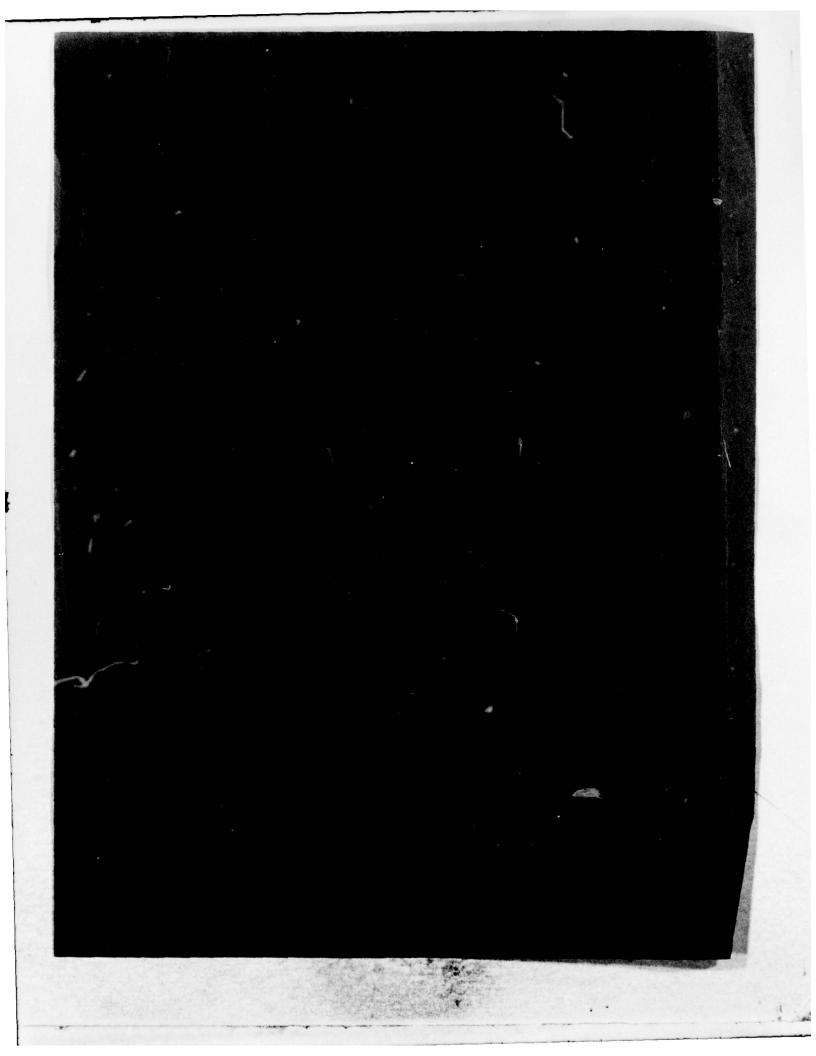


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PREFACE

The work described in this report was authorized under Project 1M263721D604, Collective Protection for Combat Vehicles. It was begun in September 1977 and finished at the end of June 1978.

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PREFACE

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I. INTRODUCTION.

To ensure that the current combat vehicle fleet has adequate nuclear, biological and chemical (NBC) protection, the Army established an armored-vehicle program managed by US Army Tank Automotive Research and Development Command (TARADCOM). The central effort of this program is at Chemical Systems Laboratory (CSL), Aberdeen Proving Ground. To characterize a vehicle's vulnerability to NBC agents, physical parameters are defined and a series of challenge tests are conducted to quantify the data base. Vehicle leakage enables modeling of air exchange between the vehicle and its environment: Air exchange determines the concentration of NBC agent that infiltrates the vehicle. The purpose of this report is (1) to summarize three sets of M113A1 Armored Personnel Carrier (APC) leakage data which has been acquired from Aerophysics Company, Donaldson Corporation, and Research Division, CSL and (2) to prepare preliminary modification for major leak areas.

II. TEST PROCEDURES.

Test methodologies were reviewed in a previous report* and it was recommended that a standardized-leakage-testing procedure be utilized. A standardized-vehicle-leakage test procedure enables comparison of leakage data generated by different sources. A short description of each test procedure is provided.

CSL supplies air through commander's hatch with a centrifugal blower and measures the flow rate with a calibrated-axial-vane anemometer immediately before discharge into the vehicle. The exterior and/or interior of the vehicle is then examined (generally by feel) to locate sources of air leakage which are then sealed with duct seal or tape. Once all accessible leaks are sealed, the unaccounted leakage is measured. Next, each individual leak is unsealed, and each associated leakage measured at several differential static pressures. Each leakage measurement is then repeated. The leak area is resealed prior to measuring the next leak area.

