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THE TEARING OF WEATHERED RUBBER-COATED FABRICS

by

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### SUMMARY

The wing-rip tear strengths of a nylon and of a cotton fabric, each coated with natural rubber, neoprene, polyurethane or chlorosulphonated polyethylene and exposed to various weathering conditions, were determined.

The coated nylon fabrics had higher tear strengths than the cotton ones, but were more variable. Polyurethane-coated nylon increased in tear strength on exposure at two Australian sites, but natural rubber coated cotton decreased on exposure in UK. Load during exposure reduced the tear strengths of the natural rubber coated fabrics.

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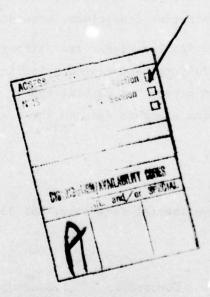
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### INTRODUCTION

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The exposure of rubber-coated fabrics for up to one year of weathering and the effects of this on their flexibilities, strengths and breaking extensions have previously been reported  $^{1,2}$ .

In a collaborative trial involving several Establishments of MOD(PE) and the Joint Tropical Research Unit (JTRU), nylon and cotton base fabrics of similar mass per unit area were coated with natural, neoprene, polyurethane (PU) or chlorosulphonated polyethylene (CSPE) rubbers. These coated fabrics were exposed for three, six or twelve months, and a second period of six months (6S) commencing at the end of the first, under loads of 1% or 10% of the nominal breaking strengths. Pieces of fabric were positioned at 45° to the horizontal and facing the equator at a site in the UK (PERME, Waltham Abbey, referred to as ERDE in the earlier reports) and at two sites in Queensland (hot, dry at Cloncurry and hot, wet, cleared jungle at Innisfail).

The coated nylon fabrics were found to be thicker, heavier and less flexible than the coated cotton fabrics; PU rubber, particularly on nylon, stiffened more than the other rubbers during exposure. The coated nylon fabrics were stronger and more extensible than the cotton ones, but those coated with natural rubber lost strength and extension at a faster rate when exposed under load. Nylon coated with PU was initially stronger and more extensible than when coated with the other rubbers, but lost these properties faster at Innisfail. Extension was more severely affected than strength by load during exposure.

The present Report gives the results and their analyses for the wing-rip tear strengths of these coated fabrics on weathering.

### 2 DETERMINATION OF TEAR STRENGTHS

The wing-rip tear strengths, the preferred British Standard method at slow speeds, were determined in accordance with the standard<sup>3</sup>, except that the rate of jaw separation was 5 cm/min instead of 10 cm/min and that only two test pieces were available per condition, both for tearing across warp threads, instead of five (except in the original controls, though to maintain uniformity in the subsequent processing of the results, the first two recorded were those used).

A 15cm cut was made across the warp in each test piece, of which the dimensions were 12.5 cm warpway  $\times$  20 cm weftway. Lines at angles of 55° to the

cut were marked on both tails, which were then inserted into the jaws of a recording tensile testing machine, with the marks along the edges of the jaws; the machine was situated in a room at  $20^{\circ}$ C and 65% relative humidity and test pieces were conditioned in this atmosphere for at least 24 h before testing. Ignoring the first peak in each tear trace, the median and maximum forces were recorded.

Most specimens gave satisfactory tears, except that in eight cases, where the tear strength was high, there was thread slippage or coating flaking. Nevertheless, tear values were obtained in all cases, and these were used in the subsequent analyses.

The uncoated cotton fabric had a median tear strength of 5.1 N, and a maximum of 7.1 N. The uncoated nylon fabric had a median tear strength of 100 N, and a maximum of 255 N.

### **3 ARRANGEMENT OF RESULTS**

The median and maximum tear strengths for each condition are given in Tables 1 and 2 respectively, the duplicate results referring to replication. The determinations were inevitably separated in time of determination by well over a year, and some were not made until more than two years after the end of the exposures. The effect of this on the conclusions is not known.

As noted previously<sup>1,2</sup>, the three month specimens from Australia were not differentiated as to their loading conditions; the columns containing the lower nylon/natural rubber tear strengths were therefore ascribed, as with breaking strength, to the 10% loading.

The tear strengths were divided into the same nine sets as for the breaking strengths<sup>2</sup>, it not being possible to consider the results as a whole because of specimen losses. Since the median and maximum tear strengths were closely correlated (correlation coefficient = 0.996, slope = 1.18), only median strengths were analysed in detail. The 368 usable values were analysed by computer using the following columns from Table 1:

Set	No.of columns in set	Columns from Table 1 used	Brief description <sup>1</sup>
(a)	2	A, B	Controls
(b)	6	C, D, K, L, S, T	3 months
(c)	12	C, E, G, I, K, M	17
	an antice shares an	0, Q, S, U, W, Y	
(d)	24	C-Z	Natural rubber
(e)	8	C-J	PERME
(f)	6	A, B, C, E, G, I	PERME, 1%, with controls
(g)	6	A, B, K, M, O, Q	Cloncurry, 17, with controls
(h)	6	A, B, S, U, W, Y	Innisfail, 1%, with controls
(i)	24	C-Z	Nylon with 3 rubbers

However, because the variability of the nylon fabrics was significantly greater than that of the cotton (see section 4.1), the analysis of variance assumption that the error was randomly-distributed over all the results was strained. Thus significant cotton effects could be missed, and unjustifiably significant conclusions might be drawn for the nylon fabrics. The nylon and cotton results were therefore treated separately, though the combined analysis was also performed for additional effects not obtainable in the separate analyses, making 24 altogether  $(3 \times 8 + \text{set (i)})$  which contained only nylon nylon results from set (d) which were obtainable from set (i)).

### 4 RESULTS AND DISCUSSION

### 4.1 Analysis of errors

005

The variances, standard deviations and degrees of freedom of the errors are given in Table 3. The nylon/cotton error variance ratios were significant in all the sets, necessitating separate analyses (see section 3). There was little evidence for differences in variability between the sets, however: for nylon, the highest variance ratio was 3.8 for (g)/(e); and for cotton, 4.4 for (a)/(b).

The means and coefficients of variation are also given in Table 3. Both measures were smaller for cotton than for nylon. Overall, the coefficients for tear strength were slightly higher than for breaking strength<sup>2</sup> but as there were no separate analyses for nylon and cotton breaking strengths, separate comparisons could not be made.

### 4.2 Analysis of median tear strengths

### 4.2.1 General

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Variance ratios derived from analysis of variance within each set are given in Table 4. The effects are discussed below in their order of occurrence in the tables, it not being possible to base them on order of importance because this differed widely in the various sets. Only those effects which had better than 99.9% probability of being correct were considered.

The means of the median tear strengths for each effect are given in Table 5. These are given complete, since it was found that most were important in at least one set, and it was felt that there might be confusion if results were omitted in some cases.

The differences between pairs of means required for significance at 99.9% probability are given in Table 6.

The variance ratios in Table 4 for the interactions of fabric with the other factors were obtainable only from the overall analyses. The means in Table 5 for the fabric interactions were those from which the effects for the individual base fabrics were derived.

### 4.2.2 Effect of fabric (F)

This was obtainable only from the overall analysis. The variance ratios were upwards of 500, with the coated nylon fabrics always having higher tear strengths than the cotton: this tear strength ratio in set (a) was 5.4; in sets (c), (g) and (h), which included the longer exposures and the Australian sites, it rose to about 7 (*cf* FT and FS below).

### 4.2.3 Effect of rubber (R) and fabric × rubber interaction (FR)

These were important in all the sets except (a) and (i). The effect on the nylon-based fabrics was greater than for the cotton ones in sets (c), (g) and (h), and greater for cotton than for nylon in sets (b), (e) and (f). This was due mainly to an increased tear strength on weathering for the PU-coated nylon, particularly at the Australian sites, and a decreased tear strength on weathering for natural rubber coated cotton at PERME (*cf* RS and TS below). Because the coating tended to come off the weathered PU-coated nylon during the tear tests, its tear strength approached that of uncoated nylon (section 2).

