	913.7	1,000.1	393.8	314.6	3,931.3
RРМ (х 10 ⁶)	722.9	590.4	610.8	190.4	219.7	2,334.3
ENPLANEMENTS (x 10 ⁶)	1.348	1.236	1.313	0.482	0.520	4.899
AVG. EQUIPMENT UTILIZATION (HRS/DAY)	9:11	9:21	9:19	8:08	9:52	9:12
AVG. STAGE LENGTH (MILES)	529	416	459	383	361	443
AVG. LOAD FACTOR	0.552	0.646	0.611	0.484	0.699	0.594

with regard to routes and market strategies we have undoubtedly exaggerated the extent to which airlines would change their network in response to slot pricing and allocation.

One advantage of the real situation is that over several six-month periods the equilibrium of slot supply and demand may be easier to obtain due to the inherent stability of the air transport system over time. The existence of previous prices and slot allocations will speed up the convergence of the Slot Exchange auction. In the exercises there was no such history of prices to guide the players and the equilibrium was accordingly harder to obtain.

4.2.2 Service to Small Communities

Same and the second second second

The six minor airports in the evaluation exercise were KKK, LLL, MMM, NNN, OOO and PPP. Together, they had only 5.75 percent of all traffic (passengers enplaned per day) in the base case and each individual market involving a small community had less than 1 percent of all traffic. In contrast, the AAA-CCC market claimed 8.59 percent of passenger traffic. It should be noted that the simulated demand for air service did not allow for any traffic <u>among</u> these six airports. After the Period 1 auction, the rescheduled network showed an overall drop of 49 percent in these small markets (Table 4.16). Service to and from airports OOO and PPP was dropped entirely. Only KKK, of the six minor airports, did not lose significantly. Following the Period 2 auction, some of the small community service was restored--mostly for MMM and NNN. Two airports, OOO and PPP, still had no service. This remained true after the Administrative Allocation even though overall traffic from the six small airports was slightly up (Table 4.16) relative to the Period 2 auction.

		PEI	RIOD	
AIRPORT	BASE	1	2	AA
KKK LLL MMM NNN 000 PPP	500.2 255.2 231.8 273.8 94.5 172.6	469.6 78.8 69.8 156.7 	470.2 96.8 219.9 279.8 	536.2 98.2 219.8 278.4
TOTAL	1,528.1	774.9	1,066.7	1,132.6
REL. CHANGE OMPARED WITH BASE	I	-49.3%	-30.2%	-25.9%

4.3 The Slot Exchange (Aftermarket)

ALL STREET, MAL

The aftermarket was organized as an openbook exchange. The players could bring written offers to buy or sell specific (time-of-day) slots at specific capacity-restricted airports (AAA, BBB or CCC) to the exchange. These offers were posted immediately on a blackboard. The forms for making such offers (to sell) or bids (to buy) are shown in Figures 4.1 and 4.2. The aftermarket administrator attempted to match sells with buys at each airport and time of day. Those slots which had not been purchased in the Slot Exchange Auction (unclaimed slots) were offered on a first come-first served basis at a nominal price of one dollar. Buyers of unclaimed slots were limited to four slots per team each 15 minutes so long as the exchange remained open and the desired slots were still available.

The activity on the exchange was not extensive. Far more offers to sell slots occurred than bids to buy slots, and the number of transactions, other than

AIRLINE:

THIS IS A FORM FOR AN AIRLINE TO SUBMIT BIDS TO $\underline{\text{BUY}}$ slots on the AFTERMARKET.

				SLOT	S REQUIRED)	
AIRPORT	HOUR	1	2	3	4	5	6
• • • • • • • • • • • • • • • • • • •							
وي والمحمد المحمد ا							
						<u></u>	
					,		
					 	<u> </u>	···· .
							····
				······			
						<u> </u>	
						····	
			-	۰ 		-	

FIGURE 4.1 AFTERMARKET FORM A--BUY

35

Ň

AIRLINE:

A 1944 B

1000

4

THIS IS A FORM FOR AN AIRLINE TO OFFER TO <u>SELL</u> SLOTS WHICH IT HOLDS ON THE AFTERMARKET.

				SLOTS OFFERED			
AIRPORT	HOUR	1	2	3	4	5	6
*							
* <u>, ***_, *</u> ,							
• <u> </u>							
					<u> </u>		*
				····			
						·····	
*			·				<u></u>
<u> </u>							<u>. </u>
				····	<u></u>	<u>. </u>	

FIGURE 4.2 AFTERMARKET FORM B--SELL

TABLE 4.17 AFTERMARKET ACTIONPERIOD 1					
TRANSACTION	AIRPORT	TIME	BUYER*	SELLER*	PRICE** (\$/OPR.)
$ \begin{array}{r} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ 23 \\ 24 \\ 25 \\ 26 \\ 27 \\ 28 \\ 29 \\ 30 \\ 31 \\ 32 \\ 33 \\ 34 \\ 35 \\ 36 \\ 37 \\ 38 \\ 39 \\ \end{array} $	CCC CCC CCC AAA BBB CCC AAA BBB CCC AAA BBB CCC AAA BBB CCC AAA BBB CCC CCC	$\begin{array}{c} 21\\ 21\\ 21\\ 21\\ 15\\ 17\\ 12\\ 11\\ 10\\ 7\\ 18\\ 6\\ 11\\ 17\\ 12\\ 6\\ 11\\ 17\\ 12\\ 6\\ 11\\ 11\\ 16\\ 16\\ 8\\ 13\\ 14\\ 14\\ 20\\ 15\\ 22\\ 21\\ 19\\ 20\\ 10\\ 19\\ 20\\ 10\\ 19\\ 20\\ 11\\ 21\\ 22\\ 6\\ 10\end{array}$	BL BL GL GL GL GL GL GL GL GL GL GL GL GL GL	BL BL WT BL WT	1 1 1 1 1 1 1 1 1 1 1 1 1 1
*TEAMS IDENTIFIED BY TWO-LETTER CODE ARE: BL=BLUE, GL=GOLD, GR=GREEN, RD=RED, WT=WHITE. ** A ONE-DOLLAR PRICE WITH NO SELLER IDENTIFICATION DENOTES A PURCHASE OF					
AN UNCLAIMED SLOT FROM THE SLOT AUTHORITY.					

P

TABLE 4.18 AFTERMARKET ACTIONPERIOD 2						
TRANSACTION	AIRPORT	TIME	BUYER*	SELLER*	PRICE ^{**} (\$/OPR.)	
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	CCC CCC AAA ABB AAA BBB AAA CCC CCC AAA AAA	17 15 7 14 15 10 12 14 12 12 12 12 12 12 12 11 12 10 22	RD GL GL GR WT WT GR GL GL GL RD RD RD RD RD GL	BL GL GL GL BL WT	1 1 1 1 1 1 300 150 1 1 1 1 75 50 150 50 250 1	
<pre>*TEAMS IDENTIFIED BY TWO-LETTER CODE ARE: BL=BLUE, GL=GOLD, GR=GREEN, RD=RED, WT=WHITE. **A ONE-DOLLAR PRICE WITH NO SELLER IDENTIFICATION DENOTES A PURCHASE OF AN UNCLAIMED SLOT FROM THE SLOT AUTHORITY.</pre>						

And the second second second

201 1

TABLE 4.19 SLOT PAYMENTS IN AUCTION AND AFTERMARKET (\$ PER DAY)						
		PERIOD 1		PERIOD 2		
AIRLINE	AUCTION TOTAL	PURCHASES	SALES	AUCTION TOTAL	PURCHASES	SALES
BL GL GR RD WT	32,806 16,742 19,875 5,601 11,559	7 1,096 4 209 4	692 0 0 596	9,823 13,241 11,177 1,020 4,866	0 7 201 527 302	350 350 0 325

the \$1.00 purchases, fell short of the number of offers by an order of magnitude (Tables 4.17 and 4.18). The total slot payments by all teams for exchange activities are shown in Table 4.19, also indicating the small volume of activity when compared with the total auction slot payments.

The airlines apparently did not behave speculatively in the slot auction and exchange, but many auction acquisitions were in excess of slot requirements as evidenced by the pressure to sell in the exchange. Some airline players informed us that they were attempting to buy "insurance" slots for important flights--slots at adjacent hours in the same airport. This may account for the excess supply in the exchange.

In a real exchange there undoubtedly would be more activity because of the six months duration of each period in real time compared with approximately two hours in simulated time. Furthermore the changing environment in the real air transportation system might necessitate slot exchanges and the pricing of such slots might not be an important consideration to the airlines. Naturally, this would change if any tendency towards speculation in slots developed.

5. COMMENTS BY THE AIRLINES

Those airlines which sent participants to the Evaluation Exercise in Washington, February 11-15, 1980, were invited to comment in writing. During March 1980 the participants were mailed a document of game results and ECON's and the FAA's brief analyses of these results.² They were asked to respond promptly to the following questions.^{*}

- 1. Which method did you prefer--the Trading Post Auction or the Administrative Allocation? Why?
- 2. In each of the two methods did you significantly alter your airline marketing approach as a result of the slot allocation? If so, in what way?
- 3. Do you consider the two methods to be fair? If not, in what way are they unfair?
- 4. Were you able to handle the total information flow comfortably in the time available in each method? Was more time required (a) for rescheduling, (b) for bidding, and/or (c) for submitting preference plans in the Administrative method?
- 5. Was the evaluation exercise sufficiently realistic to allow conclusions to be drawn from the real world? If not, how would you make it more realistic?
- 6. Assuming one had to implement one of the two alternative allocation methods, what changes would you recommend in each method to make it more practical?

Their responses are reproduced here in facsimile; they speak for themselves

and hence we shall not discuss them other than to state that the factual errors

which W. Jeffrey Rowe points out were corrected in this report.

- American Airlines Donald F. Roach and R. Bradley Jensen
- Delta Airlines W. Jeffrey Rowe
- Eastern Airlines W. H. Pacelli

"Note that "Trading Post Auction" was the term then in use for the Slot Exchange Auction.

- Piedmont Airlines R. L. McAlphin and R. L. James
- Trans World Airlines R. J. Zablocki
- USAir Jerry A. Frissora

ALL DUN

A DESCRIPTION OF A DESCRIPTION

a.

AmericanAirlines

April 2, 1980

Mr. John M. Rodgers Acting Chief, Economic Analysis Branch Federal Aviation Administration 800 Independence Avenue, S. W. Washington, D. C. 20591

Dear Mr. Rodgers:

Statistics of the state of the

.

4

State of the second sec

同時は

Ħ

t

By letter dated March 7, 1980, you forwarded to us an evaluation of the slot allocation exercise conducted during the week of February 11 at the FAA (the "Evaluation"). This allocation exercise explored two methods of allocating airport slots: an auction system and an administrative allocation system. On January 15, 1980, American submitted detailed comments on the auction system proposed by the Polinomics Research Laboratories. The general principles addressed in those comments apply as well to the present Evaluation. We have the following additional comments in connection with the two systems analyzed in the Evaluation:

I. BOTH THE AUCTION SYSTEM AND THE AD-MINISTRATIVE ALLOCATION SYSTEM WERE BASED ON TWO INVALID PREMISES.

The Evaluation concluded that the airline teams were able to show considerable profit improvement under both the auction system and the administrative allocation system, and implies that this improvement was due to the institution of slot allocation. However, the mock airlines that the exercise participants were asked to manage were initially

operating at very low capacity utilization. The participants were able to dramatically increase the efficiency of the mock airlines simply by streamlining aircraft utilization and scheduling. The institution of the allocation methods clearly had nothing to do with the increased profits.

The Evaluation was cognizant of the problem*, but failed to recognize the degree to which the problem affected the results. The impact of this fundamental deficiency on the overall conclusion regarding the two allocation methods cannot be lightly swept aside. Under both methods, the improvements in profitability were clearly a function of commor sense resource allocation, not the institution of allocation systems.** In the real world, airlines already operate at very high efficiency levels. It is simply not realistic to expect that an auction system would generate enough of an increase in efficiency to offset the cost of slot payments.

The second invalid premise of the auction and the

* Evaluation, pp. 16, 40.

** For example, the first action the red team took in response to the slot limitations imposed was to cancel the flights which were making the least profit. Because the pro fits were calculated using variable cost (i.e. direct operat ing and passenger related costs, but no depreciation and amortization) naturally the rate of return would go up. In the real world, however, the cost of aircraft ownership cannot be disregarded.

administrative allocation systems is that they both assume that airlines have complete flexibility to alter schedules at will. This is obviously not the case. A schedule change at one airport has a ripple effect which would impact all of the subsequent segments served by the affected flight. Furthermore, passengers have come to rely on, for example, American's 6:00 p.m. flight from LaGuardia to O'Hare. Airlines are therefore not free to capriciously revamp their schedules in order to accommodate a particular allocation method. Safeguards must be built into the system to avoid inconvenience to the traveling public.

II. THE AUCTION SYSTEM FAILED TO PRODUCE AN EQUILIBRIUM.

From an economic efficiency point of view, the auction was suppose to produce a supply/demand equilibrium that would accurately reflect the value of a given slot. However, in the auction that was conducted there was no convergence of the supply and demand curves to an equilibrium point. This appears to have been caused by the amount of uncertainty and speculation involved in the bidding process. Because the slots won in a given round of the auction were not guaranteed to the next round, it was usually necessary to increase the bid for a slot already won in a previous round. In subsequent rounds, it sometimes became prudent to drop a slot that

had been won in a previous round. Speculation and lack of convergence put an artificial upward pressure on prices. But since the auction was terminated after only three rounds, it was not possible for slot prices to reach a true supply/demand equilibrium.

III. THE ADMINISTRATIVE ALLOCATION METHOD SIMPLY DID NOT WORK.

The administrative allocation procedure was a twostep process where each carrier was awarded a specific number of slots according to an entitlement formula, and then slot assignments were made by a computer after each carrier had submitted a number of alternative plans specifying the hour by hour utilization of its awarded slots.

Both steps in this process are flawed. First, the weights in the entitlement formula were very arbitrary and cannot be shown to favor all carriers equally at all airports. As a result of this, carriers would end up tailoring their schedules to serve the entitlement formula, rather than to serve passenger convenience. For example, some carriers may run through plane service at a particular airport while others make turnarounds. In order to maximize the number of slots to which they would be entitled under the formula, carriers operating through plane service would find it beneficial to publish all of their multi-stop service as

connections in order to achieve the greatest number of enplanements. This would create unnecessary passenger inconvenience. Moreover, it is doubtful that the interested parties would ever be able to agree on fair definitions and weightings in the entitlement formula.

The most significant drawback of the administrative allocation procedure is that the computer program employed to find the solution did not, in fact, find the solution. The carriers were asked to submit a number of different scheduling alternatives which, as discussed above, they simply do not have the flexibility to do. Nevertheless, the computer program could not find a suitable hour by hour allocation to meet the carriers' needs. Since the computer was able only to make a partial allocation, it was necessary to get all the team players into a large room with the slot requests posted on a board and then solicit volunteers for sliding. This is precisely what the scheduling committee already does.

The failure of the computer program to find a suitable allocation for all carriers is a function of the inability of the system to focus on specific problem areas. In practice, the slot allocation problem is really a peculiar combination of events occurring at specific times. It is unrealistic to expect the computer to arrive at an acceptable solution merely by presenting it with a myriad of random slot

plans. This approach did not work during the FAA exercise and it will not work in the real world. Specific individual adjustments to resolve specific problem areas are always going to be necessary.

IV. A SUPERIOR ALTERNATIVE TO THE CURRENT SCHEDUL-ING COMMITTEE SYSTEM HAS STILL NOT BEEN POUND.

In its January 15, 1980 comments to the FAA and the CAB in connection with the Polinomics study, American set forth several reasons why the current committee system should be maintained in the absence of a superior alternative. Neither of the approaches explored in the February 11 FAA exercises proved to be superior. The committee system permits intelligent interaction on specific problem areas without going back to square one each time. This is the essence of the committee system and it is why the committee system works. Neither the auction system nor the administrative allocation system has been demonstrated to more equitably or efficiently accomplish what the committee system already accomplishes.

V. RECOMMENDATIONS

In its Polinomics study comments to the FAA and the CAB, American set forth several considerations regarding an auction-type system. These included recommendations that all slots should be auctioned (including general aviation and

small cities slots), that slot auctions should cover a sixmonth period and be held six months ahead of time, and that an open, multi-step auction process would be preferable. Any auction system that may ultimately be adopted must take into account these basic considerations.

Clearly, the two systems explored during the Pebruary 11 PAA exercises did not meet the desired objectives. Neither exercise can be considered to have tested the respective systems sufficiently for application to the real world. In fact, the only concrete conclusion that can be drawn is that neither system worked. It is again urged that current scheduling committees be maintained in order to avoid disruption of a process that effectively offers the traveling public the convenience it requires.

Very truly yours,

Donald F. Roach Manager - Scheduling Systems Development

Manager - Schoule Planning

COMMENTS OF W. JEFFREY ROWE ON FAA SLOT ALLOCATION EVALUATION

IC IS

1

W. Jeffrey Rowe Analyst - Economic Research Department 973 Delta Air Lines, Inc. Hartsfield Atlanta International Atlanta, Georgia 30320

- 1980 - X. - B. M. H. 🗸

بالمبتار الرار سرامانه

GENERAL COMMENTS

The FAA is to be commended for its bold venture into assessment of policy options by computer simulation techniques. In my opinion, this type of analysis can offer valuable insight and a broader understanding of what proposed changes in the national air transportation system will accomplish. Nevertheless, this simulation exercise was flawed, as any such initial effort is bound to be. These flaws are detailed in the sections that follow, particularly section 5. My conclusion is that the defects in the exercise preclude using it to compare the two allocation methods with each other or with the scheduling committee method.

The simulation model is an extremely versatile tool and should not be abandoned in these ground-breaking difficulties. Another simulation exercise with airline participants (not necessarily the same ones) should be conducted, with some changes in the scenario (see section 5). Slot allocation should be simulated using (a) the scheduling committee, to establish a realistic baseline case, (b) common-price and discriminative-price auctions, and (c) a refined administrative allocation method. Each method should be simulated for several periods to allow schedules to reach an equilibrium and to minimize the chances of anomalous events appearing in the results. The time required for this additional study would be on the order of several weeks, and would therefore preclude attendance by airline participants in Washington. However, interaction between the participants and administrators could be accomplished via the same telephone line computer peripherals that afford the participants access to the simulation model.

1. PREFERRED ALLOCATION METHOD

The administrative allocation procedure exerted less pressure on the Blue team than the slot auction. This resulted from Blue having already developed a schedule during the period 2 auction which (a) met the slot quotas, and (b) produced Blue's largest pretax earnings during the exercise (before slot payments) - \$4.73 million. With this information in hand when the administrative allocation began, Blue felt that developing another slot-constrained schedule from the baseline schedule would be wasted effort in terms of the maximum-profit goal.

Blue's decision to implement its period 2 auction schedule in the administrative allocation simulation had a profound effect on the allocation process for all five airlines. For airport AAA, where Blue had used 83 slots in the baseline schedule, Blue requested only 61; this contraction by itself would have been enough to reduce the baseline (uncontrolled) movements in restricted hours from 213 to 191, below the daily quota of 195. Requests totaled only 176, or 19 less than the quota. Obviously the only challenge to meeting the slot quota at AAA was to arrange a few slides, and this was done quickly. The same comments apply to BBB, where the daily quota (180) exceeded requests (164) by 16 slots.

Airport CCC was more difficult to resolve because it was the only case where requests (167) were at the quota level (165). A fairly complex series of slides, coupled with a few outright reductions, was necessary to resolve CCC. These maneuvers were accomplished in short order by the teams in a scheduling committee-type meeting; yet the computerized assignment procedure might have continued indefinitely without any resolution.

As this discussion indicates, my preference for the administrative allocation method is qualified and is based upon circumstances in the exercise which would not parallel any real situation. In my opinion, although the exercise utilized a sophisticated simulation model capable of closely approximating reality, for various reasons (detailed in sections 4 and 5) the results of the exercise are not an adequate basis for selecting one allocation method over the other, or over the scheduling committee method.

2. MARKETING APPROACH UNDER SLOT CONSTRAINTS

The Blue team approach to market entry/exit and schedule adjustments on Blue's existing system was oriented toward maximizing profits under both methods of slot allocation, as well as in the initial simulation period when no slot constraints were imposed. Blue felt no need to pursue other goals as a result of either slot allocation method, and in fact would not have had the time to do so in any case (see section 4).

3. FAIRNESS OF ALLOCATION METHODS

The fairness of any slot allocation scheme to a given airline will depend on the particular viewpoint of that airline. Imposing a slot auction at a given airport might be less fair to an established carrier with extensive operations and connecting complexes at that airport, than it would be to a new carrier whose schedules are more flexible and can, if slot payments are too burdensome, shift its operations elsewhere. Conversely, imposing the administrative allocation on carriers with similar situations at the same airport might favor the larger carrier, which would get many slots based on its extensive pattern of service and large volume of connecting enplanements/deplanements, while the entrant would get just four slots. This is an important question, but it cannot be answered without some agreement as to what constitutes a fair slot allocation method. Such an agreement should balance the interests of passengers, shippers, airport authorities, local governments, air carriers, and other affected parties; given the broad constituencies involved, Congress might be an appropriate forum for this debate.

4. TIME CONSTRAINTS IN THE EXERCISE

In my opinion, there was not enough time to analyze the available information and develop plans of action based on it during any phase of the exercise. The Blue team neglected to reschedule many flights which our printouts identified as relatively unprofitable simply because time ran out. Likewise, we could have developed a more sophisticated bidding strategy had time allowed, particularly in the period 2 auction after we had the benefit of some bidding experience. I doubt that we would have acted differently given more time to prepare plans in the administrative allocation, since our plans simply represented various slides from a schedule we knew would be profitable (see section 1), and slides were the only changes we made to achieve resolution. However, had the quotas actually been such a serious constraint on operations in the administrative allocation that major rescheduling was required, we would have needed much more time. Lack of time to respond to all available information was one factor limiting the realism of the exercise (see section 5).

5. REALISM OF THE EXERCISE

This exercise was a pioneering effort in its use of computer simulation techniques to explore the effects of alternative policies on the national air transportation system; it proved that such simulations can serve as a tool in policy assessment. As might be expected in such a first-time endeavor, several features of the simulation scenario prevented the exercise from effectively approximating reality. Most serious was the quick transition from a route-regulated system having no slot constraints (the "initial state" at the beginning of the exercise) to a completely deregulated route environment with slot controls at the three busiest airports and an auction allocation system. $\frac{1}{2}$

1/ The "initial state" of the system given to the participants in the FAA exercise was created in December, 1979, at MIT by faculty and students at the Flight Transportation Laboratory (FTL). According to Dennis Mathaisel of FTL, the airline route structures created at MIT reflected the dictates of a central authority requiring the smaller lines to serve the smaller cities and limiting competition in large markets.

5. REALISM OF THE EXERCISE (continued)

Only one rescheduling attempt was allowed the teams between these two states, corresponding to a six-month period. The results of this rescheduling (the "base state" in the FAA description) certainly did not represent an equilibrium state under route deregulation, nor did this state reflect <u>any</u> airport congestion problems, slot constraints, or other access problems. In reality, of course, slot controls have existed for more than a decade and domestic route deregulation has been proceeding apace for the past 18 months. In order to simulate the process of route deregulation under slot constraints, the exercise should have allowed for several rounds of scheduling, with slot allocation by scheduling committee, before alternative slot allocation methods were evaluated.

Another major oversight in the simulation was the lack of alternative airports at the slot-controlled cities. In reality, the three cities with slot- controlled airports can be accessed through other airports which are not slot-controlled (Chicago-Midway; New York-Newark; Washington-Dulles/BWI). The simulated network should have included such airports.

Lesser defects of the simulation were the omission of pricing freedom and the absence of transitional market entry/exit costs. In reality, airlines incur large costs to shift resources (personnel, facilities, ground equipment, advertising, etc.) from their existing system to new markets; in the model no such costs were assessed. For example, in the first scheduling attempt airline White (the smallest of the five airlines, flying only DC-9's) was able to raise its after-tax profits from \$320,179 to \$4,018,298 by entering thirteen markets, dropping three, and increasing daily nonstop flights from 35 to 50. One of the markets entered by White was the 1938-mile AAA-XXX market, where White competed with three other airlines flying 727's and 707's. In reality, such an ambitious expansion program by such a small carrier would not generate a 1,255 percent increase in net income in the first six months, as White did in the exercise.

To generate valid predictions of the impact of various slot allocation methods on a deregulated air transportation system, the scenario should have allowed complete, or at least some, pricing freedom. In fact, it allowed none. The teams were not able to set fares so as to exploit the differences in their segment costs dictated by differing aircraft types and network characteristics. This omission is particularly serious when considering the results of the slot auction simulations, when carriers with pricing freedom would have had the option of either increasing fares in markets involving the slot-controlled airports or, by not raising fares, cross-subsidizing the slot payments with profits from other routes.

Other problems with extrapolating the results of the slot auction simulation to a real slot auction arise when one considers that no real slot auction has yet been conducted or even proposed in detail.

In the Polinomics study, an auction is described in which carriers proposing to serve small communities from a slot-controlled airport would participate in a separate auction process, bidding among themselves for slots reserved exclusively to them. 2/ Congress' historical concern for and sensitivity to small community service suggest that some such mechanism could be part of a real slot auction procedure. Since no special treatment for small communities was incorporated in the simulation scenario (in fact, service disappeared completely from two small cities in the network), the results have no bearing on an auction process which does allow for such preferred treatment. Obviously, if some slots were removed from the general auction at a given level of demand, slot prices would go up.

Perhaps the most critical feature of a real slot auction system would be the distribution of slot revenues. Logically, the money should be used to expand capacity at the congested airport, allowing higher quotas, lower slot payments, and lower costs to the airlines. This effect could be noticeable within the sixmonth simulation period for some airports, and the results of a simulation including this feature would be valuable. If, on the other hand, one assumes there will be no relief from quotas associated with slot payments, the simulation scenario should allow for fare differentials (as suggested above) which would discourage traffic using the slot-controlled airports. In either case, more than two simulation periods under the auction allocation system would be needed to fully explore its effects.

As noted above (see section 1) the administrative allocation procedure, as simulated, acted to assign requests for 507 slots at the three controlled airports when 540 were available. Realism requires that the number of desired slots be higher than the quota by five to ten percent or more, as is now the case at Washington National Airport.

In addition, a realistic simulation of administrative allocation would include some new entrants and carriers providing essential air service to reduce the slots available to established carriers. As is the case for auction allocation, several simulation periods would be necessary to explore the major effects of administrative allocation on the air transportation system.

2/ D. Grether, M. Isaac, C. Plott, Alternative Methods of Allocating Airport Slots, section VI, at 12-14 (prepared by Polinomics Research Laboratories, Inc. for U.S. Civil Aeronautics Board, August, 1979).

In summary, the task of applying the MIT simulation tool to analyze the effects of alternative slot allocation methods is neither a success nor a failure; it is simply not finished. Simulation iterations, incorporating the variations mentioned herein must be undertaken before conclusions can be drawn from the exercise and applied to reality. To avoid the logistical problems and expense involved with convening a subsequent longer session in Washington, the participants could access a central computer by telephone lines from their home offices; they could then assimilate the exercise into their c her activities. This would require more time for coordination in each phase of the exercise due to the geographical separation of the participants and administrators, but in my opinion this additional time would allow more thoughtful decisions by the participants and, therefore, a more realistic simulation (see section 4).

6. SUGGESTIONS FOR CHANGING THE ALLOCATION METHODS

The auction allocation method as it was simulated seems entirely practical. The question is whether the results it produces are the results that would be desired of a real auction allocation method. As noted in section 3, no definition of desirable results exists. A number of features that might be incorporated into an auction, but were not part of the exercise, are discussed above in section 5. Other possibilities include allowing retraction of bids, with the slots released to be sold on the aftermarket, and accepting successful bids at the bid price (discriminative price auction) rather than at the "common price". All of these variations should be studied further with definite performance criteria (in terms of passenger/shipper service, prices to consumers, costs to airlines, ease of entry, small community service, etc.) in mind.

The administrative allocation method, on the other hand, must be refined before it can be implemented. The exercise revealed that the computerized matching of plans (the assignment phase) may never result in a combination that satisfies the hourly quota. Once the daily allocations for each carrier are determined, the most effective procedure would be to convene a scheduling committee to arrange slides so that the hourly quota is met. If no face-to-face contact between carriers is permitted, then FAA will have to engage in a tedious process of soliciting plans, finding problem hours, and soliciting more plans to reduce operations in the problem hours, unless a better idea surfaces. Again, variations in the administrative allocation method should be studied in additional iterations of the simulation exercise, with performance measured against definite criteria.

ERRATA

The FAA description of the exercise contains some factual errors which should be corrected before the description is translated into a final report.

Page 1 - W. Jeffrey Rowe attended the exercise for Delta and participated on the Blue Team, not Ted Maples.

Page 18 - The figures presented in Table 3.4 as net earnings before taxes or slot payments for the period 2 slot auction simulation are actually net earnings before taxes for the administrative allocation.

Page 21 - The operating statistics presented in Table 3.7C for the period 2 slot auction actually correspond to the administrative allocation.

EASTERN AIR LINES INCORPORATED / INTERNATIONAL AIRPORT / MIAMI, FLORIDA 33148 / 305-873-2211



March 24, 1980

Mr. John M. Rodgers Acting Chief, Economic Analysis Branch Department of Transportation Federal Aviation Administration Washington, D. C. 20591

Dear John:

Attached are my comments on the Draft Evaluation of the slot allocation test conducted during the week of February 11.

It is my understanding that the test focused on three main issues:

- 1. The practicality of two alternatives to the Schedule Committee process for slot allocation.
- 2. The impact of those alternatives on carriers' financial performance.
- 3. The impact on service to individual communities.

I believe the test uncovered specific implementation problems associated with each of the two methods. These are detailed in the attached. However, the results do not permit a valid evaluation of the impact of either method on carrier profitability or service levels by city-pair.

Since the participants were unfamiliar at the outset with their own networks and with the decision rules built into the MIT model, you would expect financial performance to improve with each iteration. That reflects both the learning process and a trend towards competitive equilibrium.

Mr. John M. Rogers

ومعادية محمولة والمستحكمة

March 24, 1980

Therefore, the fact that profits did not deteriorate under the slot allocation methods tested does not suggest the absence of a significant economic penalty. Instead, I would conclude that the learning curve effect offset the cost of slot allocations.

Moreover, because of the limited time available to properly analyze the data and schedule alternatives, resource allocation decisions did not necessarily reflect the economics of service in specific city-pairs. In fact, a post-test review of the data suggests significant changes to service patterns. This is discussed further in the attached.

Therefore, I would urge that any definitive conclusions be limited in scope to the implementation issues. Clearly, additional work has to be done to determine the effect of the slot allocation alternatives on carrier financial performance and on service patterns.

Sincerely,

:u

W. H. Pacelli Specialist Planning

Attachment

SLOT ALLOCATION EVALUATION TEST

Response to Questions on Page 41 of Draft Report

1. The two methods are based on different criteria. The Trading Post Auction gives priority to profit/revenue per flight and therefore longer haul flights. The Administrative method is based on passengers carried and airports served regardless of length of haul. In effect, that is a policy question, which I cannot address in these comments. Instead, I will focus on the practical implementation issues.

The test suggested serious problems with the Trading Post Auction in achieving the hour-by-hour adjustments needed to fully utilize the slots available. Indicative of this problem are slot prices of over \$700 in one hour while some slots in an adjacent hour were unused.

In addition, slot prices tended to be above those which one might expect based on economic theory. The upward pressure on slots was caused by (1) a basic tendency to protect existing operations, regardless of cost, (2) the uncertainty of slots in any given hour, resulting in bids for unneeded slots in adjacent hours, and (3) uncertainty about the real value of a slot, both to the individual airline and to competitors.

The Administrative allocation approach did provide more stability and generally was easier to work with. However, its utility was limited in the hour-by-hour assignment in that so many submissions of differing plans were necessary for a "computer solution." This would suggest some type of schedule committee to finalize hour-by-hour assignments.

2. We did not alter our marketing approach, but, had we had time to more fully evaluate the effect of slot reductions and price, we undoubtedly would have.

Had financial information been presented by segment and operating profit show rather than contribution, the resulting aircraft deployment would have been much different. For example, the revenue generated in the A-C market could have supported more flights than the B-C market. Yet, after Auction 1, there were 42 A-C flights vs 51 B-C flights. (See Exhibit A). There was insufficient time to examine the effect of slot payment on flight profitability, particulary on the double slotted segments. It was discovered after the test that slot costs on short-haul flights between slotted airports so drastically lowered the profit that redeployment of these flights would have + been necessary.

- 3. The term fair is very subjective and depends on the criteria used.
- 4. More time was needed to make schedule changes necessitated by not receiving desired slots and the price of a slot, especially in the Trading Post method.

Time allowed for the bidding process was totally inadequate. The amount of data that is generated and must be analyzed in order to make intelligent bids is very large. Only after inordinately high price levels (4.8% of total revenue) were reached in Auction 1 did some carriers drop out of the bidding While, it is true that things settled down in Auction 2, it must be remembered that in the test certain pressures were absent. These pressures are new aircraft deliveries and market aggressiveness.

5. No. Several iterations should have been made prior to testing the slot allocation methods to give the teams a familiarity with the game and the route network. The "noise level" of the Blue team's losses and massive swings in load factor and utilization from period to period render analysis of the economic data highly suspect. It is obvious from tables presented in the Draft Report that Blue had trouble finding a niche in this exercise and impacted the entire industry. Other participants, to a less obvious extent, also were going through a learning process. It is doubtful, therefore, that any concrete conclusions can be drawn about the financial impact on the industry.

6. Trading Post Auction

This alternative needs a mechanism that relieves the upward pressure on the price of slots and facilitates the process of moving to adjacent hours. We are not sure what that should be, but believe the system is ineffective without it.

Administrative Allocation

éa.

The criteria used to allocate slots, we believe, should include through passengers because they are using the airport runway capacity every bit as much as connecting passengers. This alternative would function better as a slot assignment tool if flexibility could be allowed in the maximum per hour quota by carrier. Having a maximum per hour seemed to work against an airport solution rather than assist in reaching one. Also, once the slot allocations by carrier are determined, an interactive process between carriers (similar to the schedule committee) should be permitted to reach an airport resolution.

Exhibit A

	<u>A-C</u>	<u>B-C</u>
Passengers (Both Directions) <u>1</u> / X Net Fare <u>2</u> /	4,514.1 \$ 51.66	3,358.5 \$ 18.88
Net Revenue	\$233,198.40	\$63,408.48
+Average O-W Direct Cost of 727	2,946.11	1,047.89
Maximum number of trips that could be economically operated	79	61

1/ Base state

and the second second

2/ Published fare less 15% for general and administrative expenses and less \$14.00 for passenger handling cost.



PIEDMONT AIRLINES SMITH REYNOLDS AIRPORT WINSTON-SALEM N.C. 27102

March 20, 1980

Mr. John M. Rodgers Acting Chief, Economic Analysis Branch Department of Transportation Federal Aviation Administration Washington, D. C. 20591

Dear Mr. Rodgers:

1

The week we spent in Washington reviewing the two slot allocation methods was enjoyable as well as educational. Our only regret was that more time was not allocated to the Administrative Method, which in our view, could offer a feasible solution to a very complex problem.

Aside from the cost, we believe the trading post auction to be too cumbersome to administrate. It would require a team of airline personnel with the technological know-how in scheduling, computers, and finance. In addition, schedule stability would be much in doubt. This method would also favor the larger carriers with the longer hauls in that they would be in better shape financially to afford slots.

Although the administrative method attained little success during the testing period in Washington, it does appear to have a number of points worthy of consideration. Some of these are:

- 1. Carriers current slot allocation considered.
- Number of passengers enplaned/deplaned (except for exempted flights serving essential air service points, flights would have to maintain good load factors to remain).
- 3. Number of cities served on a nonstop basis considered.
- 4. Restraint on new carriers entering a slot controlled airport.

It would appear a combination of the Administrative System and Schedule Committee could be an alternative to any method submitted thus far. With a firm approach toward total numbers, administered by the FAA, the Schedule Committee could in most instances, attain resolution by sliding thru out the day. Mr. John M. Rodgers Page 2 March 20, 1980

The following are some thoughts on the actual exercise.

Problem 1:

On Page 13 of the slot allocation evaluation, the indication is that there may be an efficiency involved with the auction system because of the comparison of profitability during the various iteration. Such a comparison, in our opinion, is not valid. Since each of the teams were given their base schedules, and except for a few minor changes, these schedules formed a base period. Any comparison to it fails to recognize efficiencies through the scheduling changes made by "scheduling experts" in the latter iteration. The slot allocation evaluation makes mention of this very fact in the last sentence on Page 16.

Problem 2:

The MIT model is an excellent model but does not compare to the real world scheduling practices. For example:

- (a) Inter-line connections were not considered.
- (b) The "schedulers" did not have a good feel of their cost levels.
- (c) There was no traffic advantage of market identity.
- (d) There was no cost penalty that we could determine for significantly reducing operations at one station or increasing it at another, i.e., at the extreme, a carrier could drop a city and enter another city with no cost penalty.
- (e) The model contained three types of airplanes including the DC-9, 727 and a 707. It is hard to determine, but we do not believe an aircraft preference factor was used and if there was one, it did not seem to be comparable to real world experience.
- (f) One of the greatest advantages in a slot auction system would be the use of wide-bodies equipment because of its efficiency in terms of cost, the public appeal of such aircraft and the greater number of passengers carried by this equipment in relation to narrow-bodied airplanes. This makes us wonder why such an aircraft was not used in the MIT model.
- (g) The larger airlines are much more sophisticated and better equipped to handle their massive systems in the real world. The MIT model does not reflect this adherent advantage.

Problem 3:

The model was set-up to maximize short term profit. Doing such, it overlooks real world realities. In our opinion, bigger carriers would be willing to sacrifice short term profit in order to become more dominate factors in the market in the long term. They would be in a better position to force small carriers out of markets and suffer short term losses in order to reap better long term profits. Mr. John M. Rodgers Page 3 March 20, 1980

We would not advocate another meeting in the same posture as before. Cost of MIT Personnel, computer equipment, hotel rooms, etc., would be unreasonable for what we would expect to accomplish. We would suggest further refinement of the administrative system and a later review or evaluation exercise.

Sincerely,

PIEDMONT AIRLINES

R. L. McAlphin

Staff Assistant Vice President -Airline Scheduling

R. L. James

Director - Route Development

RLM/1r

605 THIRD AVENUE, NEW YORK, NEW YORK, U.S.A. 10016

March 25, 1980

John M. Rodgers Acting Chief, Economic Analysis Branch Department of Transportation Federal Aviation Administration Washington, D.C. 20591

Dear Mr. Rodgers:

Enclosed are comments pertaining to the FAA slot allocation exercise as you requested.

It is the desire of Trans World Airlines to see the slot allocation problem resolved to the mutual satisfaction of all interested parties. In light of this, TWA fully backs the position the ATA has taken to perserve the current system for slot allocations until a new system is developed that will fully satisfy the needs of the industry.

The enclosed comments are in no way to be taken as an endorsement of either one or both of the methods under study, but hopefully, will assist in the search for a solution to this very serious problem.

Sincerely, abback ...

hard J. Zablocki

Enc.

TRANS WORLD AIRLINES, ING.

I. Which method did you prefer - the Trading Post Auction or the Administrative Allocation? Why?

The Administrative Allocation procedure, although flawed, seems to be the better method. The main objection to the Trading Post Auction was the considerable expense required to obtain the desired slots. This added expense obviously has to be passed on the the consumer either in the form of peak hour surcharges or across the board fare increases. This does not serve the best interests of the airline or the travelling public. With the Administrative procedure it was possible to acquire all of the desired slots that Airline White needed without incurring any additional costs. Unfortunately, the flaw in this method showed up in the hourly distribution of these slots. It is not realistic to expect to schedule an airline using an even distribution of operations throughout the day. Natural peaks will occur due to length of haul and connection bank timing, in addition to passenger preference.

II. In each of the two methods did you significantly alter your airline marketing approach as a result of the slot allocation? If so, in what way?

The Trading Post Auction allowed Airline White to maintain its schedule intact simply by using a method of progressively inflated bidding for the desired slots. Since the number of peak hour slots that were desired by Airline White were minimal it was fairly safe to assume that a high bid would be less damaging for this Company than any of its competitors due to the overall number of bids tendered. Those airlines desiring more slots in the peak hours would or should be more conservative in their bidding to insure a minimum expense.

The Administrative Procedure actually worked differently for airport AAA than at airports BBB and CCC. The allocations at airport AAA seemed to be handled strictly by the rules of the game and in so doing created a situation for Airline White that was less than desirable. In offering alternative plans to reach an overall solution, Airline White found this situation coming to a resolution using its least desirable plan. This, in conjunction with the limits placed on the maximum number of slots an airline could request in an hour, in my opinion, was a serious blow to this airline's profitability.

At airports BBB and CCC the rules were somewhat more relaxed when a solution by the original procedures could not be reached. Through the committee method, Airline White was not only able to assist in reaching a solution by rescheduling, but did so in such a way as to improve its profit making potential. Slot allocation by means of a scheduling committee was a definite plus for Airline White. III. Do you consider the two methods to be fair? If not, in what way are they unfair?

The Trading Post method seems to favor the smaller airline that is not heavily scheduled at the slot restricted airports. As long as the airline was willing to pay the price, the slot was relatively easy to acquire. Although we did not fully see it during this demonstration, a serious escalation in the bids seems destined to take place every time the participants sense a particular round of bids may be final.

The small airline can afford to pay the high price and spread the cost out over its entire route structure, which for the most part is operating at unrestricted airports. The larger trunk carriers that are heavily concentrated at the restricted airports will have to either pay the high prices and pass these increased costs on to the consumer or reduce its operations.

The Administrative method, as an alternative, tended to be too restrictive. It is my opinion that an administrative procedure set up with the original guidlines will most likely enable the large, strong airlines to retain their strength and grow while creating a downward spiral for the smaller, weaker competitors. With each successive allocation period as the smaller airlines' share of traffic shrinks due to a reduced number of operations, their total number of slots allocated will decrease. Thus, less operations are allowed, less destinations are served and, of course, fewer enplanements and deplanements will be accounted for. The following period's allocation of slots will be still smaller to these airlines based on the previous results.

IV. Were you able to handle the total information flow comfortably in the time available in each method? Was more time required (a) for rescheduling, (b) for bidding, and/or (c) for submitting preference plans in the Administrative method?

As the representative for Airline White, the smallest yet one of the most profitable airlines, I had sufficient time to handle all aspects of the agenda. After the initial period of scheduling, the relative strength that was developed due to the overall profitability allowed me to have a lot of control over the various situations in terms of my own schedule.

V. Was the evaluation exercise sufficiently realistic to allow conclusions to be drawn from the real world? If not, how would you make it more realistic?

The only major problem in terms of this exercise being realistic was the aspect whereby the airlines were able to change their schedules

with relative ease. There are many constraints that a scheduler must face in the process of developing a schedule, slots being only a minor issue. But, once a schedule has been developed, even a small 5 minute change has the potential to create problems at various other points on the route structure. Certainly, additions and deletions of service and likewise, major time changes can create a catastrophic chain reaction.

I raise this point to indicate the great deal of difficulty a scheduler could have when trying to come up with alternative plans for the Administrative method or trying to maneuver an operation so as to avoid a high cost slot in the Trading Post method. In the real world I think you will find that the airlines are not able to be as cooperative or be able to restore the same profit potential to a flight or series of flights that must go through forced schedule moves.

VI. Assuming one had to implement one of the two alternative allocation methods, what changes would you recommend in each method to make it more practical?

Some changes that I think are worth experimenting with for the Trading Post Auction would be to eliminate bidding with money and instead devise a point system. Points would be allocated to each airline based on variables such as airline size, history, traffic and efficiency similar to the Administrative method. The airlines would than be free to bid on whatever slots they desire using these points. A post trading period would be desirable where the airlines would be allowed to swap slots on a one for one basis. This would allow the airlines that were not able to acquire their desired slots to try to make the best situation they can out of it.

The Administrative method might best be improved by simply limiting its use to the overall allocation of slots to the individual airlines. In conjunction with this, a scheduling committee type of operation could then take over and go through the current processes in use for deciding the hourly allocations. This would satisfy the needs of the new entrants and yet preserve the flexibility of the scheduling committees.

US Air

WASHINGTON NATIONAL AIRPORT + WASHINGTON, D.C. 20001

March 31, 1980

John M. Rodgers Acting Chief of the Economic Analysis Branch Department of Transportation Federal Aviation Administration 800 Independence Avenue Washington, D.C. 20591

Dear Mr. Rodgers:

This is in reply to your letter of March 7, 1980 with which you forwarded the results of the management game. First let me apologize for the delay in responding but as f already mentioned to you I did not receive this report until March 17, 1980 and with the press of closing out our summer schedule plus digesting the information contained in this report, it was not possible to respond earlier.

Per your request the following are my thoughts and observations concerning this subject:

For reasons which will be discussed below, I do not feel that I can support either the trading post auction or the administrative allocation.

The base schedule on which the entire management game was predicated was developed in the short period of one afternoon. In the early stages I can say that I was not sufficiently familiar with either my own airline (Gold Airlines) or with the market place in which this airline would operate to provide profitability comparisons between periods of time. I know in my case that during the various auction periods I made improvements to my own airline as my familiarity increased with the markets available and the schedules of other carriers. While I certainly cannot speak for the other airlines, I am convinced that this was true of each participant. As a result, it is my impression that the base period was grossly understated in terms of industry profitability and the comparison of profitability results with later option periods was distorted. The implied result on page 13 that slot purchasing did not interfere with airline

U.S.ALL March 31, 1980 Page Two

profits (and costs to travelers) is not a logical conclusion. Again, it was the action of the schedulers becoming more familiar with industry traffic, the competition, their aircraft and the model manipulations that allowed the results to occur as they did.

Further to the model itself, I do not believe that there was sufficient realism to determine if the results could be applied to the real world airline operation. On the operational side, there were no constraints or costs considered for maintenance, airport facilities, ground servicing, crew restraints or airport curfews. On the traffic side which is indicated on page 4 as the heart of the game, it appears that the model contained unduly large amounts of traffic stimulation evidenced by the results generated by operating off-peak schedules. As an example Gold Airlines added a very late night short haul roundtrip and generated a load factor of approximately 85% which did not appear realistic. I also found that in one particular market the break even level was only twelve passengers. This again demonstrates that the only reason the industry showed a profit increase after paying for slots is because the participants learned how to use the model'sidiosyncrasies to their advantage. The equipment types used in this exercise did not offer sufficient disparity of capacity. In the real world, the price carriers are willing to pay for slots will be directly related to revenue potential and carriers with large capacity aircraft could easily outbid those with smaller aircraft. The largest aircraft used in the model was a B-707 and the smallest a DC-9 while in reality equipment could vary from jet type aircraft of as little as 74 seats to the Boeing 747s with potential capacity of 400 seats or greater.

Based on my participation, it is my impression that neither method is totally fair. Under the auction method the cost of obtaining the necessary slots would result in either increased operating costs or higher fares to the traveling public. These added costs could result in discouraging competition in cases where a new segment under consideration has one or both airports under slot allocation. Further, carriers themselves could speculate in slots by purchasing unnecessary slots and then attempting to sell them at a profit in the after market. In the exercise Gold Airlines did this with some degree of success. Carriers could even purchase slots in excess of their needs to stifle competition.

Under the administrative allocation system provision is made for new carriers to automatically receive four slots. However, incumbent carriers could find it much more difficult or perhaps impossible to either enter new markets or expand existing ones.

U.S.Air March 31, 1980 Page Three

Under this system they have no way of being reasonably centain of obtaining the slots necessary for such service. Infact, under this system I believe it possible for incumbent carriers to have to involuntarily reduce existing services to the public to accommodate a new carrier's slot request. This I believe would severely restrict the free market place.

Based on the above, I believe that a great deal of additional study is required on both plans before a final decommination can be made as to the viability of either option. Considering the limited experience the industry has had with these two options, I believe that as currently constituted both fall far short of the intended goal of providing a vehicle which satisfies the interests of both the public and the airline industry. However, if either plan were mandated by the government I presume the industry would have a way of making it work, yet this study fails to identify many of the ramifications for the traveling public and the industry.

Very truly yours,

Jun a Frieson

Jerry A. Frissora

JAF/kml

6. CONCLUSION

The testing of two slot allocation methods in the environment of the Airline Management Game has been demonstrated. In particular the Slot Exchange Auction has been subjected to a gaming/simulation test in conjunction with fairly realistic airline scheduling. The test was inconclusive in regard to (a) convergence to equilibrium, (b) the economic efficiency and equitability of the Slot Exchange method. Further testing should be undertaken before implementation can be seriously advocated. These further tests should provide for more time for bidding; more rounds of bidding; possible application of one or another stopping rule; improved realism in the game scenario; and, finally, an experimental design with controls for participant learning. Under these conditions the advantages and disadvantages of the Slot Exchange can be fully discovered in the testing environment so as to avoid faulty implementation or adoption of an inferior allocation method.

REFERENCES

- 1. Antonio Elias, <u>The Development of an Operational Game for the U.S.</u> <u>Domestic Airline Industry</u>, Flight Transportation Laboratory, Massachusetts Institute of Technology, Cambridge, MA, FTL Report R78-5, February 1979.
- 2. Federal Aviation Administration, Slot Allocation Evaluation, March 1980.

Ð

SECONDIX A

PPENDIX

.

A CARLES AND A CARLES

Table 3.1	Aircraft Data
e de L'auto Millouis	Network Data
1. I	Airport Data
2041 AL	unitial Schedules
	Traffic Data
्य धन्त्र हो	eriod 1 Schedules
NO STRUCT	Period 2 Schedules
Exits House	Period 1 Traffic Data
	Period 2 Traffic Data

TABLE 3.1 AIRCRAFT DATA

UNIVERSE FILE PRINTOUT FILE ID:FAA_0001 MIT-FTA CASS

LAST MODIFIED 80/01/18 14:16:27.00

ALC: NO

0:47 1:06 0:43 SPEED DOC/M DOC/D DOC/D DOC/S-M TF/DP TF/DAY (MPM) \$ \$ \$ MIN HHIMM RANGE SF TYPE SEATS (M) (M. DC9 90 2000 4 727 150 2000 4

EXPLANATION OF TERMS:

DOC/H is the direct operating costs per sircraft block hour. It includes all the costs that can be allocated to flight time, e.g. fuel, crew, direct maintenance, etc.

QQC/O is the direct operating costs per aircraft takeoff/landing cycle. It includes all the costs that can be allocated to a takeoff/landing cycle, such as dispatching. grownd servicing, tire eest, etc. It does not include landing fees or slot charges.

DQC/D is the indirect operating costs that are independent of the flight time, such as maintenance burden, insurance, etc. It does not include depreciation or financial or lease costs.

The above three items are the components of the openating costs. The following three items are derived from the above costs, and are presented for reference only:

DOC/5-M the derived direct operating costs per seatheile.

16/00 The number of flight minutes that would cost the same as a landing/takeoff cycle.

17/Day the number of fiight minutes that would cost the same as the daily indirect costs.

State State State

TABLE 3:2 NETWORK DATA

ALC: NO

Sec. 17.

in the second

77

ی.