Aerophysics supplies the air through the air intake port using a "code tester" built in accordance with the Joint Air Moving and Conditioning Association, Inc. — American Society of Heating, Refrigerating, and Air Conditioning Engineers' specifications published in April 1975. The "code tester" has the capability to measure airflow up to 6000 ft³/min. The air mover is a variable-speed centrifugal fan, controlled by a variable voltage-variable frequency "varidyne" electric generator. Initial leak identification is made by feel. After all accessible leaks are sealed with duct tape, the unaccounted leakage is measured. Next, each leak is unsealed and the associated leakage measured at several differential static pressures.

Donaldson Corporation leakage data was extracted from a report.** It is assumed that the data was measured by a similar procedure.

^{*} Ferriter, J. M., and Beeson, L. J. ARCSL-TR-79041. Summary of M60A1 Tank Leakage Testing, June 1979.

^{**} Krisko, W. J., Camplin, H. R., and Schoen, D. W. Donaldson Corporation. Contract DAAK-11-78-C-0020. Final Report. Investigative Study of Positive Pressure Collective Protection for Combat/Armored Vehicles. August 1978.

III. LEAKAGE DATA RESULTS.

The data from the three sources are collected in the table. CSL and Aerophysics* conducted their tests on the same M113A1 APC's. The Donaldson Corporation data are from an unknown vehicle. Some of the Donaldson data are estimated from M577 Command Post Carrier (CPC) leakage data.

IV. DISCUSSION OF RESULTS.

Total leakage and individual leakage points are reported and are compared where applicable. All data are reported in standard cubic feet per minute at 1.5-inch water-gage static pressure.

A. Total Vehicle Leakage.

Serial No.	Aerophysics		CSL		Donaldson
	69569	55469	69569	55469	_
ft ³ /min	347	422	403	474	555.9

Aerophysics supplied air through the air inlet valve and did not measure a recordable leak at the driver's hatch. Leakage for firewall auxiliary blower was not measured on the vehicles tested by Aerophysics and CSL. If the data are corrected to reflect similar leak points, the comparative values are as follows:

Aerophysics		CS	Donaldson		
Serial No. ft ³ /min	69569 414	55469 487	69569 403	55469 474	513.8
В.	Commander's Tu	rret Ring.			
	Aerophysics		CS	<u>L</u>	Donaldson
Serial No.	69569	55469	69569	55469	
ft ³ /min	116	149	92	141	157

This is a major leak area.

^{*} Jackson, W. P., Foshag, W. F., and Boehler, G. D. Aerophysics Company. Contract DAAK11-78-M-0013. Final Report. Static Air Leakage on Two M113A1 Full Tracked Armored Personnel Carriers. August 1978.

Table. M113 APC Leakage - Comparison of Results

Leak location	Aerophysics 12B55469	Aerophysics 12C69569	CSL 12B55469	CSL 12C69569	Donaldson
		std ft ³ /n	nin at 1.5 in	wg*	
Vehicle as received	422	347	474	403	555.9
Commander's turret ring	149	116	141	92	157**
Ventilator control (closed)	103	56	109	67	39
Rear door	43		33	1	0
Grommets to engine		3	GR	3	6.9
Scupper valve	40	93	44	100	183
Ramp	17	8	0	3	
Torsion bars	12	24	16	28	
Bilge pump	15	15	11	13	7.4
Driver's periscope cover	11	9	12	9	6
Cargo hatch	2	1	0	0	4**
Engine access door	2	1	3	4	1**
Unaccounted leakage	28	21	11	9	25**
Firewall auxiliary blower				entro.	42**
Driver's hatch	o et ones est	Baetosa Lene di			5.5**
Air inlet valve (closed)			65	67	

^{*} Wg = water gage pressure ** Projected data

C. Ventilator Control (closed).

Serial No.	Aerophysics		CSL		Donaldson
	69569	55469	69569	55469	<u> </u>
ft ³ /min	56	103	67	109	39

Good agreement is obtained between Aerophysics and CSL. This leak value may depend on the tolerances of the valve.

D. Scupper Valve.

Serial No.	Aerophysics		CSL		Donaldson
	69569	55469	69569	55469	_
ft ³ /min	93	40	100	44	183

Leakage of the scupper depends on the position of valve.