### 4.2.4 Effect of time (T) and fabric × time interaction (FT)

These were important in all sets except (a) and (i). In sets (d), (e) and (f) there was a tendency for tear strength to decrease with time, because of the

effect on natural rubber coated cotton, particularly at PERME; in sets (c), (g) and (h), there was a tendency to increase, because of the effect on PU-coated nylon, particularly at the Australian sites (cf RS and TS).

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### 4.2.5 Effect of load (L) and fabric × load interaction (FL)

In set (b), *ie* at short times, these were of no importance, but in (d), (e) and (i) the higher load caused some significant loss of tear strength in the nylon fabrics.

### 4.2.6 Effect of site (S) and fabric × site interaction (FS)

In set (b), the coated nylon fabrics at Cloncurry had lower tear strengths than at the other sites; with set (c), the coated nylon fabrics had higher tear strengths at Cloncurry and Innisfail than at PERME, this being due to the effects on PU-coated nylon at the longer times. For set (d), the natural rubber coated nylon fabrics were not significantly affected by the site, but the natural rubber coated cotton at PERME suffered losses in tear strength. In set (i), which did not include PU or cotton, there was no significant effect of site (cf RS).

### 4.2.7 <u>Rubber × time interaction (RT) and fabric × rubber × time</u> interaction (FRT)

In sets (a) and (i) these were of little importance. However, in (c), the PU-coated nylon fabric increased in tear strength with time of exposure, whilst the natural rubber coated cotton fabric decreased. In sets (e) and (f), the natural rubber coated cotton also decreased in tear strength with time. With sets (g) and (h), the PU-coated nylon increased in tear strength with time.

# 4.2.8 Rubber × load interaction (RL) and fabric × rubber × load interaction (FRL)

These were testable only in set (b), where they were not significant, and (e), where the natural rubber coated nylon and cotton fabrics under 10% load had lower tear strengths than when exposed under 1% load.

### 4.2.9 <u>Rubber × site interaction (RS) and fabric × rubber × site</u> interaction (FRS)

In set (b), the PU-coated nylon had higher tear strength at PERME and Innisfail. With (c), the PU-coated nylon had higher tear strength at Cloncurry and Innisfail, whilst the natural rubber coated cotton had lower tear strength at PERME.

### 4.2.10 <u>Time × load interaction (TL) and fabric × time × load</u> interaction (FTL)

In set (d), the natural rubber coated nylon fabric under 10% load lost tear strength with time. The effects were not significant in sets (e) and (i).

### 4.2.11 <u>Time × site interaction (TS) and fabric × time × site</u> interaction (FTS)

In set (c), the coated nylon fabrics increased in tear strength with time at the Australian sites. In set (d), the natural rubber coated cotton fabric lost strength with time. The effects were not significant in set (i), which did not include PU or cotton.

### 4.2.12 Load × site interaction (LS) and fabric × load × site interaction (FLS)

In set (b), *ie* at short times, these were not significant. With set (d), the natural rubber coated cotton fabric at PERME, and, in sets (d) and (i), the natural rubber coated nylon fabric at PERME and at Cloncurry, lost more tear strength after exposure under the higher load.

### 4.2.13 <u>Rubber × time × site interaction (RTS) and fabric × rubber</u> time × site interaction (FRTS)

In set (c), the PU-coated nylon increased in tear strength with time at the Australian sites, and the natural rubber coated cotton lost more strength with time at PERME than at the other sites. The effect was not significant with set (i), there being no PU and no cotton.

### 4.2.14 Other interactions

The other testable interactions were: RTL and FRTL in sets (e) and (i), TLS and FTLS in sets (d) and (i), LSR and FLSR in sets (b) and (i), and RTLS in set (i). Some of these just reached significance at 99.9% probability, but they did not add appreciably to the information gained from the experiment.

### 5 CONCLUSIONS

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(1) The wing-rip tear strength of nylon and cotton fabrics of similar mass per unit area and coated with natural, neoprene, PU or CSPE rubbers have been determined after exposure to weathering in UK or Australia for up to one year under a load of 1% or 10% of the nominal breaking load.

(2) The ratio of tear strengths for the nylon to the cotton fabrics was more than 5, but the nylon had greater variability.

(3) The tear strength of the PU-coated nylon increased with time at the Australian sites, due to failure of the coating permitting yarn slip and bunching.

(4) The tear strength of the natural rubber coated cotton decreased with time in UK.

(5) The tear strengths of the natural rubber coated nylon and cotton were lower after exposure under the heavier load, especially after longer times of exposure.

(6) Fabrics coated with CSPE were least affected by weathering.

### Acknowledgment

The authors thank Mr D.E. Lloyd of Mathematics and Computation Department, RAE, for discussions and the arranging of the computer programs.

