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ARMY MISSILE RESEARCH AND DEVELOPMENT COMMAND REDSTO--ETC F/G 20/4
USER'S MANUAL FOR THE MARTIN-MARIETTA HIGH ANGLE OF ATTACK AERO--ETC(U)
JUN 78 G C WINN

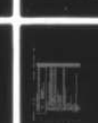
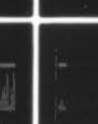
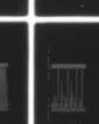
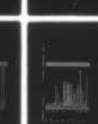
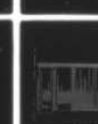
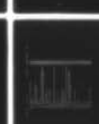
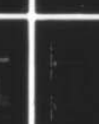
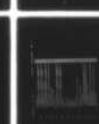
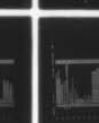
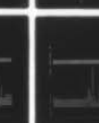
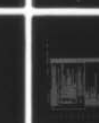
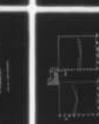
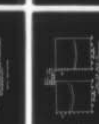
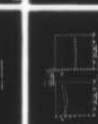
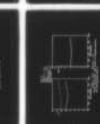
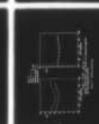
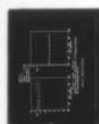
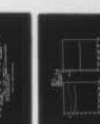
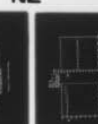
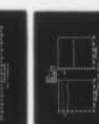
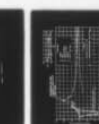
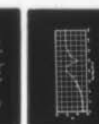
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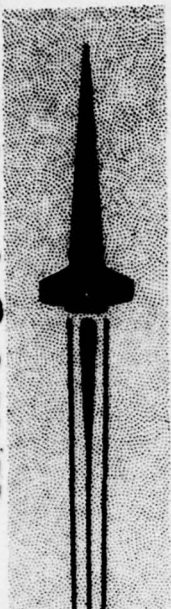
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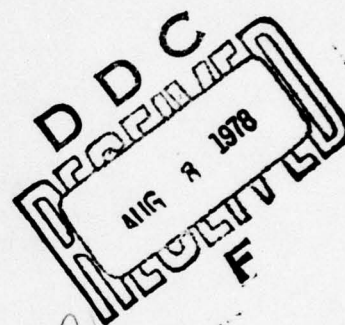


TECHNICAL REPORT T-78-63

**USER'S MANUAL FOR THE MARTIN-MARIETTA
HIGH ANGLE OF ATTACK AERODYNAMIC
METHODOLOGY FOR BODY-TAIL MISSILES**

Gary C. Winn
Aeroballistics Directorate
Technology Laboratory

JUNE 1978



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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report documents the computer program developed by the Army to evaluate and implement an aerodynamic methodology developed by the Martin Marietta Corporation. The methodology was developed to predict aerodynamic forces on slender missile bodies with low aspect ratio tails at low and high angles of attack, at arbitrary roll angles for both transonic and supersonic velocities.		

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I. INTRODUCTION

The Martin Marietta Corporation, Orlando Division, has developed an aerodynamic methodology and published a report (Ref. 1) under Contract No. DAAH01-74-C-0621 with the US Army. The report describes the development and application of semiempirical methods for predicting aerodynamic characteristics of slender body and body-tail configurations.

In an effort to evaluate the Martin Methodology, a computer program was developed to incorporate the various theoretical and empirical procedures called for in the Martin report. The results of this evaluation are covered in detail in Ref. 2. As a follow-up to the Martin Methodology analysis, a few modifications of the methodology were accomplished in an attempt to correct certain disagreements found between measured experimental data and associated predictions derived from the methodology.

This report is intended to be a user's guide for the use of the methodology program. The methods and procedures used in developing the aerodynamic methodology are covered extensively in Ref. 1 and only those modifications to the methodology implemented by the Army will be discussed in this report.

II. PROGRAM CAPABILITIES

The Aerodynamic Methodology Program can predict aerodynamic characteristics of slender body and body-tail missile configurations, to include the following predictions:

- 1) Body alone normal force, center of pressure, and axial force.
- 2) Isolated tail panel normal force and center of pressure.
- 3) Mutual interference effects that enable the prediction of normal force and center of pressure of body-tail combinations.

The program in its present form was developed to predict these characteristics for missiles with four fins in cruciform configuration, with the fin trailing edges flush with the missile body base. The fin numbering convention, as well as the conventions for angle of attack (α) and roll angle (ϕ), are shown in Figure 1.

The range of input parameters for the program are:

- | | |
|-------------------------------------|---|
| 1) Mach number | 0.8 to 3.0 |
| 2) Angle of attack | 0 to 180 for isolated components
(roll angle = 0). 0 to 45 for
body-tail combinations at arbitrary
roll angles from 0 to 180 . |
| 3) Tail leading edge
sweep angle | 0 to 70 degrees |

- | | |
|------------------------------------|---|
| 4) After-body length
(calibers) | 6 to 18 |
| 5) Nose length
(calibers) | 1.5 to 3.5 |
| 6) Tail taper ratio | 0 to 1 |
| 7) Tail aspect ratio | .5 to 2.0 (aspect ratio of two
tail panels joined at root chord) |

III. DISCUSSION

Certain modifications of the original methodology were incorporated into the methodology computer program. These modifications were an attempt to correct certain disagreements between experimentally obtained data and associated predictions from the methodology which became apparent during an evaluation of the **original methodology** (Ref. 2).

The modifications are limited to the body alone normal force prediction methods and involve the addition of newly obtained unpublished data. Specifically, equation 16, page 36 as depicted in Figure 20 of Ref. 1, has been eliminated and replaced by values of η (correlation factor for end effects) as shown in Figure 2 of this report. In addition, the crossflow drag coefficient versus crossflow Mach number curve shown in Figure 22a of Ref. 1, has been replaced by Figure 3 of this report.

Comparisons of predictions generated from the original methodology and those with the above modifications, compared with the experimental data, are shown in Figures 4 through 10 of this report.

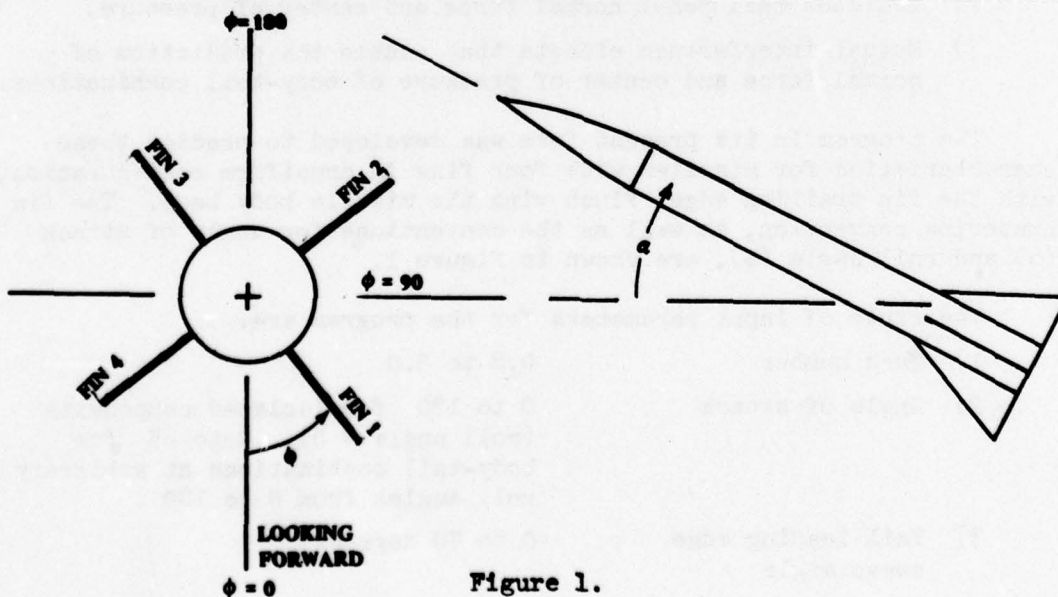


Figure 1.

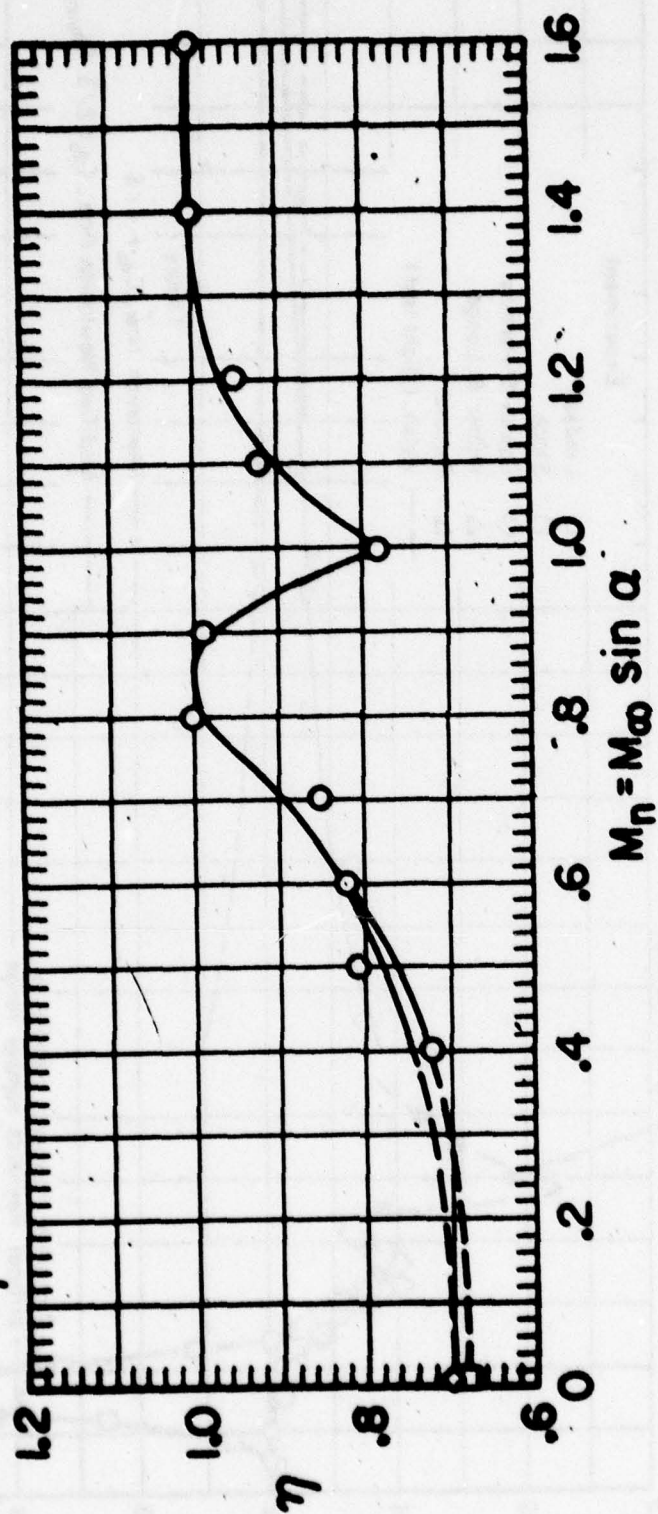


Figure 2. Values of η .