•••• AIRPORT DISTANCES AND BLOCK TIMES : 10:1A._0001 DC0 707 DC0 707 10:00 10:00 10:00 10:00 10:00 00:00 10:00 10:00 10:00 10:00 10:00 10:00 228 :5: - 714 CASS **MITTA**

LAST MODIF: 80/01/18 14:16:37.00

i i

**** AIRPORT DISTANCES AND BLOCK TIMES **** - FILE ID:FAA_0001 1222525 8878788 1992 12 ŝ MITFIA CASS 2

4.10.1

TIMES **** LAST MODIF: 80/01/18 14:18:37.00

LAST MODIFL 30/01/18 14118137.00 **** AIRPORT DISTANCES AND BLOCK TIMES **** ##7774 CASS - FILE 10:FAA_0001

Ī				ļ	
2	2	1	SX A	707	727
Ī	-	755			
Į	3	258	1:54	0:54	0:54
į	500	3	1:07		
Į	000	3	1:26		
Ī	EEE	Ī			1:44
Ī	111	Ş	uit	1:51	1:51
Ī	200		÷ (6 : : 6
Ī		5			1:20
į	71				
		;	74		
I		ţ	D 🖬	•••	
			۱đ		
Ī	000	265) (1		
į		573	I Ĥ	1:24	
Ĩ	N.N.N.	2200		4:55	
Ξ	444	e	••	1:08	ē
	į	12	45:0	••	0:54
=	222				
Ξ	8	235	6 7 :0	0:49	61:0
Ξ	EEE	28	9: io	••	
3	555	Ş		••	••
Ξ	33	538	ē.		
=	Į	5		••	••
Ξ	2	6.4	•	••	
Ξ	KAK	ź	<u>.</u>	••	04:0
	ווו	ŝ	0:33		
	Ī	124	6	••	0:55
	Į	•		••	
	8	•	÷.,	••	0
			1		
3		655	••	••	1:26
3		233	Ŧ	919	
3			0	•••	
3		; ;	••		82:5
				77.1	
				•••	
33	31	250			
3			ē	•••	
3	line in the second s	23	R	1:20	1:28
3	111	300		0:47	
ł	I	628	ä		
ł	Į	134	1:41		
₹	8	Ĩ	6		
₹		ž	ñ.		
3		Ī	÷,		
	4	Į			
		7			
	}	5			
				•	

80

			1	1
	1	Š	101	727
	Ā	9	9:9	1 🕈
_		1:20	1:20	ü
1	150	0:53	0:53	5
23	95	1 5:0	5:0	<u>ي</u>
I	i			1:28
ŧ	160		65:0	1
31			0:20	
lä				0:48
8	370	1:0:1	1:01	10:1
	276	0:47	0:47	0:47
1 1 1				
Ī	15	:01	1:07	1:07
Ξ	151			0:33
31			6.4.	
	ñ			
I	20	••	[::]	[::]
8	E	••	4	
1;		••••		
		•••		
i	530	••	1:25	1:25
ដូរ	8		1:22	1:22
32	[7		0:23	
	8	•••	5	05:0
g	5	•• •		1:20
=				
:3	5			
ž.	95		65:0	0:53
31	<u> </u>			
I				
ŧ	244	•••	94 :0	07:0
	52		5	4:01
ŭ	101	••	1:47	1:47
	21			
g	628		16:1	1:31
E	55	6 0:2	7:0 0	2:09
:3	12			
	696	1:21	1:21	1.21
E	95		1:13 0:17	1.1.1 1.1.1
8	4	8	5	1:05
		19:10 19:10	6:20 6:10	55:0

LAST MDDIF: 80/01/18 14:18:37.88

**** AIRPORT DISTANCES AND BLOCK TIMES **** 4:19 4:00 3:36 10:FAA_0001 4:18 ------ FILE MITFTA CASS

LAST MODIF: \$0/01/10 14:16:37.00

A. 13 8 8 9 9 7 1

Į		5	707	727
	1			
~ #			DCHC	1484
		1524	2690	5861
		674	6621	661
		202	2161	
		5001	3415	5762
		1117	2127	1456
			2649	1010
		1214		1552
			1222	629
		693	1327	106
		416	1746	E 51 1
		695	1001	
		6656	6761	4670
		1452	2754	1681
				0001
			1212	
		1277	7542	499
			2768	0054
÷				5191
			2220	1526
		134	1410	959
ē.		2721	2604	1747
à l		679	3179	2185
		191	2277	1560
			2061	1261
- 2				
- L				
			2041	1991
: 2		1245	2067	1623
		1569	2973	2043
	~	195	2834	1946
- 2		1100	2096	4541
-	•	200	1539	1048
- E (٠	104	2103	6011
-		848	1814	1239
		825	1581	1077
# 7			222	PE41
	•		0120	1022
		100 C		
		1524	2890	1985
		1117	2127	1456
	~		1602	1001
14	m	1214	2308	1582
**		699	3161	5173
. 2		1960		
6 8		200		

ST MODIF: 80/01/18 14:18:37.00

A CONTRACTOR OF A CONTRACTOR O

83

MITTA	TA CASS	- 114	10:FAA_000	-9001	÷	i	0	•			*	-	i
E.	10	1	ŝ	707									
	İ	595	i i	2684	1842								
		179		1271	2								
		370		9061	8								
88]		264	2012	1647								
				2012	: 8								
		2		2296	5								
		267		87.05									
		147		1299	98								
				2427	1664								
				2367	1623								
				2308	1582								
					2210								
				2535	1738								
				1689	1152								
	•			1553	1058								
				6 50	570								
				1539	E+01								
				1936	6261								
				1215	823								
	-			1154	6494								
					168								
				80/2									
				1605	6411								
				2026	1366								
				1200	2284								
				2354	1613								
				2434	1608								
					980								
				1299	681								
				1403	954								
	-			6249	4315								
					0601								
				28.24	1946								
				2005	2291								
				2583	1772								
				2026	9901								
-				2440	1678								
1					18/1								
					1916								
				1036	1323								
3				2664	1842								
				2776	1907								
				1240									
33					2074								
	-									·			

ER STAGE **** LAST MODIF: 00/01/10 14:10:27.00

•

S. D. S

÷,

.

727 23165 23
 - 714
 D::7A.001

 755
 100
 701

 756
 1100
 703

 756
 1100
 703

 756
 1100
 703

 756
 1100
 703

 756
 1100
 703

 756
 1100
 703

 756
 1100
 703

 756
 1100
 704

 756
 1100
 703

 756
 1100
 703

 757
 1001
 703

 756
 1100
 203

 757
 1001
 703

 758
 1011
 703

 759
 1011
 703

 750
 1011
 703

 751
 1011
 703

 753
 1011
 703

 754
 1011
 703

 755
 1011
 703

 753
 1013
 703

 754
 1014
 703

 754
 1014
 703 BITFTA CASS
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1

LAST MODIF: 80/01/18 14:18:37.00 ::: STAGE ω • C 0 5 1 ••••

÷.,*,4

A REAL PROPERTY.

1 1 1 1		ž	8			
		2				
-				595	516	
1	3:					
_		951		1727	1178	
_	Į	3	1316	2489	1707	
_	8	¥2 9	113	2681	1840	
-		191	Ş	ē	1292	
		3				
	5				101	
	; 8					
_		276		5551	1058	
		0.90	1003	1915	6001	
_	9		1015	1936	1323	
_	Ī	435	1106	2106	1441	
	11	151	607	6411	194	
-	3	300	0.0	1553	1058	
-	N M M	150	5	1730	1011	
_	I	150	56	1730	181	
_	Į	80%	1197	2277	1560	
-	8	110	020	1591	1084	
_	4	153		1041	101	
	XX	1 935	3956	7440	5141	
-		149	633	1222	628	
		005	1372	2604	1787	
	1	200	ICCI	2528	1734	
3	9	405	1264	2402	1647	
ت د 1				850	570	
1	1	000	955	1636	1115	
3 1	3	601	5171	2684	1842	
Ĩ	I	202	1757	3325	2267	
-	-	92E	929	1776	1212	
5 1	77	628	1420	2695	1850	
ž	N N	350	505	1727	1178	
j Ri	ŗ	351	5	1730	181	
zi Zi	E			1271		
5 i 1 i	33					
L Ú			101	1000	4412	
		179	689	12E1	106	
ă Ş	į	569	1679	3179	2185	
ũ	ដ្ឋ	704	169	3210	2207	
ă I	8	722	1669	3161	2173	
ة ت 2	5	272		1539	1048	
n ê F i						
9 3 t 8					26.40	
	=	525	COCI	2475	1697	
5 8	3	134	1617	1900	2105	
ž	N N	5	1210	2483	1707	
ĩ	i.	80,5	1.97	2277	1560	
z: Z:	ł	218		1271	862	
		44	1074	2047	1400	
L 1					1202	
4 E						

South Manager

A . L. M. Water

86

÷.

BC3 707 727 914 1746 1197 914 1746 1193 1197 2777 1550 1398 3012 2069 1398 3012 2069 1398 3012 2069 643 1240 840 643 1240 840 644 1299 1811 643 1240 840 644 1299 1811 644 1299 1811 645 1713 1693 1321 641 1306 1606 1606 641 1306 1606 1606 641 1306 1607 1270 641 1306 1607 1270 641 1306 1607 1270 641 1306 1271 903 7301 1607 1270 903 7301 1270 903 923
,
2000 2010 2010 2010 2010 2010 2010 2010

COSTPERSTAGE **** LAST MODIF: 80/01/18 14:16:37.00

	2 OF 2						
ĺ							

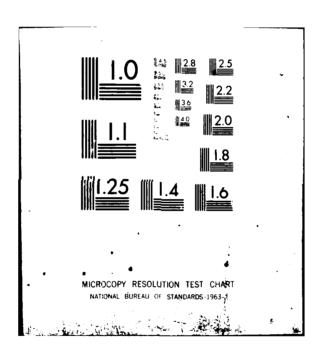


TABLE 3.3 AIRPORT DATA

. . .

A STATE

and the second stands about the second

1. 64.

LAST MDD[F]ED 80/01/10 14:16:37.00	nest
281×5856 F146 PR181001	MARKET LATITUDE LENGITUDE TIME COME BASIC BASIC COST/ REST
	MARKET LATITUD
#11-FTA CASS FILE ID:FAA_0001	

217-FTA CASS	FILE ID: FAA_0001			-	۵ ۵			-		
10 CITY MARE	MARKET SERVED	LA TI TUDE DD : MM: 55	LCAGI TUDE DD: MU: 55		W 100	BASIC TIME	BASIC COST	COST/ SEAT	REST CODE	
AAA ALMAA	AAA	41:00:00	62:00:03	~	8	2	a	8.0	0	
DATE SO	649	00:00:9C	74:00:00	-	ñ	2	•	0.0	•	
CCC CMARLIE	CCC	00:00:00	77:00:30	-	2	1	•	0.0	0	
DOD DELTA	000	41:00:00	75:00:00	-	3	=	•	0.00	9	
EEE ECHD	EEE	42:00:00	00:00:58	~	2	•	•	0.00	•	
FFF FORTROT		00:00:6E	00:00:06	~	20	•	•	8.0	•	
CCD COLF	999	00:00:CC	00:00	~	2	•	•	8.0	q	
New MOTEL	Ī	00:00:2E	77:00:00	-	2	•	¢	0.00 0.00	•	
III INDIA	111	40:00:09	00:00:00	-	2	2	9	0.00	•	
		33:30:C0	82:00:00	-	•	ŝ	ø	8.8	-	
MMM KILD	MAM	43:00:00	78:00:00	-	2	•	•	0.00	-	
LLL LIMA	111	34:00:00	82:00:00	-	9	uf)	•	0.00	-	
]	43:00:00	99:00:09	~	2	ufi	•	0.00	-	
NAME NOVEWORR	ł	43:00:00	91:00:00	•	2	•	•	0.0	-	
	8	00:00:90	60:00:68	•	2	•	0	0.00	-	
	114	00:00:6C	85:00:00	~	2		•	0.00	-	
	XXX	30:00:00	120:00:00	•	s	ç	¢	8.0	9	

TABLE 3.4 INITIAL SCHEDULES

Constant of the light

90

とうちゃう あんちょう ちまうゆう いい

Ő

...

								ł														•																												
		33	5	Į į	• •	-		8 3	2	Ē	21	E	3	ES	33	8	3		8	g					8		8	8		ş		8	8			R	2 2	18												
			-				_	-	-	_				_		_			_	_	B				_	_			-	_			_	_				_			}									
		33	-		_	_	_	_								-		_	-	-												_	-	-	_															
		-					_	_	_	_															_		_	_	_	_			_	_		_		0												
		127				_				-		_		_							0 73			!	Š	8	Š n																							
	NEO.	0100	6		000	000	000		5						100	022	023	020	5	6.0			111						-	-	::		2	2	Ř					5										
						•••	•••		-					 4	•••								•			4	-					•		•	•													-		
														-							999 1		-												_										0	o				
		7 0	9	2 9		,																_	-		U	.0	4	<	<	< 4	> <	. 0		8	-		< •	•	. •			ø	×		800	_	ų.	HÇ.		
							1																								33																			
- 1		AAA U	-		-	_																					-		-									_					-							
			-	-								_	-	-			-	_	-	-				-		-							-	-	-						-		-	-	-	-	-	-		
<		121	727			DC9			-						_	_		_	_	-							-	•						-										-		-				
u z	900	1221	1223		504	1403			GREEN		= :		5 8		22	5	17	ę	9	5	5	5		9		2	201	202	203		56	EQE	ğ	į	4	į,				503	603	50	701	702	ē	00	ā			
									•••				-	•	* *	•	•									-						• •								• • •	• • •		-		••			•••	•••	
																								-					_								_										N.K.K.			
H															KKK				_	_			3		FFF				Ī		_		-	_			R			Ξ				XXX ·			200			
		4 4 4 9 8 8																	8	-					-	000		-		_				_	-	-	-			-	898						_			32
-						-					-					_	-	_	_	-		-																												34
		AAA											32	;:			8	ບິ	8							Ī	8	Ş	M M M	Ē	3	8	Ī	000						-	XXX		8	???	MMM	Ī	8			ġ
		101								1		121	22		ŝ	Ì	727	727	727	727	727	52	52	Ì	600	727	727	727	727	121	121	127	727	727	727	127	121			ŝ	2	ŝ	ŝ	5	ŝ	50	S.	727	727	727
	3	752	ē		3	50			505	-	8	5	3	3			8	ē	07	5	5																													
	ē 				•••				J			-	•••	••					_																•••							-	-			-	-			
ł				83	202	3	2	y										8					ŧ		ł	8	8	YY					4	ł	Z							UUU	U	ü		ÿ	Ĩ	ប្អ		13
							_											-							_	-	_							-	÷.	· ·					-	-	_	_		-	-	-	-	
111		33	8	22					-	~	-									-			-			-	_	_					_	-		-								-	-	-				
INLT IN		-							1					ļ	į		i i	Ē	÷.	<u>.</u>	3	23	2 4				2	ð.	<u>s</u>	Ē	Į	1	3	₹	Š.	3	2	ļ				2	5	ÿ	ä	ö	ä	Š,	5	11
		84			30		5	ບິ	-	-								-	-	-	-							-	-							-	-						-	-	-	-	-	-	•	
CASS	¥	727 000	727 EEE	727 EEE		727 CCC	727 CCC	727 CCC	127	127	727						127	121	727	727	22	52			127	727	727	727	127	127	124	121	127	121	127	121					2	107	101	707	Į.	707	101	5	707	
	91 NE	84	727 EEE	727 EEE		727 CCC	727 CCC	727 CCC	127	127	727						127	121	727	727	22	52			127	727	727	727	127	127	124	121	127	121	127	121					2	107	101	707	1	707	101	5	707	

NTER A

• •

. .

A

ITTA CAR	ä	MLT LA						0	4 1 1 1										
TO ALPHA		Í		AA 2	TA DI	HA HA				TO ALPHA				14	TO ALMA			I	
																			•
		75.1	2	-				-				_	9				- 1		•
		; •	·	-	15:20	16:09		-	•		0		•	0				9	•
6:55 7:5	•	•	101 72		11:11	16:27			97 0				-	•			••	S	•
	2				19:91	17:11								0				5	•
1:00 00:2	•				16:15	16:71			- (101								
						60 . L I		-					•	• •			29 53		• •
ID: AC 11:5	22					19:07					2							2	•
11:12 11:4	: 2		102	227	00:0	60:01	. n 5	203 73	727 0	21:56 22	22:26		127	•••	FR MIKE			ł	*
11:14 13:5	~		-		19:12	18:81		-	0		}					3	N. 21	l	
12:30 13:5	5		-	-	90:61	20:15		-	0 10	FR FOXTRO	-			11 2	B:24 10:0	8	1 28	727	•
1161 06:21	5		-	-	10:02	21:10		•	0						Ξ.	-	H 231		•
12:27 12:21	2			•	21:57	22:36			0 (6:07	GL 600							•
					22.13	20.72													•
								đ											v
															•				•
	2		•				1 211	898	BL 742	,	2			•				124	•
17:38 10:1	M			•	97:01		1 211			FR COLF			-	3	1		L1222	727	
5				0 23	1 19:10	32	L 213					2.11			2	-	1 255	727	•
5	6		•	17	21:00	ö	L 902				7:35	GL 1220		0					
2	2		•	0	*-							10004	0 727	0	FR OSCAR			ğ	•
2			•	0 2	FA DELT	1.4			- 000	-		BL 2 8		0			53.37		
20:20 20:55	0	-		••		Ċ	93.	2 <u>-</u> :	•	18:09 18	- 1	80001		•	5:5 00:5	3	IL 200	121	•
2 2		5 C	: 2 5 :				58							į				ł	•
2		50	5 7 9	•	7:57	6	55									2	41.50		•
8:30 12:3	10	2 30			8:00		9L 2		0	FA HOTEL				- I				727	•
11:15 15:0	19 61	9.00			8:25						_	99.8			14:31 15:12	-	BL 253	121	•
14:56 18:0					00:8				1	6:30 7		BD002		0				1	(
14:56 18:1	1	2	55	PL 751	11:07				0		15:53	BL 28	1 727	•	FR KRAY				•
11/1 QC: 11											1	#00022							
FR CMARLIE				1 222	12:40			-		E1 E1:01	Í	270	9						•
	8	•			13:46	_		-	-	2	10 12:01	270	I	1		5		727	•
6:55 7:1	:	• • •	•	•	14:09	-		-	•						ö		•	707	•
7:00 7:1	<u>e</u> :			0					••	FR INDIA									1:
			-	• •	20.01			·						9					
• •	2		•	0	15:50	-	÷	402 73	727	-		5			FR ALPHA			3	
2	11	•	·		18:25	-		•	0	-				•		_			
9:59 11:4	•				16:34				- 0		13:57			•	ē			Ē	• •
															Ë				•
10:40 11:2				•	20:49			-		-			-		ġ				-
11:12 11:5			•	0		1				FR JULIET			-	- 3	2			į	•
12:07 12:4	•			••			1 261				3				Ξ			23	
																		5	- •
				-	11:35		1 212	38		20:30 22:				-				124	•
13:45 14:51	2			•	17:25	22:15 B	1 212	ប្ល	124		}				2		Ī	101	•
	29	3; 5;	87 51		17:25		L 212	ÿ		922			-	 	11 55	80	73 88	ŝ	- (
	25			••							5		2						•
	2				-						Ŗ		ĺ	-					•

ŗ.

žřž JJJ Ā ŧ z CAB 64.64 COMECTIONS 133 BL 200 AM Fasassasaassassassassassassassassass C: 0 16:5: 10 CHARLIE 212 ÿ 99999990N ******** BRAVO OSCAR PAPA 13:38 15:31 16:31 10:00 1212 . £ ----- 0000000 0-0 -2231 MMM DC9 DC9 727 727 Ī 727 **** z CAB 74.35 COMMECTIONS 1 15:33 BL 290 AAA 1 15:33 BL 251 AAA 23:29 BL 254 AAA VVV BL 270 R00030 GL 1141 R00042 R00042 R00032 46.58 RD0030 GL 322 GL 124 RD0032 GL 924 65.56 GL1120 GL 601 GL 804 GL 1205 2.03 812433 CT TON 6.9 252 CONNEC 17:53 BL TO BRAND FR MOTEL BRAND FR MOTEL 10:14 11:09 11:00 11:55 17:13 20:40 10:01 15:55 17:13 20:40 18:14 11:42 17:13 20:40 8:15 11:42 13:45 11:42 13:45 11:42 13:45 11:42 13:45 11:42 13:45 11:42 15:13 16:15 CAB 10:28 14:09 14:09 14:46 20:46 20:46 20:46 CA 11:42 17:12 14:20 ۲ NOVENBER JULIEF 4 7:30 12:43 16:30 17:15 7 17:15 7 Part 18:00 19:00 1 3 Ä 15:05 10100 11:24 11:49 18:51 6 Ĩ æ **.** 2 x ų ----2000 200 2000 2 . 23 200 2 23 29 200 2 23 N 0 0 0 ~ 000 231 HHH 0C9 727 727 5 E E 555 999 -737 727 727 727 727 727 727 727 727 201 au 000 727 009 009 CAB 69.95 9:12:07 10:27 16:10 20:37 16:10 20:36 14 223 16:10 20:36 14 223 16:10 20:36 14 224 12:11 22:13 11:51 15:13 14 221 AAA 11 11:51 15:13 14 221 AAA 11 16:31 19:39 14 221 AAA 11 16:31 19:39 14 221 AAA 11 16:31 19:39 14 221 AAA 11 16:31 12:16 14 221 AAA 11 16:31 12:16 14 221 AAA 11 16:31 12:19 15 22 AAA 11 16:31 15:39 14 222 AAA 11 15:59 19:59 14 232 AAA 11 55 z CAB 66.76 1:09 800030 DV 1:20 81 272 7: 1:53 800031 DV 1:54 800032 DV 1:00 800032 DV 1:00 800032 DV 1:33 BL 280 AAA B đ 49.27 RD0040 GL 800 GL 800 -... . 3885 7:11 1 12:10 1 12:10 1 12:11 1 11:20 15 11:20 15 ~ ----DAAD ECHO SL *** 2 2 2 ដ្ឋ 8 000 000 000 000 000 00 00 00 00 00
 64
 53

 64
 64

 64
 64

 64
 64

 64
 64

 64
 64

 64
 64

 64
 60

 64
 60

 64
 60

 64
 60

 64
 60

 64
 60

 64
 60

 64
 60

 64
 73

 64
 73

 64
 73

 64
 73

 64
 73

 65
 73

 74
 66

 75
 66

 75
 66

 75
 66

 75
 66

 75
 75

 75
 66

 75
 75

 75
 75

 75
 75
 3.6. 3.6. 3.6. 3.6. 3.6. 3.7. 4.6. 3.7. 4.6. 4.7. 4.6. 4.7. 4.6. 4.7. **INETIME** * 55335553335555 CASS CMARLIE TO BRAVD DELTA ATTTA £ E

> л, Л

> > Jos Anna 12

and the second
822322222222222222222222 *****83353336333383**834388883858**3 **** ALMA A 8 1212 . L 712 11 740 11 743 000 2 A -- 1000 ē22 KKK DC9 DC9 DC9 DC9 DC9 DC9 Ξ I 22 8 3333 z z 22 4444 **H** ゴゴゴ 74.15 GL 600 8 ECT1005 1 L 290 AAA 1 251 AAA 8 251 AAA 8 240.38 CR 901 CR 702 FCTIDWS 790 AAA F 790 AAA F CAB 61.36 COMECTIONS 1:28 8L 291 AAA 1 1:51 8L 253 AAA 1 1:46 8L 253 AAA 1 CAB 77.35 CONNECTIONS 1:40 BL 200 AAA 1 93.73 ECTIONS L 250 AAA 1 L 255 AAA 1 **m00220** GL 322 GL **5**22 GL **5**02 \$58 - 23:6 4 NDVEMBER COMMECT. 12:27 BL 250 9:59 BL 250 ¥33 10:09 CAB 10:09 COMMEC 15:34 BL 15:34 BL 15:34 BL . 888888 1 1222 -TO CHARLE TR UCHARLE T ĕñ **78 898**8 Ï OSCAR R LINA 9:15 1 1:4:45 10:00 1 FR PAPA 7:51 7:51 11:23 10:01 10:01 10:01 10:01 9:30 a 2 z 5 -00 - -0-00-11 -----.... W1 102 DC9 0 3 22 33 Ξ Ŧ CAB 57.16 16:45 EL 223 723 1 16:45 EL 223 723 1 21:33 EL 224 737 COMMECTIONS 2 13:03 EL 220 MAB E 2 13:03 EL 230 MAB E 2 13:03 EL 230 MAB E 1 15:34 EL 231 AAA E 1 15:34 EL 221 AAA E 1 15:35 EL 241 EB 2 15:47 EL 240 EA 2 15:58 EL 222 EA 2 15:47 EL 240 EA 2 15:58 EL 222 EA 2 15:47 EL 240 EA 2 15:58 EL 222 EA 2 15:47 EL 240 EA 2 15:58 EL 242 EA 2 15:47 EL 240 EA 2 15:47 EA 2 15:4 59.36 800040 0 GL 820 7 GL 822 7 GL 822 7 GL 142 0 GL 142 0 GL 142 0 CC 110044 0 CC 110045 CC 120045 CC 120047 CC 12 80.54 GL1220 RD0310 RD0330 5.0 i f 81.96 #00208 GL1401 . -322 2222 3225 333 3 TA COLF 0:05 10 0:05 10 0:05 10 0:05 10 15:00 10 17:50 15 1 CHARLIE F COD 2011 2010 CMALK 2010 2012 15:10 192 15:10 192 15:10 192 15:10 192 10:12 195 11:51 11:51 11 ÷Ξ 88 3=8 INET LAL 3 MIL

22222

1813

AND ADDRESS OF

94

Э ٥ z + X

CC 1 11:00 11:100 11 202 AM. EZZ ž ž 111 i i i i 3 Ł 22 8 i 555 22 **3**333 CAB 78.15 COMMECTIONS 1 15:15 BL 200 AAA 1 1 15:40 BL 200 AAA 1 1222 222 ¥55 ----F DELTA F DELTA 16:29 19:40 16:29 19:40 10:00 20:20 11 20:00 20:20 11 20:10 20:20 11 10:37 20:00 11 10:37 20:00 11 10:37 20:00 12 1 FOXTNOT CAB 12:15 13:48 18:21 19:54 388 FR INDIA 5 10:38 10:3 12:28 12:2 JULIET R MANO 12:36 13 15:15 11 15:15 11 14:39 14:31 20:56 75 88--12:15 19:21 19:36 2 19:36 2 2 . E

 10
 DELIA
 000
 1

 19
 19
 17
 19
 17

 19
 19
 17
 19
 17
 19

 19
 19
 17
 19
 1
 19
 17

 19
 19
 17
 19
 1
 10
 10
 10

 19
 19
 11
 12
 11
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 12
 2 500 S. Se CA R 8400 231121121121 ë 2 ā £ 000 1 727 1 727 1 727 0 727 0 727 0 727 0 009 0 NMN 2 BL 261 111 1 0000 0 N O N 0 5.53 260 • 0000000 37 1 KKK I -ಕಕತ z 73.75 ECTIONS 290 AAA 251 AAA CAB 95.53 CONNECTIONS :31 BL 250 AAA 81.84 800200 611401 800220 800220 CAB 70.75 COMMECTIONS 41.28 61120 61120 61 922 61 922 61 923 61 923 61 923 50.38 . 8555 CAR COMMEC 14:50 BL 14:50 BL 23:19 BL CA 13:07 14:52 14:52 CA 9:34 9:35 17:55 19:35 19:35 CAN 11:26 16:41 NOVEMBER 6:30 1 10:55 13 12:40 14 12:40 14 12:40 14 MINE PAPA 12:01 9:30 2 . £ 1 1 121 ----272 261 263 260 -~ n n-- --22 555 3 Ī 56 đ 727 44 22 CAB 69.65 14:50 61 301 00 14:15 01 13 00 14:09 01 202 72 14:09 01 202 72 15:52 01 200 000 CAB 93.13 19:30 BL 242 72 CONNECTIONS 12:31 BL 240 AAA \$8.03 GL 1220 ND0310 78.15 61 800 61 820 INI TIAL CAB 13:56 17:30 6:15 11:48 8:00 11:36 4 4 C CHARLIE BITTA CASS PR FORTROT ëë HOTEL FR ECHD 202 111157 9:30 7:30 2 2 .

95

77. .

A CONTRACTOR

uu DC⊮ EEE DC9 Ē \$\$\$\$\$ 44466 **4**02 5 - 5 66.36 GL 924 79.24 80011 81 2021 81.84 80.148 80.216 80.123 80. 7..... - 8 -#85888 11:57 12:04 11:57 12:04 20:02 22:05 20:03 22:05 20:04 10:26 13:15 11:00 13:15 11:00 13:15 11:00 13:15 11:00 13:15 11:00 13:15 11:00 13:10 355555 08 F 3 10.00 1 NOT TO INDIA 91510514 ECHO 37387 Į ----æ z 000 1 727 1 DCS 0 - ----DC9 C 582 EEE Cost •••••• 8 8 30 22 ž 0 GL 82 CAB 94.43 CONNECTIONS 1:33 BL 221 AAA 221 AAA 74.25 R00030 49.37 RD0030 85.43 66.1140 61.172 61.172 222288229 8222228 28225 858 **7**85 ²8833888 TO MOTEL TO MOTEL FR DELTA 17:33 19:50 18:00 19:37 FR ECHO 71-35 9163 451-85 921-15 451-85 921-15 451-15 70 10014 CA5 9:54 CAE 8:54 5.5.5.5.5.5.5 5.5.5.5.5.5 5.5.5.5.5.5 5.5.5.5.5 5.5.5.5 5.5.5.5 5.5.5.5 5.5.5.5 5.5.5.5 5.5.5.5 5.5.5.5 5.5. CAB 5153 385535855 33: w 7100 11:00 12:20 16:20 12:20 16:20 12:20 16:20 12:20 16:20 12:20 16:20 12:20 16:20 12:20 16:20 12:20 15:10 12:20 15:10 12:20 15:10 12:20 15:10 12:20 15:10 12:20 16:20 12:20 12:20 16:20 12:20 1 JULIET 9:12 B ŝ ÷. ٤ 11:51 R GOLF 7:11 1210 3 7:00 DEL :: ٥ ۲ F# . a. Ľ I FR CHARLE FR CHARLE FR CHARLE 13:35 14:14 RD0320 727 0 CONNECTIONS 8:30 13:58 8L 210 688 8L 272 11:09 13:58 8L 210 688 8L 272 11:09 13:54 8L 214 688 8L 272 12:25 14:14 RD0320 727 1 000 1 U DC9 0 1444 -5 HHHH DC9 , ULU DC9 80 727 727 727 727 727 727 727 727 727 8 222222 t c 74.25 R00032 48.47 RD0032 49.27 RD0030 BL 270 RD0041 LL 821 LL 821 LL 821 RD0032 GL 142 GL 142 GL 845 RD0045 -----su un R00020 BL 281 R0022 59.36 GL1140 ND0041 ND0043 GL 823 ND0045 78.15 61 821 80 80021 61142 61 841 61 841 CA3 65 CAS 208 18:21 18:28 46.0118:05 10.0018 10.0018 10.0018 10.0118 10.0018 10.0018 10.0018 10.0018 10.0018 10.0018 CA 17:11 22:51 CAB 8:54 8:53 11:31 11:31 13:23 13:23 13:23 13:23 13:53 13:53 13:53 13:53 13:53 13:53 13:53 13:53 13:53 13:53 13:54 13:54 13:54 13:54 13:54 13:54 14:54 15:55 15:555 15:55 155 CAR 13:23 17:12 17:13 17:13 17:13 17:13 10:38 14:33 20:38 CMARLIE 1.46 9:55 9:30 11:3 5:10 17:1 8:43 19:55 0:50 22:55 FR HOTEL 17:12 18: FR JULIET BRAVO DELTA 7:50 8-4-3-4-6 8-9-9-9-6-6 ----. . . FF 2 FF CMARLIE 64.54 FF CMARLIE 64.54 13:59 15:47 64.601 059 1 16:50 18:51 64.242 727 1 21:57 23:25 64.602 059 1 21:57 23:25 64.231 065 84.273 13:40 19:06 84.231 045 84.240 13:40 19:05 84.231 045 84.273 13:49 19:35 84.731 AAA 84.240 13:49 19:35 84.731 AAA 84.273 13:49 19:35 84.731 AAA 84.273 13:49 19:35 84.732 AAA 84.273 13:58 19:35 84.732 AAA 84.273 17:58 19:55 84.732 70 000 1 17:58 18:51 84.242 000 1 17:58 18:51 84.242 727 0 - - -222 . 000 727 1881 7 881 7 81 81 211 121 121 121 121 121 000 MMM ដ្ឋ 31 93.12 81.242 7 81.242 7 81.242 7 261 648 7 261 648 7 21 664 8 C4B 82.64 12:43 15:47 GL 601 D 10 COLF CAL 76.25 20:30 23:35 GL 602 DX CONNECT IONS 20:31 1:35 BL 282 AAA 1 71.55 ND0010 81,280 81,280 81,280 ------66.76 100030 11 273 100033 100033 11 1233 80.54 800300 INITIAL 2 1944) 2 2 **2 2 2 2** 2 **2 2 2 2** តីតិត C.49 9:19 9:19 9:19 a; 17:35 23:35 23:35 2 0.000 CASS CHARLIE JULIET 17:58 1 8:00 1 13:55 1 13:55 1 15:15 1 #110 15:57 21:56 0010 ATTTA . g

いたちのころである

96

Sec. 1

1 H

1. 1. A.

16 00 151 AM 01 240 *** žž 200 11 ir m ž z X Ï Ē ą į Į 81 ŧ ğ ł Ħ 121 55 đ È CAN 116.01 CONNECTIONS 1 20:20 BL 201 AMA 1 11 CAB 47.70 COMIECTIONS 9:30 13:26 BL 249 AAA CAB 06.06 COMECTIONS 17:23 21:20 01 742 AM 333 CAB 01.23 COMECTIONS 21:28 BL 202 EEE CAB 45.29 9:40 11:26 01 25: 16:51 18:28 01 25: 10 05:08 CAB 96.53 117 611221 CONNECTIONS F 203 85 ž CAD 77.25 COMMECTIONS 16:10 21:20 8L 792 A 16:24 21:20 8L 751 A 9:00 13:36 0L 260 i z CAB 12:33 14:17 FR CHARLIE 16:40 20:20 19:12 22:51 CAD 10:34 19:20 NICH NICH NOVEMBER CHARLIE FR FDATADT DELTA DELTA HOTEL 15:53 FR MIKE 17:29 Ó 2 E Ē 2 E œ FR ALPHA FR ALPHA 6:57 7:31 6L 600 0C9 8:27 9:01 6L 250 727 0 15:32 16:06 6L 250 727 0 PPP 2 CAB 47.79 14:31 16:06 BL 253 727 1 TO NOVEMBER NWW 2 BL 250 BL 253 - 80 FFF 2 -555 -BL 253 • 121 AAA 727 727 727 g į ö ŝ ***** *** CAB 92.83 16:15 20:28 10.273 AAA 11 16:15 20:28 10.273 AAA 11 17:23 20:28 10.273 AAA 11 17:29 20:28 10.262 AAA 11 18:07 22:51 10.262 AAA 11 19:31 22:51 10.292 AAA 10 CAB 74.15 COMMECTIONS B:00 11:01 BL 721 AAA B 15:00 18:06 BL 712 AAA B COMMECT 1045 111 CAB 93.73 COMMECTIONS :26 BL 740 AAA :28 BL 723 AAA 53.37 GL 600 45.20 01 250 41.28 81.251 81.251 81.255 FR NOVEMBER CAB 7:30 9:01 CAB 10:45 11:26 13:36 14:17 17:47 18:28 20:10 20:51 CAB 6:00 7:31 FR FOATROT CHARLIE CHARLIE 222 BRAVD FR DELTA 0-0 ëëë E £ 2 I 7:51 11:57 51 60 009 1 10 LIMA CM 56.37 AM 2 7:50 1:25 56.37 AM 2 7:50 1:25 56.37 AM 2 7:50 1:25 56.37 CM 2 12:30 17:06 56.37 CM 2 12:30 17:07 CM 2 12:30 17:30 17:30 CM 2 12:30 17:3 1 11 ~ • 37 80 ដ ŝ 111 50 55 222 I 43.48 GL 320 86.14 61 322 61 322 89.43 GL1142 8.58 8.88 842243 8235 -\$335 ³33333 ⁸55555 14:00 17:09 18:00 21:11 7:00 10:42 7:00 10:42 9:25 10:09 12:30 13:14 10:29 11:50 16:15 17:06 CAB 17:52 20:16 59 3889 387878 1:30 10: FR CHARLIE 9.75 FR HOTEL FR JULIET 10 KILO FR INDIA FR DELTA FR INDIA FR MINE 7:00 F# MILD CAB 96.14 WWW 1 12:00 19:15 06.12 0C9 2 12:43 19:41 0.1 002 0C9 2 12:43 19:41 0.1 002 0C9 1 12:43 19:41 0.1 0.0 0C9 1 10 MILO MWW 1 TO JULIET JULIET JULIE 10 JULIET JULIE 14 FOXTHOT FFF J 18:07 19:41 GL 601 DCB 1 ~ ~ ~ ---..... • I g 3 111 8 3 5 55 ÿ 25 ŝ 48.47 N00030 49.37 R00032 66.38 BL 301 69.45 GL 600 GL 1201 65.54 61 802 61 142 61 142 53.67 61 920 61 609 61 1201 61 122 41.28 41.28 61.929 61.122 61.122 61.123 61.123 82.64 GL 600 INITIAL CAB 6:57 11:57 10:55 15:47 13:00 15:05 15:06 15:05 16:25 20:16 19:06 21:11 5.46 10.43 11:00 11:97 14:00 15:47 16:12 17:09 19:19 20:16 CAB 11:57 7:11 0:52 10:01 E1:41 CAB 0:48 11:50 BITFTA CASS PR CHARLEE FOATADT FE INDIA FR NOTEL FR BRAVD FR DELTA FR 20LF 00:0 2

97

. . . 3 3 FLIGHT SCHEDULES TO KRAY XXX 4 TO KRAY XXX 4 FA CHAPLE GR 902 727 1 15:30 19:14 GR 902 727 1 15:30 0:47 8L 721 AAA 8L 791 16:34 0:47 8L 751 AAA 8L 791 000 1 CAB 249.87 CONNECTIONS 15:10 22:32 BL 291 AAA BL 792 16:37 0:47 BL 262 AAA 9L 791 FR DELTA FR CMARLIE CAS 61.36 CCC 1 CAMECTIONS CCMMECTIONS 8:00 11:52 8L 720 AAA 8L 200 9:00 11:52 8L 722 AAA 8L 200 12:12 15:46 8L 722 AAA 8L 252 70 PAPA PPP 2 PPP CAB 46.28 0:00 0:52 0L 200 727 1 10 May XXX 4 Fr Alpha 727 0 727 0 BBB : 000 2 CAB 230.90 17:30 20:47 Bt 791 707 1 COMMECTIONS 14:36 22:32 Bt 211 CCC Bt 792 CAN 57.07 COWNECTIONS 11:46 15:46 BL 794 AAA BL 252 12:12 15:46 BL 231 AAA BL 252 CAB 60.56 CONNECTIONS 11:39 15:46 BL 280 AAA BL 252 7 H --050 1 - 200 33 727 1 Į 127 727 707 727 41.58 BL 200 BL 252 59.56 BL 252 CAB 240.30 6:55 10:14 Ca 701 15:19 18:32 BL 792 INITIAL CA8 0:14 9:52 13:06 13:46 6:00 10:14 15:19 10:12 17:00 19:14 19:33 20:47 C40 12:11 13:46 FR HOVEMBER BUTPTA CASS FR CHARLIE PR CHARLIE FR BRAVD PA BRAVO FR DELTA FR OSCAR FA 60LF

.

Starting Barrier

ē 103 E 04347 04343 0435043 **U1503B** STAT Ξ ខ្លីខ្ញ 5555555555555 ***** **33355**555 0 00 0044000444 < 0 < < 04 ~ ~ ~ ~ <00< ٥ õ 17:50 TIME 2885588 8 ۳ 8588888 Ł 2262222 22222 22222 222222 222522 22522 2252 22522 2252 ACTIVI E 188855333**1**85 Ξ 22222222225522222 *************** 53 35522222522 -----000 400404444 <0000<00<<0<0< 0 < 0 0 < 00 ALAPORT 13:57 13:57 TIME 178-88-1-1-888 -----55 22222222 EC 200 CG 201 CG 202 CG 3 3 0 0040 ----------........ ~ ~ ~ ~ 0 0004004440400 10:00 10:12 10:25 10:27 10:27 10:27 10:55 10:55 10:55 9:25 Ĩ 1131 88111181881111818118118118118144 11111717171884 818171 4 0 1101 000111110180101118118118118144 11111717171884 81817174 4 1101 0001111118188111181181181181181 193 8=8<u>5</u> 3 3558353 4553585345834 444554454544545454545454545455 4535 2 đ 0 • 0000<00 0444 2823 Ĭ **MITTA**



Seco

No.

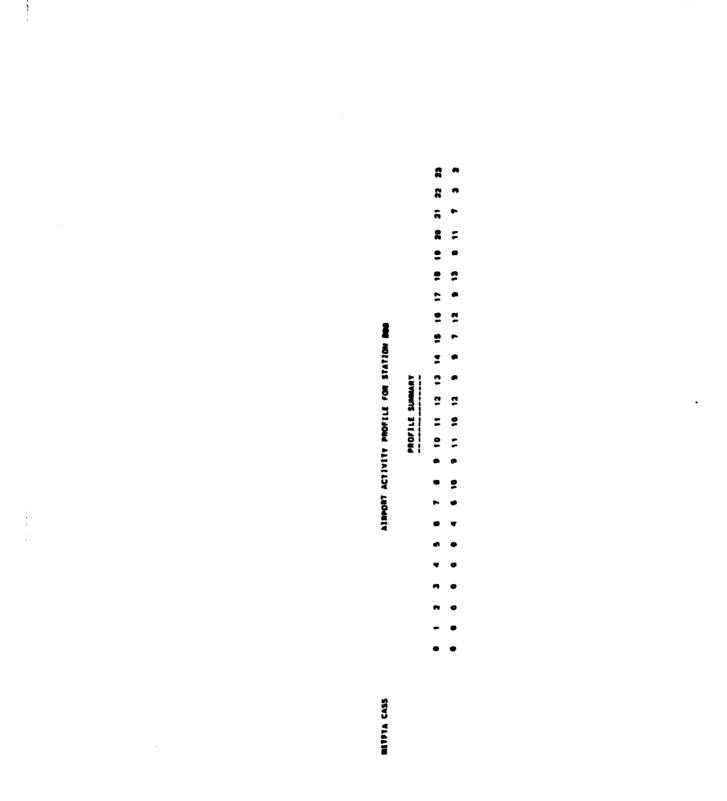
2.2.1

100

3 S STATION FLIGHT 400 5 < 0 õ 23:03 TIME PROFILE ž ACTIVITY 20 Ξ 885 5 00004440 040444404*4 >00 0 < <000 ø LIRPORT 17:07 17:12 17:12 17:57 17:57 21:06 21:13 21:13 21:56 ::: 3 222 ä 19 3 สรี 00 0<<<0 0<004< • 88 Ĩ 12 ā CASS Ĭ ILT FIA

101

and the second second second



į

a state burner burge

The state of the s

1. B. I. M. M. P. M.

102

3. 27 A 200

644.25

6										-		-			**			~	**		••							••		••	-		-		-	-	-					-	••		-	-	**		~~	**	-	,				
g	0		Ē	121	Ì	727	701																																																	
110H	E		100	204		101	÷																																																	
STAT	Ē	i	13	: 3		5	đ																																																	
ē	0	•	< 6	d)	4	۹																																																	
	Ĭ	•		1		3																																																		
2	=			18	1	ä	•																																																	
PROFILE	*		-	• ••	• • •	-		**		-	-	-		•••			••		••	••						-			-	-		-	-	-		-	-	-	-	•	-										-	-				
>	8	727				727	127	727	727	727	S	727	707	ŝ		727	ŝ	727	727	707	ŝ	727	ŝ	727	ŝ	707	ŝ	3		727	727	S	Š	727	727	707	727	2	707		727	ŝ	727	727	707	ž	S		727	ŝ	727	ŝ	727	Š	727	ž
11	Đ	501	35	2		403	53	8	2	8	8	5	5	8		5	8	ŝ	ç	2	3	33	ç	2	Ş	3	142	ĉ		8	8	Ş	Ş	202	3	2	3	53	Ş	I	8	\$	2	5	113	ç	6		3	3	2	8	2	924	3	3
ACTIVI	19				•	3	2	ī	3	8	ŝ	~	5	ŝ													-				-		-	-			_				а 	ŝ	2	ĩ	1	8	2									
	1 0	33									4		ē	ā o		3 0											10	3						5											ā				-					J V C V		
NPORT	¥	2		_		_	_	_					52	ŝ		_	-		_	_	_		_	_		_	5	ę	ŀ	_		_	_	_		-			-		_				ē	_	-		_	_			-	3		
					•	Ë,	ř	ř	÷	ñ	Ē	÷	÷	ï		••	••	••	••	••	••	••	••	••	**	••		••						9:20	•										20:3				÷	#	÷	-	-	-	2	Ξ.
•			-			-	_	-	_	-	-	-	-			-	-	ž	-	ē.	-	-	-	-	÷	-	-	-		-	-	Ē		-	-	-		-	-		Ň	~	e.	~	~	ć.	2		2	~	~	•	**	~	~	~
	0		2		2		0	1	5		2	2		2	2	5	2	2		2			2			5	5	•	ŝ		2	2	5	2		2		2	2	5	2	2	5	E		2	727		5				t	8		2
	2	ä														727																																								
	ā	ş			Ē	=	ē	503	ā	5	ŝ	::		ĝ	69	į	202	ŝ	ž	22	22	923	22	ž		112	ã	220	823	12	ā	560	222	1		101	5	292	3	233		212	751	ŝ	2	102	22	2	ž	23	322	 	22	322	2	22
	11	Ì		13			•							Ž	5	3	5	Ë	3	_	Ż	z	5	j		_	Ë	ĝ	5	ē	5	-															3							5		
	0	4		. 6		-	-	-		-				-	ŏ			-											0										-								š						-	0	_	-
	X		5	36	2	2	:	2	2	2	1	3		ů	5	2	'n	Ŕ	2	Ş	1	ş	ţ	3		8	8	2	5	5	39	S		4		ā	2	-	5	1	2	5	2	2	ā	ä	5	ţ	ş	5	3	1	8	ç	ñ	8
	ž.	Ē	•		••	••	••	••	••	••	•••	••			••	ë	••	••	••	••	••	••	••			••		••	Ĩ		••	••	••					•••	•••	•••	••	••	••	••	••	••	ä	••	••	••	••		••	ë	••	••
						-	_	_	-	-				_						•••					••	-				-		-			-							-	-	-	_			-		_	-					••
	•	727	2	5	g	51	5	:	5		-		727	3	5	:	51			5	2	3	5	5	5	27		5	ž	5	53		5	727						5	5	-	37	5	53	5	5	53		:	27	-	5	727	01	5
	ŭ.				_			_																									-			_		_					-	-		_										
	3	Ř		-		ā	ě	ě	-		ž	1	ŝ		š	Ē	Š			2	Š	ž	ğ	ĩ	ž	2	ē	\$	25	2	ē		•	214	ŝ	•	4	5	1	Š	12	ž	Ē	9	\$	21	ř	Ĩ		3	ĉ	8	2	ē	2	-
8	2	- 21	3	đ	13	8	ē	ş	3		đ	3	đ	5	ž	ā	đ	5		8	đ	z	ತ	8	ž	8	ತ	ತ	3	đ	đ		8		3	3	3	Ž	3	3	8	đ	ž	3	3	ě	z	ě		đ	ž	3	đ	3	đ	3
5	0			đ	0	۵	<	_	٥		9	-	<	<	۹	٥	•	•		<	•	<	4	<	٥	0	٩	0	٥	٥	0		•	0	-	•		•	-		<	۲	•	•	•	٥	•	٥		٥	٥	-	٥	٩	•	•
TTA	Ĩ			8	8		ä	2	5		8	2	ŝ	ŝ	Ŧ	1	ŝ	5		2	:		2	5	ŝ	:	ŝ	5	-	1	5:		ē	5	:	5		2	5	2	5	2	2	ŝ	8	-	-	1		ŝ	ŝ	ē	21:	:22	:37	5
Ĩ	Ē	Ű									Ő	ő	Ő	ë	ë	Ő	ë	Ű		ë	ë	ë	ë	ê	Ő	ê	ë	•	Ő	Ő	Ő		Ő		2	2	-	2	2	2	2	2	2	Ë	ŝ	2	ÿ	2		Ē	2	-	-	-	=	:

1949 . 60**2** - 51.

g . 2 2 • : 2 ٠ • 2 2 5 . 1 2 10 2 : • 9 2 ~

the state of the second

2 4

A STATE AND ADDRESS OF

1000

大学のない、大学のなどのない ちょくみん

MITFTA CASS

AIRPORT ACTIVITY PROFILE FOR STATION CCC

PROFILE SUMMARY

TABLE 3.5 TRAFFIC DATA

a second second second

and the second stands which are a second second

. .