Table 1

# MEDIAN TEAR STRENGTHS, N, OF WEATHERED COATED FABRICS

works         Original         Final         3         6         12         65         3         6         12         65         3         6         12         65         3         6         12         65         3         6         12         10         11         10         11         10         11         10         11         10         11         10         11         10         11         10         11         10         11         10	Site	. Controls					8	PERIE							Cloncurry	urry							Inni sfai 1	5			
well, <b>X</b> 1         10         11         10         11         10         11         10         11         10         11         10         11         10         11         10         11         10         11         10         11         10         11         10         11         10	fille, sonths	Original	Final		3		5	4	~	65		~		9		12		65		~		6		12		65	1.00
Mathematical         A         B         C         D         E         F         G         H         I         J         K         L         M         D         P         Q         R         S         T         U           Rubber         Rub         Rubber         Rubber	Load level, X			-	10	-	10	-	10	-	10	-	4	-	10	-	10	-	9	-	6	-	2	-	ę	-	9
Rubber         24.5         71.8         23.5         72.0         13.3         23.5         19.0         32.2         13.1         23.2         19.1         22.6         23.2         19.1         22.6         23.6         19.1         22.0         23.5         19.0         32.2         19.1         12.2         8.1         18.1         17.1         22.0         11.2         22.6         22.8         18.1         12.1         22.0         11.1         22.5         32.5         19.0         32.2         19.1         22.6         21.6         22.8         18.4         17.1         22.9         19.0         32.2         18.1         12.1         22.6         22.8         18.1         22.1         19.1         22.6         22.8         19.1         22.6         22.6         21.1         22.1         23.1 <t< th=""><th>Column</th><th>۲</th><th>8</th><th>U</th><th>a</th><th>w</th><th>Ŀ</th><th>9</th><th>=</th><th>-</th><th>~</th><th>×</th><th></th><th>E</th><th>z</th><th>0</th><th>a</th><th>0</th><th>œ</th><th>5</th><th>-</th><th>3</th><th>-</th><th>-</th><th>×</th><th>-</th><th>~</th></t<>	Column	۲	8	U	a	w	Ŀ	9	=	-	~	×		E	z	0	a	0	œ	5	-	3	-	-	×	-	~
Matural         28.5         71.8         87.5         72.6         73.5	Fabric Rubber																					-					
25.9         20.8 $22.6$ <th>Nylon Natural</th> <th></th> <th></th> <th>23.5</th> <th></th> <th></th> <th>18.8</th> <th></th> <th></th> <th></th> <th>_</th> <th></th> <th></th> <th>and the second second</th> <th></th> <th>200</th> <th></th> <th>25.1ª</th> <th></th> <th>_</th> <th></th> <th></th> <th>19.6</th> <th>19.6 18 16.7 1</th> <th>18.1</th> <th>26.3</th> <th>23.9</th>	Nylon Natural			23.5			18.8				_			and the second second		200		25.1ª		_			19.6	19.6 18 16.7 1	18.1	26.3	23.9
PU         28.0         24.9         28.4         77.7         25.1         25.9         27.5         27.5         27.9         27.5         27.9         27.5         27.9         27.5         27.9         27.5         27.9         27.5         27.9         27.5         27.9         27.5         27.9         27.5         27.9         27.5         27.9         27.5         27.9         27.5         27.9         27.5         27.9         27.5         27.9         27.5         27.9         27.5         27.9         27.5         27.9         27.5         27.9         27.5         27.5         27.0         27.1         27.5 <th2< th=""><th>Nylon Keprene</th><td>25.9 25.1</td><td>and the second sec</td><td>22.6</td><td></td><td>22.4</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>and the second se</td><td>_</td><td></td><td></td><td></td><td>_</td><td>and the second second second</td><td></td><td>24.3 2</td><td>22.4 30</td><td>30.4</td><td>20.6</td><td>25.7</td></th2<>	Nylon Keprene	25.9 25.1	and the second sec	22.6		22.4									and the second se	_				_	and the second second second		24.3 2	22.4 30	30.4	20.6	25.7
CSPE         22.4         23.1         23.2         20.8         20.0         20.4         22.0         23.5         27.6         20.8         20.6         27.0         23.5         27.5         20.8         20.6         23.0         23.7         21.6         22.7         23.7         21.6         22.7         23.5         23.6         23.7         21.6         22.0         23.9         23.7         21.6         23.7         21.6         22.7         23.7         21.6         22.7         23.7         21.6         23.7         23.7         23.6         23.7         23.6         23.7         23.6         23.7         23.6         23.7         23.6         23.7         23.6         23.7         23.6         23.7         23.6         23.7         23.6         23.7         23.6         23.7         23.6         23.7         23.6         23.7         23.6         23.7         23.6         23.7         23.6         23.7         23.7         23.7         23.7         23.7         23.7         23.7         23.7         23.7         23.7         23.7         23.7         23.6         23.7         23.7         23.7         23.7         23.7         23.7         23.7         23.7 <th< th=""><th></th><th>29.0</th><th></th><th>28.4</th><th></th><th>25.1 26.3</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>27.9</th><th></th><th>89.8ª</th><th></th><th>52.5ª</th><th></th><th></th><th>Contraction and the second</th><th>7.56 83. 0.4 81.</th><th>44</th><th>71.6ª</th><th></th><th>57.4</th><th></th></th<>		29.0		28.4		25.1 26.3								27.9		89.8ª		52.5ª			Contraction and the second	7.56 83. 0.4 81.	44	71.6ª		57.4	
Matural       4.5       4.6       4.3       4.2       3.1       3.1       1.8       0.5       3.9       4.5       4.5       3.8       3.8       3.2       4.3       3.9       4.5       3.7         Watural       4.7       4.4       4.3       2.9       2.9       1.4       0.5       3.9       4.5       4.5       4.3       4.1       4.3       3.9       4.5       4.5       4.3       3.6       3.8       4.4       3.9       4.5       4.5       4.3       3.6       3.6       3.9       4.3       3.7         Webrene       4.7       4.8       4.6       4.1       4.3       3.9       4.1       4.5       4.3       3.6       3.6       3.6       3.9       4.5       3.7         Webrene       4.7       4.8       4.6       4.1       4.3       3.9       4.1       4.1       3.9       4.3       3.7       3.7       3.6       3.8       4.4       3.9       4.5       3.7         Webrene       4.6       4.7       4.8       4.3       3.9       4.1       4.1       3.9       4.3       3.7       3.7       3.7       3.7       3.7       3.7       3.7		22.4		23.3		20.8							_	50									22.8 2	24.0 2	23.5	23.1	23.5
Weoprene       4.7       4.8       4.6       4.1       4.3       3.9       4.1       4.1       4.3       3.9       4.3       3.7       -       3.3       -       3.8       3.6       3.9       4.3       3.7         Weoprene       4.6       4.7       4.8       4.6       4.1       4.1       3.9       4.3       4.3       3.7       -       3.3       -       3.7 <th< th=""><th>Cotton Natural</th><th>22</th><th>4.6</th><th>4.4</th><th>4.3</th><th>3.1</th><th>3.1 2.9</th><th>1.8</th><th>0.5</th><th>3.9</th><th></th><th>50</th><th></th><th>3.9</th><th></th><th>3.6</th><th>3.2</th><th></th><th></th><th>- and and a</th><th></th><th></th><th>3.9</th><th>3.9</th><th>3.5</th><th>11</th><th>4.9</th></th<>	Cotton Natural	22	4.6	4.4	4.3	3.1	3.1 2.9	1.8	0.5	3.9		50		3.9		3.6	3.2			- and and a			3.9	3.9	3.5	11	4.9
PU         4.0         4.0         4.1         4.2         3.5         3.7         3.9         3.0         4.4         -         4.0         4.1         3.7         3.7         3.9         3.0         4.4         -         4.0         4.1         3.7         3.9         3.0         3.0         4.1         3.7         3.0         3.0         3.0         4.1         3.9         3.0         3.0         3.0         3.0         3.0         4.4         -         4.1         3.0	Cotton Nsoprene		4.8	8.4 8.4	4.4	22	÷;	3.9	4.1	4.1		3.9		3.7		3.3	• •						3.9	3.5		3.9	3.8
CSPE 3.9 4.0 3.7 3.6 4.1 3.9 3.7 3.5 3.8 3.9 3.7 3.9 3.9 3.9 3.7 3.3 - 3.1 - 3.5 3.5 3.9 3.7 3.9 3.7 3.9 3.7 3.9 3.7 3.9 3.7 3.9 3.7 3.9 3.7 3.9 3.7 3.9 3.7 3.9 3.7 3.9 3.7 3.9 3.7 3.9 3.7 3.9 3.7 3.9 3.7 3.9 3.7 3.7 3.7 5.7 3.7 5.7 3.7 5.7 5.7 5.7 5.7 5.7 5.7 5.7 5.7 5.7 5		97	4.0	1.4	4.2	3.9	3.9	3.7	3.5							11						3.9		4.0	3.5	15	4.5
		3.9	0.4	3.7 3.7	3.6	4.1	3.9	3.7	3.5					3.3	• •	3.1		3.5	5.0				3.7	3.7	0.4	3.5	···

