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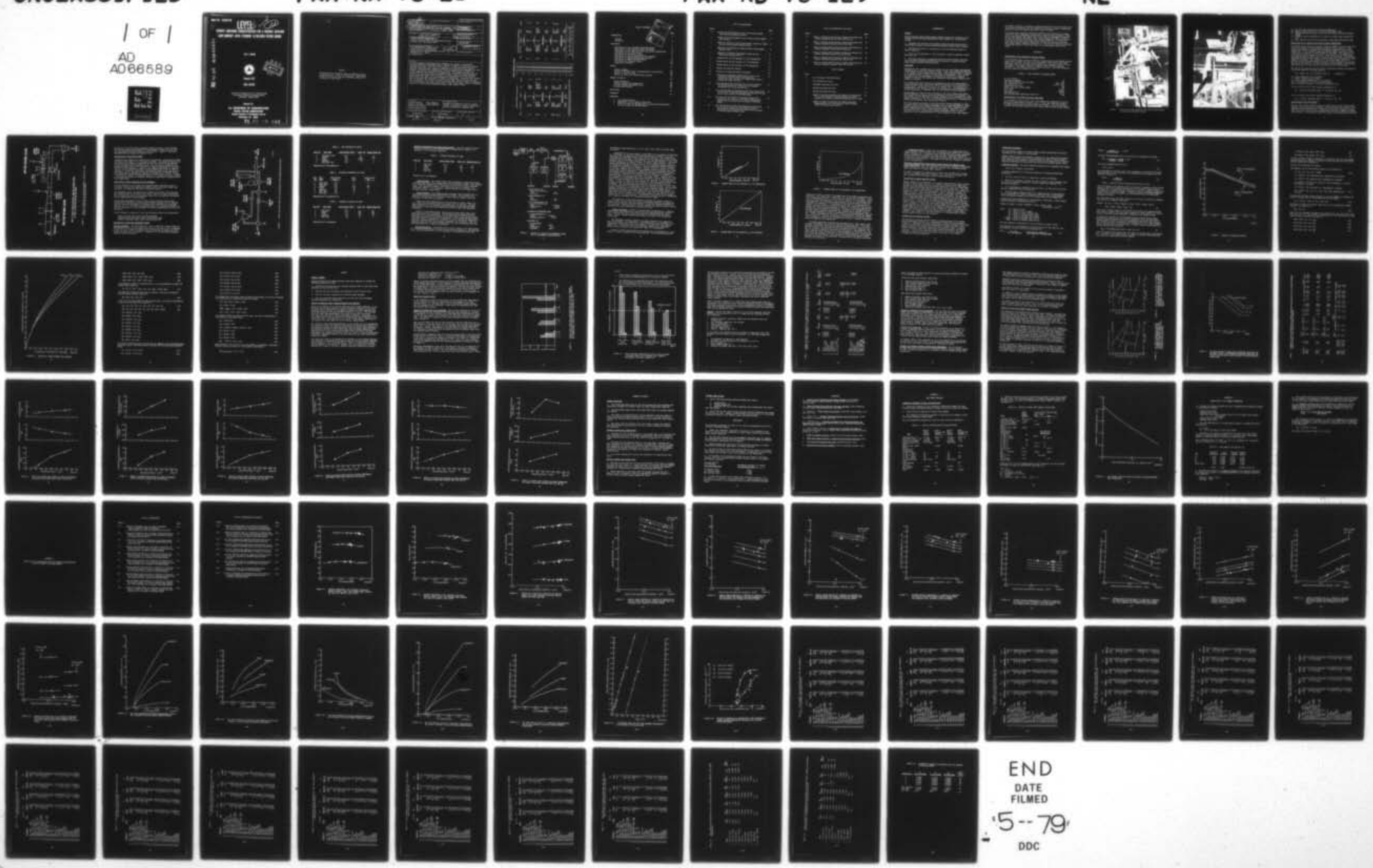

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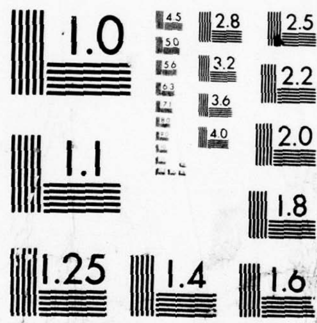

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Report No. FAA-RD-78-129

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EXHAUST EMISSIONS CHARACTERISTICS FOR A GENERAL AVIATION LIGHT-AIRCRAFT AVCO LYCOMING IO-360-B1BD PISTON ENGINE

Eric E. Becker

February 1979

FINAL REPORT

Prepared for

U.S. DEPARTMENT OF TRANSPORTATION
FEDERAL AVIATION ADMINISTRATION
Systems Research & Development Service
Washington, D.C. 20590

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16. Abstract

The Avco Lycoming IO-360-B1BD engine (S/N887-X) was tested at the National Aviation Facilities Experimental Center (NAFEC) to develop a steady state exhaust emissions data base. This data base consists of current production baseline emissions characteristics, lean-out emissions data, effects of leaning-out the fuel schedule on cylinder head temperatures, and data showing ambient effects on exhaust emissions and cylinder head temperatures. The engine operating with its current full-rich production fuel schedule could not meet the proposed Environmental Protection Agency (EPA) standard for carbon monoxide (CO) and unburned hydrocarbons (HC) under sea level standard-day conditions. The engine did, however, meet the proposed EPA standards for oxides of nitrogen (NO_x) under the same sea level conditions. The results of engine testing under different ambient conditions are also presented, and these results show a trend toward higher levels of emissions output for CO and HC while producing slightly lower levels of NO_x.

17. Key Words
General Aviation, Piston Engines, Oxides of Nitrogen, Carbon Monoxide, Emissions (Pollution), Unburned Hydrocarbons

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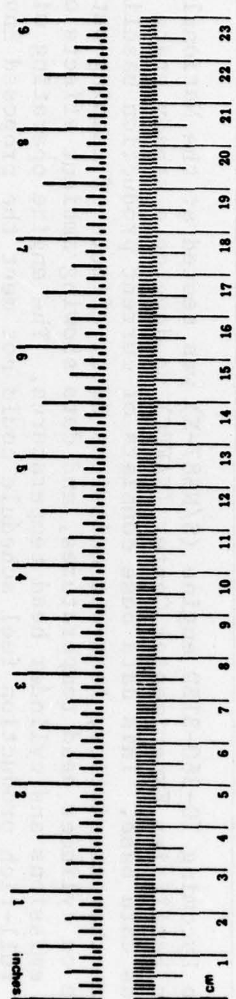
METRIC CONVERSION FACTORS

Approximate Conversions to Metric Measures

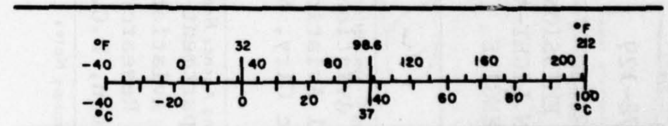
Symbol	When You Know	Multiply by	To Find	Symbol
		LENGTH		
in	inches	*2.5	centimeters	cm
ft	feet	30	centimeters	cm
yd	yards	0.9	meters	m
mi	miles	1.6	kilometers	km
		AREA		
in^2	square inches	6.5	square centimeters	cm^2
ft^2	square feet	0.09	square meters	m^2
yd^2	square yards	0.8	square meters	m^2
mi^2	square miles	2.6	square kilometers	km^2
	acres	0.4	hectares	ha
		MASS (weight)		
oz	ounces	28	grams	g
lb	pounds	0.45	kilograms	kg
	short tons (2000 lb)	0.9	tonnes	t
		VOLUME		
tsp	teaspoons	5	milliliters	ml
Tbsp	tablespoons	15	milliliters	ml
fl oz	fluid ounces	30	milliliters	ml
c	cups	0.24	liters	l
pt	pints	0.47	liters	l
qt	quarts	0.95	liters	l
gal	gallons	3.8	liters	l
ft^3	cubic feet	0.03	cubic meters	m^3
yd^3	cubic yards	0.76	cubic meters	m^3
		TEMPERATURE (exact)		
°F	Fahrenheit temperature	5/9 (after subtracting 32)	Celsius temperature	°C

*1 in = 2.54 (exactly). For other exact conversions and more detailed tables, see NBS Misc. Publ. 286, Units of Weights and Measures, Price $2.25, SD Catalog No. C13.10:286.



Approximate Conversions from Metric Measures

Symbol	When You Know	Multiply by	To Find	Symbol
		LENGTH		
mm	millimeters	0.04	inches	in
cm	centimeters	0.4	inches	in
m	meters	3.3	feet	ft
m	meters	1.1	yards	yd
km	kilometers	0.6	miles	mi
		AREA		
cm^2	square centimeters	0.16	square inches	in^2
m^2	square meters	1.2	square yards	yd^2
km^2	square kilometers	0.4	square miles	mi^2
ha	hectares (10,000 m^2)	2.5	acres	
		MASS (weight)		
g	grams	0.035	ounces	oz
kg	kilograms	2.2	pounds	lb
t	tonnes (1000 kg)	1.1	short tons	
		VOLUME		
ml	milliliters	0.03	fluid ounces	fl oz
l	liters	2.1	pints	pt
l	liters	1.06	quarts	qt
l	liters	0.26	gallons	gal
m^3	cubic meters	35	cubic feet	ft^3
m^3	cubic meters	1.3	cubic yards	yd^3
		TEMPERATURE (exact)		
°C	Celsius temperature	9/5 (then add 32)	Fahrenheit temperature	°F



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INTRODUCTION

PURPOSE.

General aviation piston engine exhaust emission tests were conducted at the National Aviation Facility Experimental Center (NAFEC) for the following reasons:

1. Determine and establish total exhaust emissions characteristics for a representative group of current production general aviation piston engines.

2. Determine the effects of leaning-out of the fuel metering system on exhaust emissions.

3. Verify the acceptability of test procedures, testing techniques, instrumentation, etc.

4. Determine reductions in operating limits and safety margins resulting from fuel system adjustments/modifications evaluated for improved piston engine exhaust emissions characteristics.

BACKGROUND.

Beginning in 1967, Congress enacted a series of laws which added environmental considerations to the civil aviation safety, control, and promotional functions of the Federal Aviation Administration (FAA). This legislation was in response to the growing public concern over environmental degradation. Thus, the FAA was committed to the development, evaluation, and execution of programs designed to identify and minimize the undesirable environmental effects attributable to aviation.

In accordance with the Clean Air Act Amendments of 1970, the Environmental Protection Agency (EPA) established emission standards and outlined test procedures when it issued EPA rule part 87 in January 1973. The Secretary of Transportation, and therefore the FAA, was charged with the responsibility for issuing regulations to implement this rule and enforcing these standards.

Implementation of this rule was contingent on the FAA's finding that safety was not impaired by whatever means was employed to achieve the standards. For this reason, the FAA undertook a program, subsequent to the issuance of the EPA emission standards in July 1973, to determine the feasibility of implementation, verify test procedures, and validate test results.

There was concern on the part of the FAA that the actions suggested in order to comply with the EPA emission standards, such as operating engines at leaner mixture settings during landing and takeoff cycles, might compromise safety and/or significantly reduce engine operating margins. Therefore, the FAA contracted with Avco Lycoming and Teledyne Continental Motors to select engines that they considered typical of their production, test these engines as normally produced to establish a baseline emissions data base and then alter (by lean-out adjustments) the fuel schedule and ignition timing to demonstrate methods by which the proposed EPA limits could be reached.

In the event that hazardous operating conditions were indicated by the manufacturer's tests, independent verification of data would be necessary. Therefore, it was decided that duplication of the tests be undertaken at NAFEC to provide the needed verification. This report presents the NAFEC test results for the Avco Lycoming IO-360-B1BD piston engine (S/N887-X). It should be noted that since the time of these tests, the EPA has rescinded the promulgated piston engine standards (reference 1). This work is reported upon herein in the same light as it would have been if the requirements were still in effect.

DISCUSSION

DESCRIPTION OF AVCO LYCOMING IO-360-B1BD ENGINE.

The IO-360-B1BD engine tested at NAFEC is a fuel-injected, horizontally opposed engine with a nominal 360 cubic inch displacement (cid) rated at 180 brake horsepower (bhp) for a nominal brake specific fuel consumption (bsfc) of 0.50. This engine is designed to operate on 100/130 octane aviation gasoline (appendix A -- Fuel Sample Analysis of NAFEC Test Fuel). The vital statistics for this engine are provided in table 1.

TABLE 1. AVCO LYCOMING IO-360-B1BD ENGINE

No. of Cylinders	4
Cylinder Arrangement	HO
Max. Engine Takeoff Power (HP, RPM)	180, 2700
Bore and Stroke (in.)	5.125 x 4.375
Displacement (cu. in.)	361
Weight, Dry (lbs)--Basic Engine	299
Prop. Drive	Direct
Fuel Grade	100/130
Compression Ratio	8.5:1
Max. Cylinder Head Temperature Limit (°F)	500

DESCRIPTION OF TEST SETUP AND BASIC FACILITIES.

For the NAFEC sea level static tests, the engines were installed in the propeller test stand shown in figures 1 and 2. This test stand was located in the NAFEC General Aviation Piston Engine Test Facility. The test facility provided the following capabilities for testing light aircraft piston engines:

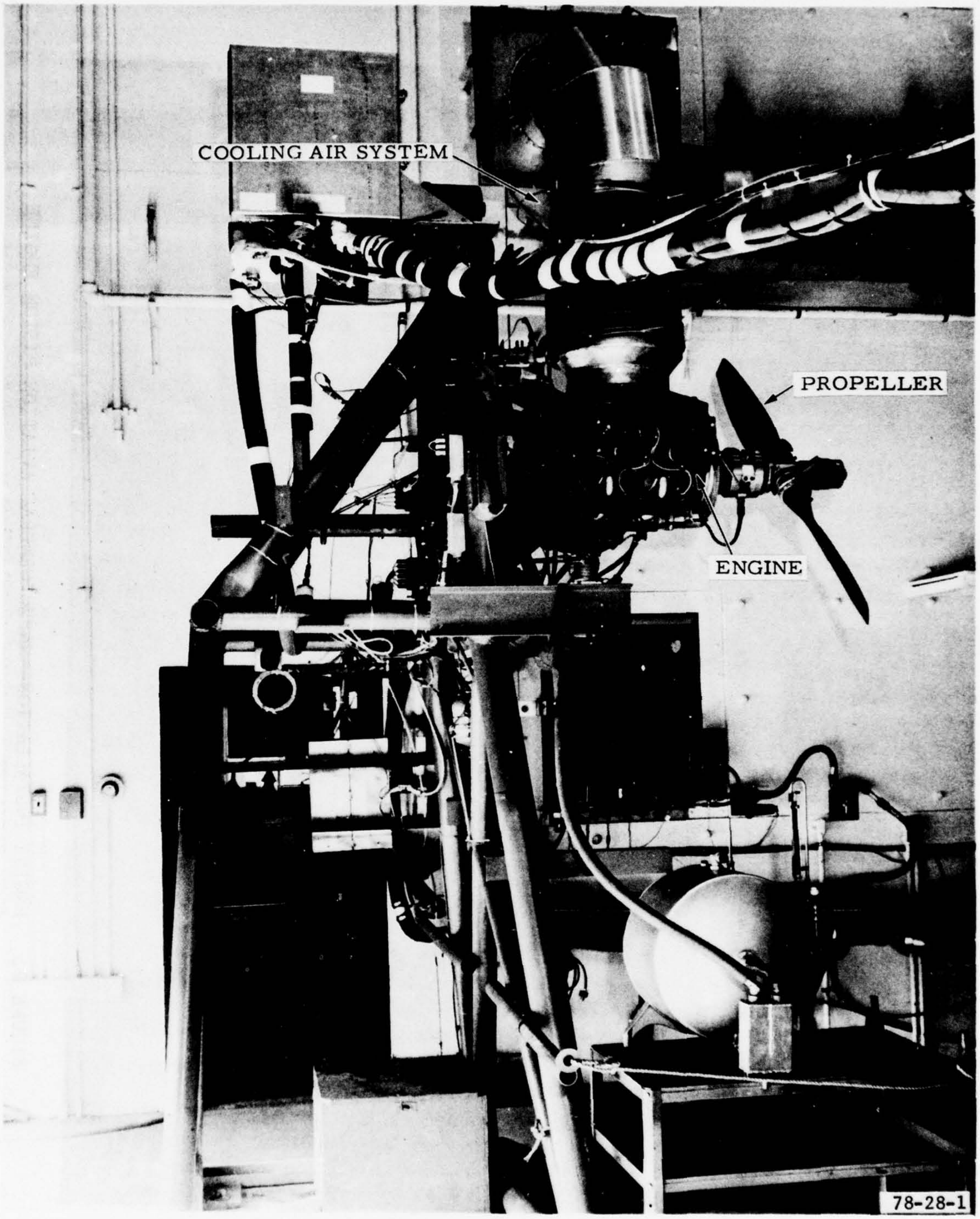


FIGURE 1. TYPICAL SEA LEVEL PROPELLER TEST STAND--PISTON ENGINE INSTALLATION--EMISSIONS TESTING

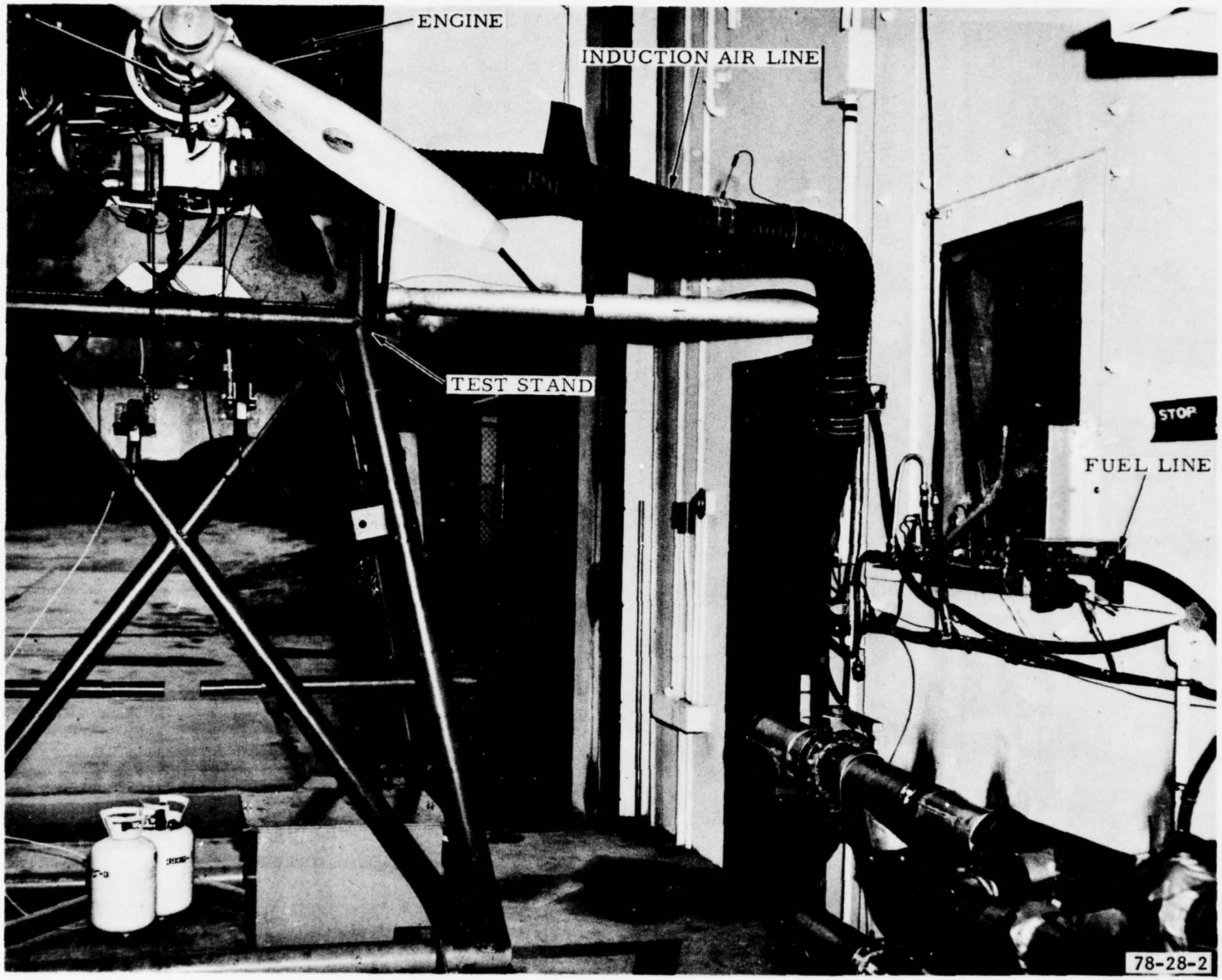


FIGURE 2. ENGINE INSTALLATION--NAFEC GENERAL AVIATION PISTON ENGINE TEST FACILITY

(1) Two basic air sources--dry bottled and ambient air
(2) Ambient temperatures (20 to 140 degrees Fahrenheit (°F))
(3) Nominal sea level pressures (29.50 to 30.50 inches of mercury absolute (inHgA)
(4) Humidity (specific humidity--0 to 0.020 lb of water (H_2O) vapor/lb dry air)
(5) Fuel (100/130 octane aviation gasoline--a dedicated 5,000 gallon tank)

DESCRIPTION OF AIR INDUCTION SYSTEM AND AIRFLOW COMPUTATIONS.

The airflow system (induction system) utilized at NAFEC for testing light aircraft piston engines is illustrated in schematic form in figure 3. This system incorporated a redundant airflow measuring system for accuracy and reliability. In the high-flow measuring section, NAFEC utilized a 3.0-inch orifice and an Autronics air meter (model No. 100-750S). The capability of this high-flow system ranged from 400 to 2,000 pounds per hour (lb/h) with an estimated reading tolerance in flow accuracy of ± 2 percent. The low-flow measuring section utilized a small 1.0-inch orifice and an Autronics air meter (model No. 100-100S). The capability of this system ranged from 40 to 400 lb/h with an estimated reading tolerance in flow accurancy of ± 3 percent. The size of the basic air duct was 8.0 inches (inside diameter) for the high-flow system and 2.0 inches (inside diameter) for the low-flow system.

The airflow was computed from the orifice differential pressure and induction air density using the following equation:

$$Wa = (1891)\ (C_f)\ (d_o)^2 \left[(.03609)\ \Delta P_\rho\right]^{1/2} \qquad \text{(reference 2)}$$

ΔP = inH_2O (differential air pressure)
ρ = lb/ft^3 (induction air density)
d_o = inches (inside diameter (i.d.) of orifice)
C_f = flow coefficient for orifice (nondimensional)
1891 = conversion constant for airflow in pounds per hour.

For the 3.0-inch orifice this equation simplifies to:

$$Wa = (10{,}381.6) \left[(.03609)\ \Delta P_\rho\right]^{1/2} = 1972.23\ (\ \Delta P_\rho\ )^{1/2}$$

For the 1.0-inch orifice this equation simplifies to:

$$Wa = (1{,}189.4) \left[(.03609)\ \Delta P_\rho\right]^{1/2} = 225.955\ (\ \Delta P_\rho\ )^{1/2}$$

DESCRIPTION OF FUEL FLOW SYSTEM.

The fuel flow system utilizied during the NAFEC light aircraft piston engine emission tests incorporated rotameters, turboflow meters, and a burette. The high-flow section incorporated a rotameter in series with a high-flow turbometer while the low-flow section incorporated a low-flow turbometer in series with a burette. The high-flow system was capable of measuring fuel flows from

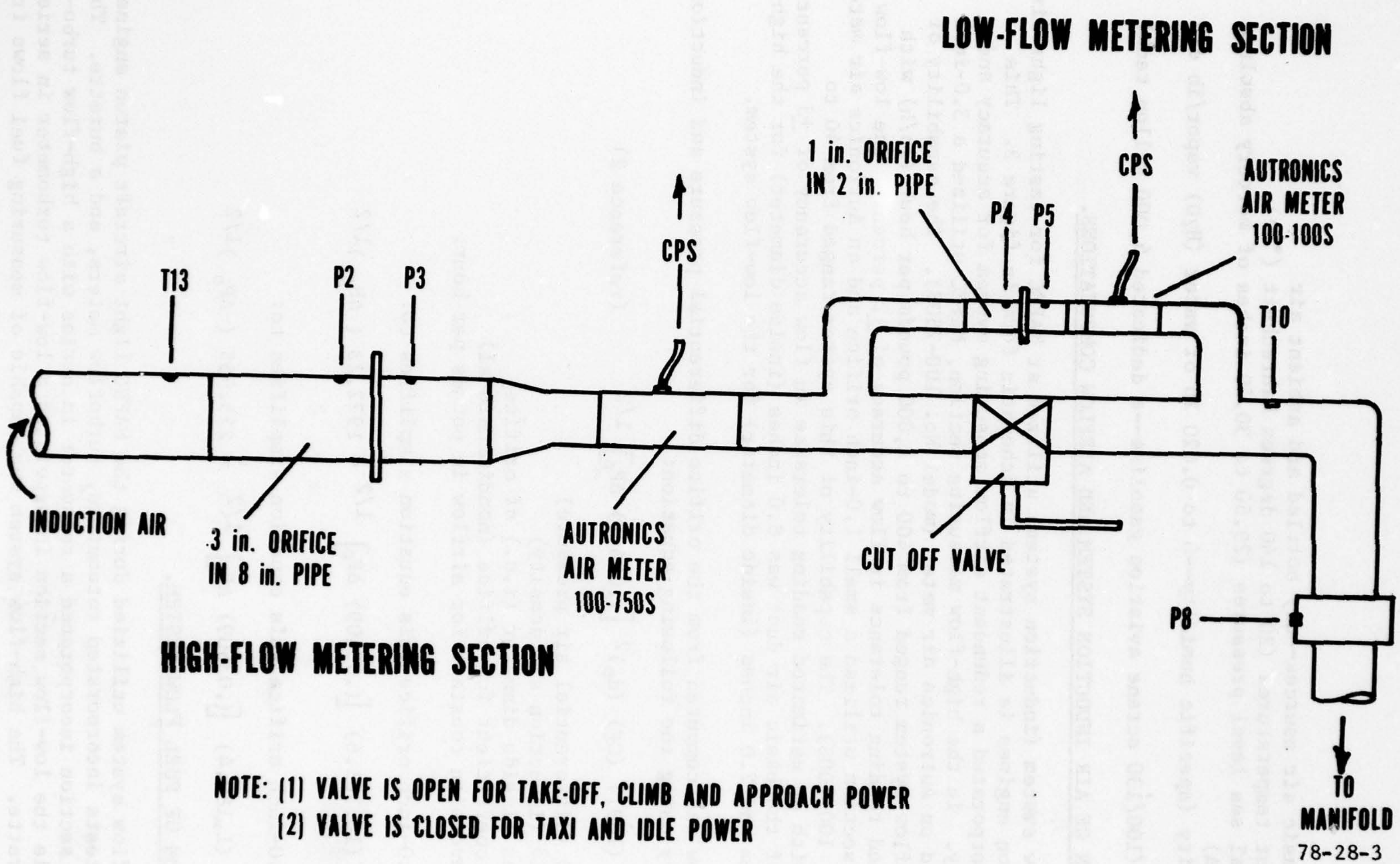


FIGURE 3. NAFEC AIR INDUCTION (AIRFLOW MEASUREMENT) SYSTEM FOR LIGHT-AIRCRAFT PISTON ENGINE EMISSION TESTS

50 lb/h up to 300 lb/h with an estimated reading tolerance of ±1.0 percent. The low-flow system was capable of flow measurements ranging from 0-50 lb/h with an estimated reading tolerance of ±2.0 percent. Figure 4 illustrates the NAFEC fuel flow system in schematic form.

DESCRIPTION OF COOLING AIR SYSTEM.

The NAFEC piston engine test facility also incorporated a system which provided cooling air (see figure 1) to the engine cylinders. The engine mounted in the test stand was enclosed in a simulated nacelle and cooling air was provided to this enclosure from an external source. The cooling air temperature was maintained within ±10°F of the induction air supply temperature for any specified set of test conditions. This not only minimized variations in temperature but also minimized variations in the specific weight of air for all test conditions. All of the basic cooling air tests with the IO-360-B1BD engine were conducted with differential cooling air pressures of 3.0 inH_2O. A range of differential cooling air pressures from 1.0 to 6.0 inH_2O were also evaluated to determine the effects of variable cooling air conditions on maximum cylinder head temperatures.

DESCRIPTION OF TEST PROCEDURES AND EPA STANDARDS.

The data presented in this report were measured while conducting tests in accordance with specific landing and takeoff cycles (LTO) and by modal lean-out tests. The basic EPA LTO cycle is defined in table 2.

The FAA/NAFEC contract and inhouse test programs utilized an LTO cycle which was a modification of the table 2 test cycle. Table 3 defines this modified LTO cycle which was used to evaluate the total full-rich emission characteristics of light-aircraft piston engines.

An additional assessment of the test data clearly indicates that further evaluations of the general aviation piston exhaust emission must be analyzed with the climb mode emissions at 100-percent and 75-percent power settings (tables 4 and 5). This would then provide basis for a complete evaluation of test data and permit a total assessment of the EPA standard based on LTO cyclic tolerances.

The EPA Standards (reference 1) that were evaluated during this program were:

Carbon monoxide (CO)--0.042 lb/cycle/rated BHP
Unburned hydrocarbon (HC)--0.0019 lb/cycle/rated BHP
Oxides of nitrogen (NO_x)--0.0015 lb/cycle/rated BHP

DESCRIPTION OF EMISSIONS MEASURMENT SYSTEM.

EMISSION ANALYZERS. The instrumentation used to monitor the exhaust emissions from general aviation piston engines was basically the same as that recommended by EPA, but with a number of modifications and additions to enhance the reliability and accuracy of the system. A schematic of the emissions measurement system is shown in figure 5.