00.68:11:E1 12/10/00

A STATE OF A STATE

ATTIM	CASS	5	INITIAL	STATE			a 		C 0 V	T A	
LINNEL	0151.	PAR/DAY	X101	KPM/DAY	X T01	2	PAK/DAY	\$101	SCAR N	K PW/DAY	XCAR
	5	1086.7	•	561.0		4 53	489.1 449.1 148.4	19.54 19.61	4 4	252.9 232.3 76.7	5.65 6.78 3.55
AA-CCC	675	2276.4	0.59	1227.1	10.72	435 	81.5 919.7 245.5	::: ::::	5.01 10.01 10.01	529.0 511.9 196.2	11.03
12 0- 444	•	785.6	3. 2	462.1	4	8419 	502.5 177.6 63.0	83.94 8.02 8.02 5.45	× • • • •	295.5 104.4 37.1	
444-EE	147	291.4	1.13	43.9	9.38	413 	186.6 69.5 49.3	63.20 20.20	2.10	27.7 8.8 1.2	0.02 0.14 0.14
33-AAA	181	185.8	0.70	39.1	0.25	ಕತ	137.7	74.09	1.53	20.0	
900-444	4	204.8	0.17	80.7		59년 1	107.2 66.3 31.4	52.33 32.36 15.31	4 4 8 	51.7 31.6	5.31
	755	176.8	0.67	5.661	1.17	8 d 	116.6 60.2	65.97 34.03	4.56	88 .1	9.06 1.02
111-444		9°°6	0.34	93.4	0.29	3	90.6	100.00	1.32	33.4	0.98
~~~~	• 58	109.6	0.41	6.13	45.0	특물명 	50 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	84. 84. 84.	0-0 9-7 9-7	29.8 27.0	0.78
AA-KKK	Ŧ	10.9	0.07	<b></b>		19 :	10.9	100.00	0.28		0.40
111-444	330	45.7	0.17	5.1		5 i	<b>5</b> .1	100.00	0.67	19.1	9.4
		112.6	0.43	•		ತತ		12.91	9.53 9.53		
	179	134.5	0.51	24.1	0.21	<b>1</b> 3	101.9	75.76		5.9 5.9	0.41
AA-000		40.0	0.15	12.3	0.11	1	40.9	100.00	<b>4</b> .0	12.3	0.27
44-W	162	70.0	0.26	12.7	0.11	<b>i</b>	70.0	100.6	<b>8</b> .9	12.7	9.28
		1.166	£	\$57.6	4.87	51	207.0 123.3	62.76 37.24	1.1	201.1	10.22
			<b>1</b> .9	<b>34.1</b>	<b>8</b> <b>7</b>	8 4 4 	523.5 429.7 131.6	10.00 10.00 10.00	828	270.0 222.3 66.6	
	153	1310.5	<b>H</b> .4	200.5	1.75	<b>a</b>	1.64	35.78	<b>6</b> .23	1.0	3.

106

1.000

**00/01/31 13111163.00** 

	XCAR 2.55 1.15 2.55			1.1.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4	0.50 2.73 2.79	0.75	1.61	1.53	1.00	e. 32 e. 31	•	12.58	4.79 4.79	
	KPM/DAY 55.0 39.2 34.5	116.1 109.7 32.1 32.5	6 - 6 6 - 6	· · · ·	20.1 21.2 21.2	27.2	39.0	33. ) 16.0		1.1	273.5	562.8 520.5 104.4	• • • • • 5 5 6 7	144. 144. 14. 14. 14. 14. 14. 14. 14. 14
4 0 0	SCAF 3.32 9.85 8.82	4.60	5.5 6.7 6.7 6		0.44 4.70 6.51	1.63	2.4 0.62	1.16	0.72	0.37 0.48	1.47	5.5 2.5 2.5	4 % 4 8 8 % 4 8	8.57 8.52 8.52 8.52 8.52 8.52 8.52 8.52 8.52
	x101 27.42 19.57 17.22	12.94 19.94 19.94	97.03 2.06 9.91	100.00 57.84 28.29	13.25 29.54 29.54 29.54	588	86.82 11.10	100.00 100.00	•	100.00 100.00	100.00	\$3. \$2. *	34.17 36.27 17.38	<b>4</b> 10 10 10 10 10 10 10 10 10 10 10 10 10
	PAX/DAY 359.3 256.5 225.7	8,9,0 8,0,0 8,0,0 8,0 8,0 8,0 8,0 8,0 8,0 8	24.2	105.7	29.4 2.4 4.5 4.5 4.5	4.11	167.3 21.1	78.5	•	1.65	9.161	1043.8 965.7 193.8	438.1 388.1 234.1 222.0	414 410 1940 1981 1981 1980 1980
	- 2355	5342	<b>5</b> 53	<b>a</b> 2a	9 954		5 B 	a 5	-	<b>a</b> a	<b>1</b> 	ಷ 5 ಶ 	132 132	33223
	<b>\$101</b>	2.52		0.51 0.70	0.40	60	0.36	0.29 0.14		0.13 0.12	2.39	10.30	1.71	2.63
STATE	A Par/DAY	200.4	100.5	2 T	8.7	<b>4</b> .4	43.9	33. I 16. 0	4.1	19.4	273.5	1187.6	196.2	300.7
INTTAL	X101	<b>5</b>	<b>9</b>	* *	8.	5		e.30 0.32	0.24	0.12 0.15	0.50		<b>T</b>	5.6
Ĩ	AAU/JAP	••••	220.0	105.7 105.2	365.3	182.6	103.4	76.5 85.7	4.4	1.0	9.161	2203.3	1282.2	140.4
CASS	. 1810	ŝ	ŧ	27	ŝ	ž		55 101	5	414 117	2076	655	3	303
MITTA CI	L Y MAN	8		111- <b>000</b>	Ĩ		3				¥3¥- <b>44</b>	CCC-AAA	- CCC-988	CCC-900

MITTA C	CASS		INITIAL	STATE			*		4 0 U	T A	
CCC-EEE	0151 . 418	PAR/DAY 147.0	x 101 6.55	K	8101 8.58	223	PAK/DAY 124.7 22.4	\$101 84.80 15.20	XCAR X 1.39 0.33	K PEL/DAY 54.6 9.8	XCAR 1.22 0.45
CCC-775	612	67.2	•.33	<b>\$</b> 3.4	0.47	13 	61.6 25.5	70.70 29.30	0.59	37.7 15.6	0.01
569-333	\$12	130.1	9.45	6.7	9	23	107.5 12.6	95.02 10.50	4.20	61.5 7.2	6.32 9.16
CCC-Heat	ż	182.0		65.0	0.57	ಕ 2	150.8 32.0	82.51	2.23	6.13 1.1	2.51
111-333		112.7	. 43	20.7	0.10	5 d	4.14	63.30 36.70	1.04	13.1	0.30
***-333	ž	151.0	0.57	58.3	0.51	2 J	90.0 51.2	<b>86.04</b> 33.92	3.90	8.9 9.9	5.90 0.97
CCC-REK		244.5	0.92	74.1	0.65	ช 	244.5	100.001	3.62	74.1	3.43
111-333	236	74.2	0.28	17.5	0.15	3	74.2	180.00	1.06	17.5	0.51
-333	Ī	41.7	0.16	21.2	0.19	đ	41.7	180.00	0.47	21.2	0.47
CCC-1111	104	34.3	0.13	24.2	0.21	<b>ď</b>	34.3	100.00	0.38	24.2	0.54
CCC-000	j	19.6	0.07	10.7	6.93	1	19.6	100.00	0.22	10.7	0.24
664-300		38.3	0.14	14.6	0.13	1	5. 90 1	100.00	0.43	14.6	0.33
VVV-000	:	705.4	3.%	461 . B	4.94	5345	349.0 200.7 159.9	122.	4 4 6 - 6 - 6 - 4	20.01 20.01 20.01	5.99 5.46 9.73
	n í		3.06	286.7	2.50	5541 	348.0 245.1 245.1	42.60 42.50 11.41	5.95	122.1 121.0 32.7	9.0 9.0 9.0
	393	1320.5	8	266.7	2.33	: 425	232	8 <b>7</b> 8	222	242	
	1	1	;	1		51 1					
<b>.</b> -	7					i			17	1.1	
11-000	Ī	81.8	•	¥.		<b>a</b>	51.6	100.00			
	747	44.1	0.17	33.6	0.23	2	4.4	100.00	1.72	33.0	9 5
	I	1.0.9	•	<b>6</b> 5.1	0.51	925 "	57.4 20.6	<b>*</b> ?7 775			

00/01/31 1311160.00

80/01/31 13111163.00

1412

ALL CONTRACTOR OF THE CONTRACTOR ... FO SHE

MITTA C	CABG	=	INITIAL	STATE			-		0 V 0 V	4 4	
111-000	0151 . 235	743/104 76.9	X107 0.37	K PW/DAY 33.8	\$101 9.20	2355 	PAK/DAY 50.3 29.0 17.6	x101 51.90 29.90 18.20	жсан 9.74 ж 1.27	KPW/DAY 11.8 8.8 4.1	KCAR 0.55 1.00
	593	50.3	0.1	29.4	0.26	ភ្ល :-	33.2	66.00 33.92	0.4 4 1 4	19.4	0.90 1.03
AU1-060	178	1.96.0	0.70	33.4	0.29	5 	105.8 80.8	56.70 43.30	1.57 5.84	14.9 14.9	9.40
111-088	370	29.9	E. 0	1.11	0.10	8 i	16.0 13.9	53.40 46.52	0.23	9 N 9 N	0.17 1.24
	i	18.9	0.01	8 6	0.06		18.9	100.00	0.21	8. <b>6</b>	0.21
<b>₽</b> ,	132		0.01	13.5	0.12	ತ 	12.7	67.94 32.06	0.19 0.07	9.4 1.7	0.43
000-008	679	•	0.02	9.9	0.03	1	4.9	100.00	0.05	3.3	0.07
	474	13.3	0.05	6.9	9.06	1	13.3	100.00	0.15	0.J	0.14
VVV-333	147	318.6	1.20	46.8	0.41	<b>4</b> 533 	192.5 67.6 58.5	2: 21 12: 22	2	800 90 90 90	0.63 0.79 0.79
111- <b>141</b>	455	233.0	<b>9.8</b>	106.4	0.63	555 	213.2 16.5	1.15	2.19 9.19 9.08	87.0 7.5 1.0	2.17
LEE-CCC	964	139.0	0.52	60.9	0.53	ਛ ਤ 	126.8			9.9 9.9	1.24
££1-000	453	96.8	6.33	39.3	9.34	27 	46.1	53.13 46.87	0.51	20.9 18.4	0.47 4.43
886-FFF	296	39.9		<b>.</b> .7	0.0E	1	29.9	100.00	0.33	8.7	0.19
CEE-1000	711	11.2	0.0	7.9	0.07	1	11.2	100.00	0.12	1.0	0.18
111-333	256	78.7	0.30	20.1	0.18	. WT	78.7	100.00	<b>2</b> .5	20.1	1.11
885-AAA	151	177.0	0.67	28.9	0.23	<b>1</b> 3	163.2	91.74	1.82 0.22	24.6	0.55 0.10
111-900	55	122.9	9.4	61.9	ô.59	<b>a</b> 3 	9.4 39.6	<b>69.63</b> 30 <b>.9</b> 7	0.95 0.56	48.4 21.0	1.05 0.97
11-000	612	109.9	÷.	8	0.58	ੱ ਹੋ 	<b>86</b> .2 12.6	<b>80</b> .40	1.07 0.19	50.9 7.7	1.32 0.36
111-000	3	36.3	0.14	25.3	0.22		36.3	100.00	0.40	25.3	0.57
JJJ-644	290	32.5	0.12	9.4	0.0		32.5	100.00	9.36		0.21
777-222	128	•	2.4	5.3	0.05	10	•••	100.00	0.15		0.24

-----

----

..

A STATES THE

109

J+170413

ATTA I	CASG	-	INITIAL	\$7ATE			-		0 V 0	4 F	
		PAL/DAV 199.9	5101 9.74	K M/DAY	5101 9.82	2233 -	PAK/DAY 107.1 50.4 28.3	2382 2382	40.54 10.54 10.54	KPM/DAY 51.6 29.1 29.1 13.6	
	1	194.7	6.73	8.8	0.74	2 <b>1</b>	119.7 75.1	61.45 38.55	<b>3 .</b>	51.8 32.6	8.34 0.73
	<b>612</b>	132.2		4. E	9.95	2 J 	120.7	÷	4.73	5.0	7.10
	141	4.14		35.0	16.9	2 J 	37.3	77.00	₽ # - •	27.0	2.96
111-200	J	14.1	<b>9</b> .0	7.7	0.07	<b>.</b>	14.1	100.00	0.16	7.7	0.17
	i	4.2	<b></b> 2	2.1	0.02	2	4.2	100.00	0.16	. 2.1	0.22
	ž	22.7	0.0	8.7	0.05	2	22.7	100.00	0.89	5.7	0.59
	785	186.4	0.03	125.6	1.10	음 글 ··	5.3 1.1	51.28 48.72		7.5 5	6.63 1.37
	289	236.9		4.19	0.54	통 역 복 	139.2 77.5 20.2	58.75 32.73 8.51	5.4. 1.1. 2.2. 2.2. 2.2.	20.1	- 8- 0 - 8- 0 - 8- 0
	0 <b>96</b>	199.3	0.75		0.63	ತ <b>೯ ಕ</b>	160.2 26.7 4.4	11.37 13.40 2.23	2 - 0 4 - 0 5 - 0 5 - 0	9 <b>•</b> •	0.0 0.0 0.0 0.0
000-100	3	131.3	0.50	72.0	<b>.</b>	 	9.99 9.99 9.09 9.09	51.51 35.70 12.21 0.58		37.1 25.7 0.4	
202-100	505	5.5	0.02	2.0	0.02	2	S.5	100.00	0.21	2.8	0.29
	360	17.1	•.6	•••	0.04	2	17.1	100.00	0.67	•••	0.46
AAA-111	ŝ		0.37	36.5	0.32	5	98.9	100.00	1.45	3 <b>8</b> .8	1.07
	11	1.1.1	s	44.4	0.33	3 d 	106.7 75.2	5.5 5.1	<b>8</b>	 	
111-660		83.6	e. 35	17.2	0.15	2 Q 	82.8 10.8	<b>86</b> .45	1.21	 2.0	;;
	225	106.4	*	35.1	0.22	992 	42.0 24.6 29.0	40.13 22.73 27.16		••••	::I ::-
111-466		17.8	0. <u>7</u>	19.6	0.17	18 1	77.5	100.00	8.9	19.0	4.77
MP-111	430	13.0	0.05	<b>9.9</b>	0.05	ъ	13.0	100.00			0.27
	ŝ	101.0		<b>9</b> .7 <b>8</b>	•	21 	<b>5</b> 3.7 40.7	52.07 30.92		8.9 8.1	85

00/01/31 13:11:83.00

AND A ADDRESS AND ADDRESS ADDR

60/01/31 1311189.00

a state of the second se

817774 CA55	CASS	ă	INITIAL STATE	STATE			*		C D A T	4 1	
mme t	DIST.	PAK/DAY	<b>X</b> 101	K PM/DAY	X101	ខដ	PAK/DAY 7.6	X107 7.41	XCAN X 0.11	KPM/DAY 4.2	XCAR 0.20
	533	175.4	<b>.</b> .	40.4	9. 36	5 <b>2</b> 	140.3 35.1	79.99 20.01	2.00	32.7 8.3	1.51 0.04
W-CC	Ĩ	182.0	0.61	62.5	0.55	3 <b>2</b> 	90.8 71.2	56.05 43.95	1.34	35.0 27.5	1.62 2.83
000-111	5	45.7	9.17	26.7	0.23	ನ 2 	31.6	69.11 30 <b>.8</b> 9	0.47	10.5 0.3	0.85 0.85
333-014	5	15.2	0.0	9.9	0.01	1	15.2	100.00	0.17	9.9	0.19
111-111	<b>5</b> 23	11.7	0.04	6.2	9°02	ם פים יי	6.9 7.0	58.53 41.47	0.0 0.0	3.6	0.08 0.12
908-MF	251	22.3	0. O	9.9 2	0.05	5	22.3	100.00	0.67	5.6	0.58
	260	12.7	0.05	3.3	0.03	2		12.7 100.00	0.50	3.3	46.0
111-111	430	9.0	0.02	2.1	0.02	נ יי	5.0	100.00	0.07	2.1	0.10
NKH-AAA	Į.	12.2	0.05	5.6	0.05	ฮ 	12.2	100.00	0.18	5.6	0.26
Null-900	422	78.2	0.29	33.6	0.29	<b>5</b> 	78.2	100.00	1.16	33.0	1.53
NMM-CCC	303	214.2	0.81	64.9	0.57	ך 	214.2	100.00	3.17	64.9	3.00
000-VW	179	195.6	0.74	35.0	. 16.0	31 	145.9	74.59 25.41	2.16 3.59	26.1 8.9	1.21 2.14
111-444	330	49.7	0.1	16.4	0.14	8	49.7	49.7 100.00	0.73	16.4	0.48
111-111	187	97.9	0.37	18.3	0.16	3	97.9	100.00	64.1	18.3	0.53
111-666	236	76.7	0.29	18.1	0.16	5	76.7	100.001	1.12	10.1	0.53
000-111	370	30.9	0.12	11.4	0.10	51	16.7	54.07 45.93	0.24	6.9 9.7	0.18 1.26
		112.5	0.42	16.8	0.15	3	112.5	100.00	1.25	16.8	0.37
Ī	958	47.7	0.18	25.3	0.22	đ	47.7	100.00	0.53	25.3	0.56
202	2	9.05	0.19	25.7	0.22	<b>ಷ</b> ಕ	33.7	<b>66.57</b> 33.43	e.3 6.25	17.1	0.38 0.40
00	101	21.0	0.0	10.6	0.09	: 81	21.0	100.00	0.23	10.6	0.24
	179	147.8	9.56	26.4	0.23	<b>ಷ</b> ನ 	112.8 34.5	76.60 23.40	1.26	20.2 6.3	0.45
999-499	5	6.2	0.26	47.4	4.0	ತ <b>ಕ</b>	53.5 14.7	78.47 21.53	0.78	37.2 10.2	1.72 0.23
	704	45.2	0.17	9. IC	0.20		45.2	100.00	0.50	91.16	0.71

KCAR 0.21 0.29 0.23 96.0 0.28 9.36 0.41 0.09 10.42 4.72 12.0 10.2 15.3 12.4 5048 8 PM/DAY 15.9 18.4 356.8 211.3 4.2 TRAFFIC DATA 1.13 0.32 0.76 4.48 0.26 0.53 0.54 0.10 1.69 3101 10 PAK/DAY \$101 0.08 : 81 13.1 100.00 211.9 56.33 151.4 41.67 42.7 100.00 68.1 100.00 23.4 100.00 28.4 100.00 47.2 100.00 48.5 100,00 101.7 100.00 0.01 0.00 5.34 : GR 0.11 : BL 0.09 : 81 0.13 : BL 0.11 : BL 0.14 : 61 0.16 : BL 0.04 1 BL 1.85 : BL 12.4 15.9 211.3 12.8 10.2 15.3 1.4 101 KPM/DAY 611.7 4.2 INETIAL STATE ... 0.16 0.11 0.10 0.03 0.0 0.26 0.10 1.37 28.4 47.2 1.1.1 MARKET DIST. PAR/DAY 42.7 ..... 2.686 4.65 10.5 : 300 3070 į 900 3 102 50 Ř 74 BITFTA CASS DOD-AAA PP-AAA 222-444 000-644 000-VII AAA-AAA

## 00/01/31 13:11:23.00

INITIAL STATE T R A F F I C D A T A 340/01/31 13:11:63.60 1D PAX/DAY NPW/DAY 6L 6973.0 4473.7 6L 6973.0 4473.7 6L 6973.0 4473.7 6R 2556.2 977.2 PT 1384.0 416.1 25512.4 11445.4

いたい、大学のないので

**BITFTA CASS** 



and a start of the start

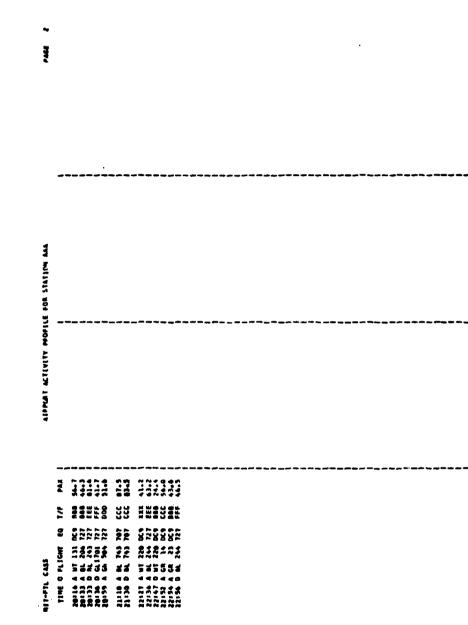
A.1. 36

Contraction of the

114

-																																																						
PACE	<b>P</b> AE	43.9	71.0	53.1						11.3	53.7											2.13		14-1	<b>6</b> 5.0	1-11		~~~			;;				101.1	55	1	25.0									-		1.12					
	11	XXX	1					XXX	F.	ÿ	111	2	CCC	000				15		į	Į	22		30	8	8	5						12	3	5	i	1	FFF				;;			Ĩ	111	EEE		5	3	8		i	
	2	121	ŝ	121	121	101		121	ŝ	727	50	127	101	121		5	111		121	727	121	121		727	ŝ	727	121	101	121	2				ŝ	707	707	727	727		2			101	121	121	121	è		ŝ	727	22	121	121	
	3	505	27	273	õ	242													13					102	2	3	ĩ	Ē	\$ ;	ŝ	Ē		1	1	11	154	218	*12			::	-		è	5	282	3		i	ã		Ê	ē	1
	Ξ	3	5	5	5	95	1	3	ï	3	85 A	1	1	3	1	5		3	i	8	202	5		ತ ೧	5	ತ	5				2			53		500	30	1		1	ಷ ೧	5		3	đ	1	5		ತ	3	3	5 i	3	i
	a l	1 1 1	16155	22	2	20.		8	201	ŝ	111	-	-				9	2	2	143	20	1 55		202	8	5	5		2		2				1	2	121													å				
	=-	<u>ة</u>	2		Ĩ	2	-	Ē	2	11	5	1	1	1					-		1 17	1	_	=	1	2		<u> </u>								1	-	-	_		-				-	1	1	-	202	1 202		2:	2-	;
	A.K.	~	31.1	9	•	9	~	•	•	9	1	3	5		4							-		•••	;	•	ţ		-	~	•					2	5.2	-		-	•	-		•				~~~		52.8	•	7	:	
	•																						8										-																					
	1/1	-	000		-	-			-														50							-				33				-	-		-		-							999				
¥	8		121	_		-		-											-		-	_	707		-	-			۰.					000						-										500				ľ
8	THELT		505	-	-				-		÷							• 6					1 712	-										1103	۰÷.			-									-	Ā		HT 420	-			
STAT!	50	3	A C	1	0	4	3	3	S O	2	4	9		i F	-	• =	• •	•	10	-	0	4	A BL	۲	<	4	<		ō (	6	•	• •	2 0		. 0	•	0	-	۹.	•	•	•		• •		-	0	٥	«	• •	•	<b>«</b> I	0	•
FOR STATION	11 MC		22 12																				4139						8	10161						51 32	5145	5+15	5:53	5157	51 58									14: 35				
113004			_	-	-	_	-	_	-	-	-	-	-		-				-	-	-	-	-	-	-	_	-			_						-	-	-	_	-				-		-	_	-	-	_	-		-	
č	PAK.	.3.2		20-1	*!.*	÷-2+	36.3		4.0¥	56.0	39.3	77.0	47.0						62.1	1		46.9	50.8	11.2	4-96	61.9	71.0	6. et	1.0	22.5						65.3	78.5	66.0	39.7	57.2				00-1	69.5	29.7	68.2	45.4	36.5			13° 8	3	
ACTIVITY	1/1	683	ដ្ឋ		S		1		õ			5			15					000		~~~	000	MNN	33	8	u u	2	Ξ	Ξ	Ī		33	, u , u , u		898	3	3	1				38		ľ	FFF	CC	848	300			ບູ່	-	
	2	51	2	N	S	2	5		ŝ	5	23	12	5						22	1			707													121	101	127	ç,			51				2	ē	121	121		21	121	27	
110-11	E		=		_		-		-	_									202				-	-		· .											722 1		-	_									-			22		ľ
Ĩ	FLE	-	5			۰.				-	-						-		53			0	2													1	1	3	5	5	3	5	5	3		3	1	3	3		1	5	3	1
	¥	24 4	9125 0	22 0	₹ 3	2	•		8	000	8											000	1:06 4	4 80	12 0	210	27 A	28.0		: > به	÷.					010	2:11 0	15	ŝ	0	<b>8</b> -						\$	57 0	5		8	:	3	
	=	ē	õ	ě -	÷	ē _	ž	_	õ	ē	ā	ē	9	İ					Ì	101	; 	1	11	Ī	Ē		Ē	=								123	12	1121	2	2	2				1	2		2	1	-	-	2	Ĩ	
	2	•	-	•	•	•	1.1	~		•	-												•	ŗ	7	2		•	•		ņ		•				•	2	•	•		ļ		•		4		ŗ	•		•		Ģ	1
	•	-		-		•		-															76.5																-										•					
	1/1	XXX					ÿ															-	50		-	-		<u> </u>	-	_							-	-	-	-					-				-				-	
	5	707					127	-				-											127							•••				1		_		•-			• •						•					8	-	
22	FLICHT	2					102 4	-										- 2	<u>ا</u>				50 FO		ā					-						۰.								1.7					۰.					
3	2	4		3 4	30	3	3 0	3 4		ē	3			i 3	•		•	•	• •	•	-	-	0	0	٥	ā		0	0	0	-	•	•	52	1 0	0	•	0	0		•		• •		-		•	•	o	4	•	•	0	
Ľ.	-						÷ 19															-		-	-	-													2														1	

1. 10 B. 1. 1. 1. 1.



0000 * 0000 * 0000 * 0000 ~ 0000 ~	~ Jeesa	•	10 11 12 13										
<pre>v 3000 </pre>	~ _****	9] ; • ;	12										
				11 15	9	2	19	2	21	22	23	101	
	~ @ N -4	• • 	11 15 17	24	2	5.	<u>e</u> r	30	~ ~	4 N		22 70	
	~~	~~(	~~~ ~~~	m e -	 -	- • •	-	n c a ~ -	000	a ~ c	a o a	~ <b>-</b> -	
		30 3-	- N		•••	~ ~			• •	• ~	• •	2	
DEPARTURES AGAI	AREVALS ENPLI	ENPLANEMENTS	DE PLANENENTS		AV E	AV ENP/DEP		Å	AV DEP/ARA	Ę	4	AV PAR/OP	
5		3101.3	1-5/16		12.5	12.5			2-21	~		12.2	
	11	1.121.1	1451-0									• • • •	
	•	206-8	195.3			51.7						50.3	
10	9	432.9	1.664			• • • •			;	•		45.8	
1		116	FILES USED!										
	FILE	LAST MODIFIED	F1E0	LA:	LAST USED	9			INS	UNI VEN SE		LAST MODIFIED	
UNIVERSE FILE:									FA	F AA_0001		00-01110 14170/00	
	6LUE-01	11/20/09	80/02/11 10:02:47.00	_	00.15:63:63 11/20/00	2162	.16.6	88	FAA	FAA_0001		00/01/10 14:14:37.00 00/01/14 14:14:37.00	
	CREEN-01	11/20/09	17:04:27-00		0/02/11		231231516	88	FA	1000		00.74141141 01/10/01	
	RED-01 WHITE-01	80/02/11 80/02/11	80/02/11 16:13:31.00 80/02/11 16:34:08.00		60/02/11 60/02/11		2312313131.00 23123121.00	88		FAA_0001 FAA_0001		0/01/18  +11+1913-90	ĬŤ

166	2							14.2	;;		\$ 3.24	41.2		33.4	4-26	24.8	53.4	1																																		
•	1/1				32								_	Ĩ																																						
	g		2:			-		23	15	22	ĉ	5	20	121		5	÷				;				1						• •																					
	Ę		22								_	_		1218						2.20											,																					
	FLIGHT		20		•									3						í a																																
	•		••					0 0	•	*	4	4	9		• •		~	4	) () ) ()		:																														÷	
	TI ME		201 26		2014			2111	21.2	2112	21:2	2113	21:4	21143	5112	6112	2																																			
							• •••		•			-				-							-		-		-	_	-						• ••		-		-	-		-	-		-					-	-	-
	PAX	1.10	***			C.1					10.	78.1	24	14-2	2		1.29				1	63.6	6	20.2			8	65.5	51-2	ź	÷.	2				51-2	\$				-15		1.04	::		-				1		Ī
	11	80	¥ e	82	•	-	I		I	A A	5	Y	ŝ	1. 444	5	-		5		:6	44		I AA	3	õ		ŝ	Š	ł	9	3	5			ŝ	I	3	:	25	39	3	ŧ	ដ	ដ្ឋ		33	23	13	3	4	3	Ţ
	2	_	121		-		-		_		-			101	-		5													-		2;		_	-	-	-						-	-	-				121		-	
I																																ŝ									_								200	_	_	
ð	FL IGHT	106 V	ಷ : ವ :	Ì		A AC	8		80	ية. لة		2112	5 1	10		-	2001 10	4 : 9		100		18 20	ב ד	3	≂ ≍							5;				•		1			Š	5	217	≈ ≓	х 5		- ; ::		~ 10		s	⊼ ⊒
STAI	•	۵	0 0		r	a	0	0	0	0	0	۲	•	•	•		• •	• •	-	r e	-	•	0	o	a		•	•	9	•	•	-	= c	•	• •	-	۲		•	<	0	۲	۲	0	•	•	9 9	• •	•	•	۲	٥
10	35-11	5143	3			100	0	41.00	119	6123	10	6:3	1	5							7126	71.37	71.3	7:51	122		8.0			2	2	10:24			5		113			į		116	Ē	3	2						1516	6.6
3							-	-			-	-	-	-	-	-	-			-		2	-	-	-	-		_	_	_	-					-	-	-			-	-	-	_	-		-			-	-	-
PRIMEILE FOR STATION	P.A.K	67.6	9.9.						36.5	15.4	31.0	50.0	42.9	53.4	•••		2					37.0	17.9	20.0	24.44		£8. 7	, . ,	18.9	ę.,	35.0			9			52.1	0.2			1.64	11.6	• *						2		:	11
VI TY	1/F								۱.					80						٤.											1						2												12			
ACTIVITY	50 1	-	227											2 2										_				-			1				-		50												121	-		_
1 RPORT		•	272 72						_				-	801.72	_													_		-	-	-		_			-				_		_		-				100	•	-	•
AIR	FLIGHT		2						8	2	Ň	2	Ξ	8 5	: ب			5.					<u>ب</u> ر ا	*	2		2	8	2		2	#00045		-	~		10011		23							-			אי 5			-
	٠	•	0		•		•		٥	0	<	4	٠	۵,	•	0	<b>~</b> (	> <	1 6		•	9	. 4	4	a		9	<		a	<	• •	• •	. e	. a		<	<u>.</u>	-		•	٥	4		<	• •	•	• •	. 4	•	-	۹
	11.	1129	11.17				1.58		2100	2.0	2116	112	2:18	2110	212	01.12	2				1	2:45	5	2135	2:34		22		3:28	2							\$1.22	:			112	2014			5				202	1.5	5130	2:40
				-			-	-		_	_	_	_	-	2.		_	-			-	-	_	_	-		_	-	_	-	_				-	_	<b>-</b>	_			_	2	_	_	_					-	-	-
	2						1.4				•••	1	1.7	90.7				•				8.4		;;	2.2	2	•								1	-				1	-	2		7	•				1.1		4.0	ł
		4					-		£.					5														-									1									•				3		
	11								-					-	-	-								-		-		-		-	Ξ,							-			_	-		-	-				-		-	-
	2	ŝ		2	-		_					-		2			-			ŝ												8													-				-	127		-
z	FLIGHT	1 224	į			2	1	1	ģ	2	236	8	100	91 753	2	001				-												Ĩ				-														162		
CASS	1.0	A 41		52	10	5	0	1	11	10	ē	ี ส			5 4	3 0	2	-				5 *	30	1 0	5 4	35 0	3 -	3 4		3	3) a (		50	50		3		ថ ត			4	4	ã 0	3	2	<b>8</b> 8	3 4 > 4	5		3	0	ø
	Ĩ	-	-				8		8	-	100	Ĩ	135	7	5		ŝ	8	1			•23	2			÷	5	• 5 •		• • •	2	0716				150					127		Ĩ	1		Ĩ			ŝ	11112	:	11
Ŧ	Ξ.	-	1			•	-			-	-			1	~ '	-	~				•	•	•	•	•	•	-			•	•	* (	* *	• •	-	•	, [.]	2	2	: 3	-	2	2	2		2:	::	2	Ξ	1	Ξ	1
· _			1	·,					1		_	: ••		ì			17	_		) 									-*-							-							_		•-		-					-

ALAPOAT ACTIVITY PASFILE FOR STATION AND

~

PAGE

**
-2
-
-
2
7
÷.,
2

101	<u>5</u> \$\$\$22	AV PAK/DP	
2			i
22		Ĩ	1
12	9~~~~ <b>o</b>	2	
20	*****	AV DEP/ARR	1
1	*****	•	ĺ
2	24-440	٠	
16 17 18	3~~~~	AV ENP/DEP	
1	2*****	2	
5	5-++	-	
1	ent0	33	
=	3*~	DEPLANENSW75	
12	3N+~-~	EPLA	122**
=	=====	ā	
2	~~~~	LIS .	
٠	*****	NEMEN	1.44.1
•	20040-	ENPL ANENENTS	32375
۴		Ű	
٠	~~~~	3	
•		ARTIVALS	N#\$**
٠		3	
*		_	
~	*****	ž	~~~~
-		DEPARTURES	~~~
•		ō	

## PROFILE SUMMARY

101445: R E

•••	DEPARTURE	****		142:		
525	CARAIER	43525	***	universe file:	R UR COLO CAREN NED NED	
UL J		•	2		42252	
			<b>U3EA</b>			

119

00/01/10 1411457.00 00/01/10 1411457.00 00/01/10 1413457.00 00/01/10 1413457.00 00/01/10 1413457.00

00-16162162 11/20/08 00-16162172 11/20/08 00-16162152 11/20/08 00-16162162 11/20/08

86/92/11 11:19:197:47.90 80/92/11 21:54:12 80/92/11 11:24:00 80/92/11 11:13:12.00 80/92/11 11:13:90

M. UE-01 COL D-01 CAEEN-01 AFD-01 METE-01

- 10 C.

90/01/10 14:14:37.00

UNIVERSE LAST NODIFIED

LAST USED

FILES USED! LAST 40D(F1ED

•

FILE

1111	CASS								ALAP	140 141	ALAPORT ACTIVITY	Y MOFILE FOR STATION CCC	Le T	5	TAT	5	2							-	Yet
¥I.	0 FLIGHT	en	8	1/1	14		3 W 1 I	0	FL IGHT	5	1/1	PAK		1 I NE	5	0 FLIGHT	8	1/1	PAK	1 TIME	۰	FLIGHT	5	1/1	<b>P</b>
	5:	3	121	W	59.0	_	10:51	0	GR 52	500 7	999	4.64	5	15:10	20 i	E\$000			14.9	1910	•		-		4.5.1
2614			Z				6010	9		_	-	6.50			ة د 0 د	7 2 Z	52		103.7	1 191 10	< <	33			
82	20	121	2		4.99		11:02	< (	11 300	5	888	a•++	5:	2	20 20	123		AAA	3.8	1 19:21	9	-			1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-
85	32	5	22			-		•			-			121		212 1				X 141.	•		_		
	; 2 2	2	ŝ				ĩ	• •	5				2	2	< 6 > <	502 J					• •				
1	3	2	8		74.7	_	1:22	٥			-	1.1	5	16.5	تن ۲	22	_	Ξ	45+2	1 19:44	<				0.0
		8	5				1:27	•				8°6		ġ	ن ق • ◄	202		AAA	2.0	5 26 1	۵		-	-	37.5
	3		ŝŝ					< c							ن و • •		_			1 20101		1000			74.4
5514	5	Ī	2		10.9		1	. «		-		20.4			÷ e	22			90.90	20:02	1 4				
	i		-			-	1154	۲		_		17.9		151	3	2	_		0.14	1 2010	4	≂ *			
			èè				2100	6				19.4		161	3 0		_	K K K	12.4	20115					4-16
	50		Š	996	67.1	-	2003	•				,	*	201	٥			AAA	1	2012	•	12			
90 20	1 0		ŝ	***	42.1	2	2107	۰				40.7	1	1 30	-			FFF	9	1 20121	•	3 			51.7
~	3		ŝ	¥ 4 6	66.J		12:13	••	:: ::	202		6		16130	50	69 a	22	444		2013	•	2			
	;;														r 4						3 0				
			28				2132	•			, ⁻	1 + 2	-	2	0				105.4	102	50	י <u>ב</u> נש			54.7
	802		ŝ		75.1	-	2144	٥				8	-							1 20131	۵	000			
0.50	0 66.5		ž		48.8								-	3	0	9 8		AAA	15.0	2012	۲	¥			•1.•
5	5		ŝź	H				••	00170					101	•	1 22		555	59.0						
	1		ŝ	222	ì			• •	19				-		• •	, .					9 4			-	
9187	A 100		127	H	24.3		1.1	3 <					-		• ۱	1 212		000	1	2114	•				
1114	5 ₹		727	***	1.17	1	31.25	۲	GA 20			62.1	1	11 26	0	L 602		AAA	11.4	1 21152	٥	1 2	224 727	EEE	5
	133 8		ŝ	X X X X		_		0	100			25	-	11 28	-	80.33		500	1	2115	-			-	•
			121					0 4	2001			1.1			• •			33							
			101				2	t 4							• 0	Š					• •	13			
	10		121		1.5.1	-	****	a	N III				-	-	-			VVV	13.	1 22121	•	-	-		1.15
- 02 F	004 0	_	ŝ	848	• 3. 3	_	9100	۲	12002			4-95	2	1	-	41700		688	110.5	1 2212	◄			-	110.2
	5		22		11-0			۰ ۰	2			1.1		2	c (	0.00		000	103.5						
			ÌÈ					• •	- 13 - 13 - 13					11:52	3 4		202			20162		: Z 5 =			
	3		121	1	5.4			1					-	1 52	-	11103									
5634	1	_	ŝ		1	_	90.7 7	0	N. 71.			÷-0	2	15	0	828			53.0	-					
			5			_	8	•				51.5			•										
	52		ŝ				*	•							• 0										
5	5		ŝ		67.8	-	4114	•	1 11		-		-	101	٠	T LDI		000							
10412	5		ŝ		2.5	_		۲	16. 79			79-2	-	2	•	512 J		848	4.8	_					
	3		121				1214	• •	800			61.7		21	0				103-3						
								۰.	•; 5:						• •			į	, , ,						
	5.							• •							3 0				2						
	1		121		7		7	•	12				-	2	•	000 52		ŧ							
10:20			22		28.4	_		•	9) 3)			4.64	=	1.29	٥	11701			4-26						
	53		20					•	2 ° 3 1		-				< <	5 - 									
	5	(j 5	121	8			14159	•	12	5				1111	0	AD0052	22	ĮĮ	Ŕ						
3	2		5		<b>6.</b> 0	_							-	121	•	22		¥							
	2 2 0		121					•	9 3	1 727	8	•••		2	•	2		KAK	72.4						
	5					-		•	1 5000		-	54.00	-							_					

and the second of the second second second second second second second second second second second second second

A STATE

#11-61L CASS	C ASS						۹.	LAPOR	Г. Н	INI	Ē	110	ALANGAT ACTIVITY PROFILE FOR STATICH CCC	STA	5	ÿ								ž	
											PROFILE	2	PROFILE SUMMARY	<b>2</b> 1											
:		-	-	N	•		•		•	•	2	=	12	2	1	11 11	-		:	5	12	22	2	101	
	TOTALS: el	3	••	••	••	••	••	~~	21	3"	:*	2~	• *	5-			27	37	<b>P</b> N	<b>a</b> ~	<b>W N</b>	**	~-	Ë:	
L	4 <b>25</b> 2	-,	••••	••••	••••	••••			• • • • • • •	* 10 -				****	***	****			4-100	N###				332X	
÷	CMAIEA	1	7430	DEPARTURES	x	AAA	ARRIVALS.		ENPLANENENTS	WENE	MTS	ð	GEPLANEMENTS	ENENI	2	A	AV ENP/DEP	96		AV D	AV DEP/ARK	z	4	AV PAK/OP	
	1238			223			22		122			Ē.	23	1.12	ľ										
	125						212		•				238	201.										1	
:	ł	•		ļ	1	1					E	FILES USED:	101		:									÷	
	2	¥					-	FILE		LAST	8	LAST MODIFIED	~		3	LAST USED	560				Ĭ	UNIT VEA SE		LAST MODIFIED	
1		WUYERSE FILE	1971	ł				:			ļ		:								FIN. MIL	Ĩ	ž	M-101111 111111	
	13825	. 2 4			,			AL UE-01 COLO-01 CREEF-01 AED-01 AED-01 AED-01	ŦŦĨŦĨ		11/20/00 11/20/00 11/20/00 11/20/00		19.09.191.191 11.191.121.00 11.191.121.00 11.191.121.00 11.191.111 10.101.00	****		10/02/11 10/02/11 10/02/11 10/02/11			*****			ÍÍÍÍÍ			11119

<b>NU</b> In 727 444 MUU In 727 MON 444 In 727 MON 444 Pr 727 MON 444 Pr 727 444 CCC																	
			6 1 0	ł				1 GPFC					1.550.				
<u>.</u>	000 11	• ••	11/ 7/7	27 64		000 000		÷	Ľ		VVV		1 00	õ	NN	948 CCC	J
12222		-1.			1000				뉩	1.1	NAW 944 112 240		1 2635	a	3	CI CCC PPA MM	
222	0 844	• •						53					1 99 1	- 1	HHH		Ŧ
22	A. CCC 444		12/1	50	0 000				ŝ					Ξ.			2 4
22	10 FEC 444	-	1 14	37 6	1 1 1	LFE NA		13	12	100				1			
	11 F(C 141	•	20.2	- 2 MM				102		100				- 2		3	7
121	CC RHR CCC	-	101 7	20	-	444 12		10	1.2					5 ¢			
127	C BAS CCC	-	0 11,	5	C RAA	AAR AAA		102 1	2				0/10	12			
1 23	10 100 000	-	33.2 D	3	A	BRR CC	- -	1 202	121		CC AAA		1 0330	ă			
	C PPR CCC		- 00 ·	00 47	0.444			5.2	727		48 DOT 44	H		1			
		-		4	500	000	-	1 204	121		:		-				
22				27 000		1		100	223		00 NAN 00	c	31148 1				
	E AAA FEF	- - 				11		101	1	220	A AA AI						
		• -				000	H		2				-		50		*
		• •							2				-		***	13 22	
1	A FE ARA			00				i					120		3	111 00	
		•			4 000										000		
1.73		-	861 D						2								
-	011. A48 AMA 110		0			000		1			-				P.F.F		AMA BUL
12		000							1				-				
2	-	• •							2							44 44 44 44 44 44 44 44 44 44 44 44 44	A 500 PER
131	14 3 A 100	-		27 7.8				1				1					
127	0 4 4 4 D 0	-	10.00			CC 00											
	PDD ### 200	-	1011 101	1 H H H	300 4	11 11 11	C) (16 + #14 100 CC +44 177 1				222 6						日本市 たりき ノイイ しんしょう かいき ししし メイヤ 人名英
151		-	1007 0	20 20	WET 7	000 44		ł	12	CCC OL	D RAN						
2	A PIR 000	-	0 1011	DC 9 PK	100	Ť L N	-		127	0 200	e		006 1				
2		-	110.0	N-H-H - 5 J	N CC	848 UUQ			127	00L C1	5		01.		1	RAA CC	000
		-	0 (.11	10 RAS	502	5	1 111 184	101	22	14 8 H B	A TRE	•	165 4		ŝ	NHH BA	17
29		-		8 H H	600	ະ		202	12.7	A NU A			00.0			ŝ	
		- -			ŧ		-	104	2		14 eve 44	_	114-1-		000	11.51	1 A1 554
							-	208	22		2		0		999	JJ BUN	7 AAA
									121			*	-				
÷.	TAL TAL	-  -					( ; ;										ļ
		• •							121				-				
				5				_					-				
ł	A A A A A	•  •											-				
		•	42.00				- •						-				
1.01	TAA 744												- ,				
-	Y TAT RA	-	11 11	00 000	0.6.0	000 440 444 555 600	000		- 11				-				
101	2 444 KYZ																
Ĩ	1 144 555	-	52.52		227			100									
Þ	C 144 PCC	F	1.1		233			100			1 5 4 5 4 4 4		-				
	C 444 CCC	-	21 00			111		0000									
	FCC 848 FCC	-	22 00			223	•	1022		566 N.	-						
		-	Ne In		111	CCC LLL		10/0		AL HHM	NNN A						
		-	5		-		-	4200									
8 OI D		-	50 55			010	•	00.00			5 411						
		F	F		- 44	0.0	ſ	1694		ANN De	A GEC						
121		1 999			111	111 001		1012 127		111 66			• •				
2	FUB PAR CC BAR	-	43 DC4		PER CCC BER	11		2046 727			377 448						
1		F						1000		CCC MM	A Heat		-			ļ	
127	*** FCC	-	2 2		Bat LCC	618	-	2045									

100 m

1.2.42.1.1.1.2.42.44

		2 777	Γ-	TT ALENS	T T T T T T T T T T T T T T T T T T T				•	ANAJA O		10 AL PWA		2 444		TO AL PHA		1	
		Ŧ	-	FR CHARLIE	111			222	• •	P FARTH	10	FR FARTHANE FEE 2	555	1 2 1	F. R. J.		F. A.J.C.		
ļ		62			14:01 10:41	72	5							-			N 30.29		1
Ť.		1.1	-	14: 30	17:3-	-		-	• -	12:15 1	12:52	11 222					; ;	204 127 308 DC+	•
Du a			Ľ	1.1.1	1610-	-	*0*	127	-	1 2:00 1	1:11			•	8	34:46	3	1	۲
ML 746		5 6								18:21 1	141.58			•					
F	1	-	ŀ		10.0	1		191		2000							L		
					20:15						CAN	71.44			4 1 0 3				•
æ		127	•	20: 20	70:54		64 122	171	-	4:20		61 700		9	10201				• •
-		181	F	16:14	21:22	Γ	204	-	-		19:00	× 00030	121		11:39	10:02			ŀ
•		23	•	72:13	22:		=		-	1 50:01		AL 245		•	_				•
~1		Ż	-þ						-	12:20 1		101 19	- 1	7	FR. KRAY	1	1		1
						:		2	•	1 00 1		11 440	ŝ	~	;	CAR	Ξ		
_						1	213 001					R10032		•	2:0	0:20 5:57		121	•
	1				-1-6	:		ł	•							12: 11		Ľ	Ĺ
											10 0720	18 To		242		13:37	nt.1707		•
				130 0 0	:					F NOTES									•
	1 546 14	121	-			I.	12.10		-		3	64.49	l				L	Ľ	ł۰
		23	-	7:00	÷			• 10	-		1:10	800020	•10						
		5	-	1:31		10	1	127	-	4.40	1.62	68 801			14:25	14:25 22:02			
	5	21	•	A:00	10:05	2	250	121	-		•: 24	61.011		-	10:36	22:07		1	•
		21		•::•	10:0	-		127	-		17:30	EL 0.02		~	10:96	14:50 22:27	LT 220	5	•
											1717	2100012	1	1					ł
				10:00	11:24								5	•	OATU DI -	041		5	=
	ĩ	23		11:07	13:12	5		1.21		11:17 1	10:30 EL	1102 64	- 4						
	41 1946	12	5	11:20	13:24	[	110	000		19:21 22:14	1 0 V : 2	N 12 331 808 1							
	-	÷	-	1 1: **	14:24	5			-				•		4230				
	10 611701	2	-	14:00	10:51	ŧ		127	5	A 19PLA					1 9214	101.75	1	e 127	• -
			-	99:98		-		5	-			40-24		-	15:4		1	1	-
	230 6:5	ñ T			14:14 15:00 14:44 17:10	3 8	101			9:15 11:32	1:32	HE 89		~ .		\$1 \$	đ	121	•
		נננ	F	16:51	11:34	Γ		127	-	13:50 14:02	20:1	5					Г	T	
			•	19:00	13:00 15:42	ŧ	103	127 (	-					-		11:33	5		•
	tue au	727	-	15:37	15:37 1s:7C		242	777 1	1 5				111		10:02		đ		•
				11:11	96:41 49:55			127	-		CAR	10.94		-	11:32	NG:21 1	5		ŀ
		È			14:42 17:24	: <del>ب</del>	204		-			6L 11 32	ţ	~	11:45		GL 802	-	v
- E	- 6									21:01 20:01	t	111018	- [	•	12:07	1		ł	٩
									•		1			-	12:57	12:97 15:23			•
		127		10:14		1		177		7: 14 1			10 10						•
	F	È	Þ	-	A1:02 41:4	3	F.	111		17:16 27:54 GL1002	2: 24 61	1 00 2 96	179	102			L		ŀ
	-	ţ	1		2				-				ł	-		11.1	12		•
	2	ţ	-	10:40	:•1	ЯL	120 NRH	a l	5	A SLO			K R R		19:33	20:00	2		•
	~ 1 4		-	13:10	12:10 14:37	RL 241	wull 14	522 Ju	-			\$1.95		-	17:21		61 NG		•
	-				,				•	1 21201	12261			 N -	02:97	20144	-		÷
				2433 4 4		l				1 01 : 11	- 1		- 1	+	11:22	50:00	_1		٩
					1				•						50:41	121231	1. 263		•
	11132					1													- 1
	1		ĺ																•
				19.141	• 6 : 5 -	-	l	A 6 78		1 11 1		2				•			ł
		12.1		12:41	17:44 13:24	5 5	1.0	010	Ē	11:11 11:11		16 89	904	•	7 2: 28				••

and the second second second second second second second second second second second second second second second

Section 2010

			-ŀ				-				4		1222221	222222	1222222	:
			• •					5			-	TO CHARLIE			222	-
			-	FP DEI 14		000									ü.	ä
11: 32 21:n9 6	611133 CC	CCC 64 1103	-	10:41 11:	NT 111	ä		41.40	LT 300							1
			1 17:44	441 881 84	6P & C.		1 11:46	12:34	64.11.32							•
THE CHARLIE		- 30 		11: 24 19:04	11240	0 121	1. 46:16 17:02	17:02	611902	1	-	7				
							_				-		•: 27	64 100		•
7:10 0:10				00.17 00.			I FP AILC		,	A K R	-		-	100 801		
7:55 10:11	58 101							5	62.26	-	-	7.00 9	٦	- i	- 1	4
81.14 A.14	15 U S							96.1	61117	2	-	7:30 11	11:02	MI 300		-
8110 8114	611131	0.0		10.01 61		121				10	-	7:54 10	-	1171		•
111 10:15	51 100	127 0	.01 1	10:30 12:53	61,302			17.14 30.00	11201		- 		11:22	101 33	1	
10:00 10:40	BIOLS!	127 0	1 11:	11:11 13:33		6.00				5						<b>.</b>
10:01 0LIV		127 0	1 10:	41:01 UQ.	AL 233	121	0.11									•
10:10 12:54	50 02	127 1	1 1 1	14:11 20:20	AL 224	727	1111								1	ģ
		• • • •	:02 1	14 22:27 H	RL 276	127										•
	51 52	0.0	-	1	NECTIONS		I FR LING									•
1.11 12:14		0.00	=	11:51 15:31 AL 221 AAA	AL 221 A4	1 AL 21	÷	CAR			4- 					
	112 14	727 0	::	19:5	AL 223 CC	C #C 213		11:02		900						• •
	61 101		- 21:14	2:1	41 640 AA	3 MT 440 AAA WT 27C 5		17-04 17:42	68 34	50		11:00 17				
9.1110221		6C9	-			•	1				-		1-			1
24:44 12:35	61 101	127 0		f0#1#0)		5 S	I FR MINE			-						P 4
11:12 15:50	۰.	22	_		78.01			CAN	76.15							<b>.</b>
12:10 12:40	~	127 0	1 0:52	12:4 25	6L &00		4:73	4.52		ors .	-				÷.	• :
1111 121	••	0 5 3 -1	1 131.	13115 15040	61 121		10.0	12:53	61 102							э.
81.91.01.19	68 600	127 1	1 1 1	22.22	AL 274	5 101	-		CT Dev							•
		90 × 30	-				10.1		201 12	ŝ						
	NL 719	127 0	9 <b>1</b> 1	6.15		1995	14:04		11:38 GH 33 AAA	1 64 201	-					•
		6		÷.	44.74	,	-				-					<b>.</b> .
				18 14:30			JAN BAUK BA I	H Jaki			-		1			• •
	6 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	0 4 10	1 22	10 14:32			_	CAN	29.45		- 20				1	• •
				(+ 10; )e	- 1		20:4	10:35	64, 100	127 2				1 115	ā	
		0		118:00		- - -	\$F:9	• 7 : •	68 6J	0.00	2	22:27 0:				1 -
				40:02 14	#000 25	-	1 10: 11	15:34	111 17	* * 20	-		CONNEC	CTLUMS		•
					:		11:25	20:46	FL 207	727 1	-	145 141	38 61	8 C 2 P 8	3	
	~		Í .	הטינו. ביי			_	C ONNE	C IT CAS		-	13:12 17:	27:45 M 222	222 EEE	đ	
10 E E A							80.5	19:11 GL	100 A4A	6 6L A12	-					
					4 4					1		PRAVO			488	-
01:0 01:		r e u					AVAX KJ			• * * *	-		CAR	34.66		
							_	CAR			-	:08 1:		1 312	010	•
- JU	727	8 - 66k				í	0		68 101	177	- -	1:00 7:	1	GR 31	004	0
							2:00	1 5 2 2 3		127 1	-	:00:			ž	•
					1 100 Cin		R: 30	15:24		707 0		1:34 4:22		841000	ŝ	9
		-				ł	9 : 00	14:23		107 1	-	:93		01010	727	U
						1	20:4	10:26		127 1	-	: 30 11:			01.	1
				•==		C 4T 411 1	10:31	17:35		107 0	-	14 92 1		1 210	121	•
					:		11:25	64101		127 1	-	1104 1152		11 500		
								20:46		707 1	-	10: 44:				•
			_	Ę	47.78	-	01:11	27:46		127 1	-	101 101				•
		-	4 7 4		61	00 • 1		9: 4B		004	1	0:14 11:02				• <
	194 1	0 171	-		C. MR.CTJUNS		14:50	1:13	N 220	• • •			ſ			ŀ
			57:01		· 31 CC	[ ER -2 ]										•••
		0 171	-			-	_									• <
LASUE LES	242 14	127				ŗ			******	1	T		ł	•.		1
											-					•
11:10 14:14	11 11	1 + 20	-	5	14.45								-	6L 302	121	

	32523			-			•	•	-		212	1 222			•	•••			-	•	•	1	••		•	••		-			1	~		3	L 263			1		-			-		
E.	12 22			ĥ	ů.	1			Ĩ	3							1					1		: 2	21	2	122	2				00	- 9		-				22					21	- 1
			The second second second second second second second second second second second second second second second s	11 247	61 1007	58.203		RL 261			1 211 55		8.1.8 1	<u>806208</u>			66 92	1	-	61 401	6L 1102	202 20		91.212	50° US			EL 102		44.45	NT 519	ME 120	CONFECT 045	1 302 8	4 224 888 AL 243		*J.15	19	RL 121			44.03 0110	RL 700	AL 201	2121 AM
	22222222	1		14:10 20:14	17:22 10:20	19:01	14:51 19:57	22:57	10112			N IE	5	2	•		10:30 11:26	12:13 13:01	2111 11:11	12:01 65:61	14:32	11:11 11:11	10:59 15:47	11:15	19:50 14:30		10:09 10:52	21:35			15:47	13:30 1.23		1	20:11 23:51 W	TAAT	<b>4</b>	11:01	19:15 17:06	AZ 10 Z		10:15	13:50	10:01 14:12	
	111122	TO DELTA	F A RA	14:20	17:22	12:20	14:91	16:12	22:00			FA CHARLIE		1	5534		10:30	12:13	12:51	11:33	13:44	11:15		15:21	15:50		0:01	20:47	202		11:10	13:30		12:30	11:02	CO KOVTAGE		4102	51:11		FA GUL	J: 10	02:0	10:01	
				-	~	7	-					-	•	7			]-	•	]	-	•	7.			-	• •	-	_		-		0 15		1-			-	7	~ •			• •	-	• •	-
					727	50	•		190			127	727	ä	121	32	50	e Da	121	127	127	5	121	0.1	121		181	121				5	IN 641 002				1.6.1	3	•		14	[2]	14	222	
				240.34	FL 1700	51 112	GR 22					EP 301			101			~								101		EL 102					14138 CTI 100 HUN		14.64		1 31	11000	=======================================			68 402 F8 802		112 12	
~				CAR			64:0							16:01			11:21					1									C ORAE	11.07 WT 011			-						1				1
		TO CHARLIE	FR DRAV		0:02 11	<u> </u>	9:30		VI 10 DI			1 01:4		1 25.4				10:00 17:29	21 4213			11: 1 1:11		5:00 17	11 21:6	14:02 18:24 14:02 18:11	7: 05 20	12 4 5 2	100 21	14:05 22:51		1 3: 12 14	100 10	DAUNE BI				1:30	1 0 1		1 6010	11:14 17:20	1 6 1 1		
	-		: 2	L	-	1	-	::: 					-				_	-	1	-	_	]			-			-						2		_ -		_			-		ľ		-
-			666.2		1 1 1	9 9	11 C	-					•		•	121 L	-	0		1 1 1		0 0	1 666	:	1 + 20		00.0		61119	FRE 1		_		-	•		5 VNN					;;		∼ ₩	
•						-		2			1	Ł		- 1								1					ŧ.																	:	1
				A0. 44	61 101	ena3	61 114	CURRECTIONS				1		- 1			Ł				41.74	1			611000		64.11.32	Cubar CT 10KS	64 10 02		1							11.11			. 20.	32	1	:	
				E	12:40 15:36	17:24	15:14 17:44	5	1757 1951 5 BA 200 644		1		11:54	17:04 14:07		14:00	17:04 19:40	14:24		•	CAF	10:00	111				1	410	11:10 72:00 0F1005 Haw		CAH	1.30	10:10 11:54	12:54	10101			C &	70:11 17:4	5	11:43 10:1. 6. 204 AAA	A1.73 14245 WT		475 3A78	
			Fe Sut		12:40	15:00	15:14					04:9	14:01	12:00			17:04	11:17		F R 1 ND		4:13			15:4		11			11 = -1			1018	1:11	17:14		3914 83				<u> </u>			378 8.4	
			-	6	-	•	~	•				-	•	-	•	 ,	-	•	4 2	•	-		, . , a		•	-		-			-	-		-			-	2		, -			•	~	-
			A PA	F	127	127	630	5				121	•26	2			010		904	90.4	00			127	121	122	121	121	121		• 20	121		Let					127	121		i z		555	
					F. 473		1420		11/00			H 711	5 9	1111				4 3. 5A	68 11	111111	101 10	R00 120		102 02	11 297		101 12	00230		(011.0)	61 701			-		41-14	51 102				للاست و لا است				
15		TO CHAPT JE		Ł		1			1			1		-1					11:45 6			ł					Ł	_	1			[.		-							LUNT				
				1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	14:74 14:40		14:40 30:44	14:11 11:11	4.11 Du: 11			10:14 70:04	:10 20	34:14 11:44			PYJJG PT		7:05 11	•		11:40 11:41	05:01 00:21	17:40 11:10	0521 1221 123 123 123 123 123 123 123 123		69 29 L 96 25 J	14:04 14:54			11:44 19:74			11:10 72:10			11 11 11	11:10 11:11				LT:12 15		F 34 F 8-01	

e f

125

A CALL PROPERTY

With Mark 1         Mind 1         Mind 1           1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1	1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1 <th>TC (Con TC (Con EA MOILL Con 10:41 17:59 wf 110 BC9 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0 0 0 FR 10 0 0 0 0 FR 10 0 0 0 FR 10 0 0 0 FR 10 0 0 0 FR 10 0</th> <th>1 TO FORTROT 855 2000</th>	TC (Con TC (Con EA MOILL Con 10:41 17:59 wf 110 BC9 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 1011 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0.07 1 FR 10 0 0 0 0 FR 10 0 0 0 0 FR 10 0 0 0 FR 10 0 0 0 FR 10 0 0 0 FR 10 0	1 TO FORTROT 855 2000
102 **** 6 102 **** 6 103 **** 6 103 *** 7 103 ***	╸╸ <b>┑</b> ┑╸ <b>╸</b> ╡╸╸╺╎╸╸╸╸╸┑╶╎╸╸╸╸╻╶╎╸┉╺	TC Cond FR MOTEL CAN 00.01 10:41 12:30 41 110 10:0 FR Nols Can 00.07 FR Nols Can 00.	1 TO FORTROT 665 2
101         20           701         20           701         20           701         20           701         20           701         20           701         20           701         20           701         70           701         70           701         70           701         70           701         70           701         70           701         70           701         70           701         70           701         70           701         70           701         70           701         70           701         70           701         70           701         70           701         70           701         70           702         70           702         70           703         70           700         70           700         70           700         70           700         70	╸ᄚᅕᄚᄚᆌᆓᄚᄥᆙᆕᆕᆃᆕᅑᅟᆣᆤᆃᆃᆃᆂᆇᆣᇉᄴᇻ	FA MOLEL CAN 94.91 CAN 94.91 10:11 17:39 WT 110 DC9 FR 1901A CAN 94.97 171 231 231 24 81 941 CC9	
101         103         104           101         104         104           101         104         104           101         104         104           101         104         104           11         104         114           11         104         114           11         104         114           11         104         114           11         104         114           11         104         114           11         104         114           11         104         114	┦ <b>┑┍╺</b> ┥┥┍╺╶┥┑┥┥╸╸╸╻╶╎╴╺╸		11121111111111111111111111111111111111
No.15         No.15           No.15         No.15           No.15         No.15           Stilling         Stilling	• • • • • • • • • • • • • • • • • • •	10:41 17:30 01 100 FR 1011 CA 04.01 111 12:12 12:40 04.01 111 111 111 111 111 111 111	L F& ECMO
Mill         Mill           Tat. Jr         Tat. Jr           Tat. Jr         Tat. Jr           Rit end         Tat. Jr           Rit end         Tat. Jr           Citrat         Litration           Rit end         Tat. Jr           Citrat         Litration           Rit end         Litration           Rit end         Litration           Rit end         Litration           Station         Litration      <	• = = = = = = = = = = = = = = = = = = =	10.11 12.14 11 10 10.1 1.1 10.1 12.14 11 11 12.1 1.1 12.12.12.14 11 11 12.1	1 4:51 31:31 H 22 727 1
Ten.11 11 11 11 11 11 11 11 11 11	·   • • •   • • • • •   • • • • • • •   • • •	C10 01.07 111	275
	• = = = = = = = = = = = = = = = = = = =	CA 44.07 111 22 11 911 559	
(111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2) (111.2		22 11 0 11 02	
CETT (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)			Cta 00.32
C(1)-MC 011 M- C 011 M-			CONTECTUNE
011 011 011 011 011 011 011 011 011 011 011 011			1 6:34 13:39 61 911 998 67 17C
40.00         111           40.00         100           41         100           41         100           41         100           41         100           41         100           41         100           41         100           41         100           41         100           41         100           41         100           41         100           41         100           41         100           41         100           41         100			_
111 <b>6.0</b> <b>6.1</b> <b>110</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>111</b> <b>11</b>		÷	1 FR JULIET
64.47 64.47 64.120 64.120 64.120 64.120 64.120 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.1200 64.12000 64.1200 64.1200 64.12000000000000000000000000000000000	7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10         7.10 <td< td=""><td>2 403 004 V (CT)1 001 1</td><td>1 CAN 74.25</td></td<>	2 403 004 V (CT)1 001 1	1 CAN 74.25
Ra 41 009 W1 120 009 31 770 00 31 770 68 00 11 80 00 00 61 000 00 00 121 121			1 CONNECTORS
11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11           11         11         11		L	17130.12126. 611000 BER. 64. 1.4.
31 CCC 68 -CC 31 CCC 68 -CC 61.000 CC 61.000 CC 800200 127			-
1. 10 1.			1 FA # JLO 444 1
31 CC 68 1. 10 1. 10	1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1	10.10	_
61.000 CC 61.1000 CC 80.0700 22		1 C:57 11:18 61 102 127 0	1 13:10 15:46
61.1000 CC 61.1000 CC 8012712 22	1919 W 1919		
611000 CC 611000 CC 807777 72 805719 72	17:76 MT 420 14:54 MT 420 22:21 ML 140	1 TC ( ) L 10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 10 601 E
6111000 00111000 01111000	14141 141 141 14141 141		
+1610a	22.21		
.16100			1 ** 4LFHA 44 2
			L. 22.53
		11:34 61 120	6L 100
ł	5	11:30 91 221	
	14 114 114 14 Parts 1 11/1 1	It's start	11 211
ă			61 111
			41 <b>4</b> 31
			1 19:55 21:39 64 701 069 2
	CAH 67.14		
	1 6:59 8:24 EL 301	- CAR 78.44	-
1001 1		1 11:14 11:54 61 120 777 6 1	I FR MRAYO BAG 1
	110		COR 44.74
17:14 17:41 54 1143 6C* 0	R1 223 327	117.1	
	11 2/1	ANCT TOWN	
1.117	ALCTICLS		0. A A
		1 4 4 2 1 4 3 1 3 0 6 2 1 4 0 5 1 1 0 5 1 4 1 5 3 1	66 39
	I the Te web 112 Te 1511 Barts I	-	AL 277
1:44 4:15 64 41 DC4 1	1 12:14 70:54 K] 4:1 384 K1 840 1	I FR CHARLIE CCC 1 4	600031
	-	CAR 84.44	
	1 LB DEF 14	14:12 27:09 GLI701 777 2 1	I FR CHARLIE CCC 1
	54°84 440	CONAECT TONS	CAP A0.54
10:40 11:20 EB 11 DCa 1	1 11:20 12:2- LT AT DE 1	10:47 11:44 55 10A MRB 51 130 1	
CORP.C 71.585	C. MALCEIDAS		
21 11:22 69 204 441 CO 101			0263.04
TIN TUNE LY THE ALL T. S.			
			+ 28:00 21:34 64 703 DC4 6
		-	
10:01 20 10 10 10 10 10 10 10 10 10	1 10:37 21:54 PL 202 AAA PL 274 1	9:44 11:54 6t 120 727 1 1	1 . 6:30 .13:50 BL. 210 BLP BL 272
	-		1 11:09 13:56 M. 214 MD8 B4 272
	I FE FUELAGE FEE 2 1	CUMMECTIONS	
Can 45.41	1.11	9:00 11:50 KL 247 ALA RL 221 1	I FR DELTA DOD 1
فللسلام فأسلام والمستعد	1 12:14 15:0. 0. 222 757 1	1 11 10 10 10 10 01 01 01 01 01 1	7 A 0 01
HILS 13:24 EI TUG TIT M 100	1 34:21 19:54 AL 274	PO:10 1:00 6L 122 AAA 6L1701 4	1 1:30 11:00 m1212 727 1
42 13:30 8. PI MAR 8. 203	-	20: 11 ":UT GL 113 AAA GL1701 1	12:49 100 120
	I Fu 6.1F		19:01
1444 FER 4			
へきょうさく ささし	1		

in the second second

126

1

T D

1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100     Image: 100       Image: 100 <td></td> <td></td> <td>-</td> <td></td>			-	
	╺╺┝╺╺┝╸╸┝╸╸┝╸╸┝╴╸┝╴╴┥ _╴ ╸┥ _╸ ╸┥ _╸ ╸╷╴╴╷╴╸ _┝ ╸╺┝╸╸┝╸╴┥╸╸╷╴╸╷		TYC THOTA	1 1 TO JULIET	111
	· · ▶ · · ▶ · · ▶ · · ▶ · · ↓ · · ↓ · · ↓ · · ↓ · · ↓ · · ↓ · · ↓ · · ↓ · · ↓ · · ↓ · · ↓ · · ↓ · · ↓ · · ↓ · · ↓		· · · · · · · · · · · · · · · · · · ·		
1:1:1:1:1:1:1:1:1:1:1:1:1:1:1:1:1:1:1:	· · · <mark> · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · ·  · · · ·  · · · ·  · · · ·  · · · ·  · · · ·  · · · ·  · · · ·  · · · ·  · · · ·  · · · ·  · · · ·  · · · · · · · · · · · · · · · · · · · · </mark>	7 7 67 7 V	11 CO CO CI VL	1 13.00 14.14	1
Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state         Image: Second state		• 101 DC •			
1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1		11111		1 1 10:39 20:25	
11:31:30:31:31:31:30:31:31:30:31:31:30:31:31:30:31:31:30:31:31:30:31:31:30:31:31:30:31:31:30:31:31:30:31:31:30:31:31:30:31:31:30:31:31:30:31:31:30:31:31:30:31:31:30:31:31:31:30:31:31:31:30:31:31:31:31:31:31:31:31:31:31:31:31:31:	╷╺╞╴╴╺┝╴╴╵┝╴╴┥╴╴┥╴╴┥╴╴╷╴╴╷╴╴╺┝╴╴╺┝╴╴╺┝╴╴	1+0014			
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	╺╴╸┝╴╸╺┝╴╸╺┝╴╸╺╎╸╸╺╎╸╸╺╎╸╸╺┝╸╸╺┝╸╸╺┝╸╸┍┝╸╸┝╸╸┝	171 1-0004			EEF.
0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes       0:0:0:0: Classes <td< td=""><td>╸╺┝╴╴╺┝╴╴┥╴╴┥╸╴┥╸╸╻╴╴╷╴╴╷╴╸┝╴╴┝╴╴┝╴╴┝╴╴</td><td>800052 727</td><td></td><td>CBA</td><td></td></td<>	╸╺┝╴╴╺┝╴╴┥╴╴┥╸╴┥╸╸╻╴╴╷╴╴╷╴╸┝╴╴┝╴╴┝╴╴┝╴╴	800052 727		CBA	
13:5:70       13:5:10       13:50       15:5       13:5       15:5       14:5       14:5       14:5       14:5       14:5       14:5       14:5       14:5       14:5       14:5       14:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5       15:5 <td>┝╸╸┙┶╺╺╎╸╸┥╴╸┥╸╸┥╴╸┥╸╸┥╸╸┝╸╸┝╸╴┝╸╴┝╸</td> <td>CHUDIN NH</td> <td></td> <td></td> <td></td>	┝╸╸┙┶╺╺╎╸╸┥╴╸┥╸╸┥╴╸┥╸╸┥╸╸┝╸╸┝╸╴┝╸╴┝╸	CHUDIN NH			
No.213 0:134 Ge 000 MD (4 2(1))       FT (7)       FT (7) <td>~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~</td> <td>1.4 14 010 11 17 1.4</td> <td>159 17</td> <td>-</td> <td></td>	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	1.4 14 010 11 17 1.4	159 17	-	
Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model         Model <th< td=""><td>╸ ╸╴╴┑╴╴┑╴╴┑╴╴┑╸╴┑╸╴╸╴╴┑╴╴┑╴╸╺┝╴╴╺┝╴╴╸┝╴╴╴┝╴╴</td><td>1141 Co 404 DAU 48 703</td><td></td><td>I Fh GOLF</td><td>999</td></th<>	╸ ╸╴╴┑╴╴┑╴╴┑╴╴┑╸╴┑╸╴╸╴╴┑╴╴┑╴╸╺┝╴╴╺┝╴╴╸┝╴╴╴┝╴╴	1141 Co 404 DAU 48 703		I Fh GOLF	999
1       13:50       13:10       11:10       13:10       11:10       13:10       10:11       13:10       10:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:10       11:			CAR 44.47	1 0130 10210	
Image: second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in the second state in	╺╴╸╴╴╴╴╴╴╴╴╴╴╴╴╴╴╴╴╴╴╴╴		WT 120	1 11:54 13:35	
11:11:11:12:13       10:1       1:13       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1       1:13:1 <td></td> <td>h 74.15</td> <td></td> <td>1 CONNECTION</td> <td>1</td>		h 74.15		1 CONNECTION	1
11111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       1111       11111       11111       11111	╸╺╎╸╺╷╡╸╸╺╎╸╸╺╎╸╸╺╎╸╸╺┝╸╸╺┝╸╸╺┝╸╸╺┝╸╸	101 101		•	49 MI 99
1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1			C44 34.00	a se water	
1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1		Ge 203 727		5	
1       0       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1120       1	· · · · · · · · · · · · · · · · · · ·			2 1 17:44 14:34	
1       FF       7:3       7:3       7:3       7:3       7:3       7:3       7:3       7:3       7:3       7:3       7:3       7:3       7:3       7:3       7:3       7:3       7:3       7:3       7:3       7:3       7:3       7:3       7:3       7:3       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4       7:4<	·····································	ui.	1	ž	ł
1       6:02       12:13       61 (00)       23       10       0.01       10       0.01       10       0.01       10       0.01       11       0.01       11       0.01       11       0.01       11       0.01       11       0.01       11       0.01       11       0.01       11       0.01       11       0.01       11       0.01       11       0.01       11       0.01       11       0.01       11       0.01       11       0.01       11       0.01       11       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01 <t< td=""><td>╸╸╸_┥╸╸_┥╸╸_┥╸╸_┥╸╸_┥╸╸_┥╸╸_┥╸╸</td><td></td><td>1 7:73 9:54 1 × 204 AAA 58</td><td>1 8:34 11:47 87</td><td>1</td></t<>	╸╸╸ _┥ ╸╸		1 7:73 9:54 1 × 204 AAA 58	1 8:34 11:47 87	1
F 6.1F         F.6.7         F.7.1         F.7.1 <t< td=""><td>╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸</td><td>0.0 19</td><td></td><td>1 74 8 140</td><td></td></t<>	╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸	0.0 19		1 74 8 140	
I       A:15       Constraints       Fine 11:15       F		566 2		Can 10.41	
I = 15:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10       1:10		14.25	CAN 79.29	1 11:10 15:10	ŧ.
16:14:11:31       400010       73       11:13:12       10:110       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:12       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13       11:13	╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸╸	121 010040 000000 000	011028	1 17:16 21:10 6111	93 869
I = Jul I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I       JJJ I		3345	MALE CT TONS	I TO AILO	
1         10:13         11:13         400010         77         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1 <th1< th=""> <th1< th="">         1         &lt;</th1<></th1<>		rrr 1		-	
10       11       10       11       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10 <td< td=""><td>╸╸╸╸╺╺╺╺╺╺╺╺╺╺╺</td><td></td><td></td><td>1 FR ALPHA</td><td>İ</td></td<>	╸╸╸╸╺╺╺╺╺╺╺╺╺╺╺			1 FR ALPHA	İ
04.67         66.41         66.41         66.4         1         67.9         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1 <th< td=""><td>94.67 11.2001/12.12 10.001/12.12 10.001/12.12 10.001/12.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 1</td><td>424 01000</td><td></td><td></td><td></td></th<>	94.67 11.2001/12.12 10.001/12.12 10.001/12.12 10.001/12.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 11.12 1	424 01000			
000010       777       7       13:73       11:10       00:0       0       17:12       20:0       0       17:12       20:0       0       17:12       20:0       0       17:12       20:0       0       17:12       20:0       0       17:12       20:0       0       17:12       20:0       0       17:12       20:0       0       17:12       20:0       0       17:12       20:0       0       11:12       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0<	000100         777         2           000100         777         2           000100         777         2           000100         777         2           000100         777         2           000100         712         1           1         7         1           01         717         1           1         77         1         1           1         77         1         1         1           1         77         1         1         1         1           1         77         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1 <t< td=""><td></td><td>1/:47 641111</td><td></td><td></td></t<>		1/:47 641111		
Minor         Iconomic (C)	Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123           Ministry         123	49.45	13:14 611001	_	
0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0	Ga yar 787 7 7 7 8 Ga yar 787 7 1 7 8 Ga 112 723 1 9 1 Ga 112 723 1 1 1 AAA 1 1 17 AAA 1 17 AAA 1 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAA 1 17 AAAA 1 17 AAA  1 17 AAA 1 17 AAAA  1 17 AAAAAAAAAA				5
0000/) [0:0]       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01       01	CI 412 729 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			I FR BRAVO	
GI       A12       727       1       111.2       777       2       A13       10       17.1       11.1       11.1       11.1       10       10       11.1       10       10       10       11.1       10       10       10       11.1       10       10       10       11.1       11.1       11.1       11.1       11.1       11.1       11.1       11.1       10       10       11.1       11.1       10       10       10       11.1       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10	GI         A13         723         A         1         1           A         A         Y         A         A         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1 <td>11.114</td> <td></td> <td>1 I CAR</td> <td></td>	11.114		1 I CAR	
Also         I         IST Number	A40 1 1 10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1: 11 61 812 777 2	<b>1 1 1 1 1 1 1 1 1 1</b>		Т
0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0	40.77 E[ AN 7.7 E[ AN 7.7 1.7 80.01 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.				
CI AND 727     I I F 4 [Wid     U.4.2     1 5: 14: 14: 14     C. 11     C. Marcellans       Consert 271     0     1: 5: 0     0: 20. 26     1     1: 5: 0     C. Marcellans       Consert 271     0     1: 5: 0     0: 20. 26     1     1: 5: 0     C. Marcellans       Consert 271     0     0: 5: 0     0: 2: 0     0: 2: 0     0: 1     1: 15: 0     0: 1       Partition     0: 1: 0     1: 1: 0     1: 1: 0     1: 1: 0     0: 0     0: 0     1     0: 0       Consert 271     0: 1: 0     1: 1: 0     0: 0     0: 0     0: 0     1     0: 0       Consert 28     0: 0: 0     0: 0     1     1: 0: 0     0: 0     0: 0     0: 0       Consert 28     0: 0: 0     0: 0     1     0: 0     0: 0     0: 0     0: 0       Consert 28     0: 0: 0     0: 0     0: 0     0: 0     0: 0     0: 0     0: 0       Consert 28     0: 0: 0     0: 0     0: 0     0: 0     0: 0     0: 0     0: 0       Consert 28     0: 0: 0     0: 0     0: 0     0: 0     0: 0     0: 0     0: 0       Consert 28     0: 0: 0     0: 0     0: 0     0: 0     0: 0     0: 0     0: 0       Conse	FI 475 727 1 75 806-41 229 0 1 807-51 229 0 1 807-52 00 0 807-52 00 0 1 80 201 227 1 1				
00041         773         01         11:1:1:2         20:30         10:1:2         20:30         10:1:2         20:30         10:1:2         20:30         10:1:2         20:30         10:1:2         20:30         10:1:2         20:30         10:1:2         20:30         10:1:2         20:30         10:1:2         20:30         10:1:2         20:30         10:1:2         20:30         10:1:2         20:30         10:1:2         20:30         10:1:2         20:30         10:1:2         20:30         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2         10:1:2 <th10:1:2< th=""> <th10:1:2< th=""> <th10:1:2< <="" td=""><td>808141 221 0 1 6:50 90.041 727 0 1 6:50 86.701 727 1 10:00</td><td>~ 711</td><td>6L1 103</td><td>1 1 CONFECTION</td><td></td></th10:1:2<></th10:1:2<></th10:1:2<>	808141 221 0 1 6:50 90.041 727 0 1 6:50 86.701 727 1 10:00	~ 711	6L1 103	1 1 CONFECTION	
Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany         Normany <t< td=""><td></td><td>****</td><td>COMMEC TITAS</td><td>M 26:02 26:61</td><td>4</td></t<>		****	COMMEC TITAS	M 26:02 26:61	4
	58 241 727 1 1 10:00	10 11 11	7:54 11:47 66 901 MM8 641	┥	
		5			
				1 1 0:00 0:01	-
			Can 01.10	1 0:02 10:20	90 BC9
	-		6113		

																		1		The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon																
			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	64 701 727 0 1 441794 747 0 1	121		ſ	÷ Ja	61 103 127 0 1			2 10.01	1	AL1703 207 0 1			58 352 727 1 I	10		H 1700 207 1 1		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		1 711 0C0 2 1		arc a a	244.47	j.		1	61 811 727 2 1	RFE 1 1	277.59 1 LT 211 009 5 1	í		-
1.1 n <u>1 1 n 2</u>		-	I TE ALEYA CAN		ł.			1 13:51 14:05			L		1 A: 52 10: 24	11:01 00:0 1		11:49 14:08		1 15:00		11:06 20:11				1 11: 46 1A: 09		<u> </u> = = =				CAR	7:34 17:14 (	I FR ALL	1 10:34 10:05	į		
	I d deu		10 11 11 DC 0 1		19.15	211 6L 301 727 2	A CTIONS	12:00 14:51 64 21 AAA 68 32	51- 64 13 443 68 922	1 000		17:11 71:10 MT 111 DC4 1 CJAN CTIONS	14:05 23:17 b1 311 AN MT 111	13. 64 403 604 60 0C3	[ FE 2	10.14	211 61 901 727 C			1 AN 01 . VP	51	102 14	61 122	1 HAR	54.53			CAN 93.73	9:44 41 400 BC9 1 22:11 61 1/2 777 1	F10+5	121 BR 44 BAR CR 94	000			71.17 0111 6L 115 AA4 6L 122	
	- -		111 11 11 1	-	-		┥╾	-	10:01 10	1 1 1 5P DEL 1A	-	2   17:11 21	-		2 1 FR FCHL	-		•;•	- • 		• D : • •	2 1 1 1 1 2 0 1 0	11:22 01:12 1 0	CANAN BE L		1 10:02 10:54				-		2 7 70 06112			5 1 5 1 5 1 5	
					ł	1 200 1C0			611003 DC1	Ŧ		64 11 0 5 11 C 4	1 77	86.10 51100 UT •		İ.		1 1223 12216 - 1 166 666 5	化化合物 化化合物 化化合物 化合物合物 化化合物合物合物		5 444 51 14	- Kn YF UCh -	5 <b>8</b> - 54	Ove			1 333	10 16 19	111	ĺ		< 184		14.74 68 12 DC9	-131 669	19
للحرية ذائد	V) ell.		14:00 14:4)	F. 04114		1116 9141 1116 9141	11:11 12:11	41:41 14:41	11:44 14:27	tatum ee		11:51 11:41	Fe JULIET		14:14 14:27			11:41 Lein			F# ALPH4	UTLAST.	10:07 14:42	DAAVE BY			Fe CHARILE	11:11 04:11		1.1		Jala Su	FR ALPHA	1.21 1.21	21.16 26.24	Same an

		:4-50 5111			
هنزي إن مامن	-111-	LIST NOBIFIED	Last usen	UNTVERSE	01131004 1377 ]Se]a[un
:_1135w_Alan				FAA. 0001	FAA. 8801 80/01/18 10:10:17 .00
	10- JN74	80,03/14 10:27:36.00	))"[]:L5:11 +1/20/04	FAA_0001	48/81/18 14:14:33°40
	6-01-01		80/02/14 11:57:03-00	LAA BABL	AB/81/18 15:11:41 817(8766
4 80 860 9 61 64175	10-1114	80/03/13 14:14:54.00 80/03/13 14:14:54.00 80/07/11 15:44:44.00	40/02/14 11:57:73.00 40/02/14 11:57:03.00 40/02/14 11:57:03.00	FAA_0001 FAA_0001 FAA_0001	10/01/18 14:14:37.00 10/01/18 14:14:57.00
				, , ,	
-					

r r i

TABLE 4.13 PERIOD 2 SCHEDULES

7

- And world michaided

State Action

į

いって ちまい 美国語

	·		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	ALA CCC BH ALA CCC ALA ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCC ALA CCCC ALA CCC ALA CCC ALA CCCC ALA CCCC ALA CCCC ALA CCCC ALA CCCC ALA CCCC ALA CCCC ALA CCCC ALA CCCC ALA CCCC ALA CCCC ALA CCCC ALA CCCC ALA CCCC ALA CCCCC ALA CCCCC ALA CCCCC ALA CCCCC ALA CCCCCC ALA CCCCCC ALA CCCCCCC ALA CCCCCCC ALA CCCCCCCC		1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
797         700         700           797         700         700           797         700         700           797         700         700           797         700         700           797         700         700           797         700         700           797         700         700           797         700         400           797         700         400           797         700         400           797         700         400           797         700         400           797         700         400           797         700         400           797         700         400           797         700         400           797         700         400           797         700         400           797         700         400           797         700         400           797         700         400           797         700         400           798         400         400           799         400         400													
737         757         645         655           737         757         645         757           737         757         645         757           737         757         645         757           737         757         645         757           737         757         645         757           737         757         645         757           737         757         645         757           737         766         646         646           737         766         646         646           737         766         646         646           737         766         646         646           737         766         646         646           737         766         646         646           737         766         646         646         646           737         766         646         646         646           737         766         646         646         646           737         766         646         646         646           737         766         646         646         6	• • • • • • • • • • • • • • • • • • • •							1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1					
737         CCC         FOR         CCC           737         CCC         AMM         CCC           737         CCC         AMM         CCC           737         FOR         CCC         AMM           M           737         FOR         CCC         AMM         AMM           737         FOR         CCC         AMM         AMM           737         FOR         AMM         AMM         AMM           737         FOR         AMM         AMM         AMM           737         FOR         AMM         AMM         AMM           738         FOR         FOR         AMM         AMM           733         FOR         FOR         AMM         AMM           7						00 00 00 00 00 00 00 00 00 00 00 00 00		CCCC 711 CCCC 711 CCCC 711 CCCCC  711 CCCCCC 711 CCCCCC 711 CCCCCC 711 CCCCCC 711 CCCCCCCCCC					
737         CCC         Ama         CCC           737         CCC         Ama         CCC           737         TCC         Ama         Lin           737         TCC         TCC         TCC           737         TCC         Ama         Lin         TCC           737         TCC         TCC         TCC         T	•							CCC 710 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 2010 20					
						101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12 101 12	CCC CCC CCC CCC CCC CCC CCC CCC CCC CC	A 44 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4					
23         24         24         24           23         24         24         24           23         24         24         24           24         24         24         24           25         24         24         24           25         24         24         24           25         24         24         24           27         24         24         24           27         24         24         24           27         24         24         24           27         24         24         24           27         24         24         24           27         24         24         24           27         24         24         24           27         24         24         24           27         24         24         24           27         24         24         24           27         24         24         24           27         24         24         24           27         24         24         24 <tr tr="">          28         24</tr>						101 101 101 101 101 101 101 101 101 101	CCC 000 000 000 000 000 000 000 000 000	1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1					
1771         1771         1771         1771           1771         1771         1771         1771           1771         1771         1771         1771           1771         1771         1771         1771           1771         1771         1771         1771           1771         1781         1781         1781           1771         1781         1781         1781           1771         1781         1781         1781           1771         1891         1761         1781           1771         1891         1761         1781           1771         1891         1761         1881           1771         1891         1761         1881           1771         1891         1881         1881           1771         1881         1881         1881           1771         1881         1881         1881           1771         1881         1881         1881           1771         1881         1881         1881           1771         1881         1881         1881           1771         1881         1881         1881	·					201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 20							
717         717         717         717           713         711         711         711           713         711         711         711           713         711         711         711           713         711         711         711           713         711         711         711           713         711         711         711           713         710         711         711           713         710         711         711           714         710         711         711           713         710         711         711         711           713         711         711         711         711           714         711         711         711         711           713         711         711         711         711           714         711         711         711         711           714         711         711         711         711           714         711         711         711         711           715         711         711         711         711	• • • • • • • • • • • • • • • • • • •					201 12 12 12 12 12 12 12 12 12 12 12 12 12					000000000000000000000000000000000000000		
1319         711         400         611           1319         711         600         611         610           1319         600         111         600         611         610           1319         600         111         600         612         610         610         610         610         610         610         610         610         610         610         610         611         610         610         611         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610         610	·					201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12 201 12					8538533		FEREN FEREN Control Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Feren Fere
				A 144 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 43 14 44 44 45 14 44 45 14 44 45 14 44 45 14 44 45 14 44 45 14 44 45 14 44 45 14 44 45 14 44 45 14 44 45 14 44 45 14 44 45 14 44 45 14 44 45 14		901 72 902 72 902 72 901 72 901 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 904 72 907 907 907 9007 90000000000000000000							HINN HINN DEE DEE HINN ANN ANN ANN ANN ANN ANN ANN ANN ANN
						902 727 902 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 727 903 72							
127 AGM 416 AM 41 127 AGM 416 AM 4 177 AGM 41 AM 4 177 AGM 41 AM 4 177 AGM 744 AM 4 177 AGM 744 AM 4 171 AGM 744 AM 4 171 AGM 744 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171 AM 4 171				A B C C C A B C C C C C C C C C C C C C	 1 1 1 1 1	901 72 902 72 903 72 903 72 903 72 903 72 903 72 903 72 903 72						방금방물성종 王남문방명문	
727 007 448 444 70 737 000 545 444 70 737 000 544 00 737 000 444 00 737 000 444 00 737 000 444 444 737 145 04 000				A CCC A DO	 	902 12 901 12 902 12 902 12 900 12 900 12 900 12							11 11 11 11 11 11 11 11 11 11 11 11 11
				10 CCC 44 00 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCC 44 000 CCCC 44 000 CCCC 44 000 CCCC 44 000 CCCC 44 000 CCCC		401 72 901 72 902 72 903 72 903 72 903 72 903 72 903 72	000 1 1 000 1 1 000 1 1 000 1 1 000 1 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 00	000 CCC 444 CCC 444 CCC 900 A44 888 A44 000 A44 CCC CCC CCC 890 A45 888 A44 888			100 CCC 100 CCC 111 AAA		
727 MAN 110 LLA M 777 MAN 110 LLA M 727 MAN 141 MAN 727 MAN 144 B09 727 MAN 144 B09				A CCC AA CCC AA CCC AA CCC AA A CCC AA A CCC AA		90, 12 90, 12 90, 12 90, 12 90, 12 90, 12 90, 12	CCC 0 000 000 000 000 000 000 000 000 0			200			
777 100 111 100 727 100 111 100 727 100 111 100 727 100 110 110	╺ ╸╸╸			M CCC AA M CCC AA M CCC AA D CCC AA D CCC 66		901 12 902 72 903 72 904 72 904 72 905 72 92 72				212	100	IL AAA	
727 ND0 444 N00 727 A00 NA0 800 727 A00 NA0 800 727 A40 909				M CCC AA 14 DDD AA 14 DDD CCC 66	-	902 72 903 72 904 72 904 72 904 72 905 72 72 905 72	1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000 1 000	000 AA1 000 AA1 000 CCC 000 CCC		1 200		IFE AAA	Part III
727 ABD PHE DOD 727 ABD ARD 444 727 145 FME DOD				A D00		505 72 509 72 601 72 603 72 72 100				100			CCC MK DBB AAA FFF
727 ABA 444 666			PUD -	10 CCC 66	•	504 72 401 72 402 72					1		POR FEE
727 BAS PM 000			AAA DI CCC A	10 CCC 66	(	401 72 402 72 72 72		000 CCC CCC 000 CCC		111 1		FF AAA	AA FFF
			200	4	-	403 72				1 600		1000 × 1	
	-				-	403 721	222	000 CCC			10 10	An CCC	A44 800
		ļ	W WY	A DOO KK	-		200	000 111		1 111	0C2 11	RE AA	CC. MA
	•			C RAN	•	00 33				1 420	9C.9	AA 44	200 113
		57		21 444 H		121 509	2	8		1 200 1	5		CCC EEE
	f					404 12	000	30		1916 1	1		200 333
727 AAA 144 727													
727 PAG 444	•	ţ											
TAT BOT AL	ŀ	ĺ,				101 600						111 00	<u> </u>
727 444 848 444	-	5		C 000 444		01 13							LLE AAA
707 865 111 865	-	103 004	KAN DO	DON CCC A	_	104							
707 RA4 TAF	ŀ	131 664	Lat D	IN CCC NON		902 72							
101 TEN 100 XEN	•	1 52 OC4											
707 XKH ANA	-	133 BC1	AAA CO		-					• •			
707 PBA 444 333	-	120 0011	N III	100 MM 000	-	10				-			
	-	761 727			•								
AA KEE	-				-		500	111 966					
							999	age mr		-			
	-				-		ł	777 398		-			
	-		(	ļ	-				_	-			
		100	14 0.0	H AAA CC	CCC 000 1		Ì		AAA	-			
	•	17 004	1000		-		H	11		-			
	-	11 71		1 444	-		666	NAN BUN	-	-			
							HHH	AAA MAN		-			
	~	21 001			-			I		•			
	-   	** 0C4			-		Ī	ORE AAA	-	-			
	-	11 004	I TVT	1 202 1	1 111 1		Ē	ANN A66		-			
	-	33 004	AAA 00	ç	-			666 AAA	-	-			
	-	20.5	11 ONU	000 v	-		i	AAA CCC		-		I	
		1 20	111 377 944	aa 111 ]		9941 964	Ĕ	HIN NH		-			
	-				•			DAR CCC		-			

Sector Sector

فيترا ومنكرية

			-								1 3 2 2 2 2 2	1 2 2 2			922222	*****************	\$ . t
2 31 PMB		4 4 4	-	TO ALPH	4		-		TO ALPMA			121	NO ALPH			444	
		*****	-	*****						*************			2200012		101000	********	
			_				ย่		FA FORTHIT		비 	2	FR NUVER				~
				14:46 17:27	17:23	AL 205						-					•
	7			2.2				-	12:15 12:52	i i	222			5			•
Γ.	000 I.a	004	-		10:40		•	-	17:00 17:	5		•	FR XMAY			H	-
06:1 61:1 07:07 67:1	10 200 AU	227		12:51	20:1.	11111			16:21 14:50	-		•		e e			,
									5 . C. C		202		22.22		102 YO		
	1								•	PAA 71.55				1.00 11:17			
•	61 M12	171	-		22:12	81 204			÷		0 000	0	102		641700		
10:01 01:4	16 18	12 1 0	-	22:13	72:54	81 a9	1	-				•	11:25	17:02	FR 70.	Ł	0
11:12 11:41	RC 231	127 0	-		C.UMMC	Ĩ		-	101 01 10:	54 HL 280		0	11:34 17:31	17:31	91170		•
12.01 010 11	214 89	121 1	-)	. 6:30	b: 3r 13:07 ML		1 11 2	11	12:20 14:		ł	~	11:00 10:11	10:32	64 012	- 1	9
41:21 45:11	3	• • •		11:12	11:12 15:24 6	7 500 EFE	5		14:00 19:54		5	~	1 14:23 22:02	22:02	3	2	0
									141 14 191	54 R00012	- N 1	•	14:30 22:01	22:07			•
	<u> </u>	Pro 1	-					-	C		14 04 0						
11:11 12:21	112 14			4 1 JU 4 3			000				-						; •
11:45 14:20	NL 250	127			CAH	82.18		-	FR MOTEL		Ĩ						
11:52 10:30	101 19	727 A	-	1:00	7.4.1	811715	102	-		CAN 99.6	-		FR ALPWA	-			
19:19 14:33	RL 273	1 121	-	1:00	\$010	11 03	900	-	4: 10 7:			0		5	20.03		•
14:00 14:43	11	127 0	-	90.8	\$0:01	61 7-6		-	1.1.2 0414		1 21	-	4:27	6113	68 301		
14:00 14:13	NT #20	000	-	0010	54:0	11 200	121	-	7: 34 9:		i –	-	4:54	10: 35	64 100	ì	-
	*1 257	127 0	-	8:23	1.57.8	61 400		- 0	14:05 17:			~	14:14	:: 23	3		•
14515 17510		121 0	-	1.24		100 00	i	- •	1.13.15	1	1. 127	•	1:00	1:00 10:30	61.12	ì	
11:04 11:03	M 3708	101 0	-		3 <b>8</b> 7	AL 258		•	17:19 19:54	54 RD0012		~	1:30	1:34	MT 300		·
17:45 10:70	BL 242	127 0	-	11:01	13314	64 307		-	14: 34 19:	34 80002	227 6	•	2:3	10:31	BL 27		•
		121	-			91119	ł			ACTT JANO 3	5		12:1	11:33	58.40	)	-
			-					~ •			و س	2	10:05	12:28	87 298		6
								 > c				;		10.41			~ 6
1	611701	122						ين م م	F. D. P. B. L. D. L.							ì.	
18200	LC 11 nus	Ì	• -	14:05		11 11	010	-		CAR 40.24							, c
A: 30 12:74 M	230 66		-	1.10	1 1 1 2 2	AL 241	1.7.1		-			~					. 4
			-	10:10	00:51	61 701	430	- 0	12:32 19:40	169 14 635	1 004	-	1 14:00 14:24	16:24	611700	1	•
FR CHAPLE		202	_		1 7:30			-	13: 40 14:			•	14:40 16:30	10: M	RL 299		-
		1.000	ļ	19:12				-					14:47 11:42	11:42		٦	-
			-			297 18					3						•
	101 47				11:24					-							
Г	LUR TO	0 000	1		20:16	1111	00		11:01 (0:61	Γ		-	11:22 10:40	10:01	SO 202	¥.	•
	N 100	000	-		20:34	GL 122	127	-	18:27 19:34			-	19:18	20:17	91170		•
	104 99	127	-		20110				19: 71 19:		11	9	19:00 21:20	21:24	N 112	T	-
	;				201100												
14:21 15:ut	1			10:00	A 95 14 5	1 2.20 2.				64 1000							- 0
11:11 11:11	1111	107 0	1	1	14:37 6	AL 241 BAN	Ē	-				1	22:47	Ē		1	•
11:00 13:11	12 5	50	-					-	FR 411.0	,	11 H H	-			1611 104	ž	
							Ë	-		ة: 	1		17:32	21:00	6L1133 CCC		131
1 2 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2				7:10	445							~ -				2	
		227	-			AL 221	121			5	_	-		CAN	39.46	, ,	-
	464 74	1 144	L	13:44	13:34		1	-	FR LIM		E	2	06:0	1:11	2 3		•
(u:91 +2:61		2	-	19:97						Can 94.3	-	-	1:30		1	0 727	•
		121	-									•				22	-

132

100											, E
ì											
2		F. ECHO			1 FR #140		KAK L	E FR ALPHA			2
11 72 000		10:36 12:5	102	227	0 17:14 20:0	61101			;;		- 4
P0041 DC9	•	11:11 13:11	WT 510			CONNECT I'NS		1 15:32 10	2		•
164 727		1.01 00:01	<b>z</b> :	171 0	1 11: 12 14:0	14:04 MI 211 CCC	114 14 3	NC:01 56:51 1	2		-
		14:11 70:24	₫;	-	· 18:14 20:5	51 804 CC	C 411 701	1 14:23 14:		RL1713 70	•
								1 17:00 20:08	1		
				i	1 1 1 1 1 4 1			12:02 05:21 1	3	101 121	•
									1		-
111 121		21:14 2:15	V 440	1	1 17:02 17:42		0.00		1	Ł	ſ
	•				-		•	11:25 21	1		•
	•	FR FURTEDT		6 555	I FR ALEE		<	16 M. 104			•
Ł	0	CAN	. 78.4					22:22			
FD0043 DC9	0	4:02 4:2>		1 121	1 9:57 12:51		1 22		3		•
257 727			đ	127 0		1					
Ľ	-		41 274	6 664	I CO MONT MAP		200				
			!						8		5
+ DC +		F. B. GAL		6 233					1		
1								33 25571-1	27 IL 17 IL		
		12:14 14:51			1 14111 1 10 10 10 10 10 10 10 10 10 10 10 1						1
	•						1		:	•	
CE 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2								I.		Т	ľ
							-				•
						11		1 1:00			•
			1	Ì.				1	1	٦.	ľ
184 727		16161 06111	ź	11.2.10							
	-				1 B: n2 14: 44		727				••
ā	010 1 1	FP NQTEL		T HMH	1 10:31 17:55		707	•	i i	Ľ	ľ
54.64		CAB	8 44.27		1 11:25 10:44		1 1 1 1				•
_	•	4:40 11:53	ē	157 2	11:35 #2:11 1	AL 1704	202	101 101	1		•
Ē		6:40 7:35	i i	00.0	1 13:00 21:20		127	01 0 0	1	1	
RL 254 727				121	1 14:25 7:41				3		•
	-	11:00 11:54		• • •		13					
756 127	F	12:05 1 3:00		127 0	ſ		707	1 12:54			
	•	27204 17:59		9 • JQ	***************************************	2		1 13:00 13:			-
_	•	1111 12:01	3	• • • •	I TO CHARLTE		CCC 1	1 11:11 13:13	13.74		•
	•		UNALCTIONS					1 13:53 14:	5	516 60	
167 127	•	11:51 14:14	LI 110 CCC	NT 411	I F R ALPHA		2 2 1 2	1 11:54 10			•
121 729	•				Ū	A 77.25		1 14:24 14	2		
Ľ	F				1:5 60:0 1	ER 701	727 0			141 727	ľ
121 149	•	3	n 17.74		1 4:50 10:40	đ	004	1 14200 20200	3		-
121 127	-	6:44 11:04		1		3	101	1 14:14 17:			•
101 727	1		1						ł		ł
						1					•
		Î		-		ť					•
			.		1 1 1 1 1 1 1 1 1		-	10:51 21:07	5	20 22	1
121 121		A: 50 7:10	3	0 0.0		Ĩ	107 0	1 19:00 19:94	Qu		-
	••			•	1 9:03 11:26		127 0 1	1 19:14 20:	4		•
710 727	•	11:40 12:34		0 • JO	1 9:04 11:32	3	127 0	1 10:10 20:	3		•
Art 323	1		611062						۰.		ľ
									ť		
		C. 114									
1					11:78 11:36			_			l
			2 (	-	1 12:31 14:34	11115 ·	101 0	I F# DELTA			- §
					2		12 7 0	-	C + + 2		
	-	10:32 1/:1.	13	-	1 13:14 19:44		1 2 2				•

Ċ.

	1221	
5 J J A B J C J J A B J C J J A B J C J J A B J C J J A B B B B B B B B B B B B B B B B B		
	1225	
		010 1 1 10 DELTA
	1111	10
ſ	-	-
	:	6
	÷	5
- {	2 6 8	
L		
Ē		
F	222	
	111	2
-	222	8
Ē	2 5	CCC 1 1 TO DILTA
-	:	-
-		20
- Ē	i i	-
Ē	12	
مإ	522	
Ē	Ë	
	222	
	ÿ	3
ì		ł
		3
	H	5
		-
		J
-	1	5
	2	
Ē		
- i	i ii	
Ē	Ĩ	CCC 1 1 10 CMARL 15
2		L
Ē	Ē	Ē
Ē		
Ē		6
Ē	**	Γ
	•	

ľ

1244

				**********				1 040			
	â	1 00	I ER HUTEL	;	- HHH	ER ALPHA		444	-		222
		•	1 17:04 19:44			12214 14247	91/179	2	1 11:44 1	3	
			11.11 17.24							5 i	-
	1	•			1111	14:12 14:04			1 15:27 1	1	Г
		•	CAN CAN			15:35 11:24	3	•	1 15:30 1	3	
	1	-	A0.01 CT.	1							1
					1 11						
773     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1<				41.94		14:00 20:29			2 20:07 2		
177         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1	5	0	•		-	1 14:21 20:50	3	181	-		
		•			2	19:05 27:57	a) a	121			
				1		41:12 01:02		101			Ŧ
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$								1			
727       0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0       51.0 <td< td=""><td></td><td></td><td>60 H H G</td><td></td><td></td><td>14:00 14:28</td><td></td><td>61.10</td><td></td><td>1</td><td></td></td<>			60 H H G			14:00 14:28		61.10		1	
121       0       1011       1012       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       1011       10111       1011       1011 <t< td=""><td>1</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>1 10:12</td><td>Ŧ</td><td></td></t<>	1								1 10:12	Ŧ	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		0 0								5	32
If (f 2 1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1	γ.					AC 00 14	20100	151	1 12411 5		
If (f 2 l)         If (i a)		,	11:11 12:59					e u		1	665
731       1       1713       1110       1713       1110       1110       1110       1110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       11110       111100       111100       1111100 <td>7</td> <td>FC 2 1</td> <td>17:14 19:01</td> <td></td> <td>C• 1 ]</td> <td></td> <td>16</td> <td>127 1</td> <td>-</td> <td>C.P. 3.</td> <td></td>	7	FC 2 1	17:14 19:01		C• 1 ]		16	127 1	-	C.P. 3.	
070       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1			1 17:39 10:35		•		-	• 30		3	í
101       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1		-			-	1110 11:00	3	•		3	
7/37       1       1/37       1       1/37       1       1/37       1       1/37       1       1/37       1       1/37       1       1/37       1       1/37       1       1/37       1       1/37       1       1/37       1       1/37       1       1/37       1       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       1/37       <						1 1 1 1 1 1 1 1			1 17:00 2	5	- 1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			137 13799	9	•						255
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		-				11:11 12:20	5			CAN No.	
N N. 2101       C. 0       0.77       1       175       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50       0.50	afc110mS	-	FR BUVERBER		NRM 2	1 12:34 17:44		101	1 26:1 1 1	1	
If N = 11       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1			CAB		-	1 13:45 17:09	ę	171	1 0::0 1		
				1		11:00 10:52	╞	12	1.1.1.1.1.1	- į	1
FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF         No.         FF			101111111111		-		i				
T. M. 221       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)       1 (1)		-	60 18A1								
F       M       273       1       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100 <td>284</td> <td></td> <td>}</td> <td>200.30</td> <td></td> <td>14:00 17:04</td> <td>1</td> <td></td> <td>1 10.201</td> <td>d -</td> <td></td>	284		}	200.30		14:00 17:04	1		1 10.201	d -	
M. 64 (1)00         L (222)         L (232)         L (232) <thl (232)<="" th=""></thl>	E - 13	273 4			27 2	14:18 20:14	ę	127	-		
646 Z       1       00011       1       173       0       130       131       0       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131       131 </td <td></td> <td>1700 1</td> <td>14:25 1:54</td> <td></td> <td>۰ ۲</td> <td>17:72 JA:20</td> <td>6</td> <td></td> <td>D F.F.R. HOTEL</td> <td></td> <td>MMM</td>		1700 1	14:25 1:54		۰ ۲	17:72 JA:20	6		D F.F.R. HOTEL		MMM
666         7         00111A         0000         1         1011         1013         0         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         00000         00000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000         0000<		1				1 17:56 19:04		127			51
737     0     1     737     0     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1			F0 DEL 14		1 000	10:01 10:01	5	121		-	
727     1     1     727     0     127     0     127     0     127     0     127     0     127     0     127     0     126     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0								111		T	٦
777     6     6.277     10     779     14.54     17.15     14.54     17.15     15.1     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14     15.14 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>											
727     01     526     01     100     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770     770			A:27 10110	1	-	5		C 81 21			
It         It         Totol         Totol <thtotol< th=""> <thtotol< th="">         Totol<!--</td--><td>ł.</td><td>6</td><td>10:01 9:0</td><td>000</td><td></td><td></td><td>1</td><td></td><td>1</td><td></td><td></td></thtotol<></thtotol<>	ł.	6	10:01 9:0	000			1		1		
I. 6. a.(1         1:00         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0         10:0		-	7:00 0:24	120	•	I FR CHARLIE		J			111
Image: 1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1<		5	8:00 10:54	-	•	C					
New I         1         7:00         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1:10         1		[	16:01 20:0	(		20:0 0:11	Į –	141		3	
UCC 1 1 10:00 12:20 66 11 0:00 12:0 11 0:00 02:0 0 1 14 04 12 0 0 1 14 04 12 0 0 12 0 1 14 04 12 0 0 12 0 0 1 14 04 12 0 0 12 0 0 1 14 04 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 12 0 0 0 12 0 0 12 0 0 12 0 0 0 12 0 0 0 12 0 0 0 0			9:02 11:31		•	[ ]:45 4:43	-	727		5	
CC 1 11:100 12:20 41.700 020 1 1 1:20 11:00 020 20 1 1 1.20 41.11 CC 1 11:121 12:20 41.70 020 11:10 11:20 11:20 11:20 11:20 11:20 11:20 020 CC 1 1 11:21 12:21 41.01 777 1 1 12:13 11:20 41 1277 1 1 2:14 12:19 04.100 020 DC 1 1 11:21 12:30 01.21 777 0 1 12:11 11:21 00 11 12:00 11 12:00 01 12:00 020 12 D2 1 1 11:21 12:30 01.21 21 77 0 1 12:101 11:20 00 12 777 0 1 13:25 12:10 00110 17:20 020 D2 1 1 11:21 12:30 01.21 21 70 0 1 12:10 11:25 00 001 17:00 001 12:00 01 12:00 020		-	10:51 52:01		-  -  2	50 B 100		2	-		
OCC         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I         I		-		000		0 8:45 4:20	-	e ja	JI TH THIS		3
		•				10:20 11:00	-	127		_	
	1	-		1		10:34 11:24		14			-1
			421K1 L0111		•		5				
		- '				10:11 10:11	3	127			

CIA 90.03 CIA 90.03 CIA 90.03 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 CIA 91.20 EEE 2 L2:44 13:63 WT 431 0C9 1 LT.T.T.M. CIA 76, 79 MDH 4 12:09 13:01 400051 727 1 17:19 19:19, 900912 859 4 0:34 13:16 6L 011 886 6L 10 Ę 
 Cat
 98.07
 6

 11:22
 11:00
 M01212
 727
 6

 10:22
 11:00
 M00012
 007
 0

 10:27
 10:10
 00012
 007
 0

 7:03
 13:10
 611000
 M004
 0.4
 ~ ~~~~ -200 11:00 13:55 BL 210 BM BL 272 COMATCY TOWS 4:40 13:16 6L1131 006 6L 1.0 6:40 13:16 5L1131 CCC 6L 1.0 
 9. W.U.T.
 6.6.7
 7.1.7
 7.1.7
 7.1.7
 7.1.7
 7.1.7
 6.6.7

 9. J.M.U.T.
 J.J.1
 FF CAMPLE
 CCC.1
 1.7.1
 11.1.9
 11.2.1
 11.1.9
 11.2.1
 11.1.9
 11.2.1
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 11.1.9
 1 000 200 COMFCTINES 12:31 17:09 61 411 444 61 621 CIN 04,76 1 7:59 4:70 00030 71 1 10:59 11:16 6L 100 72 1 11:37 11:54 6L 100 72 1 11:37 11:54 6L 000 72 
 Can
 Can
 Can
 Can

 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1
 1 Can 77.15 12:32 15:01 WT 631 0 | 6 MUVE MALA. 0 | FA MUVE MALA. 0 | 6 04.14 COMPLETIONS 
 freuiet
 Caracter
 Freuit
 Caracter
 Freuit
 Caracter
 Freuit
 Caracter
 Freuit
 Caracter
 Freuit
 Caracter
 Freuit
 Caracter
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 Freuit
 CCC 1 1 FA CHARLIE I FR DELTA 8:14 17:54 61 811 APU 61 120 5 FR HUTEL FR ECHD 
 I
 C(4
 92,17
 I
 Vision
 C(1)
 Vision
 C(1)
 Vision
 C(1)
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 Vision
 <thVision</th>
 Vision
 Visi . CAN 76.75 1 CONNECTIONS 1 7:45 11:56 6L1000 ANN 6L 270 1 **D**11 CAN 84.54 1 19:11 22:07 GL1701 727 2 1 CUMPECTITAS C40 52.97 11:30 11 22 127 1 1 17:47 11:54 64 170 ANB 64 170 1 1 1 EFE 2 - 77 
 177
 2
 2.4
 71.45

 1
 277
 2
 2.4
 11.4

 1
 277
 2
 2.4
 11.4
 277

 1
 777
 0
 1
 11.2
 11.4
 277

 1
 777
 0
 1
 11.2
 11.4
 177
 10.4
 11.7

 1
 777
 0
 1
 11.2
 11.1
 11.1
 177
 10.4
 11.1
 177
 10.4
 11.1
 177
 10.4
 11.1
 177
 10.4
 11.1
 177
 10.4
 11.1
 177
 10.4
 11.1
 177
 10.4
 11.1
 177
 10.4
 11.1
 177
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4
 10.4 CAN 99.52 CONNECTIONS F I LUK KLASLCHULLU I F FR JULIET FFF 2 1 FA OFLTA FR MTEL NHH 1 FF ECHO 44.43 UT 110 DC4 1 1 
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig
 Fig</th C.MAECTIONS C.MAECTIONS 15:10 12:13 MI 201 CCC MI 200 15:10 12:13 MI 201 MP ML 273 14:06 10:11 MI 311 A41 070 05:17 21:54 ML 202 A44 AL 270 1 111 
 T:00
 11:54
 64
 36.48

 1
 7:00
 11:54
 64
 270

 15:01
 11:50
 64
 272
 313

 15:02
 15:35
 44
 273
 312

 11:28
 72:07
 54:1701
 713
 38.44 10:51 12:3V 10+1403 # 3 
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 <thKing Opin</th>
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 <thKing Opin</th>
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 King Opin
 <thK FR JUL IFT CARRA NO 3#]m #J 
 Cit
 A. M.
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200
 M. 200 2 WWN 2 1 22 1242 13296 68 41 404 68 303 004 KKK • â 7:54 0:12 60 11 FAR 95. 43 11-11 CISS 11E-11 1110 1120 1110 1110 1110 FR RUNCPECS FP CHAPTEL UATER 21 6 Lind FA RUAT

4

135

Contra C

AND AND A CONTRACT OF

..............

							•	1. 722225252525525255555555555555	211111111	1. 1. 1. 1. 1. 1
13498 84			1 10 MOTEL		TO JOLIEY	7	•	Th 4160		
					T T L WORLD		ł			
					1 1: 40 10: 4)					
					11:10 15:14			10:11 10:34	61. 802	
	0.000		1 60 6 71 0		1 17:10 19:20		ł	17:22 19:27	\$1 1Cn2	BC 0
	10. 701	127	Cen		1 19:21 21:10	-	-	CONN	COMMEC ? LONS	
	11.3	2 1 21	1 8:03 30:7+	611101 DC* 1 1	TO NOT	AC11245	-	15:52 20:52 6L 101 CC	A ADA CCC	212.12
10:00 22:10	1	127 1			0 8:00 11:47 6L 301 8PP 6L111	. 301 RPB 6L	1 111			
	C 2 8 8 8 1	127			1 19:21 21:29 M	1 131 899 VI	116	FR CHARLIE		3 8
			-1							
		Ĩ	1 13100 22134	61 812 727 2 1	I FA DELTA		000 1 1	4:00 4:41		ŝ
	11.27				CAR	1.14		8:42 10:20	66.1080	
-	- 1	121	Tiont ut f	i a fire i de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la company		M.11.11 057	Ì	1121 22:11		
							•			
			1 FF ALPHA	2 444	91141 40121			24141 44191		100
			1	0.00	10.01 10.01	1				
-		1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2				FT 551 [CF				-
21 20 22 14 I		0 121		: اي	10112 21136	MI103 004				
14.14 00:48	5 T L D D B		1 10:00 13:15 MI 400	1 400 DWG VI 411 1				7101 1141	N1 200	
:							EEE 2 9		81 1000	5
33 MAAND 44		100			L CAR	1.1	-		6L 3302	5
_			. Can	+1.70		CONNECTIONS	-	13:57 14:M	500 13	52
ĺ		0 0 0	1 1:50 8:24	64 41 DCe 1 1	1 12:34 14:31 61	:31 6L 302 0NB 6L	611001 1	18:48 19:27	GL 1002	•••
		•	1 12:39 13:30	2	_		-			
		DC •	-	1	I FR GOLF		665.2.1	FB 10166		L ANM
		00.4	1 F 8 DELTA	000	CAR CAR		-		(). <b>H</b>	
	1,000A	00.0	1 (148		B:36 10:14			12:17 15:31	64.1202	
		0 • JO	1 11:20 12:12	LT 411 DC 0 0	11:34 13:35	RD1214 127				
	40045	004 1	4		1 CONNI	CONNECTIONS	-	F5 JULIET		
1.980	COMME C 7 2 0 4 5		CH3 # 1 1	EEE 2 1	1 16:00 21:25 MT 440	T 440 ANB WT	1116	CAN	1.1	
((0 UIS IN BUIST 01)	510 033	MT 55.1	649	18.47			-	4:30 10:24	641000	•
96551 25596 6L	1107 288	3	1 13:30 19:17	MT 120 0C4 01	FR NOTEL	-		14:14 19:27		00 1
					CAN				- 11	
50 M () 1		1 000	A FR LIMA			PD0012 000	•	TO LINA		
	11.11			16.46	1 10:21 20:25	1 331 000	ŀ			222222
		00 1	1 7:54 A:24	61 11 Dr 0	Ĩ			5.0 A1 PUA		
	64 400	727 0	******		1 8:34 11:47 6L 811 848		ELITT P	CAB	54.37	
Ł	MT 351	0.07	1	1				A:10 31:11	12 13	629
	68 203				1 5 B 5 1 1 0	-		11:47 14:47	;;	
1	CONFERENCES		I CD ALPHA	C			-			
32 46 11:36 61 1131 CCC	1131 666	101115	1 7 64	79.24	A2 45 10:47	611131 009		FR ARAVO		
			1 0:59 10:19	80010 004 1	11:14 15:14		-	CAN	92.00	
F. LCHO		EEE 2	1 11:00 13:21		1 17:14 21:10		-	6:50 7: M		
	Cam  04.49		Ł	i			-			
L ORIAL	CONFECTIONS		ł		1 TO 4110	-		FR CHARLIE		ž
M 22121 1911	M 221 104	BL 201	1 17:32 22:14 61	22:1+ 6L1133 CCC FL11C3 1				CAR	14.90	
			l		I FR ALPHA		1 2 444	11:11 02:01	11 10	1 1 20
F# #GIT901		FFF 2	DAVAS AS 1		_		-			
_ !	i				•	11 100 004	~	F# 1MDIA		
		127 3			90191 66111 1	BL 102 DC9	~			
342 03					COMPECTIVES			11211 4124		
	10.10			20 112 10 10 10 10 10 10 10 10 10 10 10 10 10	9 26 20 24 11 1	11 1 3 1 CCC 01				
14211 1120	C11008	1 0.00								
				•						

136

. inthe

1. 1.

23-1 A.H.J.S._L H.J.J. 1.J. 
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.