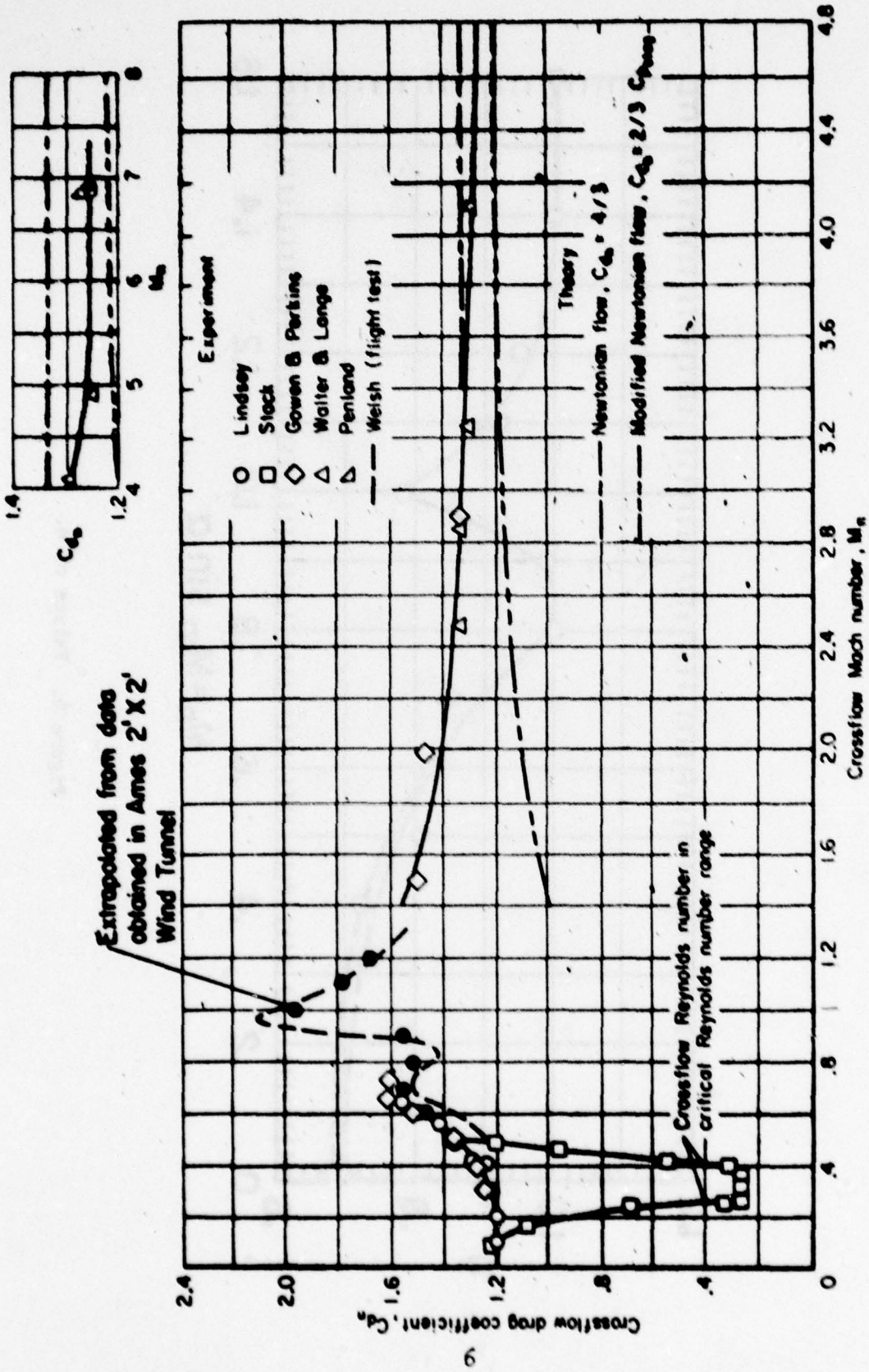


Figure 3. Unpublished data.

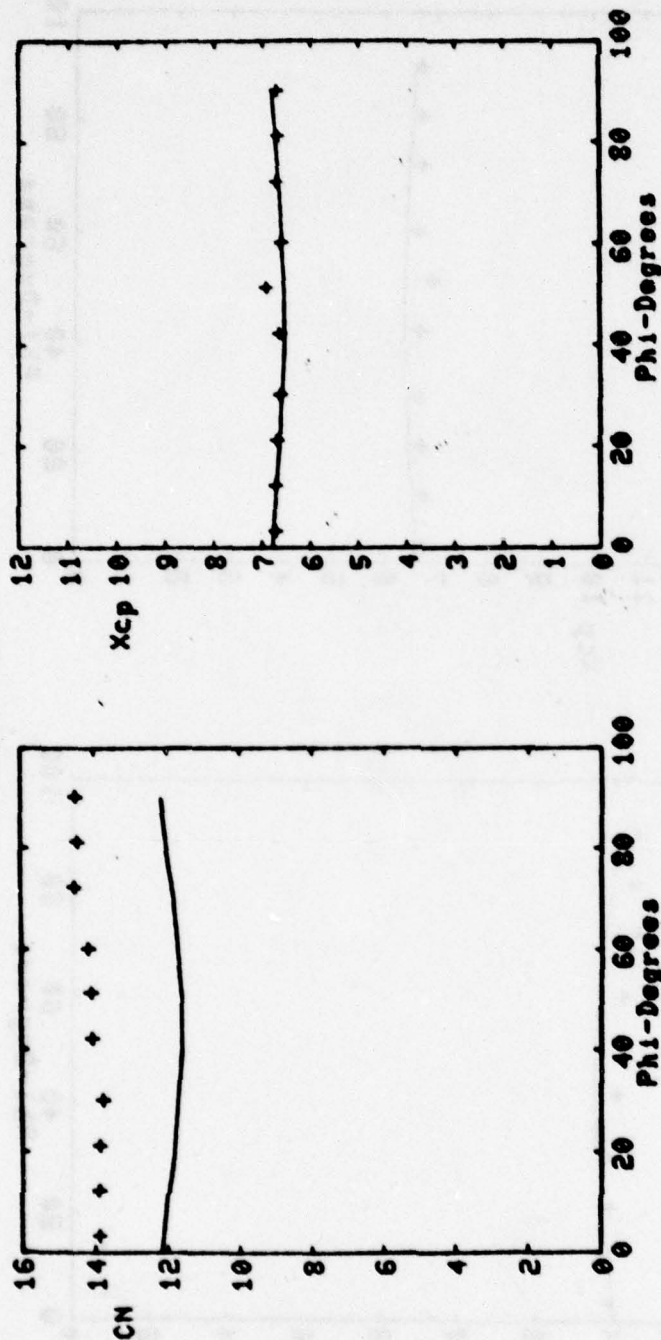
B3T1-5

Mach No = 1

Alpha = 44.92

Methodology--(-)

Experiment---(+)



Alpha = 44.92 Mach No = 1

Normal Force Coeff. And Center of Pressure Location
For Configuration B3T1-5

Figure 4a. Original methodology.

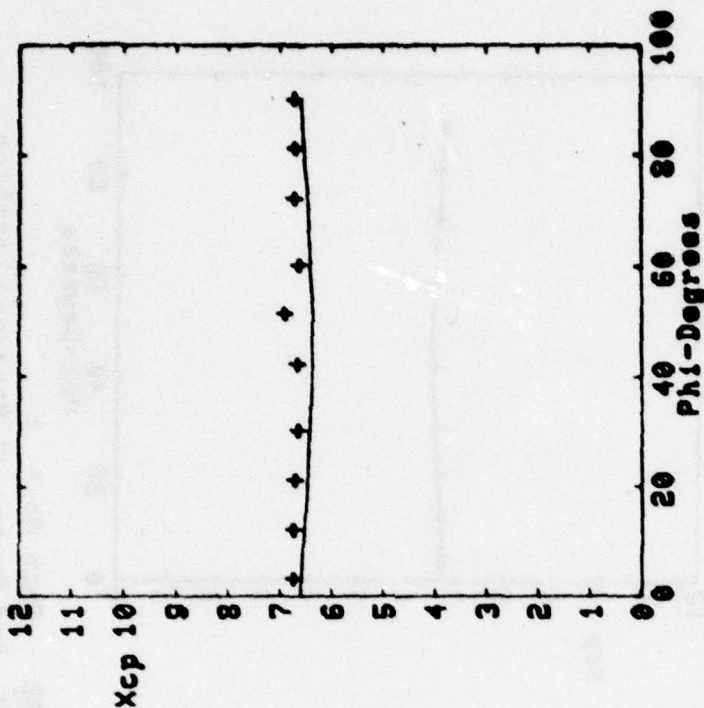
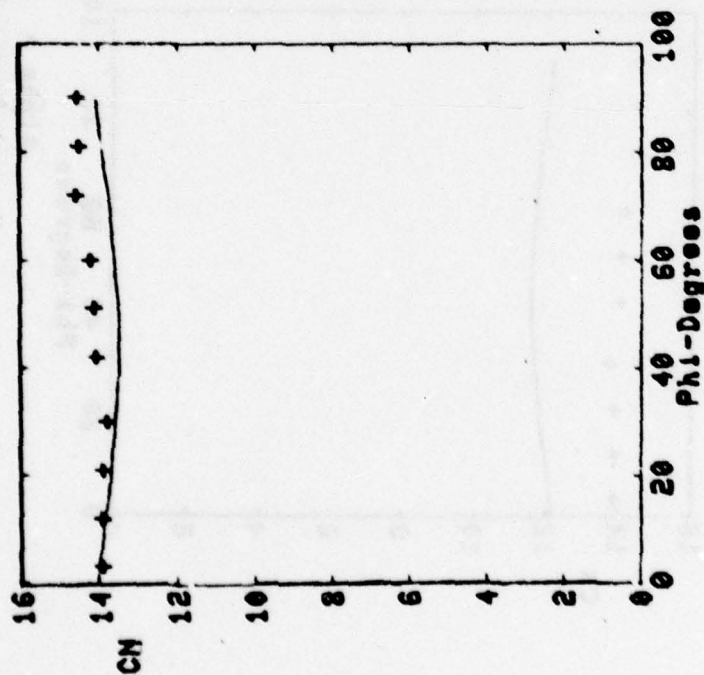
B371-5

Mach No. = 1

Alpha = 44.92

Methodology--(-)

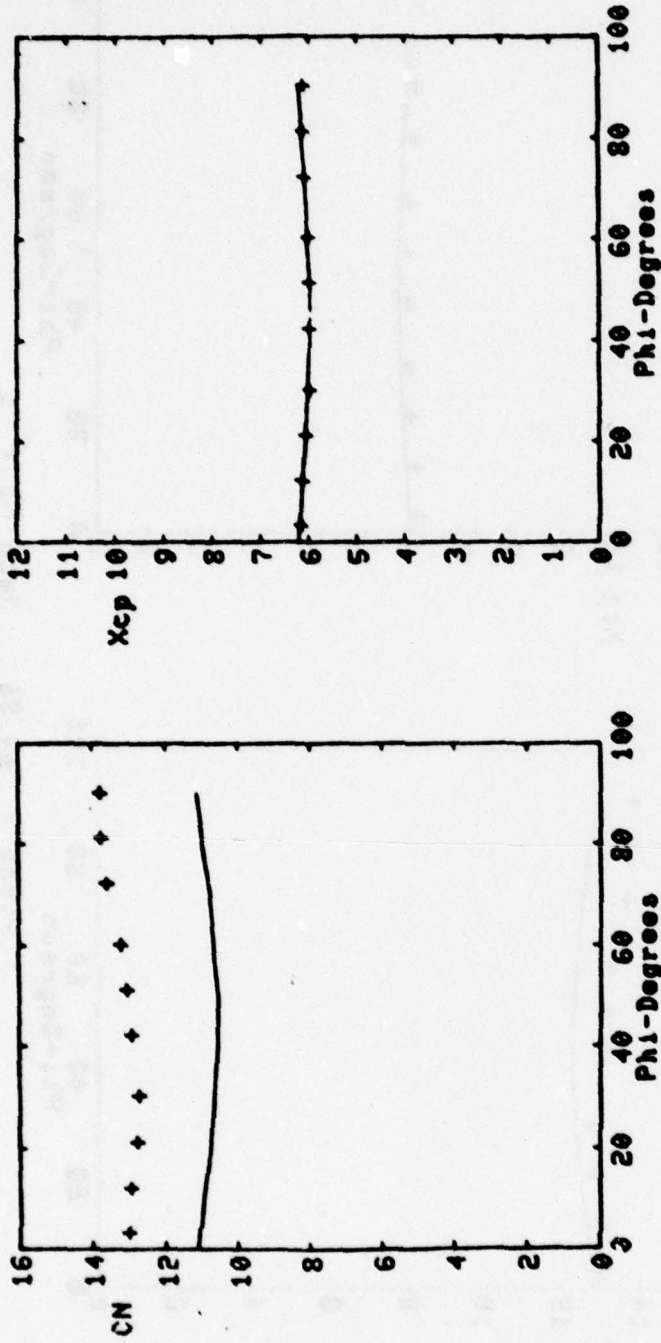
Experiment---(+)



Alpha = 44.92 Mach No. = 1
Normal Force Coeff. And Center of Pressure Location
For Configuration B371-5

Figure 4b. Modified methodology.

B2T1-5
Mach No. = 1
Alpha = 44.88
Methodology--(-)
Experiment---(+)



Alpha = 44.88 Mach No. = 1
Normal Force Coeff. And Center of Pressure Location
For Configuration B2T1-5

Figure 5a. Original methodology.

