



DELAWARE RIVER BASIN SAMBO CREEK, MONROE COUNTY PENNSYLVANIA

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DACW31-80-C-0017

MIDDLE DAM

NDI ID No. PA-00256 DER ID No. 45-3

BOROUGH OF EAST STROUDSBURG

PHASE I INSPECTION REPORT

NATIONAL DAM INSPECTION PROGRAM

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Prepared by

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For

DEPARTMENT OF THE ARMY Baltimore District, Corps of Engineers Baltimore, Maryland 21203

JANUARY 1980

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PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the spillway design flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The spillway design flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

i

DELAWARE RIVER BASIN AMBO CREEK, MONROE COUNTY 9 PENNSYLVANIA National Dam Inspection Program, MIDDLE DAM (NDI-ID - PA-00256) (DER-ID 10-45-3) BOROUGH OF EAST STROUDSBURG-PHASE I INSPECTION REPORT - ; NATIONAL DAM INSPECTION PROGRAM 12/103 JANUARY 1980 15 DHCN(31-80-C-0017/ CONTENTS Description Page SECTION 1 - Project Information . . 1 SECTION 2 - Engineering Data ... 7 SECTION 3 - Visual Inspection . . . 10 SECTION 4 - Operational Procedures . . 13 SECTION 5 - Hydrology and Hydraulics 14 . SECTION 6 - Structural Stability 17 SECTION 7 - Assessment, Recommendations, and 19 Proposed Remedial Measures APPENDICES Appendix Title Are Section 1 Checklist - Engineering Data. Α Checklist - Visual Inspection В

Hydrology and Hydraulics. Plates.

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PHASE I INSPECTION REPORT

NATIONAL DAM INSPECTION PROGRAM

BRIEF ASSESSMENT OF GENERAL CONDITION

AND

RECOMMENDED_ACTION

Name of Dam:

Middle Dam NDI ID No. PA-00256 DER ID No.45-3

<u>Size</u>:

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Small (24 feet high; 197 acre-feet)

Hazard Classification: High

<u>Owner</u>:

Stream:

Borough of East Stroudsburg Larry Comunale, Borough Manager Box 303 East Stroudsburg, Pa. 18301

State Located:

County Located:

Date of Inspection:

13 November 1979

Pennsylvania

Sambo Creek

Monroe

Based on visual inspection, available records, calculations, past operational performance, and according to criteria established for these studies, Middle Dam is judged to be unsafe, non-emergency because the spillway capacity is rated as seriously inadequate. Under existing conditions, the spillway can pass only about 22 percent of the Probable Maximum Flood (PMF) without overtopping of the dam. If low areas on the top of the dam were filled to the design elevation for the top of the dam, the spillway would pass about 33 percent of the PMF. For either condition, it is judged that the dam could not withstand the depth and duration of overtopping that would occur for the 1/2 PMF. Failure of the dam would cause an increased hazard for loss of life downstream. As a whole, the dam is judged to be in fair condition. No stability problems were evident for the embankment. Stability analyses were performed for the spillway weir for this Report. The results do not deviate significantly from recommended guidelines for stability under normal loading conditions, but the results indicate that the weir might fail by over-turning under the assumed maximum loading conditions because the resultant was found to be located outside of the toe. It is noted that the analyses were based on a number of assumptions and that the results are only approximate.

There are no drawdown facilities at the dam. Water can be discharged from facilities at a treatment plant located 0.3 mile downstream, but the ability of the facilities to drawdown the reservoir is questionable.

The following measures are recommended to be undertaken by the Owner, in approximate order of priority, immediately:

(1) Perform additional studies to more accurately ascertain the spillway capacity required for Middle Dam as well as the nature and extent of measures required to provide adequate spillway capacity. Take appropriate action as required.

(2) Make repairs to the spillway apron. Perform additional investigations and studies to more accurately assess the stability of the spillway weir as well as the nature and extent of measures required to provide adequate factors of safety for all expected loading conditions. Take appropriate action as required.

(3) Provide properly designed facilities to collect and dispose of water along the toe of the dam and in the valve chamber. The facilities should include measurement devices. Seepage should be monitored, and records of seepage should be maintained.

(4) Perform a study to determine whether the reservoir could be drawn down over a reasonable period of time with the existing facilities at the treatment plant. Take appropriate action as required to ensure adequate drawdown facilities.

(5) Undertake remedial measures for other minor maintenance items.

All investigations, designs, and supervision of construction should be performed by a professional

engineer experienced in the design and construction of dams. The seepage monitoring program should also be performed or supervised by a professional engineer.

In addition, the Owner should institute the following operational and maintenance procedures:

(1) Develop a detailed emergency operation and warning system for Middle Dam.

(2) During periods of unusually heavy rains, provide round-the-clock surveillance of Middle Dam.

(3) When warnings of a storm of major proportions are given by the National Weather Service, the Owner should activate his emergency operation and warning system.

(4) Institute an inspection program such that the dam is inspected frequently. As presently required by the Commonwealth, the program should include a formal annual inspection by a professional engineer experienced in the design and construction of dams. Utilize the results to determine if remedial measures are necessary.

(5) Expand the existing maintenance program so that all features of the dam are properly maintained.

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MIDDLE DAM

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Submitted by:



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Vitiliuding. FREDERICK FUTCHKO

Project Manager, Dam Section

Date: 11 February 1980

Approved by:

DEPARTMENT OF THE ARMY BALTIMORE DISTRICT, CORPS OF ENGINEERS

W. PECK JAMES Colonel, Corps of Engineers District Engineer

Date: 29 Fab / 980



MIDDLE DAM

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Overview

DELAWARE RIVER BASIN

SAMBO CREEK, MONROE COUNTY

PENNSYLVANIA

MIDDLE DAM

NDI ID No. PA-00256 DER ID No. 45-3

BOROUGH OF EAST STROUDSBURG

PHASE I INSPECTION REPORT

NATIONAL DAM INSPECTION PROGRAM

JANUARY 1980

SECTION 1

PROJECT INFORMATION

1.1 General.

a. <u>Authority</u>. The Dam Inspection Act, Public Law 92-367, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a program of inspection of dams throughout the United States.

b. <u>Purpose</u>. The purpose of the inspection is to determine if the dam constitutes a hazard to human life or property.

1.2 Description of Project.

a. <u>Dam and Appurtenances</u>. Middle Dam is an embankment dam 24 feet high at its maximum section and 634 feet long, including the spillway. The dam has a stone masonry corewall with earthfill upstream and earthfill and rockfill downstream.

The spillway is located near the right abutment of the dam. The spillway weir is concrete that was placed over stone masonry. The structure is 42 feet long, but a 2-foot wide pier at the center reduces the effective crest length to 40 feet. A concrete apron is located at the toe of the weir. The outlet channel is rectangular and is lined with stone.

An intake structure is located in the reservoir upstream from the toe of the dam. Three slide gates are located at various levels within the structure. 16-inch diameter cast-iron pipe extends from the base of the intake structure to a point near the upstream toe of the dam. At that point, fittings provide connections with two 10-inch diameter cast-iron pipes that extend through the dam. A valve chamber is located along the downstream side of the corewall. A tunnel extends from the valve chamber to the downstream toe of the dam, providing access to the valve chamber. One gate valve for each 10-inch pipe is located in the valve chamber. From the valve chamber, the two 10-inch pipes extend downstream about 0.3 mile to a treatment plant. There are no conduit outlets at the dam itself, but blowoff valves are located at the treatment plant.

The various features of the dam are shown on the Photographs in Appendix C and on the Plates in Appendix E. A description of the geology is presented in Appendix F.

b. <u>Location</u>. Middle Dam is located on Sambo Creek in Smithfield Township, Monroe County, Pennsylvania, approximately 3 miles north of East Stroudsburg. Middle Dam is shown on USGS Quadrangle East Stroudsburg, Pennsylvania, at latitude N 41° 03' 00" and longitude W 75° 10' 50". A location map is shown on Plate E-1.

c. <u>Size Classification</u>. Small (24 feet high, 197 acre-feet).

d. <u>Hazard Classification</u>. High hazard. Downstream conditions indicate that a high hazard classification is warranted for Middle Dam. (Paragraphs 3.1e and 5.1c (5)).

e. <u>Ownership</u>. Borough of East Stroudsburg, Larry Comunale, Borough Manager, Box 303, East Stroudsburg, Pa. 18301.

f. <u>Purpose of Dam</u>. Water supply for Borough of East Stroudsburg.