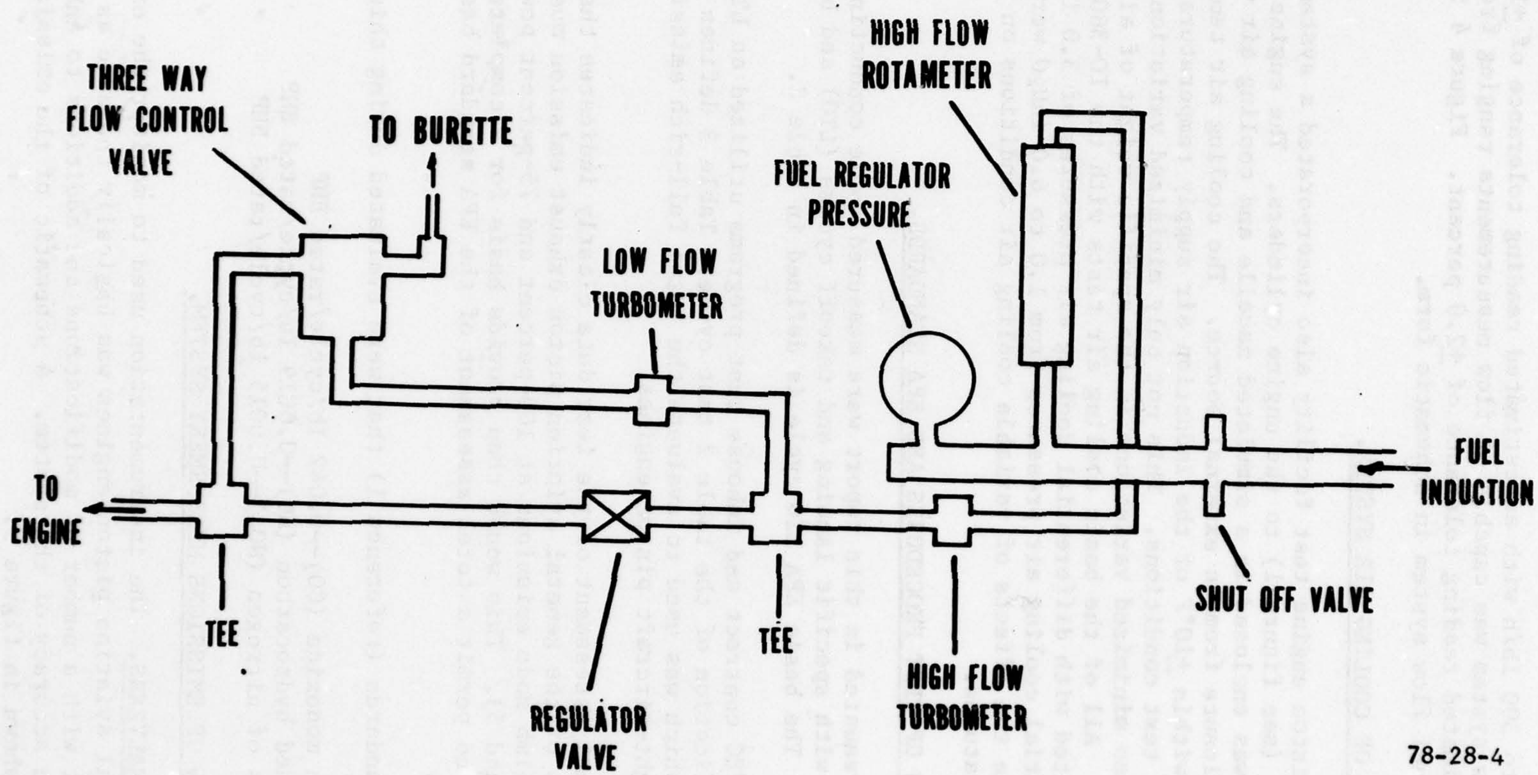


FIGURE 4. NAFEC FUEL FLOW SYSTEM FOR LIGHT-AIRCRAFT PISTON ENGINE EMISSION TESTS

TABLE 2. EPA FIVE-MODE LTO CYCLE

Mode No.	Mode Name	Time-In-Mode (Min.)	Power (%)	Engine Speed (%)
1	Taxi/idle (out)	12.0	*	*
2	Takeoff	0.3	100	100
3	Climb	5.0	75-100	*
4	Approach	6.0	40	*
5	Taxi/idle (in)	4.0	*	*

*Manufacturer's Recommendation

TABLE 3. FAA/NAFEC SEVEN-MODE LTO CYCLE

Mode No.	Mode Name	Time-In-Mode (Min.)	Power (%)	Engine Speed (%)
1	Idle (out)	1.0	*	*
2	Taxi (out)	11.0	*	*
3	Takeoff	0.3	100	100
4	Climb	5.0	80	*
5	Approach	6.0	40	*
6	Taxi (in)	3.0	*	*
7	Idle (in)	1.0	*	*

*Manufacturer's Recommendation

TABLE 4. MAXIMUM FIVE-MODE LTO CYCLE

Mode No.	Mode Name	Time-In-Mode (Min.)	Power (%)	Engine Speed (%)
1	Taxi (out)	12.0	*	*
2	Takeoff	0.3	100	100
3	Climb	5.0	100	100
4	Approach	6.0	40	*
5	Taxi (in)	4.0	*	*

*Manufacturer's Recommended

EMISSION INSTRUMENTATION ACCURACY/MODIFICATIONS. The basic analysis instrumentation utilized for this system, which is summarized in figure 5, is explained in the following paragraphs.

TABLE 5. MINIMUM FIVE-MODE LTO CYCLE

Mode No.	Mode Name	Time-In-Mode (Min)	Power (%)	Engine Speed (%)
1	Taxi (out)	12.0	*	*
2	Takeoff	0.3	100	100
3	Climb	5.0	75	*
4	Approach	6.0	40	*
5	Taxi (in)	4.0	*	*

*Manufacturer's Recommended

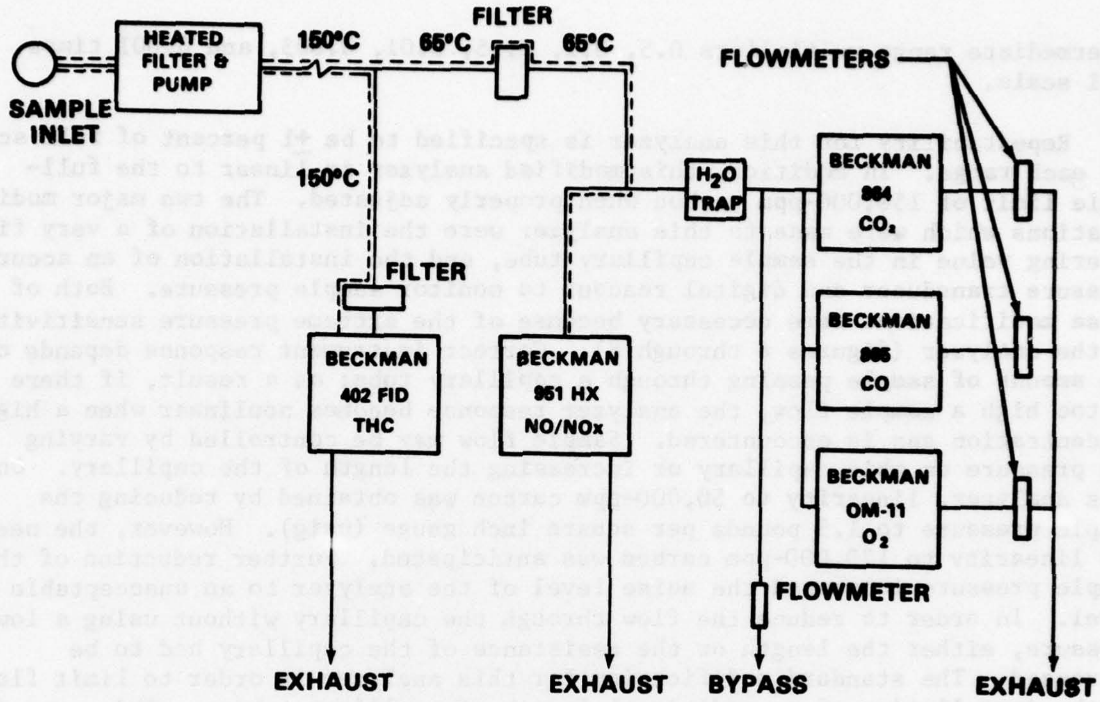
Carbon Dioxide. The carbon dioxide (CO_2) subsystem is constructed around a Beckman model 864-23-2-4 nondispersive infrared analyzer (NDIR). This analyzer has a specified repeatability of ±1 percent of full scale for each operating range. The calibration ranges on this particular unit are: Range 1, 0 to 20 percent; Range 3, 0 to 5 percent. Stated accuracy for each range is ±0.2 and ±0.05 percent, respectively.

Carbon Monoxide. The subsystem used to measure carbon monixide (CO) is constructed around a Beckman model 865-X-4-4-4 NIDR. This analyzer has a specified repeatability of ±1 percent of full scale for ranges 1 and 2 and ±2 percent of full scale for range 3.

Range 1 has been calibrated for 0 to 20 percent by volume, range 2 for 0 to 1,000 parts per million (ppm) and range 3 for 0 to 100 ppm. The wide-range capability of this analyzer is made possible by using stacked sample cells which in effect give this analyzer six usable ranges when completely calibrated.

Effects of interfering gases, such as CO_2 and water vapor, were determined and reported by the factory. Interferences from 10-percent CO_2 were determined to be 12-ppm equivalent CO, and interferences from 4-percent water vapor were determined to be 6-ppm CO equivalent. Even though the interference from water vapor is negligible, a condenser is used in the CO/CO_2 subsystem to eliminate condensed water in the lines, analyzers, and flowmeters. This condensation would have decreased analyzer sensitivity and necessitated more frequent maintenance if it had been eliminated.

Total Hydrocarbons. The system that is used to measure total hydrocarbons is a modified Beckman model 402 heated flame ionization detector. This analyzer has a full-scale sensitivity that is adjustable to 150,000-ppm carbon with



- **CARBON DIOXIDE — CO_2**
  - NONDISPERSIVE INFRARED (NDIR)
  - RANGE — 0-20%
  - REPEATABILITY — ± 0.2% CO_2
- **CARBON MONOXIDE — CO**
  - NDIR
  - RANGE — 0-20%
  - REPEATABILITY — ± 0.2% CO
- **TOTAL HYDROCARBONS — THC**
  - FLAME IONIZATION DETECTOR (FID)
  - RANGE — 0-150,000 ppm_c
  - MINIMUM SENSITIVITY — 1.5 ppm_c
  - LINEAR TO — 150,000 ppm_c
- **OXIDES OF NITROGEN — NO_X**
  - CHEMILUMINESCENT (CL)
  - RANGE — 0-10,000 ppm
  - MINIMUM SENSITIVITY — 0.1 ppm
- **OXYGEN — O_2**
  - POLARAGRAPHIC
  - RANGE — 0-100%
  - REPEATABILITY — 0.1% O_2
  - RESPONSE — 200 ms

FIGURE 5. SCHEMATIC OF EMISSIONS MEASUREMENT SYSTEM AND ITS MEASUREMENT CHARACTERISTICS

intermediate range multipliers 0.5, 0.1, 0.05, 0.01, 0.005, and 0.001 times full scale.

Repeatability for this analyzer is specified to be ±1 percent of full scale for each range. In addition, this modified analyzer is linear to the full-scale limit of 150,000-ppm carbon when properly adjusted. The two major modifications which were made to this analyzer were the installation of a very fine metering value in the sample capillary tube, and the installation of an accurate pressure transducer and digital readout to monitor sample pressure. Both of these modifications were necessary because of the extreme pressure sensitivity of the analyzer (figures 6 through 8). Correct instrument response depends on the amount of sample passing through a capillary tube; as a result, if there is too high a sample flow, the analyzer response becomes nonlinear when a high concentration gas is encountered. Sample flow may be controlled by varying the pressure on this capillary or increasing the length of the capillary. On this analyzer, linearity to 50,000-ppm carbon was obtained by reducing the sample pressure to 1.5 pounds per square inch gauge (psig). However, the need for linearity to 120,000-ppm carbon was anticipated. Further reduction of the sample pressure increased the noise level of the analyzer to an unacceptable level. In order to reduce the flow through the capillary without using a lower pressure, either the length or the resistance of the capillary had to be increased. The standard modification for this analyzer in order to limit flow is the installation of an additional length of capillary tubing. This procedure requires trial-and-error determination of proper capillary length and is a permanent modification that limits sensitivity at low hydrocarbon levels. By installing a metering valve in the capillary, flow could be selectively set at either low flow for linearity at high concentrations or high flow for greater sensitivity at low concentrations. Installation time was reduced by eliminating the cut-and-try procedure for determining capillary length.

The addition of a sensitive pressure transducer and digital readout to monitor sample pressure was needed since the pressure regulator and gauge supplied with the analyzer would not maintain the pressure setting accurately at low pressures. Using the digital pressure readout, the sample pressure could be monitored and easily maintained to within 0.05 inH_2O.

Oxides of Nitrogen. Oxides of nitrogen (NO_x) are measured by a modified Beckman model 951H atmospheric pressure, heated, chemilluminescent analyzer (CL). This analyzer has a full-scale range of 10,000 ppm with six intermediate ranges. Nominal minimum sensitivity is 0.1 ppm on the 10-ppm full-scale range.

The atmospheric pressure analyzer was chosen because of its simplicity, ease of maintenance, and compactness. Anticipated water vapor problems in the atmospheric pressure unit were to be handled by the heating of the internal sample train. Interference from CO_2 quenching, common in the atmospheric pressure type CL analyzer, was checked and found to be nonexistnet.

A series of major modifications were performed by the manufacturer on this analyzer to insure compliance with specifications. One such modification was

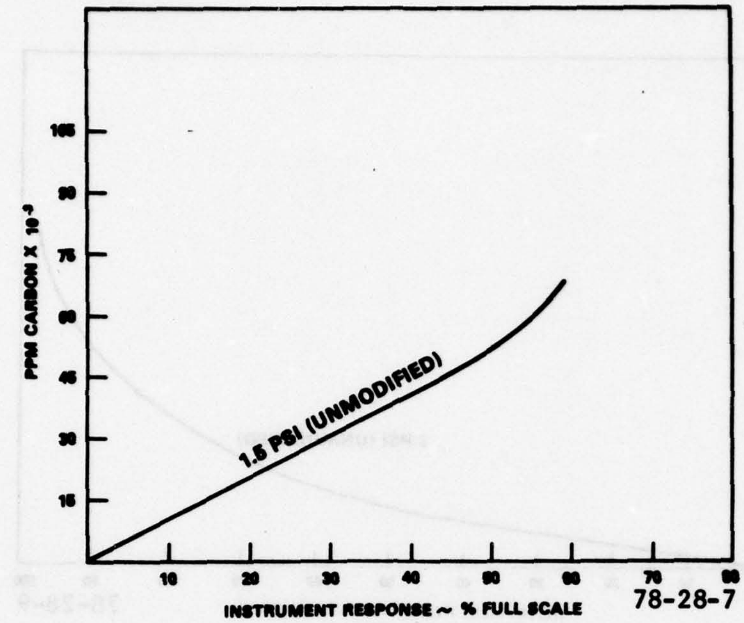


FIGURE 6. BECKMAN MODEL 402 THC ANALYZER (1.5 PSI UNMODIFIED)

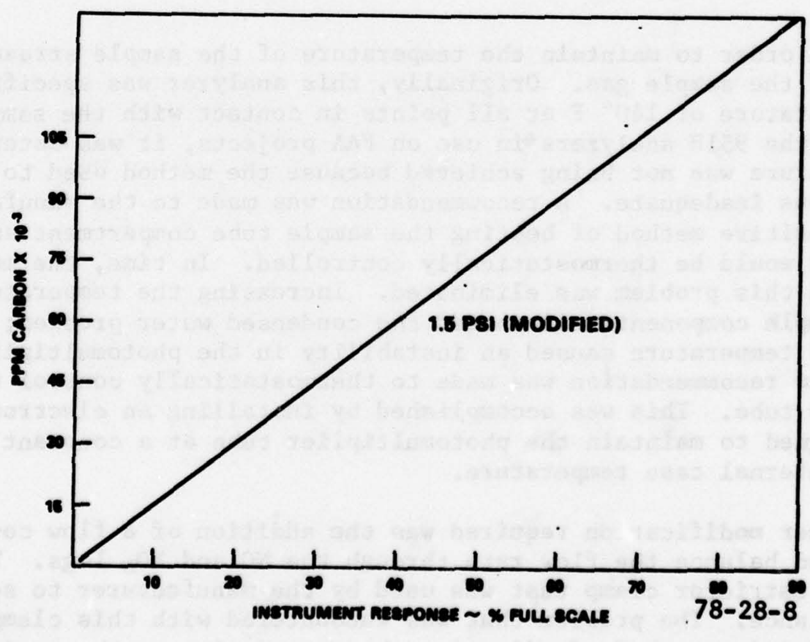


FIGURE 7. BECKMAN MODEL 402 THC ANALYZER (1.5 PSI MODIFIED)

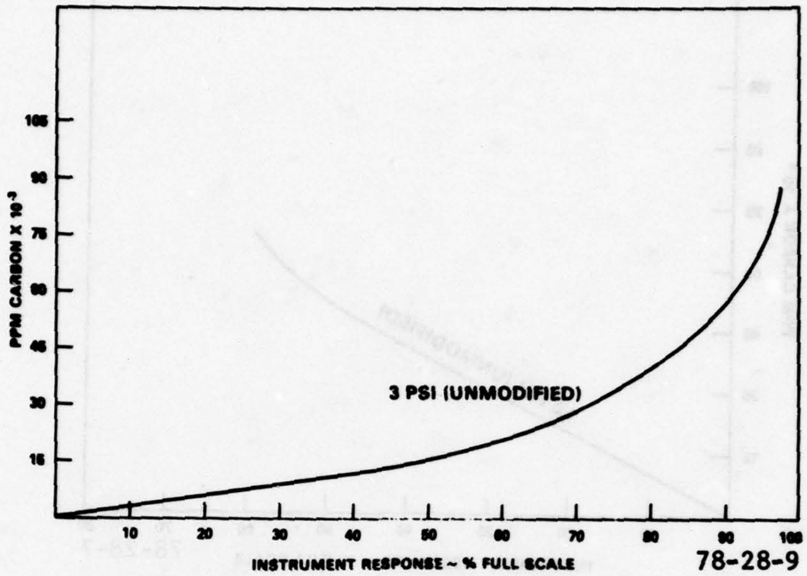


FIGURE 8. BECKMAN MODEL 402 THC ANALYZER (3 PSI UNMODIFIED)

installed in order to maintain the temperature of the sample stream above the dew point of the sample gas. Originally, this analyzer was specified to maintain a temperature of 140° F at all points in contact with the sample. After a survey of the 951H analyzers in use on FAA projects, it was determined that this temperature was not being achieved because the method used to heat the components was inadequate. A recommendation was made to the manufacturer to install a positive method of heating the sample tube compartment and reaction chamber that would be thermostatically controlled. In time, the modification was made and this problem was eliminated. Increasing the temperature of the internal sample components eliminated the condensed water problem; however, the elevated temperature caused an instability in the photomultiplier tube output. Another recommendation was made to thermostatically control the temperature of this tube. This was accomplished by installing an electronic cooling jacket designed to maintain the photomultiplier tube at a constant temperature below the internal case temperature.

A further modification required was the addition of a flow control value to adjust and balance the flow rate through the NO and NO_x legs. This value replaced a restrictor clamp that was used by the manufacturer to set the NO to NO_x flow balance. The problem that was encountered with this clamp was that it was not a positive method of adjusting the restriction on the capillary. The clamp compression was affected by the flexible material on which the clamp was mounted and the variable flexibility of the Teflon® capillary as it was heated. This caused the restriction on the capillary to change with time and caused permanent deformation of the capillary, allowing only an adjustment that would increase the restriction.

Oxygen Measurement. Oxygen (O_2) was measured by a Beckman model OM-11 oxygen analyzer. This analyzer uses a polagraphic-type sensor unit to measure oxygen concentration. An advanced sensor and amplification system combine to give an extremely fast response and high accuracy. Specified response for 90 percent of final reading is less than 200 milliseconds (ms) with an accuracy of less than $\pm$0.1-percent O_2. The range of this unit is a fixed 0 to 100 percent O_2 concentration.

EMISSIONS INSTRUMENTATION MODIFICATION STATUS DURING THE TESTING OF THE IO-360-B1BD ENGINE.

The tests conducted with the Avco Lycoming to IO-360-B1BD engine utilized the model 742 oxygen (O_2) analyzer and a prototype Beckman model 951H oxides of nitrogen (NO_x) analyzer.

The model 742 oxygen (O_2) analyzer did not have the extremely fast response rate of the Beckman model OM-11 analyzer, and it was not as accurate. The data recorded with this analyzer reflect these deficiencies.

DESCRIPTION OF SAMPLE HANDLING SYSTEM.

Exhaust samples are transported to the analysis instrumentation under pressure through a 35-foot-long, 3/8-inch o.d., heated, stainless steel sample line. The gas is first filtered and then pumped through this line by a heated Metal Bellows model MB-158 high temperature stainless steel sample pump. The pump, filter, and line are maintained at a temperature of 300° $\pm$4° F to prevent condensation of water vapor and hydrocarbons. At the instrument console, the sample is split to feed the hydrocarbon, oxides of nitrogen, and $CO/CO_2/O_2$ subsystems which require different temperature conditioning. The sample gas to the total hydrocarbon subsystem is maintained at 300° F, while the temperature of remaining sample gas to the NO_x and $CO/CO_2/O_2$ system is allowed to drop to 150° F. Gas routed to the oxides of nitrogen subsystem is then maintained at 150° F, while the gas to the $CO/CO_2/O_2$ subsystem is passed through a 32° F condenser to remove any water vapor present in the sample. Flow rates to each analyzer are controlled by a fine-metering value and are maintained at predetermined values to minimize sample transport and system response time. Flow is monitored at the exhaust of each analyzer by three 15-centimeter (cm) rotameters. Two bypasses are incorporated into the system to keep sample transport time through the lines and condenser to a minimum without causing adverse pressure effects in the analyzers.

DESCRIPTION OF FILTRATION SYSTEM.

Particulates are removed from the sample at three locations in the system, thereby minimizing downtime due to contaminated sample lines and analyzers (figure 5). Upstream of the main sample pump is a heated clamshell-type stainless steel filter body fitted with a Whatman GF/C glass fibre paper filter element capable of retaining particles in the 0.1-micron range. A similar filter is located in the total hydrocarbon analyzer upstream of the sample capillary. A Mine Safety Appliances (MSA) type H Ultra Filter capable of retaining 0.3-micron particles is located at the inlet to the oxides of nitrogen and $CO/CO_2/O_2$ subsystem.

COMPUTATION PROCEDURES.

The calculations required to convert exhaust emission measurements into mass emissions are the subject of this section.

Exhaust emission tests were designed to measure CO_2, CO, unburned hydrocarbons (HC), NO_x, and exhaust excess O_2 concentrations in percent or ppm by volume. Mass emissions were determined through calculations utilizing the data obtained during the simulation of the aircraft LTO cycle and from modal lean-out data.

COMBUSTION EQUATION. The basic combustion equation can be expressed very simply:

Fuel + Air = Exhaust Constituents

An initial examination of the problem requires the following simplifying assumptions:

1. The fuel consists solely of compounds of carbon and hydrogen.

2. The air is a mixture of oxygen and inert nitrogen in the volumetric ratio of 3.764 parts apparent nitrogen to 1.0-part oxygen (see appendix B for additional details).

3. If a stoichiometric combustion process exists, the fuel and air are supplied in chemically correct proportions.

4. The fuel (which consists usually of a complex mixture of hydrocarbons) can be represented by a single hydrocarbon having the same carbon-hydrogen ratio and molecular weight as the fuel; usually C_8H_{17} as an average fuel.

Applying the above assumptions for stoichiometric conditions, a useful general reaction equation for hydrocarbon fuel is:

$$M_f C_8H_{17} + M_a \left[O_2 + 3.764 N_2 + M_w H_2O\right] \rightarrow M_1 CO_2 + M_3 H_2O + M_5 N_2 \qquad (1)$$

(references 3 and 4)

Where
- M_f = Moles of Fuel
- M_a = Moles of Air or Oxygen
- M_1 = Moles of Carbon Dioxide (CO_2)
- M_3 = Moles of Condensed Water (H_2O)
- M_5 = Moles of Nitrogen (N_2)--Exhaust
- $3.764M_a$ = Moles of Nitrogen (N_2)--In Air
- M_aM_w = Moles of Humidity (H_2O)--In Air

The above equation is applicable to dry air when M_w is equal to zero.

From equation (1), and assuming dry air with one mole of fuel (M_f=1.0), the stoichiometric fuel-air ratio may be expressed as:

$$(F/A)_s = \frac{\text{Wt. Fuel}}{\text{Wt. Air Required}} = \frac{12.011\ (8) + 1.008\ (17)}{12.25\ [32.000 + 3.764(28.161)]} \qquad (2)$$

$$(F/A)_s = \frac{113.224}{12.25(137.998)} = 0.067$$

The mass carbon-hydrogen ratio of the fuel may be expressed as follows:

$$C/H = \frac{12.011(8)}{1.008(17)} = \frac{96.088}{17.136} = 5.607 \qquad (3)$$

The atomic hydrogen-carbon ratio is

$$17/8 = 2.125 \qquad (4)$$

The stoichiometric fuel-air ratio may be expressed as a function of the mass hydrogen-carbon ratio of the fuel. The derivation of this equation is presented in reference 3.

$$(F/A)_s = \frac{C/H + 1}{11.5(C/H+3)} \qquad (5)$$

$(F/A)_s$ = 0.067 for a mass hydrogen-carbon ratio of 5.607

With rich (excess fuel) mixtures, which are typical for general aviation piston engines, some of the chemical energy will not be liberated because there is not enough air to permit complete oxidation of the fuel. Combustion under such conditions is an involved process. By making certain simplifying assumptions based on test results, the effect of rich mixtures may be calculated with reasonable accuracy.

For rich (excess fuel) mixtures, equation (1) will now be rewritten to express the effects of incomplete combustion:

$$M_fC_8H_{17} + M_a\ (O_2 + 3.764N_2 + M_wH_2O) \longrightarrow M_1CO_2 + M_2CO + M_3H_2O + M_4H_2 + M_5N_2 + M_6NO + M_7CH_4 + M_8O_2 + M_9C \qquad (6)$$

Since only a limited number of the exhaust constituents were measured during the testing of general aviation piston engines, the above equation can only be solved by applying certain expeditious assumptions and imperical data.

An important requirement of the FAA/NAFEC General Aviation Piston Engine Emissions Test Program was the accurate measurement of air and fuel flows. These parameters provide the data for determining engine mass flow (W_m) and with the aid of figure 9 (developed from reference 5) it is a simple computation to calculate the total moles (M_{tp}) of exhaust products being expelled by general aviation piston engines.

$$(M_{tp}) = W_m \text{ (engine mass flow)} \div \text{(exh. mol. wt)} \qquad (7)$$

Since the unburned hydrocarbons (HC) and oxides of nitrogen (NO_x) are measured wet, it becomes a very simple matter to compute the moles of HC and NO_x that are produced by light-aircraft piston engines.

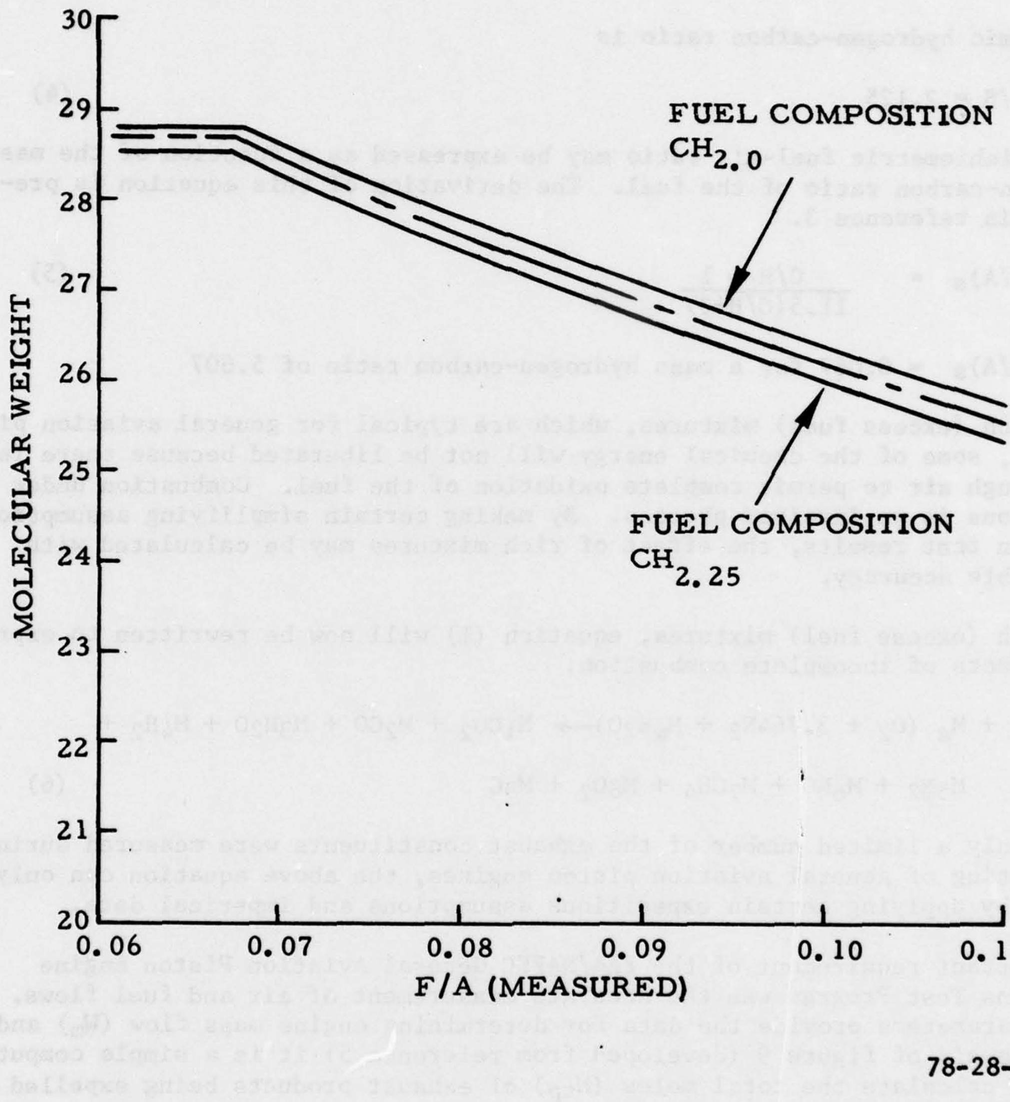


FIGURE 9. EXHAUST GAS MOLECULAR WEIGHTS

M_7 (Moles of HC) $= (\text{ppm} \div 10^6) \times M_{tp}$ (8)

M_6 (Moles of NO_x $= (\text{ppm} \div 10^6) \times M_{tp}$ (9)

If the dry products (M_{dp}) of combustion are separated from the total exhaust products (M_{tp}) it is possible to develop a partial solution for five of the products specified in equation 6.