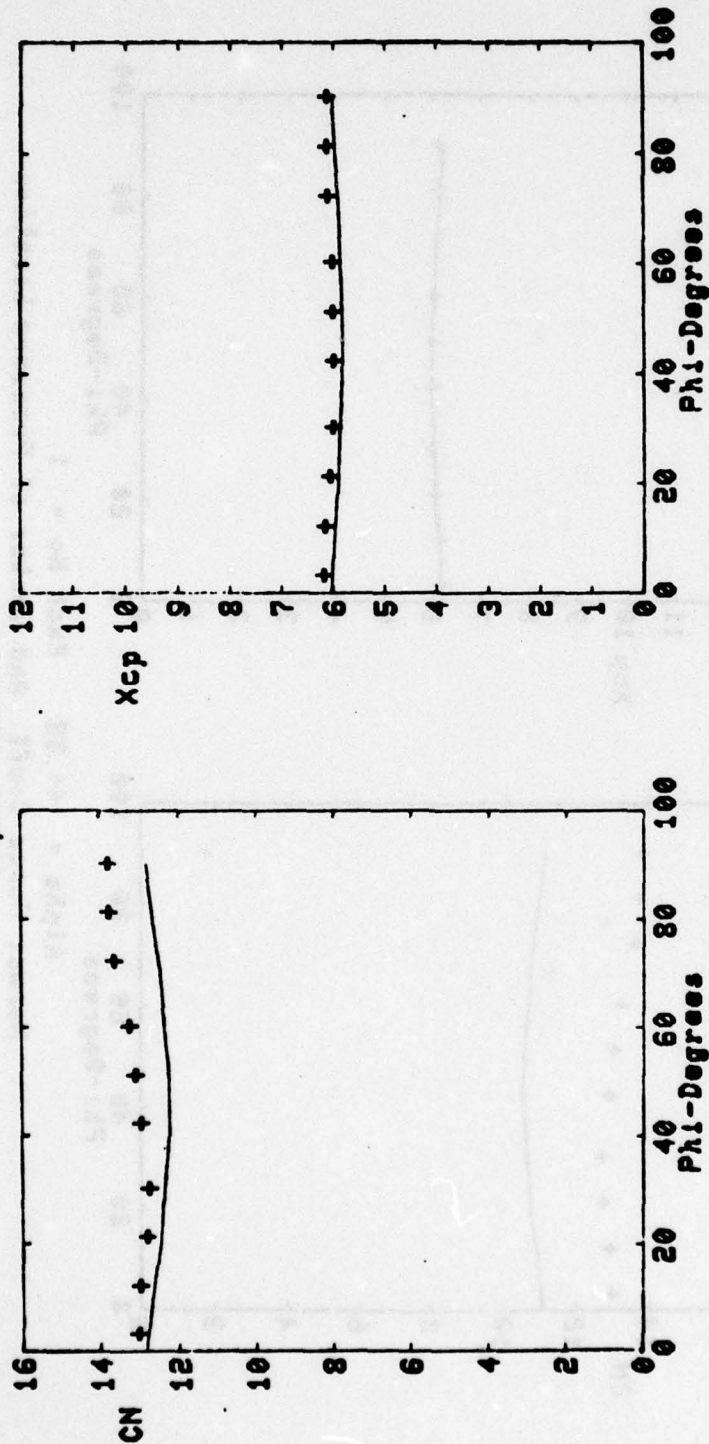
B2T1-5

Mach No. = 1

Alpha = 44.88

Methodology--(-)

Experiment---(+)



Alpha = 44.88 Mach No. = 1

Normal Force Coeff. And Center of Pressure Location

For Configuration B2T1-5

Figure 5b. Modified methodology.

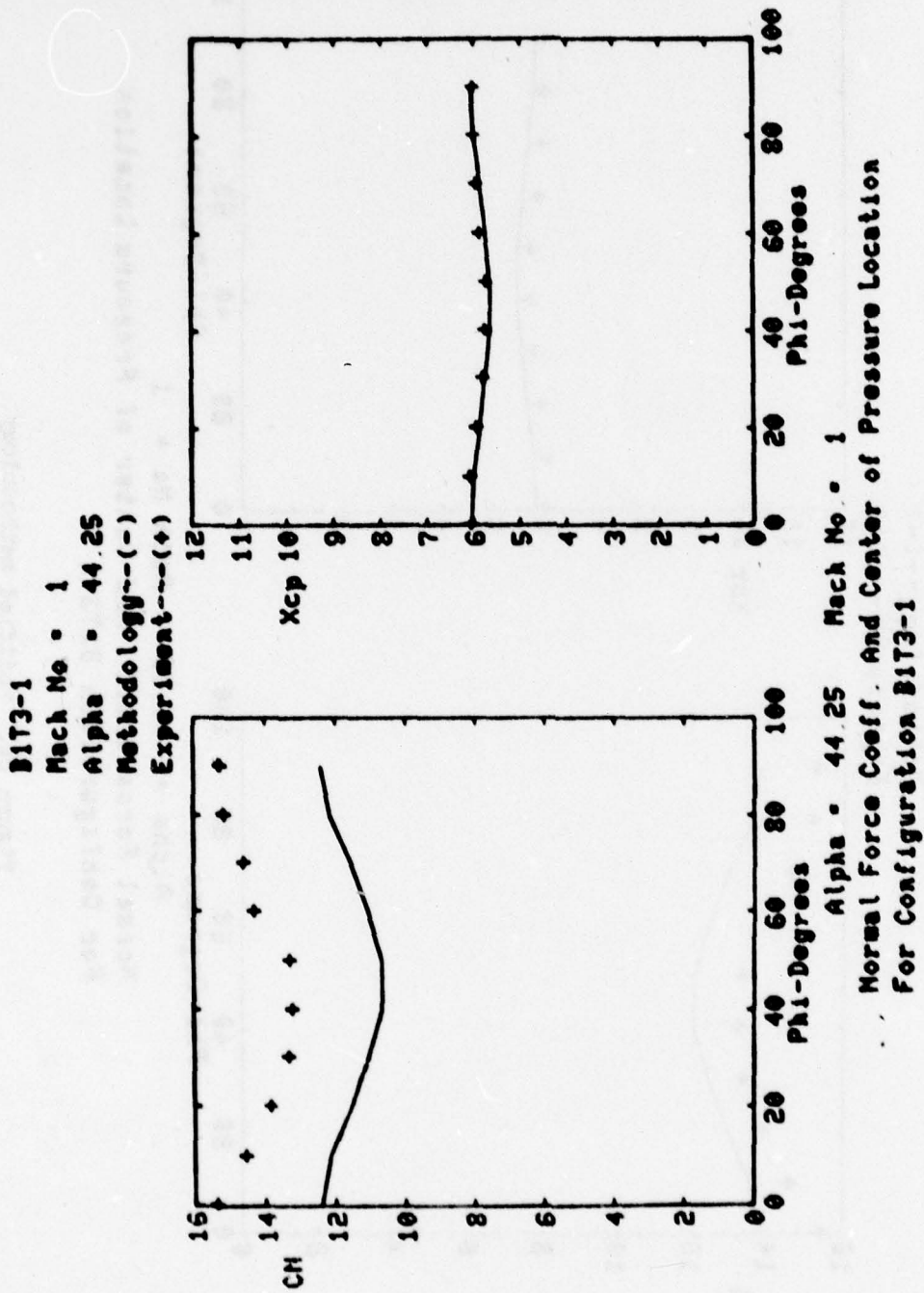
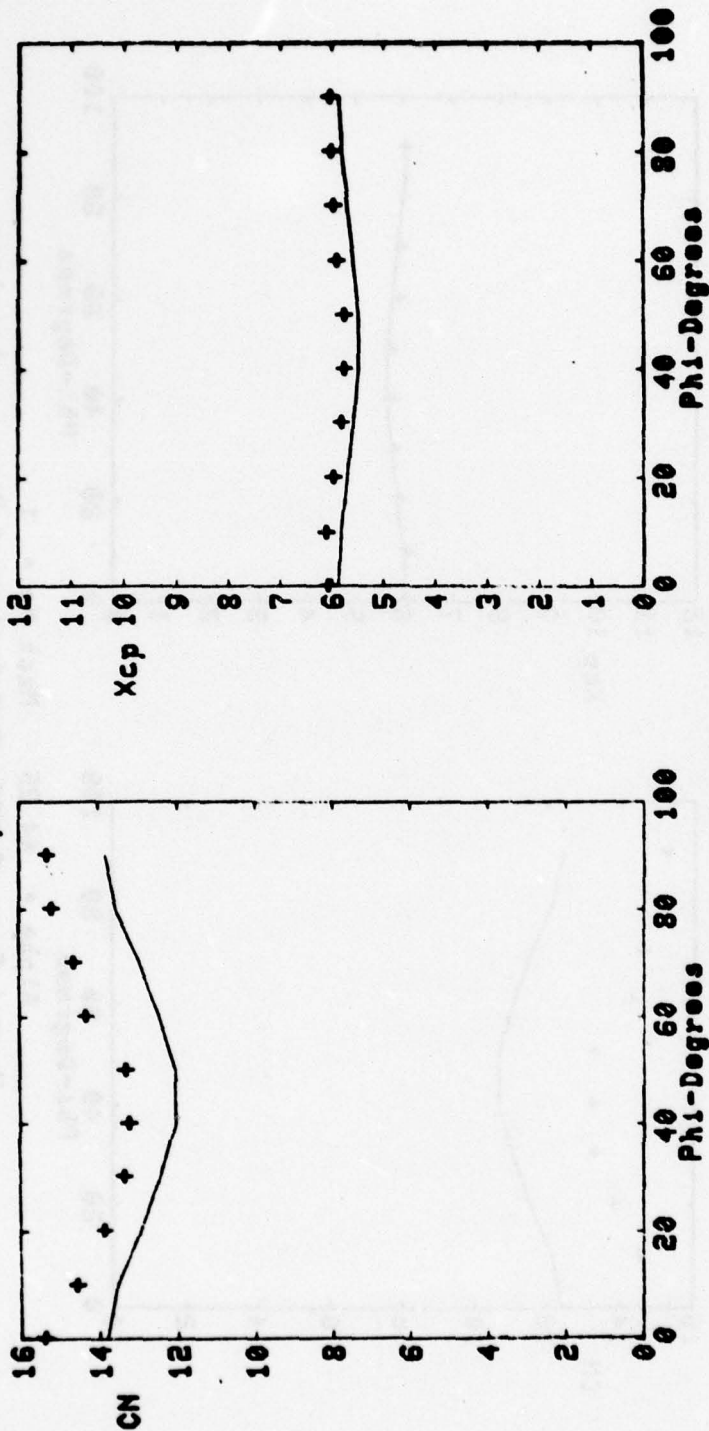


Figure 6a. Original methodology.

B1T3-1
Mach No. = 1
Alpha = 44.25
Methodology--(-)
Experiment---(+)



Alpha = 44.25 Mach No. = 1
Normal Force Coeff. And Center of Pressure Location
For Configuration B1T3-1

Figure 6b. Modified methodology.

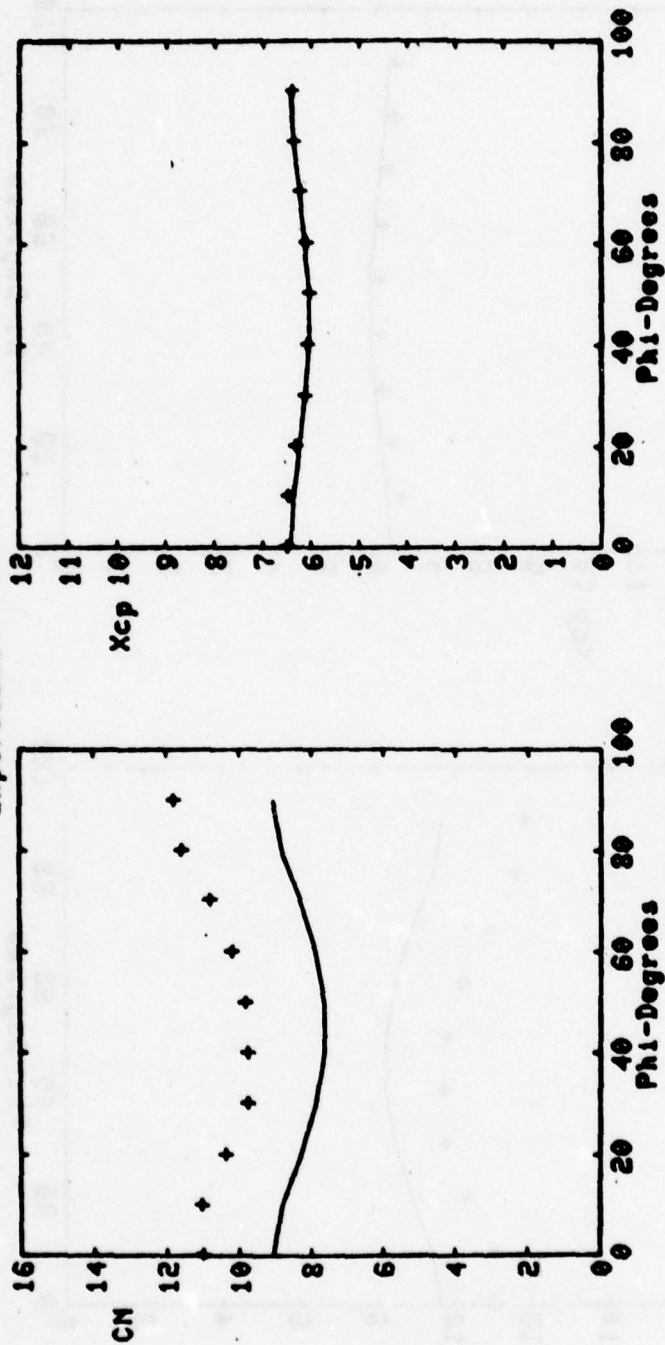
BIT3-1

Mach No. = 1

Alpha = 34.95

Methodology--(-)

Experiment---(+)



Alpha = 34.95 Mach No. = 1
Normal Force Coeff. And Center of Pressure Location
For Configuration BIT3-1

Figure 7a. Original methodology.