-2-

Design and Construction History. The original 2. design of the dam was performed in 1914 for the Borough of East Stroudsburg by Westbrook and Voss, Civil Engineers and Surveyors, of Stroudsburg, Pennsylvania. Construction was started in 1914 under the supervision of P. L. Voss, of Westbrook and Voss, and W. E. Van Vliet, who was both Superintendent of construction and President of the Borough Council. Numerous changes in design were approved by the Pennsylvania Water Supply Commission (PWSC) while the dam was under construction. Although most of the work was finished by 1916, the dam was not completed in full accordance with the approved plans until 1922. The design drawings for the original construction are shown on Plates E-2 and E-3. Changes that were approved during construction are also shown on those Plates.

In 1930, the Borough wanted to increase the storage capacity of Middle Dam. The design of the necessary modifications was prepared by E. F. Hess, the Borough Engineer. An as-built survey was made by Mr. Hess in 1930 prior to design of the modifications. Results of that survey are shown on Plate E-4. The proposed modifications included raising the embankment by 4 feet and raising the spillway by 3 feet. The spillway crest length was to be increased from 20 feet to 40 feet. The modifications were approved by the Commonwealth. The approved design is shown on Plate E-5. The construction work was performed in 1931 under the supervision of the Borough Engineer, and was the last major change made to the embankment and spillway. Measurements made during the inspection for this Report indicate that the embankment was not modified in accordance with the approved design.

In 1964, a new intake structure was constructed in the reservoir area upstream from the toe of the dam. The design was performed by Buck Seifert and Jost, Consulting Engineers, New York, New York. The old intake structure was abandoned and a pipe from the new intake structure was connected to the two existing pipes that extend through the dam and lead to a treatment plant 0.3 mile downstream. Details of the new intake structure are shown on Plates E-6 and E-7.

-3-

h. <u>Normal Operational Procedure</u>. The pool is maintained at the spillway crest level with excess inflow discharging over the spillway. About 1.6 MGD are withdrawn through the intake structure for water supply purposes.

1.3 Pertinent Data.

a.	Drainage Area. (square miles)	2.7
b.	<u>Discharge at Damsite</u> . (cfs.) Maximum known flood at damsite	1955 Flood- unknown discharge.
	Outlet works at maximum pool elevation	N/A No outlet at dam.
	Spillway capacity at maximum pool elevation Design conditions Existing conditions	1,150 785
с.	Elevation. (Feet above msl.) Top of dam Design conditions Existing conditions Maximum pool Design conditions Existing conditions Normal pool (spillway crest) Upstream invert outlet works Streambed at toe of dam	781.1 780.2 781.1 780.2 777.1 757.0 756.2
d.	<u>Reservoir Length</u> . (miles) Normal pool Maximum pool	0.30 0.34
е.	<u>Storage</u> . (acre-feet) Normal pool Maximum pool	144 197
f.	<u>Reservoir Surface</u> . (acres) Normal pool Maximum pool	14 20

-4-

g.	Dam.	
U	Туре	Embankment with corewall
	Length (feet)	634
	<u>Height</u> (feet)	24
	<u>Topwidth</u> (feet)	Varies, 3 to 6
	<u>Side Slopes</u> Design conditions Upstream Downstream	1V on 3H 1V on 2H
	Existing conditions Upstream Downstream	Not Available Varies, 1V on 1.5H to 1V on 2.3H.
	Zoning	Earthfill upstream; earthfill and rock- fill down- stream.
	<u>Cut-off</u>	Stone masonry corewall in trench.
	<u>Grout Curtain</u>	None.
h.	Diversion and Regulating Tunnel.	None.
i.	<u>Spillway</u> . Type	Concrete weir.
	Length of Crest (feet)	40.0
	Crest Elevation	777.10
	Upstream Channel	Reservoir, vertical concrete walls.

-5-

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i.	<u>Spillway</u> . (Cont'd.) Downstream Channel	Concrete apron and rock-lined channel.
j.	<u>Regulating Outlets</u> . <u>Description</u>	No outlets at dam. Intake structure has 3 gates and a 16-inch diameter cast- iron pipe that feeds two 10- inch dia. water supply lines. Blowoff at treatment plant 0.3 mile downstream.
	<u>Closure</u>	Three slide gates at intake structure; two 10-inch gate valves at downstream side of corewall.
	<u>Access</u>	Intake structure- bridge from top of dam. Gate valves - tunnel from downstream toe of dam.

4

SECTION 2

ENGINEERING DATA

2.1 <u>Design</u>.

a. <u>Data Available</u>. Engineering data available for review included the following:

(1) Plans for original construction, including changes approved during construction (Plates E-2 and E-3).

(2) Results of an as-built survey performed in August 1930 (Plate E-4).

(3) Plans for proposed modifications of dam and spillway (1931) (Plate E-5).

(4) Plans for intake structure constructed in 1964 (Plates E-6 and E-7).

(5) Specifications for original construction.

(6) Specifications for construction of intake structure.

(7) Permit application reports prepared by the Commonwealth for the original construction and subsequent modifications.

b. <u>Design Features</u>. The project is described in Paragraph 1.2a. The various features of the dam are shown on the Photographs in Appendix C and on the Plates in Appendix E. The embankment is shown on Plates E-2 through E-5 and on Photographs A through E. The spillway is shown on Plates E-2 through E-5 and on Photographs F and G. The outlet works is shown on Plates E-6 and E-7 and on Photographs H and I.

(c) <u>Design Considerations</u>. Design considerations for Middle Dam are discussed in Section 5 and Section 6.

2.2 Construction.

a. <u>Data Available</u>. Construction data available for review included construction photographs and six construction progress reports prepared by the Commonwealth for the original construction. No construction data were available for subsequent modifications. b. <u>Construction Considerations</u>. A trench averaging about 4 feet deep was excavated for the corewall foundation. The foundation, described as impervious clay and hardpan, was inspected by the Commonwealth and judged to be satisfactory. In August 1914, another inspection was performed by the Commonwealth and the report noted the following deficiencies and/or variations from design:

(1) Mortar for the foundation course of the corewall did not have a suitable proportion of cement and sand. A mix of 1 part cement to 5 parts sand was being used instead of the specified 1 to 2 mix.

(2) Some stone for the corewall were not being cleaned of mud and dirt.

(3) The embankment material was being deposited in layers that were too thick (10-18 inches), large stones were not being removed, dry embankment material was not being wetted, and some portions were not compacted well.

(4) The Engineer reported that the Superintendent of construction would not follow the specifications.

(5) The corewall was found to be about 2 feet thicker than shown on the plans.

The Commonwealth directed that construction practices be modified to conform with the specifications. The Commonwealth inspected the work again in September 1924. The inspection report noted the following:

(1) Mortar quality was improved but not satisfactory. One part cement and three parts sand were being used.

(2) Stones for the corewall were clean.

(3) The earthfill placement was unsatisfactory. Layers were too thick, and no moisture control or compaction was used.

Another inspection was performed by the Commonwealth in November 1914. The dam was nearly complete, and the Commonwealth concluded that the overall appearance was excellent. It was also concluded that deficiencies in construction practices that had occurred would not cause any significant problems.

-8-

2.3 <u>Operation</u>. There are no formal records of operation. Periodic inspections have been performed by the Commonwealth. The inspection reports, and statements by the Owner, indicate that no incidents of failure or overtopping are known to have occurred over its 65-year life.