 No.</th 240. 16 61 311 0C0 2 1 61 303 327 2 1 1 000 TPT DELTA Canado Cara 91, 50 Canado Cara 91, 50 1 75:95 78:34 00 000 68 -54 1 7:94 12:14 61 011 77 2 1 7:94 12:14 61 011 77 2 - uu 107 107 _ C C C _ 1 -|• 50 1 1 CAF 244.47 50 1 11:07 13:00 60 302 727 2 500 1 1 14:05 20:10 60 603 727 2 R R R CAN 237.59 ..... ł ****** 10:51 15:54 11:48 16:05 14:48 19:84 C.A. FP CHARLIE T'F' DELTA CCC L F P ARAVO 011 # 44 1 FAN 01.24 01.24 1 E 113 ZI 17 Is also state P.16 TOTAL JUNERALIC 11 10 11 F# &CH3

and the second

			FILES USED:			
[KER ] 10 +1+F			FILE LAST 4001FIED		35#3A [4n	UNIVERSE LAST NUNIFIED
1113 354JA180					FA. 0001	f14.0001 f(/01/18 14:1e:7:.98
0109 19 3014 18	: : : ;	10-UTH	MLUF-01 BA/02/12 17:11:07.00 Full-01 Ba/02/12 07:57:55.00			00.7114151 01/10/00 00.71141 01/10/00
		64554-01 #60-11 #44347-01	80/02/12 21:12:15.00 80/02/12 20:27:44.00	40/02/13 07:34:03.00 40/02/13 07:34:03.00		FAR_0001 80/01/18 14:14:37.88 FAA_0001 80/01/18 14:14:37.88

- ¥2	23.6		2.4	4. <b>1</b>	110.7	<b>60.</b> )																																			ļ	ŗ											4137.00	4:27.00
1		2	727 000		707																																					-	Tar	<u>.</u>	83	79							1141 01/10/00	1141 01/10,
7.1017	N	:	-		84.1714																																						8	<b>n</b> -	• •	-0	•	1						
5 5 11		8	0 V C	٥		•																																					2				ູ່		<u>،</u>				F.M. 0001	8
ALT.	21:52	3118	22:00	ä	23:03	ä					_		_			_				_											_												8			<b>4</b> (1			25	s i	3	1	52	2
ž	7		•••	،					•	-		•				n -				•		2	-	•			• •		-		2								2				:	2	- #	~#	•	1						8
•	a a		È Ì																																								5	:="	•	( <b>1</b>	"							K
11	2	3	19	3	ğ	33	1		8		3	ž	33	33		2		3	8	ğ	31	Ì	Ŧ		łŧ	Ī		ä			ł	83		8					3		ł		5	=*	• • •	4 (4	°				3			6
្ទ	F		22	21	22	21	2							56	2	8	68	5	8	-	9	1	2		ĝ						2	21							5	121	2	g	5	2	<b>i</b> n <i>i</i>		•						5	E1/20/00
	00230	ę	38	8: 8	2			3	<b>G</b> 112	1200	113	0CCODI	3		Ę	ē.		1111	8	L1103	¥ ;		5000		000	1000		3	122		1 <u>8</u> 			00000	23 23		202 10		Š		2	Ē	5			<b>-</b>	•						5	Ì
E C	4	1	55	20	5 Z < <	8	2 8 2 4	18 18	4	4	۲	a	•	6 G		3	5 8 < 4	<	8 0	4	80	5 8 5 #	2		15	4	<	8	<b>₹</b>	20	66	<b>E</b> 2	5 8 C A	2	50	t (	58	2 8 2 4	4	5 4 P 4		TAT Y	2							• •	-			8
5 H	4134		88	1	22				1	* 2	8	8	1010		2	0:21		1210		1014	8:0		2			-		00100	8	81	1.2	22		64:01	4 9 2 9			};			18	2				••			1710.0	ŝ	1	; ;		Ċ.
3.		•				•		•	•	•••			•		•	•	• •	•		-	• •		•			•		•	•			• •	-	4			• •	-	4							~ 0	<b>,</b>				Į			11:11
82	-	8		8.3	6.74	8 1		Å	ŝ	5 H	ig		5.10	s s		37.5				1				į		ŝ		74.1	2		00.2	51										Ē		Ð		••	- 2						-	
AL INI	ğ		I							81			8			Ŧ	84	-	13				Ī					_	8			3		8	3	I	Ĭ	įż	8			Ž,	•	=		<b>n</b> ~	- ]						j	<b>0/02/12</b>
	5	-	88	-	37	R	56	10	8	66	2		5	57	2	2	2	2	22	5			ê		_	_	-	5	5	2	10	5	1	5		5	52	16	5	66		2	•	5	<b>n</b>		-}			ā t	a di	•	-	-
	3	5	20	2	14 7	5	:8		3	8	 					02		02		8					2	Â			8		2	ĝ	58	8		Ĩ		ş	8	28	Ì	Ē	•	•		• •	- *	1						ý S
35	5	5	58	5		5	58	15	8	ġ.	13		PLCODA	5 a	13	3	8	8	25	8	2		Ē	5 1	1 8		5	ĝ	5				18	8	8	Ĩ	l	1 8	8		15	ł	•			-0	1		• •			i		đ
		₹' 8'	**	*	8	2:		2	* 8		) 4   }		8	6 -	12	* *	84	\$	4 4 10	(∢  \$	1	3 1	*	« « R 3	2 (4) 7 5	8	\$	8	8		-	** 81	د د 13	8	1	88	8 8	• « {	8	< 8 8 9	18			• •	•	••	Ĵ		= N	2 :	-			
F	3	3	==	=	13	ä	10	1	ä	ä	13		9		ä	Ë.	Ë	ŝ	<u>ä</u>	12		12	2		1	2	Ë.	Ĩ.	Ĩ	Ĩ	19	Ű	Í	é	1	11	Ĭ	11	1	1	1						•	1						
2	•		Ņ		••	e i	ņ	iġ.	•	-	•	•	3	<b>,</b> •	5	-	••	•	•		ņ	n •	•	N 4	•	3	4	••			,	•	: ]	•	•	13	•	2	•	<u>,</u>						••	Ì							
	ł		101.7		102.4	<u>s</u> :	16	:3	8	51	t	8	-	53	12	2			85		ğı			-			_									:£:	33							- 4					28	2:	2			
ž	ł		1		33	3	33	I	8	83		8			Ĩ	ğ		-	I		2		1		•							•											0	• •	• •	• •	• "	'					<b>FILE</b>	
5	-		ÊÈ		66				2	21		2	5	61	1	8		8	22				2		ģ	Ē	61	1		6	1	81	16			12			5		if			"									j	
12	L 312		<b>į</b> į	ļ		12		;¥	000	88 8	Ī	200				101			ē.			200	2	9 / 8		Ř	ž				Č	8 8		117	5 i 6 c	18	2 X	6 6	Ř		13	8		Tel a		52	ļ		ا ا	8 1	5		ij	3
35	4		55	1	88	# i a <	€8	15	2	88	ľ	5	8		58 ( <	4	28 < 0	3	28		44		4				81 01					21			52 44				3	لا تو م د		5 2		71	5	3 Z	50	11				9		đ
	M ,		88		22.20	81			10%	RI Zi		8	3	81		8			81		22		1214		18	8.4					10 10 10	10112		101 27																		[		- ž

- ĮŽ	<b>61.0</b>		13	•			1.0		5	i		ì				2		1.3	3																									Ţ													4:27.40		
2	72) 000	121	88 88	5		8	2		ġ	ţ.		į	1			ŝ		12	ŝ																									-		Tot	21	13	\$!	2	W PALY	7.17		ĪŦ			1101 01/10/00	01/10 1411	
Leir o	A 81.701													2		5																														2' 2'	0 C	• •		• •	5								
TIM.		- 20100	38 22	. 20117		12 12 12	<b>1</b> 8	•						18:12 .		8		12:22 .	£ 22	• •		•	• •			•	• •			•						•					•					2 8	~ ~	• •	n.	- 0		3.6	3	Î¥	\$		52	S	
	88					• • •									-				2.4.3		3												1 42.4													1	2 4 2 4	• •	- -	- •					•			38:03.00	
2	E	èş	12	121	121	T27	ŝ	ŝ	2	È		â	1	Ê	2	1		2	ŝ	2	2	2			i	ŝ	121	È	12	ŝ	2	10	707 KEK	ē.		8	2		ŝ	22	1	ŝ	2			14 17	ā.	• •	-	- 0				ġ	3			0/02/13 07:34	
	A CL 121				B CL 121	D 01 303	B MT 420	10000U 0							B N00022			0 11/00	3			A 11701	7) 51 01			200				3			D 8L1702			DOOM I			198 IN V		2 ji 5 5		A 66 703	TATION P	-	14 13	="	10 CN			BUB				~			à 8	
			88		14:00	14:00	14:00	. 14:10						811.	. 1614	•		8.4	. 17:12	81 <u>1</u>	8141 -	8.2.	17:57			- 18:02	8			42:01 .			9			. 19:00	8		. 19114							12 13	=			9 M		1767.				İ	8		
ł	R	-		81			1						į	9.76 G	2.9	2			1.1	чч 8 2 2 2			4.9 4 1		6.13	9.75	4 8 8			8.9		-		19 19 19			• : ; ;			2						101	2 '	• •		~ •		•	a -	• •				00/02/12 17:11:07	
1		22				ŝ	121	ŝ		6							8		12	2	ŝ				5	727	5		2	200	2	ŝ		2	12	ŝ	5		ł	2		Ē		- <b>5</b>		•		• •	•	• -		Ŕ	Ë	172.	424 4		-	ē	
- 7.184	8			7 ( 8 (				0 M. 272		8						A 0L1132	5		5				A MD0031				A 47 510			D MT 510			A GL #02		22 2	10	9 9 8 4 8 4					19	A BL1703			4		• •		0 0 0 0	I	z	2	<b>-</b>	•	;	1		
	8101			811.		411.	. 11119	10111 J		ħ = .				. 12:17	12:30	. 12: 1				12:52			8000	82	2	- 13:24	8 i i i			<b>1</b>		. 14:07	. 1411	2	8	16:51	11.33						15:24			•	•		•••										
ž	2 2 4				Ń	33.2											n É I													3									8""4							~		- 0 			U-MATURES	X	<b>a</b> 1	<b>3</b> •	•		2		
	1	1					E	224						iF	ŝ	8	81 61	iĥ	į	ê		Ê			i C	2	E	6	-	127	61	ŝ	12	ţ	16	ŝ	ŝ	G	121	8		Ē	ŝ			•	- (	• -		• •	-								
	A 4. 242					3	5	10.50			5 5 5 6	])			A TOOLO							A III 210			15		100 100 100 100 100 100 100 100 100 100		96 IF 6						; § ; d ; d	8			18 18 18 19			<u>8</u>   8						d d		12			<b>a</b> 1	i 2	5	-			
						4100	8	84	I	8	81			8		1				83		2	R 1	8 8	1	1	22		82	91 14			8	# 1 5 i		<b>\$</b>				19	12101	Rio														ļ	ļ	-	ĉ

-

-																																																					-													1	Ŗ
¥Ž			•	•	•					2	2	-	2.2	2			41.0		2	2			g	n X	2																												¥														
_ع ب			3			_									19		E							_																													2		5	:1	8	9:	<u>≏ 8</u>	ş							1
ي و		-	•	•		-											127					2																																						ž	2	23	1			2	
			121 0	-	_				-						22 22																																								81	• •	•	••		٤						3	ŝ
2		¥ S			3	200		~ ~	5				ì	2	2	1	AL 1 701			18		1 m	5	14 5	5																														8'		-	<b>e</b> (	<b>n</b> 0						1	ž	ź
- 		a e	۹ 6	- - 1	۰ ۲	o X		• 5			•	2	2	4		:	8	1	•		•	10	•	a 5	•																														2	- 0		•		N.			2				ž
Ē		1		1		192		202	ġ	ŝ	ŝ	ġ	2	8	1		21126			8		ŝ	ä	Ä	ñ																														81	• •	•	•	• -	7							
	•	•	-	•			•	•	•	•	•	•	•	•			•		• •	••		•	:	•	•••	 			<u>.</u>	:		•	•	•	•••	• •				n	 		• •	•		•	•		•		••				:	:*	-	-	n								
ž			8	ŧ	į	ġ	8	2		Ş	ŝ			3		1			İc	ĥ		2	\$	İ	i	į	;	ŝ	112.	ġ	\$	ŧ	110.	5	ġ	į		ţ	\$	Ż	ğ	ć	ġ		2		÷	F	2	8	¢:	5			:	•		•	• -				_				
1			8	Ę	1	8	8	1	ł	ŝ	8		8	8	19	8				1	ġ	<b>!</b>	2	Ē	1				g	i			ğ	£	81	Į	ł	XXX	ŝ	222	8		8	}	8	8	Ē	1		ł	븮	₿			21			•	n 0	ž	Ē	\$	S			8	
, 8			2	ŝ	23	ŝ	ŝ	121	10	Ş	ŝ		20	2	2	202	2		1	12		5	23	727	1	5		ŝ	727	727	202	ĝ	121	5	2	È		121	ģ	ē	2	2	È	22	2	2	23	202	1	5	2	12			1		•	•	0 -	ł						3	
1.5			ē	_	<u> </u>	_	_			-	200				-			_				Ē				83						_						-	_	ğ		3	5		12	ģ	2		2	£	2	10	1		20		-									3	
Ĩ.			đ	5	8	5	8		1	ła	2		ł	1		i	18	15	1	1	ł		8	*	1	51	5 8	1 8	8	8	1	5	8	i	2	1	1	8	5	Ĩ	8	4	8	5	18	ial		8	5 1		2	5 8	ATIO		1				-	Ľ		••					
E H			8	6 6	12 0				2		1		8		2	1				; #			8	2	1	88	38	12	2	8	1	37	ŝ	4	9 (	F1		8	8	8	< ع	8	ដ			1	ŝ	5	38	8	21			i				-		Į	ŝ	È	Ś	Ś_	: 1		
27 M.			Ë	Ë	ë	ë				Ì			142	1			1					1	ž	3	1	5		2			Ĕ	. 17	. 17:	Ë	Ë		Š	ä		ä	ÿ.	<b>.</b>			ļ		<u>.</u>		Ē	5	2		1		-				_ ^	ş			•	ļ		8	
5,	•	•	•	0	•							•								•			•	-	•				-	ļ	•	•	•			•	44			-		•					•			•	•		ī						- 0								
23		ğ		-																															-			14														55	21	Eİ				10 e	• •	į.		÷		. "	• •	5	
TIVITY TAF		ğ		g	111	8			2		ļ	000	8		I		ł	12	3		1	18	2	ł	2	2		8	I		3	33	8	2	8			1		8		ł								3	81		TIVE					•	- 4	ş	à		ŝ	Î		3	
28		ê	22	727	727	727		ŝ	1	i i	ŝ	ŝ	Î	ŝ	12						121	è	è	ģ	5	61	Ì	Ē	727		5	121	727	2	2		3	Ż	12	ŝ	Ŝ,	õ	-		ìŝ	i î	121	Ş	12	2	<b>ģ</b> ;	2	1					•		8							
25		ğ	â	ş	221	2		ē	2	ļ	ł	ž		ā	į	2	lâ	-			2	11	714	i	į.	8		8	ź		8	ŝ	=	ã	8	2	5	12	8	ŝ	211	101		Į	į	Ŕ	ş	22	Ŕ	3	āi	58	ł						- 0		ļ					3	
35		1	4	8	1	1	1	8			5		5	8		18					8		2	đ	8			5 8 3 4	5		1	d 0	8	8	5		1		8	5	5	Ì	ł	Ī	5 2 		8	8	j	8	51	18	4				'0	• •	• •	NIVN.	я	17	n	2			
Ĭ		ŝ	10.20	2	101	8		8	8	3	8	12	8	8		1				Ŗ	101	5.5		ä	è	8		1	121		8	113	:12	ŝ			; 9		8	1	10	191	1	8	12	8	ŝ	Ŗ	8	2	ŝ	26			• (		•	•	• •	5							
-		2	2	2	2	2	•	:	;;	::			-	;		;;;							3	2	3			12	3	•		. 12	:	3	2:		25	12	:3	1		9				12			i z	1	Z :						•	•	• •	8							
Ŧ		•	3	0.1	2	-									2										*			12	•	•		-	2	2	ž			2		-	2	2	2				1	~		2	-				-	<b>b</b> d	• •	•	• •	Į	2	2:		2			
			i			-	·						_																	_																jġ		_		_	_ '	ŝŔ			-	<b>b</b> d	• •	•	• •	ž						į	FILES
2		H	1	Ē	8	8		ŝ	1	ł			8	ł			1	12	32	1		8	8		<b>Ş</b>		1		ž		1	8	3	8	Ē	1	1	18	1	ł	2			2	1	1			-	-					0	• •	• •	•	• •							i	
1			727								_											ê	•			6													_	_					-	P		_		-		22			į	ĩ				5				_	(	, i	3
"Š		ã	Ĩ	8	9	100		5	Į		100		2	1	į		ļ			1	1		ŝ		ŝ.	8	=		276	8	2	ŝ	ž	8	R		2	19	-	\$	8	ŝ	5	Ĩ		2	ł	8	8	Ř	Żi	R A			ļ	Ĕ,	ير ا	<b>£</b> 1	8 5	Ę	╡	41		5	1	Į	Ĵ
35		8	8	8	4	8							4				19		1 : c <				5		đ B	5 (		12				8	4	5	1	1			8	ŝ	4	۹. ۲				[ <b>#</b> 1 <					<b>z</b> (	5 /1 c 4	3							•	•				1	2	
Ę		ê	121	8. II	1	100	1						200	8		ļ			ļ	1			P		8	8	39	29	R	2	8	8		8	Ē	1	3		8	2	6	È.	ţ,	91	1	3	j	88	8	8	83		Ę													Ş	

Ì.

141

ŝ

TABLE 4.14 PERIOD 1 TRAFFIC DATA

1.0

THE REPORT OF

AAA-CCC AAA-CCC	151.		1-1×	40/4d#	1111	Ļ	101.74	1011	<b>XCAR</b>	KPH/FAY	3 C A B
							VAU X NAV	2			
				1			•				
	2						-117.5	28.08		164.0	
						2	217.1	10-12	3.70	122.7	0
							74.2	A. 75	2.78	39.	ir n
						u a	10.7	50°U	0.0	5.5	0.5
	6 t 0	0.00.0	2.5.2	1170.6	4	ia.			5		10.4
			•				770.7		29		
						5	85 °		11.5		41.4
Ł	( I										
444-UGD	E E 5	7 °0 ° 7	3.36	505 <b>.</b>	4.19	ב ד	#21.ª	5 1. 20	6.23		
	,			:		<b>ور</b>	203.8	23.71			2.0
						5	114.7	1 7. 26	1.78		2.2
							84.5	9.83	3.08		•
11-11	F	1.53.	1.00	1-11	11.0	AL	1112	A 1.94	2. 88	11.	
	•			ί.		3		16.06			0.54
828-FFF	141	. u ° o 9 L	1.66	25.5	12.0	. <u>4</u>	95.2	54.35	1.30	-	0.36
						3	41.4	2	1.53	£	0.5
						6	31.9		0.50		0.1
			Ł					I .			
888-666	2 H 3	201.1	0.79	96.9	0.80	20 20	88.5		3.31	•	
				i		פ	1.1	20.42	.0	10.	0.6
		4				٦	R.C#		0.55	-	00
						5	30.4		7	34.	1.3
			6 T V	1 10 5	-	6					
								в и • с с			
								n •			
1			ſ					12.0			
						•					
111-888	9 4 9	51.5	C. 20	19.0	9.16	а9 		۲.	0.62	14.	
	i I					3	11.6	22.51	0 <b>.</b> # 2	ñ • •	0. 30
				2	5	10.			0. 0	10	
			•	<u>م</u>	•			•			
						7 3					
						5		•	•		
111-11	111	14.1	0.74	0.0	0.16	5	4 41	96.14	11.0		1.0
						5		28.61	0.16	0°2	91.0
		•	:					. X.X. X.X.			
1]]- VVP	5			<b>^</b> ••		٥	•	100.0		•	
MM-444	179	69.A	0.27	12.5	0.10	5		A1.90	1.57	٦.	0. 70
	, 1		1	1			26.	30.10			0.14
		0 - 401		151	4		18.2	10.45		25.7	đ
C I		-	•	-100							
						5		0.00			
								A. 65	1.22	•	
	ĺ		1			ï					
8 8 8 - N X X	517	1094.3	# 2 #	4.047	5 V B	1.	524.4	7 G. MA	7.1.7	. 17 .	6.7n
					:	8 (*	٠	22.17	٩.	-	

	UIST.	PAX/PAY	1101	APD/4CH	1018	5	PAX/DAV		CAR	VPR/NAV	2 C A R
						<b>ر</b> 9	171.2	-		8 ° 8	2.9
						3	130.4		4.7.	67.5	6.15
			1		•			1	•		•
BMB-CCC	153	1692. 1	4.41	258.9	2.15	85	537.4	31.75	6.39	82.2	2.7
						Ē	<u>.</u>	25.67	5.91	64.5	1.6
						3		21.17		5 	
							100.2	10.65	6.57	27.6	2.51
			•				1		•		, ;   '
100- 44×	545	6 ° 1 U H		263.	5			11.05	<b>N</b> 1	347.2	
									<b>`</b> ["		
						5		0.8 0		 	0.71
		1		i		•	- 1				
88 <b>8-EEE</b>	4 1	231.7	0.91	106.4	0.98	<del>ا</del> ہے 	•		2.26	75.6	1.09
			·			3		99° U.N	1.76		2.00
							eí 👘		AF • A	0.0	•>
848-51£	543	87.5	0.35	0.04	14.0	6L	60.7	68.49	0.95	-	7
						5	27.9	11.51	0.36	15.4	0.38
888 - 666		172.1	0.67	77	0.62	08 :	105.7	41-20	3.92	1.74	<b>4</b>
						đ	5	20.40			0. 10
						F		1A.20	0.0	1	1.
888-WWH	250	224.1	94.0	5.8.5			175.5				
	1		•				- , -	<b>1</b>			
						49		2.27	0.04		0.0
HI-HNB	116	104.5	10.41	25.8	14.1	49	105.5	10.001	1.65	24.6	0. 17
				•	;		;	;	•		•
			•	•		5				10.01	
					:			;	•		
			•					19.61			
			•			)			,		
	141		11.0		0.07	<b>a</b> 5	C	100.00	• • •		
139 - <b>2</b> 84	015	47.6	0.19	25.2	0.71 :	: GL	47.4	101.00	0.74	2.2	0. 84
Buit - Rad	207	1.19	1.75	43.4	1.16	<b>a</b> 9	4 4 4	11.11	0.10	1.4	F
						5	15.5	24.44	0.56	8°38	
НЕПХУХ	2076	330.8	1.31	495.6	5.11.2		1.81.4	4 4 <u>4 6</u>	. 17.6-	1.644	11.65
						<b>4</b> (9		• •	1.01	1 4 1	
						ور	R. 86	16.37	<b>48</b> • C	111.0	5.73
						-	14.0	50°5	64.0	34.2	5.5
CCC-AAA	519	7121.1	4.29	1143.7		<del>ا</del>	799.0	11.11		5.164	_
						80		- 12,35 -		-	12.41
						פו	594.7	24.20	A.67	•	
			; ; ;			5		1.04	•1	• • •	5
-14-333	1 4 1			ł							
	1		, , ,	235.5	2.12	2		3 2 . 40	6.5.°	83.3	2. 81

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		0147.					A 4 0 / A 10				
7/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2         1/2 <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>:</th> <th>35 26</th> <th>- 1</th> <th></th> <th></th>							:	35 26	- 1		
277         17.5         17.5         17.5         17.5         17.5         17.5           277         12.5.7         17.5         12.5.7         17.5         5.6.7         77.3           277         12.5.6         5.6.7         77.3         5.6.7         77.3           841         12.6.6         71.6         6.6.7         76.0         5.6.7         77.3           842         14.5         0.44         71.6         6.7.7         5.6.7         77.3           842         14.5         0.45         14.1         0.5.7         5.6.7         71.5           842         14.1         0.51         14.1         0.51         6.6.7         5.6.7         71.5           842         14.1         0.51         74.1         0.57         6.6.7         5.6.7         75.0           742         140.1         0.51         74.1         0.5.7         0.5.7         74.2           740         201.2         0.48         74.2         10.6.7         6.6.9         76.9           740         201.2         0.48         74.2         10.6.7         5.6.7         10.1           740         201.2         14.1         10.5.7						10		****			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$								7.34	•••	6. H 1	
No.         Color         Total of the state         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State         State		e ve			3	. 01	1	10 25			
Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         Product         <		•		•		•		55 M 0	5.67		
with         120.0         6.4.1         1.31         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1         2.4.1 <th2< td=""><td></td><td></td><td></td><td></td><td></td><td>Ua</td><td>284</td><td>19.98</td><td>10.61</td><td>57.6</td><td>5.8</td></th2<>						Ua	284	19.98	10.61	57.6	5.8
Ri $91.7$ $6.85$ $1.23$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ $12.7$ <td></td> <td></td> <td></td> <td></td> <td></td> <td>5</td> <td>120</td> <td>R.47</td> <td></td> <td>24.4</td> <td>2.2</td>						5	120	R.47		24.4	2.2
NB       183.5       0.44       71.4       0.49       11.4       6.7       9.0       1.16       97.1         612       61.4       0.25       34.1       0.13       16       5.7       6.0       7.1         612       61.4       0.25       34.1       0.13       16.1       5.1       2.15       2.15       2.15         772       130.1       0.51       74.4       0.62       80       62.5       61.0       2.19       70.8       81.1         560       201.2       0.51       7.4       0.62       80       2.5       61.1       70.8       70.1       70.9       71.4         561       201.2       0.51       70.4       81.1       10.5       6.1       70.8       71.5       70.9       71.6         561       201.2       0.51       70.4       20.7       70.9       70.9       70.9       70.9       70.9         574       40.1       0.5       50.1       50.1       50.1       50.1       70.9       70.9       70.9       70.9       70.9       70.9       70.9       70.9       70.9       70.9       70.9       70.9       70.9       70.9       70.9       70						e e	97.7	6.85	1.33	19.7	0.4
$u_1$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,2}$ $u_{n,3}$ $u_{n,2}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,2}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,2}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$ $u_{n,1}$	ככה -1 ג ג	8r. 4	143.5		4.17		9. 9	40°C	1.10		
612         61.0         0.37         34.1         0.32         61.4         507         507         507         81           572         130.1         0.31         78.4         0.402         11         67         30.95         293         399           572         130.1         0.51         78.4         0.402         18         0.21         991         399           561         50.17         72.4         0.402         18         11.0.5         593         399         151           561         11.0.5         561         11.0.5         561         11.0         91         141           57.0         201.2         019         726         571         192         111           57.0         201.2         010         11.0         011         111         111         111         111         111         111         111         111         111         111         111         111         111         111         111         111         111         111         111         111         111         111         111         111         111         111         111						13		19.34	2. 15		2.51
0.2 $3.4.9$ $0.2.5$ $3.4.1$ $0.2.3$ $4.1$ $0.2.5$ $6.1$ $2.0.5$ $5.0.5$ $6.1$ $3.0.5$ $6.1$ $3.0.5$ $6.1$ $3.0.5$ $6.1$ $3.0.5$ $6.1$ $3.0.5$ $6.1$ $3.0.5$ $6.1$ $3.0.5$ $6.1$ $3.0.5$ $6.1$ $3.0.5$ $6.1$ $3.0.5$ $6.1$ $3.0.5$ $6.1$ $3.0.5$ $6.1$ $3.0.5$ $6.1$ $3.0.5$ $10.6$ $10.6$ $6.1$ $3.0.5$ $10.6$ $10.6$ $6.1$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10.6$ $10$						19	14.0	R.57	0.22		0.00
N1 $6.7$ $105$ $76$ $61$ $76$ $61$ $76$ $61$ $76$ $61$ $76$ $61$ $76$ $76$ $61$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$ $76$	197- DDD	612	÷.		34.1	. 32 :	~	•	0.89	14.0	1.10
772       130.1       0.51       74.4       0.62       27       0.01       70.4       70.4 $81$ 13.4       10.5       74.1       0.41       0.21       0.41       70.4 $81$ 10.2       0.19       72.4       0.40       51       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4       10.4 <t< td=""><td></td><td></td><td></td><td></td><td></td><td>H</td><td>0.7</td><td>10.54</td><td>÷0*3</td><td></td><td>0.10</td></t<>						H	0.7	10.54	÷0*3		0.10
3/40     201.2     0.73     72.4     0.40     8/1     55.7     46.1     70.6     59.1     70.6       3/40     201.2     0.73     72.4     0.40     8/1     10.2     40.7     10.1     70.4       3/40     201.2     0.73     72.4     0.40     8/1     10.2     40.7     10.1     10.4       3/40     141.1     0.55     55.1     0.46     8/1     70.4     11.4     11.4       3/13     191.6     0.75     58.1     0.48     64     11.4     70.7     27.9     0.15     11.4       3/13     191.6     0.75     58.1     0.48     64     11.4     75.7     50.7     27.2       3/14     10.1     0.10     11.0     0.11     64     10.7     70.7     70.2       3/14     10.2     0.10     11.0     0.11     64     70.6     60.9     70.4       3/18     10.1     11.4     75.7     50.7     50.7     50.7     50.7     27.4       3/14     10.2     0.11     11.1     64     70.6     10.6     70.7     70.4       3/14     10.5     5.4     10.7     10.7     10.7     10.7     70.7 <t< td=""><td>000-000</td><td>\$72</td><td>ş</td><td>1</td><td></td><td></td><td>.4</td><td>40.05</td><td></td><td>16.4</td><td>1</td></t<>	000-000	\$72	ş	1			.4	40.05		16.4	1
31.0       201.2       0.79       72.4       0.40       81       10.2       4.10       39.1         31.0       201.2       0.79       72.4       0.40       81       10.2       4.10       39.1         31.0       201.2       0.79       72.4       0.40       81       82.0       5.05       31.1         31.0       191.0       0.75       59.1       0.46       80       37.1       30.5       31.4         31.1       191.0       0.75       59.1       0.46       81       61       31.5       30.5       31.4         31.1       191.0       0.75       59.1       0.46       81       61       31.5       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6       31.6							5	40.12	0.01		
360     201.2     0.79     72.4     0.40     8 In     110.2     74.10     39.1       314     141.1     0.55     55.1     0.46     80     82.0     57.2     3.05     31.4       314     141.1     0.55     54.1     0.46     80     82.0     57.2     3.05     31.4       314     141.1     0.55     54.1     0.46     80     87.1     39.6     27.0     27.0       315     191.6     0.75     54.1     0.48     61     110.4     61.0     27.1       313     191.6     0.75     54.1     0.48     61     110.4     60.5     71.4       314     101.0     0.10     13.0     0.48     61     110.4     60.5     72.0       216     90.2     0.10     13.0     0.11     61     25.4     101.00     0.40     11.0       714     16.7     16.1     75.1     30.1     60.1     13.0     21.0       714     16.7     16.1     16.2     16.7     101.0     0.40     11.0       714     16.7     16.7     16.1     16.2     16.7     101.0     10.1       714     70.1     16.2     16.1     16						HL H	15.4	11.83	0.21		0. 2
314       141.7       0.55       55.3       0.46       81.9       72.0       15.1         314       141.7       0.55       55.3       0.46       80       57.21       3.05       31.4         315       191.6       0.75       55.3       0.46       81       82.0       7.21       3.05       31.4         315       191.6       0.75       56.1       0.48       61       17.5       7.9       0.13       1.0         315       191.6       0.75       56.1       0.75       31.2       27.0       27.0       27.0         276       8.10       9.5       61       10.5       10.6       0.45       11.6       1.5       1.6       2.5       2.6       4.5       2.7       4.5       2.7         276       8.11       7.5       5.41       10.6       0.45       1.1       4.5       4.5       2.7       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5       4.5	<u>ссс-ннн</u>	340	201.2	0.79		: 09-		16.92	4.10	10.1	10
314     141.1     0.56     55.3     0.46     80     87.0     57.21     3.05     31.4       313     191.6     0.75     59.1     75.9     0.15     1.6       313     191.6     0.75     59.1     0.46     81     87.1     3.05     31.4       314     191.6     0.75     59.1     0.48     54     110.3     1.6     27.0       315     191.6     0.75     59.1     0.48     54     107.00     0.49     1.4       315     27.4     90.10     11.0     0.11     54     75.7     30.3     37.2       316     29.4     0.10     11.0     0.11     54     27.4     107.00     0.49     11.4       714     1.6.7     7.47     36.1     16.7     17.6     2.19     27.4       714     1.6.7     7.41     3.02     272.5     3.87     1.41     3.67     3.12       941     13.1     4.5     7.41     50.7     5.44     1.47     1.60       711.6     3.02     272.5     7.23     7.41     1.76     2.19     27.4       941     95.1     5.41     10.7     2.41     1.76     2.43     2.44							•		44.0		
346     141.1     0.55.3     0.46     80     87.0     51.0     51.0     51.0       313     191.6     0.75     58.1     0.48     61     57.3     59.6     0.15     1.6       313     191.6     0.75     58.1     0.48     61     11.4     61.6     27.3     27.6       314     191.6     0.75     58.1     0.48     61     11.4     61.6     27.5       516     9.5     0.10     11.0     0.11     61     27.4     100.00     0.90     17.0       518     29.4     0.10     11.0     0.11     61     27.4     107.00     0.90     17.0       714     16.7     0.10     11.0     0.11     61     27.4     10.7     10.0       714     16.7     0.10     11.4     0.11     16.1     27.4     11.4       714     16.7     0.11     16.1     27.4     11.4     10.7     27.4       714     16.7     0.11     16.1     27.4     11.4     10.7       714     16.7     0.11     16.1     74.7     5.19     17.4       715     71.6     17.6     17.64     2.19     24.4       711.6						5		20.95			
3n3       191.6       0.75       58.1       0.48       64       37.3       39.87       0.49       27.0         3n3       191.6       0.75       58.1       0.48       64       11.5       75.3       39.31       2.75       27.0         276       8.1       0.10       11.0       0.11       61       75.3       39.31       2.75       27.0         3n8       23.4       0.10       11.0       0.11       61       25.4       10.00       0.40       11.4         7m       16.2       0.10       11.0       0.11       61       25.4       10.00       10.0       11.0         7m       16.2       0.10       11.0       0.11       61       25.4       10.0       10.0       10.0         7m       16.2       16.1       16.1       25.4       10.0       0.40       11.4         7m       16.1       16.1       16.1       16.2       11.4       10.0       10.0       11.4         7m       16.1       16.1       16.1       16.1       10.1       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.0       10.	FFF- 300	18.6	1					10.72	10.1		
b1       0.1       7.9       0.15       1.0         303       191.0       0.75       50.1       0.40       1.02       75.3       27.5       27.6         230       0.10       0.10       9.5       0.10       10.0       0.45       27.6       27.6         370       370.1       0.10       0.10       13.0       0.11       6L       27.5       27.6       27.6         370       23.6       0.10       13.0       0.11       6L       27.5       17.0       9.5       11.4         774       16.2       0.10       13.0       0.11       6L       27.5       11.4       14.7       14.7       14.7       14.0       14.0         774       16.2       14.1       16.2       5.44       10.7       29.6       14.4         548       79.1       14.1       16.0       11.4       10.7       24.4       24.4         543       711.4       3.02       27.2       27.4       16.0       17.6       24.4       24.4         543       711.4       5.02       7.41       7.64       2.19       24.4         543       71.7       5.41       6.64       49.4			2		;			39.67		22.0	
313       191.6       0.75       58.1       0.48       61       11.5       10.46       1.82       35.2         23.6       40.2       0.10       11.0       0.11       61       27.6       9.5       27.6         518       23.6       0.10       11.0       0.11       61       25.4       10.00       0.40       13.0         518       23.6       0.10       11.0       0.11       61       25.4       107.00       0.40       13.0         714       16.7       0.06       11.4       7.7       11       16.7       10.0       14.0         548       793.1       3.10       406.5       3.87       141       306.7       5.87       11.4         548       793.1       3.10       406.5       3.87       17.4       2.19       27.4         548       793.1       3.11.4       3.02       272.5       3.2.2       5.48       1.56       26.3         543       77.6       61       40.4       7.48       5.48       1.56       26.4         543       77.6       61       40.5       7.48       5.48       1.47       2.42         543       77.4       <						-	4.9	2.92	0.15	1.0	0.1
216       02       0.10       4.5       0.0.6       56       50.7       30.3       2.75       72.0         518       254.6       0.10       11.0       0.11       51       25.4       101.00       0.01       11.0         714       16.7       0.06       11.4       0.11       51       25.4       101.00       0.01       11.0         714       16.7       0.06       11.4       0.11       61       25.4       101.00       0.00       11.4         548       793.1       3.10       0.06.5       3.87       M1       30.67       5.80       11.4         548       793.1       3.10       0.06.5       3.87       M1       30.77       5.80       27.4         543       771.6       3.02       272.5       2.26       68       438.0       5.48       15.8       26.8         543       771.6       3.02       272.5       5.81       6.69       27.6         544       47.7       7.71       7.71       7.71       7.76       27.6         544       47.7       7.71       74.7       7.72       27.6       5.81       6.81       27.6         545	-	303	•		- 30		4	4U.69	1.82	35.2	1.1
276     02     0.10     11.0     0.11     6L     25.4     10.00     0.40     13.0       714     16.7     0.10     11.0     0.11     6L     25.4     10.00     0.40     13.0       714     16.7     0.10     11.0     0.11     6L     25.4     10.00     0.40     13.0       714     16.7     0.10     11.4     0.11     6L     25.4     10.00     0.40     13.0       548     793.1     3.10     406.5     3.87     ML     306.4     46.17     40.7       548     793.1     3.10     406.5     3.87     ML     306.4     46.17     47.4       548     70.7     5.44     1.764     2.19     80.6     80.6       543     77.6     51     43.7     54.8     1.56     24.8       543     77.6     51     43.7     61     2.19     24.8       543     77.6     51     45.6     7.28     5.64     1.56       544     14.7     7.41     2.19     7.28     5.64     8.6       545     5.64     7.28     5.64     7.28     5.65     5.65       547     51     4.66     7.66								39.31	2.75	22.0	2.08
9.4       25.6       0.10       11.0       0.11       6L       25.4       101.00       0.69       11.4         144       16.7       0.00       11.4       0.77       14       16.7       11.4       14.0         548       793.1       3.10       406.5       3.87       14       306.7       5.60       14.0         548       793.1       3.10       406.5       3.87       14       30.77       5.60       219.4         548       793.1       3.10       406.5       3.87       14       30.77       5.60       219.4         541       233.9       5.48       13.67       5.60       3.63       25.4         353       771.6       3.02       272.5       2.20       60       438.0       5.60       3.6         553       711.6       3.02       272.5       2.20       60       438.0       7.27       29.0       3.6       24.0         553       713.6       5.60       5.60       3.60       3.6       3.6       3.6       3.6         572       7.27       290.7       2.81       1.81       7.28       3.6       3.6       3.6       4.0       4.0	כנה-ווו	276	ċ	0.16	9 .5	. C.B. :	40	10.00	•	4.5	<b>5(</b> .0
714         16.7         0.06         11.4         16.7         100.01         0.59         11.4           548         793.1         3.10         400.5         3.87         14         300.1         40.17         4.09         715.4           548         793.1         3.10         400.5         3.87         14         300.1         6.17         5.09         715.4           573         744         2.19         7.24         180.7         7.44         2.51         24.4           573         71.4         3.02         272.5         7.26         68         438.0         5.46         159.4         24.4           573         71.4         3.02         272.5         7.26         68         438.0         5.46         34.6         64.6           572         73.7         91.4         1.45         1.00         27.2         5.0           772         157.5         7.81         64         95.6         37.6         94.8         94.8           77.2         14.7         1.45         7.28         7.28         7.28         5.0           77.2         14.1         129.4         9.51         5.95         5.0         5.0 <td>CCC-MMM</td> <td>8 u S</td> <td>25.6</td> <td>0.10</td> <td>13.0</td> <td>••</td> <td>- <b>-</b></td> <td>101.00</td> <td>•</td> <td>- <b>"</b>*</td> <td>0. 43</td>	CCC-MMM	8 u S	25.6	0.10	13.0	••	- <b>-</b>	101.00	•	- <b>"</b> *	0. 43
5/8     793.4     3.10     0.0.5     3.87     HL     30.4     0.17     5.80     24.4       6     74.5     5.0.7     5.80     1.7.6     2.19     72.5       6     100.4     17.64     2.19     72.5     24.8     73.5       5     81     93.5     5.88     1.53     25.8       353     771.6     3.02     272.5     2.26     68     938.0     5.68     158.0       353     771.6     3.02     272.5     2.26     68     938.0     5.69     3.60     89.0       7     1637     5.37     7.61     251.9     97.9     9.9     9.0     27.6       7     18.7     7.51     7.56     5.84     5.44     87.5       7     18.7     7.68     5.93     5.43     5.44       7     18.7     7.66     5.93     5.45       7     18.7     7.66     5.91     6.91     8.7       847     7.17     14.7     7.16     17.5     7.24	CCC-NHA	114	16.2	0.06	11.4	••		100-01	C.59	• 11	1.04
51     241.4     30.77     5.80     147.4       51     711.6     3.02     272.5     2.26     69     430.7     5.46     1.58     27.6       353     771.6     3.02     272.5     7.26     69     430.7     5.46     1.58     24.6       353     771.6     3.02     272.5     7.26     69     430.7     5.46     159.8       353     771.6     3.02     272.5     7.26     69     430.7     7.71     1.02     27.6       272     1437     5.41     5.67     7.81     24.7     7.84     8.7       272     1437     5.41     7.66     9.91     9.91     8.7     8.7       274     447     27.6     130.6     9.91     4.96     27.6       443     47.7     7.17     14.7     7.16     1.02     36.4	000-AAA	846	793.7	3.10	. 66		366.7	44.17	90 T	215.4	1.5
353     771.48     5.02     272.5     5.24     1.56     25.4       353     771.48     3.02     272.5     5.24     1.59     25.4       353     771.48     3.02     272.5     5.24     5.44     159.4       353     771.48     5.02     272.5     5.24     5.44     15.7     24.2       772     1437     5.41     7.41     7.41     7.41     1.42     7.43       772     1437     5.43     7.41     7.41     7.41     7.41       770     7.41     7.41     7.41     7.44     8.47       770     7.41     7.41     7.44     8.47       770     7.41     7.44     8.47     8.47       770     7.44     7.44     8.47     8.47       770     7.44     7.44     8.47     8.47       770     7.44     7.44     8.47     7.44       770     775.4     2.45     5.45     5.45       770     77.5     7.44     7.44     7.44       770     77.5     7.45     7.45     7.44       770     77.5     7.45     7.44     7.44								1	3.00		
353     771.48     5.02     272.5     7.26     58     434.0     5.46     194.6       94     94     94     94     94     94     94       11     95.7     7.51     1.07     27.2     27.2       11     95.7     7.51     1.07     27.2       11     14.7     1.05     27.2     5.0       272     1437     7.85     0.57     5.0       272     1437     7.86     5.27     94.2       272     1437     7.86     5.27     94.2       272     1437     73.66     8.93     5.4       11     10.7     73.67     2.41     8.7       12     130.5     9.51     5.0     7.6       444     70.6     130.5     9.51     9.4       14     130.5     9.51     9.9     7.6						69			2.19	8 2 - 5 2 5 - 6	2.5
RI     231.0     3.40     80.0       RI     251.0     3.41     80.0       Zn2     1437.5     5.0     1.02       Zn2     1437.5     5.0     1.02       Zn2     1437.5     5.0     1.02       Zn2     1437.5     5.0     1.02       Zn2     1437.5     5.0     5.0       R1     239.8     1.05     5.0       R1     239.8     10.6     1.25       R1     130.6     9.5     2.48       R1     130.6     9.5     2.48       R1     130.6     9.5     2.48       R1     130.6     9.5     3.6	888- 000	<b>ب</b>	771.8	3.02		: •2				154.4	
RI     65.7     7.5     7.5     7.5       ZMZ     1437.5     5.07     290.4     2.41     5.4     1.65     0.52     5.0       ZMZ     1437.5     5.47     290.4     2.41     5.4     94.2     94.2       ZMZ     1437.5     5.47     290.4     2.41     5.4     94.2       RM     5.9     6.4     496.4     37.4     94.2       RM     239.4     10.45     1.45     84.2       RM     239.4     10.45     2.45     2.45       RM     130.6     9.51     6.48     27.6       444     231     5.41     5.48     1.55							251	32.90		9.96	2
W1     14.4     1.85     0.52     5.0       Zm2     1437.5     5.40.4     Z.41     GR     406.4     92.4     7.28     94.2       GL     414.1     2.94.1     Z.41     GL     414.1     2.41     8.4       R1     2.94.1     2.94.1     Z.41     2.41     2.42     8.4       R1     2.94.1     1.4.5     7.4     8.4     8.4       R1     1.90.5     1.30.4     9.9     2.4       8.4     1.00.5     1.30.4     9.9     2.0       8.4     1.00.5     1.4     2.4     8.4       8.4     1.00.5     1.4     5.4     2.4						19		16.51	1.07	21.2	0.7
ZHZ TR37.5 5.57 290.4 2.41 5 GP 466.6 57.45 7.28 94.2 GL 414.1 2A.81 6.41 8.7 RT 239.8 16.66 8.93 88.4 RL 191.5 7.5 2.42 35.4 WT 130.6 9.51 2.49 27.6 451 47.5 7.17 19.5 1.6 1.1 531 54.3 0.20 5.6						1	-	5 <b>0</b> - 1	0.52	5.0	
GL 414.1 234.81 6.41 87.1 87.1 87.1 87.1 87.1 87.1 87.1 87.	000-000	2112	1437.5	24.2	290.1	••		37.41	1.26	94.2	1.1
All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All     All <td></td> <td></td> <td></td> <td></td> <td></td> <td>6<b>1</b></td> <td></td> <td>24.83</td> <td>6.47</td> <td>6 . 7</td> <td>2.7</td>						6 <b>1</b>		24.83	6.47	6 . 7	2.7
WI 130.A 9.51 4.98 27.6 WI 130.A 9.51 4.98 27.6 WI 120.A 9.5 0.17 19.16 14 231 54.37 5.34 1A.5 MI 19.8 4.5 0.24 14.5											
444 42° 42° 1° 1° 1° 1° 1° 1° 1° 1° 4° 4° 4° 4° 4° 4° 4° 4° 4° 4° 4° 4° 4°						1.	130.4	15.9		27.6	2
		i	- <b>3</b> - <b>6</b> - <b>8</b>			- 1					
				11.0	14.5	•					

فالأفعانين وسيند

$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1 38484	nist.	ATU/XTO	#101	K PH/UAY		VAN'X PS	1012		* PH/NAY	AC AP
N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1         N1	1 1 - 000	80 4	C • 0 #	0.19	2 · * F	• 58 •	27.7	50.45	C	19.3	0.64
No.         Desc.         =""><td></td><td></td><td></td><td></td><td></td><td><b>1</b></td><td>11.1</td><td>23.04</td><td></td><td>7.9</td><td>0.73</td></thd<>						<b>1</b>	11.1	23.04		7.9	0.73
101         64.4         0.2.5         90.4         0.41         91.4         0.2.5         72.4         0.41         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         10.4         <						₽		20.44	0.14	1.0	0
Ri         12.6         1.6         1.6         1.1         1.6         2.9         0.01         1.1           Ma         132.6         0.45         72.8         0.40         1.1         2.9         0.11         2.1         2.9           Ma         132.6         0.45         11.5         0.50         11.4         0.50         11.3         2.9         2.9         11.3         2.9         2.9         11.3         2.9         2.9         11.3         2.9         2.9         11.3         2.9         2.9         11.3         2.9         2.9         11.3         2.9         2.9         11.3         2.9         2.9         11.3         2.9         2.9         11.3         2.9         2.9         11.3         2.9         2.9         11.3         2.1         2.9         2.9         11.3         2.1         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9 <th2.9< th=""> <th2.9< th=""> <th2.9< th=""></th2.9<></th2.9<></th2.9<>	100 - 666	7.07	•	0.26	÷	. 1	53.7	A 1.4A	1.98	39.8	<b>*.</b> 07
NM       112.5       0.0.2       72.4       0.01       1.4       2.3       0.00       1.1.1         7M       0.13       0.13       1.0       0.13       0.13       0.13       0.13       0.13         945       5x.1       0.22       12.3       0.71       0.7       1.0       0.13       0.14       11.4         945       5x.1       0.22       12.3       0.71       10.7       1.14       11.4         945       5x.1       0.20       11.4       0.71       10.4       11.4       11.4         174       174.1       0.44       11.4       0.71       11.4       11.4       11.4         174       0.44       11.4       0.70       11.4       0.71       2.44       11.2         174       1.14       0.71       1.1       1.1       2.11       1.1       1.1         184       282.4       0.51       1.1       0.51       1.1       0.71       0.43       1.1         184       282.4       0.52       0.52       1.4       1.7       1.4       1.4       1.4         184       184.7       0.11       0.11       1.1       0.11       0.11 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>10.4</td> <td>14.21</td> <td>0.17</td> <td>7.9</td> <td>4 4 0</td>							10.4	14.21	0.17	7.9	4 4 0
9.6 $132.6$ $0.52$ $72.6$ $0.47$ $10.6$ $1.6$ $312.5$ $0.516$ $11.2$ $30.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ $20.13$ <						61	1.5	2.32	0.06	1.1	0.10
64     87.4     87.4     94.0     0.47     27.1       74     87.1     6.15     71.5     0.73     80     84.8     71.5     11.6       949     55.1     6.22     32.3     0.271     80     84.8     71.9     11.6       74     17.6     7.7     7.7     7.7     7.1     7.6     1.1       77     6.4     7.0     7.7     7.6     1.1     2.9     1.1       77     6.4     7.0     7.7     7.6     7.1     2.4       77     6.4     7.1     1.4     7.1     2.4     7.1       77     6.4     7.1     1.4     7.1     2.4     7.1       77     6.4     7.1     1.4     7.2     7.1     7.1       77     6.4     7.1     1.4     7.2     7.1     7.2       71     1.8     7.1     1.4     7.1     2.6     7.1       71     1.8     7.1     1.4     7.1     2.6     7.1       71     1.8     7.1     1.4     7.1     2.6     7.1       71     1.8     1.1     1.1     1.1     1.1     1.1       71     1.1     1.1     1.1	4MH- UUU	548		0.52			53.4	40.19	1.95	•	2.41
$6^{\circ}$ $31.6$ $7.7$ $57.6$ $11.5$ $006$ $11.3$ $006$ $11.3$ $7^{\circ}$ $7.16$ $016$ $11.5$ $007$ $11.6$ $012$ $11.6$ $17^{\circ}$ $17.6$ $012$ $11.6$ $026$ $11.6$ $012$ $11.6$ $17^{\circ}$ $17.6$ $012$ $11.6$ $012$ $11.6$ $24.0$ $17^{\circ}$ $17.6$ $012$ $11.6$ $012$ $11.6$ $24.0$ $17^{\circ}$ $10.7$ $10.7$ $11.1$ $012$ $11.6$ $24.0$ $17^{\circ}$ $10.7$ $10.7$ $11.1$ $016$ $11.2$ $11.7$ $11^{\circ}$ $10.7$ $10.1$ $11.1$ $10.7$ $11.1$ $11.2$ $11^{\circ}$ $10.7$ $10.1$ $10.1$ $10.1$ $11.2$ $11.2$ $11^{\circ}$ $10.7$ $10.1$ $10.1$ $10.1$ $10.2$ $10.1$ $11^{\circ}$ <td< td=""><td></td><td></td><td></td><td></td><td></td><td>19</td><td>47.9</td><td>14.04</td><td>0.75</td><td>24.3</td><td>0. 87</td></td<>						19	47.9	14.04	0.75	24.3	0. 87
744         71.5 $11.5$ $0.271$ 80 $44.4$ $10.60$ $1.74$ $11.2$ $5^{+5}$ $5^{-1}$ $6.23$ $32.1$ $0.271$ $80$ $44.6$ $2.6.3$ $2.6.3$ $176$ $176.1$ $7.23$ $51.1$ $3.5.7$ $0.12$ $4.9$ $176$ $176.1$ $7.26$ $51$ $10.5.1$ $72.2$ $1.1.2$ $177$ $6.4$ $0.764$ $56$ $5.64$ $0.12$ $1.7$ $177$ $6.4$ $0.764$ $56$ $5.64$ $2.61$ $2.61$ $177$ $6.4$ $0.764$ $56$ $6.16$ $7.2$ $1.72$ $177$ $5.64$ $0.764$ $11.14$ $0.94$ $1.72$ $2.64$ $171$ $12.76$ $0.21$ $11.16$ $2.64$ $1.116$ $171$ $12.75$ $10.96$ $111.14$ $0.94$ $1.95$ $1.95$ $171$ $12.92$ $110.16$ $2.64$						8	31.6	23.75	0.49	[.'1	ř 0