E. Rear Door.

Serial No.	Aerop	nysics <u>CSL</u>		<u>L</u>	Donaldson
	69569	55469	69569	55469	- 100
ft ³ /min	-	43	1	33	0

The rear door on vehicle 55469 was warped.

F. Ramp.

Aerophysics			CSL		Donaldson
Serial No. ft ³ /min	69569 8	55469 17	69569 3	55469 0	

Leakage appears to depend on how securely the ramp is closed.

G. Air Inlet Valve.

Aerophysics			CSL		Donaldson
Serial No.	69569	55469	69569	55469	
ft ³ /min	_	_	67	65	-

H. Torsion Bars.

Aerophysics			CSL		Donaldson
Serial No.	69569	55469	69569	55469	_
ft ³ /min	24	12	28	16	_

I. Bilge Pump.

	Aerophysic	s	CS	Donaldson	
Serial No.	69569	55469	69569	55469	_
ft ³ /min	15	15	13	11	7.4

J. Driver's Periscope Cover.

	Aerophysic	5	CS	Donaldson	
Serial No.	69569	55469	69569	55469	-
ft ³ /min	9	11	9	12	6

V. LEAK REDUCTION MEASURES.

Proposed leakage reduction modifications were suggested by Donaldson Corporation, Aerophysics, and CSL. The following leakage reduction measures were suggested by Donaldson Corporation; however, Aerophysics Company and CSL had similar recommendations.

- A. The commander's turret ring could use a grease or a felt/"bristle pad" seal.
- B. A manual scupper valve device, as installed in the M577A1 CPC for NBC operation, would be advantageous.
- C. The combination of a gasket and fasteners should reduce the leakage for the air ventilator control and air inlet valve.
 - D. A more pliable and wider gasket for hatches and doors could be used.
- E. The installation of a manual valve in the bilge pump discharge line should be considered.
 - F. Grommets could be located at points where cables pass through the firewall.

VI. CONCLUSIONS.

- A. M113A1 APC leakage data indicates the possibility for leakage reduction in the following areas: commander's turret ring, scupper valve, hatches, doors, air ventilation control, air inlet valve, and bilge pump.
- B. The average leakage value for the M113A1 APC is 458 ft³/min at 1.5-inches water gage.

VII. RECOMMENDATIONS.

The six leakage reduction suggestions mentioned above ought to be examined. Incorporation of the suggested-leakage-reduction measures has a potential of reducing the M113A1 APC leakage value to 110 ft³/min at 1.5-inches water gage.

APPENDIX TABLES

Table A-1. M113 Armored Personnel Carrier (12B55469)
Aerophysics Company

Leakage areas	Leakag	Leakage rates at the internal static pressure (in water, gage) immediately below	e internal st	atic pressur	e (in water,	gage) imm	ediately bel	ow
coop of the coop o	1.0	2.0	3.0	4.0	5.0	0.9	7.0	8.0
				ft ³ /min	u			
Cupola	120	177	227	259	293	327	357	391
Ventilator (closed)	83	123	149	171	161	213	239	261
Rear door	34	52	99	81	25	109	122	137
Scupper valve	32	48	59	89	78	88	76	109
Ramp	13	20	25	79	78	32	34	40
Torsion bars	10	14	17	18	18	19	115	17
Bilge pump	12	17	21	23	25	29	59	31
Driver's periscope cover	∞	14	18	20	21	24	23	27
Main hatch	-	2	2	2	7	2	8	4
Engine access doors	16	3	2	2	-	-	0	0
Sealed tank	22	33	43	51	09	99	9/	8
Total (measured)	341	495	919	719	817	905	966	1094
Total (added)	351	503	629	721	811	910	995	1098