2.4 Evaluation.

a. <u>Availability</u>. Engineering data were provided by the Bureau of Dams and Waterway Management, Department of Environmental Resources, Commonwealth of Pennsylvania. The Owner made available the Borough Manager, the Superintendent of Public Utilities, and the Borough Engineer for information during the visual inspection. He also researched his files for information at the request of the inspection team.

b. <u>Adequacy</u>. The type and amount of available design data and other engineering data are limited, and the assessment must be based on the combination of available data, visual inspection, performance history, hydrologic assumptions, and hydraulic assumptions.

c. <u>Validity</u>. There is no reason to question the validity of the available data.

SECTION 3

VISUAL INSPECTION

3.1 Findings.

a. <u>General</u>. The overall appearance of the dam is fair. Deficiencies were observed as noted below. A sketch of the dam with the location of deficiencies is presented on Exhibit B-1 in Appendix B. Survey information acquired for this report is summarized in Appendix B. On the day of the inspection, the pool was 0.1 foot above spillway crest elevation.

b. <u>Embankment</u>. The top of the embankment is covered with grass. Most of the upstream slope was submerged and could not be inspected. Riprap on the upstream slope is intact, but it does not extend to the top of the dam (Photograph A). The portion of the slope above the riprap is covered with grass.

The downstream slope of the dam is covered with grass and is generally in good condition (Photographs B and C). One bare area about 500 square feet in size exists near the left abutment (Photograph D). The Owner stated that the area was disturbed in 1964 when the intake structure was constructed. No erosion has occurred at the bare area. Two burrowing animal holes are located on the downstream slope.

An extensive network of wet areas is located along the downstream toe of the dam (Photograph E). The affected area extends about 150 feet along the toe of the dam and about 120 feet downstream. No individual sources of seepage could be located, but such sources could easily have been obscured by the relatively deep pools of standing water. All water observed in the wet areas was clear. At the downstream end of the network, there was a small watercourse that seemed to be the outlet for most of the wet areas. A clear flow estimated at 15 to 20 gallons per minute (gpm) was observed.

The survey of the embankment that was performed during the visual inspection was based on the elevation datum used for construction of the intake structure in 1964. The survey indicates that the lowest area on the top of the dam is located about 120 feet from the left abutment. This is the area previously described as having been disturbed during construction of the intake structure. The lowest area is at Elevation 780.2, which is 0.9 foot lower than the design elevation for the top of

-10-

the dam. Most of the embankment was about 0.4 foot lower than the design elevation. Although most of the upstream slope was submerged and could not be surveyed, the exposed portion was found to be about 1V on 2H. The measured topwidth of the dam varies from 3 to 6 feet. At the surveyed section, the downstream slope is about 1V on 1.5H from the top of the dam to about Elevation 768, and about 1V on 2.3H from Elevation 768 to the toe of the dam.

c. <u>Appurtenant Structures</u>. The concrete spillway weir is in good condition (Photograph F). Minor cracking and leaching are present on the spillway sidewalls and on the bridge pier. The right wall also had some spalling at the weir. The concrete apron at the toe of the weir on the left side of the spillway is damaged. Pieces of concrete about 3 inches thick are broken and displaced over about a 30-square foot area. It did not appear that the toe of the weir was undermined. Beyond the end of the concrete apron, the spillway outlet channel is in good condition (Photograph G). No erosion is present in the stone-lined channel. The underside of the spillway bridge is at Elevation 781.2, which is 0.1 foot above the design elevation of the top of the dam.

The intake structure located in the reservoir is in good condition (Photograph H). The Superintendent of Public Utilities stated that the three slide gates in the intake structure are all in good working order. Since there are no outlets at the dam, it was not requested that the gates be operated for this inspection. An examination was made of the valve chamber located along the downstream side of the corewall. Standing water about 12 inches deep and mud were present in the tunnel (Photograph I) and valve chamber. The two gate valves were nearly submerged. The source of the water could not be determined. The exposed portion of the corewall in the valve chamber is in good condition. It was damp at several locations, but there were no leaks.

d. <u>Reservoir Area</u>. The watershed is about 90 percent wooded and has only a minor amount of development. East Stroudsburg Dam is located within the watershed about 1.3 miles upstream from Middle Dam (Photograph J). A Phase I Inspection Report was prepared for East Stroudsburg Dam in April 1979.

e. <u>Downstream Channel</u>. No obstructions were located in the downstream channel near the dam. Lower Dam, a small, concrete gravity dam also owned by the Borough of East Stroudsburg, is located about 0.5 mile

-11-

downstream. PennDER records indicate that Lower Dam has a storage capacity of about 21 acre-feet. The first dwelling is located about 1.3 miles downstream from Middle Dam. At a distance of 1.7 miles downstream, there is a group of about 10 dwellings constructed close to Sambo Creek. Sambo Creek joins Broadhead Creek, which flows through East Stroudsburg, approximately 3 miles downstream from the dam. It is estimated that at least 10 dwellings would be flooded should Middle Dam fail. Significant property damage farther downstream is also likely.

SECTION 4

OPERATIONAL PROCEDURES

4.1 <u>Procedure</u>. The reservoir is maintained at the spillway crest with excess inflow discharging over the spillway and into the downstream channel. One of the slide gates at the intake structure is normally open for withdrawal of water for water supply purposes. Both gate valves in the valve chamber are normally open.

4.2 <u>Maintenance of Dam</u>. The dam is visited at least monthly by the Superintendent of Public Utilities. He makes informal inspections of the dam and appurtenant structures. Brush and weeds are cut each spring. Repairs to riprap are made as the need arises.

4.3 <u>Maintenance of Operating Facilities</u>. The operating mechanisms for the slide gates are maintained as needed. The slide gates are operated as necessary to meet water supply needs. Screens in the intake structure are cleaned twice each year. The gate valves in the valve chamber are maintained as needed.

4.4 <u>Warning Systems in Effect</u>. The Owner has no emergency operation and warning system.

4.5 Evaluation of Operational Adequacy. The maintenance of the embankment, spillway, and outlet works is generally good, but some deficiencies do exist. Detailed inspections are necessary to detect hazardous conditions at the dam. An emergency operation and warning system is necessary to reduce the risk of dam failure should adverse conditions develop and to prevent loss of life should the dam fail.

SECTION 5

HYDROLOGY AND HYDRAULICS

5.1 Evaluation of Features.

Design Data. The permit application report for the 1931 modification of the spillway indicates that the spillway design head is 4 feet and that the design weir coefficient is 3.6. The coefficient was considered reasonable and was accepted for use in determining the design capacity for this Report. The existing capacity computed and used for this Report was based on the maximum available head under existing conditions. Data presented in the Phase I Inspection Report for East Stroudsburg Dam, located 1.3 miles upstream from Middle Dam, were used in evaluating the effects of East Stroudsburg Dam on the hydrology of Middle Dam. Conditions that existed at the time of the inspection of East Stroudsburg Dam were used. There is a diversion system that effectively increases the drainage area of East Stroudsburg Dam. The effects of the diversion system were included in the Phase I Inspection Report for that dam.

b. <u>Experience Data</u>. No records of maximum pool levels were available. The 1955 Flood resulting from Hurricane Diane is believed to be the flood of record. The Owner stated that he had no knowledge of the dam being overtopped during any flood.

c. Visual Observations.

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(1) <u>General</u>. The visual inspection of Middle Dam, which is described in Section 3, resulted in a number of observations relevant to hydrology and hydraulics. These observations are evaluated herein for the various features.

(2) <u>Embankment</u>. The low areas on the top of the dam limit the existing spillway capacity to less than the design capacity.

(3) <u>Appurtement Structures</u>. The spillway was in satisfactory condition except for minor maintenance items.

Although blowoff valves exist at the treatment plant, the ability of the existing outlet work

-14-

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facilities to drawdown the reservoir is questionable because of head losses in the two 1,400-foot long supply lines.

(4) <u>Reservoir Area</u>. East Stroudsburg Dam, located 1.3 miles upstream, does affect the hydrology of Middle Dam. Its effects have been included in the hydrologic analysis.