This can be accomplished as follows:

The summation of the mole fractions $(MF)_d$ for dry products is:

$m_1 + m_2 + m_4 + m_5 + m_8 = 1.0000$ (10)

$m_1 = MF(CO_2) = \%CO_2$ (measured dry), expressed as a fraction

$m_2 = MF(CO) = \%CO$ (measured dry), expressed as a fraction

$m_4 = MF(H_2) = K_4\ (\%CO)$ (see figure 10, also references 4, 5, and 6), expressed as a fraction

$m_8 = MF(O_2) = \%O_2$ (measured dry), expressed as a fraction

$m_5 = 1.0000 - (m_1 + m_2 + m_4 + m_8) = \%N_2$ (dry), expressed as a fraction (11)

Utilizing the nitrogen balance equation, it is now possible to determine the moles of nitrogen that are being exhausted from the engine.

$M_5 = 3.764\ M_a - (M_6 \div 2);\ M_6 = \text{moles (NO)}$ (12)

The moles of exhaust dry products (M_{dp}) may now be determined by dividing equation 12 by equation 11.

$M_{dp} = M5 \div m_5$ (13)

Using all the information available from equations (7), (8), (9), (10), (11), (12), and (13), it is now possible to determine the molar quantities for seven exhaust products specified in equation 6.

Moles $(CO_2) = M_1 = m_1 \times M_{dp}$ (14)

Moles $(CO) = M_2 = m_2 \times M_{dp}$ (15)

Moles $(H_2) = M_4 = m_4 \times M_{dp}$ (16)

Moles $(N_2) = M_5 = m_5 \times M_{dp}$ (17)

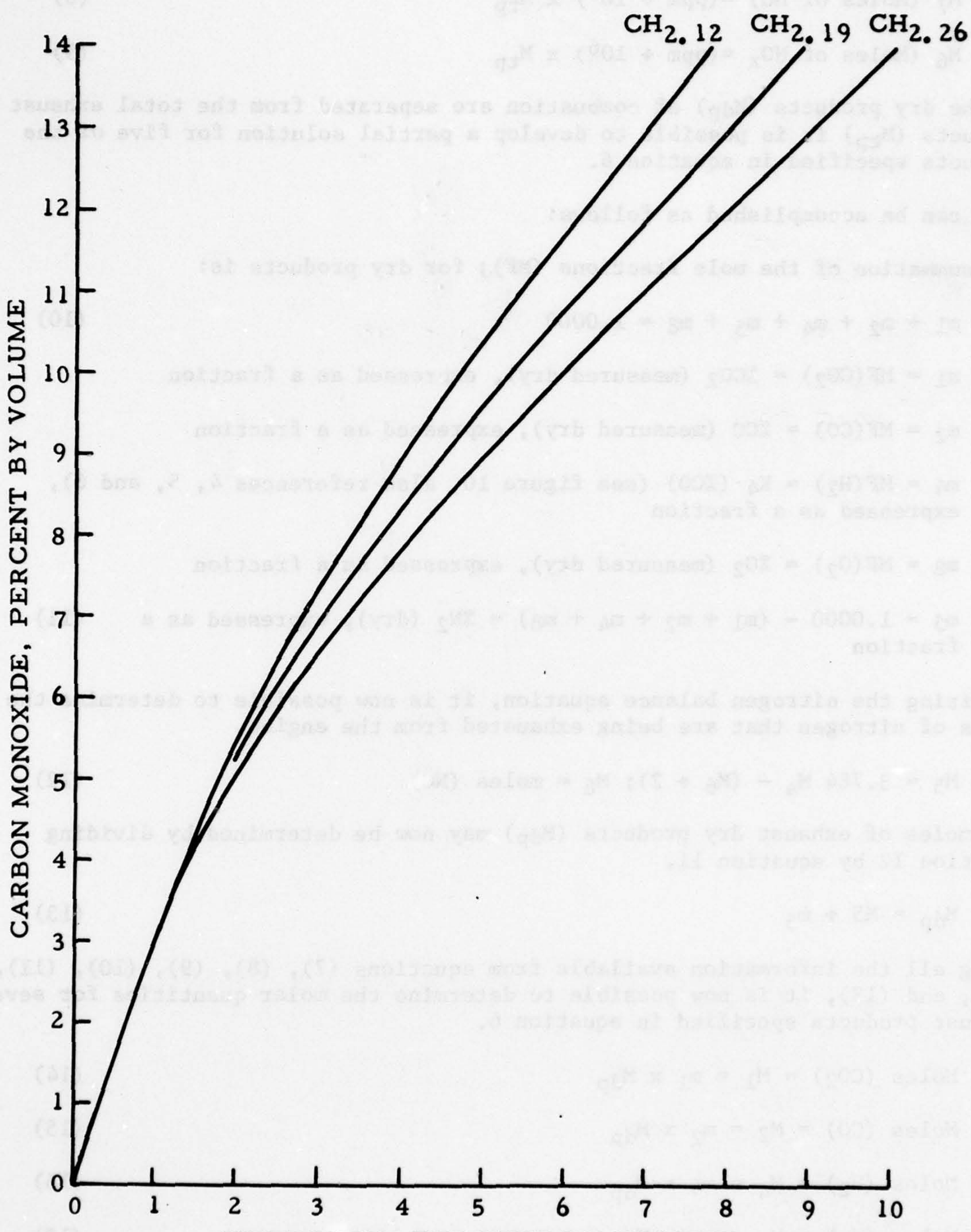


FIGURE 10. RELATION OF CARBON MONOXIDE AND HYDROGEN

$\text{Moles } (O_2) = M_8 = m_8 \times M_{dp}$ (18)

$\text{Moles } (CH_4) = M_7 = (\text{ppm} \div 10^6) \times M_{tp}$ (19)

$\text{Moles } (NO) = M_6 = (\text{ppm} \div 10^6) \times M_{tp}$ (20)

To determine M_3 (Moles of condensed H_2O), it is now appropriate to apply the oxygen balance equation.

$M_3 = M_a\ (2 + M_w) - (2M_1 + M_2 + M_6 + 2M_8) = \text{Moles } (H_2O)$ (21)

The remaining constituent specified in equation 6 may now be determined from the carbon balance equation 22.

$M_9 = 8M_f - (M_1 + M_2 + M_7)$ (22)

A check for the total number of exhaust moles (M_{tp}), calculated from equation 9 may now be determined from equation 23.

$M_{tp} = M_1 + M_2 + M_3 + M_4 + M_5 + M_6 + M_7 + M_8 + M_9$ (23)

$\dot{m}_1 + \dot{m}_2 + \dot{m}_3 + \dot{m}_4 + \dot{m}_5 + \dot{m}_6 + \dot{m}_7 + \dot{m}_8 + \dot{m}_9 = 1.0000$ (24)

$\dot{m}_1 = MF(CO_2) = M_1 \div M_{tp}$

$\dot{m}_2 = MF(CO) = M_2 \div M_{tp}$

$\dot{m}_3 = MF(H_2O) = M_3 \div M_{tp}$

$\dot{m}_4 = MF(H_2) = M_4 \div M_{tp}$

$\dot{m}_5 = MF(N_2) = M_5 \div M_{tp}$

$\dot{m}_6 = MF(NO) = M_6 \div M_{tp}$

$\dot{m}_7 = MF(CH_4) = M_7 \div M_{tp}$

$\dot{m}_8 = MF(O_2) = M_8 \div M_{tp}$

$\dot{m}_9 = MF(C) = M_9 \div M_{tp}$

The exhaust constituent mass flow rates may be computed in the following manner using each exhaust constituents molar constant with the appropriate molecular weight.

$M_1 \times 44.011 = CO_2 \text{ in lb/h}$ (25)

$M_2 \times 28.011 = CO \text{ in lb/h}$ (26)

$M_3 \times 18.016 = H_2O$ in lb/h (27)

$M_4 \times 2.016 = H_2$ in lb/h (28)

$M_5 \times 28.161 = N_2$ in lb/h (29)

$M_6 \times 30.008 = NO$ in lb/h (30)

$M_7 \times 16.043 = CH_4$ in lb/h (31)

$M_8 \times 32.000 = O_2$ in lb/h (32)

$M_9 \times 12.011 = C$ in lb/h (33)

The exhaust fuel flow (W_{fe}), base on exhaust constituents, can now be calculated on a constituent by constituents basis as follows:

$(M_1 + M_2 + M_9) \times 12.011 = lb/h$ (34)

$M_7 \times 16.043 = lb/h$ (35)

$[(M_3 - M_aM_w) + M_4 + 2.016] = lb/h$ (36)

$W_{fe} = (34) + (35) + (36) = lb/h$ (37)

In a similar manner the exhaust airflow (W_{ae}) can also be calculated on a constituent by constituent basis:

$M_1 \times 32.000$ lb/h (38)

$M_2 \times 16.000 = lb/h$ (39)

$(M_3 \times 16.000) + (M_aM_w \times 18.016) = lb/h$ (40)

$M_5 \times 28.161 = lb/h$ (41)

$M_6 \times 30.008 = lb/h$ (42)

$M_8 \times 32.000 = lb/h$ (43)

$W_{ae} = (38) \rightarrow (43) = lb/h$ (44)

Using equations (37) and (44) it is now possible to determine a calculated fuel-air ratio on the basis of total exhaust constituents.

$(F/A)_{calculated} = (37) \div (44)$ (45)

RESULTS

GENERAL COMMENTS.

General aviation piston engine emission tests were conducted to provide the following categories of data:

1. Full-rich (or production fuel schedule) baseline data for each power mode specified in the LTO test cycle.

2. Lean-out data for each power mode specified in the LTO test cycle.

3. Data for the above categories at different spark settings.

4. Data for each power mode specified in the LTO test cycle utilizing different quantities of cooling air.

RESULTS OF BASELINE TESTS (LANDING-TAKEOFF CYCLE EFFECTS).

Based on an analysis of the factors affecting piston engine emissions, it can be shown that the mode conditions having the greatest influence on the gross pollutant levels produced by the combustion process are taxi, approach, and climb when using the LTO cycle defined in tables 3, 4, and 5. The five-mode LTO cycle shows that approximately 99 percent of the total cycle time (27.3 min) is attributed to these three modal conditions. Furthermore, the taxi modes (both out and in) account for slightly less than 59 percent of the total cycle time. The remainder of the time is almost equally apportioned to the approach and climb modes (22 and 18 percent, respectively).

As a result of these time apportionments, it was decided that an investigation and evaluation of the data should be undertaken to determine which mode(s) has the greatest influence on improving general aviation piston engine emissions. The subsequent sections of this report will show the exhaust emissions characteristics for an Avco Lycoming IO-360-B1BD engine (S/N 887-X) and what improvements are technically feasible within the limits of safe aircraft/engine operational requirements based on sea level propeller test stand evaluations conducted at NAFEC.

The first set of data to be presented and evaluated is the five-mode baseline runs conducted to establish the current production full-rich exhaust emissions characteristics of the IO-360-B1BD engine. These are summarized in tabular form in appendix C (see tables C-1 through C-16) and includes data that were obtained for a range of sea level, ambient conditions specified as follows:

Induction air temperature (T_i) = 50° F to 110° F
Cooling air temperature (T_c) = T_i ±10° F
Induction air pressure (P_i) = 29.20 to 30.50 inHgA
Induction air density (ρ) = 0.0690 to 0.0795 lb/ft^3

Figure 11 presents five-mode baseline data in bargraph form (for different sea level ambient conditions). It also compares the total emissions characteristics of the IO-360-B1BD engine (current production configuration) with the proposed EPA standards as a function of percent of standard. The data that were utilized to develop figure 11 are tabulated in appendix C and plotted in various forms for analysis and evaluation in figures C-1 through C-19. Tables C-14 and C-15 provide the data tabulation that was used to construct the bargraphs for T_i = 60° F and T_i = 103° F.

RESULTS OF LEAN-OUT TESTS.

In the subsequent sections of this report it will be shown what improvements can be achieved as a result of making lean-out adjustments to the fuel metering device: (1) taxi mode only, (2) taxi and approach modes combined, and (3) leaning-out the climb mode to "best power" in combination with taxi and approach mode leaning.

EFFECTS OF LEANING-OUT ON CO EMISSIONS. The test data obtained as a result of NAFEC testing the Avco Lycoming IO-360 B1BD have been evaluated on the basis of leaning-out the taxi, approach, and climb modes while continuing the operation of the test engine at the production rich and lean limits in the takeoff mode. The results of leaning-out under this procedure are shown in bargraph form in figure 12.

When the taxi modes (out and in) were leaned-out from the production rich or lean limits to a fuel-air ratio of 0.075 or lower, but not lower than stoichiometric (F/A = 0.067) (see figure 12), CO emissions were reduced approximately 20 percent. However, adjustments to the taxi mode fuel schedule alone are not sufficient to bring the total five-mode LTO cycle CO emission level below the proposed federal standard.

Simultaneously, leaning-out both the taxi and approach modes to fuel-air ratios between 0.067 to 0.075 will result in additional improvements in CO emissions. In the case of operating the engine at production rich limits for takeoff and climb while operating taxi and approach at F/A = 0.075, the total five-mode LTO cycle CO emission level will be reduced approximately 60 percent as shown in figure 12.

Additional improvements in the total five-mode LTO cycle for CO emissions can be achieved, as shown in figure 12, if the engine as adjusted to operate at "best power" fuel-air ratios in the climb mode while operating the approach and taxi modes at F/A = 0.075 or lower (not lower than fuel-air ratio = 0.067).

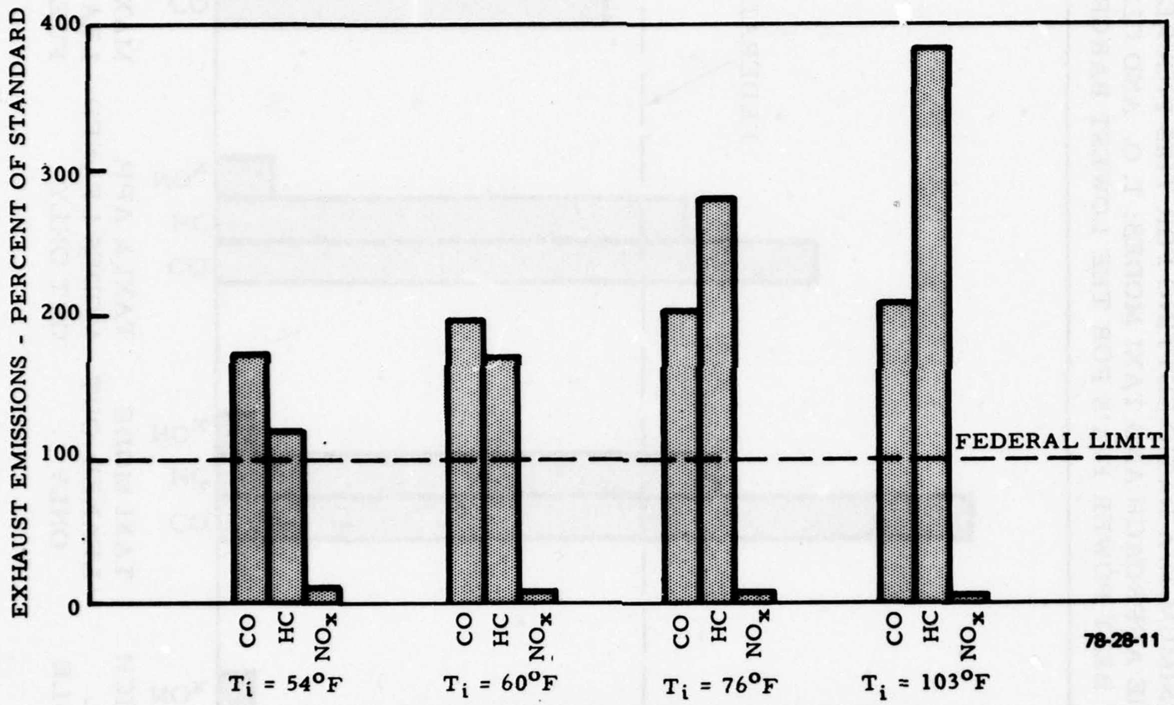


FIGURE 11. AVERAGE TOTAL EMISSIONS CHARACTERISTICS FOR AN AVCO LYCOMING IO-360-B1BD ENGINE OPERATING UNDER VARYING SEA LEVEL INDUCTION AIR TEMPERATURES--TABLE 5 MINIMUM FIVE-MODE LTO CYCLE

NOTE:

1. THIS FIGURE IS BASED ON THE TABLE 5 LTO CYCLE WITH THE CLIMB MODE AT APPROXIMATELY 75 PERCENT POWER.

2. THE MINIMUM F/A RATIO SETTING FOR THIS FIGURE IS 0.075 FOR THE APPROACH AND TAXI MODES; T. O. AND CLIMB WERE SET AT BEST POWER F/A'S FOR THE LOWEST BARGRAPH.

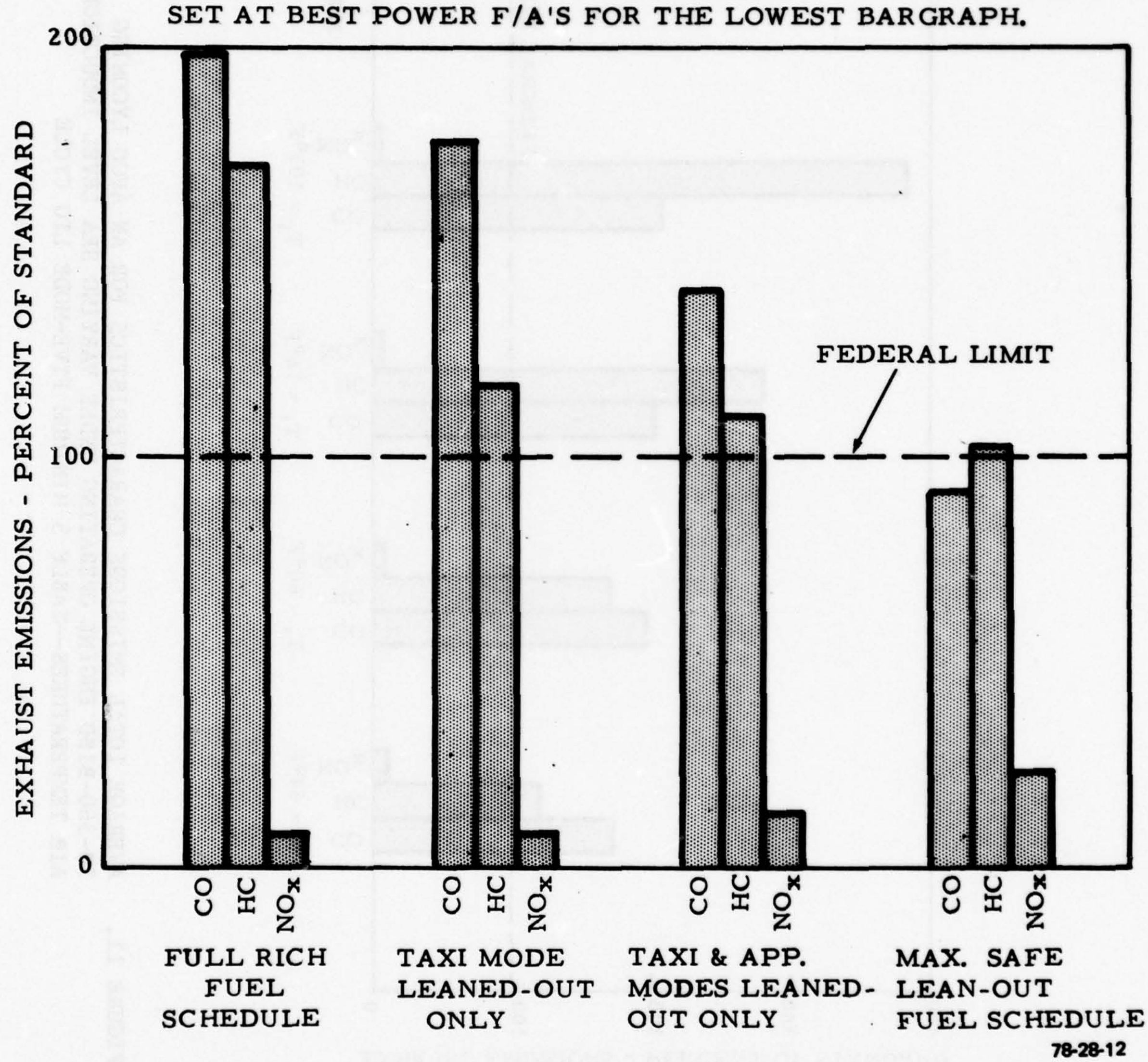


FIGURE 12. TOTAL EMISSIONS CHARACTERISTICS FOR AN AVCO LYCOMING IO-360-B1BD ENGINE WITH DIFFERENT FUEL SCHEDULE ADJUSTMENTS--SEA LEVEL STANDARD DAY

The preceeding evaluation of CO emissions characteristics was based on the LTO cycle defined by table 5. However, the EPA five-mode LTO cycle defined by table 2 implies that the climb mode power levels can range from 75 to 100 percent. The exhaust emissions produced will be drastically affected. Examination of the measured data produced at NAFEC show that there is a significant difference in each engine's total LTO cycle emissions output when climbing at 100-percent power compared to climbing at 75-percent power. This data evaluation also show that whereas a CO limit of 0.042 pounds per cycle per rated brake horsepower may be achievable as described previously by using the LTO cycle defined by table 5; it is not achieveable using an LTO cycle defined by table 4. When one considers the following safety considerations: (1) sea level, hot-day takeoff requirements with an aircraft at heavy gross weight and (2) altitude hot-day takeoff requirements with an aircraft at heavy gross weight, it would appear that the EPA 0.042 limit for CO is not realistic and cannot be complied with, unless engine operational and safety limits are totally ignored.

Table 6 provides a summary of the NAFEC data which indicate what levels of improvement in CO emissions can be achieved by applying simple fuel management techniques (leaning-out by mixture control manipulations), albeit with drastically reduced margins between actual measured maximum cylinder head temperature (CHT) and the maximum CHT limit.

Example: Consider the engine installed in a sea level propeller stand and operating with cooling air at a $\Delta P = 3.0$ inH_2O and the following critical test conditions:

1. Ambient conditions (pressure, temperature, and density)--sea level standard day
2. Fuel schedule--production rich setting
3. Power setting--100%
4. Measure max. CHT--435° F
5. Max. CHT limit--500° F
6. Margin-- (5) minus (4) --65° F

If this engine fuel schedule setting is adjusted to best power (all other parameters constant based on above conditions), the following changes take place:

1. CO emissions are improved by 105% (nominal)
2. Measured max. CHT increases 9.2% (from 435° F to 475° F)
3. Max. CHT -- 500° F
4. Margin -- (3) minus (2) = 25° F
5. Reduction in margin (max CHT) -- (40 ÷ 65) x 100 = 61.5%

TABLE 6. SUMMARY OF EXHAUST EMISSIONS (CO) REDUCTION POSSIBILITIES FOR AN AVCO LYCOMING IO-360-B1BD ENGINE--SEA LEVEL STANDARD DAY (EXCEPT AS NOTED)--COOLING AIR $\Delta P = 3.0$ inH_2O

	Modes	F/A	CO lb/Mode	Max. CHT-°F	F/A	CO lb/Mode	Max. CHT-°F	Max. CHT-°F	Max. Limit CHT-°F
1	Taxi	0.0925	2.400	-	0.0750	1.067	-	-	-
2	Takeoff (100%)	0.0990	0.640	435	0.0850	0.425	475	495	500
3	Climb (100%)	0.0990	10.667	435	0.0850	7.083	475	495	500
4	Approach	0.0925	5.000	335	0.0750	2.250	350	375	500
5	lb/Cycle		18.707			10.825			
6	lb/Cycle/RBHP		0.104			0.060			
7	Federal Limit		0.042			0.042			
8	Diff. = 6 - 7		+.062			+.018			
9	(8 + 7)x100		147.6			42.9			
10	% of STD = 9 +100		247.6			142.9			
				This Column For SL. Standard Day			This Column For SL. Standard Day	This Column For SL. Hot Day	
11	Taxi	0.0925	2.400	-	0.0750	1.067	-	-	-
12	Takeoff (100%)	0.0990	0.640	435	0.0850	0.425	475	475	500
13	Climb (75%)	0.0925	6.667	420	0.0825	4.500	435	450	500
14	Approach	0.0925	5.000	335	0.0750	2.250	350	375	500
15	lb/Cycle		14.707			8.242			
16	lb/Cycle/RBHP		0.082			0.046			
17	Federal Limit		0.042			0.042			
18	Diff. = (16) - (17)		+.040			+.004			
19	((18) + (17))x100		95.2			9.5			
20	% of STD = (19) +100		195.2			109.5			

Now, if we apply the above results to a sea level hot-day condition, we arrive at the following results:

Production Rich Limit Schedule (100% power)

1. Ambient conditions--sea level hot day
2. Fuel schedule--production rich setting
3. Power setting--100% (nominal)
4. Measured max. CHT--445° F
5. Max. CHT limit--500° F
6. Margin--(5) minus (4) = 55° F

Best Power Fuel Schedule (100% Power)

1. Ambient conditions--sea level hot day
2. Fuel schedule--best power fuel schedule
3. Power setting--100% (nominal)
4. Measured max. CHT--495° F
5. Max. CHT limit--500° F
6. Margin--(5) minus (4) = 5° F
7. Reduction in margin (max. CHT)--(50 ÷ 55) x 100 = 90.9%

EFFECTS OF LEANING-OUT ON HC EMISSIONS. The test data show that the Lycoming engine can be leaned-out sufficiently in the taxi mode to bring the unburned hydrocarbon emissions below the federal standard (figure 12). Additional leaning-out in the approach and climb modes provides added improvements, but is not required to produce HC emission levels below the federal standard. The taxi-out mode data from this engine were not influenced by procedural effects such as clearing-out prior to conducting tests. Therefore, this engine exhibits somewhat higher hydrocarbon levels than other naturally aspirated engines in the same power/size category.

EFFECTS ON NO_x EMISSIONS. Oxides of nitrogen emissions are not improved as a result of applying lean-out adjustments to the fuel metering devices. In fact, the NO_x levels are at their lowest when the engine is operating full rich as shown in figure 11. Test results have shown that if all the test modes (take-off, climb, approach, and taxi) were leaned-out excessively (F/A = 0.067), the NO_x emission level would exceed the federal standard.

The negative effect on NO_x emissions is one of the reasons why it was decided to evaluate and study the effects of adjusting/manipulating selected mode conditions rather than adopt the philosophy of adjusting all modes.

EFFECTS ON ALLOWABLE MAXIMUM CYLINDER HEAD TEMPERATURE. One of the major problems that occurs as an effect of leaning-out general aviation piston engines in order to improve emissions is the increase or rise in maximum cylinder head temperatures.

Most general aviation aircraft are designed to operate with cooling air pressure differentials of 4.0 inH_2O or less. The tests conducted with the Avco Lycoming engine utilized 3.0 inH_2O as the basic cooling flow condition.

Additional tests were conducted using variations in cooling air flow to evaluate these effects on different lean-out schedules. Some of the tests were also conducted under different ambient conditions so that changes in ambient conditions could also be evaluated.

Data shown in tables C-1 through C-15 and plotted in figures 13 through 15 show the results of these tests.

In summary, it can be concluded that any attempts to lean-out current production type horizontally opposed general aviation piston engines in the takeoff mode to F/A ratios lower than production lean limits will produce CHT's that are higher than the manufacturer's specified limit.

Any attempt to lean-out the climb mode to F/A ratios below best power will result in higher than normal CHT's. This could become particularly acute under hot-day takeoff and climb conditions at sea level or altitude.

RESULTS OF TESTS WITH VARYING SPARK SETTINGS.

This engine was also evaluated with different spark settings. The basic production setting is 25° before top dead center (BTC.) Two other settings were evaluated: 20° BTC and 15° BTC. Table 7 summarizes the results of all the tests conducted and presents the data on an average-of-three runs basis. The three basic power modes (takeoff, climb, and approach--100, 75-80, and 40 percent, respectively) are tabulated using average data based on three test runs for each power mode condition and each spark setting.

The percent changes in emission output are shown in table 7. For a change in the spark setting from 25° BTC to 20° BTC it may be noted that the CO increases 0.3 to 5 percent in the takeoff and climb modes for a 5-percent reduction in power and a nominal 3.85-percent reduction in maximum CHT. Even though the percent changes in unburned HC and NO_x appear to be significant, it should be noted that both of these pollutants are being measured on a fraction of a percent basis. Changing the spark setting from 25° BTC to 15° BTC shows that the CO emissions increase (0.8 to 1.6 for takeoff and climb, respectively) with a nominal 14.5-percent reduction in power and a 7.7-percent reduction in maximum CHT.

The data presented in table 7 and the plotted results in figures 16 through 21, for the various power conditions and spark setting indicate that the most optimum condition for the IO-360-B1BD engine is the 25° BTC spark setting if it is important not to compromise the available power at the significant modal conditions (takeoff, climb, and approach).