Table A-2. M113 Armored Personnel Carrier (12C69569)
Aerophysics Company

Leakage areas Leakage rates at the internal static pressure (in water, gage) immediately below 1.0 2.0 3.0 4.0 5.0 6.0 7.0 Cupola 94 138 171 202 228 258 290 Ventilator (closed) 45 66 82 93 108 116 127 Grommets (engine/driven) 3 3 3 3 4 4 5 Scupper valve 77 109 134 155 171 187 202 Ramp 7 9 9 9 9 9 9 10 Bilge pump 12 18 21 23 25 28 30 Brige pump 12 18 21 23 25 28 30 Brige pump 12 18 21 22 22 28 30 Wire channel 1 1 1 1 1 1 1 Sealed tank									
tor (closed) 1.0 2.0 3.0 4.0 1.1 94 138 171 202 1.2 45 66 82 93 1.3 3 3 3 1.4 109 134 155 1.5 99 99 99 1.5 99 99 99 1.5 99 99 99 1.5 99 99 99 1.5 99 99 99 1.5 99 99 99 1.5 99 99 99 1.5 99 99 99 1.5 99 99 99 1.5 99 99 99 1.5 99 99 99 1.5 99 99 99 1.5 99 99 99 1.5 99 99 99 1.5 99 99 99 1.5 99 99 1.5 99 99 1.5 99 99 1.5 99 99 1.5 99 99 1.5 99 99 1.5 99 99 1.5 99 99 1.5 99 99 1.5 99 99 1.5 99 99 1.5 99 99 1.5	Leakage areas	Leakage	e rates at th	e internal stat	tic pressure	(in water, ga	ige) imme	diately belo	W
tror (closed) 45 66 82 93 nets (engine/driven) 3 3 3 3 3 sr valve 77 109 1134 155 7 9 9 9 9 7 9 9 9 9 n bars ump 12 18 21 23 ump periscope cover 7 10 12 12 12 atch 0 1 1 1 1 atch 0 11 2 2 tank 17 25 32 40 added) 283 412 505 580		1.0	2.0	3.0	4.0	5.0	0.9	7.0	8.0
tor (closed) 45 66 82 93 nets (engine/driven) 3 3 3 3 3 sr valve 77 109 134 155 n bars 19 29 9 9 n bars 19 29 35 39 nmp 12 18 21 23 periscope cover 7 10 12 12 12 atch 0 1 1 1 1 1 atch 0 1 1 3 3 31 tank 17 25 32 40 measured) 267 397 493 572					ft ³ /m	,s			
tor (closed) 45 66 82 93 nets (engine/driven) 3 3 3 3 sr valve 77 109 134 155 n bars 7 9 9 9 9 n bars 19 29 9 9 9 9 n bars 19 29 35 39 <	Cupola	96	138	171	202	228	258	290	318
nets (engine/driven) 3 3 3 3 sr valve 77 109 134 155 n bars 7 9 9 9 n bars 19 29 35 39 ump 12 18 21 23 periscope cover 7 10 12 12 atch 0 1 1 1 access doors 1 1 2 2 nannel 1 3 3 1 tank 17 25 32 40 added) 267 397 493 572 added) 283 412 505 580	Ventilator (closed)	45	99	82	93	108	116	127	138
r valve 77 109 134 155 n bars 7 9 9 9 n bars 19 29 35 39 ump 12 18 21 23 periscope cover 7 10 12 12 atch 0 1 1 1 access doors 1 1 2 2 namel 1 3 3 40 measured) 267 397 493 572 added) 283 412 505 580	Grommets (engine/driven)	ю	3	æ	8	4	4	8	5
n bars 19 9 9 9 n bars 19 29 35 39 ump 12 18 21 23 periscope cover 7 10 12 12 atch 0 1 1 1 access doors 1 1 2 2 namel 1 3 3 1 tank 17 25 32 40 added) 267 397 493 572 added) 283 412 505 580	Scupper valve	77	109	134	155	171	187	202	215
19 29 35 39 12 18 21 23 ope cover 7 10 12 12 o 1 1 1 1 s doors 1 1 2 2 1 3 3 1 red) 267 397 493 572 ned) 283 412 505 580	Ramp	7	6	6	6	6	6	10	=
12 18 21 23 ope cover 7 10 12 12 o 1 1 1 1 s doors 1 1 2 2 1 3 3 1 red) 267 397 493 572 b 283 412 505 580	Torsion bars	19	29	35	39	43	47	20	53
Ope cover 7 10 12 12 6 doors 1 1 1 1 8 doors 1 1 2 2 1 3 3 1 1 red) 267 397 493 572 red) 283 412 505 580	Bilge pump	12	18	21	23	25	78	30	33
o 1 1 1 s doors 1 1 2 2 1 3 3 1 17 25 32 40 red) 267 397 493 572 o 283 412 505 580	Driver periscope cover	7	10	12	12	12	13	4	4
s doors 1 1 2 2 1 3 3 1 17 25 32 40 red) 267 397 493 572 0 283 412 505 580	Main hatch	0	-	-	-	-	-	-	-
red) 1 3 3 1 17 25 32 40 267 397 493 572) 283 412 505 580	Engine access doors	-	-	2	2	ю	8	8	4
17 25 32 40 267 397 493 572 283 412 505 580	Wire channel	-	3	æ	-	-	-	-	-
267 397 493 572 283 412 505 580	Sealed tank	17	25	32	40	45	20	\$	28
283 412 505 580	Total (measured)	267	397	493	572	645	717	778	843
	Total (added)	283	412	205	280	059	717	787	851