(5) <u>Downstream Conditions</u>. No conditions were observed downstream that might present significant hazard to Middle Dam. Lower Dam, located 0.5 mile downstream, is judged not to affect the flooding that would occur should Middle Dam fail. Failure of Middle Dam would result in flooding of at least 10 dwellings in the first 1.7 miles downstream from the dam. Additional damage farther downstream is possible. The downstream conditions indicate that a high hazard classification is warranted for Middle Dam.

d. Overtopping Potential.

(1) <u>Spillway Design Flood</u>. According to the criteria established by the Office of the Chief of Engineers (OCE), the Spillway Design Flood (SDF) for the size (Small) and hazard potential (High) of Middle Dam is between one-half of the Probable Maximum Flood (PMF) and the PMF. Because of the downstream conditions, the PMF is selected as the SDF for Middle Dam. The watershed was modeled with the HEC-1DB computer program. A description of the model is included in Appendix D. The assessment of the dam is based on existing conditions, and the effects of future development are not considered.

(2) <u>Summary of Results</u>. Pertinent results are tabulated at the end of Appendix D. The analysis reveals that Middle Dam can pass about 22 percent of the PMF without overtopping of the dam. The dam is rated at its existing top elevation. At its design top elevation, the dam can pass about 33 percent of the PMF without overtopping of the dam.

(3) <u>Spillway Adequacy</u>. The criteria used to rate the spillway adequacy of a dam are described in Appendix D. Because an occurrence of the 1/2 PMF would result in overtopping of the dam, a failure analysis was performed. Assumptions used to model the failure are described in Appendix D. The resulting outflow was routed through stream sections downstream to the dwellings. Failure of Middle Dam would raise water levels at the

-15 -

dwellings by 2.1 to 4.8 feet over the levels that existed just prior to failure of the dam. There is an increased hazard for loss of life. Therefore, the spillway capacity is rated as seriously inadequate. If the low areas on the top of the dam were filled to the design elevation, the spillway capacity would still be rated as seriously inadequate.

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SECTION 6

STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability.

a. Visual Observations.

(1) <u>General</u>. The visual inspection of Middle Dam, which is described in Section 3, resulted in a number of observations relevant to structural stability. These observations are evaluated herein for the various features.

Embankment. The combination of riprap and (2) vegetation on the upstream slope apparently provide adequate protection against wave erosion. However, the narrow topwidth of the dam (3 to 6 feet) requires that the slope protection be inspected frequently and carefully maintained. The downstream slope of the embankment was generally in good condition except for minor maintenance items. Although the slope is steep, there was no evidence of stability problems. The wet areas located downstream from the dam apparently developed shortly after construction was complete. Inspection reports subsequent to 1921 mention seepage at the toe. A report made in 1935 indicates that a 200-foot long reach along the toe was swampy. No quantitative records of flows are available, so changes in conditions cannot be determined. Because of its long history and because no concentrated sources were apparent, the clear seepage was judged not to be a serious deficiency at the time of this inspection.

(3) Appurtenant Structures. The cracking, leaching, and spalling of the concrete spillway sidewalls are maintenance items and do not significantly affect the stability of the structures. The broken and displaced concrete in the apron was minor in terms of effect on stability at the time of the inspection. However, additional deterioration of concrete might lead to significant erosion of underlying material that would affect stability.

The standing water and mud in the valve chamber are undesirable because they could conceal potentially adverse conditions.

-17-

b. Design and Construction Data.

(1) Embankment. No stability analyses were available for the embankment. Design drawings for the modified embankment (Plate E-5) indicate that the topwidth of the dam was to be 8 feet and the downstream slope was to be 1V on 2H. Survey information acquired for this Report indicates that the dam was not completed in accordance with the plans. Construction progress reports prepared by the Commonwealth were critical of the original construction of the dam (Paragraph 2.2b.), but they concluded that the dam was satisfactory. Much of the criticism concerned the upstream earthfill, which could not be inspected for this Report.

(2) Spillway. No stability analyses were available for the spillway weir. The spillway design was not approved by the Commonwealth prior to construction. report by the Commonwealth on the as-built structure indicated dissatisfaction with the design, but stated that it would not fail provided that it was carefully maintained. A stability analysis of the weir was performed for this Report. Numerous assumptions were required for the analysis because the as-built drawing from 1931 did not show all the design details and because the existing structure differs somewhat from the as-built drawing. It was assumed that the difference in appearance is due to minor repairs, and that the 1931 as-built drawings are essentially valid. Earth pressure and uplift were considered in the analyses. The analy es indicated that for normal conditions, pool level at spillway crest, the results do not deviate significantly from stability criteria established by the Office of the Chief of Engineers (OCE). For the assumed maximum loading conditions, pool level at design top of dam elevation. the analysis indicated that the structure might fail by overturning because the resultant was located outside of the toe. It is noted that the analyses performed for this Report are based on limited data and are only approximate.

c. <u>Operating Records</u>. The Owner has no formal records of operation. According to PennDER records, no stability problems have occurred for the dam or appurtenant structures.

d. <u>Post-Construction Changes</u>. Modifications made to the dam are described in Paragraph 1.2g.

e. <u>Seismic Stability</u>. Because the stability of the spillway weir is questionable, it is assumed that the dam could not withstand an earthquake.

-18-

SECTION 7

ASSESSMENT, RECOMMENDATIONS, AND REMEDIAL MEASURES

7.1 Dam Assessment.

a. <u>Safety</u>.

(1) Based on available records, visual inspection, calculations, and past operational performance, Middle Dam is judged to be in fair condition. Based on existing conditions, the spillway will pass about 22 percent of the PMF before overtopping of the dam occurs. If the low areas on the top of the dam were filled to the design elevation for the top of the dam, the spillway would pass about 33 percent of the PMF. For either condition, it is judged that the dam could not withstand the depth and duration of overtopping that would occur for the 1/2 PMF. Failure of the dam would cause an increased hazard for loss of life. Therefore, the spillway capacity is rated as seriously inadequate. According to criteria established for these studies, the dam is judged to be unsafe, non-emergency, because the spillway capacity is seriously inadequate.

(2) No stability problems were evident for the embankment. Stability analyses were performed for the spillway weir for this Report. The results do not deviate significantly from recommended guidelines for stability under normal loading conditions, but the results indicate that the weir might fail by overturning under the assumed maximum loading conditions because the resultant was found to be located outside of the toe. It is noted that the analyses were based on a number of assumptions and that the results are only approximate.

(3) There are no drawdown facilities at the dam. Water can be discharged from facilities at a treatment plant located 0.3 mile downstream, but the ability of the facilities to drawdown the reservoir is questionable.

(4) A summary of the features and observed deficiencies is listed below:

Feature and Location	Observed Deficiency		
<u>Embankment</u> :	Low areas on top; bare area on downstream slope; burrow- ing animal holes; seepage and wet areas at toe.		
<u>Spillway</u> :	Minor deterioration of concrete sidewalls; apron concrete broken and dis- placed.		
Outlet Works:	No drawdown facilities at dam; standing water in valve		

chamber.

b. <u>Adequacy of Information</u>. The information available is such that a preliminary assessment of the condition of the dam can be inferred from the combination of visual inspection, past performance, and computations performed prior to and as part of this study.

c. <u>Urgency</u>. The recommendations in Paragraph 7.2 should be implemented immediately.

d. <u>Necessity for Further Investigations</u>. In order to accomplish some of the remedial measures outlined in Paragraph 7.2, further investigations by the Owner will be required.

7.2 Recommendations and Remedial Measures.

a. The following measures are recommended to be undertaken by the Owner, in approximate order of priority, immediately:

(1) Perform additional studies to more accurately ascertain the spillway capacity required for Middle Dam as well as the nature and extent of measures required to provide adequate spillway capacity. Take appropriate action as required.

(2) Make repairs to the spillway apron. Perform additional investigations and studies to more accurately assess the stability of the spillway weir as well as the nature and extent of measures required to provide adequate factors of safety for all expected loading conditions. Take appropriate action as required.

(3) Provide properly designed facilities to collect and dispose of water along the toe of the dam and

-20-

in the valve chamber. The facilities should include measurement devices. Seepage should be monitored, and records of seepage should be maintained.