,

a thread slippage

- specimen lost or damaged

b coating flaked

Table 2

MAXIMUM TEAR STRENGTHS, N, OF WEATHERED COATED FABRICS

-				-							10.0	~
	55	9	2		27.9	29.6 28.3		28.0	6.1	5.5	5.6	6.2 5.7
		-	*		31.2 31.8	26.0	68. 2 <sup>a</sup> 64. 5	30.4	6.0 5.8	5.4	6.0	4.7
	2	9	×		20.3	33.7	• •	28.0	5.0	• •	5.3	5.1 6.2
Inni sfai 1	12	-	-		25.3	28.3	80.9 <sup>a</sup> 89.8 <sup>a</sup>	29.9	5.3	5.2	5.6	5.5
Innte	9	10	>		22.1	31.0	104.0 <sup>b</sup> 95.7 <sup>b</sup>	28.6	5.6	6.1	••	6.3
		-	-		19.9	27.0	87.9 <sup>b</sup> 10	28.4	5.1	5.7	6.3 5.4	4.8
	3	10	F		30.1	26.4	40.2	28.3 29.2	5.4	6.7 6.0	5.4	5.0
			s		30.0	31.5 29.8	31.0	29.4	6.2	5.7 6.6	5.4	5.6
		10	æ		23.1 26.0	26.7	• •	27.5	5.5	5.0	6.4 6.1	5.2
	65	+	•		35.7 <sup>a</sup> 35.1 <sup>a</sup>	25.3	61.3 <sup>a</sup> 67.7 <sup>a</sup>	28.3	5.3	4.9	5.1	4.8
1	~	10	٩		17.9	24.9	• •	27.9 26.9	4.7	• •	• •	• •
Cloncurry	12	1	0		>39.2ª	27.1 30.8	94.2ª 96.1ª	26.5	5.4	4.9	6.1 5.6	3.9
Clon	6	10	z		25.7	27.2	• •	26.3 25.8	5.7 6.4	• •	5.2	
		+	=		28.3	26.9 25.9	34.1	27.4	5.3	5.8	4.8 5.8	4.6
	3	10	L	3	22.1	31.7 28.9	22.3	27.5 29.2	5.8	6.0	5.2	5.0
		1	K		28.6	26.0	31.9	30.2	6.2 6.1	5.4	5.3	5.5
	6S	10	٢		25.2	27.0	36.1	28.1 29.0	5.2	5.5	5.5	5.2
	9	1	-		29.0	26.3 27.8	31.7 38.7	25.7 28.6	5.1	6.2 5.8	4.9	5.0
	12	10	Ŧ		17.2	29.0	33.6 35.0	24.9	1.0	6.0	4.5	5.0
PERKE	+	1	9		31.8	28.9	34.8	25.8 27.3	2.6	5.1 5.8	4.6	5.2
×	6	10	F		29.1	25.2 26.8	34.2	23.7 28.8	4.6	6.2 6.2	5.4	3.4
		1	E		29.9	26.3	34.8	26.9 28.3	4.2	6.0	5.5	5.8
	3	10	D		27.5	32.4	35.3	26.9	6.2	6.3 6.1	6.0	4.6
		-	J		29.8	31.4	39.2	28.6 26.9	5.9	5.9	5.5	5.5
-	Final		8		27.3	27.5	29.4.	28.7	6.1	6.0	5.8	4.9
Controls	Original		A		31.8 31.4	32.8 29.9	29.0	26.9	5.9	6.1	5.9	5.1
		1. 2		Rubber	Natural	Neoprene	5	CSPE	Natural	oprene	8	CSPE
Site	Fine, nonths	Load level, Z	Column	Fabric R	Nylon Ni	Ny lon Nee	Nylon	Nylon 1	Cotton Na	Cotton Neoprene	Cotton	Cotton (

b coating flaked

specimen lost or damaged
 a thread slippage

Table 3 ANALYSIS OF ERRORS

Property	Source					Set				
		(a)	(9)	(c)	(P)	(e)	(£)	(g)	(H)	(i)
Error variance	Nylon	3.509	2.432	3.216	١	1.611	2.483	5.182	2.282	2.672
	Cotton	0.0391	0.0088	0.0161	0.0350	0.0278	0.0233	0.0216	0.0255	•
	Nylon/cotton error variance ratio	96	275	197	1	57	1117	239	6	•
	Overall	1.774	1.220	1.616	2.082	0.819	1.253	2.602	1.157	1
Set mean, N	Nylon	23.6	33.2	28.2	1	22.9	23.6	27.6	28.7	22.2
	Cotton	4.4	4.1	3.8	3.8	3.7	3.9	4.6	4.1	1
	Overall	14.0	13.6	16.0	12.6	13.2	13.7	15.8	16.4	1
	Nylon	1.874	1.560	1.793	1	1.269	1.576	2.276	1.513	1.635
deviation, N	Cotton	0.198	060.0	0.127	0.187	0.167	0.152	0.147	0.160	1
	Overall	1.332	1.105	1.271	1.443	0.905	1.119	1.613	1.075	1
of	Nylon	7.9	6.8	6.4		6.4	6.7	8.2	5.2	7.4
variation, X	Cotton	4.5	2.4	3.3	4.9	4.5	3.8	3.6	3.9	1
	Overal1	9.5	8.1	7.9	11.5	6.9	8.2	10.2	6.5	1
es of om in	Nylon Cotton	80	24	48	24	32	24	24	24	72
error	Overal1	16	48	96	48.	64	48	48	48	1

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	T	ab	1	e	4
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TABLE OF VARIANCE RATIOS

Effect		Degrees of	No.of	No.of					Set				
FILECT	Source	freedom	levels	results per level	()	(6)	(c)	(d)	(e)	(f)	(	(h)	(i)
,	Overall	1	2	16	1668								
7	Overall	1	2	48		7106		3625.6		840	517	1267	
	Overall	1	2	96	1000		18569			1			*
	Overall	1 -	2	64					16958				
R	Nylon	3	4	4	5.9			1.1.1				1	
R	Cotton	3	4	4	12.1		1					-	
R	Overall	3	4	8	5.3						-		
R	Nylon	3	4	12	1.1	12.8				18.9	177.7	845.9	
R	Cotton	3	4	12		112.8			1.11	47.3	37.1	17.1	
R	Overall	3	4	24		9.8		1.1.1	N. C. M.	20.5	181.7	833.6	
R	Nylon	3	4	24	1		855.5		1.2017	201		1	
R	Cotton	3	4	24		4	17.6						
R	Overall	3		48			912.0	19.19				Cinstal	
R	Nylon	3	4	16	1				58.2			Luciel	
R	Cotton	3	4	16	1.1.1			•	150.4	601 ST	-		
R	Overall	3	4	32	1		1.		73.8	a a		and a	
R	Nylon	2	3	48						1	1	ai.	7.
FR	Overall	3	8	4	6.6			4.10		1		1.000	
TR	Overall	3	8	12		16.5		1.11		22.8	177.7	839.2	
FR	Overall	3	8	24		1.	897.0						
n	Overall	3	8	16					65.3				
T	Nylon	1	2	8	13.5			1.1.1.1	41				
T	Cotton	1	2	8	1.3				1.1.1				
T	Overall	1	2	16	12.6		1.1		1.0		1	1	
T	Nylon	3	4	24		30.216	128.0			-		-	
T	Cotton	3	4	24			80.7			12.1			
T	Overal1	3	4	48	0		114.4					and the second	
T	Cotton	3	4	12				154.3			1999	-	
T	Overal1	3	4	24				11.3					
T	Nylon	3	4	16		1.201		4.1.4	9.2			a since	
T	Cotton	3	4	16				19-11-12	121.4			and and	
T	Overal1	3	4	32	1000			1.1.1	28.6			-	
T	Nylon	5	6	8				10-54		5.1	68.5	128.4	
T	Cotton	5	6	8		1.1.1		1		72.9	36.4	23.2	
T	Overal1	5	6	16			1991		1. 2.	8.9	93.3	118.1	
T	Wylon	3	4	36		100		Sido			1. 17	James	2.
n	Overall	1	4	8	14.3						12000	1.51.10	
n	Overall	3	8	24			141.3		1.2.1.2.1			in and	
π	Overal1	3	8	12				4.7	1.00				
n	Overall	3	8	16			1.50	1	6.0	1. 1. 1. 1.	1.	in the	
n	Overall	5	12	8	1.		a Carlo			6.1	102.8	136.3	
L	Nylon	1	2	24	1	0.0	1. 1	1	13.55			. Array	
L	Cotton	1	2	24		0.0		5.4	a second		1. 2.		
L	Overal1	1	2	48		0.0	1.1.1.1	72.9	12010		-	N. S. S.	
L	Nylon	1	2	32	1	Shire .	- 65		17.5			Savan 1	
L	Cotton	1	2	32				- Frank	2.9		and the second	Thursday.	1.00
L	Overal1	1	2	64		in the second		1.4.1.4.1	15.7	S. CEL	Sec. 1		
L	Nylon	1	2	72	al in	1000				65.000			23.

13.