5*5         5*1         6.2         12.1         0.271         80         13.6         0.12         1.46         2.4.3           179         176.1         7.6.4         31.6         0.26         64         1.3.7         75.35         1.13         2.4.3           179         176.1         7.6.4         31.6         0.26         64         1.3.7         75.34         1.13         2.4.3           177         6.4         0.70         1.14         0.94         11.1.4         0.94         1.44         7.2.4           187         792.1         1.14         0.94         111.4         0.94         1.91         7.2.9           187         792.1         1.14         0.94         1.92.4         7.2.9         7.2.9           187         792.1         1.14         0.94         1.92.4         7.2.9         7.2.9           187         792.5         61         21.1         7.2.9         7.2.9         7.2.9           187         7.2.5         62.5.5         0.52.5         1.41         7.2.17         2.63         7.2.9           184         185.5         7.4.5         7.2.17         7.4.19         7.2.19         7.2.9	111-200	745	1.8	1	- 11.5	••	1.7.	10.021	1.74	11.2	1.02
174 $7.5$ $17.5$ $0.12$ $0.12$ $0.12$ $1.46$ $7.2$ $177$ $6.5$ $7.6$ $0.16$ $0.16$ $1.6$ $7.2$ $1.46$ $7.2$ $177$ $6.5$ $7.0$ $1.6$ $7.6$ $1.66$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$ $7.6$	111-111	545	55.1	~		. 17.		80.49	1.65	24.0	2.6(
VI         J.9         5.85         0.12         1.9         7.2           174         176.7 $7.64$ $31.6$ $6.28$ $6.1$ $1.46$ $7.2$ 172 $6.4$ $7.03$ $4.1$ $90.7$ $27.48$ $1.46$ $7.2$ 187 $782.4$ $1.14$ $0.94$ $1.1$ $20.61$ $71.16$ $7.63$ 187 $782.4$ $0.73$ $81$ $27.17$ $2.63$ $71.2$ 187 $187.6$ $0.25.6$ $0.53.6$ $0.717$ $2.63$ $71.2$ 187 $187.8$ $0.73$ $81$ $20.4$ $72.17$ $2.63$ $71.2$ 187 $187.7$ $0.73$ $81$ $81.7$ $0.73$ $0.73$ 187 $18.5$ $0.72$ $0.121$ $0.211$ $0.23$ $0.19$ 187 $18.6$ $0.72$ $0.72$ $0.72$ $0.72$ $0.29$ 187 $19.7$ $0.72$ $0.72$ $0.72$ $0.$							1.4	13.61	0.12		0
174     176.1     0.84     31.6     0.26     5.6     136.7     77.31     2.11     36.6       172     6.4     0.03     8.6     0.26     5.6     1.1     0.01     2.6     1.0     8.6       187     289.3     0.07     111.4     0.36     111.4     0.36     111.5     2.6     81.5       187     289.3     0.97     111.4     0.98     11     36.7     10.30     1.33       878     187.3     0.55     0.25     0.52     81.4     192.4     77.17     2.67     81.5       878     187.3     0.57     0.51     111.4     0.96     111     9.7     9.7       878     187.3     0.57     0.51     111.7     0.99     111     17     2.0       878     187.3     0.56     0.11     0.52     81.4     17.7     2.67     1.7       879     0.11     0.26     0.1     0.11     17     0.15     0.1     0.4       876     0.11     0.21     0.11     0.21     0.11     0.21     0.1       876     0.11     0.21     0.21     0.21     0.21     0.21     0.21       876     0.21     0.21						5	3.2	5.85	0.12	1.9	0.1
$k1$ $q_{0.1}$ $2.46$ $1.2$ $4.6$ $1.2$ $6.1$ $1.46$ $1.14$ $91.0$ $1.2$ $6.1$ $2.48$ $1.01$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$ $1.04$	000-KKK	911		0.60		-26		16.11	2.13	2.0	0.0
772         6.4 $7.03$ $4.6$ $7.64$ $5.64$ $7.11$ $2.63$ $7.07$ $7.5$ 187         292.1         1.114         0.96         H1         206.1 $7.11$ $2.63$ $7.07$ $7.5$ 85.5         292.5         1.11.4         0.99         H1 $5.7$ $7.51$ $2.67$ $7.5$ 85.4         18.5 $7.51$ $1.71$ $8.50$ $1.11$ $2.75$ $8.7$ 85.4         18.5 $0.52$ $81$ $85.6$ $1.12$ $0.7$ $0.7$ 87.7         187.7 $7.75$ $0.23$ $0.7$ $0.7$ $0.7$ 87.9 $0.23$ $0.23$ $0.21$ $0.21$ $0.19$ $0.19$ $0.7$ 9.7 $0.70$ $0.7$ $0.7$ $0.7$ $0.7$ $0.7$ 8.7 $0.7$ $0.7$ $0.7$ $0.7$ $0.7$ $0.7$ 8.7 $0.7$ $0.7$ $0.7$ $0.7$ $0.7$ $0.7$						3		22.69	1.46	7.2	
	NAM-DUD	224	4.4	80.0	9.1	: •3•		1 60.00	C.10	0.4	0.14
WIN     #55     289.3     0.97     111.4     0.994     HL     192.4     77.17     2.65     71.5       -011     #55     61     21.4     73.17     2.65     71.5       -011     #5     111.4     0.994     HL     197.4     71.17     2.65     71.5       -011     #5     113.4     0.994     HL     95.5     1.19     0.33     6.7       -011     #5     73.2     0.264     33.1     0.213     10.21     HL     35.6     40.6     1.19       -011     #5     73.2     0.29     33.1     0.213     4.7     0.08     1.19       -011     #5     73.2     0.29     33.1     0.213     4.9     6.7     0.20     2.2       -011     #5     19.5     4.1     35.6     4.6     6.7     0.08     2.2       -011     75.6     5.1     15.6     1.15     15.6     0.15     14.2       -111     75.6     5.6     7.12     14     15.6     10.0     0.19       -111     75.6     5.6     7.7     15.6     0.08     1.2       -111     75.6     5.6     7.6     10.6     1.2     1.1	LEE-AAA	147	- 6		-	: 96.	208.1	71.18	2.83	30.6	0.7
OHH         451         249.3 $0.07$ 111.4 $0.94$ H         192.4 $77.17$ $2.62$ $71.5$ $0.73$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$ $0.72$			1		-		84.7	28.82	3.07	12.4	
-CCC       4.1       95.1       10.40       1.30       10.42         -CCC       4.1       12.5       62.5       0.52       81       66.6       1.13       1.19       7.19         -UUU       4.3       73.2       0.52       81       66.6       77       1.79       27.4         -UUU       4.3       73.2       0.29       33.1       0.21       46.5       77.7       1.18       77.9         -UUU       4.3       73.2       0.29       33.1       0.21       41       27.4       46.7       77.9       1.19       27.4         -UUU       4.3       73.2       0.29       33.1       0.21       41       27.4       46.7       6.7       1.19       27.4         -GU       23.4       0.00       0.4       0.01       11       15.4       10.00       0.32       6.4         -HW       711       15.4       0.01       15.4       0.12       11.5       15.4       10.00       0.19       7.4         -HW       74       15.4       10.00       1.1       15.4       10.00       0.19       7.4         -HW       71       15.4       1.1       15.4	ŁEF -844	454			115. 4	. 94	192.4	11.11	2.62	87.5	2.1
61       21.1 $n.53$ $0.23$ $0.13$ $0.13$ $0.13$ $0.13$ -CCC       0.1       10.5 $0.22$ $0.52$ $0.52$ $0.6$ $1.10$ $37.9$ -UUU       0.1 $1.27$ $0.23$ $0.23$ $0.15$ $0.23$ $0.2$ -UUU       0.1 $1.27$ $0.29$ $31.1$ $0.21$ $0.21$ $0.15$ $0.20$ $21.1$ $0.21$ $0.21$ $0.15$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.22$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.22$ $0.20$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0.21$ $0$							35.7	04 1	1.30	11.2	1.
-CCC WW 187.M $n.56$ 62.5 $0.52$ M $0.65$ $1.19$ $1.70$ $20.4$ 61 9.7 $0.79$ $1.70$ $20.4$ 61 9.7 $0.79$ $1.70$ $20.4$ 61 $9.7$ $0.79$ $1.19$ $2.2$ 61 $9.7$ $0.79$ $1.19$ $2.2$ 61 $3.7$ $4.5$ $1.19$ $2.2$ 61 $3.7$ $4.5$ $1.19$ $1.19$ $1.4$ 61 $3.7$ $4.5$ $0.08$ $2.2$ 61 $3.7$ $4.6$ $1.19$ $1.19$ $1.4$ 61 $3.7$ $4.6$ $1.19$ $1.2$ $1.19$ $1.2$ 61 $3.7$ $4.6$ $1.19$ $1.2$ $1.19$ $1.2$ 61 $3.7$ $4.6$ $1.19$ $1.2$ $1.19$ $1.2$ 61 $3.7$ $4.6$ $1.19$ $1.2$ $1.2$ 61 $3.7$ $4.6$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ 61 $3.7$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$ $1.2$						19	21.1	8.6.8	0.33		0
-010       4:3       72.5       1.70       71.5       4.2         -010       4:3       73.2       0.29       33.1       0.21       41       55.4       40.61       4.2       4.2         -11       5       41       61       4.3       55.4       40.61       0.48       1.19       71.2         -11       27       61       4.3       55.4       40.60       0.32       4.8         -666       580       15.4       0.09       6.8       0.07       1       15.4       10.0       5.3       4.8         -666       580       15.4       0.07       1.1       15.4       100.0       0.32       4.8         -666       580       15.4       0.07       1.1       15.4       100.0       0.32       4.8         -111       25.4       15.4       100.0       0.55       1.4       55.4       10.2       1.4       4.7         -111       25.4       55.4       15.5       15.6       1.5       1.5       1.5       1.5       1.5       1.5       1.5       1.4       1.2       1.4       1.5       1.4       0.7       1.4       0.7       1.4       0.7		818	i	ñ. 56	62. K	: 25 .	86.6	<u>^0.65</u>	1.10	17.9	0.0
-000     4:3     73.2     0.29     33.1     0.23     W1     35.4     49.61     0.48     16.1     0       -010     4:3     73.2     0.29     33.1     0.23     W1     33.7     49.61     0.48     16.1     0       -61     4.7     61     4.7     6.7     0.08     7.2     0       -616     541     1.4     15.4     10.07     0.32     6.8     1.19       -616     541     15.4     10.07     0.13     6.8     1.19       -616     541     15.4     10.07     0.32     6.8     0.2       -616     541     15.4     10.0     0.5     6.8     0.2       -6111     75.4     107.0     0.5     6.8     10.6       -1111     75.6     0.00     3.4     0.01     1.4     0.4       -1111     75.6     0.02     3.4     0.01     1.4     0.4       -1111     75.6     0.00     3.4     0.01     1.5     1.4     0.4       -1111     75.6     0.02     3.4     100.00     0.10     1.4     0.4       -1111     75.6     0.00     3.6     0.1     7.4     0     1.4								12.51	1.70	20 .	1.4
-0000     4:3     73.2     0.29     33.1     0.21     4.1     55.4     49.67     0.48     16.1     9       61     4.7     5.7     4.6     1.19     14.8     14.4       61     4.9     6.7     5.7     4.6     1.19     14.4       61     4.9     6.7     5.0     8     7.2     0       61     5.4     0.07     0.1     1.1     14.4     14.4       61     5.4     0.07     0.1     1.1     15.4     0.32     4.8       600     5.4     0.07     1.1     15.4     107.01     0.5     4.4     0.4       700     9.4     0.07     1.1     15.4     107.01     0.5     4.4     0.4       711     15.4     0.07     5.1     15.1     15.4     107.01     0.5     1.4       711     25.4     0.07     5.1     1.1     5.4     107.00     0.10     7.4     0.7       711     25.4     0.07     5.4     0.01     5.5     1.4     0.4     0.7       711     25.4     0.07     0.12     1.1     15.4     107.01     0.7     1.4       711     26     0.7     0.1<						5	9.7	6.79	0.15	~•	
wit     32.7     ************************************	666-DUD	£ - 4		~	-	.23 :	35.4	•	0.4.0	1.41	00
6L       0.9       0.7       0.08       7.2       0         -616       500       23.4       0.09       0.6       NL       21.4       10.00       0.32       A.8       0         -606       500       15.4       0.09       0.6       NL       21.4       10.07       0.55       A.8       0         -606       500       15.4       0.07       4.1       15.4       100.01       0.55       A.8       0         -111       25.4       0.07       0.1       1       15.4       0.07       0.5       1       0.7       0         -111       25.4       0.02       3.4       0.03       5       1       15.4       100.00       0.10       1       0       0       1       0       0       1       0       1       0       0       1       0       1       0       0       1       0       1       0       0       1       0       1       0       0       1       0       0       1       0       0       0       1       0       0       1       0       0       0       0       0       1       0       0       0       0						13	32.7	4	1.19	14.6	
-FF 290 23.4 0.09 0.8 0.6 1.4 21.4 10.00 0.32 A.8 0 -GGG 540 15.4 0.06 4.4 0.07 : 1 15.4 107.01 0.56 A.4 0 -HHH 711 13.7 0.05 9.7 5.78 1 15.4 107.01 0.56 A.4 0 -HH 25.4 10.00 2.02 14.2 14.2 14.2 14.2 1 -JJJ 55.4 10.00 2.00 2.02 14.2 14.0 0 -HH 35.4 15.7 7.87 26.0 7.57 81 92.4 10.00 0.10 7.4 0 -HH 51 171 7727 7.87 26.0 7.72 14. 92.4 11.01 1.29 45.0 1 -HH 53 101.4 0.40 50.1 0.23 14.1 14.9 11.7 0.59 5.7 0 -HH 51. 10.7 0.57 10.10 1.7 15.0 0.51 15.1 0.5 -HH 51. 10.7 0.5 14.1 0.1 15.1 15.1 0.5 -HH 51. 10.1 1.29 45.0 10.7 0 -HH 51. 10.1 15.0 0.5 11.1 15.1 15.1 0.5 -HH 51. 10.1 15.0 0.5 11.0 11.7 0 -HH 51. 10.1 15.0 0.5 11.0 11.7 0 -CCC 512 48.9 2.1 13.5 0.23 14.1 14.1 0.1 11.7 0 -CCC 512 48.9 2.1 13.5 0.23 14.1 14.1 0.1 11.7 0						9		<b>~</b>	0.08	2.2	0
-GGG 548 15-4 0.06 4.4 0.07 ; 1 15.4 100.01 0.56 8.4 0.7 0 -MMK 711 13.7 7.05 9.7 5.78 : 11 13.6 105.07 6.19 0.7 0 -111 24. 55.4 0.22 14.2 0.12 : 47 55.4 105.00 2.02 18.2 1 -JJJ 55.4 6.2 0.02 3.4 0.03 : 61 6.2 107.00 0.10 7.4 0 -4.4 151 772.7 5.57 7.57 0.23 : 61 6.2 107.00 0.10 7.4 0 -4.4 55.4 15.7 7.57 5.7 15.7 15.7 15.7 15.0 15.7 15.0 10.5 -4.4 55.4 101.4 0.4 56.1 7.47 61 82.5 41.07 1.29 45.0 1 -4.4 55.4 101.4 0.4 56.1 7.47 61 82.5 41.07 1.29 45.0 1 -4.4 55.4 10.7 0.51 15.1 0.23 : 41 25.4 57.42 0.35 15.4 0 -4.4 10.1 25.4 57.42 0.35 15.4 0.30 11.7 0	ttt-FFF	0.2	-	0.09		 9	- FF	10.00	0.32	• •	0.17
	ŁEE -GGG	548	15.4	9 U P O	<b>H.</b> H	••	15.4	100.001	0.54	A. A	0. 77
-111 2°C 55.8 0.22 19.2 0.12 1 4 55.8 100.00 2.02 19.2 1 -JJJ 5°C 6.2 0.02 3.8 0.03 5 G 6.2 100.00 0.10 7.8 0 -11 91.8 29.07 1.57 10.0 0 -11 91.8 29.07 1.51 1.2 0 -11 91.8 29.07 0.59 5.7 0 -11 91.8 25.0 0.59 5.7 0 -10 1.2 98.9 2.18 27.5 0.23 1 1 1.4 10.9 0.51 10.7 0 -CC 012 98.9 2.18 27.5 0.23 1 1 2.1 10.1 0.3 11.7 0		ш	13.8	10.0	1.0	•	13.6	100.001	0.10	1°0.	0.24
-JJJ 559 A.2 0.07 J.8 0.03 EL 6.2 100.00 0.19 7.4 0 -AAA 151 172.7 5.0 1.87 26.0 1.22 A.1 92.4 29.03 1.51 A.2 0 61 30.0 22.04 0.59 5.7 0 -HM 553 101.8 0.40 56.1 5.47 6L 82.5 41.07 1.29 55.0 1 -CC 512 48.9 2.18 27.5 0.23 HL 25.8 57.42 0.35 15.8 0 -CC 512 48.9 2.18 27.5 0.23 HL 25.8 57.42 0.35 11.7 0	-	756	1	~		.12 :	55.4	1 CO. 00	•		
-414 141 172.7 5.87 26.0 7.72 141 92.4 55.69 1.51 14.0 0 -1 91.4 24.0 1.51 1.2 0 -1 91.4 24.0 1.59 45.0 1 -1 14.1 14.0 1.29 45.0 1 -1 14.1 14.0 1.29 45.0 1 -CCC 12 44.0 2.18 27.5 0.23 141 24.1 14.9 0.3 11.1 0	<u> </u>	958	6.2 A	0.07	3.8	•	6.9	100.00	0.19		0.1
		-141	C.571	16.1	29.0	22	<u> </u>	- <b>6 8</b> ° ( 2	72-1	-	_ d
-HMH     51     31.0     22.0     0.59     5.7     0       -HMH     53     101.4     0.40     50.3     5.47     61     80.5     1.29     85.0     1       -CCC     512     44.0     2.18     27.5     0.23     14     25.4     51.3     51.4     0								20.03			
-HHH 543 [11.4 0.41 56.3 9.47 6[ 82.5 41.07 1.29 45.6 HL 14.7 18.9. 0.26 10.7 -CCC 612 44.0 2.18 27.5 0.23 HL 25.8 57.42 0.35 15.8						64	34.0	10.03	0.54	5.7	0.1
AL 14.7 14.9 0.70 10.7 10.9 0.70 10.7 10.7 0.70 10.7 0.20 0.20 15.8 0.12 0.20 0.35 15.8 0.10 11.7 0.12 0.20 0.30 11.1	HHH- 334		111.4	•	•	. 14.	~	41.07	•	۰ <b>۲</b>	1.5
hi2 44.0 0.14 27.5 0.23 : ML 25.4 57.42 0.35 15.8 0.3 fil 14.1 42.56 0.39 11.7 0.7		•	:				14.1	•	0.74	c	0.2
ft 14.1 42.54 0.39 11.7 0.4	+ F F -CCC	612	•••		27.5	23	25.8	57.42	0.35	15.4	6.3
							1 1	42.54	0.39	1.11	0

Material Distriction         Matrix											
Qual $\mathbf{v}_{n,1}$ $\mathbf{D}_{n,1}$		51.	-		ē.	-	A A G		- 1	E	SC AR
Ym         Zm.1         0.08         S.M $n.05$ R.L         0.01         5.1         5.0           7.0 $a.7$ 0.01         5.1         0.05         6         0.11         0.10         5.1 $ar2$ 190.1         0.17         91.7         0.10         5.1         91.3         0.10         5.1 $ar2$ 197.1         0.74         91.7         0.10         5.1         20.3 $ar3$ 197.1         0.79         0.10         5.1         20.4         21.3 $ar3$ 197.5         0.74         82.0         0.66         21.4         21.6         21.7         21.6 $ar3$ 197.6         0.75         87.7         0.265         10.6         21.5         21.9         21.6 $ar3$ 197.6         0.47         82.6         10.7         21.7         21.9         21.9         21.9 $ar3$ 197.6         0.47         25.7         21.9         0.49         21.9         21.9         21.9 $ar3$ 19.6         0.47         0.41         21.4         21.4         21.4	111-110	40.9	45.8	0.18	32.0	••			C.38 0.79	16.9	0.56
$7_{\rm M}$ $h_{\rm M}$ $0.01$ $0.11$ $0.01$ $0.11$ $0.01$ $0.11$ $0.01$ $0.11$ $0.01$ $0.11$ $0.01$ $0.11$ $0.01$ $0.11$ $0.01$ $0.11$ $0.01$ $0.11$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$ $0.01$						ŀ		- 1*	5 C V		
7A         A.7         Q.03         S.1         Q.04         S.1         Q.10         S.1           M2         190.1         1.73         91.7         1.70         0.16         7.13         91.4           M3         197.1         0.74         91.7         1.76         0.16         7.15         90.1         7.15           M4         197.6         0.74         82.0         0.66         7.0         0.46         7.15           972         137.0         0.74         82.0         0.665         71         7.07         0.49         7.0           972         137.0         0.42         91.7         0.53         7.09         0.49         7.2           949         0.40         0.42         91.7         0.42         91.9         11.7           949         18.0         0.10         1.0         5.1         90.0         11.9         11.7           949         18.0         0.11         0.45         10.0         1.01         10.1         11.9         11.7           940         18.0         0.10         1.01         1.01         0.10         11.1         11.1         11.1         11.1         11.1		5	1.47	en • n	E .	•					
87.2       190.1       0.13       0.13       0.11       0.13       0.11       0.13       0.11       0.15       0.11       0.15       0.11       0.15       0.11       0.15       0.11       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15	FFF-NHH	740	4.7	0.03	5.1	••	<b>۰</b>	1	0.10		0.17
GL         MAA         75.54         075         21.5           N1         13.4         7.07         076         21.5         21.5           N1         27.5         7.07         076         21.5         11.7           N1         27.5         7.07         076         21.5         11.7           N1         27.5         7.07         076         11.7         11.7           N1         07         31.0         07         31.7         11.2           9.0         07         31.0         11.7         7.9         07         11.9           9.0         07         10.0         10.0         10.0         10.0         10.0           9.0         0.0         10.0         10.0         10.0         10.0         10.0           9.0         0.0         10.0         10.0         10.0         10.0         10.0           9.0         0.0         10.0         10.0	66-AA	5 H H	• U 6	n.74	1.19	. 76 :			11.5	40.5	4.12
No.         O.14         B2.0         O.06         H1         B4.6         O.06         D.06          th=""> <thd.06< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>- 1</td><td>0.76</td><td>21.4</td><td>0.7A</td></thd.06<></thd.06<>								- 1	0.76	21.4	0.7A
4'1         181.0         0.74         82.0         0.06         RL         55.7         7.9.5         0.06         10.4           572         131.4         0.54         70.5         10.6         0.75         7.06         0.06         70.4           572         131.4         0.54         70.1         55.6         73.01         2.07         2.07         2.07         2.07         2.07         2.01         31.7           783         96.6         0.07         30.4         0.05         11         0.5         1.03         31.7           968         18.6         0.07         30.4         10.4         0.03         10.4         1.03         1.03         10.5         1.03         31.7           968         9.4         0.01         10.4         0.01         10.4         1.03         1.03         1.03         10.5         1.03         10.5         1.03         10.6         1.04         10.6         10.6         1.04         10.6         1.04         10.6         1.04         10.6         1.05         10.2         10.2         10.2         10.2         10.1         10.6         10.1         10.2         10.1         10.1         10.1 <t< td=""><td></td><td></td><td></td><td></td><td></td><td>ā 1</td><td></td><td></td><td>0.61</td><td>21.5</td><td>0.0</td></t<>						ā 1			0.61	21.5	0.0
4'4         186.9         0.74         82.0         0.68         84.0         0.75         10.65         0.69         10.65         0.69         10.66         0.75         10.69         0.69         10.69         0.69         10.69         0.69         10.69         10.69         10.69         10.69         10.69         10.69         10.69         10.69         10.69         10.69         10.69         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61         10.61						B					
BI         55.8         70.4         200         70.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         20.4         2	666-89A		184.9	0.74	82.0		69	1	90.0	30.0	0.75
C         51.4 $7.4.7$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$						ā i			2.08	24.2	2.47
0       37.2       137.4       0.54       78.7       0.65       81       71.7       5.5.7       51.5       31.7         0       747       68.6       0.27       51.2       0.422       180       42.7       5.67       31.7       5.67       31.7         1       747       68.6       0.27       51.2       0.422       180       42.7       5.9       31.4         1       5.6       6.7       5.7       5.1.9       5.0       5.1       5.0       5.1         1       5.6       5.0       0.01       10.4       0.01       8.7       7.9       5.0       7.9         1       5.6       5.0       0.01       10.4       6.0       10.7       8.1       9.0       5.0       5.1         1       5.6       5.0       5.0       5.1       7.1       9.0       2.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0       5.0 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>1</td><td>0.75</td><td></td><td>20-0</td></td<>								1	0.75		20-0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$										•	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	666-CCC	572	5	0.54	<b>.</b>	• • • •	21.	-	2.67	37.7	1.25
1     2*1     3*1     7*1     0*0     1*1       1     2*1     31.4     0.01     10.4     1.03     1.1       1     2*1     31.4     0.01     10.4     1.04     1.0     1.1       1     2*1     31.4     0.01     10.4     1.04     1.0     1.1     0.00     2.1       1     2*1     31.4     0.11     0.5     1.0     1.0     1.0     2.0       1     2*1     0.11     0.5     1.01     1.0     2.0     2.0       1     2*1     0.11     0.5     1.0     2.0     2.0       1     2*1     0.01     129.5     1.01     1.0     2.0       1     2*1     0.01     129.5     1.01     1.0     2.0       1     2*1     0.01     129.5     1.01     1.0     2.0       1     2*1     0.01     129.5     1.01     1.0     2.0       1     2*1     0.01     129.5     1.01     1.0     2.0       1     2*1     0.01     1.2     1.05     1.0     2.0       1     2*1     0.01     1.0     1.0     1.0     1.0     2.0       1     2*1 <td>444-000</td> <td>7.47</td> <td></td> <td></td> <td></td> <td>•</td> <td></td> <td>4</td> <td>02.1</td> <td>11</td> <td></td>	444-000	7.47				•		4	02.1	11	
6         948         18.4         0.07         10.4         0.09         11         4.2         71.93         0.06         7.3           N         5.7         9.4         0.03         10.4         5.0         0.06         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         7.3         5.0         6.0         7.3         5.0         6.0         7.3         5.0         6.0         7.3         6.0         7.3         7.3         6.0         7.3         7.3         6.0         7.3         7.3         6.0         7.3         7.3<			51	•	•		25.		04 0	19.3	
n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n	999-66 E	5 4 8	å		•	: 60			0.54		0.74
9*4     9*4     0.04     5.0     0.04     RD     9*8     10.01     0.02     7.0       745     1715     1.01     8.5     1.01     87     0.17     8.0     75.53     0.29     7.0       745     1715     1.01     8.5     1.01     87     1.03     87.1     0.49     7.0       745     1715     1.29.5     1.01     87     1.51     3.08     47.2       745     1715     1.29.5     1.01     87     0.17     8.0     7.0       745     1715     1.29.5     1.01     87     0.17     8.0     7.0       745     1715     1.29.5     1.01     8.1     9.1     0.17     8.0       745     1715     1.29.5     1.05     1.29     1.0     8.0       745     171     1.29     1.51     1.52     1.0     8.0       746     1.02     1.12     1.52     1.56     1.15     0.1     8.0       740     2014     1.12     1.52     1.56     1.52     1.52       740     2014     1.15     1.12     1.56     1.57     0.01       741     1.1     1.1     1.1     1.1     1.1					4				0.00	2.3	0.04
J       2*1       31.4       0.11       8.5 $n.07$ $R$ $2^{n}$ $3^{n}$ $0.29$ $2^{n}$ a       7*5       175       1.27.5       1.07 $R$ $82.8$ $8.73$ $3.08$ $7^{n}$ a       7*5       175 $1.07$ $R$ $82.8$ $8.20$ $3.08$ $72.5$ a       7*5 $1.75$ $1.67$ $1.67$ $0.82$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ $7.08$ <	666-MMM	5 19		• •		: *0*	•		0.37	о. г	0.51
11 $129.5$ $1.07$ $10$ $23.5$ $0.29$ $2.0$ $175$ $171.5$ $1.07$ $129.5$ $1.07$ $10.7$ $0.69$ $72.6$ $111.5$ $1.07$ $129.5$ $1.07$ $15.7$ $0.42$ $20.6$ $7.0$ $111.5$ $1.07$ $129.5$ $1.07$ $15.7$ $0.42$ $70.6$ $7.0$ $111.5$ $1.07$ $0.52$ $1.07$ $15.7$ $0.47$ $20.6$ $2.0$ $111.7$ $0.52$ $1.052$ $112.6$ $0.52$ $0.52$ $0.51$ $0.52$ $0.51$ $0.52$ $0.51$ $0.52$ $0.51$ $0.52$ $0.51$ $0.52$ $0.51$ $0.52$ $0.51$ $0.52$ $0.51$ $0.52$ $0.51$ $0.52$ $0.51$ $0.52$ $0.51$ $0.52$ $0.51$ $0.52$ $0.51$ $0.52$ $0.51$ $0.51$ $0.52$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.51$ $0.$	666-JJJ	241		0.13		.07 :	25.		4 <b>6</b> -0	6°4	44° 0
A       755       1.07       107       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10			- 1					ļ	0.29	2.0	0.18
RI $43.7$ $75.44$ $0.69$ $31.0$ 574       241.7 $0.42$ $0.42$ $70.4$ 574       241.7 $0.42$ $0.42$ $70.4$ 574       241.7 $0.42$ $0.42$ $70.4$ 574       241.7 $0.42$ $70.2$ $71.2$ 574       201.7 $0.74$ $0.21$ $70.2$ 574       201.7 $0.74$ $0.20$ $0.21$ $70.2$ 574       201.7 $0.74$ $0.20$ $0.21$ $70.2$ 574       201.7 $0.74$ $0.20$ $0.21$ $0.72$ 574       201.7 $0.74$ $0.25$ $11.6$ $11.2$ 574       201.7 $0.74$ $0.25$ $11.6$ $11.2$ 574       201.7 $0.74$ $1.2.1$ $0.10$ $0.5$ $0.5$ $11.6$ 574       201.7 $0.76$ $0.71$ $1.2.1$ $0.71$ $0.71$ $0.7$ $0.7$ 574       201.7 $0.72$ $0.10$ $0.10$ $0.71$ <t< td=""><td>8 8 8 - MMM</td><td>745</td><td>1.</td><td></td><td>•</td><td>. 07 :</td><td></td><td></td><td></td><td>42.5</td><td>÷</td></t<>	8 8 8 - MMM	745	1.		•	. 07 :				42.5	÷
61 $27.0$ $15.7$ $0.42$ $70.2$ $74$ $241.7$ $0.44$ $0.21$ $71.2$ $4.36$ $0.21$ $71.2$ $74$ $241.7$ $0.44$ $0.21$ $71.2$ $1.52$ $10.2$ $71.2$ $74$ $201.7$ $0.44$ $0.72$ $71.4$ $1.52$ $10.2$ $0.7$ $54$ $201.7$ $0.74$ $72.6$ $7.64$ $0.51$ $0.7$ $0.6$ $54$ $201.7$ $0.79$ $11.5$ $0.51$ $0.51$ $0.7$ $54$ $201.7$ $0.74$ $72.6$ $1.640$ $0.51$ $0.67$ $0.7$ $54$ $21.6$ $1.31.7$ $0.51$ $1.64$ $0.51$ $0.51$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$ $0.61$						¢		_ 1		31.0	0.82
749     291, 7.1     9.10     0.20     0.10       749     291, 7     0.94     0.2,4     0.52     0.21     0.29       740     291, 7     0.94     0.2,4     1.52     1.02     0.24       741     10, 7     0.5     0.5     1.5     10, 9       740     201, 7     7, 7     1, 21     1.52     10, 9       61     31, 7     1, 21     1.52     10, 9       61     31, 7     7, 8     0.01     7, 2       61     31, 7     1, 20     0.01     7, 2       54     11, 1     1, 21     0, 5     11, 5       54     11, 1     1, 1     1, 1     1, 31       54     11, 1     1, 1     1, 1     1, 31       54     11, 1     1, 1     1, 1     1, 31       54     11, 1     1, 1     1, 1     1, 31       711     17, 1     1, 1     1, 1     1, 31       74     6     1, 1     1, 1     1, 31       74     1     1, 1     1, 1     1, 31       74     1     1, 1     1, 1     1, 1       74     1     1     1, 1     1, 1       74     1     1				-		ē				20°#	4 C
746     241.7     0.04     62.6     0.52     1.52     1.52     1.52     1.6       61     37.7     1.52     1.52     1.52     1.52     1.6       61     37.7     1.5     0.51     0.57     0.1     0.2       51     61     37.7     1.52     1.52     10.8       61     37.7     0.7     0.57     0.51     0.7       54     0.7     0.7     0.57     0.51     0.7       54     131.5     0.605     6.6     6.6     6.6       54     11.1     11.2     0.51     1.16     11.5       54     11.6     11.2     0.53     1.6     11.5       54     11.6     11.2     0.53     1.6     11.5       711     17.1     0.7     12.1     0.10     11.1     11.1       77     6.8     32.0     77.59     0.50     17.5       77     6.9     7.0     17.1     1.0     1.1       77     7.0     5.1     0.70     1.5     0.1       77     7.0     7.0     1.7     5.1     1.0       77     7.0     7.0     1.7     0.5       70     9.0						- 2			0.26	5.4	0.49
37     10     15     1     1     1     1     1     1     1     1     1     1     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0	MMM-MM8	1 14			0		641		1014	42.0	• • •
61     37.*     15.**     0.5.4     0.5.4     0.5.4       54     20.7     7.2.9     0.01     7.2       54     201.7     7.7     7.4     131.7     0.51     13.5       54     201.7     7.7     54     131.7     0.57     13.5       54     201.7     7.7     54     131.7     0.57     13.5       54     21.6     1.5     51     31.6     1.51     0.57     11.5       54     21.6     1.5     51     13.6     1.5     0.50     11.5       71     17.1     0.7     5.3     64     32.0     77.59     0.50     17.5       71     17.1     1.0     1.1     17.1     1.0     17.5     17.5       71     17.1     1.0     1.1     1.1     1.0     1.7.5       74     1.0     0.10     1.1     1.0     0.1     5.4       74     1.0     1.0     1.0     1.0     1.0     1.0       74     1.0     5.1     0.0     0.1     0.1     0.7       74     10     10.1     10.1     10.1     10.1     0.7							1		1.52	10.8	0.94
54     0.7     7.4     0.01     0.44     0.01     0.44     0.01       54     201.7     7.4     7.4     131.7     0.5     0.5     13.6       54     21.6     1.5     51.6     131.7     0.5     131.5     0.5     131.5       54     21.6     0.5     1.6     51.6     13.6     15.6     13.1     0.5     131.5       54     21.6     0.5     1.6     51.6     0.5     1.6     1.6     11.5       711     17.1     0.7     12.1     0.10     141     1.5     0.50     17.5       711     17.1     0.7     5.1     0.7     5     68     32.0     77.59     0.50     17.5       711     17.1     1.0     11.1     17.1     1.0     17.5     17.5       711     1.7     0.7     5.1     0.74     5.1     1.5     1.0       711     1.0     1.1     1.1     1.0     1.4     1.4     1.0       7     7.0     9.6     1.0     1.0     1.1     1.0     1.0       7     9.0     9.0     9.0     1.0     1.0     1.0       7     9.0     9.0     9.0 <td< td=""><td></td><td></td><td></td><td></td><td></td><td>0</td><td>37</td><td></td><td>0.58</td><td>1.0</td><td>0.32</td></td<>						0	37		0.58	1.0	0.32
3x0     201-7     7.4     7.4     13.5     66.05     6.6     6.4     6.4     6.4     6.4     6.4     11.5     11.5       541     11.6     61     31.6     13.6     15.6     13.6     13.5     0.57     11.5       541     11.6     0.51     0.51     1.51     0.51     1.51     0.51     11.5       541     11.6     0.53     64     84.0     77.59     0.50     17.5       711     17.1     0.7     12.1     0.10     14     17.1     1.51     1.55       711     17.1     0.7     17.1     17.1     17.1     1.5     0.50     17.5       711     17.1     1.0     1.1     17.1     1.0     1.5     1.5       711     17.1     1.0     1.1     1.1     1.0     1.5     1.5       711     7.0     5.1     0.74     5.1     0.5     0.1     5.6       711     7.0     5.1     0.10     5.1     0.5     0.1     5.0       7.0     7.4     7.4     7.4     1.4     1.4     1.4						9	0	•	10.0		10-0
64     30.5     14.12     0.57     14.6       94     110.7     0.44     0.3.6     0.53     5.6     04.0     77.41     1.31     04.0       711     17.1     0.07     12.1     0.10     14.1     1.00     17.5       711     17.1     0.07     12.1     0.10     14.1     1.00     0.62     17.5       711     17.1     0.07     12.1     0.10     14     17.1     1.00     17.5       701     6.4     0.11     10.10     11     17.1     1.00     0.62     17.5       701     6.4     0.17     5.1     0.14     5.1     0.17     5.1       701     6.4     7.4     17.1     1.00     0.62     17.5       701     6.4     6.4     17.4     1.0     1.0       701     7.0     5.1     0.10     5.1     0.1       702     7.4     1.0     1.0     1.0     1.0	אאא-ככל	340	201.7	61.0		: 09.		1	19.4	0.44	94.4
548     11A.r     0.44     03.6     n.53     64     08.0     77.59     0.50     17.5       711     17.1     n.07     12.1     n.10     11     17.1     16.07     12.1       7n     6.4     0.17     5.1     0.410     61     17.1     17.5       7n     6.4     0.17     12.1     0.10     11     16.0     0.62     17.5       7n     6.4     0.17     5.1     0.44     5.1     0.44     5.1     5.1       7n     6.4     0.43     0.11     5.1     0.44     5.1     5.0       51     7.0     5.1     0.64     5.1     7.6     7.0     1.0       51     7.4     7.4     19.4     7.4     1.4     1.0						ه ی			1.16	11.5	0
711     17.1     0.01     17.5     0.01     17.5       711     17.1     0.07     12.1     0.10     11.1     10.00     17.5       750     6.4     17.1     10.07     12.1     0.10     11.1     10.00     17.5       750     6.4     17.1     10.07     12.1     0.10     11.1     10.00     17.5       750     6.4     17.1     10.1     11.1     10.00     0.42     12.1       750     9.0     10.01     5.1     0.14     5.1     0.10     0.11     5.1       750     9.0     9.0     10.05     5.1     0.06     5.1     1.0     0.10     0.10     1.0       70     9.0     7.0     10.0     5.1     0.05     1.0     0.10     0.77     5.0		1 4						1			
711     17.1     0.07     12.1     0.10     17.1     10.00     0.62     17.1       7x0     6.4     0.71     5.1     0.74     6.1     6.4     17.9     0.11     5.1       5r9     9.9     0.10     5.1     0.74     6.1     7.0     6.1     5.1       5r9     9.9     0.10     5.0     0.64     6.0     1.0     5.0     1.0       70     24.4     7.1     0.5     0.1     0.5     1.0     5.0				• 1	n	• • •		1	0.0	17.5	
TAN         Row         U_003         Sel         U_004         GL         G_004         GL         Sel         G_013         G_012         G_013	MMM-Et L	111	17.1	n.07	~	.10 :	17		0.62	~	1.11
5r9 9.0 1.04 5.0 0.64 5.0 7.0 60.37 0.30 0.0 	- dd.de.Huill	141	N. N	50°0	1.2	ŀ		10-101	11.0	1.1	0.17
240 24-4 C.10 6.4 n.C5 : RD 19.4 74.31 0.72 5.0	MMM - 64, 4	8 J 6		0.00	0.5		~	1.04	010	0 ° 0	0.41
2×0 2×*** f.10 *** N.C5; RD 19** 7×*31 0*72 K.O		• :	•					10.0	0.03	.0.1	0.0
	<b>LI.L- NMM</b>	0 v 2	25.0	ر•10	¢. 0	: 5.	0 19		0.72	6° 4	0.42

	0157.	PAX/DAY	LULS	TPP/04Y	1:12	101	P 4X / FAV	1012	<b>BCAR</b>	XPM/DAY	X CAP
			+			4.		1 2.68	0.12	9.6	0° 0
						6 <b>L</b>	2.7	10.0[	0.04	L.J	0.02
111-111	946	1.1	0.29	37.1	0.23	9	0.10	A 3. 26	10.07	22.8	0.77
						-	12.4	14.74	0.45	•••	0.42
TTT-bue	244	51.9	0-20	12.7	n.11 :	ee	51.0	100.00	0.81	1.41	0.43
111-000	144	4.54	0.17	7.8	0.04 :	<b>8</b> 9	42.4	100.00	0.66	1.0	0.26
111-000	215	70.0	0.27	14.5	n.14 :	13	54.4 15.6	77.69	1.98	12.8 7.7	1.17 0.12
33 <b>3-</b> 111	256	43.7	0.17	11.2	: 60"0	1	43.7	-	1.59	11.2	1.02
111-666	518	3.7	10-0	4.1	0.01 :	-	3.2	3.2 100.00	11.0	1.1	0.15
444-IJU	559	104.8	0.42	59.7	0.50	ĉ	53.8	5.0.38	2.00	30.1	3.08
						<u>ן</u> א	32.6	30.57	0.92	11.2	0.45
		1 11 1		4 91	• • •	3	6 161	91 10			
					•	5	1.9.1	18.95	1.79		1.04
ייש-נננ	346	121.9	0.46	17.0	. 91.0	1	67.5	55.42	2.51	26.1	2.67
						ម្ម	C • C •	31.00	0.63	15.5	0.51
								00 11			
000- rrr	545	55.0	0.21	32.2	0.27	ີ ອີ	12.1	77.95	1.60	7.1	2.56
JJJ-EEE	548	1.2	£0°0	¢. •	n.c3 :	ן. פי ד	4 • • • # • •	63.70 36.30	0.17	2.6 1.5	0.23
うううーじし	526	7.6	0.03	£.#	: 60.0	GL	7.4	100-00	0.12	0.4	0.13
<u> </u>	152	36.8	¥I*0	0.7	. 94.0	1	35.6	96.62	1.32	6 ° U	10.0
							1.2	3.36	0-02	<b>6.</b> 0	0.01
HNH-CCC	645	6.15	04.A	5.7	0.05 :	80	21.9	21.9 100.00	0.92	1.2	0.58
K A A A	I v	18.4	0.07	4 . e	n.c7 :	5	18.4	18.4 1C0.00	0.68	A. A	0.7R
Ккк-848	422	57.5	n.22	24.2	0.20	55	*n.* 17.1	70.26 29.74	0.63	17.0	0.50
200-XXX	[ v	218.5	9.45	<b>66.</b> 2	0.55 :	55	179.5	79.03	2.66	51.7	1.11
KKK -0U0	179	175.0	84.0	1.1	9.24 :	55	132.7	75.86	2.07	23.8	0.74 0.64
111 - 444	330	29.9	c1. j	•••	: 90°u	89	0°02	100.00	0.47	•••	0.33
-CLT-HRAN	4.81		- T.I.T	<b>8</b> .3	. 44.0	<b>8</b> 5	19.1	-00-601_x**	0.70		0.78

No. of Concession, Name

						2				TIN THE AND	A CAN
			× 1 • 0	1 * 6 2	19 : 1	2		00*0.1 .*/*		1.1	0.43
333-444	8.5	22.5	• • •	11.0	N.09 : 64	5		22.5 100.0C	0.35	11.0	0.34
	179	51.9	02*0	• •	0.78 : 67	5		51.4 100.00	1.99	6°9	0. 85
198-114	509	67.1	A.26	4.64	49 - 46 ⁻ 4	8			0.75	31.5	1.13
						5	19.7	24.64	0.10	13.4	1. 22
אמא-ככב	R.	25.6	25.6 1.16	18.0	A.15 : 60	es :	11.0	50.72	00	1.0	0.31
						5		12.4 49.28	0.40	6 °¥	0. 11
000-1411	244	12.1	60°0	1.1	n.C7 : 68	e e		12.1 100.0C	0.10	1.1	0.30
KFT-AAA 1674	1674	+13.2 1.62	1.62	495.9	5.77 : 68	9		141.6 34.26	2.21	234.4	8.09
						5	131.7	31.88	2.04	221.8	7.35
						Ę	107.1	25.91	1.46	1 An . 3	
						5	32.4	7.95	1.20	-	5.00
848- XXX	2078		350.4 1.37	728.2	A.04 : RL	2		205.0 59.51	2.79	424.0 10.60	10.40
						64	63.8	1A.0.	0.99	1.161	4.74
						69	61.7	17.62	0.95	124.3	4. 35
						•	1	•	i		

10.000

TRAFFICDETA TD PAK/NAV KPM/NAV	RL 7345.4 4017.A	6L 6407.2 3016.1	64 643 4.7 294A. 9	qD 2664.3 977.7	LT 2742.2 1096.9
10 NULLYail					

----

**** ( ) -***

فللسنا فعلته والانورابية

ي هيروني المحمد المحمد

Farmers.

150

and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s

TABLE 4.15 PERIOD 2 TRAFFIC DATA

ľ.

ALARLIT         LILSL.         PAY/LAN         LILL         PAYLAN         PAYLA												
Own         517         112 Å. $4.20$ 562.4 $4.77$ $6.77$ $79.45$ $6.77$ $79.45$ $6.77$ $79.45$ $6.72$ $77.32$ $79.45$ $77.32$ $79.45$ $77.32$ $79.45$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$ $77.32$	Pr L 7	151	5	÷.	110/		<u>=</u> ]	AN / DAV	101	A C A	APM/UAA	A CAP
61     311.4     9.47     7.44     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.47     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44     3.44	A - b M		126.	•	29			74.	42.54	÷	244.0	£ 4. Q
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$							69	331.4	29.45	4.70	171.5	5. 31
CCC         519         7248.7         7.54         171.4         0.42         60         161         770.7         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5         17.5							5	234.1	20.96	3.67	127.0	0
-CCC       519       2248.7       0.518       1211.4       0.472       56       017.5       75.5       75.6       05.25         -DUU       548       0.15       0.11       0.12       71.5       75.5       75.6       25.6       25.6       25.6       25.6       25.6       25.6       25.6       25.6       25.7       27.6       26.2       11.7       17.5       75.2       27.6       26.2       11.7       77.5       75.6       25.6       25.6       25.6       25.7       27.6       26.7       11.7       11.7       27.5       27.6       27.7       27.6       27.7       27.6       27.7       27.6       27.7       27.6       27.7       27.6       27.7       27.6       27.7       27.6       27.7       27.6       27.7       27.6       27.7       27.6       27.7       27.6       27.7       27.6       27.7       27.6       27.7       27.6       27.7       27.6       27.7       27.6       27.7       27.6       27.7       27.7       27.7       27.6       27.7       27.7       27.7       27.7       27.7       27.7       27.7       27.7       27.7       27.7       27.7       27.7       27.7       27.7			-		;							
											2	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2	<b>m</b> 1		1	1	2	- 1	H87.5	39.47	~	\$78.3	•
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$							f a	7.4.7	4 <b>4 4 4</b>	<b>℃</b> ₹	617.5	0 9
-UUU         588         615.6         3.19         491.4         4.02         1.00         4.11         2.00         4.10         4.10         4.10         4.10         4.10         4.10         4.11         3.20         31.7         1.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10         4.10 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td>:5</td><td></td><td>3.64</td><td>3.1.0</td><td></td><td>9-19</td></t<>							:5		3.64	3.1.0		9-19
			÷		5			-				č
u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1       u1 <td< td=""><td></td><td></td><td></td><td>,</td><td></td><td>4</td><td></td><td></td><td>25.44</td><td></td><td>: ;</td><td></td></td<>				,		4			25.44		: ;	
Ge     7a.n     9.1     1.0     94.0							5		10.02	1.00	2.04	
							<b>a</b> 9		9.16	1.09	•	1. 4
LT       LT       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LS       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT       LT <thlt< th="">       LT       LT       <thl< td=""><td>-AA-EEE</td><td>111</td><td>256.6</td><td>0.98</td><td>51.7</td><td>11.</td><td>a a</td><td></td><td></td><td>- i •</td><td>ە ' بىر</td><td>0.4</td></thl<></thlt<>	-AA-EEE	111	256.6	0.98	51.7	11.	a a			- i •	ە ' بىر	0.4
							5		•		÷	0.54
w1       w2       0.17       90.7       w1       31.4       1.51       1.51       0.49       0.73       0.41       0.47       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0.41       0	111-FFF	1-1	168.4	0.64	25.5	12.			1.0	1	14	0
GL     31.4     18.4     0.40     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     0.41     <				•	•				× ۲	1	-	
-646       482       201.0       0.71       Ye.Y       0.79       H1       11.0       20.40       0.66       27.9       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0							5		- <b>- 6</b>			0.16
HI $43.4$ $71.56$ $0.666$ $77.96$ $0.666$ $77.96$ $0.666$ $77.96$ $0.666$ $77.96$ $0.666$ $77.96$ $10.66$ $11.6$ $11.6$ $0.666$ $11.6$ $0.666$ $11.6$ $0.666$ $11.6$ $0.77$ $11.6$ $0.77$ $11.6$ $0.77$ $11.6$ $0.77$ $11.6$ $0.77$ $11.6$ $0.77$ $11.6$ $0.77$ $11.6$ $0.77$ $11.6$ $0.77$ $11.6$ $0.77$ $11.6$ $0.77$ $11.6$ $0.77$ $11.6$ $0.77$ $11.6$ $0.77$ $11.6$ $0.77$ $0.77$ $0.77$ $0.77$ $0.72$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$ $0.72$ $0.77$ $0.77$ $0.72$ $0.77$ $0.72$ $0.77$ $0.72$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$ $0.77$		G.		•	- 0	. 79	x	61.7	14.54	1.25	_	4 - 1
HI $41.0$ $20.40$ $6.51$ $120.5$ $0.99$ $117.1$ $71.31$ $14.91$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.9$ $0.37$ $14.2$ $0.37$ $14.2$ $0.37$ $14.2$ $0.37$ $14.2$ $0.37$ $14.2$ $0.37$ $14.2$ $0.37$ $14.2$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$ $0.37$								43.1	21.56	0.66		0. 69
<b>1</b> $3$ $1$ $3$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$ $1$							Ŧ	c.14	20.40	C.57		0.51
-HHH 755 150.5 $6.h1$ 120.5 $0.99$ ; HD 117.1 77.3H 4.43 8A.4 8 6L 23.4 14.91 0.37 14.0 0 6L 23.4 14.69 0.75 14.0 0 -JJJ 559 96.0 0.37 51.0 0.17 69 96.1 0.44 16.7 0 -JJJ 559 96.0 0.37 53.7 0.44 20 $B4.A$ 79.61 0.44 16.7 0 -JJJ 559 96.0 0.37 53.7 0.44 20 $B4.A$ 79.61 0.13 7.9 0 -HH 12.7 0.03 5.4 0.05 20 $B1$ 8.4 66.33 0.13 7.9 0 -HH 12.0 34.7 0.13 11.4 0.74 56 36.7 160.05 0.49 11.4 0 -HH 130 34.7 0.13 11.4 0.74 56 36.7 160.05 0.49 11.4 0 -HH 179 136.5 24.3 0.70 15 11 24.3 73.61 1.10 11.9 0 -HH 179 136.5 24.3 0.70 11 24.3 73.61 1.10 11.9 0 -HH 179 136.5 24.3 0.70 11 24.3 73.60 1.41 0.73 0.9 0 -HH 100.0 0.41 1.47 0.13 12.0 0.01 7.3 0 -HH 179 136.5 24.3 0.70 11 11.0 72.61 1.0 0 -HH 179 136.5 24.3 0.70 11 11.0 72.61 1.0 0 -HH 179 136.5 0.01 1.41 0 -HH 170 25.24.3 0.70 1.41 0.14 0.00 0 -HH 100.0 0.01 1.41 0.00 0 -HH 100.0 0.00 0.00 0.0 0 -HH 100.0 0.00 0.00 0.0 0 -HH 100.0 0.00 0.00 0.0 0 -HH 100.0 0.0 0.0 0 -HH 100.0 0.0 0 -HH 100.0 0.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.0 0 -HH 100.							5		٠.	Ξ.	:	1.3