(4) Perform a study to determine whether the reservoir could be drawn down over a reasonable period of time with the existing facilities at the treatment plant. Take appropriate action as required to ensure adequate drawdown facilities.

(5) Undertake remedial measures for other minor maintenance items.

All investigations, designs, and supervision of construction should be performed by a professional engineer experienced in the design and construction of dams. The seepage monitoring program should also be performed or supervised by a professional engineer.

b. In addition, the Owner should institute the following operational and maintenance procedures:

(1) Develop a detailed emergency operation and warning system for Middle Dam.

(2) During periods of unusually heavy rains, provide round-the-clock surveillance of Middle Dam.

(3) When warnings of a storm of major proportions are given by the National Weather Service, the Owner should activate his emergency operation and warning system.

(4) Institute an inspection program such that the dam is inspected frequently. As presently required by the Commonwealth, the program should include a formal annual inspection by a professional engineer experienced in the design and construction of dams. Utilize the results to determine if remedial measures are necessary.

(5) Expand the existing maintenance program so that all features of the dam are properly maintained.

-21-

APPENDIX A

CHECKLIST - ENGINEERING DATA

6.A.

CHECKLIST

ENGINEERING DATA

NAME OF DAM: Middle Dam

NDI ID NO.: PA-00256 DER

DESIGN, CONSTRUCTION, AND OPERATION PHASE I

Sheet 1 of 4

Sheet 2 of 4

DATA
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ITEM	REMARKS
RAINFALL/RESERVOIR RECORDS	None.
DESIGN REPORTS	Permit application reports prepared by Commonwealth for original construction in 1.1.12 and for 1.916 and 1931 modifications.
GEOLOGY REPORTS	Keport of test pit investigations for oriquial construction. Description of geology included in Appendix F.
DESIGN COMPUTATIONS: Hydrology and Hydraulics Dam Stability Seepage Studies	Spillway capacity estimated in permit application reports.
MATERIALS INVESTIGATIONS: Boring Records Laboratory Field	None.
POSTCONSTRUCTION SURVEYS OF DAM	None.

A-2

Sheet 3 of 4

DATA
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T L L L L	DEMADYS
BORROW SOURCES	From within reservoir area.
MONITORING SYSTEMS	None.
MODIFICATIONS	1916: Spillway raised 2 feet. 1931: Dam raised 4 feet; spillway longthoned and raised 3 feet. 1964: New intake structure.
HIGH POOL RECORDS	None.
POSTCONSTRUCTION ENGINEERING STUDIES AND REPORTS	None.
PRIOR ACCIDENTS OR FAILURE OF DAM: Description Reports	Norc.

A-3

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ENGINEERING DATA	ITEM	TENANCE AND OPERATION RECORDS	WAY: in ctions talls	ATING EQUIPMENT: Ins talls	inde: Se ficiencies ficiencies ficiencies inde: Se inde:
Sheet 4 of 4	REMARKS		ole - See Platus in Appenduir E.	ole. See Plates in Appendive E.	Tement of crest and upstream slope; upleted in accordance with approved gracial appearance - poor. At settlenert upstream from corewall; accordance with plans. st irregular; general seepage at toe; accordance with plans. t uneven; downstream slope uneven; extremit upstream from corewall; deunstream struction by spillway buckubter; crossion struction in to to to design level; severates into it 1923.

A-4
Sheet 4a of 4

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1941: Crest narrow (4'-5'); brush; downstroom 1932: Settlement of crest after raising; some slope sterver them approved (iv on 2H); slight leakage in value chomber; toe wet over considerable length. swampy along toc. 1957: Crest 3" low right of spillway; leakage at conduit; swampy at toc. to right of blowoff; swampy along central 200 feet; conduit leak at toe. 1936: Crest s".9" 10w; brush on slopes; Slight leaknge to right of blowaff; swampy along central 200 feet swampy at toe left of outlet; downstieonu end of wastewary undermined. sides of corrivall; slight leakage; wet and swampy at toe. 1928: Crest uneven; brush on upstream slope; 1933: Downstream slope irregular; slight settlemint; swampy at toe. 1935: Crest from 3"-9" 1000; slight leakage 1925: Bruch on upstream slope; slight erocion erosion downatream slope; slight scipage right of spillway; swampy at toe. 1949: Crest 6" low right of spillinny; brush; leaking at outlet conduit; 1926 : Crest uneven ; settlement both 1938: No deficiencies noted. noted REMARKS of wasteway. 1965: INSPECTIONS (CONT'D) ENGINEERING DATA TEM PREVIOUS

A-5

APPENDIX B

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CHECKLIST - VISUAL INSPECTION

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CHECKLIST VISUAL INSPECTION PHASE I

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e of Dam:	ID No.: of Dam:	(s) Inspe	Elevatior	sction Per	H. Whit	R. Eber	
Name	Type	Date	loor	dsul	×	Ä	

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EMBANKMENT Sheet <u>1</u> of <u>2</u>

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VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SURFACE CRACKS	None observed.	Two burrowing animal holes in embantment.
UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE	None observed.	
SLOUGHING OR EROSION: Embankment Slopes Abutment Slopes	None observed.	One area on downstream slope near left abutment is bare. Approx. 500 S.F. area.
CREST ALIGNMENT: Vertical Horizontal	See survey data at and of Appendix B.	
RIPRAP FAILURES	Grad condition.	Kiprap does not extend to top of dam. Vegetation above riprap.

EMBANKMENT Sheet 2 of 2

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
JUNCTION OF EMBANKMENT WITH: Abutment Spillway Other Features	No deficiencies.	
ANY NOTICEABLE SEEPAGE	Widespread wet arcas from outlet works to 150' I left and from toe to 120' I downstream.	Low areas trap water. One outlet opprox. 120'd s appears to drawn wet areas. Clear flow approx.15.20 gpm.
STAFF GAGE AND RECORDER	Nore.	
DRAINS	None.	
VALVE CHAMBER AT Downstrham Face of Corfinal	Corewall damp but no concentrated leaks. Standing water ru floor approt. 12" deep.	

OUTLET WORKS

And a second second

Sheet 1 of 1

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CRACKING AND SPALLING OF CONCRETE SURFACES IN OUTLET CONDUIT	N/A - no conduits outlet at the dam.	No blowoffs. Nearest outlet is at treatment plant a.3 mile downstream.
INTAKE STRUCTURE	Gord condition - no deficiencies.	
OUTLET STRUCTURE	Value chamber - good condition. Starding water on floor approv. 12" dag.	Poor drainage front value chaniber.
OUTLET CHANNEL	N/A	
EMERGENCY GATE	A/A	

8-4

UNGATED SPILLWAY

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81. - Stan - Stan

Sheet 1 of 1

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONCRETE WEIR	Good condition.	
APPROACH CHANNEL	Minor fine cracks in concrete walls.	Not considered a deficiency.
DISCHARGE CHANNEL	Walls: minor cracking and leaching. Upgiling on Mght Vallaty. Levic te broken and displaced - approx. 30 S.F.	Apron concrete that is displaced approx. 2'2" thick. No apparent undermining at toe of weir.
BRIDGE AND PTERS	Gue pier - fair cordition Low chord of bridge above try f dom.	Eriège in goed condition.
OUTLET CHANNEL	Rock-lind rectangular channels steeps; gord condition.	

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INSTRUMENTATION

1.451

Sheet 1 of 1

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
MONUMENTATION/SURVEYS	None.	
OBSERVATION WELLS	None.	
WEIRS	None.	
PTEZOMETERS	None.	
OTHER	None.	

DOWNSTREAM CHANNEL

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Sheet 1 of 1

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONDITION: Obstructions Debris Other	No obstructions; dry, stone masonry channel. Wooded area downstream.	
SLOPES	Mild to steep.	
APPROXIMATE NUMBER OF HOMES AND POPULATION	1 Dwelling 1.3 miles downstream. Group of approx. 10 dwellings 1.7 miles downstream. Lower Down 0.5 mile downstream.	Estimate approx. 10 duellings would be flooded by failure of dam.