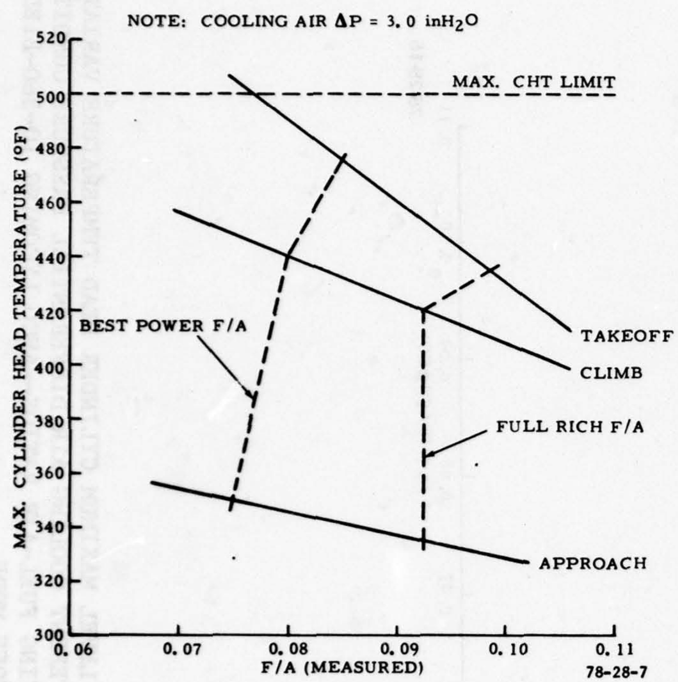


FIGURE 13. SEA LEVEL STANDARD DAY MAXIMUN CYLINDER HEAD TEMPERATURES FOR DIFFERENT POWER MODE CONDITIONS AND VARYING FUEL-AIR RATIOS--AVCO LYCOMING IO-360-B1BD ENGINE

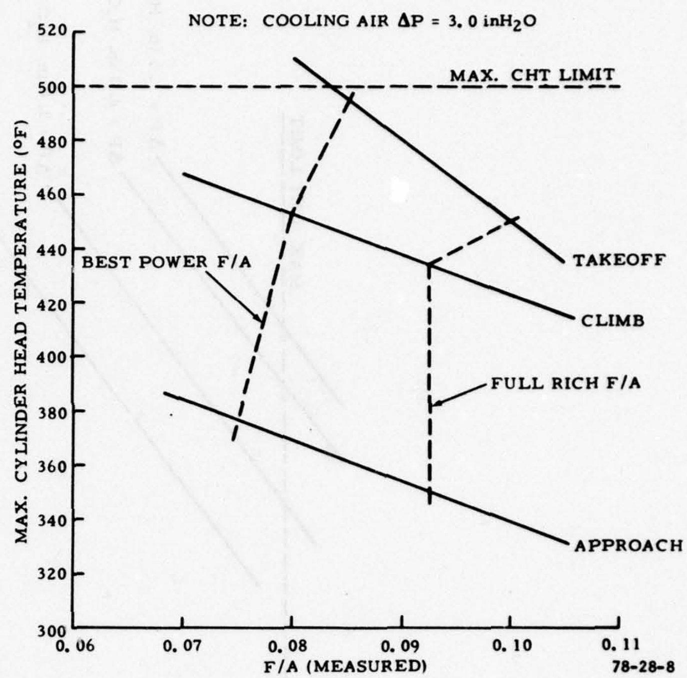


FIGURE 14. SEA LEVEL HOT DAY (T_1=103° F) MAXIMUM CYLINDER HEAD TEMPERATURE FOR DIFFERENT POWER MODE CONDITIONS AND VARYING FUEL-AIR RATIOS--AVCO LYCOMING IO-360-B1BD ENGINE

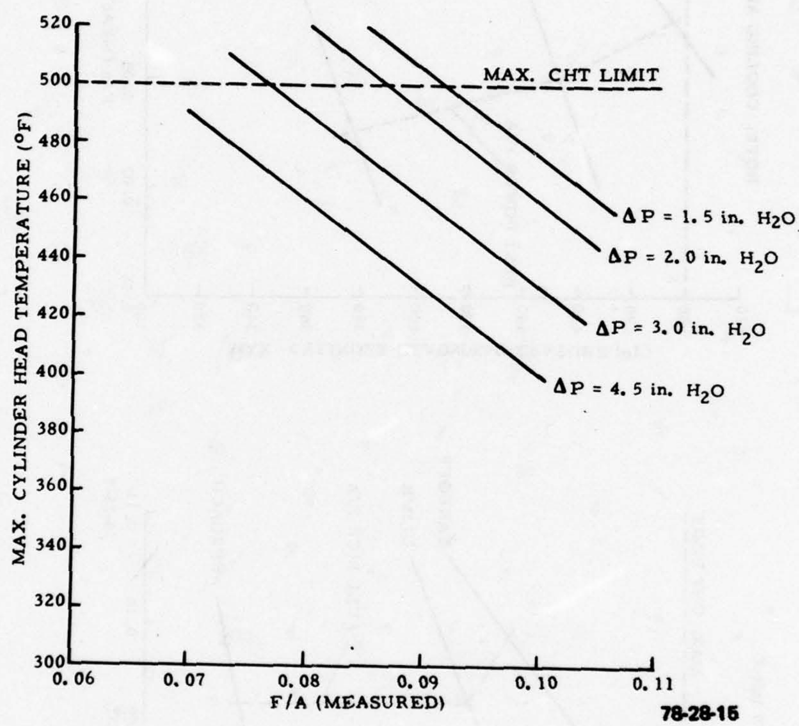


FIGURE 15. SEA LEVEL MAXIMUM CYLINDER HEAD TEMPERATURE VARIATIONS FOR DIFFERENT COOLING AIR DIFFERENTIAL PRESSURE CONDITIONS AND VARYING FUEL-AIR RATIOS--AVCO LYCOMING IO-360-B1BD ENGINE--TAKEOFF MODE

TABLE 7. SUMMARY OF ENGINE PERFORMANCE AND EXHAUST EMISSIONS CHARACTERISTICS FOR THREE DIFFERENT SPARK SETTINGS (°BTC—FULL-RICH FUEL SCHEDULE)

Mode Cond.	RPN	Torque lb-ft 25° BTC	HP 25° BTC	Ind. Air Temp. (°F)	W_f lb/h	Wa lb/h	F/A	$\%CO_2$	%CO	HC PPM	NO_x PPM	Max CHT (°F)	Run No.
Takeoff	2700	336	173	54	114.6	1179	0.0972	7.4	10.4	1900	127	438	3,16,30
Climb	2430	281	130	53	76.4	853	0.0896	8.3	8.8	1683	200	418	4,20,31
Approach	2350	142	64	53	42.2	486	0.0868	7.9	9.4	1858	113	336	5,24,32

Mode Cond.	RPN	Torque lb-ft 20° BTC	HP 20° BTC	Ind. Air Temp. (°F)	W_f lb/h	Wa lb/h	F/A	$\%CO_2$	%CO	HC PPM	NO_x PPM	Max CHT (°F)	Run No.
Takeoff	2700	319	164	56	115.3	1165	0.0990	7.2	10.7	1800	103	420	37,50,64
Climb	2430	267	124	56	77.0	843	0.0913	7.9	9.3	1542	140	403	38,54,65
Approach	2350	127	57	60	40.8	462	0.0883	8.1	9.1	1717	119	337	39,58,66

Mode Cond.	RPN	Torque lb-ft 15° BTC	HP 15° BTC	Ind. Air Temp. (°F)	W_f lb/h	Wa lb/h	F/A	$\%CO_2$	%CO	HC PPM	NO_x PPM	Max CHT (°F)	Run No.
Takeoff	2700	285	147	60	114.3	1179	0.0969	6.9	11.2	1617	77	405	71,84,98
Climb	2430	242	112	60	77.3	834	0.0927	7.5	10.4	1425	91	385	72,88,99
Approach	2350	108	48	62	40.2	449	0.0895	8.1	9.6	1567	93	334	73,92,100

Mode Cond.		ΔTorque lb-ft	ΔHP	ΔCHT(Max)	Nominal Ind. Air Temp. (°F)	%Δ HP	$\Delta\%CO_2$	Δ%CO	ΔHC(%)	ΔNO_x(%)	%Δ CHT(Max)
Takeoff	25°-20° BTC	-17	- 9	-18	55	- 5	-0.2	+0.3	- 5.26	-18.90	-4.11
Climb	25°-20° BTC	-14	- 6	-15	54.5	- 5	-0.4	+0.5	- 8.38	-30.00	-3.59
Approach	25°-20° BTC	-15	- 7	+ 1	56.5	- 11	+0.2	-0.3	- 7.59	+ 5.31	+0.30
Takeoff	25°-15° BTC	-51	-26	-33	57	-15	-0.5	+0.8	- 14.89	-39.37	-7.53
Climb	25°-15° BTC	-39	-18	-33	56.5	-14	-0.8	+1.6	- 15.33	-54.33	-7.89
Approach	25°-15° BTC	-34	-16	- 2	57.5	-25	+0.2	+0.2	- 15.66	-17.70	-0.60

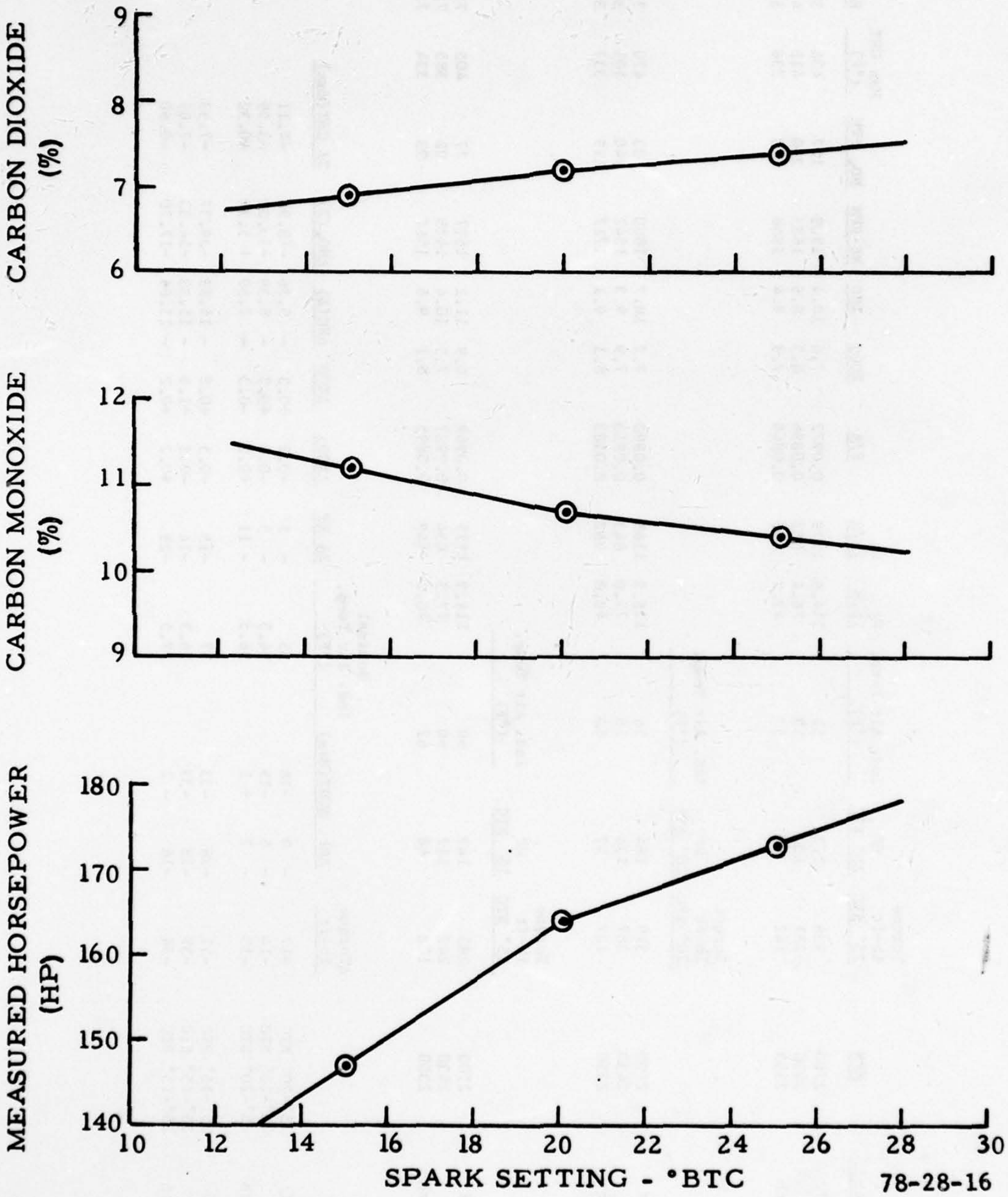


FIGURE 16. EFFECT OF VARYING SPARK SETTING ON ENGINE PERFORMANCE AND EXHAUST EMISSIONS--TAKEOFF MODE (CO_2 AND CO)

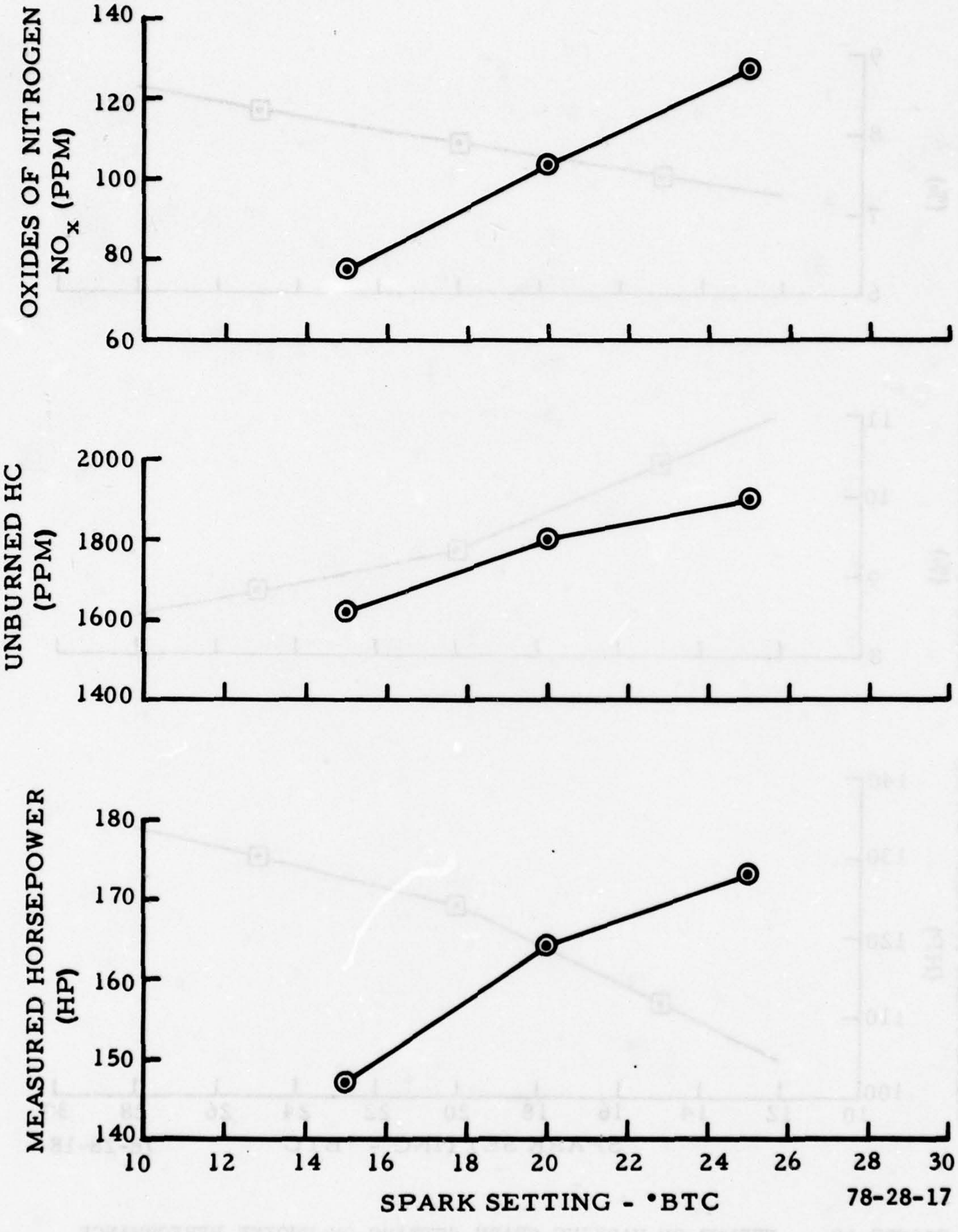


FIGURE 17. EFFECT OF VARYING SPARK SETTING ON ENGINE PERFORMANCE EXHAUST EMISSIONS--TAKEOFF MODE (HC AND NO_X)

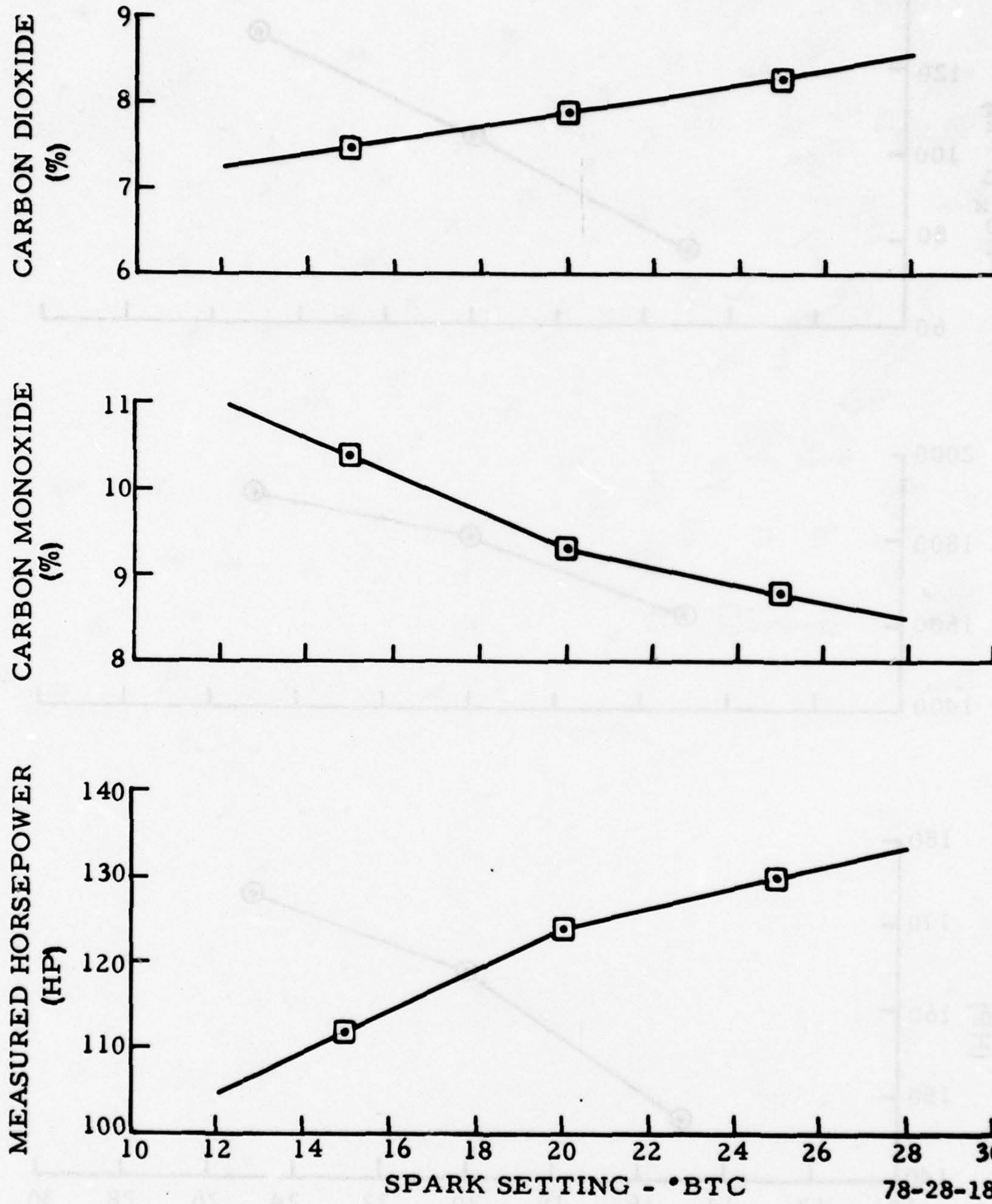


FIGURE 18. EFFECT OF VARYING SPARK SETTING ON ENGINE PERFORMANCE AND EXHAUST EMISSIONS--CLIMB MODE (CO_2 AND NO_X)

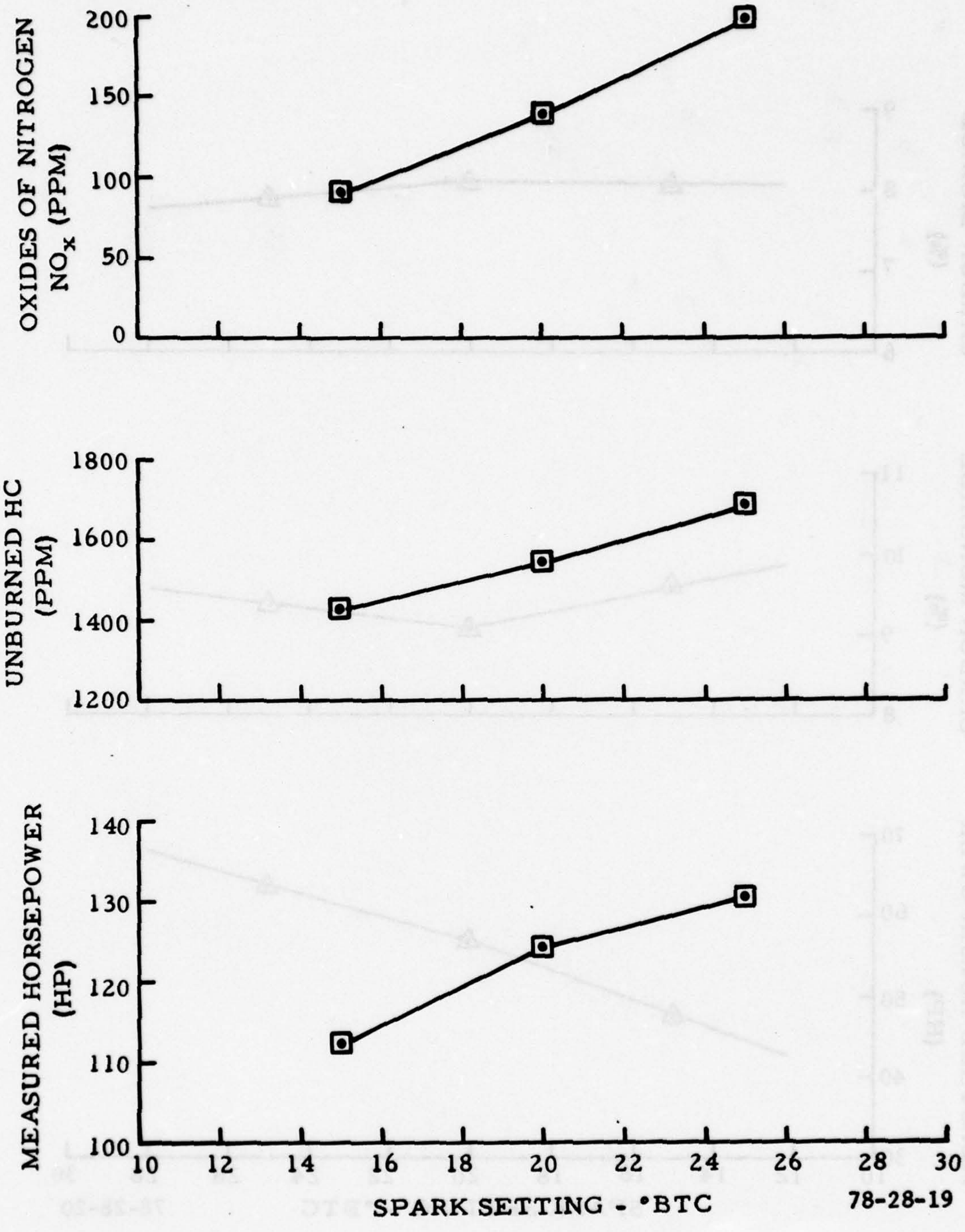


FIGURE 19. EFFECT OF VARYING SPARK SETTING ON ENGINE PERFORMANCE AND EXHAUST EMISSIONS--CLIMB MODE (HC AND NO_X)

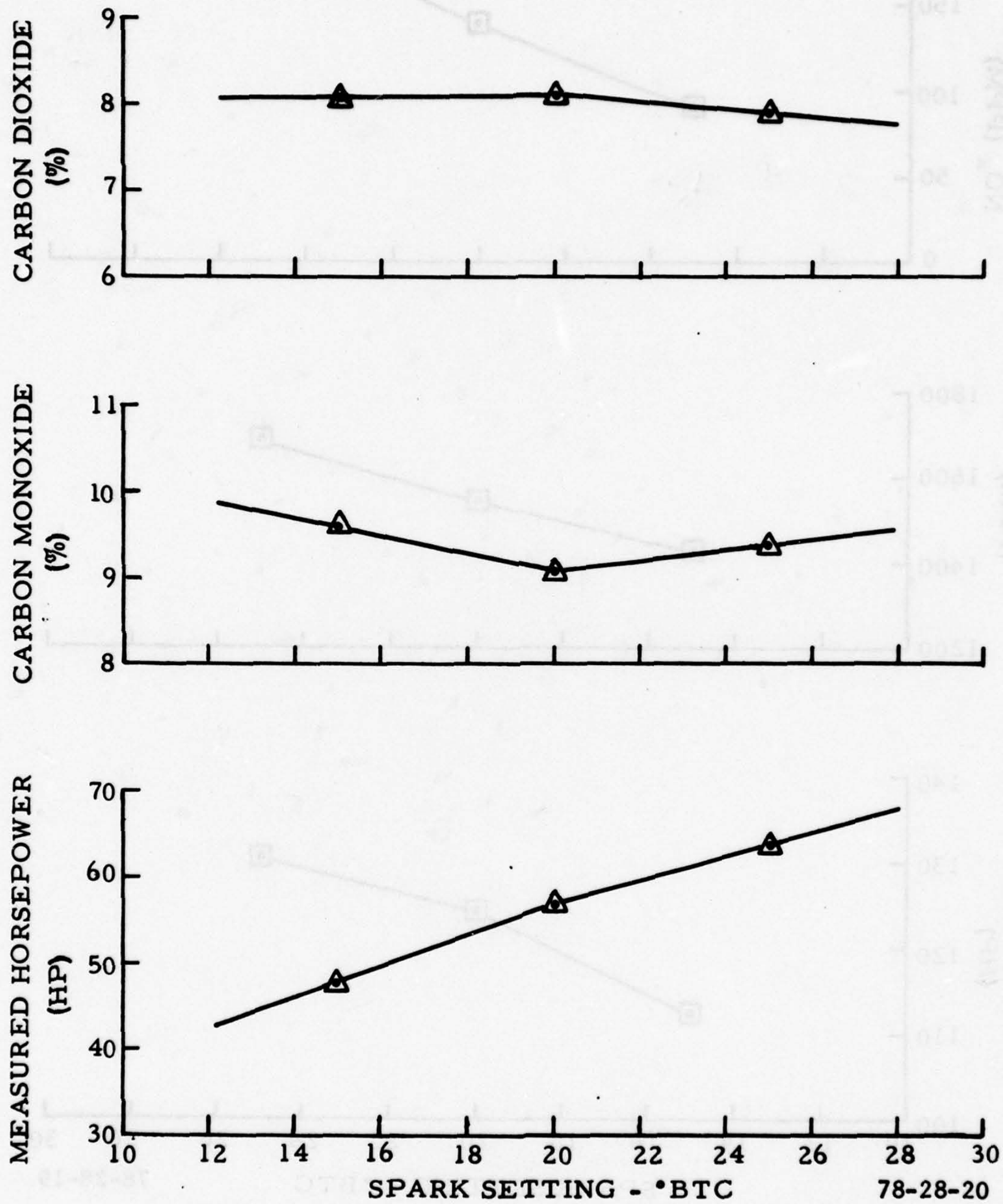


FIGURE 20. EFFECT OF VARYING SPARK SETTING ON ENGINE PERFORMANCE AND EXHAUST EMISSIONS--APPROACH MODE (CO_2 AND CO)

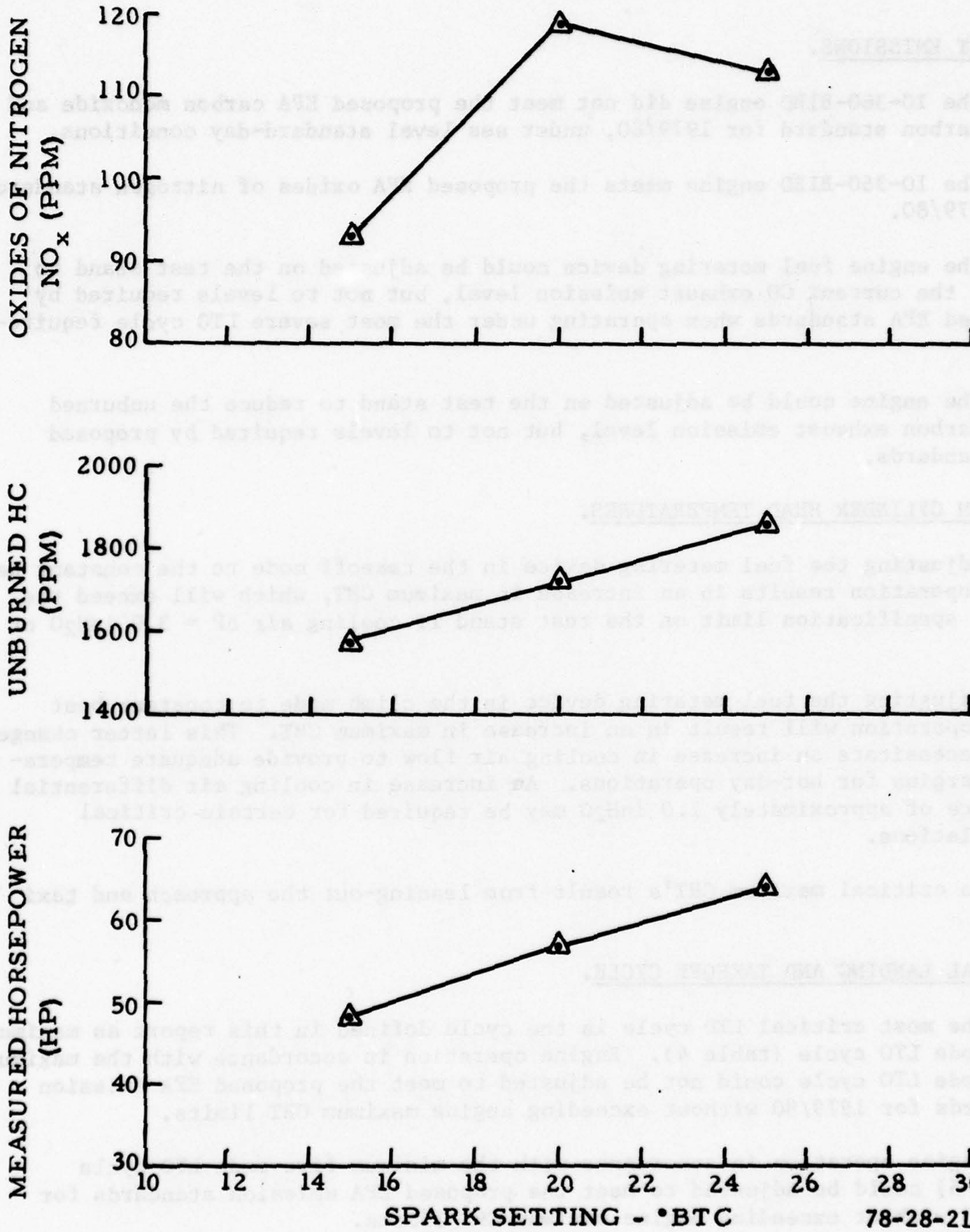


FIGURE 21. EFFECT OF VARYING SPARK SETTING ON ENGINE PERFORMANCE AND EXHAUST EMISSIONS--APPROACH MODE (HC AND NO_X)

SUMMARY OF RESULTS

EXHAUST EMISSIONS.