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Table 4 (continued)

Effect	Source	Degrees of	No.of	No.of results					Set		11071		
	source	freedom	levels	per level	(a)	(b)	(c)	(d)	(e)	(£)	(2)	(h)	(i)
n	Overal1	1	•	24		0.0		65.8					
71.	Owrall	1	4	32		1 1 1 2			12.1		1.1.1	1 Starten	
5	Nylon	2	3	16	1.	22.1					1. H. S.	Tepes	
8	Cotton	2	3	16		10.6		189.5	1.11			1 Ster	11.12
8	Overall	2	3	32		23.4	+ 11-14	4.0				1.54	
S	Nylon	2	3	32	11-1-5		165.4					1.1.1	
8	Cotton	2	3	32			11.7					1.2.64	
S	Overall	2	3	64			192.1						
8	Nylon	2	3	48	1							1.000	3.7
75	Overall	2	6	16		20.7		4.6				1. 2. 19 . 19	
<b>7</b> 5	Overall	2	6	32			178.9						1.1.7
-	Nylon	3	8	2	1.6				1				
RT	Cotton	3	8	2	0.1							1.000	
-	Overall	3	8		1.5		•			in sector			
13	Nylon	9	16	6			120.5						
73	Cotton	9	16	6			29.7						
11	Overall	9	16	12	C.C.S.		132.4					-	
m	Nylon	9	16	4					2.2				
ĸ	Cotton	9	16	4					64.9	1			
RT	Overall	9	16	8					4.1			and the second	
RT	Nylon	15	24	2						2.2	69.2	151.6	
RT	Cotton	15	24	2						24.2	7.6	4.0	
RT	Overall	15	24	4						1.7	71.4	152.1	
RT	Nylon	6	12	12									5.6
FRE	Overall	3	16	2	1.6							in the loss	
FRE	Overal1	9	32	6			122.1			-	1	1 44 AL	
TRE	Overal1	9	32	4					1.6	1		1000	
FRT	Overal1	15	48	2			1.1			4.2	66.6	147.8	
RL	Nylon	3	8	6	1.1	4.6		1.1.1				1. The days	1
RL	Cotton	3	8	6	-	7.1							
RL	Overal1	3	8	12		4.6						( here a	
RL	Nylon	3	8	8					17.8	1.	1999	a Courses	1.1.1
RL	Cotton	3	8	8			1.1.1.1.1		6.6	1.1.1			E R.
RL	Overall	3	8	16					26.8				
RL	Nylon	2	6	24								a second	43.0
FRL	Overal1	3	16	6		4.7						i preserve	
FRL	Overall	3	16	8			1.64		19.8		1.1	No.	1.00
15	Nylon	6	12		12.24	7.4				S. Contra	The star	a farmer	1
15	Cotton	6	12	4	101	16.2				1		Section 1	1
15	Overall	6	12	8		7.9					and the	111-1-5-	
RS	Nylon	6	12	8	1.535		170.2					( Street	17 STA
15	Cotton	6	12	8			58.0				1.5	and the second	
15	Overal1	6	12	16			181.1					1 in the	E. E
-	Nylon		9	16	S. Harris					3-1-2-2-4		C. S. S. S. S. S.	6.0
TRS	Overal1	6	24			6.9		111111		6	1.1.5	a and	1.5
-	Overall	and the second	24	8			181.6	Sec. 1				a series and	

		Degrees of	No.of	No.of					Set				
Effect	Source	freedom	levels	results per level	(a)	(6)	(c)	(4)	()	(£)	(	(h)	(1)
TL	Cotton	3	8	6				5.8			1.145	- 1 - 1	
TL	Overall	3	8	12		1		12.9			a start		1
п.	Nylon	3	8	8	1.1.1	1	10.00	1	4.7		1.000		
TL.	Cotton	3	8	8		-			2.5				1953
TL.	Overall	3	8	16			1		12.8			1.4. 2.	14
TL	Nylon	3	8	18		1. K. (					1.1.1	1 contra	1.7
FTL	Overall	3	16	.6		1. 1. 1	1.2	10.0	10000				
FTL	Overall	3	16	8	- in the second		the second	1 march	3.2		an ar an		
TS	Nylon	6	12	8			83.7		1			1.11	1
TS	Cotton	6	12	8			14.1	1					
TS	Overal1	6	12	16		-	98.8					1. 1.	
TS	Cotton	6	12	4				50.3				1	1.
TS	Overal1	6	12	8		-		6.9				· ·····	- Size .
TS	Nylon	6	12	12			10.04.0						3.7
FTS	Overall	6	24	8			91.7				1.1.1	11	
FTS	Overall	6	24					5.2	122				1
LS	Nylon	2	6			4.8		1.2.5		1000			
LS	Cotton	2	6	8		3.5		8.3	146.19			1 Sec. 14	
LS	Overall	2	6	16		5.2	1	14.4					
LS	Nylon	2	6	24	1.12		100	1					12.5
FLS	Overall		12	8		4.3		12.3					
RTL	Nylon	9	32	2			1.11		4.0				7
RTL	Cotton	9	32	2					3.0	1.000			
RTL	Overall	9	32	4			Seat Sea	1.1.1	6.5	1.11			
RTL	Nylon	6	24	6			1					1.00	10.0
FRTL	Overall	and the second second	64	2		Sec. 14		-	4.7				
RTS	Nylon	18	48	2			70.0						
RTS	Cotton	18	48	2			14.8	1		in the second			
RTS	Overal1	18	48				75.0	1	The Park			1	
RTS	Nylon	12	36				1		-	1			3.2
TRIS	Overall	18	96	2	a de la composición de la comp	1	73.7			130 3			
TLS	Cotton	6	24	2			1	2.3				1.000	
TLS	Overall	6.	24	4	De la com	1999		5.5		1000		1.55	
TLS	Nylon	6	24	6	155	1	1	1			1.1.1.1		3.4
FTLS	Overall	6	48	2			1.000	5.6					
LSR	Nylon	6	24	2		5.2		1					
LSR	Cotton	6	24	2	1.000	4.5		1.4.4					
LSR	Overall	6	24		13.50	5.1				1.40			
LSR	Nylon		18		1.1.1		-	1	1		1.5		5.5
FLSR	Overall		48	2									1 3.3
RTLS	Nylon	12	72	2	1.1	5.2							4.1
									1	12.40		101.00	

Table 4 (concluded)