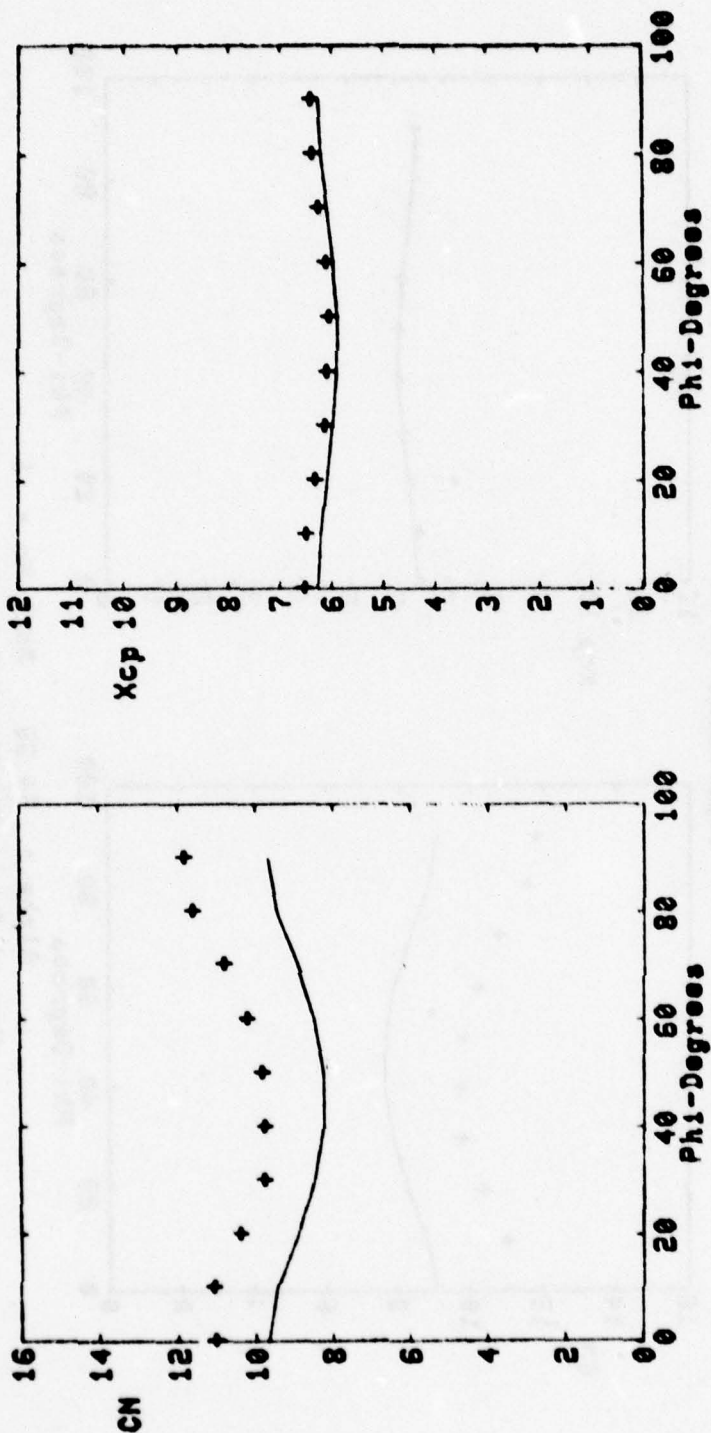
B1T3-1

Mach No. = 1

Alpha = 34.95

Methodology--(-)

Experiment---(+)



Alpha = 34.95 Mach No. = 1
Normal Force Coeff. And Center of Pressure Location
For Configuration B1T3-1

Figure 7b. Modified methodology.

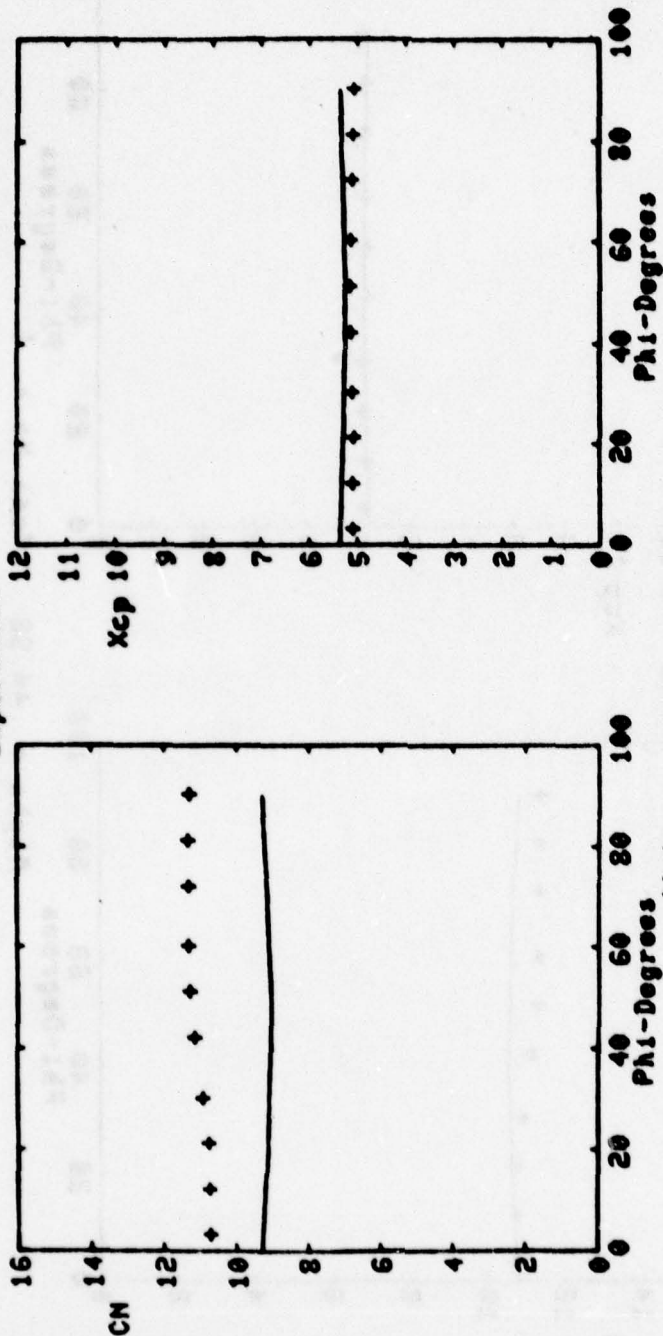
B1T2-3

Mach No. = 1

Alpha = 44.92

Methodology--(-)

Experiment---(+)



Alpha = 44.92 Mach No. = 1

Normal Force Coeff. And Center of Pressure Location

For Configuration B1T2-3

Figure 8a. Original methodology.

B1T2-3

Mach No. = 1
 Alpha = 44.92
 Methodology--(-)
 Experiment---(+)

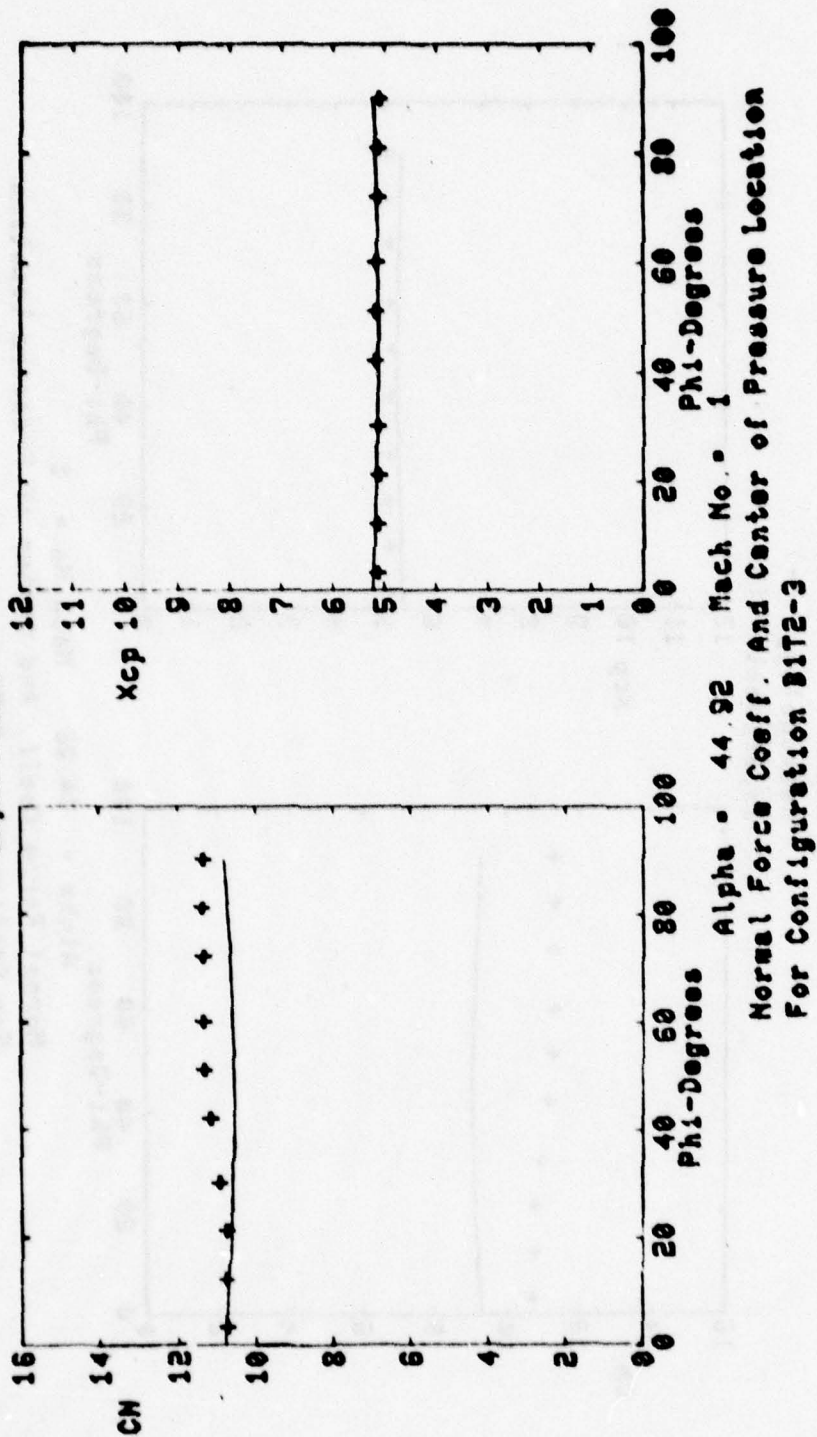
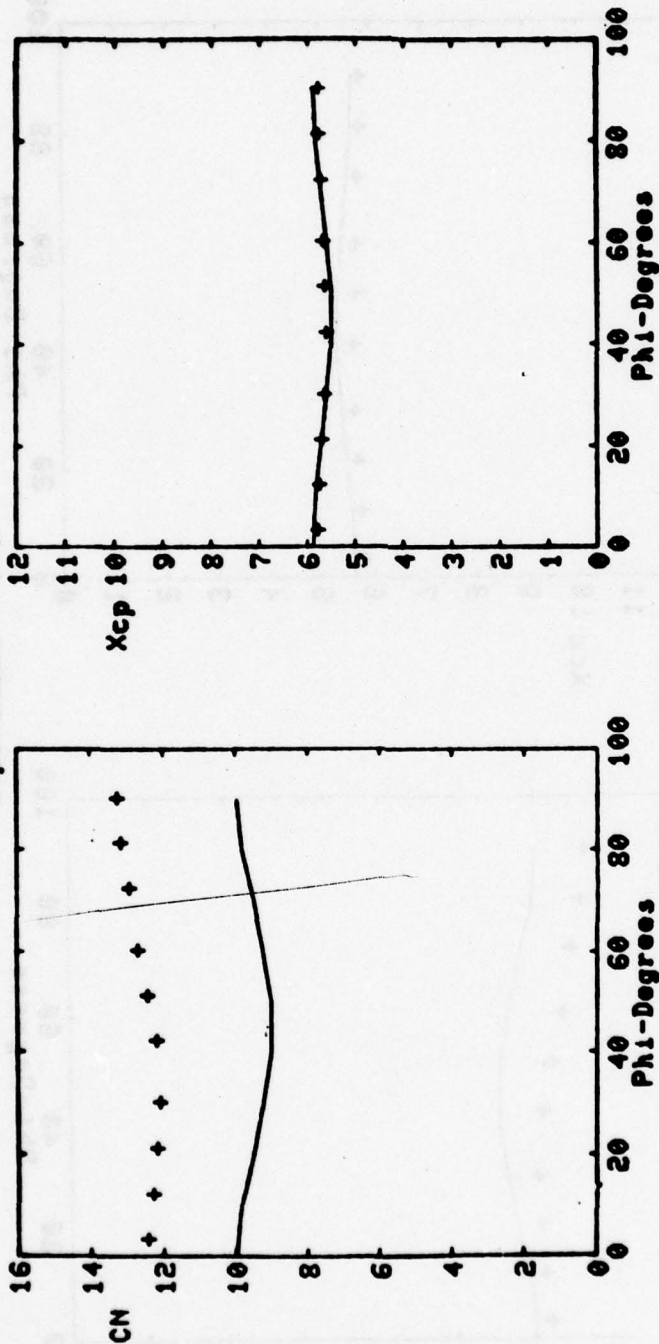