1. The IO-360-B1BD engine did not meet the proposed EPA carbon monoxide and hydrocarbon standard for 1979/80, under sea level standard-day conditions.

2. The IO-360-B1BD engine meets the proposed EPA oxides of nitrogen standard for 1979/80.

3. The engine fuel metering device could be adjusted on the test stand to reduce the current CO exhaust emission level, but not to levels required by proposed EPA standards when operating under the most severe LTO cycle requirements.

4. The engine could be adjusted on the test stand to reduce the unburned hydrocarbon exhaust emission level, but not to levels required by proposed EPA standards.

MAXIMUM CYLINDER HEAD TEMPERATURES.

1. Adjusting the fuel metering device in the takeoff mode to the constant best power operation results in an increase in maximum CHT, which will exceed the engine specification limit on the test stand if cooling air ΔP = 3.0 inH_2O or less.

2. Adjusting the fuel metering device in the climb mode to constant best power operation will result in an increase in maximum CHT. This latter change will necessitate an increase in cooling air flow to provide adequate temperature margins for hot-day operations. An increase in cooling air differential pressure of approximately 1.0 inH_2O may be required for certain critical installations.

3. No critical maximum CHT's result from leaning-out the approach and taxi modes.

CRITICAL LANDING AND TAKEOFF CYCLE.

1. The most critical LTO cycle is the cycle defined in this report as maximum five-mode LTO cycle (table 4). Engine operation in accordance with the maximum five-mode LTO cycle could not be adjusted to meet the proposed EPA emission standards for 1979/80 without exceeding engine maximum CHT limits.

2. Engine operation in accordance with the minimum five-mode LTO cycle (table 5) could be adjusted to meet the proposed EPA emission standards for 1979/80 without exceeding engine maximum CHT limits.

OPTIMUM SPARK SETTING.

1. The 25° BTC spark setting produces optimum test results:

a. Optimum Power
b. Optimum Maximum CHT
c. Emissions (CO, HC, and NO_x) compatible with optimum power and acceptable CHT margins.

2. The 15° and 20° BTC spark settings produced higher CO emissions even though HC and NO_x were lower. However, these settings also resulted in 5 to 25 percent decreases in power for the takeoff, climb, and approach modes.

CONCLUSIONS

The following conclusions are based on the testing accomplished with the Avco Lycoming IO-360-B1BD engine.

1. Simple fuel management adjustments (altering of fuel schedule) do not appear to provide the sole capability to safely reduce light-aircraft piston engine exhaust emissions.

2. The test data indicate that fuel management adjustments must be combined with engine/nacelle cooling modifications before safe and optimum low-emission aircraft/engine combinations can be achieved.

3. Spark settings other than the 25° BTC setting do not appear to produce significantly beneficial improvements in exhaust emissions.

4. The EPA CO limit of 0.042 lb/cycle/rated BHP did not appear to be achievable when hot-day takeoff and climb requirements are impacted by aircraft heavy gross weight and the need to pay close attention to CHT limitations.

5. An accessment of the maximum five-mode LTO cycle (table 4) test data indicate that the following standard changes should be made to the proposed EPA emission standards:

Proposed EPA STD. For 1979/1980 (lb/cycle/rated BHP)	Recommended Standard for 1979/80 (lb/cycle/rated BHP)
CO Standard 0.042	0.075
HC Standard 0.0019	0.0025
NO_x Standard 0.0015	0.0015

6. To avoid CHT problems in the takeoff mode (100-percent power), it is advisable not to adjust the fuel metering device. Engine operation in this mode should continue to be accomplished within current production rich/lean limits.

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6. Graf, Gleeson, and Paul, Interpretation of Exhaust Gas Analyses, Engineering Experiment Station, Oregon State Agricultural College, Bulletin Series No. 4, 1934.

7. Guide to Aviation Products, Humble Oil and Refining Company, 1969.

8. NAPTC Fuel Sample Analysis -- 100/130 Octane Aviation Gasoline, 1976.

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10. Aeronautical Vest-Pocket Handbook, Pratt and Whitney Aircraft, 1957.

APPENDIX A

FUEL SAMPLE ANALYSIS

COMBUSTIBLE ELEMENTS IN FUELS (AVIATION FUEL).

1. Carbon and hydrogen are the predominant combustible elements in fuels (aviation type), with small amounts of sulphur as the only other fuel element.

2. Liquid fuels are mixtures of complex hydrocarbons.

3. For combustion calculations gasoline or fuel oil can be assumed to have the average molecular formula C_8H_{17}.

Note: The Exxon® data presented in table A-1 may be found in reference 7.

TABLE A-1. TYPICAL SPECIFICATIONS FOR AVIATION FUELS

Item	D910-76 Grade 100/130	Exxon Aviation Gas 100/130	D910-70 Grade 115/145	Exxon Aviation Gas 115/145
Freezing Point, °F	-72 Max.	Below -76	-76 Max.	Below -76
Reid Vapor Press., PSI	7.0 Max.	6.8	7.0 Max.	6.8
Sulfur, % by Weight	0.05 Max.	0.02	0.05 Max.	0.02
Lower Heating Value, BTU/lb	18,720 Min.		18,800 Min.	
Heat of Comb. (NET). BTU/lb		18,960		19,050
Distillation, %Evaporated				
At 167° F (Max.)	10	22	10	21
At 167° F (Min.)	40		40	
At 221° F (Max.)	50	76	50	62
At 275° F (Max.)	90	97	90	96
Distillation End Point	338° F Max.		338° F Max.	
Final Boiling Point °F		319		322
Tel Content, ML/U.S.Gal.	4.0 Max.	3.9	4.6 Max.	4.5
Color	Green	Green	Purple	Purple

4. NAFEC used 100/130 (octane rated) aviation gasoline for the piston engine emission tests. The following analysis of a typical fuel sample (table A-2) was made at the U.S. Naval Air Propulsion Test Center (NAPTC), Trenton, N.J. (reference 8).

TABLE A-2. ANALYSIS OF NAFEC FUEL SAMPLE, 100/130 FUEL

Item	NAFEC Sample 100/130	Grade 100/130 (MIL-G-5572E) Spec Limits Min.	Distillation %Evaporated	Max.
Freezing Point, °F	Below -76° F			-76
Reid Vapor Press., PSI	6.12	5.5		7.0
Sulfur % By Weight	0.024			0.05
Lower Heating Value BTU/lb		18,700		
Heat of Comb. (NET) BTU/lb	18,900			
Distillation, %Evaporated				
At 158° F	10			
At 167° F (Min)		167° F	10	
At 167° F (Max.)			40	167° F
At 210° F	40			
At 220° F	50			
At 221° F		221° F	50	
At 242° F	90			
At 275° F		275° F	90	
Distillation End Point	313° F			338° F
Specific Gravity @60° F	0.7071	Report		Report
API Gravity @60° F	68.6	No Limit		
Tel Content, ML/U.S. Gal.	1.84			4.60

Computation for the fuel hydrogen-carbon ratio is based on the fuel net heating value, hf, equal to 18,900 BTU/lb and figure A-1.

$C/H = 5.6$

$C = 12.011$

$C_8 = 8 \times 12.011 = 96.088$

$H_y = (96.088) \div 5.6 = 17.159$

$H = 1.008$

$Y = (17.159) \div 1.008 = 17.022$ Use $Y = 17$

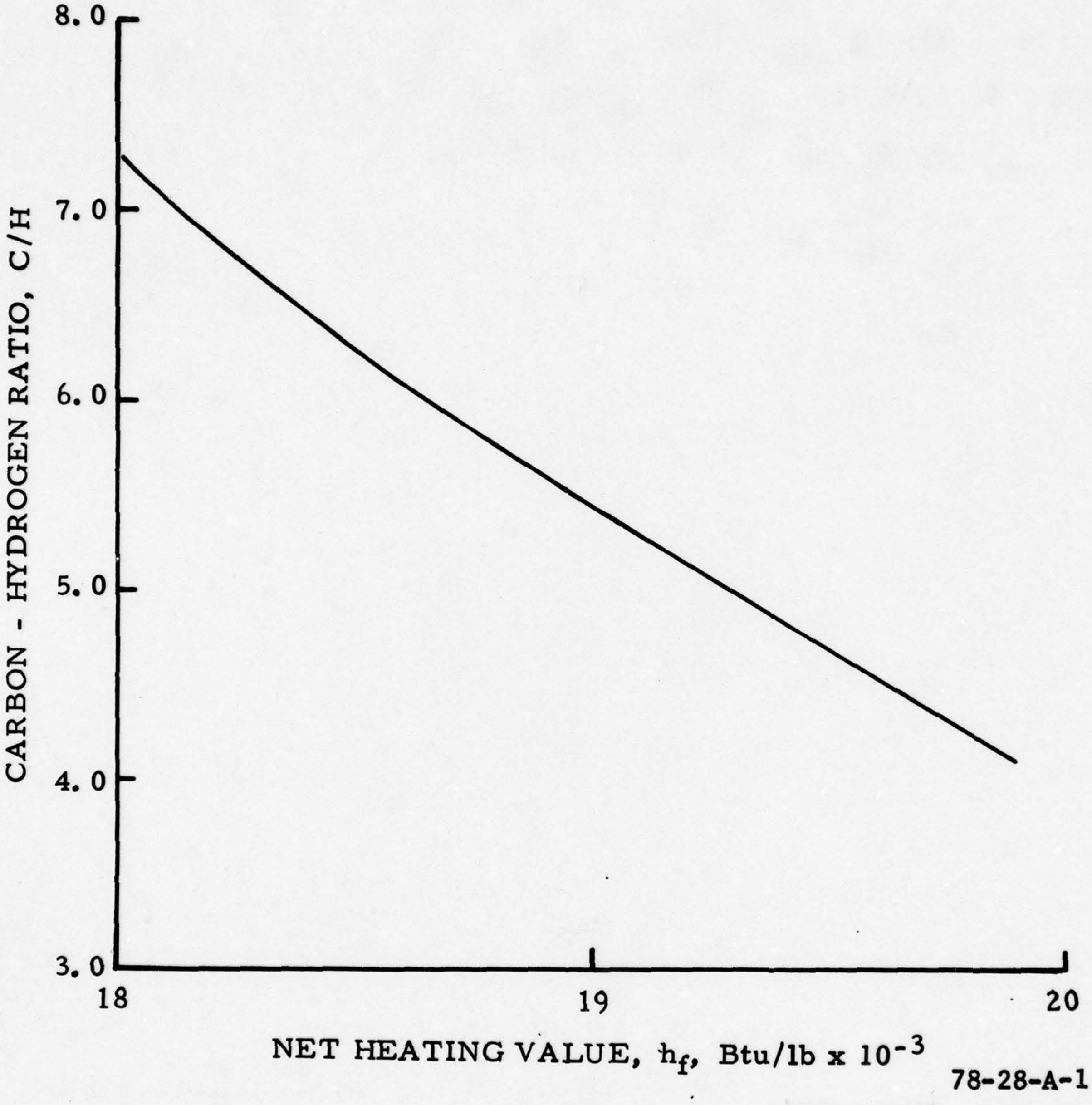

FIGURE A-1. NET HEATING VALUE FOR AVIATION GASOLINE AND CARBON-HYDROGEN RATIO CORRELATION

APPENDIX B

COMPOSITION OF AIR (GENERAL PROPERTIES)

1. Dry air is a mixture of gases that has a representative volumetric analysis in percentages as follows:

Oxygen (O_2)--20.99%
Nitrogen (N_2)--78.03%
Argon (A)--0.94% (Also includes traces of the rare gases neon, helium, and krypton)
Carbon Dioxide (CO_2)--0.03%
Hydrogen (H_2)--0.01%

2. For most calculations it is sufficiently accurate to consider dry air as consisting of:

O_2 = 21.0%
N_2 = 79.0% (including all other inert gases)

3. The moisture or humidity in atmospheric air varies over wide limits, depending on meteorological conditions. Its presence in most cases simply implies an additional amount of essentially inert material.

Note: Information given in items 1, 2, and 3 is recommended for computation purposes (references 3, 4, 9, and 10).

TABLE B-1. MASS ANALYSIS OF PURE DRY AIR

Gas	Volumetric Analysis %	Mole Fraction	Molecular Weight	Relative Weight
O_2	20.99	0.2099	32.00	6.717
N_2	78.03	0.7803	28.016	21.861
A	0.94	0.0094	39.944	0.376
CO_2	0.03	0.0003	44.003	0.013
Inert Gases	0.01	0.0001	48.0	0.002
	100.00	1.000		28.969 = M for air

4. The molecular weight of the <u>apparent nitrogen</u> can be similarly determined by dividing the total mass of the inert gases by the total number of moles of these components:

$$M_{\text{Apparent Nitrogen}} = \frac{2225}{79.01} = 28.161$$

5. This appendix advocates the term nitrogen as referring to the entire group of inert gases in the atmosphere and therefore the molecular weight of 28.161 will be the correct value (rather than the value 28.016 for pure nitrogen).

6. In combustion processes the active constituent is oxygen (O_2), and the apparent nitrogen can be considered to be inert. Then for every mole of oxygen supplied, 3.764 moles of apparent nitrogen accompany or dilute the oxygen in the reaction:

$$\frac{79.01}{20.99} = 3.764 \frac{\text{Moles Apparent Nitrogen}}{\text{Mole Oxygen}}$$

7. The information given in items 4, 5, and 6 is recommended for computational purposes in reference 4. Therefore, one mole of air (dry), which is composed of one mole of oxygen (O_2) and 3.764 moles of nitrogen (N_2), has a total weight of 137.998 pounds.

$$(O_2 + 3.764\ N_2) = 137.998$$

This gives the molecular weight of air = 28.97.

APPENDIX C

NAFEC TEST DATA AND WORKING PLOTS FOR ANALYSIS AND EVALUATION OF AVCO LYCOMING IO-360-B1BD ENGINE

LIST OF ILLUSTRATIONS

LIST OF ILLUSTRATIONS (Continued)

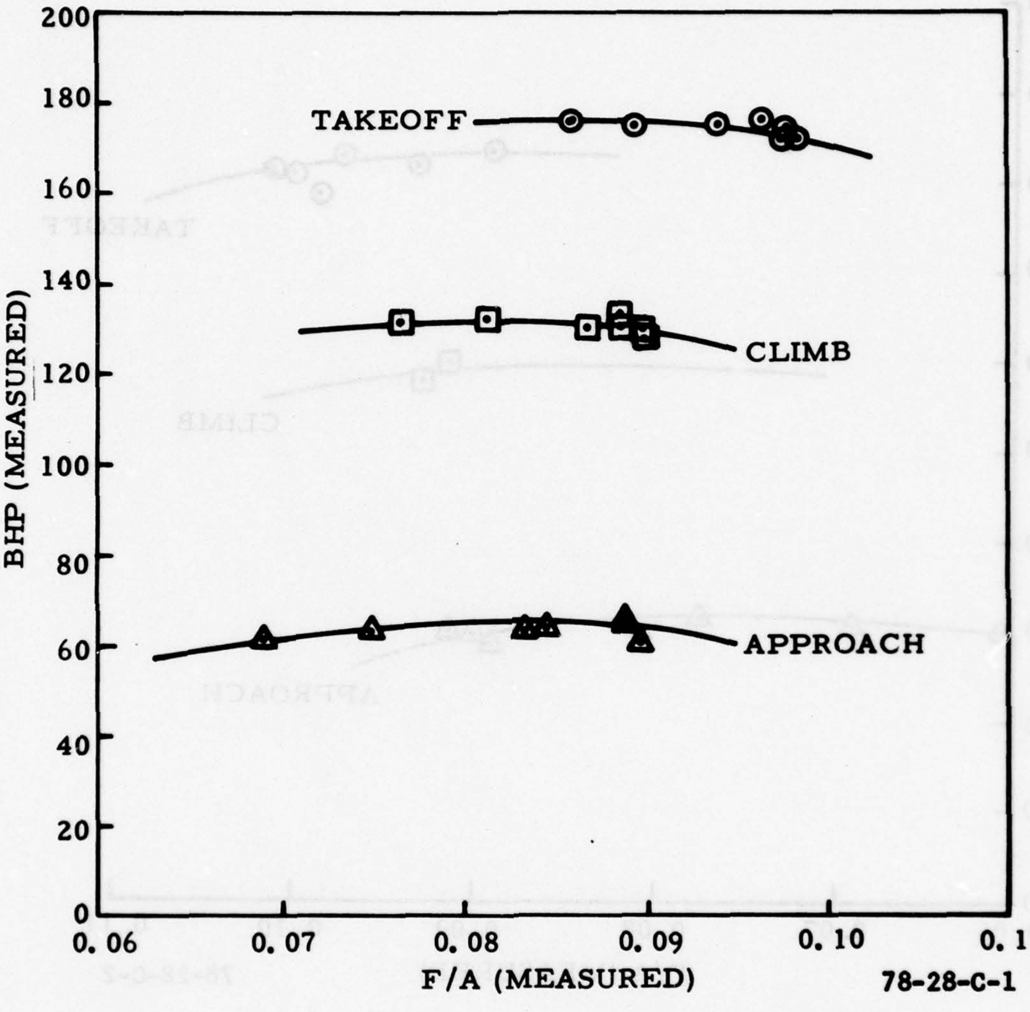

FIGURE C-1. MEASURED PERFORMANCE--AVCO LYCOMING IO-360-B1BD ENGINE--TAKEOFF, CLIMB, AND APPROACH MODES--NOMINAL SEA LEVEL AIR DENSITY 0.0777 lb/ft^3

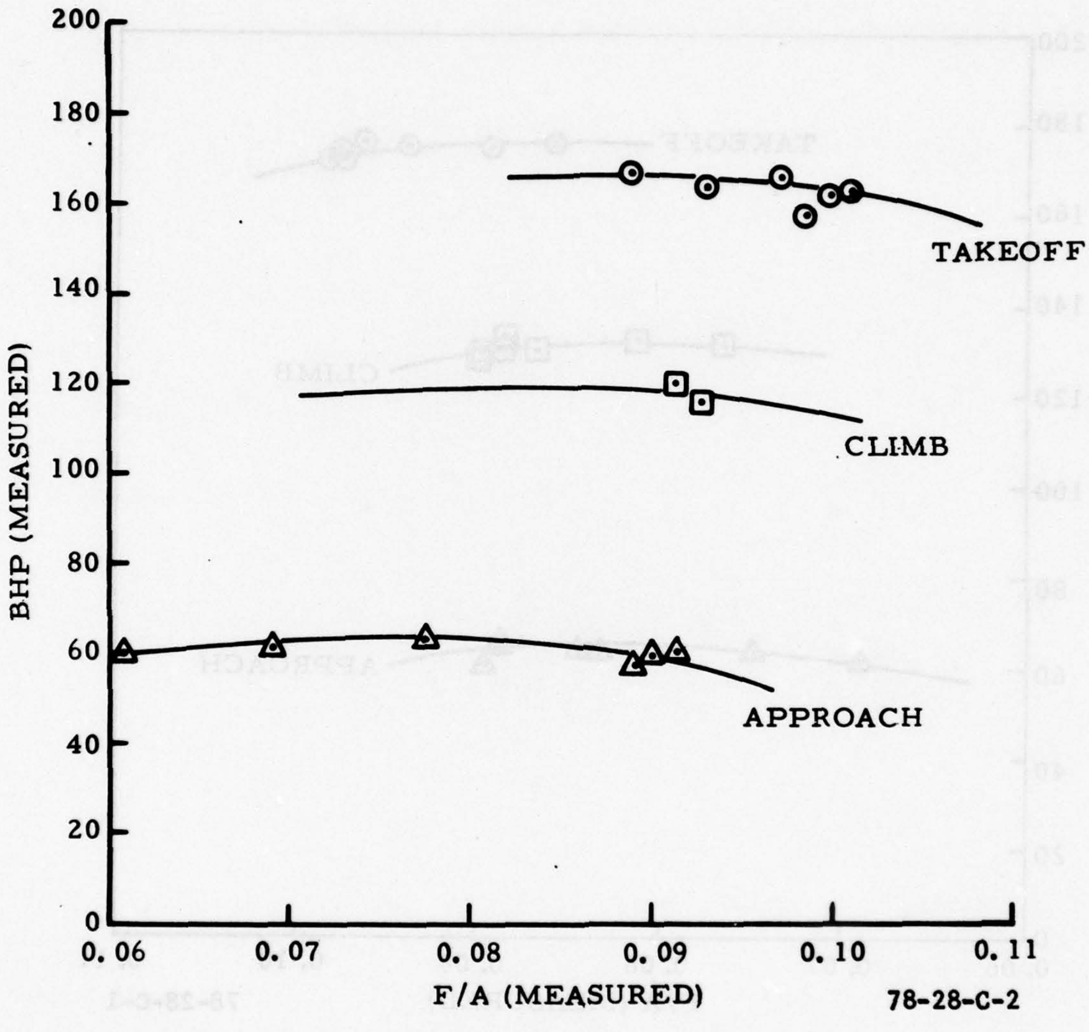

FIGURE C-2. MEASURED PERFORMANCE--AVCO LYCOMING IO-360-B1BD ENGINE--TAKEOFF, CLIMB, AND APPROACH MODES--NOMINAL SEA LEVEL AIR DENSITY 0.0720 lb/ft^3

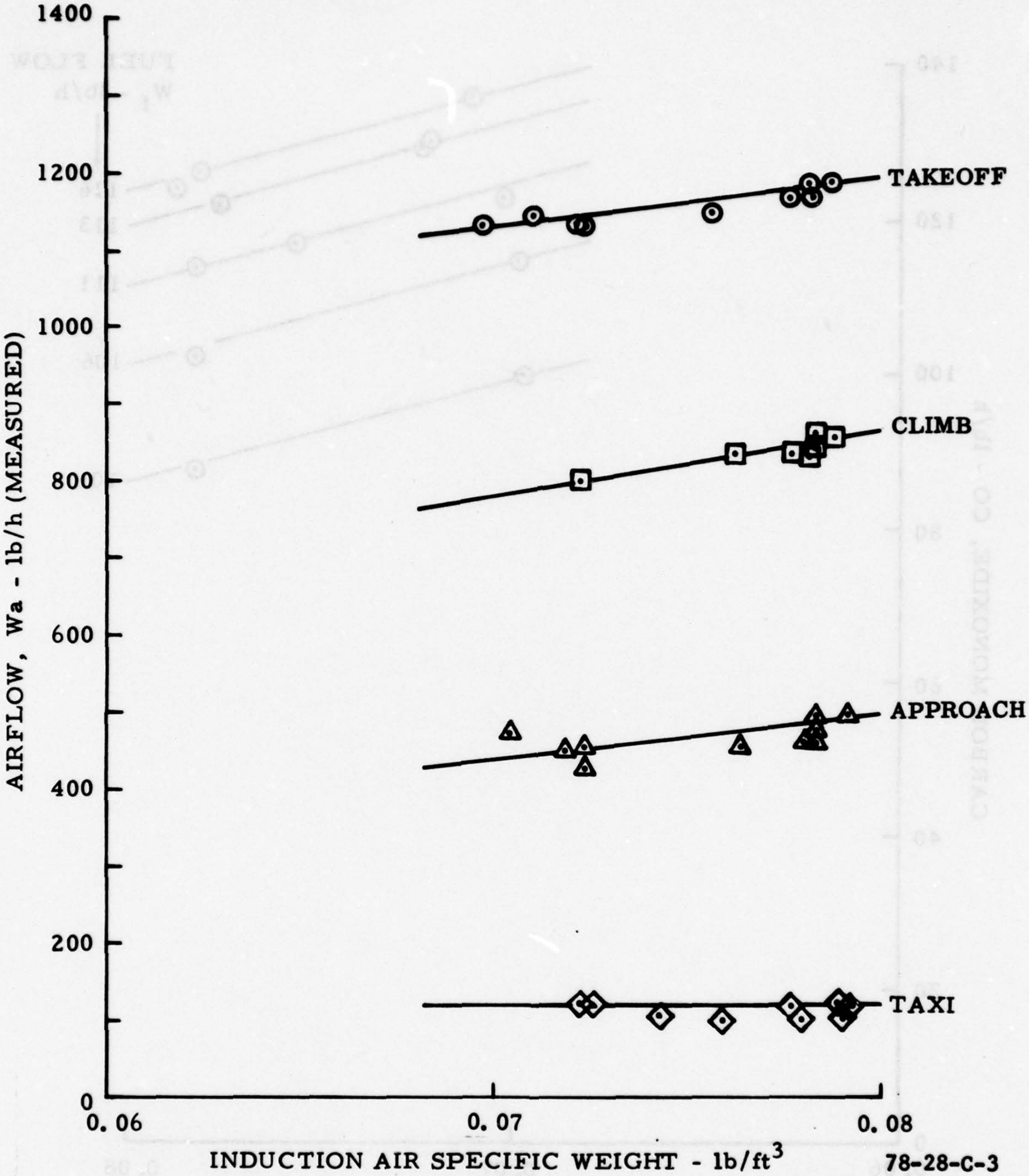

FIGURE C-3. AIRFLOW AS A FUNCTION OF INDUCTION AIR SPECIFIC WEIGHT FOR AN AVCO LYCOMING IO-360-B1BD ENGINE--NOMINAL SEA LEVEL TEST DATA

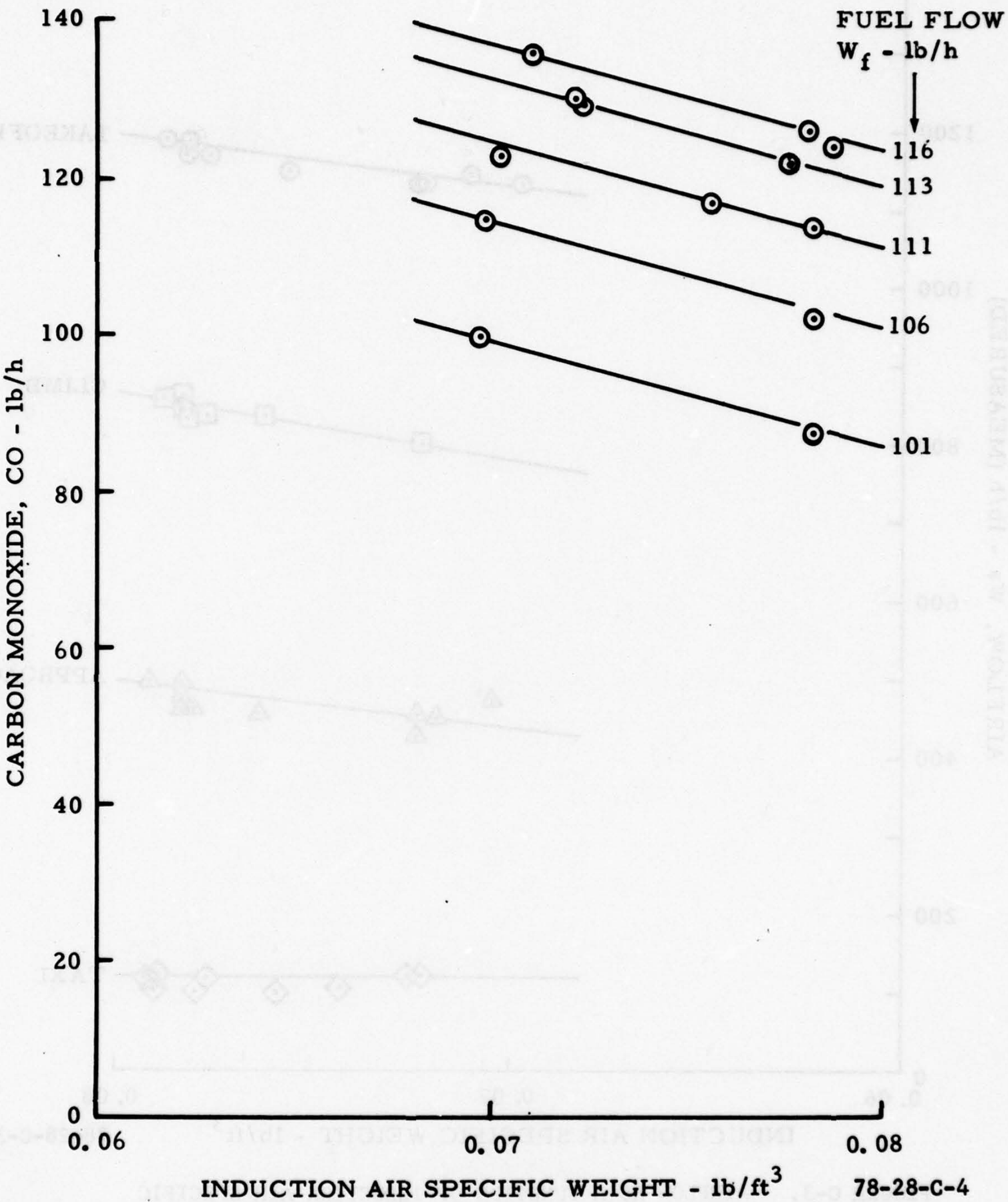

FIGURE C-4. EXHAUST CARBON MONOXIDE AS A FUNCTION OF INDUCTION AIR SPECIFIC WEIGHT FOR SEVERAL TAKEOFF CONSTANT FUEL FLOW SCHEDULES--AVCO LYCOMING IO-360-B1BD ENGINE