# Table 5

Factor	Level .					Set		and the second		
ractor	Level	(a)	(b)	(c)	(d)	(•)	(f)	(9)	(h)	(1)
F	Nylon Cotton	23.6	. 23.2	20,1 3,0	21.6 3.7	21.5 3.7	23.4 4.0	27.6 4.0	28.7 4.1	
8	Nature'; Neoprono PU CSPE	12.9 14.1 15.4 13.6	13.0 13.2 14.6 13.4	13.8 12.9 24.0 13,0		12.3 12.9 15.1 12.9	13,4 13,2 15,1 13,0	14.4 13.1 22.4 13.3	12.7 13.6 25.9 13.4	21.6 22.5 22.6
R	Hatural Hosprono PU CSPE	lylan Cattan 21,0 4,6 23,5 4,7 26,5 4,3 23,3 3,0	Nylan Cattan 21.8 4.4 22.2 4.3 25.4 3.9 23.2 3.8	Hylan Cattan 23.8 3.8 22.2 3.9 44.1 3.9 22.5 3.7		Nylon Cotton 21.5 3.0 21.6 4.2 26.4 3.8 21.8 3.8	Hylon Catton 23,2 3,7 22,6 4,4 26,5 3,9 22,2 3,8	lylon Catton 24.7 4.3 22.2 4.0 40.7 4.1 23.0 3.7	Nylon Cotton 21.1 4.3 23.2 4.1 47.8 4.0 23.1 3.8	
1	Original Final 3 months 6 months 12 months 65 months	14,8 13,1		13.6 15.6 18.2 16.4	13.0 12.0 11\\$ 13.8	14.0 13.3 12.4 13.2	14.8 13.1 14.4 13.7 12.9 13.2	14.8 13.1 12.9 13.3 22.8 17.9	14.8 13.1 13.5 19.8 19.0 18.1	22.4 21.8 21.9 22.8
FT	Original Final. 3 conths 6 conths 12 conths 65 conths	Nylon Cotton 25.3 4.3 21.9 4.4		Bylon Cotton 23.2 4.1 27.5 3.8 33.2 3.5 28.9 3.9	Nylon Cotton 21.8 4.4 19.9 3.7 20.8 2.8 23.4 4.1	Nylon Cotton 24.3 4.2 22.8 3.8 21.6 3.1 22.7 3.8	Hylon Cotton 25.3 4.3 21.9 4.4 24.6 4.2 23.7 3.7 23.5 3.2 22.6 3.8	Hylen         Cotten           25.3         4.3           21.9         4.4           21.8         4.0           23.2         3.7           41.8         3.6           31.8         3.9	Nylon-Cotton 25.3 4.3 21.9 4.4 23.2 4.0 35.8 3.8 34.3 3.7 32.4 4.0	
ι	1% 10%		13.6 13.5		13.8 11.4	13.5 12.9				22.8 21.6
FL	1% 10%		Nylon Cotton 23.2 4.1 23.1 4.1		Hylon Cotton 23.8 3.8 19.0 3.7	Nylon Cotton 23.9 3.7 19.0 3.7				
\$	PERME Cloncurry Innisfail		14.2 12.6 14.0	13.5 16.7 17.7	12.3 13.2 12.4					21.6 22.3 22.6
FS	PERNE Cloncurry Innisfail		Nylen Cotton 24.3 4.2 21.0 4.0 24.0 4.1	Nylon Cotton 23.6 3.7 29.5 3.8 31.4 3.9	Nylan Cattan 21.5 3.0 22.3 4.1 20.6 4.2					
RL.	Natural Neoprene PU CSPE		12 102 13.7 12.5 13.3 13.0 14.0 15.2 13.3 13.5			1% 10% 13.7 10.8 12.9 12.9 15.0 15.2 12.8 12.9	-			1% 10% 23.8 19.0 22.2 22.9 22.5 22.6
Fil	Rylon Natural Neoprano PU CSPE Cotton		1% 10% 23.0 20.6 22.5 21.8 24.2 28.5 22.9 23.4			1% 10% 24.1 18.8 21.5 21.7 26.2 26.6 21.7 22.0				
	Natural Nooprono PU CSPE		4.4 4.4 4.2 4.4 3.9 3.9 3.0 3.7			3.2 2.8 4.2 4.3 3.8 3.8 3.8 3.8				

TABLE OF MEAN MEDIAN TEAR STRENGTHS, N

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														Set												
Factor	lavel		(•)		-		(c)				(•)			(+)		-		(6)			(4)			-	()	
		latural	latural Neoprene PU CSPE	Pu	SPE II	Natural Neoprene	oprene	PU CSPE		Natural Neoprene	Me ene	I CSPE	Natural	Natural Neoprene	2	CSPE Natu	Natural Neoprene		PU CSPE	Natural	Natural Neoprene	2	CSPE Natu	Natural Neoprene CSPE	rene C	34S
2	Griginal Final 3 12 65 65	13.9 1.11	15.1 13.2	16.7 13.6 14.1 13.6		13.7 12.1 14.9	13.3 13.1 12.6 12.8	14.0 13. 23.6 13. 33.5 12. 25.0 13.	13.3 13.3 13.7 12.3 12.3 10.3 12.7 13.0	8 13.5 3 13.0 3 12.8	5 16.3 0 15.1 8 14.1 4 15.0		13.9 14.2 13.7 13.4 13.4	15.1 13.5 13.5 13.3 13.3 12.3	16.7 13 14.1 13 14.8 13 14.8 13 14.1 11 14.1 11 14.7 12	13.6 13.9 13.6 11.7 13.5 13.3 13.5 13.3 13.1 12.0 11.7 19.2 11.6 16.0	4.	13.2 14.1 16. 13.2 14. 12.3 14. 13.3 4.7	16.7 13.6 14.1 13.6 12.4 13.6 14.5 14.0 47.6 12.0 28.9 13.1	13.9 13.5 10.6 15.4	15.1 14.2 13.4 13.3	16.7 1 14.1 1 13.5 1 13.5 1 13.5 1 38.6 1 31.2 1	13.6 13.6 12.9 13.8 13.1 20.8 13.1 20.8		22.2 22.2 22.4 22.2 22.2 22.2 22.2 22.2	23.2
έe ·	Nylon Original Final 3 12 6 6	23.2 18.7	24.5 21.7	23.8	33.3	82.1 8.1 8	22.5	24.2 22 43.4 23 46.0 27	22.9 23.4 23.5 21.5 21.1 19.5 21.6 21.6 21.6	22.5 5 21.5 20.5 20.5 20.5	28.5 28.5 28.5 28.5 28.5	5 23.0 6 20.6 6 20.6	23.2 18.7 24.5 24.5 24.5	7.5 7.7 2.5 2.5 2.5 2.5	29.2 23 29.2 23 29.6 23 25.1 22 25.9 19 25.9 19 25.9 19 25.9 19 25.9 19 25.9 19 25.9 19 25.9 19 25.9 19	23.3 23.2 23.2 23.2 23.2 23.2 23.2 23.2		23.23.23 23.4.23 23.4.23 23.4.23 23.4.23 23.4.23 23.4.23 23.4.23 24.23 24.23 24.23 25.25 25.25 2	29.2 23.3 23.8 23.3 21.0 23.3 25.3 24.5 25.3 24.5 26.7 20.7 26.7 20.7	23.2 18.7 17.3 18.1	7.7 7.7 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5	23.8 2 23.8 2 23.8 2 23.2 2 79.0 2 73.4 2 74 7 75 7 75 7 75 7 75 7 75 7 75 7 75 7	22.0 22.0 22.8 22.8	a Antonia		
	Cotton Cotton Final 3 6 6 8 8	<b>3</b> 5	55	77	6.0.4	2222							122323	555583							328223		8.5.9.0.0.8 .5.5.9.0.0.8			

Table 5 (continued)

											Set	1									
Factor	Level		(6)	1			(c)				(d)				(•)				(1)		
RS	FERIE Cloncurry Innisfait	Natural 13,8 12,5 12,9	13.5 12.6 13.6	PU 16.3 11.8 15.9	13.3	latura) 13.7 15.2 12.7	12.9 12.6 13.4	25.8	CSPE 12.8 13.2 13.3									Netural 21.5 22.1 20.6	21.9 22.0 23.9		CSPE 21.0 22.5 23.3
<b>Fits</b>	Nylon PERNE Cloncurry Innisfail Cotton PERNE Cloncurry Innisfail	Ratural 23,4 20,4 21,6 4,3 4,5 4,4	Hesprene 22.5 20.9 23.1 4.6 4.2 4.1	PU 28.5 19.8 27.8 4.1 3.7 3.9	CSPE 23.0 22.9 23.6 3.7 3.8 3.9	listura) 24,1 26,5 21,2 3,2 4,1 4,1	Hesprene 22.1 21.5 23.1 4.2 3.7 3.8	47.8					T								
n	17 107									3 13.7 12.5	6 12.2 11.3	12 65 14.6 14, 9.0 12,		3 14.4 14.1	6 13.8 12.9	12 12.9 11.8	65 13.2 13.2	3 22.8 21.9	6 22.4 21.2		65 23.2 22.3
FIL	llylen 12 102 Cotton 12 102									3 23.0 20.6 4.4 4.4	6 21.1 18.7 3.6 3.8	· 12 63 26.1 25 15.4 21 3.0 4 2.6 4	2	3 24.6 24.0 4.2 4.1	6 23.8 21.8 3.8 3.8	12 22.6 20.6 3.2 2.9	65 22,6 22.8 3.8 3.8				
TS	PERME Cloncurry Innistail					3 14.4 12.9 13.5	6 13 8 13.3 19.8	22.8	65 13.2 17.9 18.1	3 13.8 12.5 12.9	6 12.3 12.2 11.0	12 65 10.3 12. 14.2 14. 11.0 14.	:		2		0.11	3 23.0 21.4 22.8	6 21.6 21.0 21.8	23.0	65 21.5 22.9 23.8
FTS	Bylon PERME Cloncurry Inntafat1 Cotton PERME Cloncurry Inntafat1					3 24.6 21.8 23.2 4.2 4.0 4.0	6 23.8 23.2 35.8 3.8 3.8 3.8 3.8	41.9	3.9	3 23.4 20.4 21.6 4.3 4.5 4.4	6 21.5 20.2 18.1 3.0 4.2 3.9	12 65 19.5 21. 24.7 24. 18.1 24. 1.1 3. 3.6 4. 3.9 4.	6 0 8 .7							·	
LS	PERIE Cloncurry Innistail	14	1 .4 .9 .5	12	# .1 .2 .5					1% 13, 15, 12,	2	10% 10.8 11.0 12.7	T					1 22 23 22	.5	20	7 .8 .9 .9
FLS	Nylon PERNE Cloncurry Innisfail Cotton	2	1.6 1.8 1.2	20	# .0 .3					12 24. 26. 21.	1 5	101 18.8 18.0 20.2	T								
	PERIE Clancerry Innisfail	1 1	.2	4	.1					3.	1	2.8 4.0 4.2									