B-7

RESERVOIR AND WATERSHED

Sheet 1 of 1

7.92

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SLOPES	Vary - mild to steep.	
SEDIMENTATION	None reported .	
WATERSHED DESCRIPTION	Approx. 90%. wooded ; miner development.	East Stroudsburg Dam within watershed 1.3 miles upstream. DER No. 45-155. Phase I Inspection 4/79.

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	COMPUTED BY DATE CHECKED BY	OATE



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APPENDIX C PHOTOGRAPHS

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A. Top of Dam and Upstream Slope.



B. Embankment. View from Spillway.

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C. Embankment. View from Left Abutment.



D. Downstream Slope Near Left Abutment.

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E. Wet Areas at Toe of Dam.



F. Spillway.



G. Spillway Outlet Channel.



H. Intake Structure.



I. Entrance to Valve Chambur.



J. East Stroudsburg Dam. Located 1.3 Miles Upstream.



APPENDIX D

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HYDROLOGY AND HYDRAULICS

APPENDIX D

HYDROLOGY AND HYDRAULICS

Spillway Capacity Rating:

In the recommended Guidelines for Safety Inspection of Dams, the Department of the Army, Office of the Chief of Engineers (OCE), established criteria for rating the capacity of spillways. The recommended Spillway Design Flood (SDF) for the size (small, intermediate, or large) and hazard potential (low, significant, or high) classification of a dam is selected in accordance with the criteria. The SDF for those dams in the high hazard category varies between one-half of the Probable Maximum Flood (PMF) and the PMF. If the dam and spillway are not capable of passing the SDF without overtopping failure, the spillway capacity is rated as inadequate. If the dam and spillway are capable of passing one-half of the PMF without overtopping failure, or if the dam is not in the high hazard category, the spillway capacity is not rated as seriously inadequate. A spillway capacity is rated as seriously inadequate if all of the following conditions exist:

(a) There is a high hazard to loss of life from large flows downstream of the dam.

(b) Dam failure resulting from overtopping would significantly increase the hazard to loss of life downstream from the dam from that which would exist just before overtopping failure.

(c) The dam and spillway are not capable of passing one-half of the PMF without overtopping failure.

Description of Model:

If the Owner has not developed a PMF for the dam, the watershed is modeled with the HEC-1DB computer program, which was developed by the U.S. Army Corps of Engineers. The HEC-1DB computer program calculates a PMF runoff hydrograph (and percentages thereof) and routes the flows through both reservoirs and stream sections. In addition, it has the capability to simulate an overtopping dam failure. By modifying the rainfall criteria, it is also possible to model the 100year flood with the program.

D-1

APPENDIX **D**

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Delaware River Basin
Name of Stream: Sambo Creek
Name of Dam: Middle Dam
NDI ID No.: PA-00256
DER ID No.: 45-3
atitude: N 41° 05' 00" Longitude: N 75° 10' 50"
op of Dam Elevation: 780.2 (Low Point)
treambed Elevation: 756.2 Height of Dam: 24 f
eservoir Storage at Top of Dam Elevation: 197 acre-f
ize Category: Small
azard Category: High (see Section 5)
pillway Design Flood: SDF varies from 1/2 PMF to PMF : Sclee
PMF based on downstream conditions

UPSTREAM DAMS

	Distance from		Storage at top of	
	Dam	Height	Dam Elevation	
Name	(miles)	(ft)	(acre-ft)	Remarks
East Stroudsburg				Phase I Inspection
Dam	1.3	_48_	1,358	APT: 1974
				NOI NO. PA-001 37
			<u></u>	DER No. 45-155
				·····
		 ~		
ومسيد الكوري معطي معانا مامي ويرد				
	DC	WNSTREAM	DAMS	
	<u> </u>			DER No. 45-13
Lower Dain	0.5	24	21.5	Data Leon DER
				inventory
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				Del		R	iver Ba	sin	
Name of Stream: Somba Creek									
Name of Dam: Middle Dam									
DETERMINATION OF PMF RAINFALL & UNIT HYDROGRAPH									
			UNI	T HYDRC	GRAPH D	ATA:			
	Drainage	1	1	<u></u>	الوديدية المستند في تريين				
Sub-	Area	Ср	i Ct	I L	Lan	L L I	I To	Map	Plate
area	(square			miles	miles	miles	hours	Area	
u. uu	miles)	(1)	(2)	(3)	$(\hat{\mu})$	(5)	(6)	(7)	(8)
			(-/						
4-1	1.68	0.45	1.23	2.08	1.09		1.57		A
A-2	1.02	0.45	1.23	2.22	.94	-	1.53		4
		- 212-					1.20		
	<u>+</u>	+							
	†	1	·				+		
Total	2.7	·	(See	Sketch	on She	et 0-4)	.		L
	(1) & (2):	- Snv	der	Unit Hv	drogram	h coeff	icients	supp]	lied bv
	Baltim	ore D	istr	ict. Co	rps of	Enginee	rs on m		nd
	plates	refe	renc	ed in (7) & (8	3)			
	The follow	ing a	re m	easured	from t	he outl	et of t	he sul	oarea:
(3): Length of main watercourse extended to divide									
(3): Length of main watercourse extended to divide (4): Length of main watercourse to the centroid									
(4): Length of main watercourse to the centroid The following is measured from the unstream and of the									
The following is measured from the upstream end of the reservoir at normal pool:									
reservoir at normal pool: (5): length of main watercourse extended to divide									
(5): Length of main watercourse extended to divide (6): $T_{D=C_{+}} \times (L \times L_{+})^{0+3}$, except where the centroid of									
	the subare	ic is		ted in	the res	ervoir	Then	enero.	
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compu	tei Data.		D _			eak IIC	W)		
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Data for Dam at Outlet of Subare	a(see	Sketch on Sheet $(7-4)$
Name of Dam: East Stroudsb	ung Dam	······
SPILLWAY DATA:	Existing	Design
	Conditions	Conditions
Top of Dam Elevation	B92.4	
Spillway Crest Elevation	888.0	A
Spillway Head Available (ft)	4,4	
Type Spillway	<u>Rectangular</u> se	stion
"C" Value - Spillway	NIA: Gritical	depth
Crest Length - Spillway (It) Spillway Peak Discharge (ofs)	40.0	
Auxiliary Spillway Crest Elev.		
Auxiliary Spille Head Avail. (ft) <u> </u>	
Type Auxiliary Spillway		
"C" Value - Auxiliary Spill. (ft)N/A	jõ.
Crest Length - Auxil. Spill. (ft)N/A	
Auxiliary Spillway		4/1
Peak Discharge (CIS)	N/A	<u></u>
combined Spillway Discharge (cis	1,152	<u>_</u>
Spillway Rating Curve: From, Ph	ase I Inspection R	2cport April 1979
Elevation (Spillway (cfs) (A	uviliany Snillway	(afs) Combined (afs)
	W/A	Combined (CIS)
		<u>N/H</u>
88900 124		
89010 352		
892,00 994		
<u>E93.00 1,390</u>		
<u> </u>		
	Y	
<u> </u>	N/A	<u> </u>
OUTLET WORKS RATING: 0	utlet 1 Outle	et 2 Outlet 3
Invent of Outlet	•	
Invert of Inlet		
Type		
Diameter (ft) = D		
Length $(ft) = L$		
Area $(sq. ft) = A$	20	
N		
K Entrance		
K EXIL $-$ K Emiorican-20 1.21/P4/3 $-$		
	-98	
$(1/K)^{0.5} = C$ -		·
Maximum Head (ft) = HM	30	
$Q = CA \sqrt{2g(HM)}(cfs)$	<u> </u>	
Q Combined (cfs)		

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HCASEL

Data for Dam at Outlet of Subarea <u>A-1</u> (See sketch on Sheet 1-4) Name of Dam: <u>East Stroudsburg Dam</u> <u>STORAGE DATA:</u> From Phuse I Inspection Report April 1979

			Stora	age	
Elevatio	on	Area (acres)	million gals	<u>acre-ft</u>	Remarks
843	=ELEVO#	0	Q	0	
853	=ELEV1	=A1		<u>/3</u> =S1	
863				103	
873				303	
				6.58	
				914	
				1,588	
				1,800	
		·····	······		
				_ 	
	-	·			

***** ELEVO = ELEV1 - $(3S_1/A_1)$

Planimetered contour at least 10 feet above top of dam

Reservoir Area at Normal Pool is <u>5</u> percent of subarea watershed.