Figure 8b. Modified methodology.

B1T1-4
 Mach No. = 1.2
 Alpha = 44.9
 Methodology---(--)
 Experiment---(+)



Alpha = 44.9 Mach No. = 1.2
 Normal Force Coeff. And Center of Pressure Location
 For Configuration B1T1-4

Figure 9a. Original methodology.

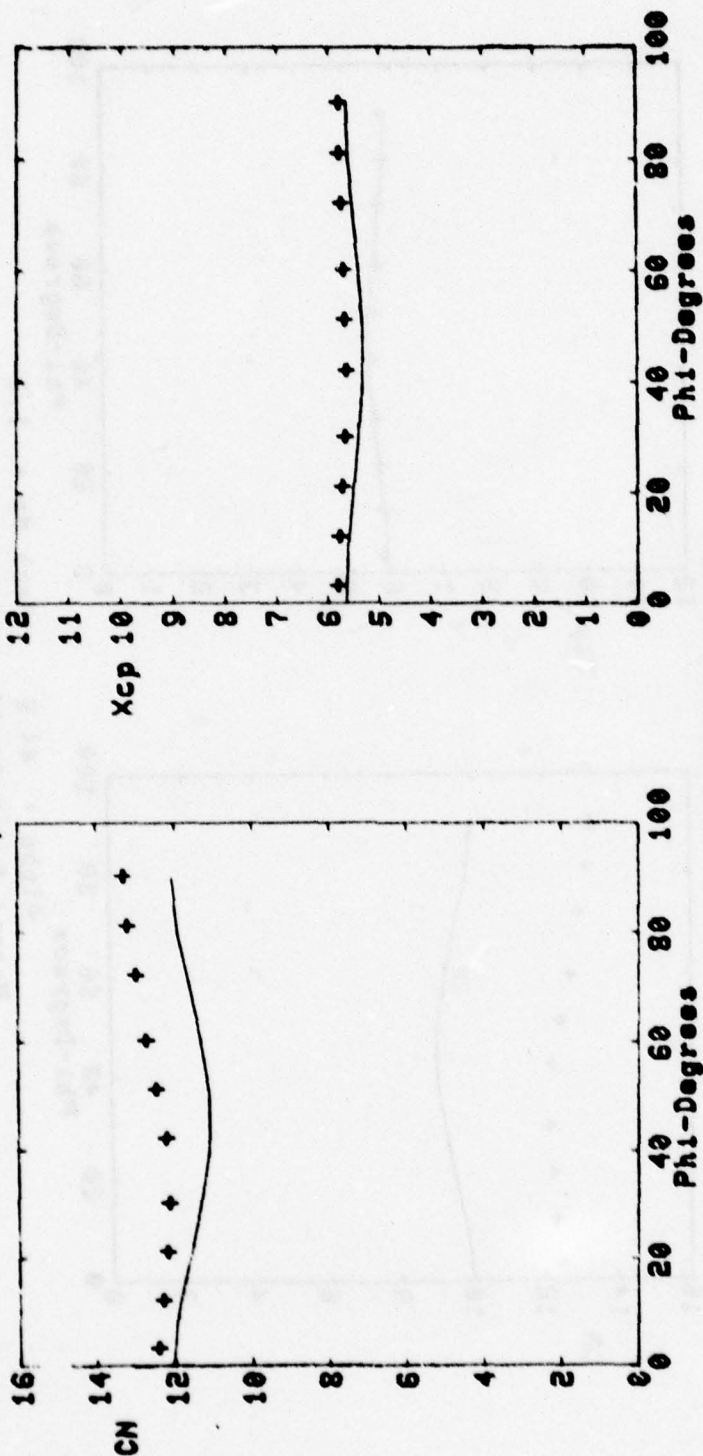
B1T1-4

L. 2

Alpha = 44.9

Methodology--(-)

Experiment---(+)



Alpha = 44.9 Mach No. = 1.2
 Normal Force Coeff. And Center of Pressure Location
 For Configuration B1T1-4

Figure 9b. Original methodology.

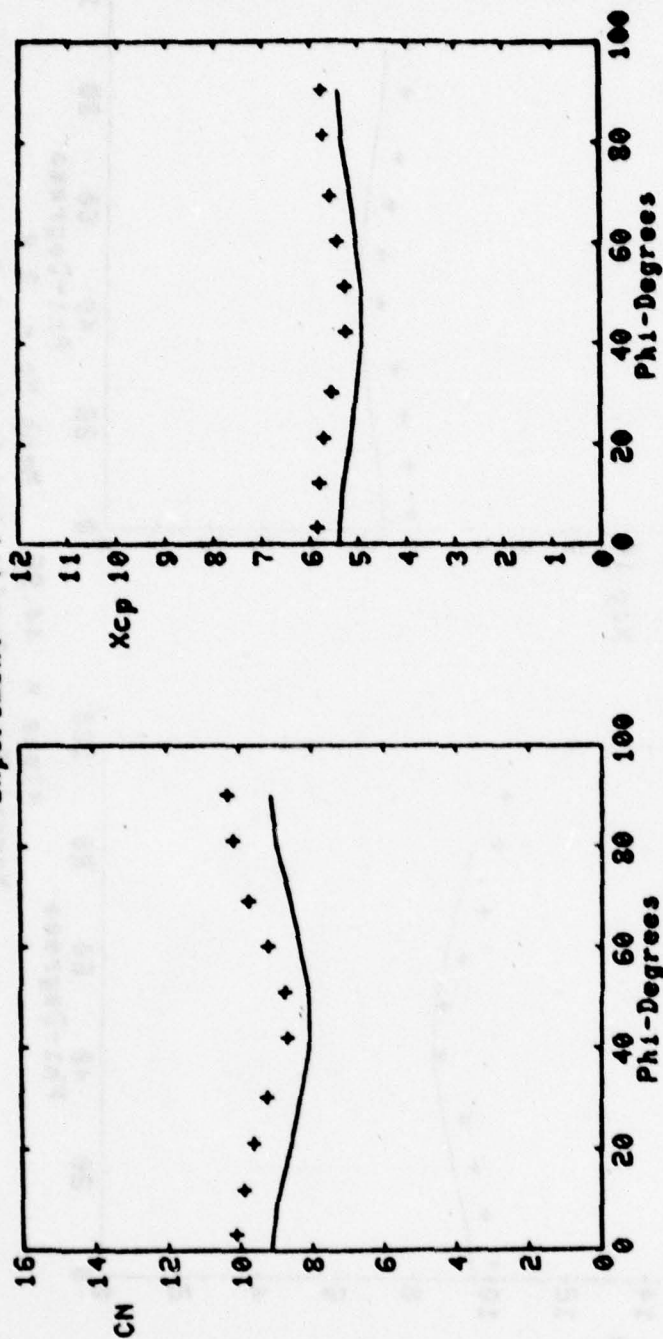
B1T1-4

Mach No. = 0.8

Alpha = 44.95

Methodology--(-)

Experiment---(+)



Alpha = 44.95 Mach No. = 0.8
Normal Force Coeff. And Center of Pressure Location
For Configuration B1T1-4

Figure 10a. Original methodology.

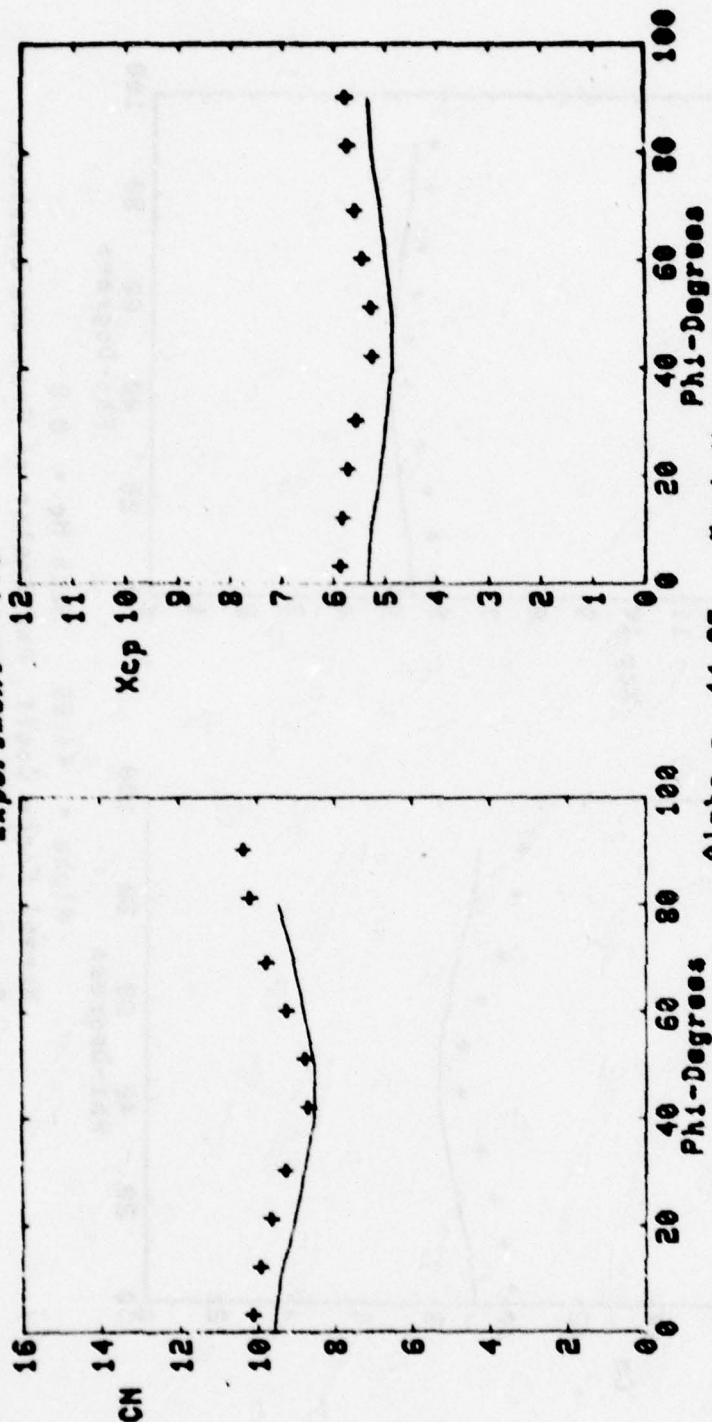
B1T1-4

Mach No. = 0.8

Alpha = 44.95

Methodology--(-)

Experiment---(+)



Alpha = 44.95 Mach No. = 0.8
Normal Force Coeff. And Center of Pressure Location
For Configuration B1T1-4

Figure 10b. Modified methodology.