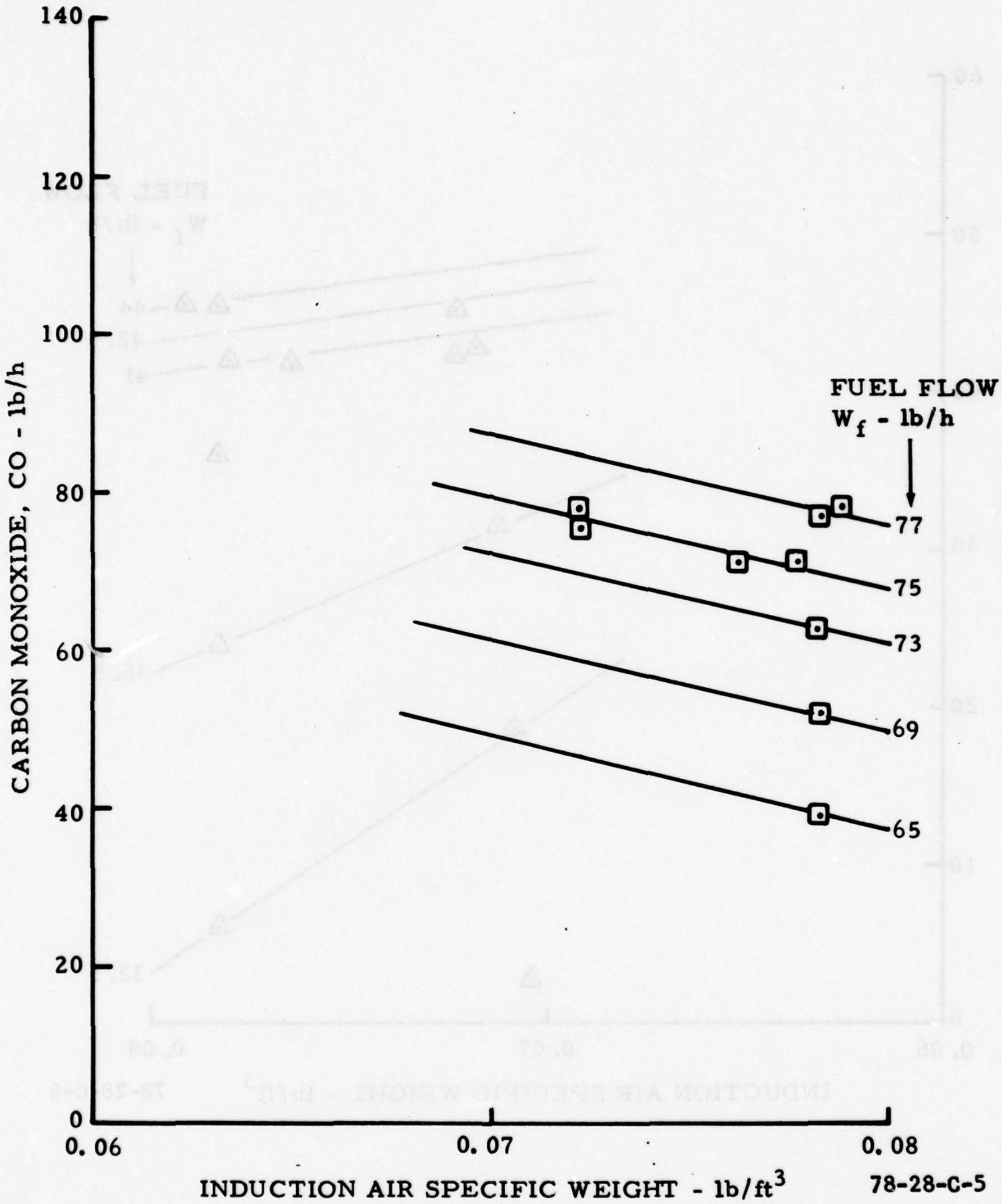

FIGURE C-5. EXHAUST CARBON MONOXIDE AS A FUNCTION OF INDUCTION AIR SPECIFIC WEIGHT FOR SEVERAL CLIMB MODE CONSTANT FUEL FLOW SCHEDULES--AVCO LYCOMING IO-360-B1BD ENGINE

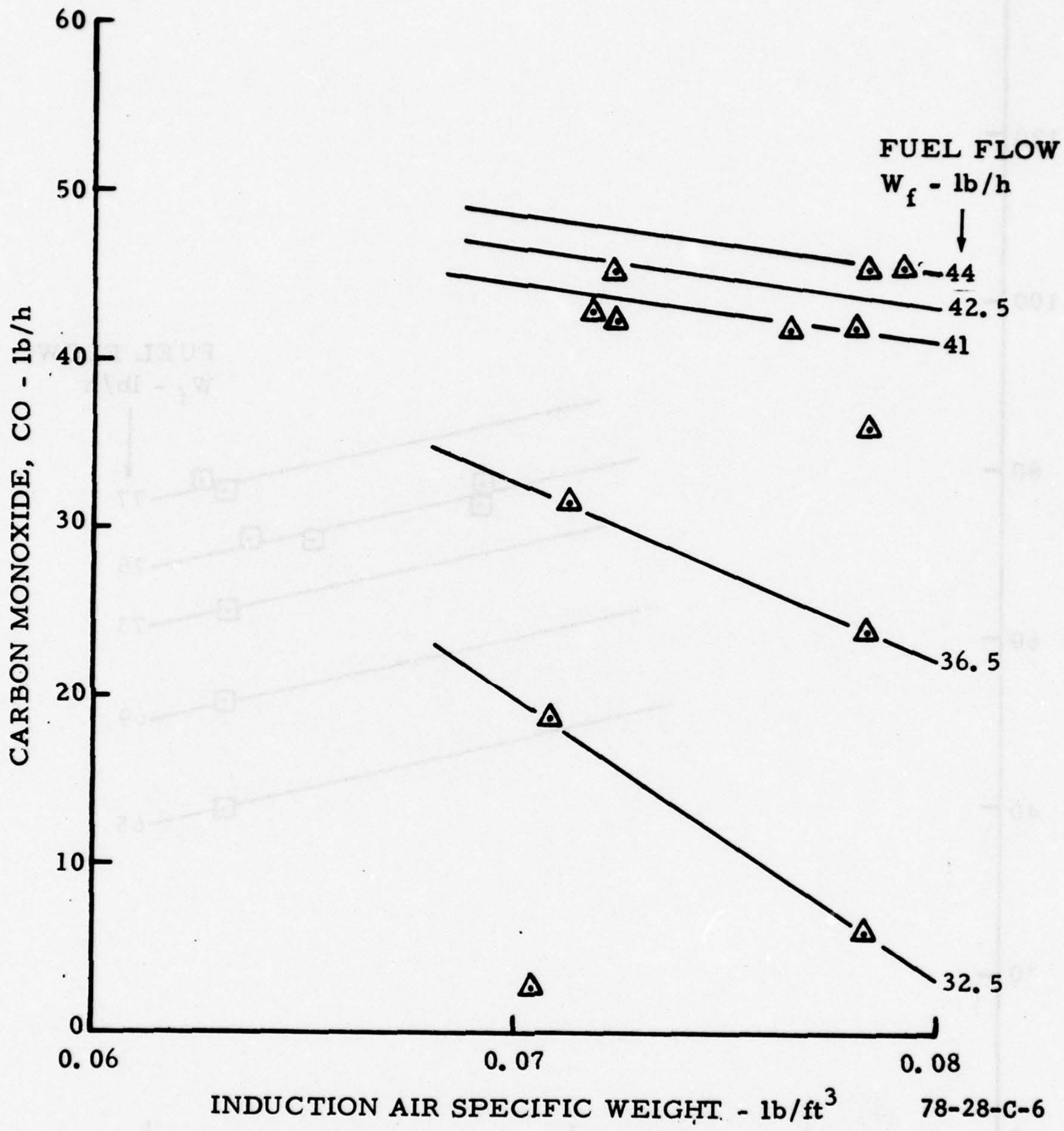

FIGURE C-6. **EXHAUST CARBON MONOXIDE AS A FUNCTION OF INDUCTION AIR SPECIFIC WEIGHT FOR SEVERAL APPROACH MODE CONSTANT FUEL FLOW SCHEDULES--AVCO LYCOMING IO-360-B1BD ENGINE**

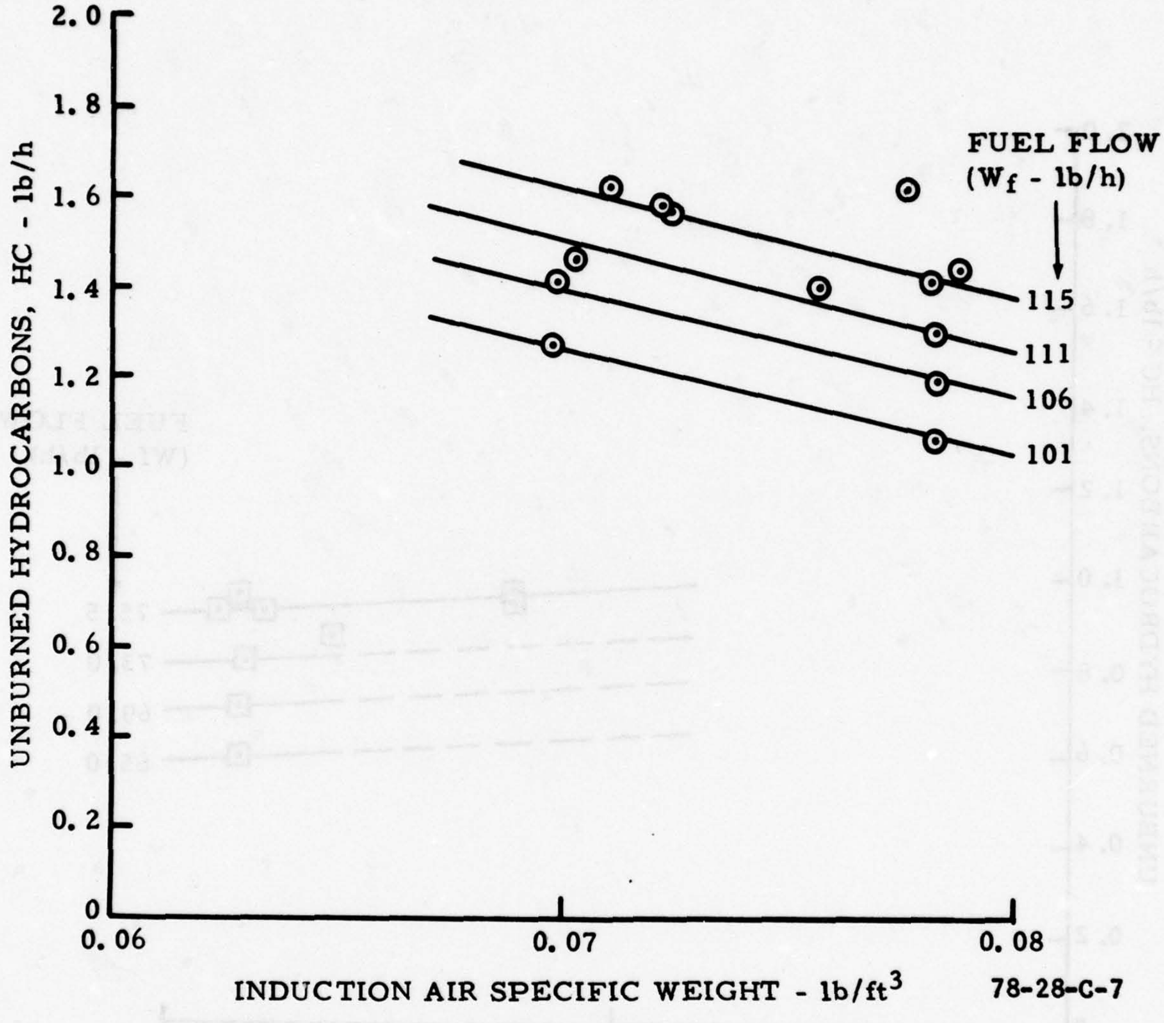

FIGURE C-7. UNBURNED EXHAUST HYDROCARBONS AS A FUNCTION OF INDUCTION AIR SPECIFIC WEIGHT FOR SEVERAL TAKEOFF CONSTANT FUEL FLOW SCHEDULES--AVCO LYCOMING IO-360-B1BD ENGINE

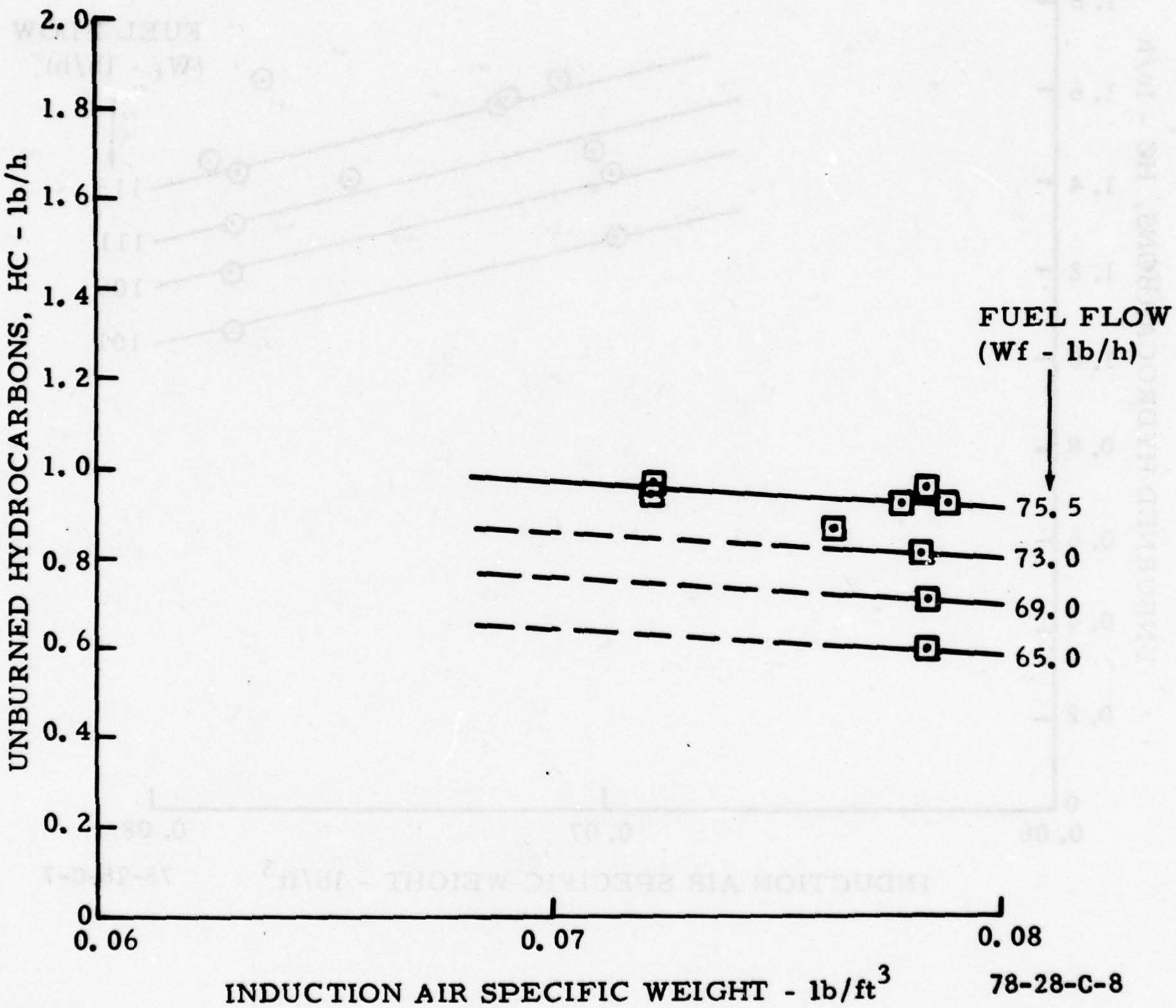

FIGURE C-8. UNBURNED EXHAUST HYDROCARBONS AS A FUNCTION OF INDUCTION AIR SPECIFIC WEIGHT FOR SEVERAL CLIMB MODE CONSTANT FUEL FLOW SCHEDULES--AVCO LYCOMING IO-360-B1BD ENGINE

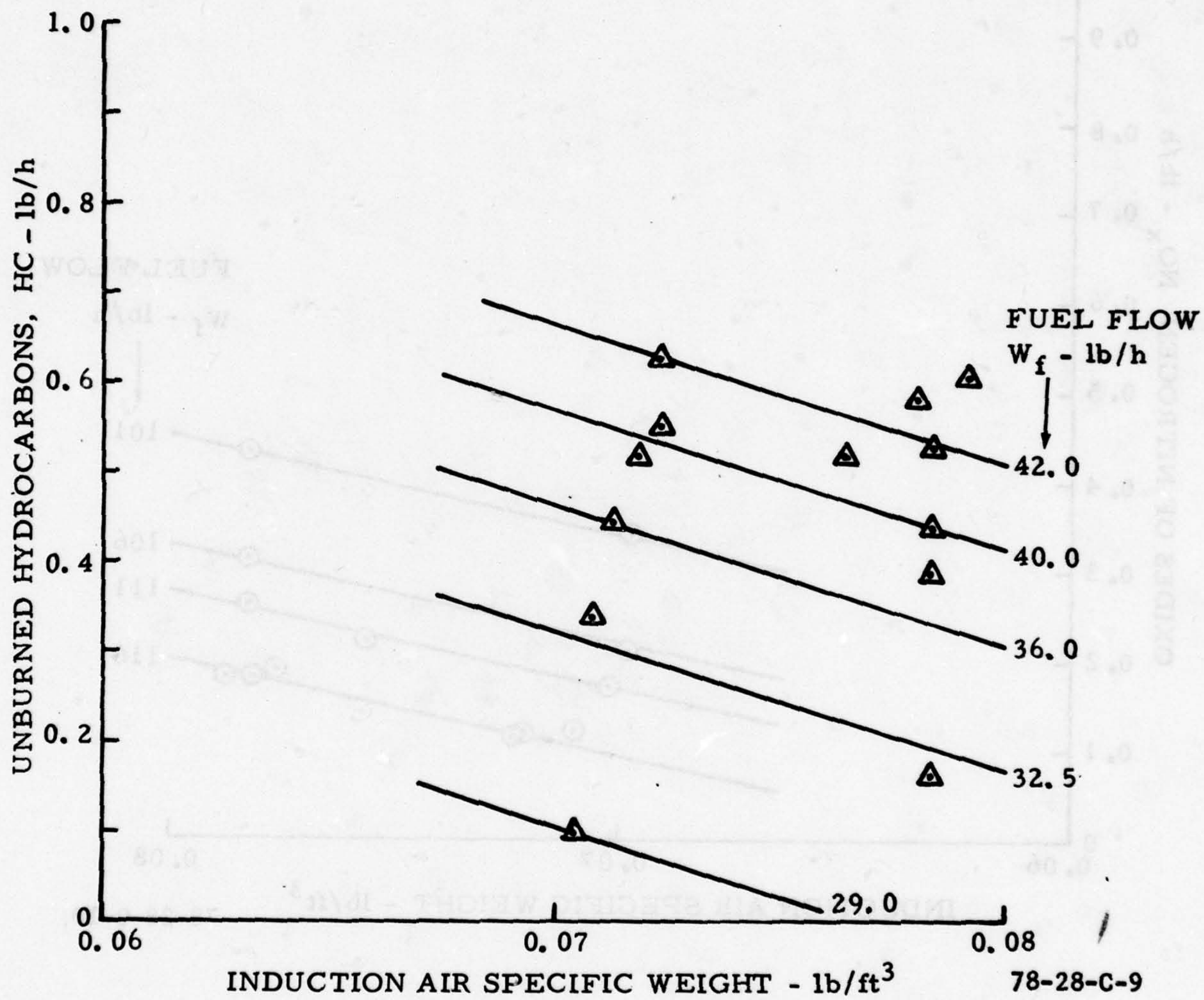

FIGURE C-9. UNBURNED EXHAUST HYDROCARBONS AS A FUNCTION OF INDUCTION AIR SPECIFIC WEIGHT FOR SEVERAL APPROACH MODE CONSTANT FUEL FLOW SCHEDULES--AVCO LYCOMING IO-360-B1BD ENGINE

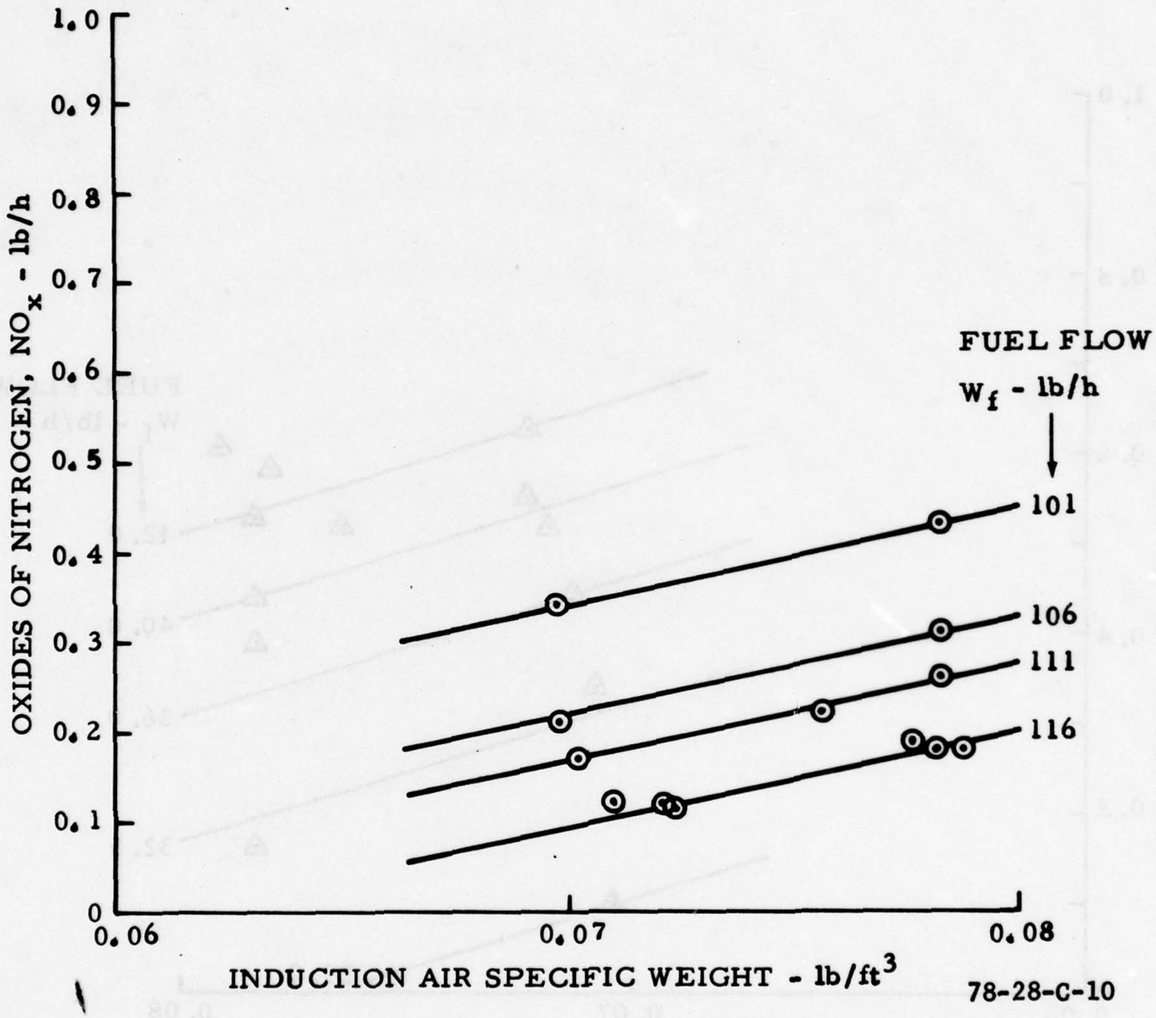

FIGURE C-10. OXIDES OF NITROGEN (NO_x) AS A FUNCTION OF INDUCTION AIR SPECIFIC WEIGHT FOR SEVERAL TAKEOFF CONSTANT FUEL FLOW SCHEDULES--AVCO LYCOMING IO-360-B1BD ENGINE

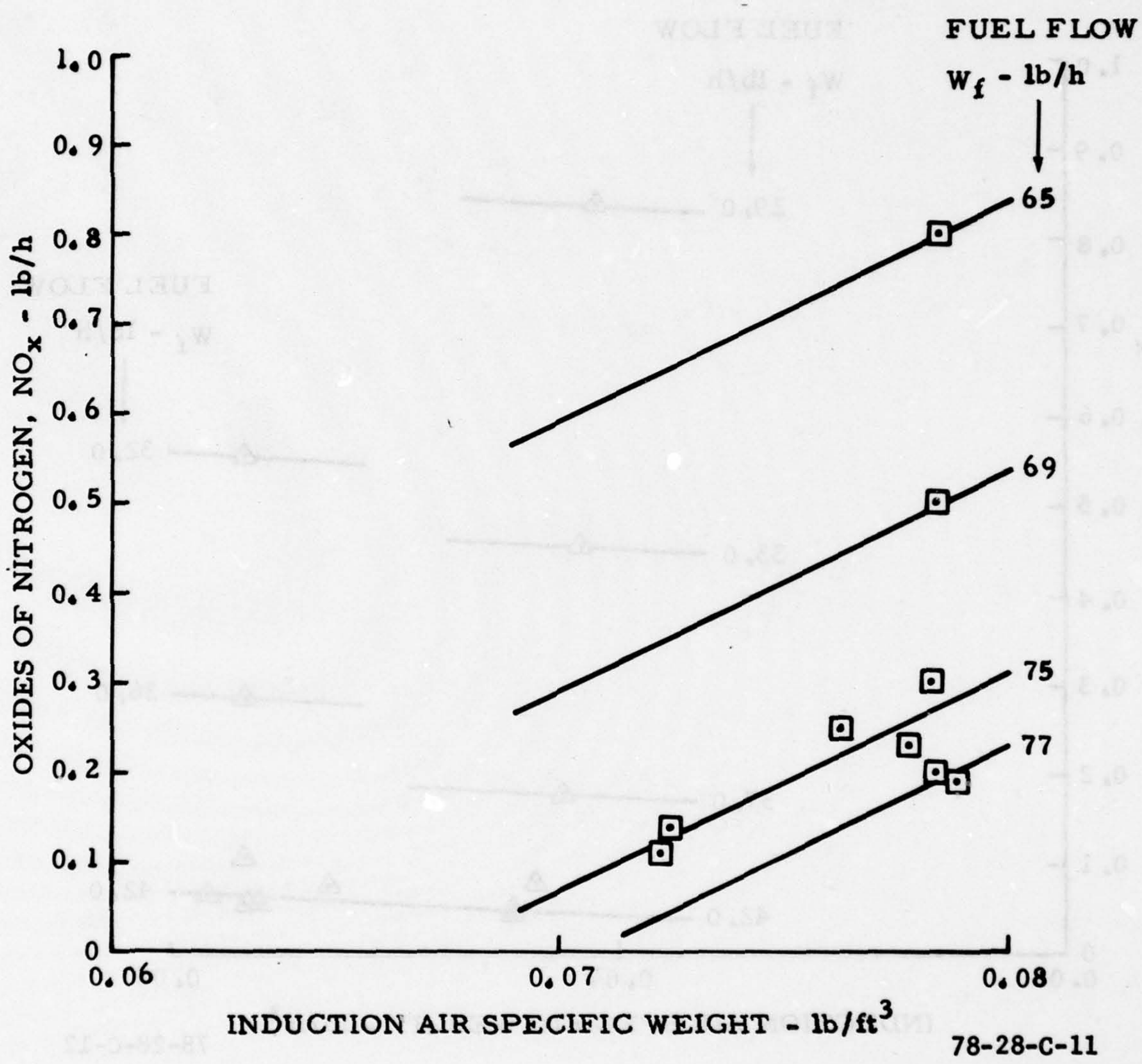

FIGURE C-11. OXIDES OF NITROGEN (NO_x) AS A FUNCTION OF INDUCTION AIR SPECIFIC WEIGHT FOR SEVERAL CLIMB MODE CONSTANT FUEL FLOW SCHEDULES--AVCO LYCOMING IO-360-B1BD ENGINE

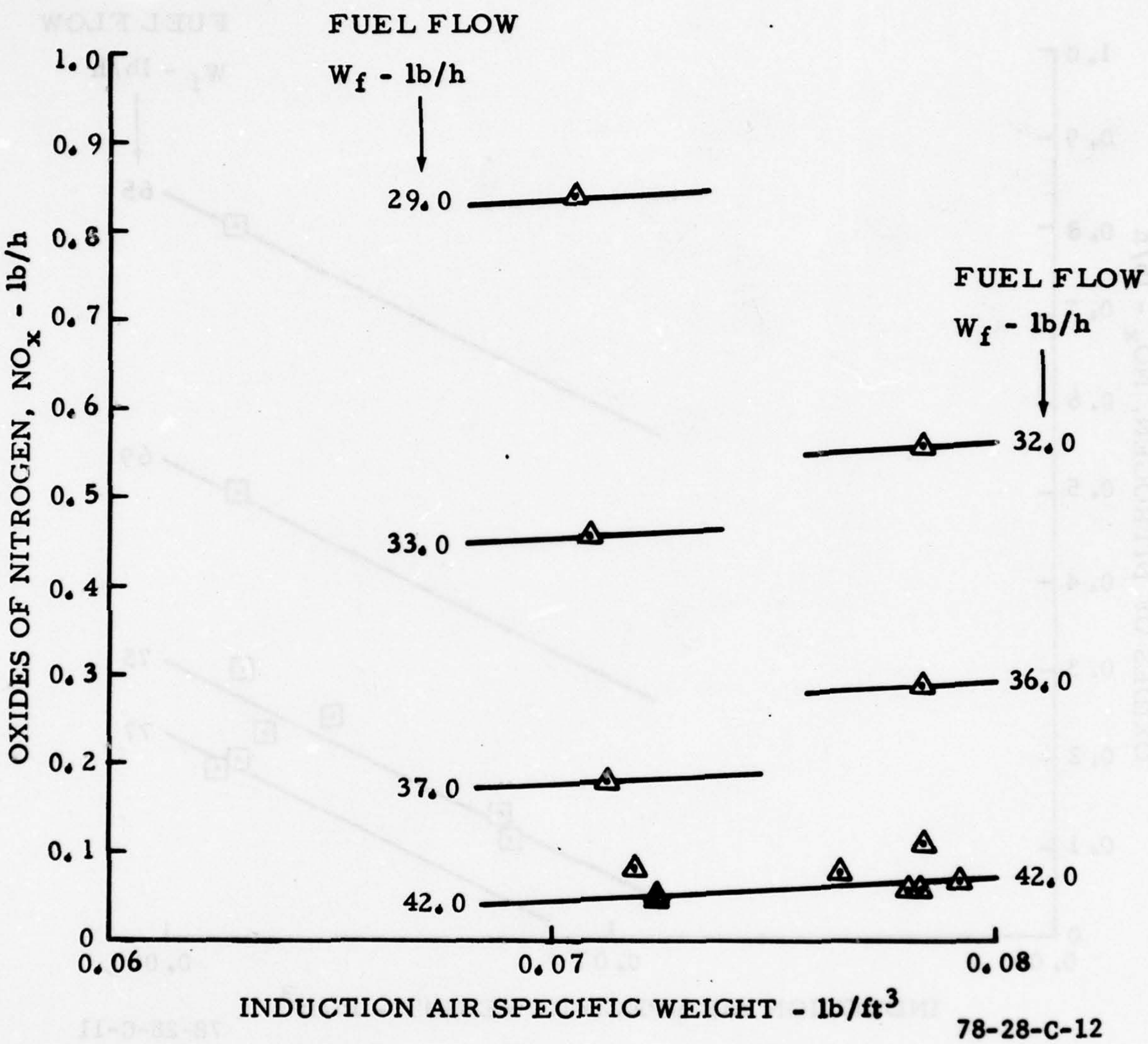

FIGURE C-12. OXIDES OF NITROGEN (NO_x) AS A FUNCTION OF INDUCTION AIR SPECIFIC WEIGHT FOR SEVERAL APPROACH MODE CONSTANT FUEL FLOW SCHEDULES--AVCO LYCOMING IO-360-B1BD ENGINE