Table 5 (continued)

Factor	Level				S	Set			
			(e	(e)			-	(:)	
RIL	14	З	9	12	6S	3	9		12
	Natural	14.2	13.8	13.4	13.3	23.0	21.1	8	-
	Neoprene	13.6	13.3	12.3	12.3	22.5	22.5	22	4.
	PU	16.4	14.8	14.1	14.8				
	CSPE	13.5	13.2	11.7	12.6	22.9	23.5	21.1	-
	101								
	Natural	13.5	10.8	7.2	12.0	20.6	18.8	15.	+
	Neoprene	13.4	12.8	13.3	12.5	21.8	23.3	24.4	4
	PU	16.3	15.5	14.1	15.2				
	CSPE	13.1	12.4	12.7	13.5	23.4	21.5	22.6	9
RIL	Nylon 1%								
	Natural	24.0	24.5	25.3	22.8				
	Neoprene	22.5	22.6	23.2	20.2				
	2	28.6	25.7	25.9	25.9				
	CSPE	23.2	22.4	19.6	21.4				
	Nylon 10%								
14	Natural	22.8	18.4	13.7	20.4				
	Neoprene	22.4	21.2	22.4	20.8				
	PU	28.4	26.9	24.7	26.5				
	CSPE	22.6	20.6	21.6	23.2				
	Cotton 1%				14 - 14 - 14 - 14 - 14 - 14 - 14 - 14 -				
	Natural	4.4	3.0	1.6	3.9				
	Neoprene	4.7	4.1	3.9	4.2				
	8	4.1	3.9	3.6	3.6	-			
	CSPE	3.7	4.0	3.7	3.7				
	Cotton 10%								
	Natural	4.3	3.0	0.5	3.5				
	Neoprene	4.5	4.2	4.2	1.4				
	2	4.1	4.0	3.4	3.8				
	CSPE	3.7	4.1	3.7	3.8				

Table 5 (continued)

Factor	Level				S	et			
ractor	Level			(c)				(1)	
		3	6	12	6S	3	6	12	65
RTS	PERME								
	Natural	14.2	13.8	13.4	13.3	23.4	21.5	19.5	21.6
	Neoprene	13.6	13.3	12.3	12.3	22.5	21.9	22.8	20.5
	PU	16.3	14.8	14.1	14.8				
	CSPE	13.5	13.2	11.7	12.6	23.0	21.5	20.6	22.3
	Cloncurry								
	Natural	13.3	12.1	19.3	16.0	20.4	20.2	24.7	24.0
	Neoprene PU	12.3	12.7	12.3	13.3	20.9	22.6	22.2	22.3
	CSPE	12.4	14.6 14.0	47.6	28.9 13.2	22.9	22.9	21.8	22.5
		13.0	14.0	12.0	13.2	22.9	22.9	21.0	
	Innisfail	47.5	-0.0		45.4				
	Natural	13.5	10.6	11.1	15.4	21.6	18.1	18.1	24.8
	Necprene PU	14.2	13.4	13.3	12.9	23.1	24.1	25.2	23.4
	CSPE	13.0	41.5	38.6	31.2 13.3	23.6	23.2	23.1	23.2
		13.0	13.0	13.2	13.5	23.0	23.2	23,1	23.0
FRIS	Nylon								
	PERME								
	Natural	24.0	24.5	25.3	22.8				
	Neoprene	22.5	22.6	23.2	20.2				
	PU	28.6	25.7	25.9	25.9				
	CSPE	23.2	22.4	19.6	21.4				
	Cloncurry								
	Natural	22.2	21.4	34.8	27.7				
	Neoprene	20.4	21.6	21.1	22.9	n ,			
	PU	21.0	25.3	90.7	54.0				
	CSPE	23.3	24.5	20.7	22.8				
	Innisfail					it is the			
1.120	Natural	22.8	17.3	18.1	26.4				
	Neoprene	24.5	23.2	22.9	21.6				
	PU	23.2	79.0	73.4	58.2				
10.00	CSPE	22.0	23.7	22.9	23.2	1.2.49			
	Gotton								
	PERME					14			
	Natural	4.4	3.0	1.6	3.9				
	Neoprene	4.7	4.1	3.9	4.2				
	PU	4.1	3.9	3.6	3.6				
	CSPE	3.7	4.0	3.7	3.7	1.			
	Cloncurry				STR.	Station.			
	Natural	4.5	4.0	3.7	4.4				
	Neoprene	4.0	3.7	3.4	3.8				
	PU	3.7	3.8	4.4	3.9	1. 1. 27.5			
	CSPE	3.9	3.5	3.1	3.6				
1	Innisfail								
	Natural	4.3	3.8	3.9	4.4				
	Neoprene	3.9	3.7	3.7	4.0				
	PU	3.8	3.9	3.8	4.3	and the			
	CSPE	4.0	3.9	3.6	3.5				

00:

Factor					S	et			
ractor	Level			(d)			(1	)	
and the second		3	6	12	6S	3	6	12	65
TLS	1%								•
	PERME	14.2	13.8	13.4	13.3	23.2	23.2	22.7	21.5
	Cloncurry	13.3	12.7	19.3	16.0	22.0	22.5	25.5	24.4
	Innisfail	13.5	10.6	11.1	15.4	23.1	21.4	21.3	23.7
	10%	1							
	PERME	13.5	10.8	7.2	12.0	22.6	20.1	19.2	21.5
1000	Cloncurry	11.6	11.4	9.1	12.2	20.8	21.2	20.3	21.4
	Innisfail	12.5	11.5	10.9	14.0	22.5	22.3	22.9	24.0
FTLS									
FILS	Nylon 1%					1993			
	PERME	24.0	24.5	25.3	22.8				
	Cloncurry	22.2	21.4	34.8	27.7	and the second			
	Innisfail	22.8	17.3	18.1	26.4	1.1.1.1.1.1			
		1		10.1	20.4				
	10%								
	PERME	22.8	18.4	13.7	20.4				
	Cloncurry Innisfail	20.4	18.9 19.0	14.6 17.9	20.4 23.2				
		20.4	19.0	11.9	23.2				Ś
Sec. 1	Cotton								
	1%								
	PERME	4.4	3.0	1.6	3.9				
1	Cloncurry	4.5	4.0	3.7	4.4	1			
	Innisfail	4.3	4.4	3.8	4.0				
	10%								
	PERME	4.3	3.0	0.5	3.5				
	Cloncurry	4.4	4.3	3.5	3.9	1			
	Innisfail	3.9	3.9	4.4	4.7				
			(b	)			(1)		
LSR	1%		Neopre	ne PU	CSPE	Natura	Neo	orene	CSPE
	PERME	14.2	13.6		13.5	24.1	2	2.1	21.7
	Cloncurry	13.3	12.3		13.6	26.2		1.5	22.9
	Innisfail	13.5	14.2	13.5	13.0	21.2	2	3.1	23.0
	10%								
	PERME	13.5	13.4	16.3	13.1	18.8	2	1.7	22.0
1.8.1	Cloncurry	11.6	12.9		13.0	18.0		2.5	22.2
12.5	Innisfail	12.5	12.9		14.5	21.1		.9	23.6