BREACH DATA: Not Applicable for Analysis of Middle Dam.

See Appendix B for sections and existing profile of the dam. Soil Type from Visual Inspection:

Maximum Permissible Velocity (Plate 28, EM 1110-2-1601) fps (from $Q = CLH^{3/2} = V \cdot A$ and depth = (2/3) x H) & A = L \cdot depth

HMAX = $(4/9 \ V^2/C^2)$ = _____ft., C = ____Top of Dam El.=____

HMAX + Top of Dam El. = = FAILEL (Above is elevation at which failure would start)

Dam Breach Data:

BRWID = ______ft (width of bottom of breach) Z = ______(side slopes of breach) ELBM = ______(bottom of breach elevation, minimum of zero storage elevation) WSEL = _____(normal pool elevation) T FAIL= _____mins = ____hrs (time for breach to develop)

D-6

Data for Dam at Outlet of Subarea_	A-2 (see Sk	etch on Sheet $\nabla -4$)
Name of Dam: Middle Dam		
SPILLWAY DATA:	Existing	Design
	Conditions	Conditions
Top of Dam Elevation	780.2	781.1
Spillway Crest Elevation	777.1	777.1
Spillway Head Available (ft) Type Spillway	3.1	4.0
"C" Value - Spillway	3.6	3.6
Crest Length - Spillway (ft)	40	40
Auxiliary Snillway Crest Elev.	785	1,150
Auxiliary Spill. Head Avail. (ft)	N/A	N/A
Type Auxiliary Spillway	NIA	
Crest Length - Auxil. Spill. (ft)	<u>N/A</u>	<u> </u>
Auxiliary Spillway	<i>nya</i> .	
Peak Discharge (cfs)	<u>N/A</u>	N/B
combined spillway Discharge (CIS)	785	1,150
Spillway Rating Curve: $Q = (3.6)\ell$	40)(H) ³¹ 2	
Elevation Q Spillway (cfs) Q Aux	iliary Spillway (cfs) Combined (cfs)
OUTLET WORKS RATING: Out	let 1 Outlet	2 Outlet 3
Invert of Outlet	A	
Invert of Inlet	•	
Diameter (ft) = D	<u>+</u>	··· ··································
Length (ft) = L		······································
Area (sq. ft) = A		
K Entrance	+	
K Exit		
K Friction=29.1 _N ^L /R ^{4/3}		
$(1/K)^{0.5} = C$		
Maximum Head (ft) = HM		
$Q = CA \sqrt{2g(HM)(cfs)}$	¥	

D-7

Data for Dam at Outlet of Subarea A-2 (See sketch on Sheet U-4) Name of Dam: Middle Dam

STORAGE DATA:

		Stor	age	
	Area	million		
Elevation	<u>(acres)</u>	gals	<u>acre-ft</u>	Remarks
743,5 =ELEVO*	0	0	0	
774.1 =ELEV1	10.5 = A 1	35	107 =S1	
777./	14	47	144	Scillway Crest
780.0	20	63	193	-,
<u>_780.2</u> _	20	_64	197	Low Pt Top Dam
<u>B00.0 **</u>	62		974	
		<u> </u>	<u></u>	
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		<u> </u>		<u> </u>
				

* ELEVO = ELEV1 - $(3S_1/A_1)$

** Planimetered contour at least 10 feet above top of dam Reservoir Area at Normal Pool is <u>2</u> percent of subarea watershed.

BREACH DATA:

See Appendix B for sections and existing profile of the dam. Soil Type from Visual Inspection: <u>Sandy</u> <u>Silf</u> Maximum Permissible Velocity (Plate 28, EM 1110-2-1601) \mathcal{Z} fps (from Q = CLH^{3/2} = V·A and depth = (2/3) x H) & A = L·depth

HMAX = $(4/9 \ V^2/C^2) = 0.2$ ft., C = 3.1 Top of Dam El.= 730.2

HMAX + Top of Dam El. = <u>180.4</u> = FAILEL (Above is elevation at which failure would start)

Dam Breach Data:



GANNETT FLEMING CORDDRY	SUBJECT
AND CARPENTER. INC.	SHEET NO OF SHEETS
HARRISBURG, PA.	FOR
	COMPUTED BYDATECHECKED BYDATE

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Selected Computer Output	
Item	Pric
Multi-ratio Analysis:	•
Input	D-10
Summary of Peak Flows	D-12
East Stroudsburg Dam	D-13
Middle Dain	D-14
Breach Analysis:	
input	D-15
Summary of Peak Flows	D-17
East Stroudsburg Dairi	D-17
Middle Dam	0-20
Stream: Sections	DU



No. 2 States



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PEAK FLOW AND STORAGE (END OF PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONDMIC COMPUTATIONS Flows in cubic ffet per second (cubic meters per second) Area in souare miles (souare kilometers)

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OPERATION	S T A T I ON	AREA	PLAN	RATIO 1 1.00	RATIO 2 •70	RATIOS APP Ratio 3 •60	LIED TO FL Ratio 4 •50	045 Ratio 5 •40	RATIO 6 •30	RATIO 7 •20
H Y DROG RA PH	AT 1	1.68 4.35)	۴	3859. 109.26)(2701. 76.48)(2315. 65.56)(1929. 54.631(1543. 43.71)(1158. 32.78)(772. 21.85)(
ROUTED TO	۴	1.68 4.35)	ب	3409. 96.53)(1758. 49.7730	1452. 41.1330	1170. 33.1430	897. 25.41)(647. 18.323C	387. 10.9530
ROUTED TO	~ ~	1.68 4.35)	۲,	3284 • 92 • 98)(1723. 48-803(1429. 40.453C	1152. 32.6230	885. 25.07)(636. 18.02)(380. 10.77.)(
HYDROG RAPH	ат 3 (1.02 2.64)	~~	2377 . 67 .3 2)(1664 • 47•1336	1426. 40.39)(1189. 33.66)(951 . 26 . 93)(713. 20.2016	475. 13.46)(
2 COMBINED	۳ ۳	2°20 2°20	-~	5219. 147.7930	2854 • 80•8230	2394 . 67•7936	1945 . 55 . 07) (1519. 43.03)(1094 . 30.993C	680. 19.263(
C- C ROUTED TO	ñ	2.66°9	۴Ŭ	5228. 148.03)(2849. 80.68)(2390. 67.67)(1941. 54.973(1515. 42.91)(1087. 30.77)(664 . 18 .82)(

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T STROL	. VALUE S 8.00 114.0	MAXIMUM STORAGE AC-FT	1547. 1472. 1409.	1342 1270 1117	LAN 1	MAXIMUM FLONACFS	3284.	1429.	885.
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			SU	MARY OF DA	E DAM	ILVSIS		
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		781.35		216	1941.	9.25	42.75	00.00
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PEAK FLOW AND STORAGE (EMD OF PENIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS Flows in cubic feet per second (cubic meters per second) Arfa in square miles (square kilometers)