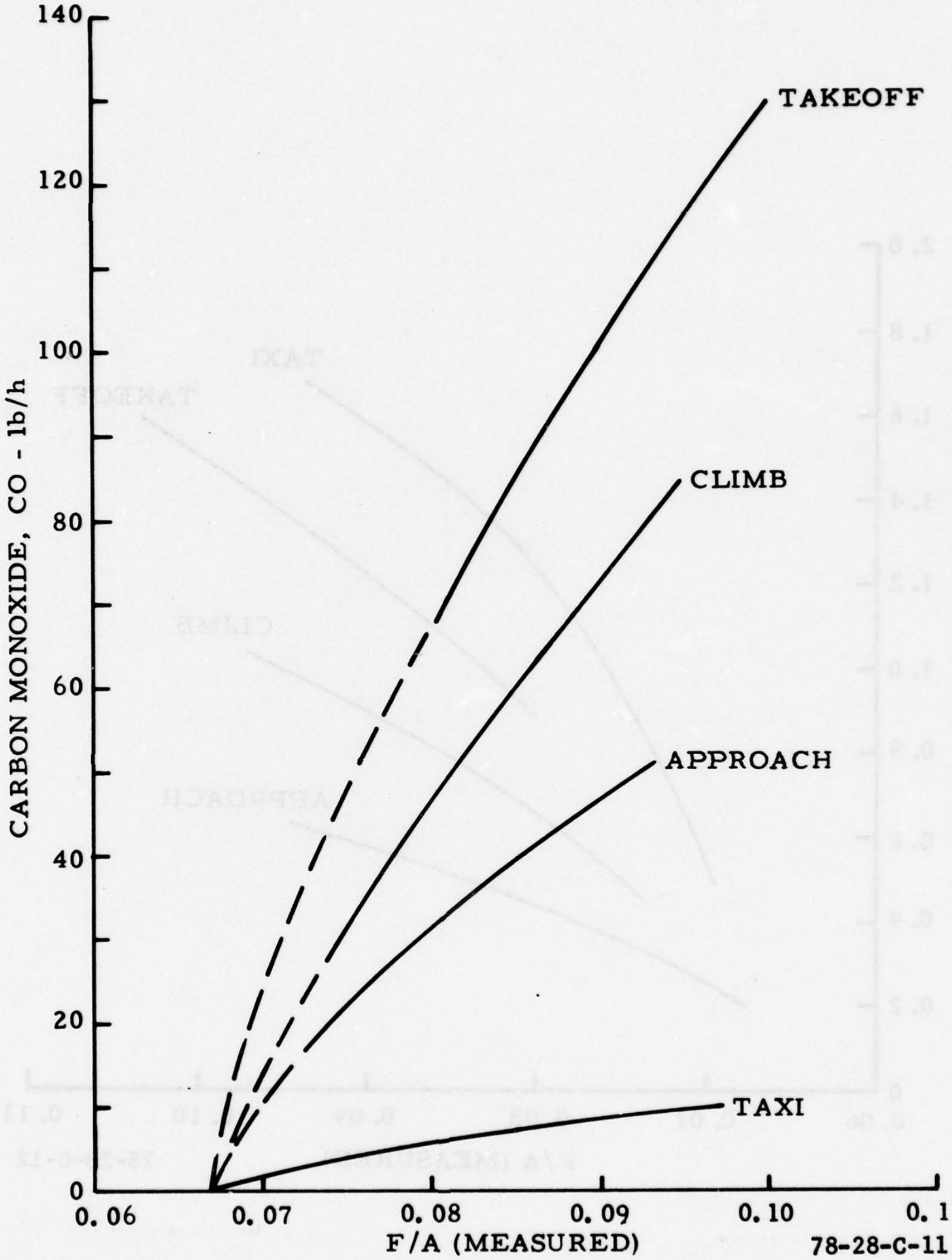

FIGURE C-13. SEA LEVEL STANDARD-DAY EMISSION CHARACTERISTICS FOR AN AVCO LYCOMING IO-360-B1BD ENGINE--CARBON MONOXIDE

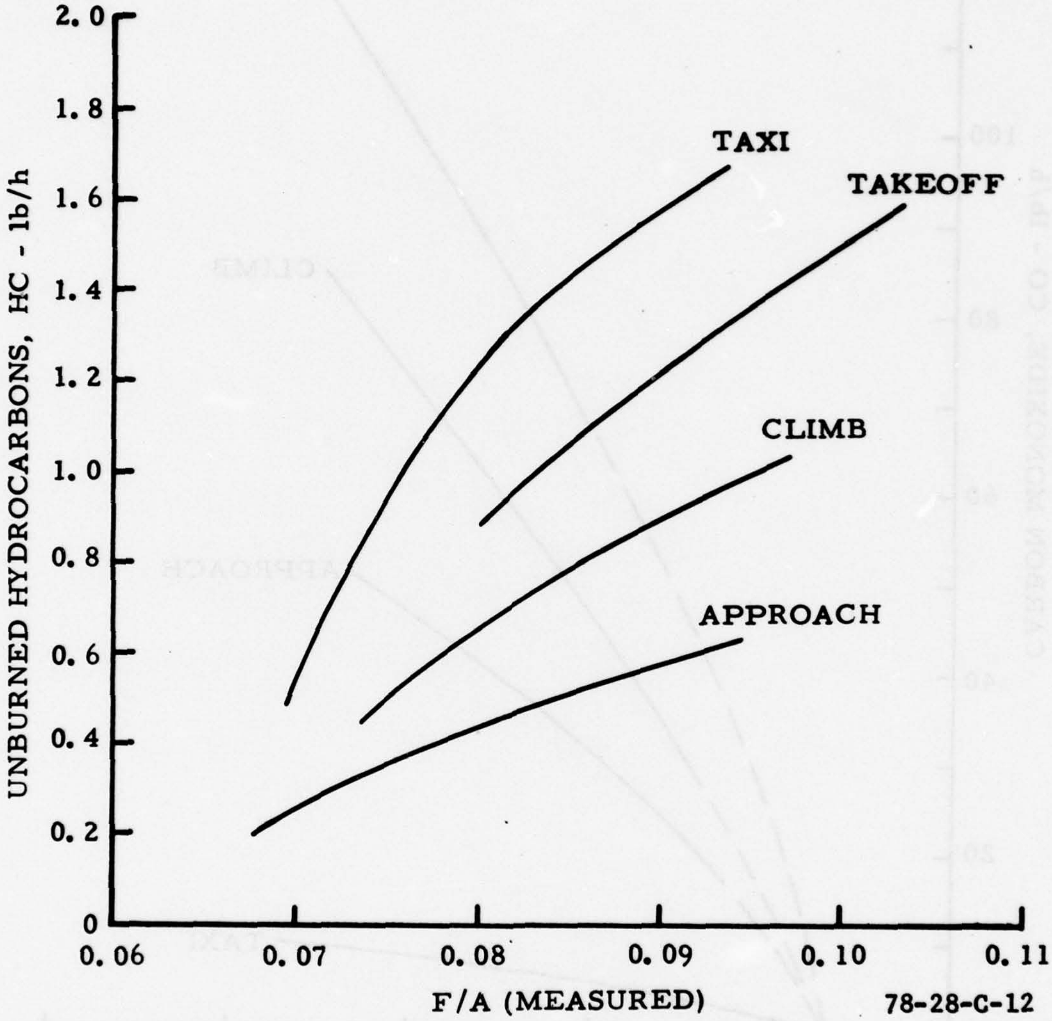

FIGURE C-14. SEA LEVEL STANDARD-DAY EMISSIONS CHARACTERISTICS FOR AN AVCO LYCOMING IO-360-B1BD ENGINE--UNBURNED HYDROCARBONS

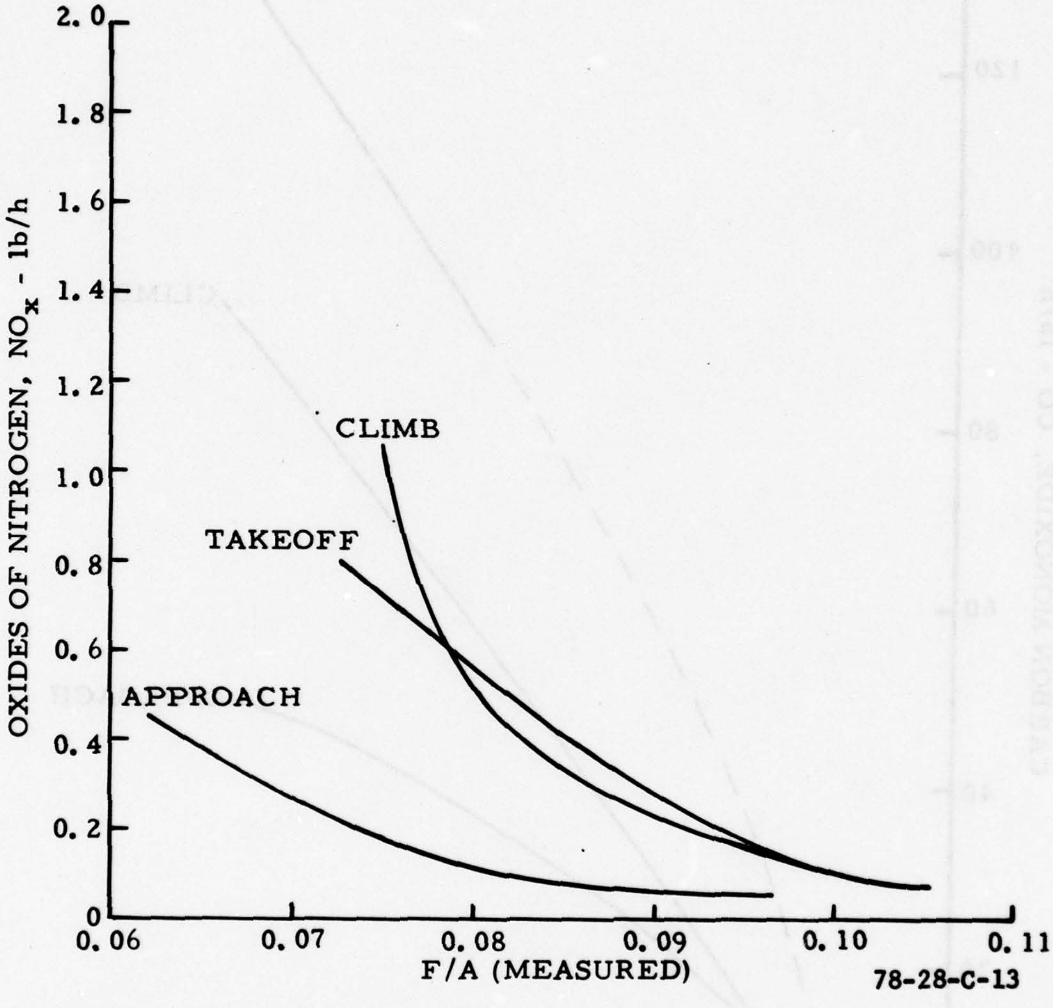

FIGURE C-15. SEA LEVEL STANDARD-DAY EMISSION CHARACTERISTICS FOR AN AVCO LYCOMING IO-360-B1BD ENGINE—OXIDES OF NITROGEN

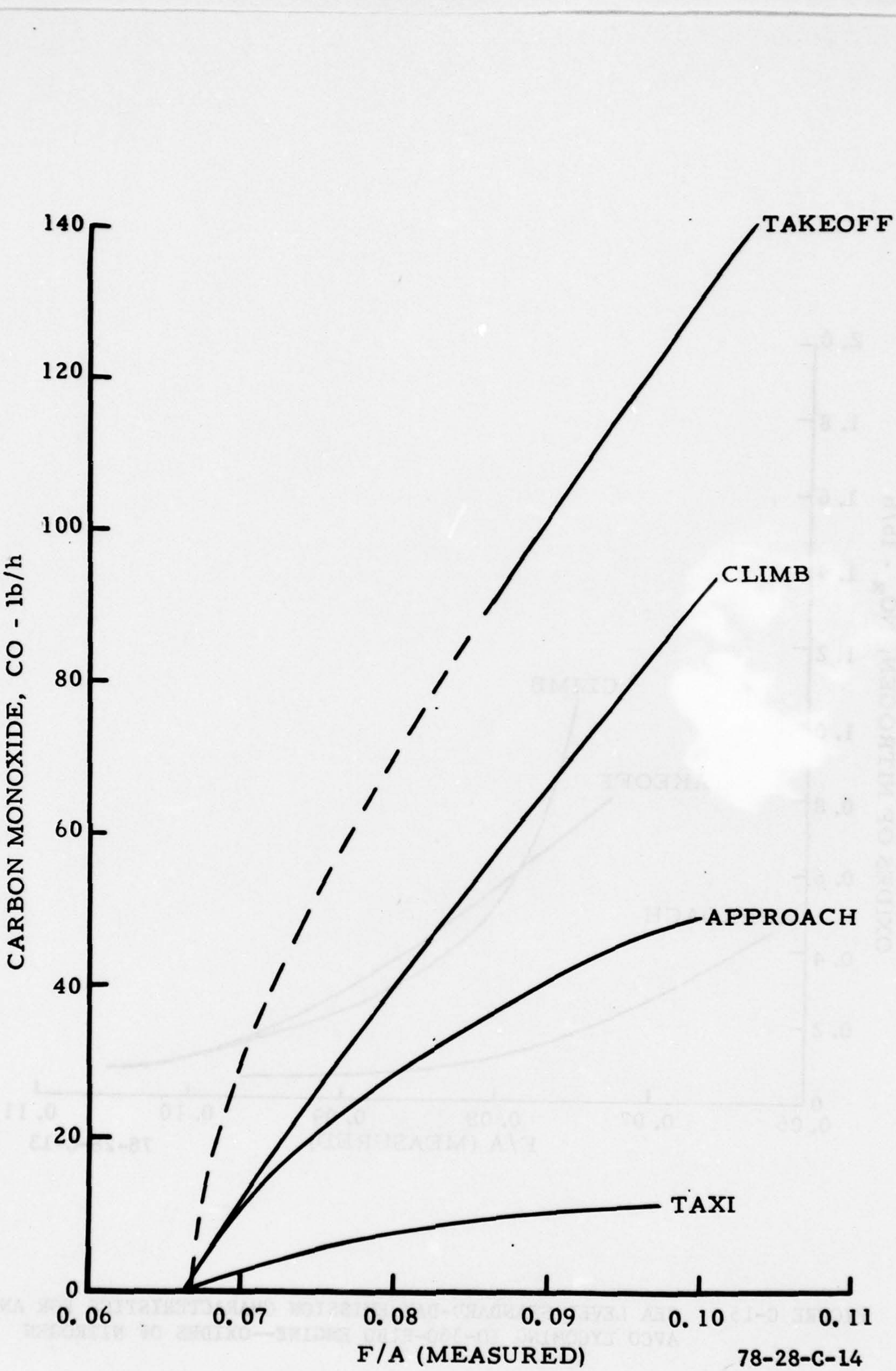

FIGURE C-16. SEA LEVEL HOT-DAY (T_1=103° F) EMISSIONS CHARACTERISTICS FOR AN AVCO LYCOMING IO-360-B1BD ENGINE--CARBON MONOXIDE

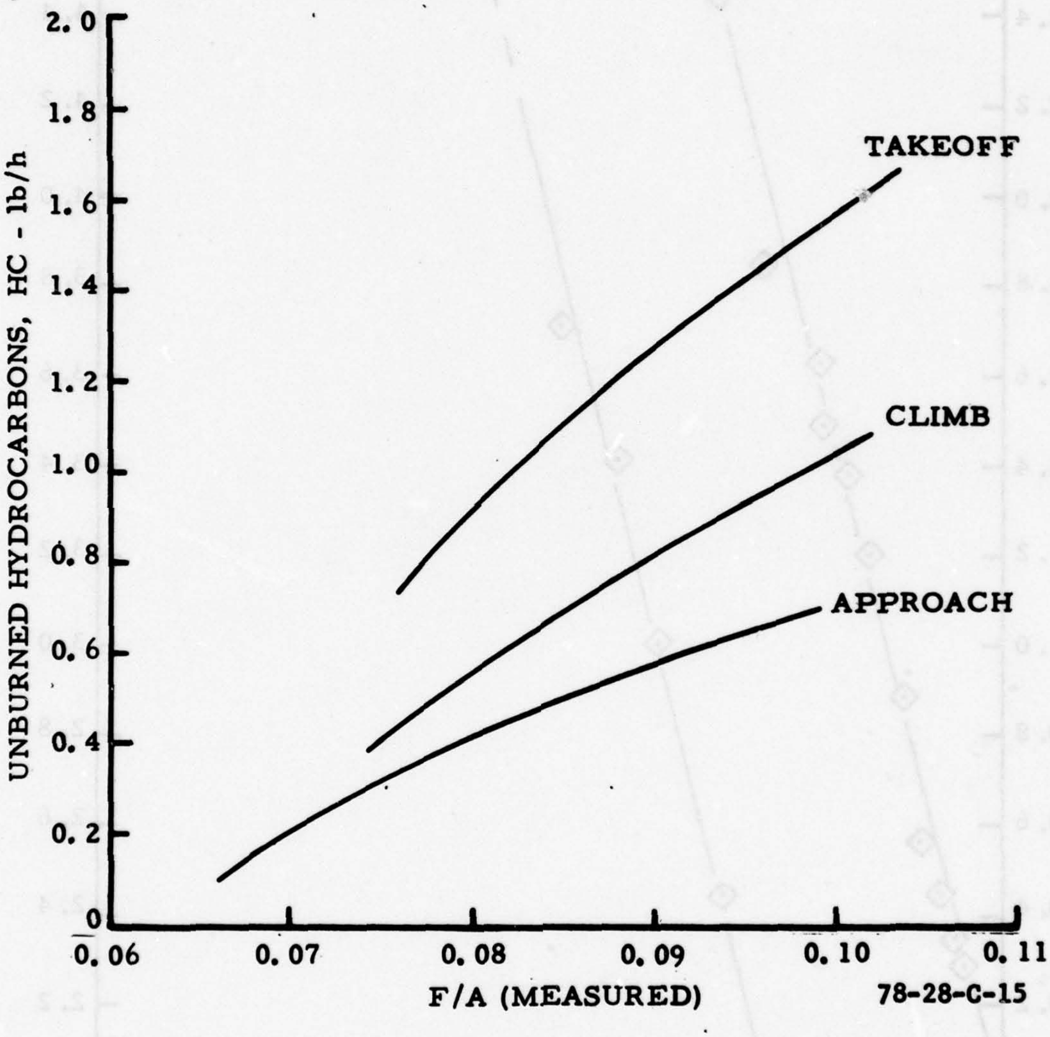

FIGURE C-17. SEA LEVEL HOT-DAY (T_i=103° F) EMISSIONS CHARACTERISTICS FOR AN AVCO LYCOMING IO-360-B1BD ENGINE--UNBURNED HYDROCARBONS

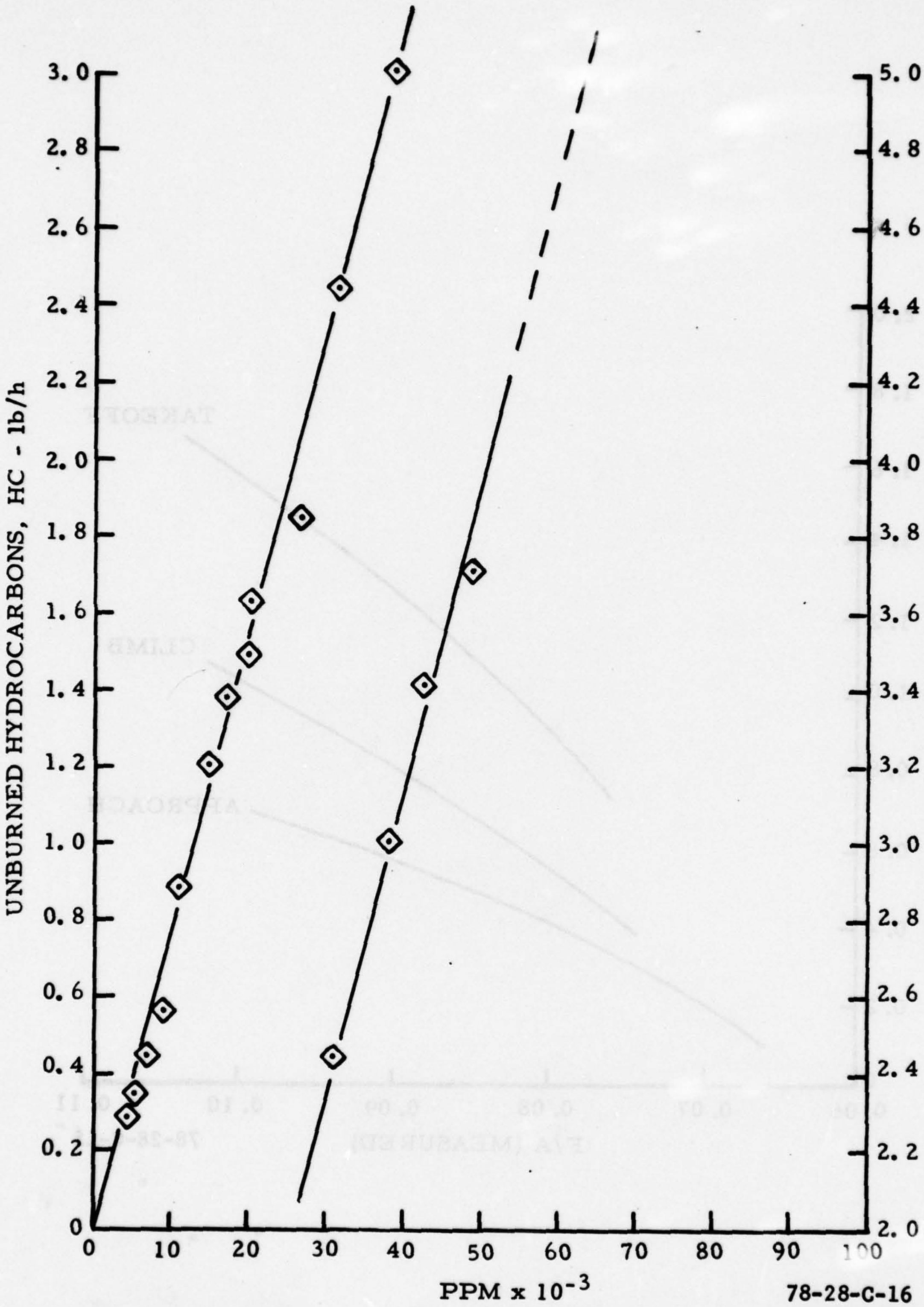

FIGURE C-18. A CALBRATION CURVE FOR TAXI MODE UNBURNED HYDROCARBONS--AVCO LYCOMING IO-360-B1BD ENGINE

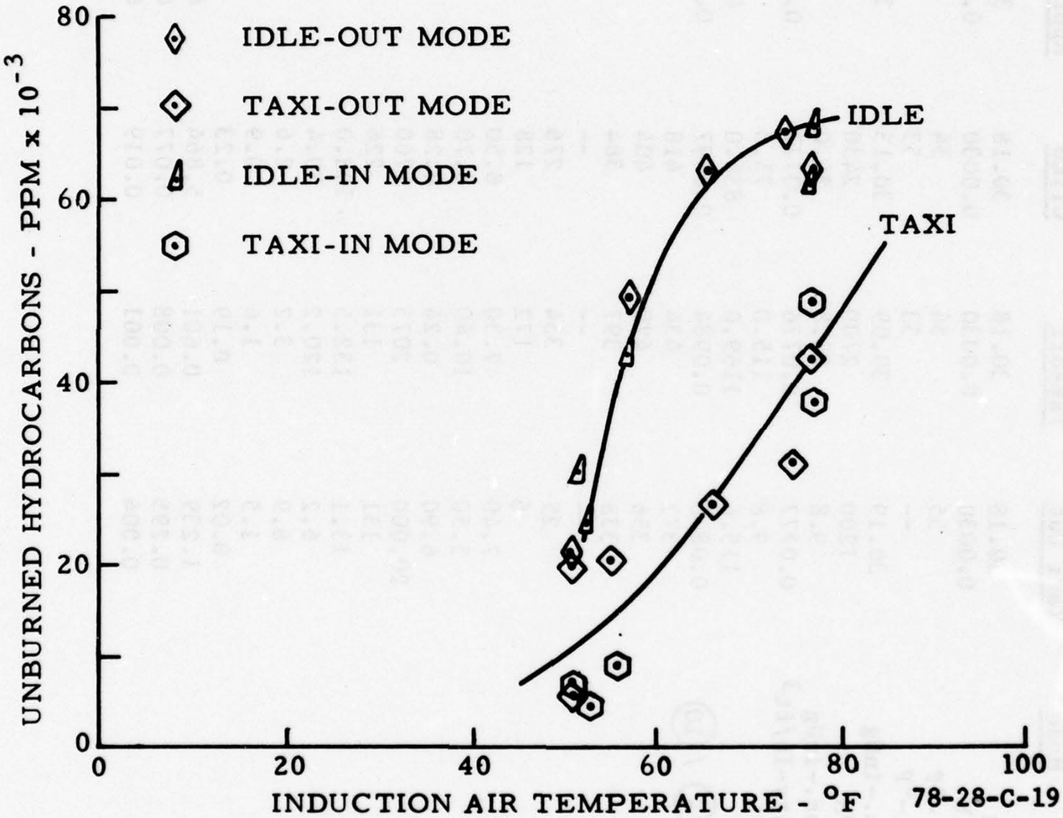

FIGURE C-19. EFFECTS OF INDUCTION AIR TEMPERATURE ON THE PRODUCTION OF EXHAUST UNBURNED HYDROCARBON EMISSIONS--AVCO LYCOMING IO-360-B1BD ENGINE

TABLE C-1. AVCO LYCOMING IO-360-B1BD ENGINE NAFEC TEST DATA--BASELINE 1
(NO IDLE, FIVE-MODE) SPARK SETTING 25° BTC

	Parameter	Run No. / Mode	2 Taxi Out	3 Takeoff	4 Climb	5 Approach	6 Taxi In
1.	Act. Baro. - inHg		30.18	30.18	30.18	30.18	30.16
2.	Spec. Hum. - lb/lb		0.0030	0.0030	0.0030	0.0030	0.0030
3.	Induct. Air Temp.-°F		55	54	54	54	53
4.	Cooling Air Temp.-°F		--	53	53	53	--
5.	Induct. Air Press.-inHg		30.19	30.09	30.13	30.17	30.19
6.	Engine Speed - RPM		1200	2700	2430	2350	1200
7.	Manifold Air Press.-inHg		9.8	28.8	26.0	17.0	8.6
8.	Induct. Air Density-lb/ft^3		0.0777	0.0776	0.0777	0.0780	0.0780
9.	Fuel Flow, W_f-lb/h		9.8	115.0	75.0	41.5	8.6
10.	Airflow, W_a-lb/h		115.6	1169.0	836.0	462.0	101.1
11.	F/A (Measured) = (9) / (10)		0.0848	0.0984	0.0897	0.0898	0.0850
12.	Max. Cht - °F		373	434	418	337	358
13.	Avg. Cht - °F		356	420	404	328	346
14.	Min. Cht - °F		338	397	384	317	332
15.	EGT - °F		--	--	--	--	--
16.	Torque, lb-ft		25	334	276	137	17
17.	Obs. Bhp		6	172	128	61	4
18.	% CO_2 (Dry)		7.40	7.30	8.50	8.10	7.80
19.	% CO (Dry)		5.50	10.40	8.70	9.20	8.80
20.	% O_2 (Dry)		6.90	0.24	0.28	0.36	1.40
21.	HC-p/m (Wet)		20,000	2075	1700	1950	4350
22.	NO_x-p/m (Wet)		131	131	226	112	44
23.	CO_2-lb/h		13.1	132.5	108.0	57.3	12.1
24.	CO-lb/h		6.2	120.2	70.4	41.4	8.7
25.	O_2-lb/h		8.9	3.2	2.6	1.9	1.6
26.	HC-lb/h		1.5	1.6	0.9	0.6	0.3
27.	NO_x-lb/h		0.02	0.19	0.23	0.06	0.005
28.	CO-lb/Mode		1.239	0.601	5.864	4.140	0.578
29.	HC-lb/Mode		0.295	0.008	0.077	0.059	0.019
30.	NO_x-lb/Mode		0.004	0.001	0.019	0.006	0.0004

TABLE C-2. AVCO LYCOMING IO-360-B1BD ENGINE NAFEC TEST DATA--BASELINE 2 (NO IDLE, FIVE-MODE) SPARK SETTING 25° BTC

	Parameter	Mode	Run No. 29 Taxi Out	30 Takeoff	31 Climb	32 Approach	33 Taxi In
1.	Act. Baro. - inHg		30.34	30.34	30.34	30.34	30.32
2.	Spec. Hum. - lb/lb		0.0020	0.0020	0.0020	0.0020	0.0015
3.	Induct. Air Temp.-°F		51	51	51	51	51
4.	Cooling Air Temp.-°F		--	53	53	53	--
5.	Induct. Air Press.-inHg		30.46	30.36	30.40	30.44	30.48
6.	Engine Speed - RPM		1200	2700	2430	2350	1200
7.	Manifold Air Press.-inHg		8.8	28.8	26.0	17.0	8.6
8.	Induct. Air Density-lb/ft^3		0.0797	0.0787	0.0788	0.0791	0.0791
9.	Fuel Flow, W_f-lb/h		9.8	116.0	77.0	42.0	9.2
10.	Airflow, W_a-lb/h		102.4	1187.0	858.0	496.0	102.5
11.	F/A (Measured) = (9) / (10)		0.0957	0.0977	0.0897	0.0847	0.0898
12.	Max. Cht - °F		384	435	417	334	327
13.	Avg. Cht - °F		374	420	400	324	317
14.	Min. Cht - °F		361	395	382	314	307
15.	EGT - °F		--	--	--	--	--
16.	Torque, lb-ft		--	338	280	144	--
17.	Obs. Bhp		--	174	129	64	--
18.	% CO_2 (Dry)		7.80	7.40	8.40	8.00	7.20
19.	% CO (Dry)		9.20	10.40	9.20	9.30	10.00
20.	% O_2 (Dry)		0.80	0.22	0.27	0.32	0.87
21.	HC-p/m (Wet)		5350	1825	1650	1975	6750
22.	NO_x-p/m (Wet)		53	124	180	130	32
23.	CO_2-lb/h		12.3	136.7	110.7	60.8	11.4
24.	CO-lb/h		9.2	122.3	77.2	45.0	10.1
25.	O_2-lb/h		0.9	3.0	2.6	1.8	1.0
26.	HC-lb/h		0.31	1.4	0.9	0.6	0.45
27.	NO_x-lb/h		0.007	0.18	0.19	0.08	0.004
28.	CO-lb/Mode		1.840	0.611	6.431	4.499	0.675
29.	HC-lb/Mode		0.061	0.007	0.077	0.062	0.030
30.	NO_x-lb/Mode		0.001	0.001	0.016	0.008	0.0003