Table 5 (continued)

Table 5	(concl	(habu)
Table J	(couc.	radea

Factor	1	Level	- di	Set (b	)	
FLSR	Nylon 1X		Natural	Neoprene	PU	CSPE
		PERME	24.0	22.5	28.6	23.2
		Cloncurry	22.2	20.4	21.0	23.3
		Innisfail	22.8	24.5	23.2	22.0
	107	Contraction and the				
		PERNE	22.8	21.4	28.4	22.6
		Cloncurry	18.6	21.4	18.6	22.4
		Innisfail	20.4	21.6	32.4	25.3
	Cotto					
	1 1	ERME	4.4	4.7	4.1	3.7
		loncurry	4.5	4.0	3.7	3.9
	12.5	nnisfail	4.3	3.9	3.8	4.0
	107					
	F	ERNE	4.3	4.5	4.1	3.7
		loncurry	4.4	4.3	3.6	3.7
	1 1	nnisfail	4.4	4.3	4.0	3.7
				Set (i)		
TLS	3 months	1%	Natural	Neoprene	61 194	CSPE
		PERME	24.0	22.5		23.2
	en suit	Cloncurry	22.2	20.4		23.3
	1.1.1.1	Innisfail	22.8	24.5		22.0
		10%	1			
		PERME	22.8	22.4		22.6
	1000	Cloncurry	18.6	21.4		22.4
		Innisfail	20.4	21.6		25.3
	6 months	1%				
		PERME	24.5	22.6		22.4
		Cloncurry	21.4	21.6		24.5
	6	Innisfail	17.3	23.2		23.7
		10%	1 6 1			
		PERME	18.4	21.2		20.6
		Cloncurry	18 3	23.5		21.2
		Innisfail	19.0	25.1		22.8
	12 months					
	1.1	PERME	25.3	23.2		19.6
	P. S. Carlor	Cloncurry	34.8	21.1		20.7
		Innisfail	18.1	22.9		22.9
	1	10%				
		PERME	13.7	22.4		21.6
		Cloncurry	14.6	23.3		22.9
	1 Contraction	Innisfail	17.9	27.5		23.3
	65 months	1%				
		PERME	22.8	20.2		21.4
		Cloncurry	27.7	22.9		22.8
	1	Innisfail	26.4	21.6		23.2
	1.1.1.1.1.1.	10%	1			
		PERME	20.4	20.8		23.2
		Cloncurry	20.4	21.7		22.1
		Innisfail	23.2	25.4		23.3

DIFFERENCES BETWEEN MEANS, N, REQUIRED AT 99.9% PROBABILITY

Bffect	0					Set				
BILECT	Source	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)
F	Overall	1.9	0.8	0.6	1.0	0.5	0.8	1.2	0.8	
R	Nylon	6.7	2.4	1.8		1.6	2.4	3.5	2.4	1.1
R	Cotton	0.7	0.2	0.1		0.2	0.2	0.2	0.2	
R	Overal1	2.6	1.1	0.9	1.1.1.1	0.7	1.1	1.7	1.1	
FR	Overal1	5.4	2.3	1.7		1.5	2.2	3.2	2.2	
T	Nylon	4.7		1.8		1.6	3.0	4.3	2.8	1.3
T	Cotton	0.5	1	0.1	0.3	0.2	0.3	0.3	0.3	
T	Overal1	1.9		0.9	1.5	0.7	1.3	2.0	1.4	
FT	<b>Overall</b>	3.8		1.7	2.9	1.5	2.6	4.0	2.6	
L	Nylon		1.7			1.2				0.9
L	Cotton		0.1		0.2	0.2				
L	Overal1		0.8	the second	1.0	0.5				
rl.	Overall		1.6		2.1	1.0				
s	Nylon		2.1	1.6	100			Sec. 1		1.1
s	Cotton		0.1	0.1	0.2	4				
s	Overal1	-	1.0	0.8	1.3			-		
FS	Overal1		2.0	1.5	2.5					
RT	Nylon	13.3		5.2		4.6	8.4	17.1	8.0	3.2
RT	Cotton	1.4		0.4		0.6	0.8	0.8	0.9	
RT	Overall	5.4	1.11	2.5		2.1	3.6	5.6	3.7	
FRT	Overal1	10.7		4.8		4.0	7.3	11.3	7.6	
RL	Nylon		4.8	1.0		3.3				2.3
RL	Cotton		0.3			0.4		1000		
RL	Overall		2.3			1.5		-		
FRL	Overall		4.5		1.00	2.8		-		
RS	Nylon		5.9	4.5		2.0				2.8
RS	Cotton	1 million	0.4	0.3		and the second	1.11			2.0
RS	Overall		2.7	2.1				i in i		
FRS	Overall Overall		5.5	4.2				2.4		1
TL	Nylon	1 1 1	5.5	4.2		3.3				
TL	Cotton				0.6	0.4		and the second		2.7
TL.	Overall		- 40		2.9	13 8 C. 1 K 1				
FTL	Overall Overall	1.2 3	1 12 10		C 100 C 1 T 100	1.5	- Maria	12.3		
TS	Nylon	1	1 1.		5.9	2.8				
			1.1.1	4.5			39.57			3.2
TS	Cotton			0.3	0.7					
TS	Overall			2.1	3.1					
FTS	Overall	1		4.2	7.2					
LS	Nylon		4.1							2.3
LS	Cotton	1	0.3	1. N	0.5			1		

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FILECC						Set				
	source	(a)	(9)	(c)	(P)	(e)	(£)	(g)	(H)	(i)
TS 0	Overal1		2.0		2.5					
FLS 0	Overall		3.9		5.1					
RTL	Nylon					9.2				6.5
KTL 0	Cotton					1.2				
RTL	Overall					4.0				
FRTL	Overall					8.1				
RTS	Nylon			12.7						8.0
RTS C	Cotton			0.9						4
RTS 0	Overall			6.0						
FRTS	Overall			11.9						
TLS N	Nylon						6			6.5
TLS 0	Cotton				1.4					
TLS 0	<b>Overall</b>				7.2					
FTLS 0	Overall				14.4					
LSR	Nylon		11.7							5.6
LSR C	Cotton		0.7							
LSR 0	<b>Overall</b>		5.5							
FLSR 0	Overal1		11.0							
RTLS N	Nylon									15.9

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3	British	Methods of test for textiles: the resistance to tearing of
	Standards	woven fabrics by the wing-rip technique.
	Institution	BS Handbook 11, Method 4/110 (1974)

### **REPORT DOCUMENTATION PAGE**

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7. The

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16. Descripton (Keywords) (Descripton marked \* are selected from TEST)

Rubber-coated fabrics. Weathering. Wing-rip tear strength.

17. Abarnes

The wing-rip tear strengths of a nylon and of a cotton fabric, each coared with natural rubber, neoprene, polyurethane or chlorosulphonated polyethylene and exposed to various weathering conditions, were determined.

The coated sylos fabrics had higher test strengths than the cotton ones, were note variable. Polyursthans-coated sylos increased in test strength on exposure at two Australian sites, but natural subber coated cotton decreased on exposure in UL. Losd during obposite reduced the test strengths of the natural subber coated fabrics.