6L $23.4$ $10.69$ $0.37$ $14.0$ $0$ $-111$ $34$ $54.9$ $0.22$ $21.0$ $n.17$ $60$ $84.7$ $79.61$ $0.42$ $4.3$ $0$ $-JJJ$ $549$ $0.22$ $21.0$ $n.17$ $60$ $11.6$ $27.9$ $0.42$ $4.3$ $0$ $-JJJJ$ $549$ $0.37$ $53.7$ $n.44$ $21.6$ $11.69$ $0.76$ $10.4$ $9$ $0$ $-JJJJ$ $549$ $0.37$ $5.4$ $n.65$ $54.6$ $n.43$ $32.7$ $0.43$ $0.13$ $7.9$ $0$ $-11L$ $370$ $34.7$ $0.13$ $11.4$ $n.70$ $54.7$ $0.13$ $7.9$ $0$ $-11L$ $370$ $34.7$ $0.13$ $11.6$ $0.13$ $7.9$ $0$ $-11L$ $370$ $34.7$ $10.11$ $11.6$ $0.13$ $7.9$ $0.13$ $7.9$ $0.13$ $7.9$ $0.13$ $7.9$ $0.01$ $7.9$ $0.01$ $0.01$ $0.03$ <td>1</td> <td>755</td> <td>159.</td> <td>6.65</td> <td>20.</td> <td>.94</td> <td></td> <td>17.</td> <td>7 3. 34</td> <td>٩.</td> <td>ď</td> <td>٢.</td>	1	755	159.	6.65	20.	.94		17.	7 3. 34	٩.	ď	٢.
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$							61		14.91	<i>.</i>	÷	0.59
-111 349 56.9 0.22 21.0 0.17 66 45.4 70.61 0.64 15.7 0 -JJJ 559 96.0 0.37 53.7 0.44 11.6 11.6 7.1 0.17 7.2 0 -JJJ 559 96.0 0.37 53.7 0.44 11.7 11.64 0.17 7.2 0 -JL 55 7.6 11.5 11.64 0.17 7.2 0 -JL 370 34.7 0.13 11.4 0.74 56 34.7 160.05 0.49 11.4 0 -IL 370 34.7 0.13 11.4 0.74 56 34.7 160.05 0.49 11.4 0 -JL 24.7 75.1 11.0 11.4 0.1 15.7 0.17 7.9 0 -JL 24.7 75.1 11.1 11.0 11.4 0.13 7.9 0 -JU 179 156.5 24.3 0.70.1 11 24.7 75.1 11.0 0.17 7.9 0 -JU 179 156.5 24.3 0.70.1 11.6 70.4 1.7 0.18 7.9 0 -JU 1116 70.4 1.4 1.4 0.0 1.4 1.10 0.17 7.9 0 -JU 10.4 1.4 1.4 1.4 0.1 1.4 0.4 1.4 0.4 1.4 0.4 1.4 0.4 0 -JU 10.4 179 156.5 24.3 0.70.1 11.6 70.4 1.4 0.0 1.4 0.4 0.4 1.4 0 -JU 10.4 10.4 1.4 0.0 1.4 0.4 1.4 0.4 1.4 0.4 1.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0							9		11.69	~		•
-JJJ       55.7       0.44       11.6       27.35       53.7       0.44       11.6       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2       11.2	11- VV	٠.	÷	਼	-	.17	5	8 ° 4 8	79.61	0.64	17	0.52
-JJJ 559 96.0 0.37 53.7 0.44 : Pf 64. 11.2 11.64 0.17 5.2 0 -14.4 4.1 12.7 0.05 5.4 0.05 15 4 4.4 66.3 0.13 7.9 0 -14.4 4.1 12.7 0.13 11.4 0.74 56 36.7 160.05 0.49 11.4 0 -14.1 310 34.7 0.13 11.4 0.74 56 36.7 160.05 0.49 11.4 0 -14.1 310 34.7 0.13 11.4 0.74 56 36.7 160.05 0.49 11.4 0 -14.1 179 154.5 5.24.3 0.20 14 0.41 45.45 0.68 11.41 0 -14.1 179 154.5 5.24.3 0.20 14 0.41 45.45 0.68 11.41 0 -14.1 10.1 0.01 0.3 0.81 1.4 0.7 0.13 7.3 0 -14.1 10.1 1.4 0.01 0.3 0.01 0.3 0.3 0 -14.1 10.1 1.4 0.01 0.3 0.01 0.3 0.3 0.0 0.01 0.00 0.00	•							11.5	27.34	0.42	F. •	0.39
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		<u>د</u>		•		44.		8 ° 79	FR.31	1.2.1	~	4.72
-•••••••••••••••••••••••••••••••••••••							5	11.2	11.04	0.17	4.2	0.21
LIL     34.7     0.15     7.0     0     7.0     0       -1LL     34.7     0.13     11.4     0     0     11.4     0       -1LL     1310     34.7     0.15     11.4     0     11.4     0       -1LL     1310     34.7     0.13     11.4     0     11.4     0       -1LL     1310     34.7     0.13     11.4     0     11.4     0       -1UL     131     17.2     11.4     0     11.4     0       -1UL     131     17.4     11.4     0     11.4     0       -1UL     17.4     17.4     11.4     0     11.4     0       -1UL     17.4     17.4     11.4     0.11.4     0     11.4       -1UL     17.4     14.4     0.14     11.4     10.4     14.4       -1UL     11.4     12.4     7.4     14.4     10.4     14.4       -1UL     11.4     12.4     7.4     14.4     10.4     14.4       -1UL     11.4     12.4     7.4     14.4     10.4     14.4		٠.		5 J J J		÷.			46.33	0.13		7
-111 310 34.7 0.13 11.4 0.04 15 34.7 150.05 2.49 11.4 0 			:	i		- i	F.		31.67	0.15		
	11-44	910				ŗ.	9	34.7	0.03	•	11 .4	۹ <b>٤.</b> 0
1     24.7     71.87     0.81     7.6     0       24.7     134.7     0.87     2.4.3     0.70     11.4     0       24.7     134.7     24.4     1.4.1     0     14.4     1.4.1     0       24.7     14.7     14.4     1.4.1     0.4.4     1.4.1     0     1.4.1     0       24.7     14.7     14.7     14.7     14.7     14.7     14.1     0       24.7     14.7     14.7     14.7     14.7     14.7     14.2     14.1	-Had-JHI	184	1.101		15.2	4	5	2.11	41.47	ī.1 r	11.5	0.36
WWW     174     13.4.7     0.57     24.3     0.7.1     0.1.4     0     1.46     1.4     0       b1     40.4     24.4     24.4     1.4     0     1.46     1.4     0       b1     40.4     24.4     24.4     24.4     24.4     2.5     0       b1     1.4     1.4     1.4     1.4     1.4     1.4     1.4       b1     1.4     1.4     1.4     1.4     1.4     1.4     1.4       b1     1.4     1.4     1.4     1.4     1.4     1.4     1.4       b1     1.4     1.4     1.4     1.4     1.4     1.4     1.4       b1     1.4     1.4     1.4     1.4     1.4     1.4     1.4       b1     1.4     1.4     1.4     1.4     1.4     1.4     1.4							5	24.3	23.82	0.87	3. 6	0. 31
0 1.4 1.3 0 0 1.4 1.4 1.5 0 0 1.4 1.5 0 0 0.01 1.4 1.5 0 0 0.01 1.4 250.3 0 0 1.4 1.4 250.4 0 0 1.4 1.4 250.4 0 0 1.4 1.7 188.5 0 0 1.4 1.7 188.5 0 0 1.4 1.7 188.5 0 0 1.4 1.1 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4	Maatzee.	. 641.	- MA		;	02	1		-68.8°	· -	. 11.1	0.2
64 31.0 72.87 3.64 5.64 5.4 5.5 0.03 0.03 0.3 3 69 1.4 1.35 0.03 0.3 3 14-311 16 ⁹⁴ 3.66.7 1.47 6.50.5 5.42 5.67 134.6 70.46 7.18 259.5 8 64 111.6 76.94 1.72 188.5 6 64 87.4 22.66 1.21 147.0 3							1	¥ ° č #	29.96	1.46		0.45
69 1.4 1.5 0.03 0.3 0.3 0 14-51x 16 ⁹⁴ 366.7 i.47 650.5 5.42 5.67 154.0 70.46 7.18 259.5 8 61 111.6 76.94 1.72 188.5 6 61 81.4 22.60 1.21 147.0 3							ĩ	1.1	78.95	0.4 H	•	0.11
иа-вих 10°4 Эрл.я 1.47 лоп.5 я.42 : GP 124.7 90.не 7.1К 259.5 В 14.111.6 76.94 1.72 188.5 6 не 87.4 22.66 1.21 147.0 3							<b>6</b>	1.1	1.35	10.0		0.0
HL 87.4 72.6 1.21 147.0 3		•	566.3	•	5° U 54	e	49		1 H * DE	-		8.07
87.7 22.6C 1.21 147.U 3		} ; ;	:	!		1	3	11.	70.04	5	e e	1
										•		

ALC: NO

All and the second

275.6 12.25.6 12.25.6 12.25.6 12.25.6 12.25.6 12.25.6 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25.7 12.25	BHR-IL		PEX/RAY	31.15	ā	-		VAR/KIG	1-21-4	RCAH	KPM/NAY	E CA P
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		15	107.1		57.	20		535.4	40.64	7.44	274.8	1.1
Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image         Image <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td>ê</td><td>1.045</td><td>22.34</td><td>3.41</td><td>124.4</td><td>3.8</td></th<>							ê	1.045	22.34	3.41	124.4	3.8
No.     119,1     119,1     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10     1,10							J	1.011	15.74	2.61	84.0	2.9
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$							5	•	11.04	8 4 . 9	1.10	5
CUL         171         0.11         7.16         6.11         7.19         7.19         7.19         7.19         7.19         7.19         7.19         7.19         7.19         7.19         7.19         7.19         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7.11         7							2	-	1.10	•		•• 0
HL         HOL         CCC</td> <td>1.1</td> <td>1721-3</td> <td></td> <td>765.4</td> <td>1</td> <td></td> <td>21.</td> <td>30.30</td> <td></td> <td>79. 4</td> <td>2.49</td>	BHH-CCC	1.1	1721-3		765.4	1		21.	30.30		79. 4	2.49
GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL         GL<							Ч Н	40204	21.55	5.64	62.0	
No.         J.M.         Zul.         J.M.          th="">         J.M.         J.M.         J</thj.m.<>							GL	401.1	71.31	6.15	61.4	2.0
NI         ITA.A         IJA.A         IJA.A         IJA.A         IJA.A         IJA.A         IJA.B         0.41         ZA.J           -UUU         JYJ         JAA.A         JALI         Z.40         GL         IVA.A         Z.41         Z.40         GA         J.20         J.40         J.41         Z.41         Z.40         L         L         Z.41         Z.40         Z.41         Z.40         Z.41         Z.40         Z.41         Z.40         Z.41         Z.41         Z.40         Z.41         Z.40         Z.41         Z.40         Z.41         ></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>C a</td> <td>214.5</td> <td>12.40</td> <td>6.12</td> <td>32.6</td> <td>5.2</td>							C a	214.5	12.40	6.12	32.6	5.2
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$							3	174.4	10.38	۰.	27.3	2
-Etc.	664-000	111	100.4	1.14	1 176	2		•	-	•  •	1	
HL         194, 7. $3$ 7. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$ 9. $3$						2				.8.6	1 • • • 1	ř
-ftt       -7.4       -6.7       -7.4       -6.7       -7.4       -6.7       -7.4       -6.7       -7.4       -6.7       -7.4       -6.7       -7.4       -6.7       -7.4       -6.7       -7.4       -6.7       -7.4       -6.7       -7.4       -6.7       -7.4       -6.7       -7.4       -6.7       -7.4       -6.7       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4       -7.4							<b>ب</b>	1 96	4 . A . A	00.0	69.2	2.0
-fth       -51.7       0.440       100.4       0.471       61       15.4       0.21       72.1         -fth       55.3       87.4       0.47       61       57.6       0.47       2.31       72.2         -fth       55.3       87.4       0.40       100.4       0.47       51.7       0.47       2.21       72.2         -fth       55.3       61       57.6       61.1       57.8       6.41       10.49       31.4         -fth       74.7       6.41       74.0       6.41       74.0       0.41       22.4         -fth       74.0       0.47       61       74.0       74.0       0.41       22.4         -fth       74.0       0.41       52.7       74.0       0.41       23.4         -fth       74.0       0.41       52.4       74.0       0.41       24.0         -fth       24.1       17.0       64       17.0       24.0       14.1         -fth       24.1       174.0       174.0       0.40       14.1       14.0         -fth       24.1       174.0       174.0       14.1       14.0       14.0       14.0         -fth       24.1<							ŗ	191	1.0		64.2	1.0
-ELL       #53       231.7       0.40       100.4       0.47       1       151.7       2.21       72.2       17.20       0.47       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0       14.0							3	•••		0.21	2.1	0
with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with       with	BMM-EEL	455		0.40	ě	. 8.7		4 4			•	
The       513       87.4       0.313       46.3       0.40       16.0       31.4       34.1       34.1         The       513       87.4       0.313       46.3       0.40       61       50.4       31.49       0.41       14.0         The       177.1       0.46       74.7       0.41       810       90.1       52.3       3.41       39.1         The       52.7       70.33       0.47       72.9       0.46       14.0       14.0         The       52.7       70.31       20.40       17.2       0.46       14.0       14.0         The       57.0       173.6       74.9       27.9       0.47       14.0       27.1       27.1       27.1       27.1       27.2       27.1       27.3       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27.4       27							1					
573     87.4     0.41     0.41     0.41     0.41     0.41     0.41     10.40       -566     4     175.1     0.40     51     0.40     51     74.9     0.41     0.41       -566     4     175.1     0.40     51     0.40     51     74.9     0.41     10.40       -666     4     175.4     74.9     0.41     22.7     70.31     22.7       -111     240     220.0     0.40     57.0     0.41     58.4     0.01     27.9       -111     243     83.9     0.47     59.4     74.9     0.63     10.6       -111     243     83.9     0.47     59.4     74.9     0.63     10.6       -111     243     10.41     59.4     7.8     0.01     27.9       -111     243     10.41     51.1     7.8     1.9     7.9       -111     243     10.41     51.1     7.8     1.9     7.9       -111     243     10.41     51.4     11.9     2.7     2.4       -111     243     0.41     1.1     51.4     0.41     1.1       -111     43.4     0.41     1.4     1.1     1.4     1.4     1.4 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>i</td> <td>•</td> <td>0 (</td> <td></td> <td></td> <td></td>							i	•	0 (			
-111       543       87.4       0.43       0.40       51.7       51.4       31.49       0.41       10.44         -655       41       17.3       0.41       74.7       0.41       17.3       0.41       17.3       0.41       17.4         -655       41       17.3       0.41       74.7       0.41       17.3       0.41       17.3       0.41       17.4         -655       41       17.4       51.7       74.9       0.65       11.4       27.2       17.3       0.41       17.4         -111       244       270.0       0.61       11.1       24.7       24.6       0.61       11.4         -111       244       27.3       161       17.4       74.9       0.65       11.7       27.5         -111       244       27.3       161       17.4       78.1       10.6       11.7       27.5         -111       244       27.3       161       17.4       78.1       1.7       27.9         -111       27.3       161       17.4       78.1       10.6       1.1       27.4         -111       27.3       161       17.4       78.1       17.4       18.1 <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td>5</td><td></td><td>() •L 1</td><td></td><td></td><td></td></th<>							5		() •L 1			
AL       2%.6       31.0       0.01       22.3       3.01       10.0         -666       414       177.1       0.60       74.7       0.61       810       90.1       22.3       3.01       3.01       30.1         -666       414       177.1       0.61       810       90.1       52.5       3.01       20.4       27.0         -0404       27.0       0.47       911       173.6       78.97       0.07       12.0         -0404       270       0.47       61       117.6       0.65       11.9       27.5         -0414       273       16.1       17.4       78.97       0.07       1.4       27.5         -0414       273       16.1       17.5       69       17.4       27.5       1.4       27.5         -0414       273       10.17       69       17.4       17.4       17.4       17.3         -0414       273       11.1       17.4       17.4       17.4       17.4       17.3         -041       27.5       11.1       17.4       67       11.4       17.4       17.5       17.4       17.5         -041       17.5       1175.7       0.41	048-FFF	33	87.4	1.	9	9		9.76	64.11	0.89	31.9	
-666     4.4     172.1     0.46     74.7     0.61     71     92.7     93.9     9.11     30.11       -1001     270.0     0.47     91     173.6     74.92     0.64     17.0       -1011     240     220.0     0.48     57.0     0.47     81     173.6     74.92     0.65     17.0       -1011     244     61     41.1     1.8.0     0.007     1.4       -1011     244     63.9     0.17     5.0     0.071     27.0       -1011     244     63.9     0.17     5.0     0.071     1.4       -111     244     63.9     0.17     5.0     0.071     1.4       -111     244     813.6     0.17     5.0     0.071     1.4       -111     244     813.6     0.21     29.1     1.4     27.9       -111     244     813.6     0.10.6     1.4     27.9       -111     243     11.1     64     18.1     27.9       -111     21     61     11.2     11.0     21.7       -111     11     11     11     11     21.9     11.7       -111     11     11     11     11     11.1     11.1 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>4.20</td> <td>11.40</td> <td></td> <td></td> <td></td>								4.20	11.40			
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$												
HL       52.7 $7931$ $071$ $227$ $7931$ $041$ $227$ $041$ $227$ $041$ $227$ $041$ $227$ $041$ $227$ $041$ $227$ $041$ $227$ $063$ $116$ $063$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $117$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $116$ $061$ $061$ $061$ $061$ <	999-949		1.211	0.66	1.	.61	Ł		52.53	3.41	39.1	i n
GL       29.6       17.3 $0.64$ $1.0$ -1011       273       220.0 $0.84$ 51.0 $0.47$ 78.92 $0.56$ $45.0$ -111       248 $220.0$ $0.84$ 51.0 $0.47$ 78.92 $0.63$ $10.6$ -111       248 $83.9$ $0.32$ $20.5$ $0.17$ $56$ $1.77$ $24.9$ -111       248 $83.9$ $0.32$ $20.5$ $0.17$ $56$ $1.77$ $24.9$ -111       248 $83.9$ $0.32$ $20.5$ $0.17$ $56$ $27.5$ -111       273 $166.0$ $34.2$ $7.17$ $51.9$ $1.77$ $24.9$ -111 $273$ $166.1$ $87.0$ $0.61$ $17.1$ $27.5$ -111 $273$ $16.1$ $6.1$ $1.77$ $21.99$ $12.9$ -111 $187$ $6.21$ $23.1$ $0.71$ $21.92$ $12.9$ $11.1$ -1111 $187$ $83.2$ $10.70$ $10.91$ $10.91$ $10.9$ <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>Ţ</td> <td></td> <td>19.33</td> <td>0.73</td> <td>22.1</td> <td>5 0</td>							Ţ		19.33	0.73	22.1	5 0
-HMH         749         220-n         0.48         51.n         0.47         61         41.1         18.66         0.69         10.6         11.6           -111         248         83.9         0.37         20.5         n.17         68         41.1         18.66         0.69         11.6         27.5           -111         248         83.9         0.37         20.5         n.17         68         43.0         10.01         11.9         27.5           -111         248         83.9         0.37         20.5         n.17         68         43.0         10.01         11.9         27.5           -111         273         168.4         0.60         34.2         1.21         1.17         21.49         1.73         24.9           -111         273         168.4         0.60         34.5         1.47         1.49         1.45         1.49         1.21         34.1           -111         187         47.3         1.45         1.47         1.47         0.40         1.41         1.41         1.45         1.45         1.45         1.45         1.45         1.45         1.45         1.45         1.45         1.45         1.49         1.							<b>1</b> 9		17.34	4 N O	11.0	0
-111     244     241     17.4     0.05     17.4     0.05       -111     244     83.9     0.32     20.5     0.17     56     83.9     10.00     1.19     27.5     0       -111     244     83.9     0.32     20.5     0.17     56     83.9     10.00     1.19     27.5     0       -111     23     106.4     34.2     0.32     20.5     0.17     56     0       -111     23     168.4     0.64     34.2     0.17     51.7     21.49     17.3     1.       -111     23     168.4     0.61     23.1     0.43     51.1     0.61     1.1     0       -111     171     83.2     0.16     0.1     1.1     1.1     1.0     1.1     0       -111     171     83.2     0.16     0.61     1.0     0.61     1.1     0       -111     171     83.2     10.61     1.1     1.1     1.1     1.1     0       -111     171     83.2     0.16     0.61     1.1     0.1     0.1     0       -111     13.5     11.1     1.1     1.1     1.1     1.1     0.51     1.1       -111     <				•								
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$				È	-			173.6	74.92	۳.	45.0	
-Ull       274 $0.37$ $20.5$ $0.17$ $59$ $0.37$ $20.5$ $0.17$ $59$ $0.07$ $1.49$ $20.5$ $0.17$ $59$ $0.07$ $1.49$ $20.5$ $0.17$ $26.9$ $0$ $0.07$ $21.9$ $0.07$ $27.9$ $0$ -Ull $2^3$ $108.4$ $0.04$ $37.7$ $1.72$ $51.7$ $31.45$ $1.77$ $27.9$ $0$ -WK $472$ $59.6$ $0.21$ $23.1$ $0.14$ $15.7$ $21.49$ $0.61$ $17.1$ $0.61$ $17.1$ $0.61$ $17.1$ $0.61$ $17.1$ $0.61$ $17.1$ $0.61$ $0.1$ $0.1$ $0.1$ $0.1$ $0.1$ $0.1$ $0.1$ $0.1$ $0.1$ $0.1$ $0.1$ $0.1$ $0.1$ $0.1$ $0.1$ $0.1$ $0.0$ $0.07$ $17.0$ $0.07$ $0.01$ $0.1$ $0.1$ $0.01$ $0.1$ $0.1$ $0.01$ $0.1$ $0.01$ $0.1$ $0.1$ $0.01$ $0.1$ $0.01$ $0.01$ $0.01$							3		α, ''	-01	C	0
-111         288         83.0         0.37         20.5         0.17         6P         83.0         100.01         1.17         20.5         0           -JJU         273         108.4         0.40         34.7         7.12         51.1         21.45         1.77         20.5         0           -JUU         273         108.4         0.44         34.7         7.12         51.1         51.1         20.49         0         17.3         1           -WK         472         54.4         0.21         23.1         0.14         51.1         0.66         18.1         0         61.1         1         1         0         61         11.1         0         61         1         1         0         61         1         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0							2			<b>o</b>	1.4	
	- 11			٠	ి	.17			0.07	7	c	
-JUJ 2*3 108.4 0.0.64 3*.7 1.22 161 115.6 115.5 1.77 26.9 0 -WK 472 54.6 0.21 23.1 1.19 15. 12.1 0.66 18.1 0 -ILL 187 43.2 0.10 8.1 1.0.7 15. 43.2 10.00 0.61 8.1 0 -ILL 187 43.2 0.10 8.1 1.0.7 15.6 43.2 10.00 0.61 8.1 0 -WW 5.1 0.51 55.7 1.6 43.6 10.00 0.61 8.1 0 -WW 605 80.1 0.51 55.7 0.40 16. 05. 81.0 0.60 16.0 0 -WW 605 80.1 0.51 55.7 0.40 16. 05. 81.0 0.60 17.0 0 -XX 2076 3.75.0 1.78 673.1 0.40 16. 04. 81.0 0.60 125.5 4 -XX 2076 3.75.1 1.75 7.51 175.7 0.51 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 17.6 5.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.6 6.61 15.61 15.6 6.61 15.6 6.61 15.61 15.6 6.61 15.6 6.61 15.61 15.61												
•1       51.0       31.45       1.00       12.3       1         •1       12.1       12.1       12.1       11.1       12.1       10.0       18.1       0.0       18.1       0         •11       11       33.2       0.10       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1	717-949	*	68-	.0.64		N.		1			4	0.8
							5	-	1	•	~	1.1
-11     17     17     16     0.43     5.1     0       -11     17     17     17     16     0.43     5.1     0       -11     17     16     17     17     16     0.43     5.1     0       -11     17     16     17     16     0.43     17.5     0.43     5.1     0       -11     17     16     17     16     0.41     43.4     17.5     0.41     17.5     0       -11     17     16     17.5     16     17.5     19.34     0.47     1     0       -11     0.45     17.5     17.5     19.34     0.55     17.6     0       -11     0.45     5.5     11     11.6     17.6     0.5     17.5     10.5       -11     5.4     17.5     5.6     17.6     0.5     17.5     17.5     19.5	ļ	- ^	-			3						
-111       1A7       43.2       0.10       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1       0.1 <t< td=""><td></td><td></td><td></td><td>•</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>				•								
-ILL IRT 43.2 (2.14 8.1 (.C7 : 6P 43.2 IC0.0C 0.61 8.1 0 -WW 510 81.4 (.11 43.4 7.36 : 6P 35.9 47.68 (.51 15.0 0 -WI 10.7 18.12 0.48 15.0 0 -WI 0.5 An.1 0.51 55.7 0.40 : 6P 04.6 81.60 0.67 35.4 0 -MW 605 An.1 0.51 55.7 0.40 : 6P 04.6 81.60 0.67 35.7 9 -XXX 2076 325.0 1.74 675.1 5.53 2.19 34.7 9 -XXX 2076 325.0 1.74 675.1 5.53 2.39 35.7 9 -XXX 2076 325.0 1.74 675.1 5.53 2.39 35.7 9 -XXX 2076 325.0 1.74 675.1 5.53 74.1 11.7 52.43 2.39 35.7 9 -XXX 2076 325.0 1.74 675.1 5.53 74.1 11.7 52.43 2.39 35.7 9 -XXX 2076 376 5.77 1175.7 0.77 67 417.4 77.9 11.57 434.2 11 -XXX 570 71.57 7.7 1175.7 0.71 41.52 10 -XXX 510 77.6 71.7 11.57 71.41.52 10								•	10.17			
	Ŧ	¢	n.	7	<b>1.</b> 3	.c.1		*	10.00	0.61		•
	Bit - SHE	11	0.14			-						
		•										0
							;;	٠			ć I	
-M4M 695 Rn.1 0.51 53.7 0.40 1 6P 64.6 R1.60 0.69 34.9 -XXY 207R 575.0 1.74 673.3 5.53 1 RL 171.7 52.43 2.39 354.7 -XXY 207R 575.0 1.74 673.3 5.53 1 RL 171.7 52.43 2.39 354.7 -XXY 207R 576.0 1.09 1.00 1.00 1.00 -XXY 207R 540 1.61 1.62 1.00 1.00 1.00 -XXY 207 71.81.5 7.77 1175.7 0.57 1.61 1.62 0.41 4.2 1.62 1.62 1.62 1.62 1.62 1.62 1.62 1.									1.1.6.1			
WI     15.4     19.34     0.56     11.6       -XXX     2078     575.0     1.44     0.75.5     5.45     354.7       -XXX     2078     5.75     1.11.7     5.35     354.7       60     76.8     76.8     76.8     2.39     354.7       61     76.4     76.4     76.9     1.09     149.6       62     76.4     76.7     17.5     547     127.5       64     17.6     7.47     175.7     17.5     414.2       74     54.7     17.5     7.77     1175.7     414.2	22-22	•	ć	1	2	•			87.06	•	- #	1.4
-XXY 2076 525.0 1.14 675.1 5.53 RL 171.7 52.83 2.39 354.7 9 6 76.8 21.6.1 1.09 140.6 4 61 58.9 18.14 0.09 127.5 4 61 17.6 5.47 7.6 7 127.5 4 -XXX 574 77.7 175.7 1175.7 1175.7 11.67 17.30 11.57 434.2 11 -XXX 574 71.67 1175.7 6.77 14							5	•	19.34	0.54	C	0
	÷	2078	75.	2	15.	.51	, R	71.	50.43		3	
-111 510 11.5 5.47 [175,7 37,9] 17.4 5.40 [1.45] 12.5 5 -111 510 11.5 5.47 [175,7 3.47] 175,7 37,79 11.45 434,2 1							e e e			• `		
-111 510 1141 1141 1141 1141 1141 1141 11												
							; ;	A. 7 1			12	
1 2 14 1 12 11 12 12 12 12 12 12 12 12 12 12 1											•	
777.3 34.33 16.71 414.2 1	111-111	5	S UH Le	21.0	1175. 4	44.	10		17.24	T1.52	i	1 J. 7
							ī		31, . 3 *	10.71		10.77

and the second second second

				TEULAA.	1.14	4	PERJURY		a Ca B	x PM/NLY	a Ca F
	:	•			i	5	82.0	- <b>- - - -</b>	2.97	44.7	. 05
нич- <u>33</u> 3	1 - 1	1072.2	0 · 34	2.065	2.10 :		467.0	54.41	f . A4	77	
						5	441.5	24.03	A. A 3		2.25
						18	- +0+		5.62	Å1.8	
			-	1		75	115.8	2.09			
									;		
				190.				4 V - 2 V		112.0	
						ت ہے 5 ع					
-			;			Ţ	67.7				
		1									
10-11-11-11-11-11-11-11-11-11-11-11-11-1	¥ .	165.5	2 ~ 3	11. 1		- 1		2	-		0.9
						13	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	39.3# 8.57	 	2 H - 2	2.54
LCC-FFF	- 715	1.17	1.25	10.6	1.12		57.0	R 9.53	0.89	. 46. 4	
		1				, m T	2	÷.	0.09	1	11.0
								1			
CCC -616	572	126.9	л <b>.</b> С	74.4	0.54	3	64.0	52.15	1.0.1	47.4	1. 25
						2		•	٠		
			ļ ļ	-		Ŧ	C . *	14.21	0.25	1 v 1	
нин- 333	340	201.0	r. 17	12.4	: fy"u		111.8	54.67	4.11	.1.0	40.4
						ថ	45.4	22.59	0.73	14.3	0.54
						5	0°0#	20.34	1.47	1 7	1.1
						8	8°C	3.4.4	0.01	<b>••</b>	0.01
CC-111_	1 44	4.82 ···	0.11	5.5	: tr)" J	GР	к. Ч.У.	10.00	د <b>د</b> د	5 • 5	0.14
rrr-333	396	145.4	0.56	1.04	0.46 :	0 r	9.54	54.43	3.14	5°°0	3. 1 H
						91	0.70	41.12	46*)	24.3	0.40
100-844	111	198.4	0.74	2.4.4			114.5		×.	15. 9	1.14
1				•		5	75.0	*U* 6.	2.12	23.0	2.07
111-000	23.6	1.1	r.17	10.4	: 60.0	3	4 . n #	10.00	0.12	11.4	<b>21</b> .0
רכר יששא	5 np	24.4	<b>.</b> [.)	13.5	. 11.		14.7	52.45	0.50	7.1	0.22
						F.	7.7	25.24	0.24	ч. ч	0.31
		• • • •				9		52.00	60°0		0.10
NNN- DOT	H uL	1.15	۰.12	¢1. v	0.10		15.5	49.45	0.24		
						5		•	0.24		5.0
						4		***	0-11		
110-91A	845 .	76.4. 5	11.5	1 67 .5	- 97.F	۲	372.4	-47.	11.5	214.7	5.48
						Ŀ	255.1		3.91	150.1	4.9
						3	114.0	-	1.62		0.2
						-	4 5 ° J	۶ <b>۰</b> 75	1.62	24.6	2.39
444-010	5-3	1.111	1 . ¹ .		2.13:	a s	444.0	а. Ф		154.5	¥ 6° 4
							140.1	1	( # · )	_	2.25
						13	61.T	~	0.94	21.6	÷.

and the second second second second second second second second second second second second second second second

Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I. INL.         Massell I.	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$									•			
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1 Jacow		40/1.0		P# /112 Y	AT.T.	<b>.</b> .	X/DAV	1.1		*	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	000-000	5	1.56.6	44.	244.2		34	564.1	30.95	, C . d	114.0	3.57
$\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$ $\theta_{11}$	$\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ $\mu_{11}$ <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td>۔ ن</td><td>414.7</td><td>28.44</td><td>f.35</td><td>P 7</td><td>2.76</td></t<>							۔ ن	414.7	28.44	f.35	P 7	2.76
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	PI         134.6 $1.0.1$ $1.0.1$ $1.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0.1$ $2.0$							θL	154.	17.05	2.56	37.2	0.97
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$k^{+1}$ $k_{-1}$ $r_{-1}$ $r_{-1}$ $r_{-1}$ $r_{-1}$ $r_{-1}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$ $r_{-2}$							10	154.6	11.61		2.16	111
$4^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ $6^{4}$ <	141     1.1     7.1.0     7.1.0     7.5.0     1.1.     2.1.0     47.50     0.29       808     44.0     (.11     31.1     7.24     0.41     21.1     2.1.0     47.50     0.29       743     66.7     (.11     31.1     7.26     1.1.1     5.1.1     5.1.0     0.19       744     66.7     (.11     31.1     7.26     1.1.2     7.1.2     2.20       745     66.1     7.1.1     5.1.1     1.1.2     7.1.1     5.1.0     0.19       745     76.1     7.1.6     1.1.7     7.40     1.1.7     5.01     0.55       746     137.0     0.11     10.4     0.40     1.1     5.4     6.10     6.10       745     55.1     0.11     1.1.7     0.11     1.1.7     5.11     1.0.6       746     135.4     0.11     1.1.7     0.11     5.1     5.1     5.1       746     135.4     0.10     1.1.7     0.11     1.1.7     5.1     5.1       746     135.4     0.10     1.1     5.6     1.1.5     1.1.5     5.1       746     135.4     0.10     1.1.7     0.11     1.1.5     1.1.5       746     135.4							5	135.4	9.3)	4.84	27.4	2.46
714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714     714 <td>600     64.4     (.1)     31.4     7.20     14.1     21.0     1.4.4     0.0       747     64.4     (.1)     31.4     7.40     1.4.1     7.4.4     0.0       747     64.4     0.41     1.1     1.2.5     74.9     2.2.7     0.4.4       747     64.4     0.41     1.4     1.4.6     0.4.9     2.10       747     64.4     0.41     1.4     2.11     0.49     2.27       745     64.4     0.41     1.4     2.11     0.49     2.27       745     64.4     0.41     1.4     0.4     1.4.6     0.4       745     64.4     0.41     1.4     0.4     0.4     0.4       745     64.4     0.40     1.4     1.4     0.4     0.4       746     175.4     6.41     1.4     1.4     1.4     0.4       746     175.4     6.41     1.4     1.4     0.4     0.4       744     175.4     6.41     1.4     1.4     1.4     0.4       744     175.4     1.4     1.5     1.4     1.4     1.4       744     175.4     1.4     1.5     1.4     1.4     1.4       744     7.4<!--</td--><td></td><td></td><td></td><td></td><td>× * _</td><td></td><td></td><td>•</td><td></td><td></td><td></td><td>10.0</td></td>	600     64.4     (.1)     31.4     7.20     14.1     21.0     1.4.4     0.0       747     64.4     (.1)     31.4     7.40     1.4.1     7.4.4     0.0       747     64.4     0.41     1.1     1.2.5     74.9     2.2.7     0.4.4       747     64.4     0.41     1.4     1.4.6     0.4.9     2.10       747     64.4     0.41     1.4     2.11     0.49     2.27       745     64.4     0.41     1.4     2.11     0.49     2.27       745     64.4     0.41     1.4     0.4     1.4.6     0.4       745     64.4     0.41     1.4     0.4     0.4     0.4       745     64.4     0.40     1.4     1.4     0.4     0.4       746     175.4     6.41     1.4     1.4     1.4     0.4       746     175.4     6.41     1.4     1.4     0.4     0.4       744     175.4     6.41     1.4     1.4     1.4     0.4       744     175.4     1.4     1.5     1.4     1.4     1.4       744     175.4     1.4     1.5     1.4     1.4     1.4       744     7.4 </td <td></td> <td></td> <td></td> <td></td> <td>× * _</td> <td></td> <td></td> <td>•</td> <td></td> <td></td> <td></td> <td>10.0</td>					× * _			•				10.0
$m_{1}$ $21,7$ $n_{1}$ $21,7$ $n_{1}$ $21,7$ $n_{1}$ $21,7$ $n_{1}$ $21,7$ $n_{1}$ $21,7$ $n_{1}$ $21,7$ $21,2$ $n_{1}$ $21,7$ $21,2$ $n_{1}$ $21,7$ $21,2$ $n_{1}$ $21,7$ $21,2$ $n_{1}$ $21,7$ $21,2$ $n_{1}$ $21,7$ $21,2$ $n_{1}$ $21,7$ $21,2$ $0.10$ $11,1$ $21,7$ $21,2$ $0.10$ $11,1$ $215$ $0.01$ $0.01$ $10,01$ $10,01$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ $10,10$ <	AL     ZIT     AL     ZIT     AL     ZIT     AL     AL       141     11.1     1.2.7     11.4.0     0.0.7       141     12.1     12.1     0.10     0.1       141     12.1     0.11     0.11     0.11       141     12.1     0.11     0.11     0.11       141     12.1     0.11     0.11     0.11       151     0.11     12.1     0.11     0.10       155     0.11     12.1     0.11     0.10       155     0.11     12.1     0.11     0.10       155     0.11     0.11     0.11     0.11       156     0.11     0.11     0.11     0.10       156     0.11     0.11     0.11     0.11       151     0.11     0.11     0.11     0.11       151     0.11     0.11     0.11     0.11       151     0.11     0.11     0.11     0.11       151     0.11     0.11     0.11     0.11       151     0.11     0.11     0.11     0.11       151     0.11     0.11     0.11     0.11       151     0.11     0.11     0.11     0.11     0.11 <tr< td=""><td></td><td></td><td></td><td></td><td></td><td>••••</td><td></td><td></td><td></td><td></td><td>· · · ·</td><td></td></tr<>						••••					· · · ·	
66         64.0         (.11         31.1         1.2         2.5.0         0.44         4.5           747         04.7         0.45         44.4         0.41         8.7         0.44         4.5           747         04.7         0.45         44.4         0.41         8.7         8.5         8.4           747         04.7         0.45         7.4         0.41         8.7         8.7         8.5           748         137.6         0.41         72.8         0.40         1.91         74.9         2.2         8.4           748         137.6         0.41         7.4         7.0         1.91         7.0         9.4           748         0.41         7.4         1.0.6         1.1         7.4         7.4         7.4           744         0.41         10.4         0.40         4.7         1.90.0         1.4         7.4           744         175.1         0.41         10.4         1.40         7.4         7.4           744         175.1         1.4         1.40         1.40         1.4         7.4         7.4           744         175.1         1.15         1.1         1.4 <td< td=""><td>A⁶B         Wein         (.17         JJ.1         n.2.b         (.17         JJ.1         n.2.b         (.17         27.5         0.0.4           747         01         01         0.41         7.0         11.45         0.01           747         01         01         7.4         0.41         7.4         0.41         11.45         0.01           745         01         7.4         0.41         7.4         0.41         1.4         0.11         0.04           745         0.11         7.4         1.4         0.11         0.04         0.04           746         1.4.1         0.41         7.4         0.41         0.04         0.04         0.04           745         9.51         0.41         7.4         1.4         0.10         0.04           746         0.14         10.4         0.40         1.4         0.4         0.10         0.14           746         17.4         11.5         0.11         1.4         7.4         0.10         0.14           744         175.4         0.11         1.4         1.4         1.4         1.4         0.14           744         17.4         1.4<td></td><td></td><td></td><td></td><td></td><td></td><td>Ĭ</td><td>· · · · ·</td><td>4 L • L •</td><td>•</td><td></td><td>62 0</td></td></td<>	A ⁶ B         Wein         (.17         JJ.1         n.2.b         (.17         JJ.1         n.2.b         (.17         27.5         0.0.4           747         01         01         0.41         7.0         11.45         0.01           747         01         01         7.4         0.41         7.4         0.41         11.45         0.01           745         01         7.4         0.41         7.4         0.41         1.4         0.11         0.04           745         0.11         7.4         1.4         0.11         0.04         0.04           746         1.4.1         0.41         7.4         0.41         0.04         0.04         0.04           745         9.51         0.41         7.4         1.4         0.10         0.04           746         0.14         10.4         0.40         1.4         0.4         0.10         0.14           746         17.4         11.5         0.11         1.4         7.4         0.10         0.14           744         175.4         0.11         1.4         1.4         1.4         1.4         0.14           744         17.4         1.4 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>Ĭ</td> <td>· · · · ·</td> <td>4 L • L •</td> <td>•</td> <td></td> <td>62 0</td>							Ĭ	· · · · ·	4 L • L •	•		62 0
NI         12.7         27.50         0.000         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.	747     06.1     0.1     0.1     12.2     27.20     0.04       747     06.1     0.1     1.4     2.1     1.4     2.1     1.00       746     0.1     0.1     1.4     2.1     1.4     2.1     1.00       747     06.1     0.1     1.1     1.4     2.1     1.00       745     0.1     0.1     1.1     1.4     2.1     1.00       745     0.1     0.1     1.1     1.4     2.1     1.00       745     0.1     0.1     0.1     1.4     2.1     1.00       745     0.1     0.1     0.1     0.10     0.18       745     0.1     0.1     0.1     0.10     0.18       74     10.1     1.1     0.1     0.10     0.18       74     10.1     0.1     0.1     0.10     0.10       744     0.1     0.1     0.1     0.1     0.1       744     1.1     0.1     0.1     0.1     0.1       744     0.1     0.1     0.1     0.1     0.1       744     0.1     0.1     0.1     0.1     0.1       744     1.1     0.1     0.1     1.1     0.1 <td>11-000</td> <td>909</td> <td>a • 3 #</td> <td></td> <td></td> <td>: 90</td> <td>19</td> <td>27.5</td> <td>1.40</td> <td>C. # . )</td> <td>19.2</td> <td>0.03</td>	11-000	909	a • 3 #			: 90	19	27.5	1.40	C. # . )	19.2	0.03
Nat         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5         0.5 <th0.5< th=""> <th0.5< th=""> <th0.5< th=""></th0.5<></th0.5<></th0.5<>	NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI         NI							1	12.7	27.20	0.44	ł	0.77
747       0+.7       0+.7       0+.4       0.41       61       0+.3       0+.10       0+.1         444       132.9       0+.41       72.4       7.40       1       1       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0	7*7         6*.7         0.4.7         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.4.6         0.							1		11.40	0.0		0.09
747       06.7       0.4.7       0.4.1       5.1       0.4.0       2.2.2       0.4.0         346       132.9       0.4.1       72.4       0.40       2.4       2.4       2.4       2.4         346       132.9       0.41       72.4       0.40       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       2.4       <	747         6x.7 $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x, x)$ $(x$												
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	61 $6.2$ $9.2$ $6.10$ $34h$ $132.6$ $6.11$ $72.4$ $6.40$ $1.206$ $74h$ $132.6$ $6.11$ $72.4$ $6.74$ $72.07$ $0.65$ $75$ $6.11$ $72.4$ $6.74$ $72.07$ $0.65$ $75$ $6.01$ $7.4$ $76.77$ $76.77$ $0.67$ $595$ $55.1$ $6.11$ $32.4$ $6.70$ $0.10$ $0.65$ $766$ $17.5$ $77.57$ $77.57$ $76.77$ $0.11$ $0.61$ $766$ $17.5$ $6.77$ $6.71$ $0.12$ $0.12$ $0.12$ $766$ $11.5$ $0.71$ $1.67$ $1.60$ $1.60$ $1.60$ $776$ $17.5$ $6.77$ $6.71$ $1.60$ $2.79$ $776$ $11.35$ $0.711$ $11.15.7$ $77.5.9$ $2.07$ $776$ $11.25$ $11.15.7$ $11.15.7$ $2.79$ $2.79$	UUU -660	147	64.7	٩.	エーアオ	14.	Ę,	54.7	87.43	2.27	8 T. B	4.16
No.     132.0     0.01     72.4     0.00     w1     95.0     70.0     10.0     70.0       235     70.0     0.11     10.4     0.00     w1     97.0     2.55     70.0       235     70.0     0.11     10.4     0.70     10.1     70.0     10.6     70.4       235     70.0     0.11     10.4     0.70     10.1     70.0     10.6     70.4       295     55.1     0.11     37.1     7.0     70.0     10.1     70.0     70.1       574     17.5     7.7.5     7.7.5     7.7.5     70.1     7.1     7.1       574     17.5     6.7     7.1     7.1     7.1     7.1     7.1       574     17.5     6.7     7.1     7.1     7.1     7.1       574     17.5     6.7     7.1     7.1     7.1     7.1       574     17.5     6.7     7.1     11.1     7.1     7.1       574     11.1     4.5     7.1     7.2     7.1     7.1       574     11.1     5.7     7.1     1.1     7.1     7.1       574     11.1     4.5     7.4     7.1     7.1     7.1       574	446     132.6     6.41     72.4     7.40     1.4     2.71     0.06       235     46.0     72.4     7.40     1.1     31.2     28.01     0.55       235     46.0     7.1     10.4     7.40     1.1     44.1     10.4     1.6       235     55.1     6.71     31.5     0.70     5.6     31.5     7.75     2.60       236     55.1     6.71     31.6     0.70     5.6     11.5     6.71     1.6       376     175.7     7.71     5.71     5.71     5.70     0.18       376     175.7     5.71     5.71     5.70     5.70       376     17.5     5.71     5.71     5.70     5.70       376     17.5     5.71     5.71     5.70     5.70       376     17.5     5.71     1.17     5.70     5.70       376     17.5     5.71     1.1.7     7.16     7.90       377     18.1     0.70     1.1     41.4     7.80     2.10       378     28.01     0.57     11.1     41.4     7.80     2.10       379     19.1     11.1     41.4     11.6     7.80     2.80       379     2							Ŀ	ç.,	9.36	0.10	<b>7.</b> *	21.6
New     132.0     0.41     72.4     0.40     w1     57.2     78.01     0.65     71.4       235     4A.0     0.11     10.4     0.71     1.0.1     0.71     1.0.5     10.4       235     59.1     0.71     10.4     0.70     1.6     77.5     70.2     0.5       295     59.1     0.71     30.4     7.0     0.10     0.18     2.9       179     175.3     0.71     1.0.5     11.5     71.5     71.5     2.9       770     175     0.71     1.1.5     71.5     71.5     2.9     2.9       771     17.3     0.71     11.5     71.5     71.5     2.9     2.9       775     18.1     0.70     1.5     11.5     7.9     2.9     7.1       775     18.3     0.70     1.5     71.4     7.1     7.1     7.1       775     18.4     0.70     1.11     41.4     7.1     7.1     7.1       775     18.4     0.70     1.11     7.1     7.1     7.1       79.5     18.4     0.70     1.11     7.1     7.1     7.1       79.5     18.4     0.71     1.11     7.1     7.1     7.1   <	New         137.9 $0.4^{11}$ 72.4 $0.40$ $0.1$ $91.5$ $71.0$ $1.00$ $0.5^{11}$ $0.40$ $1.40$ $0.5^{11}$ $0.50$ $1.45$ $0.50$ $0.45$ $0.50$ $0.45$ $0.50$ $0.45$ $0.50$ $1.45$ $0.50$ $1.5$ $0.76$ $0.11$ $0.50$ $1.45$ $0.50$ $1.45$ $0.61$ $0.50$ $1.45$ $0.61$ $0.50$ $1.46$ $0.50$ $0.11$ $0.50$ $0.11$ $0.50$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0.16$ $0$							-	1.4	2.71	1.0A	1.3	0.12
215 $0.0$ $0.1$ $1.0.4$ $0.0.6$ $7.5$ $70.01$ $0.65$ $70.4$ 215 $0.0.1$ $0.1$ $10.4$ $1.0.4$ $1.0.4$ $1.0.6$ $1.60$ $1.65$ $7.06$ $7.06$ 215 $5.11$ $6.71$ $3.7$ $7.10$ $2.65$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.61$ $2.$	715 $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.65$ $0.61$ $0.65$ $0.61$ $0.65$ $0.61$ $0.65$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$ $0.12$	HHH-000	2 <b>8</b> 5	1	5	<ul> <li>N</li> </ul>	0 <b>4</b> -	7		40 - 42	1.90	1.95	C 4 - C
715     4A.0     7.11     10.4     7.05     11     4.6     10.4     10.4       295     51.1     7.11     10.4     10.4     7.05     11     4.6       295     51.1     7.11     11.6     11.6     11.6     12.6     7.8       179     175.1     7.11     5.7     5.1     0.18     7.1       711     175.1     5.7     5.7     5.10     0.18     7.1       714     175.1     5.7     5.7     5.10     0.18     7.1       714     175.1     5.7     5.7     5.7     5.9     7.1       719     175.1     5.7     5.7     5.7     5.9     7.1       711     17.1     5.1     5.7     5.7     5.9     7.1       711     5.7     5.7     5.7     5.9     5.9     7.1       711     5.7     5.9     5.9     5.9     5.9     7.1       711     5.7     5.7     5.9     5.9     7.1     7.9       711     5.9     5.9     5.9     5.9     5.9     7.1       711     5.9     5.9     5.9     5.9     5.9     7.9       719     5.9     5.9     5.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$							1	A . C .	12.07			