Appendix A. PROGRAM UTILIZATION

The proper format and sequence for the input cards are shown in Table A-1.

TABLE A-1.

CARD	SYMBOL REFERENCE	FORMAT(FORTRAN)
1	Title card for each configuration	12A6
2	AR,S,CR,LAMDA,ALE	5F10.3
3	LND,LAD,D	3F10.3
4	ALF1,ALF2,DELAF,MACH,RN,OPTPHI, OPTMAC	4F10.3,F13.2,2I2

- AR = Tail aspect ratio (two tail panels joined at root chord)
- S = Tail Semispan including body, $(b + D)/2$, inches
- CR = Tail root chord - Inches
- LAMDA = Tail taper ratio
- ALE = Tail leading edge sweep angle - Degrees
- LND = Nose length - Calibers
- LAD = After-body length - Calibers
- D = Body diameter - Inches
- ALF1 = Beginning angle of attack for angle of attack sweep - Deg.
- ALF2 = Ending angle of attack for angle of attack sweep - Deg.
- DELAF = Angle of attack increment for alpha sweep - Degrees
- MACH = Free stream Mach number
- RN = Reynolds number - /Ft.
- OPTPHI = 1 to calculate aerodynamic coefficients as a function of roll angle. Roll angle is automatically varied between 0° and 90° in increments of 10° . No additional data cards are required. See Sample Configuration 2 Input Data.
- = 0 to delete calculation of aerodynamic coefficients as a function of roll angle
- OPTMAC = 1 allows for multiple Mach numbers for the configuration and angle of attack range determined by the four cards Table A-1. Additional Mach numbers are added after the four cards of Table A-1, one Mach number per card using F10.3 Format
- = 0 for single Mach number only

MULTIPLE CASE CAPABILITY:

Additional configurations can be input simply by repeating the card sequence of Table A-1.

If OPTMAC = 1, however, a blank card must follow the last Mach number card before the program will accept additional configurations.

Table A-2 shows a sample input card arrangement. Using this input card arrangement the program will predict aerodynamic coefficients for sample configuration No. 1 for Mach No. equal .8 and for angles of attack from 0.0 to 45. degrees in 5 degree increments. Since OPTPHI is 0 for sample configuration No. 1, the coefficients will be given versus angle of attack only (roll angle equals 0 degrees). Now, OPTMAC equals 1, therefore additional predictions will be made for the same configuration and angle of attack range for Mach numbers: .9, 1.0, 1.1, 1.2, and 1.3. A blank card follows the Mach number cards for sample configuration No. 1, which signals the program to read additional configurations.

The program then reads the cards for sample configuration No. 2, and computes the predictions of the aerodynamic coefficients and centers of pressure for this configuration. Now, since OPTPHI equals 1 in this case, these predictions will be given as a function of roll angle, for the angle of attack range 0 to 40 degrees. Also, since OPTMAC equals 0 for this case, the predictions will be made for Mach No. equal 2.0 only.

The resulting output for these sample input cards are found in Table A-3.

As a guide for time and storage requirements, the following figures for the CDC 6600 are provided:

Compile Time	-	14 seconds
Execution Time	-	2 seconds
Storage	-	Less than 100K.

TABLE A-3.

SAMPLE CONFIGURATION 1 OPTPHI=0, OPTMAC=1					
I	INPUT PARAMETERS				
I	MACH = .80				
I	TAIL ASPECT RATIO = 1.00				
I	TAIL TAPER RATIO = 0.00				
I	TAIL L-E. SWEEP ANGLE = 75.96 DEGREES				
I	TAIL ROOT CHORD = 7.500				
I	NOSL LENGTH = 3.000 CAL.				
I	AFTER BODY LENGTH = 7.000 CAL.				
I	BODY DIAMETER = 3.75				
I	TAIL SEMI-SPAN (INCLUDING BODY) = 3.75				
I	REYNOLDS NUMBER = 7000000.00				

OUTPUT DEFINITIONS					
I	CNB	XCPB	I	KCPT	I
I	CNB = BODY ALONE NORMAL FORCE COEFFICIENT				
I	XCPB = BODY ALONE CENTER OF PRESSURE				
I	CNT = TAIL ALONE NORMAL FORCE COEFFICIENT				
I	KCPT(B) = TAIL ALONE CENTER OF PRESSURE				
I	CNT(B) = TAIL IN PRESENCE OF BODY NORMAL FORCE COEFFICIENT				
I	KCPT(B) = TAIL (IN PRESENCE OF BODY) CHORDWISE CENTER OF PRESSURE/TAIL ROOT CHORD (MEASURED AFT FROM ROOT CHORD LEADING EDGE)				
I	YCPT(B) = TAIL (IN PRESENCE OF BODY) SPANWISE CENTER OF PRESSURE/TAIL SEMI-SPAN (EXCLUDING BODY)				
I	KCPT(B-T) = CENTER OF PRESSURE OF BODY PLUS TAIL (BODY) MEASURED OUTWARD FROM BODY CONFIGURATION (CAL. FROM NOSE)				
I	CNT(B-T) = NORMAL FORCE COEFFICIENT OF BODY PLUS TAIL CONFIGURATION				
I	CA = AXIAL FORCE COEFFICIENT				

ISOLATED COMPONENTS					
I	ALPHA I	CNB	I	XCPB	I
I	0.00	0.000	2.545	0.000	.651
I	5.00	.245	2.741	.140	.691
I	10.00	.612	3.181	.307	.643
I	15.00	.961	3.649	.494	.632
I	20.00	.888	3.927	.695	.620
I	25.00	1.151	3.927	.906	.616
I	30.00	1.652	3.927	1.234	.611
I	35.00	3.695	3.927	1.220	.617
I	40.00	5.701	3.927	.967	.632
I	45.00	7.039	3.927	1.213	.628
I					1.239

SAMPLE CONFIGURATION 1 OPTPHI=0, OPTMAC=1

INPUT PARAMETERS	
MACH =	.90
TAIL ASPECT RATIO =	1.00
TAIL TAPER RATIO =	0.00
TAIL L-E. SHEEP ANGLE =	75.96 DEGREES
TAIL ROOT CHORD =	7.500
NOSE LENGTH =	3.000 CAL.
AFTER BODY LENGTH =	7.000 CAL.
BODY DIAMETER =	3.75
TAIL SEMI-SPAN (INCLUDING BODY) =	3.75
REYNOLDS NUMBER =	7000000.00

OUTPUT DEFINITIONS

CMB =	BODY ALONE NORMAL FORCE COEFFICIENT
KCPB =	BODY ALONE CENTER OF PRESSURE
CNT =	TAIL ALONE NORMAL FORCE COEFFICIENT
KCPT =	TAIL ALONE CENTER OF PRESSURE
CNT(B) =	TAIL (IN PRESENCE OF BODY) NORMAL FORCE COEFFICIENT
KCPT(B) =	TAIL (IN PRESENCE OF BODY) CHORDWISE CENTER OF PRESSURE/TAIL ROOT CHORD (MEASURED AFT FROM ROOT CHORD LEADING EDGE)
YCPT(B) =	TAIL (IN PRESENCE OF BODY) SPANWISE CENTER OF PRESSURE/TAIL SEMI-SPAN (EXCLUDING CENTER OF PRESSURE OF BODY PLUS TAIL BODY) MEASURED OUTWARD FROM BODY CONFIGURATION (CAL. FROM NOSE)
CNT(B+T) =	NORMAL FORCE COEFFICIENT OF BODY PLUS TAIL CONFIGURATION
CA =	AXIAL FORCE COEFFICIENT

ISOLATED COMPONENTS		BODY TAIL CONFIGURATION		BODY TAIL CONFIGURATION		BODY TAIL CONFIGURATION		BODY TAIL CONFIGURATION	
ALPHA	CMB	KCPB	CNT	KCPT	CNT(B)	KCPT(B)	YCPT(B)	CNT(B+T)	CA
0.00	0.000	2.729	0.000	.651	0.000	.651	.335	0.000	.305
5.00	.246	2.880	.143	.651	.207	.648	.335	.708	.298
10.00	.604	3.223	.311	.644	.436	.633	.335	1.534	.275
15.00	.894	3.596	.497	.632	.664	.619	.335	2.266	.238
20.00	.893	3.835	.696	.621	.864	.613	.316	2.658	.168
25.00	1.195	3.835	.903	.616	1.017	.617	.301	3.254	.166
30.00	2.782	3.835	1.239	.612	1.241	.624	.282	5.213	.126
35.00	4.615	3.835	1.192	.618	1.192	.631	.282	7.050	.065
40.00	6.240	3.835	.991	.623	1.004	.638	.282	8.482	-.018
45.00	8.114	3.835	1.218	.629	1.253	.644	.282	10.701	-.120

EXAMPLE CONFIGURATION 1 OPTPHI=0, OPTMAC=1

INPUT PARAMETERS

MACH = 1.00
 TAIL ASPECT RATIO = 1.00
 TAIL TAPER RATIO = 0.00
 TAIL L-E SKEW ANGLE = 75.96 DEGREES
 TAIL ROOT CHORD = 7.500
 NOSE LENGTH = 3.000 CAL.
 AFTER BODY LENGTH = 7.000 CAL.
 BODY DIAMETER = 1.75
 TAIL SEMI-SPAN (INCLUDING BODY) = 3.75
 REYNOLDS NUMBER = 7000000.00

OUTPUT DEFINITIONS

CNB = BODY ALONE NORMAL FORCE COEFFICIENT
 XCPH = BODY ALONE CENTER OF PRESSURE
 CNT = TAIL ALONE NORMAL FORCE COEFFICIENT
 XCPH = TAIL ALONE CENTER OF PRESSURE
 CNT(B) = TAIL IN PRESENCE OF BODY'S NORMAL FORCE COEFFICIENT
 XCPH(B) = TAIL (IN PRESENCE OF BODY) CHORDWISE CENTER OF PRESSURE/TAIL ROOT CHORD (MEASURED LEFT FROM ROOT CHORD LEADING EDGE)
 YCPT(B) = TAIL (IN PRESENCE OF BODY) SPANWISE CENTER OF PRESSURE/TAIL SEMI-SPAN (EXCLUDING BODY)
 XCPH(B*) = CENTER OF PRESSURE OF BODY PLUS TAIL BODY MEASURED OUTWARD FROM BODY
 CONFIGURATION (SCALE FROM NOSE)
 CNT(B*) = NORMAL FORCE COEFFICIENT OF BODY PLUS TAIL CONFIGURATION
 CA = AXIAL FORCE COEFFICIENT

ALPHA I	ISOLATED COMPONENTS				BODY TAIL CONFIGURATION							
	CNB	XCPH	CNT	XCPH	CNT(B)	XCPH(B)	YCPT(B)	CNT(B*)	XCPH(B*)	YCPT(B*)	CA	I
.00	0.000	2.669	0.000	.652	0.000	.652	.335	0.000	0.000	7.097	.400	I
.00	.246	3.056	.146	.652	.214	.649	.335	.724	.724	7.097	.392	I
.00	.590	3.260	.719	.645	.447	.635	.335	1.544	1.544	6.907	.370	I
.00	.648	3.496	.505	.635	.475	.622	.335	2.046	2.046	7.360	.333	I
.00	.897	3.676	.703	.624	.873	.617	.316	2.677	2.677	7.314	.283	I
.20	1.737	3.836	.907	.620	1.821	.621	.301	3.812	3.812	5.716	.285	I
.40	3.858	3.874	1.266	.616	1.271	.627	.262	6.336	6.336	5.980	.234	I
.60	4.930	4.062	1.147	.621	1.144	.633	.282	7.310	7.310	5.722	.186	I
.80	7.082	4.180	1.058	.626	1.045	.640	.262	9.431	9.431	5.429	.130	I
.00	8.954	4.317	1.258	.632	1.309	.646	.282	11.654	11.654	5.427	.038	I