TABLE C-3. AVCO LYCOMING IO-360-B1BD ENGINE NAFEC TEST DATA--BASELINE 3
(NO IDLE, FIVE-MODE) SPARK SETTING 25° BTC (DRY AIR)

	Run No.	140	141	142	143	144
Parameter	**Mode**	**Taxi Out**	**Takeoff**	**Climb**	**Approach**	**Taxi In**
1. Act. Baro. - inHg		29.84	29.84	29.84	29.84	29.84
2. Spec. Hum. - lb/lb		--	--	--	--	--
3. Induct. Air Temp.-°F		66	55	51	51	56
4. Cooling Air Temp.-°F		--	64	63	63	--
5. Induct. Air Press.-inHg		29.84	29.75	29.83	30.00	29.84
6. Engine Speed - RPM		1200	2700	2430	2350	1200
7. Manifold Air Press.-inHg		10.0	28.9	26.0	17.0	9.0
8. Induct. Air Density-lb/ft^3		0.0752	0.0766	0.0774	0.0778	0.0766
9. Fuel Flow, W_f-lb/h		10.6	112.0	75.0	41.0	10.0
10. Airflow, W_a-lb/h		107.0	1155.0	843.0	460.0	98.9
11. F/A (Measured) = (9) / (10)		0.0991	0.0970	0.0890	0.0891	0.1011
12. Max. Cht - °F		403	453	428	345	365
13. Avg. Cht - °F		379	438	411	338	356
14. Min. Cht - °F		366	415	394	324	347
15. EGT - °F		--	--	--	--	--
16. Torque, lb-ft		15	342	286	146	25
17. Obs. Bhp		3	176	132	65	6
18. % CO_2 (Dry)		6.20	7.40	8.20	8.00	9.60
19. % CO (Dry)		6.70	10.20	8.70	9.30	11.30
20. % O_2 (Dry)		5.80	0.20	0.22	0.28	1.00
21. HC-p/m (Wet)		26,250	1750	1550	1725	8850
22. NO_x-p/m (Wet)		133	156	245	164	22
23. CO_2-lb/h		10.1	132.5	104.9	56.5	15.5
24. CO-lb/h		7.0	116.3	70.8	41.8	11.6
25. O_2-lb/h		6.9	2.6	2.0	1.4	0.0
26. HC-lb/h		1.9	1.3	0.85	0.51	0.59
27. NO_x-lb/h		0.018	0.22	0.25	0.09	0.0026
28. CO-lb/Mode		1.392	0.581	5.904	4.178	0.775
29. HC-lb/Mode		0.377	0.007	0.071	0.051	0.039
30. NO_x-lb/Mode		0.004	0.001	0.021	0.009	0.0002

TABLE C-4. AVCO LYCOMING IO-360-B1BD ENGINE NAFEC TEST DATA--BASELINE 4 (NO IDLE, FIVE-MODE) SPARK SETTING 25° BTC

	Parameter	Run No. / Mode	174 Taxi Out	175 Takeoff	176 Climb	177 Approach	178 Taxi In
1.	Act. Baro. - inHg		29.74	29.74	29.74	29.74	29.74
2.	Spec. Hum. - lb/lb		0.0130	0.0130	0.0130	0.0130	0.0125
3.	Induct. Air Temp.-°F		75	76	77	77	77
4.	Cooling Air Temp.-°F		--	82	82	82	--
5.	Induct. Air Press.-inHg		29.54	29.63	29.77	29.88	29.65
6.	Engine Speed - RPM		1200	2700	2430	2350	1200
7.	Manifold Air Press.-inHg		10.6	28.9	26.0	17.0	10.7
8.	Induct. Air Density-lb/ft^3		0.0734	0.0733	0.0735	0.0737	0.0732
9.	Fuel Flow, W_f-lb/h		11.4	113.0	75.0	41.0	12.5
10.	Airflow, W_a-lb/h		120.0	1140.0	807.0	458.5	117.5
11.	F/A (Measured) = (9) / (10)		0.0950	0.0991	0.0929	0.0894	0.1064
12.	Max. Cht - °F		387	439	428	353	351
13.	Avg. Cht - °F		370	422	407	345	341
14.	Min. Cht - °F		358	401	391	334	332
15.	EGT - °F		--	--	--	--	--
16.	Torque, lb-ft		--	305	249	127	--
17.	Obs. Bhp		--	157	115	57	--
18.	% CO_2 (Dry)		6.10	6.90	7.90	7.60	5.90
19.	% CO (Dry)		6.60	11.30	9.80	10.00	6.80
20.	% O_2 (Dry)		5.00	0.20	0.23	0.32	6.00
21.	HC-p/m (Wet)		31,000	2075	1825	2100	38,000
22.	NO_x-p/m (Wet)		88	80	111	85	60
23.	CO_2-lb/h		10.9	122.7	97.4	53.4	10.5
24.	CO-lb/h		7.5	127.9	76.9	44.7	7.7
25.	O_2-lb/h		6.2	3.0	2.1	1.6	1.2
26.	HC-lb/h		2.5	1.6	0.97	0.62	3.1
27.	NO_x-lb/h		0.013	0.113	0.110	0.047	0.009
28.	CO-lb/Mode		1.498	0.640	6.411	4.469	0.511
29.	HC-lb/Mode		0.493	0.008	0.081	0.062	0.205
30.	NO_x-lb/Mode		0.003	0.001	0.009	0.005	0.001

TABLE C-5. AVCO LYCOMING IO-360-B1BD ENGINE NAFEC TEST DATA--BASELINE 5
(NO IDLE, FIVE-MODE) SPARK SETTING 25° BTC

	Run No.	181	182	183	184	185
Parameter	**Mode**	**Taxi Out**	**Takeoff**	**Climb**	**Approach**	**Taxi In**
1. Act. Baro. - inHg		29.73	29.73	29.73	29.73	29.73
2. Spec. Hum. - lb/lb		0.0125	0.0125	0.0125	0.0125	0.0125
3. Induct. Air Temp.-°F		77	77	77	77	77
4. Cooling Air Temp.-°F		--	82	82	82	--
5. Induct. Air Press.-inHg		29.61	29.62	29.76	29.88	29.65
6. Engine Speed - RPM		1200	2700	2430	2350	1200
7. Manifold Air Press.-inHg		10.7	28.9	26.0	17.0	10.3
8. Induct. Air Density-lb/ft^3		0.0731	0.0731	0.0734	0.0737	0.0732
9. Fuel Flow, W_f-lb/h		12.2	113.0	74.0	39.5	12.2
10. Airflow, W_a-lb/h		123.1	1138.0	806.5	432.0	115.5
11. F/A (Measured) = (9) / (10)		0.0992	0.0993	0.0918	0.0914	0.1061
12. Max. Cht - °F		383	432	425	355	341
13. Avg. Cht - °F		361	416	407	348	332
14. Min. Cht - °F		349	396	391	338	324
15. EGT - °F		--	--	--	--	--
16. Torque, lb-ft		24	313	258	135	25
17. Obs. Bhp		6	161	119	60	6
18. % CO_2 (Dry)		5.20	6.70	7.70	7.30	5.20
19. % CO (Dry)		6.80	11.40	9.60	10.00	6.70
20. % O_2 (Dry)		5.90	0.19	0.23	0.28	7.00
21. HC-p/m (Wet)		42,250	2075	1775	1950	48,500
22. NO_x-p/m (Wet)		73	83	141	95	90
23. CO_2-lb/h		9.5	119.0	94.3	48.1	9.0
24. CO-lb/h		7.9	128.8	74.7	41.9	7.4
25. O_2-lb/h		7.9	2.5	2.1	1.3	8.8
26. HC-lb/h		3.5	1.6	0.94	0.55	3.8
27. NO_x-lb/h		0.011	0.119	0.139	0.050	0.013
28. CO-lb/Mode		1.589	0.644	6.236	4.194	0.494
29. HC-lb/Mode		0.698	0.008	0.078	0.055	0.256
30. NO_x-lb/Mode		0.002	0.001	0.012	0.005	0.001

TABLE C-6. AVCO LYCOMING IO-360-B1BD ENGINE NAFEC TEST DATA--TAKEOFF MODE--SPARK SETTING 25° BTC

	Parameter	Mode / Run No.	16	17	18	19
			Takeoff	Takeoff	Takeoff	Takeoff
1.	Act. Baro. - inHg		30.34	30.34	30.34	30.34
2.	Spec. Hum. - lb/lb		0.0050	0.0050	0.0050	0.0050
3.	Induct. Air Temp.-°F		53	52	52	52
4.	Cooling Air Temp.-°F		52	52	52	52
5.	Induct. Air Press.-inHg		30.10	30.11	30.10	30.11
6.	Engine Speed - RPM		2700	2700	2700	2700
7.	Manifold Air Press.-inHg		28.8	28.8	28.8	28.8
8.	Induct. Air Density-lb/ft^3		0.0778	0.0779	0.0779	0.0779
9.	Fuel Flow, W_f-lb/h		116.0	111.0	106.0	101.0
10.	Airflow, W_a-lb/h		1180.0	1174.0	1180.5	1167.5
11.	F/A (Measured) = (9) / (10)		0.0983	0.0945	0.0898	0.0865
12.	Max. Cht - °F		430	441	454	465
13.	Avg. Cht - °F		416	427	440	451
14.	Min. Cht - °F		390	403	414	425
15.	EGT - °F		--	--	--	--
16.	Torque, lb-ft		335	340	340	343
17.	Obs. Bhp		172	175	175	176
18.	% CO_2 (Dry)		7.50	8.10	8.60	9.50
19.	% CO (Dry)		10.60	9.70	8.90	7.70
20.	% O_2 (Dry)		0.22	0.27	0.28	0.26
21.	HC-p/m (Wet)		1800	1675	1550	1425
22.	NO_x-p/m (Wet)		126	170	215	310
23.	CO_2-lb/h		137.8	146.7	154.8	165.6
24.	CO-lb/h		122.7	111.8	102.0	85.4
25.	O_2-lb/h		2.9	3.6	3.7	3.3
26.	HC-lb/h		1.4	1.3	1.2	1.1
27.	NO_x-lb/h		0.19	0.25	0.31	0.44
28.	CO-lb/Mode		0.614	0.559	0.510	0.427
29.	HC-lb/Mode		0.007	0.006	0.006	0.005
30.	NO_x-lb/Mode		0.001	0.001	0.002	0.002

TABLE C-7. AVCO LYCOMING IO-360-B1BD ENGINE NAFEC TEST DATA--TAKEOFF MODE--SPARK SETTING 25° BTC

Parameter	Mode / Run No.	103	104	105	106
		Takeoff	Takeoff	Takeoff	Takeoff
1. Act. Baro. - inHg		29.96	29.96	29.96	29.96
2. Spec. Hum. - lb/lb		0.0050	0.0050	0.0050	0.0050
3. Induct. Air Temp.-°F		99	105	108	109
4. Cooling Air Temp.-°F		106	107	109	109
5. Induct. Air Press.-inHg		29.96	29.96	29.96	29.96
6. Engine Speed - RPM		2700	2700	2700	2700
7. Manifold Air Press.-inHg		29.0	29.0	29.0	29.0
8. Induct. Air Density-lb/ft^3		0.0710	0.0703	0.0699	0.0698
9. Fuel Flow, W_f-lb/h		116.0	111.0	106.0	101.0
10. Airflow, W_a-lb/h		1142.0	1136.0	1133.0	1132.0
11. F/A (Measured) = (9) / (10)		0.1016	0.0977	0.0936	0.0892
12. Max. Cht - °F		438	456	469	482
13. Avg. Cht - °F		426	442	453	468
14. Min. Cht - °F		405	420	432	444
15. EGT - °F		--	--	--	--
16. Torque, lb-ft		316	320	317	322
17. Obs. Bhp		162	165	163	166
18. % CO_2 (Dry)		6.30	6.90	7.40	8.20
19. % CO (Dry)		11.70	10.80	10.20	9.00
20. % O_2 (Dry)		0.70	0.26	0.24	0.24
21. HC-p/m (Wet)		2125	1925	1875	1725
22. NO_x-p/m (Wet)		85	119	151	250
23. CO_2-lb/h		114.0	121.9	129.4	141.1
24. CO-lb/h		134.8	121.4	113.6	98.6
25. O_2-lb/h		9.2	3.3	3.1	3.0
26. HC-lb/h		1.6	1.5	1.4	1.3
27. NO_x-lb/h		0.12	0.17	0.21	0.34
28. CO-lb/Mode		0.674	0.607	0.568	0.493
29. HC-lb/Mode		0.008	0.007	0.007	0.006
30. NO_x-lb/Mode		0.001	0.001	0.001	0.002

TABLE C-8. AVCO LYCOMING IO-360-B1BD ENGINE NAFEC TEST DATA--CLIMB MODE--SPARK SETTING 25° BTC

	Parameter	Run No.	20	21	22	23
		Mode	Climb	Climb	Climb	Climb
1.	Act. Baro. - inHg		30.34	30.34	30.34	30.34
2.	Spec. Hum. - lb/lb		0.0050	0.0050	0.0050	0.0050
3.	Induct. Air Temp.-°F		52	52	52	52
4.	Cooling Air Temp.-°F		52	53	53	53
5.	Induct. Air Press.-inHg		30.30	30.30	30.31	30.31
6.	Engine Speed - RPM		2430	2430	2430	2430
7.	Manifold Air Press.-inHg		26.0	26.0	26.0	26.0
8.	Induct. Air Density-lb/ft^3		0.0784	0.0784	0.0785	0.0785
9.	Fuel Flow, W_f-lb/h		77.0	73.0	69.0	65.0
10.	Airflow, W_a-lb/h		864.5	837.5	847.0	847.0
11.	F/A (Measured) = (9) / (10)		0.0891	0.0872	0.0815	0.0767
12.	Max. Cht - °F		417	420	430	437
13.	Avg. Cht - °F		398	404	416	426
14.	Min. Cht - °F		384	387	400	408
15.	EGT - °F		--	--	--	--
16.	Torque, lb-ft		282	282	285	284
17.	Obs. Bhp		130	130	132	131
18.	% CO_2 (Dry)		8.40	9.40	10.20	11.40
19.	% CO (Dry)		9.00	7.70	6.40	4.90
20.	% O_2 (Dry)		0.28	0.26	0.26	0.27
21.	HC-p/m (Wet)		1700	1500	1325	1125
22.	NO_x-p/m (Wet)		194	295	470	830
23.	CO_2-lb/h		110.7	118.3	127.8	141.1
24.	CO-lb/h		75.5	61.7	51.1	38.6
25.	O_2-lb/h		2.7	2.4	2.4	2.4
26.	HC-lb/h		1.0	0.8	0.7	0.6
27.	NO_x-lb/h		0.20	0.30	0.48	0.82
28.	CO-lb/Mode		6.293	5.138	4.255	3.217
29.	HC-lb/Mode		0.079	0.067	0.059	0.049
30.	NO_x-lb/Mode		0.017	0.025	0.039	0.068

TABLE C-9. AVCO LYCOMING IO-360-B1BD ENGINE NAFEC TEST DATA—CLIMB MODE--SPARK SETTING 25° BTC (DRY AIR)

Parameter	Run No. / Mode	150 Climb	151 Climb	152 Climb	153 Climb
1. Act. Baro. - inHg		29.95	29.95	29.95	29.95
2. Spec. Hum. - lb/lb		--	--	--	--
3. Induct. Air Temp.-°F		50	46	43	42
4. Cooling Air Temp.-°F		65	65	65	65
5. Induct. Air Press.-inHg		29.95	29.95	29.98	29.99
6. Engine Speed - RPM		2430	2430	2430	2430
7. Manifold Air Press.-inHg		26.0	26.0	26.0	26.0
8. Induct. Air Density-lb/ft^3		0.0778	0.0784	0.0790	0.0792
9. Fuel Flow, Wf-lb/h		72.0	68.0	63.0	60.0
10. Airflow, W_a-lb/h		830.5	818.5	791.0	775.0
11. F/A (Measured) = (9) / (10)		0.0867	0.0831	0.0796	0.0773
12. Max. Cht - °F		423	436	451	456
13. Avg. Cht - °F		404	418	432	441
14. Min. Cht - °F		384	400	416	426
15. EGT - °F		--	--	--	--
16. Torque, lb-ft		285	288	288	286
17. Obs. Bhp		132	133	133	132
18. % CO_2 (Dry)		8.50	9.50	11.20	12.40
19. % CO (Dry)		8.60	7.20	5.10	3.50
20. % O_2 (Dry)		0.30	0.22	0.24	0.26
21. HC-p/m (Wet)		1800	1600	1325	1125
22. NO_x-p/m (Wet)		230	380	850	1200
23. CO_2-lb/h		107.5	116.3	130.2	139.7
24. CO-lb/h		69.2	56.1	37.7	25.1
25. O_2-lb/h		2.8	2.0	2.0	2.1
26. HC-lb/h		0.96	0.83	0.66	0.54
27. NO_x-lb/h		0.23	0.37	0.79	1.08
28. CO-lb/Mode		5.766	4.676	3.145	2.091
29. HC-lb/Mode		0.080	0.069	0.055	0.045
30. NO_x-lb/Mode		0.019	0.031	0.066	0.090

TABLE C-10. AVCO LYCOMING IO-360-B1BD ENGINE NAFEC TEST DATA--APPROACH MODE--SPARK SETTING 25° BTC

Parameter	Run No. / Mode	24 Approach	25 Approach	26 Approach	27 Approach
1.	Act. Baro. - inHg	30.32	30.32	30.32	30.32
2.	Spec. Hum. - lb/lb	0.0050	0.0050	0.0050	0.0050
3.	Induct. Air Temp.-°F	52	52	52	52
4.	Cooling Air Temp.-°F	54	54	53	53
5.	Induct. Air Press.-inHg	30.44	30.45	30.45	30.45
6.	Engine Speed - RPM	2350	2350	2350	2350
7.	Manifold Air Press.-inHg	17.0	17.0	17.1	17.0
8.	Induct. Air Density-lb/ft^3	0.0788	0.0788	0.0788	0.0788
9.	Fuel Flow, W_f-lb/h	44.0	40.0	36.0	32.0
10.	Airflow, W_a-lb/h	495.0	479.5	479.5	463.0
11.	F/A (Measured) = (9) / (10)	0.0889	0.0834	0.0751	0.0691
12.	Max. Cht - °F	332	342	351	356
13.	Avg. Cht - °F	322	332	341	347
14.	Min. Cht - °F	310	321	328	334
15.	EGT - °F	--	--	--	--
16.	Torque, lb-ft	133	143	143	136
17.	Obs. Bhp	64	64	64	61
18.	% CO_2 (Dry)	8.00	9.60	10.40	13.70
19.	% CO (Dry)	9.30	7.20	4.30	1.40
20.	% O_2 (Dry)	0.32	0.30	0.29	.28
21.	HC-p/m (Wet)	1650	1450	1300	585
22.	NO_x-p/m (Wet)	96	190	520	1075
23.	CO_2-lb/h	60.5	68.7	73.7	89.9
24.	CO-lb/h	44.8	32.8	19.4	5.9
25.	O_2-lb/h	1.8	1.6	1.5	1.3
26.	HC-lb/h	0.53	0.44	0.38	0.16
27.	NO_x-lb/h	0.06	0.11	0.29	0.56
28.	CO-lb/Mode	4.476	3.280	1.940	0.585
29.	HC-lb/Mode	0.053	0.044	0.038	0.016
30.	NO_x-lb/Mode	0.006	0.011	0.029	0.056

TABLE C-11. AVCO LYCOMING IO-360-B1BD ENGINE NAFEC TEST DATA--APPROACH MODE--SPARK SETTING 25° BTC (DRY AIR)

Parameter	Run No. 154	155	156	157
Mode	Approach	Approach	Approach	Approach
1. Act. Baro. - inHg	29.95	29.95	29.95	29.95
2. Spec. Hum. - lb/lb	--	--	--	--
3. Induct. Air Temp.-°F	61	58	55	52
4. Cooling Air Temp.-°F	67	67	66	66
5. Induct. Air Press.-inHg	30.09	30.10	30.10	30.10
6. Engine Speed - RPM	2350	2350	2350	2350
7. Manifold Air Press.-inHg	17.1	17.0	17.1	17.0
8. Induct. Air Density-lb/ft^3	0.0765	0.0770	0.0775	0.0779
9. Fuel Flow, W_f-lb/h	40.5	36.5	32.5	28.5
10. Airflow, W_a-lb/h	466.9	468.5	470.0	444.0
11. F/A (Measured) = (9) / (10)	0.0867	0.0779	0.0691	0.0642
12. Max. Cht - °F	323	331	341	326
13. Avg. Cht - °F	314	322	332	321
14. Min. Cht - °F	307	314	322	311
15. EGT - °F	--	--	--	--
16. Torque, lb-ft	150	151	148	124
17. Obs. Bhp	67	68	66	55.5
18. % CO_2 (Dry)	8.60	10.70	13.50	13.30
19. % CO (Dry)	8.60	5.30	1.60	0.10
20. % O_2 (Dry)	0.30	0.30	0.32	1.60
21. HC-p/m (Wet)	1925	1575	875	100
22. NO_x-p/m (Wet)	199	545	1075	925
23. CO_2-lb/h	61.2	73.5	90.5	83.3
24. CO-lb/h	38.9	23.2	6.8	0.4
25. O_2-lb/h	1.6	1.5	1.6	7.3
26. HC-lb/h	0.58	0.46	0.25	0.03
27. NO_x-lb/h	0.11	0.30	0.57	0.46
28. CO-lb/Mode	3.895	2.318	0.683	0.040
29. HC-lb/Mode	0.058	0.046	0.025	0.003
30. NO_x-lb/Mode	0.011	0.030	0.057	0.046

TABLE C-12. AVCO LYCOMING IO-360-B1BD ENGINE NAFEC TEST DATA--APPROACH MODE--SPARK SETTING 25° BTC

	Parameter	Run No.	111	112	113	114
		Mode	Approach	Approach	Approach	Approach
1.	Act. Baro. - inHg		29.95	29.95	29.95	29.95
2.	Spec. Hum. - lb/lb		0.0075	0.0075	0.0075	0.0075
3.	Induct. Air Temp.-°F		91	96	99	102
4.	Cooling Air Temp.-°F		105	106	108	110
5.	Induct. Air Press.-inHg		30.20	30.20	30.20	30.20
6.	Engine Speed - RPM		2350	2350	2350	2350
7.	Manifold Air Press.-inHg		17.0	17.0	17.1	17.0
8.	Induct. Air Density-lb/ft^3		0.0726	0.0720	0.0716	0.0712
9.	Fuel Flow, W_f-lb/h		41.0	37.0	33.0	29.0
10.	Airflow, W_a-lb/h		455.0	477.5	476.0	475.0
11.	F/A (Measured) = (9) / (10)		0.0901	0.0775	0.0693	0.0611
12.	Max. Cht - °F		354	369	384	389
13.	Avg. Cht - °F		348	361	375	383
14.	Min. Cht - °F		336	348	361	368
15.	EGT - °F		--	--	--	--
16.	Torque, lb-ft		132	140	137	134
17.	Obs. Bhp		59	63	61	60
18.	% CO_2 (Dry)		7.70	9.60	11.80	14.10
19.	% CO (Dry)		9.60	6.90	4.20	0.60
20.	% O_2 (Dry)		0.32	0.31	0.24	0.44
21.	HC-p/m (Wet)		1750	1475	1150	345
22.	NO_x-p/m (Wet)		140	320	840	1575
23.	CO_2-lb/h		53.5	67.8	81.3	94.2
24.	CO-lb/h		42.5	31.0	18.4	2.9
25.	O_2-lb/h		1.6	1.6	1.2	2.1
26.	HC-lb/h		0.52	0.44	0.33	0.10
27.	NO_x-lb/h		0.08	0.18	0.45	0.84
28.	CO-lb/Mode		4.247	3.103	1.841	0.255
29.	HC-lb/Mode		0.052	0.044	0.033	0.010
30.	NO_x-lb/Mode		0.008	0.018	0.045	0.084

TABLE C-13. AVCO LYCOMING IO-360-B1BD ENGINE NAFEC TEST DATA--TAXI MODE (16 MIN)--SPARK SETTING 25° BTC (DRY AIR)

Parameter	Run No.	162	163	164	165
	Mode	Taxi	Taxi	Taxi	Taxi
1. Act. Baro. - inHg		30.01	30.01	30.01	30.01
2. Spec. Hum. - lb/lb		--	--	--	--
3. Induct. Air Temp.-°F		55	55	55	56
4. Cooling Air Temp.-°F		--	--	--	--
5. Induct. Air Press.-inHg		30.06	30.05	30.04	30.05
6. Engine Speed - RPM		1200	1200	1200	1200
7. Manifold Air Press.-inHg		8.8	9.0	9.0	9.0
8. Induct. Air Density-lb/ft^3		0.0774	0.0773	0.0773	0.0772
9. Fuel Flow, W_f-lb/h		8.3	8.6	9.0	9.0
10. Airflow, W_a-lb/h		98.4	99.3	100.3	99.3
11. F/A (Measured) = (9) / (10)		0.0843	0.0866	0.0897	0.0906
12. Max. Cht - °F		409	420	414	414
13. Avg. Cht - °F		383	397	393	393
14. Min. Cht - °F		367	375	375	371
15. EGT - °F		--	--	--	--
16. Torque, lb-ft		16	16	16	16
17. Obs. Bhp		4	4	4	4
18. % CO_2 (Dry)		7.90	7.30	7.60	7.10
19. % CO (Dry)		8.60	9.60	9.10	9.70
20. % O_2 (Dry)		0.74	0.74	0.75	0.72
21. HC-p/m (Wet)		4800	6250	4950	5330
22. NO_x-p/m (Wet)		58	47	52	41
23. CO_2-lb/h		11.8	11.2	11.7	10.9
24. CO-lb/h		8.2	9.3	8.9	9.4
25. O_2-lb/h		0.8	0.8	0.8	0.8
26. HC-lb/h		0.30	0.40	0.32	0.345
27. NO_x-lb/h		0.007	0.006	0.006	0.005
28. CO-lb/Mode		2.182	2.491	2.369	2.516
29. HC-lb/Mode		0.080	0.106	0.086	0.092
30. NO_x-lb/Mode		0.002	0.002	0.002	0.001

TABLE C-14. TOTAL EMISSIONS CHARACTERISTICS AVCO LYCOMING IO-360-B1BD ENGINE (S/N887-X)--SEA LEVEL STANDARD DAY

	Modes	CO lb/h	CO lb/Mode	HC lb/h	HC lb/Mode	NO_x lb/h	NO_x lb/Mode	F/A	Max. CHT-°F
1	Taxi (16.0-Min.)	9.50	2.5333	1.64	0.4373	-0-	-0-	0.0925	
2	Takeoff (0.3-Min.)	128.00	0.6400	1.48	0.0074	0.120	0.0006	0.0990	435
3	Climb (5.0-Min.)	80.00	6.6667	0.9500	0.0792	0.190	0.0158	0.0925	420
4	Approach (6.0-Min.)	50.00	5.0000	0.600	0.0600	0.050	0.0050	0.0925	335
5	lb/Cycle		14.8400		0.5839		0.0214		
6	lb/Cycle/RBHP		0.0824		0.00324		0.00012		
7	Federal Limit		0.0420		0.0019		0.0015		
8	Diff. = ⑥ - ⑦		+.0404		+.00134		-.00138		
9	(⑧ ÷ ⑦)x100		96.3		70.5		92.0		
10	% of STD = ⑨ +100		196.3		170.5		8.0		

TABLE C-15. TOTAL EMISSIONS CHARACTERISTICS AVCO LYCOMING IO-360-B1BD ENGINE (S/N887-X)--SEA LEVEL HOT DAY (T_i=103° F, INDUCTION AIR DENSITY=0.0706 lb/ft^3)

	Modes	CO lb/h	CO lb/Mode	HC lb/h	HC lb/Mode	NO_x lb/h	NO_x lb/h	F/A	Max. CHT-°F
1	Taxi (16.0-Min.)	11.0	2.9333	4.3000	1.1467	-0-	-0-	0.0980	
2	Takeoff (0.3-Min.)	136.0	0.6800	1.6200	0.0081	-0-	-0-	0.1020	435
3	Climb (5.0Min.)	87.0	7.2500	1.0000	0.0833	0.1450	0.0121	0.0980	420
4	Approach (6.0-Min.)	48.0	4.8000	0.6800	0.0680	-0-	-0-	0.0980	335
5	lb/Cycle		15.6633		1.3061		0.0121		
6	lb/Cycle/RBHP		0.0870		0.0073		0.00007		
7	Federal Limit		0.0420		0.0019		0.00150		
8	Diff. = ⑥ - ⑦		+.0450		+.0054		-.00143		
9	(⑧ ÷ ⑦)x100		107.1		281.9		-95.5		
10	% of STD = ⑨+100		207.1		381.9		4.5		

TABLE C-16. ARITHEMATIC AVERAGING OF BASELINE DATA AVCO LYCOMING IO-360-B1BD ENGINE

Baseline No.	CO (lb/cycle/RBHP)	HC lb/cycle/RBHP	NO_x lb/cycle/RBHP	Avg. cycle T_i (°F)
1	0.0690	0.00254	0.00017	54
2	0.0781	0.00132	0.00015	51
3	0.0713	0.00303	0.00020	58
4	0.0752	0.00472	0.00011	76
5	0.0731	0.00608	0.00012	77
Avg. Baseline	0.0733	0.00354	0.00015	63
Fed. STD.	0.0420	0.00190	0.0015	
% of STD.	174.5	186.3	10.0	63

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