215       00       0.11       104       00       14       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       104       10	235         64.0         7.18         10.4         7.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0							ت	37.2	24.01	0.5	5 U T	9.0
595       55.1 $f_{**}f_{*}$ $f_{*}f_{*}f_{*}$ $f_{*}f_{*}f_{*}$ $f_{*}f_{*}f_{*}f_{*}$ $f_{*}f_{*}f_{*}f_{*}f_{*}f_{*}f_{*}f_{*}$	585       55.1 $(1)$ $3/.1$ $(0)$ $(0)$ $(1)$ $3/.1$ $(0)$ $(1)$ $3/.1$ $(0)$ $(1)$ $3/.1$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$							•	2				
585     59.1     (1     37.1     (0 $\times$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$ $\gamma$	585     51.1     6.1     37.1     6.1     6.1     6.1     6.1     6.1     6.1     6.1     6.1     6.1     6.1     6.1     6.1     6.1     6.1     7.5     7.5     7.5     7.5     7.5     7.5     7.5     7.5     7.5     7.5     7.5     7.5     7.5     7.5     7.5     7.5     7.5     7.6     7.5     7.5     7.5     7.6     7.5     7.5     7.5     7.6     7.5     7.5     7.6     7.5     7.6     7.5     7.6     7.5     7.6     7.5     7.6     7.5     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6     7.6<	111-000	Ę			10.1	2	-		100.001	1	9.1	0. 4
17     17.5     13.5     7.15     5.0     9.10     0.18     7.9       574     17.5     5.7     31.5     0.70     5.4     1.42     7.1       574     17.5     5.7     3.1     0.71     5.7     2.16     5.1       574     17.5     5.77     5.7     5.10     2.24     1.42     7.1       574     17.5     5.71     5.74     1.5     7.1     7.1       574     17.5     5.77     5.70     2.6.4       772     18.3     0.07     13.7     7.11     11.5     6.7     3.1       773     18.3     0.07     13.7     7.11     11.6     7.90     0.22     1.0       773     18.3     0.07     13.7     7.11     11.6     7.90     0.20     1.0       18.7     796.7     1.11     45.4     7.16     11.4     7.90     2.0     1.0       18.7     796.7     1.11     45.4     7.11     1.16     1.20     1.20       44.5     79.6     1.11     11.6     1.16     11.6     1.10     1.10     1.0       44.5     75.4     11.5     11.4     11.6     11.6     1.20     1.20     1.20<	17 $7.7$ $7.7$ $5.7$ $6.77$ $5.77$ $5.77$ $5.77$ $5.77$ $5.77$ $5.79$ $5.77$ $5.79$ $5.79$ $5.79$ $5.79$ $5.79$ $1.67$ $5.748$ $1.67$ $5.79$ $5.79$ $5.79$ $5.79$ $5.79$ $5.79$ $5.79$ $5.79$ $5.79$ $5.79$ $5.79$ $5.79$ $5.79$ $5.79$ $5.79$ $5.79$ $5.79$ $5.79$ $5.79$ $5.79$ $5.79$ $5.70$ $5.70$ $5.70$ $5.70$ $5.70$ $5.70$ $5.70$ $5.70$ $5.70$ $5.70$ $5.70$ $5.70$ $5.70$ $5.70$ $5.70$ $5.70$ $5.70$ $5.70$ $5.70$ $5.70$ $5.70$ $5.97$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.07$ $5.70$	<i><b>LIL-UNU</b></i>	585	55.1	•	<b>٦</b>	: 0^.	C ¥	- <b>-</b>	16.17	1.40	26	2.44
11       5.0       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.11       0.10       0.11       0.10       0.11       0.10       0.11       0.10       0.11       0.10       0.11       0.10       0.11       0.10       0.11       0.10       0.11       0.10       0.11       0.10       0.11       0.10       0.10       0.11       0.10       0.10       0.11       0.10       0.10       0.11       0.10       0.11       0.10       0.11       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10       0.10 <t< td=""><td>k1       5.0       0.10       0.10       0.10       0.10       0.10       0.11         179       17.5       $5.77$ $5.77$ $5.77$ $5.77$ $5.79$ $2.09$ $5.79$ $2.09$ $5.75$ $2.09$ $5.09$ $5.16$ $1.6$ $39.5$ $77.57$ $2.09$ $6.16$ $5.07$ $6.11$ $6.7$ $6.16$ $1.6$ $7.50$ $6.16$ $5.16$ $0.22$         772       18.3       $0.07$ $13.7$ $0.11$ $1.1.7$ $6.700$ $0.22$         772       18.3       $0.07$ $13.2$ $0.11$ $1.1.7$ $6.10$ $0.22$         772       18.7       $0.07$ $13.1$ $0.11$ $1.1.7$ $6.10$ $0.27$         187       $799.7$ $1.11$ $4.5$ $1.1.7$ $7.9$ $2.97$ $2.97$         187       $799.7$ $1.11$ $4.5$ $0.11.2$ $0.11.2$ $0.29$ $2.97$         187       $799.7$ $0.11$ $1.1.7$ $0.11.2$ $0.29$ $2.97$ $0.29$ $2.97$         187       $1.99.7$</td></t<> <td></td> <td></td> <td></td> <td></td> <td>i –</td> <td>1</td> <td></td> <td>4°1</td> <td>14.1.</td> <td>0.12</td> <td>9.4</td> <td>0.15</td>	k1       5.0       0.10       0.10       0.10       0.10       0.10       0.11         179       17.5 $5.77$ $5.77$ $5.77$ $5.77$ $5.79$ $2.09$ $5.79$ $2.09$ $5.75$ $2.09$ $5.09$ $5.16$ $1.6$ $39.5$ $77.57$ $2.09$ $6.16$ $5.07$ $6.11$ $6.7$ $6.16$ $1.6$ $7.50$ $6.16$ $5.16$ $0.22$ 772       18.3 $0.07$ $13.7$ $0.11$ $1.1.7$ $6.700$ $0.22$ 772       18.3 $0.07$ $13.2$ $0.11$ $1.1.7$ $6.10$ $0.22$ 772       18.7 $0.07$ $13.1$ $0.11$ $1.1.7$ $6.10$ $0.27$ 187 $799.7$ $1.11$ $4.5$ $1.1.7$ $7.9$ $2.97$ $2.97$ 187 $799.7$ $1.11$ $4.5$ $0.11.2$ $0.11.2$ $0.29$ $2.97$ 187 $799.7$ $0.11$ $1.1.7$ $0.11.2$ $0.29$ $2.97$ $0.29$ $2.97$ 187 $1.99.7$					i –	1		4°1	14.1.	0.12	9.4	0.15
170       175.7 $5.77$ $5.76$ $5.16$ $5.77$ $5.76$ $24.8$ $1.42$ $7.1$ 514 $17.5$ $6.77$ $6.77$ $6.77$ $6.77$ $6.77$ $6.77$ $6.77$ $7.12$ $7.12$ $7.12$ 514 $17.5$ $6.77$ $6.77$ $6.77$ $6.77$ $7.12$ $7.12$ 725 $14.5$ $0.07$ $13.5$ $0.111$ $4.1$ $11.5$ $70.82$ $0.22$ $7.1$ 735 $14.5$ $0.07$ $13.5$ $0.111$ $4.1$ $11.5$ $0.022$ $11.0$ $187$ $794.5$ $0.022$ $11.2$ $0.22$ $7.1$ $0.22$ $1.0$ $187$ $794.5$ $0.11$ $0.21$ $0.11.6$ $1.01$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$ $1.02$	176       175.7       51.6 $0.26$ $0.1$ $0.7$ $51.7$ $5.77$ $51.6$ $51.6$ $51.7$ $51.7$ $51.7$ $51.7$ $51.7$ $51.7$ $51.7$ $51.7$ $51.7$ $51.7$ $51.7$ $51.7$ $51.6$ $51.6$ $51.6$ $51.7$ $51.7$ $51.94$ $1.42$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ $51.6$ <							1	с <b>°</b> у	9.10	0.18	2.9	0.26
5/4     1/-3     6.7     6.7     6.7     6.7     6.7     6.7     6.7     7.1       5/4     1/-3     6.7     6.7     6.7     6.7     6.7     7.1       7/2     18.3     0.07     13.7     7.11     7.1     7.1     7.1       7/2     18.3     0.07     13.7     7.11     7.1     7.1     7.1       18.7     7.4     0.07     13.7     7.11     7.1     7.1       18.7     7.4     0.07     13.7     7.1     7.1     7.1       18.7     7.4     0.07     13.7     7.1     7.1     7.1       18.7     7.4     7.1     1.1     43.4     7.1     1.1     1.1       18.7     7.4     7.1     1.1     7.4     7.4     7.4       18.7     7.4     7.4     7.4     7.4     7.4       45.8     7.4     7.4     7.4     7.4     7.4       45.7     7.4     7.4     7.4     7.4     7.4       45.8     7.4     7.4     7.4     7.4     7.4       45.8     7.4     7.4     7.4     7.4     7.4       45.8     7.4     7.4     7.4     7.4     7.4 </td <td>514     17.3     6.7     0.07     6.7     0.07     0.1     39.5     72.48     1.07       773     18.3     0.07     13.7     0.11     11.5     76.97     0.27       773     18.3     0.07     13.7     0.11     11.6     77.08     0.27       793     18.3     0.07     13.7     0.11     11.6     77.08     0.27       18.7     79.5     1.11     45.4     0.16     11.6     7.41     0.27       18.7     795.7     1.11     45.4     0.41     7.41     0.29       18.7     795.7     1.11     45.4     7.41     7.49     0.29       18.7     795.7     1.11     45.4     71.4     7.5     7.97       18.7     790.7     1.11     1.45     11.6     7.69     1.79       18.7     790.8     1.12     0.43     1.1     1.46     1.19       18.1     198.9     11.6     11.6     11.6     1.16     1.16       18.1     198.9     11.6     1.1     1.1.7     0.70     0.71       18.1     198.9     11.9     1.1     1.1.6     1.1.6     1.1.6       18.1     198.9     11.9     1.1</td> <td><u> </u></td> <td></td> <td></td> <td>5.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>94</td> <td></td> <td></td>	514     17.3     6.7     0.07     6.7     0.07     0.1     39.5     72.48     1.07       773     18.3     0.07     13.7     0.11     11.5     76.97     0.27       773     18.3     0.07     13.7     0.11     11.6     77.08     0.27       793     18.3     0.07     13.7     0.11     11.6     77.08     0.27       18.7     79.5     1.11     45.4     0.16     11.6     7.41     0.27       18.7     795.7     1.11     45.4     0.41     7.41     0.29       18.7     795.7     1.11     45.4     7.41     7.49     0.29       18.7     795.7     1.11     45.4     71.4     7.5     7.97       18.7     790.7     1.11     1.45     11.6     7.69     1.79       18.7     790.8     1.12     0.43     1.1     1.46     1.19       18.1     198.9     11.6     11.6     11.6     1.16     1.16       18.1     198.9     11.6     1.1     1.1.7     0.70     0.71       18.1     198.9     11.9     1.1     1.1.6     1.1.6     1.1.6       18.1     198.9     11.9     1.1	<u> </u>			5.						94		
5/4     1/-3     6.07     6/-     11.2     6.09     6.16     6.1       1/2     18.3     0.07     13.7     0.11     11.6     7.90     0.10     7.1       1/2     18.3     0.07     13.7     0.11     14.5     7.11     7.1     7.1       1/2     18.3     0.07     13.7     0.10     13.7     7.10     0.27     7.1       1/2     18.4     0.07     13.7     0.10     1.1     7.9     0.07     1.0       1/2     1.11     43.4     0.10     1.1     7.4     0.07     1.0       1/2     1.11     43.4     0.10     1.1     7.9     0.07     1.0       1/2     1.11     43.4     0.10     1.1     7.9     0.07     1.0       445     7.40     1.11     43.4     0.10     1.1     1.1     1.1       445     7.4     0.11     1.1     1.1     1.1     1.1     1.1       445     7.4     0.11     1.1     1.1     1.1     1.1     1.1       445     7.4     0.11     1.1     1.1     1.1     1.1     1.1       445     7.4     7.4     7.4     7.4     7.4 <t< td=""><td>544       $17.3$ $6.07$ $6.7$ <t< td=""><td></td><td></td><td></td><td></td><td></td><td>\$</td><td></td><td>• •</td><td></td><td></td><td></td><td></td></t<></td></t<>	544 $17.3$ $6.07$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ $6.7$ <t< td=""><td></td><td></td><td></td><td></td><td></td><td>\$</td><td></td><td>• •</td><td></td><td></td><td></td><td></td></t<>						\$		• •				
514     17.5     6.7     6.7     6.7     6.7     6.7     6.7     6.7     6.7     7.1       792     18.3     0.07     13.3     7.11     11.6     7.8     7.16     7.1       197     795     18.3     0.07     13.3     7.11     11.6     7.8     7.16     7.9       197     795.7     1.13     0.71     13.3     7.11     11.5     7.9     7.9       187     795.9     1.13     0.45     1.4     7.15     0.99     1.0       187     7.99     1.1     45.4     0.43     1.1     11.5     7.9       445     7.99     1.1     1.1     4.5     1.1     1.2     1.2       445     7.9     1.1     1.1     1.1     1.1     1.2       445     7.9     1.1     1.1     1.1     1.2       445     7.6     1.1     1.1     1.1     1.1       445     7.9     1.1     1.1     1.1     1.1       445     7.0     1.1     1.1     1.1     1.1       445     7.0     1.1     1.1     1.1     1.1       445     7.0     1.1     7.0     1.1     1.1     1	S11 $11.3$ $6.71$ $6.71$ $6.11$ $11.5$ $75.04$ $0.27$ 793 $18.3$ $0.07$ $13.3$ $9.11$ $11.5$ $75.04$ $0.27$ 793 $18.3$ $0.07$ $13.3$ $9.11$ $11.5$ $75.04$ $0.27$ $197$ $11.4$ $0.07$ $13.3$ $9.11$ $11.5$ $7.92$ $0.72$ $187$ $295.7$ $61$ $11.4$ $7.93$ $2.97$ $0.02$ $187$ $195.7$ $1.1$ $45.4$ $7.93$ $2.97$ $0.93$ $455$ $780.4$ $11.37$ $0.91.2$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0.127$ $0$							-					
133     14     1.1     55.04     0.22     7.1       143     0.07     13.3     7.11     14     11.5     7.84     0.10     7.9       147     795     1.1     45.4     0.02     15.0     7.9     1.0       147     795.5     1.13     45.4     0.16     14     7.41     1.0     7.9       147     795.5     1.13     45.4     0.15     7.41     1.6     7.9     1.0       455     7.95     1.1     45.4     0.15     1.1     7.9     1.0       455     7.9     1.1     45.4     0.15     1.1     1.0     1.0       455     7.9     1.1     1.1     1.1     1.1     1.1     1.1       455     7.9     1.1     1.1     1.1     1.1     1.1     1.1       451     1.9     1.1     1.1     1.1     1.1     1.1     1.1       451     1.9     1.1     1.1     1.1     1.1     1.1     1.1       451     1.1     1.1     1.1     1.1     1.1     1.1     1.1       451     1.1     1.1     1.1     1.1     1.1     1.1     1.1        451 <t< td=""><td>61     6.1     1.1.5     75.0H     0.27       775     18.3     0.07     13.3     6.11     11.5     73.87     9.16       18.7     0.07     13.7     61     1.4     7.43     9.00       18.7     795.0     1.13     43.4     0.16     14     11.5     7.43     0.07       18.7     795.2     1.13     43.4     0.16     14     7.43     0.02       18.7     796.2     1.13     43.4     0.16     11     7.43     0.02       45.9     79.4     11.3     0.13.4     0.13     1.16     11.5     7.06       45.8     75.4     0.1.7     0.1.7     0.1.7     0.1.7     0.1.7     0.0.7       45.7     75.4     11.3     1.15.7     1.15.7     0.0.7       45.8     75.4     11.1     1.1.6     1.1.6       70.7     24.7     1.1.6     1.1.6     1.1.6       70.7     24.7     7.1     1.1.7     1.1.6       70.8     7.4.4     7.7     1.1.7     0.10.0       71     1.1.7     1.1.7     1.1.7     0.10       71     54.7     1.1.7     1.1.7     1.1.7</td><td></td><td>514</td><td>1:1</td><td>6.77</td><td>1.9</td><td>6</td><td><u>9</u></td><td>11.3</td><td>60.44</td><td>1.16 -</td><td>1.5</td><td>0.14</td></t<>	61     6.1     1.1.5     75.0H     0.27       775     18.3     0.07     13.3     6.11     11.5     73.87     9.16       18.7     0.07     13.7     61     1.4     7.43     9.00       18.7     795.0     1.13     43.4     0.16     14     11.5     7.43     0.07       18.7     795.2     1.13     43.4     0.16     14     7.43     0.02       18.7     796.2     1.13     43.4     0.16     11     7.43     0.02       45.9     79.4     11.3     0.13.4     0.13     1.16     11.5     7.06       45.8     75.4     0.1.7     0.1.7     0.1.7     0.1.7     0.1.7     0.0.7       45.7     75.4     11.3     1.15.7     1.15.7     0.0.7       45.8     75.4     11.1     1.1.6     1.1.6       70.7     24.7     1.1.6     1.1.6     1.1.6       70.7     24.7     7.1     1.1.7     1.1.6       70.8     7.4.4     7.7     1.1.7     0.10.0       71     1.1.7     1.1.7     1.1.7     0.10       71     54.7     1.1.7     1.1.7     1.1.7		514	1:1	6.77	1.9	6	<u>9</u>	11.3	60.44	1.16 -	1.5	0.14
773     18.3     0.07     13.7     7.11     HL     11.5     5.42     0.10     4.3       18.7     795.7     0.11     61     5.8     7.43     0.02     1.0       18.7     795.6     1.13     45.8     0.16     1.4     7.43     0.02     1.0       18.7     795.6     1.13     45.8     0.15     1.14     7.9     1.20     7.9       18.7     795.7     1.13     45.8     0.13     1.14     1.15     7.9     1.15       45.5     780.1     1.13     45.8     0.13     1.13     0.43     1.12       45.8     780.6     11.3     0.13     0.14     1.1     1.13     0.43       45.7     75.6     11.3     0.13     0.14     1.1     1.1     1.1       45.8     75.8     1.13     0.13     1.1     1.1     1.1       45.7     75.6     11.3     0.13     0.27     7.0       45.8     75.8     7.9     7.1     1.1     1.1     1.1       45.7     75.8     7.9     7.1     7.0     7.2       45.8     7.9     7.1     7.9     7.1     1.1     7.2       70.0     7.1	7.7 $18.3$ $0.07$ $13.7$ $6.11$ $HL$ $11.5$ $7.87$ $9.76$ $9.07$ $0.02$ $18.7$ $7.9.7$ $1.13$ $4.5.4$ $0.13$ $1.13$ $7.9.7$ $0.02$ $18.7$ $79.5$ $1.13$ $4.5.4$ $0.13$ $0.14$ $1.15$ $2.97$ $18.7$ $79.5$ $1.13$ $4.5.4$ $1.25.6$ $2.97$ $2.97$ $45.9$ $79.6$ $11.3$ $0.13.5$ $0.91.7$ $0.13.7$ $0.12.7$ $0.12.7$ $0.23.7$ $45.7$ $75.6$ $11.37$ $0.12.7$ $0.12.7$ $0.12.7$ $0.27$ $45.7$ $75.6$ $0.1.2$ $0.1.2.7$ $0.1.2.6$ $0.2.7$ $0.2.7$ $45.7$ $75.6$ $0.1.2.6$ $0.1.2.6$ $0.2.7$ $0.2.7$ $0.2.7$ $270$ $24.9$ $1.1.2.7$ $1.25.6$ $0.7.7$ $0.1.6$ $0.7.7$ $270$ $24.9$ $0.1.10.0$ $0.2.7$ $0.2.7$ $0.2.7$ $0.2.7$ $270$ $24.9$ $0.10.0.0$							14		35.08	0.22	1.1	0.28
187     7.45     0.02     1.0       187     7.45.5     1.11     45.8     0.16     1.1     1.45       455     7.40.7     1.13     45.8     0.16     1.1     1.45     1.2       455     7.40.3     7.45     7.41     7.45     7.47     1.2       455     7.40.3     1.13     45.4     1.15.1     7.45     7.47       455     7.40.3     1.15.4     0.43     1.1     1.46     1.75       453     7.40     0.57     1.15.1     0.43     1.15.1     0.43       453     75.6     0.17     1.1     1.1     1.1     1.1       453     75.6     0.17     1.1     1.1     1.1     1.1       453     75.6     0.17     1.1     1.1     1.1     1.6       453     75.6     0.17     1.1     1.1     1.1     1.6       700     2.41     1.1     1.1     1.1     1.1     1.1       701     7.0     1.1     7.0     1.1     1.1     1.1       701     7.0     7.1     7.0     7.2     7.2     7.2       701     7.4     7.4     7.4     7.4     7.2     7.7     7.4 <td>11     20.7     0.02       11     20.1     45.4     0.10     1.4     7.40     0.02       11     45.4     0.10     1.1     45.4     0.10     2.97       45.5     20.1     5.4     1.1     45.4     7.40     2.97       45.5     20.1     5.1     41.5     11.5     7.93     2.97       45.5     20.4     11.5     0.12     0.12     11.5     0.03       45.4     75.6     11.5     0.12     0.12     11.6     1.06       45.7     75.6     11.5     0.1     0.1     0.1     0.1       45.7     75.6     11.5     0.1     0.1     0.1     0.1       45.7     75.6     11.5     0.1     0.2     0.2       45.7     75.6     11.7     1.1     0.2     0.2       75.6     61     17.6     1.1     0.2     0.2       70.7     24.7     7.7     1.1     1.1     0.2       75.7     5.1     1.1     1.1     0.2     0.7       75.7     5.1     1.1     1.1     0.2     0.7</td> <td><b>NPN-000</b></td> <td>664</td> <td>18.3</td> <td>0.07</td> <td>6.61</td> <td></td> <td>Ŧ</td> <td>11.5</td> <td>A 7.82</td> <td>0.16</td> <td></td> <td>0.22</td>	11     20.7     0.02       11     20.1     45.4     0.10     1.4     7.40     0.02       11     45.4     0.10     1.1     45.4     0.10     2.97       45.5     20.1     5.4     1.1     45.4     7.40     2.97       45.5     20.1     5.1     41.5     11.5     7.93     2.97       45.5     20.4     11.5     0.12     0.12     11.5     0.03       45.4     75.6     11.5     0.12     0.12     11.6     1.06       45.7     75.6     11.5     0.1     0.1     0.1     0.1       45.7     75.6     11.5     0.1     0.1     0.1     0.1       45.7     75.6     11.5     0.1     0.2     0.2       45.7     75.6     11.7     1.1     0.2     0.2       75.6     61     17.6     1.1     0.2     0.2       70.7     24.7     7.7     1.1     1.1     0.2       75.7     5.1     1.1     1.1     0.2     0.7       75.7     5.1     1.1     1.1     0.2     0.7	<b>NPN-000</b>	664	18.3	0.07	6.61		Ŧ	11.5	A 7.82	0.16		0.22
GR     1.4     7.4.0     0.02     1.0       -AA     1a7     295.2     1.11     45.4     0.16     11     2.97     31.4       -HH     b1     21.4     0.16     11     11.4     7.65     7.97     31.4       -HH     45.5     2.91     11.5     0.93     11.4     12.0     0.93     12.0       -HH     45.5     2.94     11.3     0.43     11     14.6     1.5     12.0       -HH     45.5     2.44     11.34     0.43     11.3     0.43     12.0       -HH     45.5     11.37     0.43     11.3     0.43     12.0       -CCC     45     11.5     0.77     11.4     12.0     0.77     14.8       -UCC     45     11.45     11.5     0.77     14.1     145.1     14.8       -UCC     45     7.6     34.7     14.1     35.0     0.77     10.7       -UCC     45     7.6     34.7     7.6     17.8     10.6     17.8       -UCC     45     7.6     17.8     7.6     14.8     14.8     14.8       -UCC     45     7.6     34.7     14.2     17.9     0.77     14.8	68     1.4     7.40     0.09       -44     141     43.4     0.46     11.4     72.35     2.97       -64     147     24.4     1.13     4.3.4     0.46     1.40     2.97       -64     445     740.3     6.45     11.3.4     0.43     14     74.6     2.97       -64     45.5     11.3.4     0.43     11.4     1.45     1.47     0.43       -61     24.4     11.57     0.3.7     11.4     1.45     1.47       -61     45.4     11.57     0.37     1.1     0.47       -61     45.4     11.20     0.27     1.1       -61     7.4     1.5     1.1.67     1.67       -61     45.4     1.1.5     47.0     0.77       -61     7.4     7.7     1.1     7.4     0.77							19	<b>.</b>	29.76	10-0	<b>*</b> *	0.13
-AA 107 295.2 1.11 45.4 0.16 14 211.4 72.55 2.01 12.0 -FMH 455 200.3 5.45 115.4 1.01 186.1 74.64 2.59 71.5 -FMH 455 200.3 5.45 115.4 1.01 2.5 -FM 455 200.3 12.9 -FM 455 200.3 12.9 -FM 145 11.37 0.43 12.9 -FM 145 11.37 0.43 12.9 -FM 145 11.37 0.43 12.9 -FM 145 11.27 0.43 12.9 -FM 145 11.27 0.43 12.9 -FM 145 11.2 12.00 0.77 7.0 -FM 145 11.2 12.00 0.77 7.0 -FM 145 11.0 0.77 14.0 0.77 14.0 -FM 15.4 15.4 14.1 14.1 15.4 14.0 0.77 14.1 -FM 15.4 15.4 14.1 14.1 15.4 14.0 0.77 14.1 -FM 15.4 15.4 14.1 14.1 15.4 14.1 15.4 14.1 14.5 -FM 15.4 15.4 14.1 14.1 14.1 14.1 14.5 -FM 15.4 15.4 14.1 14.1 14.1 14.1 14.5 -FM 15.4 15.4 14.1 14.1 14.1 14.1 14.5 -FM 15.4 15.4 14.1 14.1 14.1 14.1 14.5 -FM 15.4 15.4 14.1 14.1 14.1 14.1 14.1 14.5 -FM 15.4 15.4 14.1 14.1 14.1 14.1 14.1 14.1	-444 107 795.2 1.11 45.4 7.16 11.4 72.35 2.07 -444 455 700.3 C.VK 115.4 7.01 186.1 74.66 2.00 -41 34.0 13.97 0.43 -41 45.1 11.37 0.43 -41 45.1 11.27 0.43 -41 45.1 11.27 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 11.26 1.67 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41 45.1 1.61 -41							9	1.4	7.4.)	20.0	1.0	0.03
HI       KI       21.6       2.65       2.64       12.0         HH       KS       20.1       C.VC       113.4       0.01       1.50       0.43       15.0         HH       KS       20.1       C.VC       113.4       0.01       0.1       1.50       0.43       15.0         HC       MI       MS.1       11.37       0.43       12.0       0.77       15.0         HC       MI       MS.1       11.37       0.43       17.6       1.67       15.0         HC       MI       MS.1       11.37       0.77       10.77       10.77       10.8         HC       MI       MS.1       MI       MS.1       11.6       10.7       10.7       10.8         HC       MS       MI       MS.1       MI       MS.1       10.8       10.8       10.8         HU       MS       MI       MS.1       MI       MS.1       10.7       10.8       10.8       10.8         HU       MS       MI       MS.1       MI       MS.1       10.8       10.8       10.8       10.8       10.8       10.8       10.8       10.8       10.8       10.8       10.8       10.8	HHH     4%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%     7%    <		147	2	5	-	4	ī	4-11-	11.02	10.4	11.4	19.0
-FMH       4.5, 280.3       C. V ⁵ 115.4       0.93       1.59       1.59       1.59       1.59       1.59       1.59       1.59       15.9         -CCC       8.4       11.37       0.43       10.43       17.9       1.59       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9       15.9<							;		81.4	27.65	2.93	17.0	EC - 1
				1 4									
-CCC 454 148.4 1.55 61.2 0.52 1.41 81.6 54.64 11.57 0.63 12.4 -CCC 454 148.4 1.55 61.5 0.57 12.4 -CCC 454 148.4 1.67 14.8 12.6 0.27 12.6 -CCC 453 75.4 12.6 0.27 12.6 -CCC 453 75.4 12.6 1.67 14.8 -CCC 453 75.4 1.67 14.8 12.6 0.27 14.8 -CCC 453 75.4 15.6 14.2 4.0 101.0 0.35 7.6 -FUL *** 15.4 1.61 7.7 14 24.0 101.0 0.35 7.2 -FUL *** 15.4 1.61 7.1 14.1 15.8 117.0 2.35 7.8 -FUL *** 5.4 0.21 14.1 15.8 117.0 2.90 18.3	-UCC 45% 148.4 1.55 0.3.2 0.32 1.1 41.4 11.57 0.43 -UCC 45% 148.4 1.55 0.43 41 45.1 11.4 12.06 0.27 -UUC 453 75.8 7.70 34.3 7.28 1.41 35.0 47.56 0.57 -UUC 453 75.8 7.70 34.3 7.28 1.41 35.0 47.50 0.57 -11 2.4 0 1.1.0 0.2 1.1 -11 2.4 5.4 1.1 1.1 1.1 1.1 2.4 0 1.1.0 0.2 1.1 -11 2.4 5.4 1.1 1.4 1.1 1.1 2.4 0 1.1.0 0.2 1.1 -11 2.4 1.4 1.4 1.1 1.2 1.1 1.0 2.1 2.00		n. r #		•	n			1.081				
-CCC 454 148.4 1.55 61.2 0.52 1.41 81.8 54.64 1.18 35.8 -CCC 454 188.4 1.55 61.7 19.8 -CUC 453 75.4 75.4 1.57 19.8 -CUC 453 75.4 75.4 1.57 19.8 -CUC 453 75.4 1.50 1.50 1.50 14.2 -CUC 453 75.4 1.50 1.1 14.6 -CUC 453 75.4 1.50 1.1 15.8 -CUC 453 75.4 1.1 15.8 1.1 1.0 1.2 -CUC 453 75.4 1.1 1.2 1.2 1.0 1.1 1.2 -CUC 453 75.4 1.1 1.2 1.2 1.2 1.1 1.0 1.2 1.2 -CUC 453 75.4 1.2 1.2 1.2 1.1 1.0 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2	-UCC 414 144.4 1.55 63.2 0.52 HI HI.A 54.64 1.14 -UCC 415 75.4 1.55 61 17.4 12.06 9.27 -UCC 415 75.4 75.4 75.4 12.06 9.27 -UCC 415 75.4 75.4 12.0 9.77 0.11 -11 24.0 1.1.0 9.77 0.11 -11 24.0 1.1.0 9.75 1.1 -11 24. 54.4 1.1 1.4 1.1 1.1 24.0 1.1.01 2.75							5		1.37	0	12.0	0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			4		4			-	•		:		
UL 453 75.8 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0			1			:							
-UUC 453 75.4 (.70 34.2 7.28.141 35.0 47.54 6.50 14.2 -UUC 453 75.4 (.70 1.1 1.0 1.1 3.2 42.00 1.1 12.0 								30		1 2. 00	1.0.1		
-UUC 453 75.4 1. 20 34.3 7. 7.98.2 41 32.2 42.09 1.10 14.6 61 32.2 42.09 1.10 14.6 61 7.4 9.77 7.11 1.3 -++ 201 24.0 1.10 7.1 1.1 1.16 24.0 1.01.0 0.35 7.2 -fulb *** 15.4 1.1 5.4 1.17.5 UT 15.5 710.0 14.3 -111 24 55.4 0.21 14.1 1.12 51 51.4 10.0 0.0 14.3													
b1     32,2     42,00     14,0       +++     7,4     9,77     7,1       +++     7,0     7,1     7,1       +10     7,1     7,1     7,1       +11     7,4     54,4     7,1       -111     7,4     54,4     14,1	b1     32.2     42.60     1.10     14.       -+++     200     24.0     (.10     7.2     0.17     0.15     7.       -+++     200     24.0     (.10     7.2     0.16     7.2     7.2       -+++     200     24.0     7.2     1.0     7.2     7.2     7.2       -+++     200     24.0     7.2     1.1     24.0     2.35     7.2       -++     11     24.0     1.2     1.4     0.12     1.4     2.00     1.4	140-141.	4		01 · · ·	. c. 11			34.0	47.54	0.50	14.2	0.42
61     7.4     9.17     5.1     7.5       -+++     201     24.0     1.1     1.1     7.2       -fulb     **     1.1     7.1     5.4     7.7       -fulb     **     1.1     7.1     5.4     7.2       -fulb     **     1.4     5.4     7.17     1.4	64 7.4 9.77 5.11 ¹ . -+++ 20Л 24.9 (.1Л 7.2 7.76 H. 24.9 [ЛЛ.03 0.35 7. -fuu *## 15.4 г.л. 6.4 г.л.т.; H. 24.9 [ЛЛ.03 0.35 7. -fuu *## 15.4 г.л. 14.1 л.12 H. 51.4 [ЛЛ.03 2.00 14.							, ,	37.7	4 2.69	1.1.	14.0	1. 31
-+++ 201 24.0 (.10 7.2 0.16 HL 24.0 101.03 2.35 7.2 -fulb mer 15.4 F.P. 5.4 F.ATTEUT - 15.2770,077.55 F.A. -111 X5 54.4 0.21 14.4 0.12 51 50.4 103.03 2.00 14.3	-+++ 200 2440 (.10 7.2 0.06 HL 24.0 107.03 2.35 7. -Full *## 15.4 F.F. 5.4 'F.T.T.T.T.T.T.T.T.T.T.T.T. -111 X5. 54.4 0.21 14.1 0.12 14 54 10.01 2.00 14.							J	~	11.0	1.5		1.0
-Full Per IF.4 F.7 5.4 F.775 UT TIT.577777.07 F.55 F.4.4 -111 //A 54.4 0.21 14.4 0.1225 61 51.4 10.01 24.3	-fiuls and Internetics 5.4 resolution Internation ("Figure 1.4") -111 res 54.4 0.21 14.1 1.12 1.1 54.4 111.01 2.00 14.	<b>ことら - ナ ナナ</b>	<b>U</b> ed		ر ۱۰	1. 1	٩٢.	ĩ	24.9	1.1.63	٢.	•	0.19
					2								,
-111 X4A 54.4 0.21 14.1 0.12 14 54.0 0.00 14.3	-111 / 10° / 10° / 10° / 11° / 11° / 10° / 10° / 11°		•	-	•		•				•	<b>•</b>	
		cet -111		54.45	0.13		1.	5	•••	10.01	2.00	13	1. 29

PIT-FIL FILE

	134	È.	<u>M-117-</u>	6.0			•	V F F T	C 0 7	4 5	
11		PARIDAY	5	V BU LAGN	_	Ĺ	VAN/XAY		*CAR	KPM/WAY	A CAP
ttt - JJJ	558	6.5	• 0 • 0					100.00	0.1.	5 • 2	0.17
666-444	1-1	171.2	0.45	25. ⁰	10.0		80°1	52 .1 7	1.24	2.11	0.35
						1		24.14		Å. 3	0.56
						<b>1</b> 9	* ° C #	19.10	29.0		0.20
FFF-111	543	101.5	0.39	50.1	0.40		80.5	79.3	1.23	5 * # #	1.17
						Ŧ	u•12		0.29	11.6	0.30
10-11	612	1.0.1	P.1.	28.6	61.0	: #	26.9	57.55	16.0	14.5	0.43
						Ŀ	19.A	42 . 4 5	ς. 30	12.1	۳.
10-11	696		C.17	31.5	0.76		24.1		C.37	11.9	0.54
						1	20.9	*	0.75		1, 31
111-111	<b>Vo</b> ?	20.5	1 . K	6.2	50.0	H.	20.4	10.00	0.2A	6°5	0.15
HHH- 3 4 4	140	6.7	10.0	1.4	*0.0	: CL		10 3 . 00	0.10	1.?	0.17
666-AAA	4 8 2	191.1	61.0	1.24		0 à .:	86.7		3.27	41.6	4.13
			I			Ĩ	49.2		9.68	~	0.67
						ר ה ני ה	41.1	21.49	0.52	19. H	0.65
					1			1		ł	
100-844		1 84.9	0.72	82.	0.67	G :	۰. ۱	<b>`</b>	2.38		2.12
						i g		25. H9	0.75	2.12	00
						5	22.2	11.76	C.P.C		0.87
966-CCC	512	125.0	9 4 F		0.54	: er	8 J . 1	6 4 ° 0H	1.23	4	1.51
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	:	;		*		R D	0.34	36.92	1.70	24.7	2.56
000-99 <b>0</b>	707	70.4	0.27	54.6	0.43	. FU	.1.		1.56		3.07
						<b>.</b>	14.7	16.95	02.7		9.0
			-			3	19.4		0.17		
G6G-EEE	348	18.3	10.07	- 10. J	0.74	1	19.1	100.00	9.65	0 vl	0. 00
666-MMM	9 1 9	8 ° 9	4 J - J	0° \$	40° u	2	а. Э	1 00 . O C	16.0	5.0	0.50
LLL-324	231	33.8	0.13	ы. 5	0.07	U#	27.4	81	1.04	¢	•
						5	• • • • •	19.48	0.22		0.1.
8 8 - MMM	155	167.9	54.0	123.7	11	. RU	107.0	÷	4.07	41.1	8.07
			- 1			3	15.0	$\sim$	0.5	1.12	0.89
						2 <b>-</b>		5 <b>1</b> - 1	0.25		
	6 = 2	738.7	10.11	, 61 Å	0 - C	ن ۵	154 8	1	6 . V .		· 1 5
					•		÷	17.09	0.62	5	0.35
						5	30.8		1.13	Î	4 H O
						9	0.1		0.01		0-01
יאא-נרר	1 V E	1.1.7	((,))	12.4	1 . L	с. ч.	137.0	٤.	\$	40.7	46° 4
i		:				5.		<b>£</b> :	3	11.0	¥

нин-ОПО Кин-L LL Инн-L LL Инн-bbb			-	A J U Z A da						
<del>ИМИ -6 6 6</del> ИМИ -6 6 6		115.9	0	03.5	3.52 : 51	h-	64°19	1.14	42.0	1. 30
ИМН-Е ЕЕ ИНН-6 - 6 ИМН-6 - 6					<b>4</b> 9	56° 5° 56	33.61	0.56	21.5	9.0
HHH - F + F HHH - 6 66	F	1.41	0.17	12.7	n. Th : LT	17.1 107	104.03	19.0	2.51	1.10
1111-6 66	760	8.6	0.03	1.4	n.ce : 6L	4.R 1CO	20.05	C.10	5.1	0.17
	518	9.9	•0•0	5.9	0.04 : 4D	•	80.42	0.30	<b>6</b> .0	•
					61		•5₽	0.01	1.0	0.13
ררר-אאנ	240	2.95	u. l n	0°5	0°.15 : 60		••51	0.71		•
					5	•	11.92	0.11	0 C	0.08
					19	•	11.57	0.04	9°C	0.0
111-444	349	75.2	6.29	27.7	r.23:68	62.7 F1.	1.45	0.49	2.15	0.7
					14		14.55	54.0	9 · 9	0.41
111-644	2 8 8	59. K	r.23	14.6	n.12 : GP	54.R 1CO	C0 - 0 C	0.45	14.6	0 . A 5
111-000	194	13.1	0.13	•• 1	0.n5 : GR	35.7 101	101.00	0.47	<b>6.</b> 1	0.19
000-111	215	1.4	0.28	17.0	14 . 11	1 2 2 3	78.04	1.01	-	
					•		25.00	0.26		0.13
111-66	256	45.9	0.16	10.7	0.09 : 17	41.9 107	107.00	1.59	10.7	0.97
111-666	5 7.8	3.2	10.0	1.7	n.01 : WT	3.2 100	10.00	0.11	1.1	0.15
	5 4 9	101.1	0° 39	57.8	0.47 : RD 6L	74.8 77 23.5 22	77.24	3.02	4 * 4 4 * 5 1 1 2 2 2	
1.J.J668	612	100.5	0.65	34.5	n. 52 : GL		60.4 F	1.1	27.4	0.00
ĺ						1		1.00	1.01	5
111-616	386	125.2	8**0	F. 9 *	n.40 : PD 6L 41	07.5 54 00.4 35	51.89 31.40	0.71	24.1 17.9	2.59
000-665	5 a 5	55.7	12.0	32.2	0.76 : RD	e 2	82.93	67.1	20.7	2.65
						-	17.10	C.1*		A 1.0
J.J.J-E.E.E	55.8	10.3	•0•0	5.7	19 : GN.O	e.	7.62	0.04	9°C	0.10
					- 3	5.1 40	9.36	0.18	2.8	0.26
443-0P0	\$29	7.6	10.0	c • • •	N.73 : GL	7.4 107	۰.00	0.12	•••	0.13
	152	3 <b>.</b> . 5	<b>1</b> .	¢**	15 15: 40.0	35.7 9A 1.2 3	1.35	1. 34 0.02	<b>b</b> * c	0. AN
	UYC	21.9	HC*0	5.7	<b>∩</b> ,: RD	21.9 LJN	[]], 03	0.83	5.7	0.57
	F.	1.1.1	13.0	H B	n.c7 : LT	11. 1 11	דרה. הנ	C 4 2	0 • 4	64.0
1 H - 1 N	208	17.1	c	<	0. 20 . 61	37.0 65	, 0 , 1 , 0 , 1	0.54	15.4	0.52
X # 4 - 6 6 6	5.1			4.44						

HARE T	n151.	¥10/×-0	111	4 10/ ad >	111 ID	A VU/X 1d			AVE/HAX	BC AR
							1	1.42	11.7	1.23
***-600	179	175.2	0.67	31.4	0.20 : GL	131.5	74.09	÷ • 02	21.5	6.78
					1 1	43.4		1.57	7.8	0. 75
111-111	330	31.7	C.12	10.5	49 : AJ U	1.16	10.00	0.45	5.1	0.33
LL.L -HHR	197	50.5	60	10.4	a9 : 60°0	54.5	11 9.00	6.A.J	11.0	0.33
111-000	370	R. A	£0° J	5.5	A.C.S : 6P	5.5	10.01	\$1.0	2.1	0.10
*****	441	101.5	0.39	1.01	0.12 : 60	÷.,	67.	1.97	11.2	
				i.	4	33.7	2		0	
HHR-982	914	6° JÝ	5	1.45	0.26 : 64			0.42	15.0	6 <b>4</b> ° C
					9 - 9 -	52	34.62	- n -	11.6	0.18
							-	0.34	2°5	0 <b>. #</b>
	845	34.4	EL 0	111	19 . 11.	1.41	i i	- 6.2.3 -	R.2	0.21
					69	14.2	•	0.20	2.2	0.22
					17		7	0.15	2.1	0.19
000-###	<b>\$</b> u <b>\$</b>	23.1	0.09	11.4	0.10 : 47	13.7	57.52	0.45	h. 7	0.61
					9	x !	ŝ	0.12	4.2	0.1
					64	-	16.2	0.02	1.7	0.02
NNN-AAA	179	131.7	0.40	23.6	n.19 : HL	57.1	43.52	C.A.O	17.3	0.27
					5		29.57	6.4.0	7.0	0.21
					3	•••	14.42	1.27	٤.٩	0.57
Han - Ber	- 549	1 62.4	0.39	71.5	.0.5H : GP	7.24	a 3. 5d	3.63	31.J	3. 97
						4.14	40°#¢	C.5P	29°9	0.75
					19	1.01	14.1	0.06		
NNN-CCC	*uL	30.6	0.12	21.5	0.14 : GR		19.91	0-17	8.8	0.27
   						1.11		0.0		0.71
					61	7.7	23.61	0.11		0.17
000-NNN	644	1:1	0.06	19.61	U.L4 : 64	4.1	12.12	0.11	9 5	11.0
					19			<b>c.11</b>	<b>.</b> .7	0.17
<b>JUE-IU</b>	191.	- 41512	1.54	4.94.A	5.72 . GP	2241	¥4.5A	2.01	241.6	1:53
					19	131.5	33.68	10.4	1.154	1.24
					₽!:	101.5	25.40			4. YO
					5		1.84	1.1		, o, a
*****	2178	C	1. 13	7 . 5. 7	5.94 1 AL	147.4	54.62	2.75	\$19.6	1 0. 65
						4 ° 4	14.79		130.5	
						-				-

A .....

ē		
	7193.6	3854.0
	6525.5	3036.3
L	1.5201	3211.1
	2639.6	1005.0
11 2	2787.6	1110. 7

## APPENDIX B

## **RESULTS OF DECEMBER 1979 EXERCISE**

## B.1 The Experiment at M.I.T./FTL

The pilot experiment was performed at M.I.T. the week of December 17-21, 1979. The five airline teams were assigned aircraft as follows:

Team	<u>DC-10</u>	<u>707</u>	<u>727</u>	<u>DC-9</u>
Blue	3	5	12	
Gold		5	10	
Green		5	5	
Red		3	5	2
White			4	1

Each team was represented by one or more players from ECON-FTA staff and the FAA. The total air transportation network involved four major hubs, of which three were slotted, four intermediate size airports and five minor airports. There were 60 aircraft in all, allocated among the five airlines as shown above. Each airline was told its route structure and could obtain detailed information on the demand in each market.

The scheduling of flights was undertaken during the set-up phase, prior to the first slot auction on December 18, 1979, without any slot restrictions. This prior effort also served to test various aspects of the scenario and to allow changes to be made in passenger demand, costs and other structural aspects of the airline management game (AMG). Then, using the flight schedule profile (number of flights by hour and airport) artificial hourly quotas were selected for the three major hubs:

Airport	Quota (flights/hour)
Α	13
В	12
С	15

These were selected so that excess demand would surely occur at peak hours. For instance, the original schedules had 26 operations in one peak at Airport A.

The major interations of the slot auction experiment were undertaken. Each interation was conducted as follows:

Slot Auction	Bidding round 1
Slot Auction	Bidding round 2
Slot Auction	
Slot Auction	Bidding round k

Run market aggregation--print equilibrium prices Reschedule flights subject to slot allocation Trade slots in aftermarket is possible and necessary Airlines submit schedules to AMG Run AMG simulation

In the first iteration there were four rounds of bidding, in the second only two. The auction was terminated by a voting procedure: if four out of five teams voted to stop the auction, it was stopped; otherwise another round of bidding was taken. The auctioneer announced that he could terminate the bidding at any round after the first round based on other criteria, such as lack of change in prices and/or allocations, but in practice this was not applied during the pilot experiment.

**B.2** Problems with the Experiment

There was some evidence of dynamic changes in bidding between rounds, probably due to a combination of learning by the players and deliberate bidding strategy, including speculation in slots. One could not say, looking at the results that the market "settled down." Probably many more rounds of bidding were needed for stabilization of the market. Time was not available at FTL for a large number of rounds. Initially, during Iteration 1, Rounds 1-3, the mechanics of processing bids was rather slow. By the time we had achieved efficiency in bid processing there was only one day of the experiment left, and hence the abbreviated auction in Iteration 2. There were several major problems in the implementation of the experiment, as far as the scenario and groundrules were concerned.

- 1. Ambiguity about the players' freedom to change route structure
- 2. An "average" cost function which hurt the small airlines profitability
- 3. Start-up difficulties in player understanding of the bidding procedure and market mechanism
- 4. Fares were fixed and players could not change them
- 5. No cash flow constraints were imposed.

We discuss of these problems in turn.

I. Apparently some players (team Gold in particular) perceived the game as if deregulation were in full force, meaning that the airline could add or drop any <u>routes</u> it wished. Other players accepted their initially given routes as fixed and used only their ability to add or drop <u>flights</u> on those routes to make profits. This difference in groundrules between airlines emerges clearly in comparing the earnings results for teams Green and Gold ^{*}; while Gold was able to substantially improve its profitability from Iteration 0 to Iteration 2 by competing vigorously in Green's markets, Green steadily lost ground. In a properly designed experiment, all players should have identical groundrules.

It doesn't matter so much whether the groundrules do or do not reflect deregulation. It is essential that this decision be made by the game administrator and announced unambiguously to all players.

In approaching their scheduling problem for a six-month season, airlines would mostly enter the slot market with their flight cycles already mapped out. Changes as a result of slot allocation in these cycles would tend to be marginal,

"See Tables 4 and 5.

since an accommodation to slot restrictions can be expected via "sliding." The difference in behavior between airline players invalidates the simulation to this extent.

2. The cost allocation--e.g., the cost per passenger for handling passengers on each flight--was derived from averages for aircraft type, and hence did not allow for the lower overhead of a small airline (White) as compared with a large airline (Blue). This resulted in a situation where White could not possibly be profitable and Blue could hardly fail to make profits. It is impossible to say what effect this had on the players bidding. See problem (5) below for further discussion.

3. The bidding instructions were clear and unambiguous, but fairly complicated. Not enough time was available for players to learn bidding procedures and strategy. Apparently some players were mistakenly under the impression in Round 2 of Iteration 1 that all bids had to be submitted from scratch. This caused some confusion in the bid processing. Many players entered zero bids, which have no effect whatsoever on this type of market. To enable players to register damands for slots at essentially no cost to the airlines, we suggested a minimum bid of one dollar, which then allowed slot allocation to take place at a price of \$1.00 in off peak hours. From Round 3 of Iteration 1 on, the zero bid was taken as a cancellation of bids previously submitted in the same auction.

Players evidently thought they could individually influence the slot market to a greater extent than is the case. There was a considerable amount of strategic posturing in the bidding, which is a natural part of learning how to use the market, but which does not contribute useful information to the experiment.

Slot speculation was another example of unrealistic behavior--it is hard to believe the airlines would buy a great number of slots which they don't plan to use,

particularly if they must forfeit such slots after one month of nonuse. Nevertheless, speculation is a possibility which should be considered, and some thought might be devoted to penalizing more heavily slot holders who don't use their slots.

4. The fixed fares limited the players unnecessarily and do not reflect the competitive reality. This problem was significant because of the unusually high costs experienced by small airlines due to incorrect cost allocation (the "average" overhead problem--see (2)) and also entailed a lack of consideration of the airlines of whether or not to pass along slot costs to passengers.

And and a state

5. The worst problem was occasioned by the absence of adequate financial constraints. Since money was virtually "free" to the players, their bidding exceeded industry net earnings by \$43,668 per day at one point in the first auction. Subsequent rounds of bidding failed to completely correct this problem. The final round, for instance, shows net industry earnings of \$62,239 per day and slot payments of \$43,840 per day. Since the earnings include operations at nonslotted airports, the operations at slotted airports may still show a loss.

TABLE B.1A SLOT PRICES AT END OF ITERATION 1 (DOLLARS PER OPERATION)					
HOUR	A	В	С		
0600	0	0	0		
0700	151	63	0		
0800	713	353	1		
0900	2	101	100		
1000	1	152	276		
1100	1	328	0		
1200	1	351	0		
1300	100	14	305		
1400	1	176	2		
1500	126	14	500		
1600	179	76	1		
1700	301	2	2		
1800	2	353	1		
1900	1	100	14		
2000	1	276	0		
2100	0	177	0		
2200	0	0	0		

A STATE OF A STATE OF A STATE OF A STATE OF A STATE OF A STATE OF A STATE OF A STATE OF A STATE OF A STATE OF A

A State of the American State of the American State of the American State of the American State of the American

TABLE B.1B SLOT PRICES AT END OFITERATION 2 (DOLLARSPER OPERATION)				
HOUR	A	В	С	
0600	3	3	0	
0700	740	3	2	
0800	0	19	3	
0900	155	5	103	
1000	56	6	4	
1100	42	253	3	
1200	157	157	6	
1300	332	5	3	
1400	7	6	6	
1500	182	6	58	
1600	244	95	3	
1700	351	5	3	
1800	114	207	13	
1900	6	6	3	
2000	6	7	0	
2100	0	7	0	
2200	3	3	0	

TABLE B.2 POTENTIAL SLOT REVENUES (MILLIONS OF DOLLARS PER HALF-YEAR SEASON)							
AIRPORT A B C ALL							
1.1	0.468	0.745	1.080	2.293			
1.2	1.640	2.171	1.455	5.266			
1.3	2.314	3.484	2.692	8.490			
1.4	3.697	5.478	3.245	12.420			
2.1	2.972	0.320	0.032	3.324			
2.2	5.611	1.713	0.567	7.891			

TABLE B.3 NET EARNINGS BEFORE TAXES OR SLOT PAYMENTS (IN MILLIONS OF DOLLARS PER HALF-YEAR SEASON)						
AIRLINE ITERATION 0 [*] 1 2						
BLUE	4.30	4.17	4.13			
GOLD	-4.99	-1.07	1.69			
GREEN	6.00	4.98	5.53			
RED	0.270	0.067	0.720			
WHITE	-1.020	-0.994	-0.867			
ALL	4.560	7.153	11.203			
*THERE WERE NO SLOT RESTRICTIONS IN THIS INITIAL ITERATION.						

TABLE B.4 POTENTIAL SLOT PAYMENTS AFTER EACH BIDDING ROUND (MILLIONS OF DOLLARS PER HALF-YEAR)							
ITERATION         I.1         I.2         I.3         I.4         2.1         2.2							
BLUE	0.478	1.548	1.863	4,030	1.881	2.469	
GOLD	0.611	1.369	2.394	3.533	0.003	1.254	
GREEN	0.603	1.945	1.736	3.001	0.878	2.102	
RED	0.094	0.117	0.435	0.578	0.048	0.228	
WHITE	0.472	0.541	0.670	0.854	0.075	0.080	
ALL	2.258	5.520	7.0 <b>9</b> 8	11.996	2.885	6.133	

A Shirt Courses

A STATE OF A STATE OF A STATE OF A STATE OF A STATE OF A STATE OF A STATE OF A STATE OF A STATE OF A STATE OF A

TABLE B.5 NET EARNINGS AFTER SLOT PAYMENTS, BEFORE TAXES         (MILLIONS OF DOLLARS PER HALF-YEAR)					
AIRLINE ITERATION	0	1	2		
BLUE	4.300	0.140	1.661		
GOLD	-4.990	-4.603	0.436		
GREEN	<b>6.00</b> 0	1.979	3.428		
RED	0.270	-0.511	0.492		
WHITE	-1.020	-1.848	-0.947		
ALL	4.560	-4.843	5.070		

TABLE B.6 SYSTEMWIDE PERFORMANCE OF ALL FIVE AIRLINES				
FACTOR ITERATION	0	1	- 2	
1. LOAD FACTOR	0.627	0.620	0.650	
2. AVERAGE STAGE LENGTH (MILES	) 338	357	387	
3. AVERAGE TRIP LENGTH "	423	437	456	
4. RATION OF (3) to (2)	1.25	1.22	1.18	
5. TOTAL FLIGHTS	222	211	187	
6. TOTAL RUNWAY OPERATIONS	974	938	830	
<ol> <li>RUNWAY OPERATIONS AT AIRPOR A, B, C</li> </ol>	TS 580	544	488	
8. UNUSED SLOTS AT A, B, C	100	136	192	

-

.....

1.1 ×

1.3 3.4