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OPERAT ION	STATION	AREA	PLAN	RATIO 1 •50	RATJO 2 •30	
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ROUTED TO	~ັ	1.68	´ - ັ ^ `	31.86)(31.86)(1125.	620 620 17-567 620	
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TINE OF Failure Hours TINE OF Failure Hours 00.00 00-00 TIME OF Max Outflou Hours TIME OF Max Outflow Mours 19.70 20.00 19.70 20.00 TOP OF DAM 892.40 1338. 1152. TOP OF DAM 892.40 1338. 1152. SUMMARY OF DAM SAFETY ANALYSIS EAST STROUDS BURG DAM 10111AL VALUE SPILLVAY CREST TOP 888.00 888.00 914. 914. 0. DURATION Over top Hours OURATION Over top Hours TIME HOURS 20•30 20•60 TIME HOURS 20•30 20•60 0.0 00.0 SPILLMAY CREST 998.00 914.00 ~ ~ MAXIMUM Stagesft 819.8 819.3 NAXINUM Stagesft 819.8 819.3 MAXIHUM Outflow CFS MAXIMUM Dutflov Cfs 1143. 1143. STATION S 7A 71 ON MAXINUM Flov,cfs MAXIMUM FLOVACFS 1125. 1125. MAXIMUM STORAGE AC-FT MAXIMUM STORAGE AC -F T 1335. 1335. PLAN 2 INITIAL VALUE 888.00 914. 0. INITIAL VALUE 988.00 914.00 PLAN 1 30 RATIO . . . RATIO MAXIMUM DEPth Over dam MAXIMUN DEPTH DVER DAM 00**•**0 0.00 ELÉVATION Storagf Outflow ELEVATION Storage Outflov MAXINUM Reservoir V•S•Elev MAXIMUM Reservoir N•S•Elev 892.38 890.87 892+38 890+87 PLAN 1 PLAN 2 sessessesses RA 110 05 PMF RAT10 05 Phf •30 50

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		TIME OF Fallure Hours	00°0		TIME OF Failure Hours	16.30 17.60									
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LVSTS	S T 70P	DURATION Over top Hours	9 •00 5 •00	ST TOP	BURATSON Over top Hours	-23	4	TIME HOURS	18.90 19.20	-	1 I ME HOURS	16.50 17.80	2	T I ME MOUR S	19.00 19.30
H SAFETY ANA	SPILLWAY CRE 777-10 144	MAXIMUN Outflow Cfs	1901. 1058.	SPILLWAY CRES 777,10 144. 0.	MA KIMUM OU TFLOW CFS	21272. 21074.	STATION	MAXIMUN Stage "Ft	714.8 713.3	STATION	MAXIMUM S TAGE JF T	722.6	NO 11 V S	MAXIMUM Stage of T	554 •0 553 • 1
MINARY OF DA	• 10 • 10	MAX [MUM STORAGE AC -F T	216. 205.	VALUE • 10 44 0•	MAXIMUM S TORAGE AC -FT	198. 198.	LAN 1	MAXIMUM FLOW,CFS	1901. 1058.	LAN 2	MAXIMUM Flow, cf s	13346. 13051.	AN T	MAX IMUM FLOWACFS	1899. 105 6.
SI	1 N I I N I 7 7 1	MAXIMUM DEPTH Over Dam	1.13 .56	4 222 7 1 1 1 4	HAXINUM Depin Dver dam	•22 •23	ē.	RAT 10	•30	ē	RA 110	• 50	14	RAT 10	•50
	ELEVATION Storage Outflow	MAXIMUM Reservoir N.S.elev	781.33 780.76	ELEVATION S TORAGE Dutflow	MAXIMUM Reservoir Noseelev	780+42 780+43									
		RAT10 05 PMF	• 30		R АТ 10 Ог Риг	•50 •30									
	PLAN 1			PLAN 2											

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PLAN 1STATION7RatioMaximumNaximumTimeRatioFlow_cFSStage_fTMours.501897.460.719.20.301055.460.115.50 TIME HOURS 16.50 17.80 TIME HOURS 19.40 TIME HOURS 16.60 17.90 19•20 15•50 T I NE MOUR S TINE MOURS 16.60 17.90 9 • MAXIMUM Stagesft A I. . MAKINUM Stagesft HAXINUM HAXINUM Ratio Flowacfs Staceaft •50 9838• 519•4 •30 9419• 519•5 MAXIMUM S TAGE oF T 558•7 558•7 514.6 513.5 462.8 462.8 PLAN 1 STATION PLAN 2 STATION PLAN Z STATION MAX I MUM FLOV "CFS MAXIMUM FLOW,CFS 11250. 11078. 1899. 1056. RATIO FLONSCFS 8883. 8723. RA 1 10 RATIO •50 •50 20 20

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GANNETT FLEMING CORDDRY	SUBJECT
AND CARPENTER. INC.	SHEET NOOPSHEET NOOPSHEET NOOPSHEET S
HARRISBURG, PA.	FOR
	COMPUTED BYDATECHECKED BYDATE

<u>Middle</u> Dam <u>Summary of Pertinent</u> Results

PMF Rainfall = 25.2 inches PMF Runoff = 22.9 inches

Multi-ratio Analysis:	PME	1/2 PMF
East Stroudsburg Dam :		
inflow (cf:)	3,854	1-9
Outflow (efs)	3,409	1,170
Depth of Quertepping (feet)	2.17	0.05
Duration of Overtupping (nous)	7.5	0.8
Middle Domin		
inflow (cfs)	5,200	1,445
Outflow (cfs)	5,200	1,941
Depth of Questopping (feet)	2.28	1.15
Duration of Overtopping (heres)	13.5	1.3

Breach Analysis - Middle Dam (1/2 DMF): Station Stream Depth (ft) Number No Failure Falure A Depth (ft) 6 4.6 9.4 4.8 7 4.7 6.8 2.1

Notes :

1 Brooch analysis for Middle Dam did not consider presible failure of East Structurey Do. . 2. Station Number Identification: Station 6 : 1 Dwelling Station 7 : 9 Dwellings

> PHIS FACE TO SOL GLADATY FRACTOR PTF. FROM OUT Y INTERIMED TO DDC

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APPENDIX E PLATES

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	PHASE I INSPECTION REPORT	
	NATIONAL DAM INSPECTION PROGRAM	
	BURUUGH OF EAST STROUDSBURG	
	SHEET 2 OF 2	
1	JANUARY 1980 PLATE E-3	G- 1
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APPENDIX F

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MIDDLE DAM

APPENDIX F

GEOLOGY

Middle Dam is located in Monroe County in the Appalachian Plateau Physiographic Province. The most pronounced topographic feature in the area is Camelback Mountain, which is a part of the Pocono Escarpment. The greatest relief along the escarpment is 1,000 feet, which occurs at Camelback Mountain. Streams east of the escarpment drain directly into the Delaware River, while those to the west drain to the Lehigh River. The Pocono Plateau section lies to the west of the escarpment. The Glaciated Low Plateau section is east of the escarpment, and is characterized primarily by preglacial erosional topography with locally-thick, glacial deposits. Generally, local relief is 100 to 300 feet.

Middle Dam is located within the Glaciated Low Plateau Section. Bedrock units of the Section include siltstones of the Mahantango Formation, siltstones and shales of the Trimmers Rock Formation, and seven mapped members of the Catskill Formation. These members include sandstones, siltstones, and shales of the Towamensing Member; sandstone, siltstone, and shale of the Walcksville Member; sandstones, siltstones, and shale of the Beaverdam Run Member; sandstone and shale in the Long Run Member; sandstones and conglomerates in the Packerton Member; sandstones and some conglomerates in the Poplar Gap Member; and sandstones and conglomerates in the Duncannon Member.

Middle Dam is underlain by the Mahantango Formation. The Mahantango Formation is primarily siltstone or silty shale. Bedding is generally thin to medium and well-developed. Primary porosity is low, but secondary porosity due to cleavage can be significant.

The rocks of the Mahantango Formation are reported to maintain high-angle slopes, but when excavated parallel to cleavage strike, they are susceptible to rockfalls.

Bedrock is entirely overlain by glacial till of late Wisconsin Age. This till is primarily an unsorted mixture of clay, silt, sand, and gravel. It is moderately cohesive and is generally derived from the local sandstones of the Catskill Formation. The till in this area averages 15 feet in thickness, with variations ranging from 3 to 48 feet. The thickness is generally controlled by the bedrock topography with maximum thickness occuring in bedrock depressions and valleys.

The available records indicate that Middle Dam is entirely founded on the glacial till. Construction progress reports describe the corewall foundation material as blue clay and blue hardpan with occasional small pockets or streaks of gravel. The depth to bedrock is not known.