Appendix

Table A-3. Research Leakage Data. Vehicle M113A1 (12C69569)

elichert des		Leakage rates							
Leakage point			Static	pressure	,				
	0.5	1.0	1.5	2.0	3.0	6.0			
			ft ³ /	min					
Front vent open	367	523	644	746	917	1306			
Rear vent open	307	441	544	632	780	1119			
Commander's turret ring	51	74	92	108	135	197			
Front vent closed	41	55	67	76	92	127			
Rear vent closed	30	46	59	70	91	140			
Scupper valve	58	82	100	115	140	198			
Rear door	0	1	1	1	1	2			
Torsion bars	16	23	28	32	38	54			
Driver's periscope cavity plug	2	3	4	5	6	18			
Rear bilge pump outlet	7	10	13	16	20	29			
Driver's infrared (IR) periscope	1	1	2	2	3	4			
Unaccounted for leakage	4	7	9	11	15	25			
Engine compartment bulkhead area	2	3	4	5	6	9			
Ramp	2	2	3	4	5	0			

Table A-4. Research Leakage Data. Vehicle M113A1 (12B55469)

			Leakage	e rates		
Leakage point			Static p	ressure		
	0.5	1.0	1.5	2.8	3.0	6.8
			ft ³ /r	nin		
Front vent open	368	523	642	743	912	1295
Rear vent open	290	413	508	587	723	1030
Commander's turret ring	75	112	141	166	218	311
Front vent closed	58	86	189	128	180	238
Rear vent closed	27	47	63	92	114	199
Scupper valve	23	34	44	52	66	99
Rear door	17	25	33	40	52	81
Torsion bars	9	13	16	19	23	34
Driver's periscope cavity plug	5	8	10	12	15	22
Rear bilge pump outlet	6	9	11	13	17	26
Driver's IR periscope	6	9	12	14	17	26
Unaccounted for leakage	5	8	11	13	17	29
Engine compartment bulkhead area	1	2	3	3	3	5
Ramp	0	0	0	0	0	0

Table A-5. Donaldson Corporation Report Data

Leakage areas	Leakage be	fore sealing
Danage areas	1.5 in wg	7.0 in wg
	ft ³ /	min
Commander's turret ring	140*	370*
Commander's hatch	3*	8*
Commander's and driver's periscopes	14	37**
Driver's hatch	5.5**	15**
Cargo hatch	4**	11**
Driver's infrared (IR) periscope	6**	15
Firewall bilge scuppers	183	510
Firewall auxiliary blower	69	228
Firewall cable openings	43**	116
Air ventilating exhaust	39	88
Bilge pump discharge	7.4	28
Firewall access panel	1**	3
Ramp door	0	1
Personnel heater	17	39
Unaccountable leakage	25**	66
Total leakage	555.9	1535

* Estimated leakage
** Extrapolated from leakage data on M113 APC or M577 CPC.

Table A-6. M577 Command Post Carrier Air Leakage

		L	eakage rates		
Leakage areas		Internal static	pressure as in	water gage	
College and the College and th	0.40	1.0	3.0	5.0	7.0
men)			ft ³ /min		
Unaccounted leaks	-	20.0	38.6	53.0	66.5
Commander's hatch	_ å	0,7	1.3	2.3	1.5
Driver's hatch	- 61	1.7	5.1	5.7	8.3
Ramp door		0.6	0.5	0.2	0.4
Air ventilating exhaust		32.0	59.5	80.8	88.3
Driver's IR periscope	3.3	4.9	12.8	17.0	15.0
Bilge pump discharge	6.0	6.5	10.0	20.0	28.0
Firewall access panels	0.3	-	5.0	-	3.0
Firewall cable openings	29.1	52.0	83.0	98.0	116.0
Firewall auxiliary blower	44.0	49.5	127.0	177.0	228.0
Firewall bilge scuppers	81.0	145.0	295.0	410.0	510.0
Total leakage	163.7	312.9	637.8	864.0	1065.0

NOTE: These tests were performed with the crew compartment pressurized and the engine compartment not pressurized. Under normal operating conditions, leakage through the firewall and bilge scuppers would not be this great.

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