AMPLE CONFIGURATION 1 OPTPHI20. OPTWACH1

INPUT PARAMETERS

MACH = 1.10
 TAIL ASPECT RATIO = 1.00
 TAIL TAPER RATIO = 0.00
 TAIL L.O. SKEW ANGLE = 75.96 DEGREES
 TAIL ROOT CHORD = 7.500
 NOSE LENGTH = 3.000 CAL.
 AFTER BODY LENGTH = 7.000 CAL.
 BODY DIAMETER = 3.75
 TAIL SEMI-SPAN (INCLUDING BODY) = 3.75
 REYNOLDS NUMBER = 700000.00

OUTPUT DEFINITIONS

CNB = BODY ALONE NORMAL FORCE COEFFICIENT
 XCPB = BODY ALONE CENTER OF PRESSURE
 CNTE = TAIL ALONE NORMAL FORCE COEFFICIENT
 XCPTE = TAIL ALONE CENTER OF PRESSURE
 CNBTE = TAIL (IN PRESENCE OF BODY) NORMAL FORCE COEFFICIENT
 XCPBTE = TAIL (IN PRESENCE OF BODY) CHORDWISE CENTER OF PRESSURE/TAIL ROOT CHORD (MEASURED AFT FROM ROOT CHORD LEADING EDGE)
 YCPBTE = TAIL (IN PRESENCE OF BODY) SPANWISE CENTER OF PRESSURE/TAIL SEMI-SPAN (EXCLUDING BODY)
 XCP(B+T) = CENTER OF PRESSURE OF BODY PLUS TAIL (BODY) MEASURED OUTWARD FROM BODY CONFIGURATION (CAL. FROM NOSE)
 YCP(B+T) = NORMAL FORCE COEFFICIENT OF BODY PLUS TAIL CONFIGURATION
 CA = AXIAL FORCE COEFFICIENT

ALPHA I	ISOLATED COMPONENTS				BODY TAIL CONFIGURATION			
	CNB	XCPB	CNT	XCPTE	CNBTE	YCPBTE	XCP(B+T)	CA
0.00	6.000	2.626	7.000	.624	0.000	.335	0.000	.510
5.00	.246	2.788	.146	.634	.431	.335	.722	.583
10.00	.569	3.157	.713	.647	.438	.335	1.517	.480
15.00	.643	3.558	.404	.610	.460	.335	2.027	.443
20.00	.520	3.808	.487	.618	.452	.315	2.679	.393
25.00	2.351	3.529	.485	.624	.457	.301	4.399	.380
30.00	3.746	4.043	1.118	.621	.430	.282	6.121	.358
35.00	5.427	4.182	1.267	.625	.434	.282	7.968	.323
40.00	7.783	4.281	1.322	.610	.442	.282	10.408	.273
45.00	9.362	4.356	1.356	.610	.448	.282	12.124	.211

AMPLE CONFIGURATION 1 OPTPHI=0. OPTMAC=1

INPUT PARAMETERS

MACH = 1.20
 TAIL ASPECT RATIO = 1.00
 TAIL TAPER RATIO = 0.00
 TAIL L.E. SWEEP ANGLE = 75.96 DEGREES
 TAIL ROOT CHORD = 7.500
 NOSE LENGTH = 3.000 CAL.
 AFTER BODY LENGTH = 7.000 CAL.
 BODY DIAMETER = 3.75
 TAIL SEMI-SPAN (INCLUDING BODY) = 3.75
 REYNOLDS NUMBER = 700000.00

OUTPUT DEFINITIONS

CNB = BODY ALONE NORMAL FORCE COEFFICIENT
 XCPB= BODY ALONE CENTER OF PRESSURE
 CNT = TAIL ALONE NORMAL FORCE COEFFICIENT
 XCPT= TAIL ALONE CENTER OF PRESSURE
 CNT(B)= TAIL IN PRESENCE OF BODY NORMAL FORCE COEFFICIENT
 XCPT(B) = TAIL (IN PRESENCE OF BODY) CHORDWISE CENTER OF PRESSURE/TAIL ROOT CHORD (MEASURED AFT FROM ROOT CHORD LEADING EDGE)
 YCPT(B) = TAIL (IN PRESENCE OF BODY) SPANWISE CENTER OF PRESSURE/TAIL SEMI-SPAN (EXCLUDING BODY)
 XCP(B+T)= CENTER OF PRESSURE OF BODY PLUS TAIL BODY MEASURED OUTWARD FROM BODY CONFIGURATION (CAL. FROM NOSE)
 CNT(B+T)= NORMAL FORCE COEFFICIENT OF BODY PLUS TAIL CONFIGURATION
 CA = AXIAL FORCE COEFFICIENT

BODY TAIL CONFIGURATION

ALPHA	CNB	I	XCPB	I	CNT	I	XCPT	I	CNT(B)	I	YCPT(B)	I	CNT(B+T)	I	XCP(B+T)	I	CA	I
0.00	0.000		2.431		0.000		.655		0.000		.335		0.000		.335		.526	
5.00	.245		2.665		.144		.655		.207		.652		.721		.335		7.008	
10.00	.549		3.191		.307		.649		.431		.641		.335		.335		7.013	
15.00	.645		3.741		.486		.640		.649		.650		.335		.335		7.474	
20.00	1.159		4.051		.674		.632		.837		.626		.316		.316		7.155	
25.00	2.751		4.152		.869		.628		.978		.629		.301		.301		6.302	
30.00	4.082		4.253		1.145		.625		1.147		.634		.282		.282		6.056	
35.00	5.911		4.355		1.255		.629		1.252		.639		.282		.282		5.810	
40.00	8.002		4.456		1.340		.633		1.345		.644		.282		.282		5.652	
45.00	9.299		4.557		1.404		.638		1.420		.649		.282		.282		5.638	

SAMPLE CONFIGURATION 1 OPTPMI=0.0 OPTMAC=1

INPUT PARAMETERS

MACH = 1.30
 TAIL ASPECT RATIO = 1.00
 TAIL TAPER RATIO = 0.00
 TAIL L.E. SWEEP ANGLE = 75.96 DEGREES
 TAIL ROOT CHORD = 7.500
 NOSE LENGTH = 3.000 CAL.
 AFTER BODY LENGTH = 7.000 CAL.
 BODY DIAMETER = 3.75
 TAIL SEMI-SPAN (INCLUDING BODY) = 3.75
 REYNOLDS NUMBER = 700000.00

OUTPUT DEFINITIONS

CNB = BODY ALONE NORMAL FORCE COEFFICIENT
 XCPB = BODY ALONE CENTER OF PRESSURE
 CNT = TAIL ALONE NORMAL FORCE COEFFICIENT
 XCPT = TAIL ALONE CENTER OF PRESSURE
 CNTB = TAIL (IN PRESENCE OF BODY) NORMAL FORCE COEFFICIENT
 XCPTB = TAIL (IN PRESENCE OF BODY) CHORDWISE CENTER OF PRESSURE/TAIL ROOT CHORD (MEASURED AFT FROM ROOT CHORD LEADING EDGE)
 YCPTB = TAIL (IN PRESENCE OF BODY) SPANWISE CENTER OF PRESSURE/TAIL SEMI-SPAN (EXCLUDING BODY)
 XCPB+Y = CENTER OF PRESSURE OF BODY PLUS TAIL BODY MEASURED OUTWARD FROM BODY
 CONFIGURATION 1 CAL. FROM NOSE
 CNTB+Y = NORMAL FORCE COEFFICIENT OF BODY PLUS TAIL CONFIGURATION
 CA = AXIAL FORCE COEFFICIENT

ALPHA	ISOLATED COMPONENTS				BODY TAIL CONFIGURATION							
	CNB	XCPB	CNT	Y	XCPB	YCPTB	CNTB	YCPTB	XCPB+Y	CNTB+Y	CA	Y
0.00	0.000	2.242	0.000	.656	0.000	.656	.328	0.000	.328	0.000	.530	.530
5.00	.245	2.540	.142	.656	.200	.653	.328	.713	5.963	.713	.522	.522
10.00	.529	3.204	.304	.650	.411	.642	.328	1.450	7.052	1.450	.499	.499
15.00	.647	3.889	.422	.642	.619	.632	.328	1.989	7.503	1.989	.463	.463
20.00	1.491	4.252	.670	.633	.805	.628	.315	3.199	6.913	3.199	.413	.413
25.00	2.825	4.339	.865	.630	.954	.631	.302	4.828	6.369	4.828	.409	.409
30.00	4.417	4.426	1.115	.627	1.115	.636	.287	6.707	6.067	6.707	.405	.405
35.00	6.106	4.512	1.241	.631	1.237	.641	.287	8.613	5.895	8.613	.395	.395
40.00	7.536	4.599	1.339	.635	1.341	.646	.287	10.213	5.814	10.213	.379	.379
45.00	10.261	4.666	1.414	.639	1.424	.650	.287	13.067	5.661	13.067	.356	.356

SAMPLE CONFIGURATION 2: OPTPHI=1, OPTMAC=0

INPUT PARAMETERS

MACH = 2.00
 TAIL ASPECT RATIO = 1.00
 TAIL TAPER RATIO = .50
 TAIL L-C SWEEP ANGLE = 3.17 DEGREES
 TAIL ROOT CHORD = 5.000
 NOSE LENGTH = 3.000 CAL.
 AFTER BODY LENGTH = 8.250 CAL.
 BODY DIAMETER = 3.75
 TAIL SEMI-SPAN (INCLUDING BODY) = 3.75
 REYNOLDS NUMBER = 6500000.00

OUTPUT DEFINITIONS

CNS = BODY ALONG NORMAL FORCE COEFFICIENT
 XCPB = BODY ALONG CENTER OF PRESSURE
 CNT = TAIL ALONG NORMAL FORCE COEFFICIENT
 XCPT = TAIL ALONG CENTER OF PRESSURE
 CNTB = TAIL IN PRESENCE OF BODY NORMAL FORCE COEFFICIENT
 XCPTR = TAIL (IN PRESENCE OF BODY) CHORDWISE CENTER OF PRESSURE/TAIL ROOT CHORD (MEASURED AFT FROM ROOT CHORD LEADING EDGE)
 YCPTB = TAIL (IN PRESENCE OF BODY) SPANWISE CENTER OF PRESSURE/TAIL SEMI-SPAN (INCLUDING BODY)
 XCPB(4) = CENTER OF PRESSURE OF BODY PLUS TAIL BODY MEASURED OUTWARD FROM BODY CONFIGURATION (CAL. FROM NOSE)
 CNTB(4) = NORMAL FORCE COEFFICIENT OF BODY PLUS TAIL CONFIGURATION
 CA = AXIAL FORCE COEFFICIENT

ALPHA= 0.00

PHI	CNTB(1)	I	FIN 2	XCPT(2)	I	FIN 4	I	FIN 4	I	XCPT(4)	I	XCPT(4)	I	CNS(4)	I	CA	I
I	I	I	I	I	I	I	I	I	I	I	I	I	I	I	I	I	I
0.	0.000	0.000	.536	.536	.536	.536	.536	.536	.536	.407	.407	.407	.407	0.000	0.000	.343	.343
10.	0.000	0.000	.536	.536	.536	.536	.536	.536	.536	.407	.407	.407	.407	0.000	0.000	.343	.343
20.	0.000	0.000	.536	.536	.536	.536	.536	.536	.536	.407	.407	.407	.407	0.000	0.000	.343	.343
30.	0.000	0.000	.536	.536	.536	.536	.536	.536	.536	.407	.407	.407	.407	0.000	0.000	.343	.343
40.	0.000	0.000	.536	.536	.536	.536	.536	.536	.536	.407	.407	.407	.407	0.000	0.000	.343	.343
50.	0.000	0.000	.536	.536	.536	.536	.536	.536	.536	.407	.407	.407	.407	0.000	0.000	.343	.343
60.	0.000	0.000	.536	.536	.536	.536	.536	.536	.536	.407	.407	.407	.407	0.000	0.000	.343	.343
70.	0.000	0.000	.536	.536	.536	.536	.536	.536	.536	.407	.407	.407	.407	0.000	0.000	.343	.343
80.	0.000	0.000	.536	.536	.536	.536	.536	.536	.536	.407	.407	.407	.407	0.000	0.000	.343	.343
90.	0.000	0.000	.536	.536	.536	.536	.536	.536	.536	.407	.407	.407	.407	0.000	0.000	.343	.343

LARGE 43.00																
PMI	I	FIN 2	I	FIN 4	I	FIN 2	I	FIN 4	I	VCPI(B)	I	XCPI(B+T)	I	CN(B+T)	I	CA
I	I	I	I	I	I	I	I	I	I	I	I	I	I	I	I	I
0	1.245	1.245	.592	.592	.592	.592	.592	.592	.592	.407	.407	6.074	6.074	12.217	12.217	.343
10	1.052	1.427	.587	.587	.592	.587	.587	.592	.587	.400	.407	6.074	6.074	12.218	12.218	.343
20	.837	1.474	.587	.587	.591	.587	.587	.591	.587	.424	.407	6.050	6.050	12.156	12.156	.343
30	.614	1.448	.587	.587	.590	.587	.587	.590	.587	.463	.407	6.032	6.032	12.188	12.188	.343
40	.404	1.431	.587	.587	.588	.587	.587	.588	.587	.535	.407	6.040	6.039	12.129	12.129	.343
50	.218	1.291	.614	.587	.587	.587	.587	.585	.585	.407	.407	6.040	6.039	12.129	12.129	.343
60	.065	.606	.797	.607	.585	.585	.585	.585	.584	.407	.407	6.032	6.032	12.100	12.100	.343
70	-.051	.681	.831	.197	.576	.576	.576	.576	.576	1.000	.407	6.050	6.050	12.156	12.156	.343
80	-.058	.564	.577	.486	.557	.557	.557	.557	.557	1.000	.407	6.074	6.074	12.218	12.218	.343
90	-.000	0.000	.560	.560	.558	.558	.558	.558	.558	1.000	.407	6.074	6.074	12.217	12.217	.343

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1      PROGRAM MAIN(TAPE5,TAPE6)
2
3      THIS PROGRAM USES AN AERODYNAMIC METHODOLOGY DEVELOPED BY THE
4      MARTIN MARIETTA CORP. TO PREDICT AERODYNAMIC COEFFICIENTS OF
5      MISSILES WITH LOW ASPECT RATIO TAILS AT LOW AND HIGH ANGLES OF
6      ATTACK AND ARBITRARY ROLL ANGLES.
7
8      THE INPUT PARAMETERS AND THEIR LIMITS FOR THIS METHOD ARE:
9
10     MACH = MACH NUMBER .8 TO 3.0
11     ALPHA = ANGLE OF ATTACK (DEG) 0. TO 180 (0 TO 45 FOR ROLL)
12     ALE = TAIL LEADING EDGE SWEEP ANGLE (DEG) 0 TO 70 DEG
13     LAD = AFTER BODY LENGTH IN CAL. 6 TO 18
14     LND = NOSE LENGTH IN CAL. 1.5 TO 3.5
15     LMD = TAIL TAPER RATIO 0 TO 1
16     LAMDA = TAIL ASPECT RATIO (TWO PANELS) .5 TO 3.5
17     AP = BEGINNING ALPHA FOR DESIRED ALPHA SWEEP (DEG)
18     ALF1 = END POINT FOR ALPHA SWEEP (DEG)
19     ALF2 = ALPHA INCREMENT FOR ALPHA SWEEP (DEG)
20     DELAF = REYNOLDS NUMBER/FT.
21     RN = TAIL SEMI SPAN INCLUDING BODY, (B*D)/2, INCHES
22     S = TAIL ROOT CHORD INCHES
23     CR = BODY DIAMETER INCHES
24     OPTPHI = 0 GIVES NO PREDICTIONS VS. ROLL ANGLE
25
26     = 1 GIVES AERODYNAMIC COEFFICIENTS AND CENTER OF
27     PRESSURE AS A FUNCTION OF ROLL ANGLE
28     OPTMAC = 1 ALLOWS FOR MULTIPLE MACH NO. CALCULATIONS FOR
29     A GIVEN CONFIGURATION
30
31     = 0 CALCULATIONS FOR SINGLE MACH NO. ONLY
32
33     INTEGER OPTPHI,OPTMAC
34     DIMENSION ANAME(12)
35     REAL MACH,LAMDA,LND,LAD,18T
36     GO TO 11
37
38     1 IF(OPTMAC.EQ. 1) GO TO 2
39     11 READ(5,208) (ANAME(I),I=1,12)
40     IF(OPT5) 400,25
41     25 READ(5,200) AR,S,CR,LAMDA,ALE
42     READ(5,201) LND,LAD,0
43     15 READ(5,202) ALF1,ALF2,DELAF,MACH,RN,OPTPHI,OPTMAC
44     GO TO 3
45
46     2 READ(5,203) MACH
47     IF(OPT5) 400,26
48     26 IF(MACH.EQ. 0.) GO TO 11
49     3 WRITE(6,140) (ANAME(I),I=1,12)
50     WRITE(6,117)
51     WRITE(6,109)
52     WRITE(6,110)
53     WRITE(6,111) MACH
54     WRITE(6,112) AR
55     WRITE(6,113) LAMDA
56     WRITE(6,114) ALE
57     WRITE(6,115) CR
58     WRITE(6,116) LND

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115 CALL CNTPMI(WACH,AR,LAMDA,D,S,ALPHA,PHI,CR,ALE,CNTB,
    CALL I8TTC(LAMDA,WACH,AR,LAMDA,D,S,ALPHA,PHI,S,D,IBT)
    CALL XCP1B(WACH,AR,LAMDA,D,S,CR,ALPHA,PHI,XCPTB1,XCPTB2)
    CALL YCPT3(LAMDA,PHI,ALPHA,WACH,S,D,CR,YCPT3)
    CMPT = CNB + 2 * CNTB-ARATIO + IBT
    XCPT1 = LAD-LND-CR/D + XCPTB1-CR/D
    GO TO 16
120 300 WRITE(6,204) ALPHA,CNB,XCPB,CNT,XCPT,CA
    GO TO 36
125 16 XCPBT = (CNB-XCPB + 2 * CNTB-ARATIO-XCPT1
    WRITE(6,108) ALPHA,CNB,XCPB,CNT,XCPT1,XCPTB1,XCPTB2,XCPBT,
    1CA
    30 ALPHA = ALPHA + DELAF
    IF(ALPHA .GT. ALF2) GO TO 1
    KOUNT = KOUNT + 1
    IF(KOUNT .EQ. 50 .AND. OPTPMI .EQ. 0) GO TO 4
    GO TO 5
130 10 IF(KIT .EQ. 0) WRITE(6,140)
    WRITE(6,141)
    WRITE(6,101) ALPHA
    WRITE(6,105)
    WRITE(6,102)
    WRITE(6,102)
    WRITE(6,104)
    WRITE(6,105)
    KIT = KIT + 1
    IF(KIT .EQ. 3) KIT = 0
    PHI = 0.
    DO 20 I=1,10
    PHI1 = 180. - PHI
    PHI2 = PHI + 90.
    PHI3 = PHI
    PHI4 = 90. - PHI
    CALL CNTPMI(WACH,AR,LAMDA,D,S,ALPHA,PHI1,CR,ALE,CNTB1)
    CALL CNTPMI(WACH,AR,LAMDA,D,S,ALPHA,PHI2,CR,ALE,CNTB2)
    CALL CNTPMI(WACH,AR,LAMDA,D,S,ALPHA,PHI3,CR,ALE,CNTB3)
    CALL CNTPMI(WACH,AR,LAMDA,D,S,ALPHA,PHI4,CR,ALE,CNTB4)
    CALL XCP1B(WACH,AR,LAMDA,D,S,CR,ALPHA,PHI1,XCPT11,XCPT12)
    CALL XCP1B(WACH,AR,LAMDA,D,S,CR,ALPHA,PHI2,XCPT12,XCPT13)
    CALL XCP1B(WACH,AR,LAMDA,D,S,CR,ALPHA,PHI3,XCPT13,XCPT14)
    CALL XCP1B(WACH,AR,LAMDA,D,S,CR,ALPHA,PHI4,XCPT14,XCPT15)
    CALL YCPT3(LAMDA,PHI1,ALPHA,WACH,S,D,CR,YCPT11)
    CALL YCPT3(LAMDA,PHI2,ALPHA,WACH,S,D,CR,YCPT12)
    CALL YCPT3(LAMDA,PHI3,ALPHA,WACH,S,D,CR,YCPT13)
    CALL YCPT3(LAMDA,PHI4,ALPHA,WACH,S,D,CR,YCPT14)
    IF(ALPHA .GT. 90.) GO TO 35
    XCT1=LAD-LND-CR/D + XCPT11-CR/D
    XCT2=LAD-LND-CR/D + XCPT12-CR/D
    XCT3=LAD-LND-CR/D + XCPT13-CR/D
    XCT4=LAD-LND-CR/D + XCPT14-CR/D
    XCT5=LAD-LND-CR/D + XCPT15-CR/D
    GO TO 36
135 35 XCT1=LAD-LND-XCPT11-CR/D
    GO TO 36
140
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150 FORMAT(1H **I BODY DIAMETER = *F5.2**
11*)
151 FORMAT(1H **I TAIL SEMI-SPAN(INCLUDING BODY) =*F5.2**
11*)
118 FORMAT(1H **I REYNOLDS NUMBER =*F13.2** 1*)
119 FORMAT(1H **I OUTPUT DEFINITIONS
120 FORMAT(1H **I CNB = BODY ALONE NORMAL FORCE COEFFICIENT
121 FORMAT(1H **I XCPB = BODY ALONE CENTER OF PRESSURE
122 FORMAT(1H **I CNT = TAIL ALONE NORMAL FORCE COEFFICIENT
123 FORMAT(1H **I XCPT = TAIL ALONE CENTER OF PRESSURE
124 FORMAT(1H **I CNTB = TAIL(IN PRESENCE OF BODY) NORMAL FORCE
125 FORMAT(1H **I COEFFICIENT
126 FORMAT(1H **I XCPTB = TAIL (IN PRESENCE OF BODY) CHORDWISE
127 FORMAT(1H **I CENTER OF PRESSURE/TAIL ROOT CHORD (MEASURED
128 FORMAT(1H **I AFT FROM ROOT CHORD LEADING EDGE)
129 FORMAT(1H **I YCPTB) = TAIL (IN PRESENCE OF BODY) SPANWISE
130 FORMAT(1H **I CENTER OF PRESSURE/TAIL SEMI-SPAN (EXCLUDING
131 FORMAT(1H **I BODY) MEASURED OUTWARD FROM BODY
132 FORMAT(1H **I XCPB+T) = CENTER OF PRESSURE OF BODY PLUS TAIL
133 FORMAT(1H **I CONFIGURATION (CAL. FROM NOSE)
134 FORMAT(1H **I CNTB+T) = NORMAL FORCE COEFFICIENT OF BODY
135 FORMAT(1H **I PLUS TAIL CONFIGURATION
136 FORMAT(1H **I CA = AXIAL FORCE COEFFICIENT
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400 STOP
END

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230 PHIPRM = 90.-PHI
   PPRIM = 50.-PHIP
   A3=(16000.-PHIPRM-16000.-PHIPRM**2+400.-PHIPRM**3)/(400.-PHIPRM**3)
   PPRIM=40.-PPRIM**2+PPRIM**3)
   A4=(40.-PPRIM**3)/PHIPRM-1200.-PHIPRM*(PPRIM**2)-(PPRIM**3)/
   PHIPRM**2+1200.-PPRIM*(PHIPRM**2)+(PPRIM**2)*(PHIPRM**3)-40.-
   PPRIM*(PHIPRM**3)/(400.-PHIPRM-40.-PPRIM**2+PPRIM**3)
   RTBPM = RTEP*SIN(PHIP-.0174532)
   A = RTEPMP-RTBO
   CALL LOOK3(P,RT,9.,ALPHA,BEALFT,9.,ALE,BEALFT,9.,MACH,BEMACT,3,
   .IX,IY,I2,I1)
   RTE = RTBO + A*A3 + B *A4
   GO TO 80
140 RTE = RTEP*SIN(PHIP-.0174532)
   GO TO 80
90 JFLAG = 0
   RTB1 = RTB
   MACH = 1.75
   MFLAG = 1
   GO TO 40
50 JFLAG = 1
   MACTP = MACH
   MACH = 1.2
   GO TO 30
100 KFLAG = 0
   MACH = MACTP
   RTB2 = RTB
   GO TO 110
40 CALL LOOK2(RTEP,RTB2,3,AR,RTEPAR,3,LAMDA,RTBPLD,3,IX,IY,I1)
   IF(PHI .LT. 4.) GO TO 120
   RTB45 = RTEP*SIN(45.-.0174532)
   A = RTB45-RTBO
   CALL LOOK3(B,RT,5.6,ALPHA,BEALFT,5.,ALE,BEALFT,6.,MACH,BEMACT,4,I
   .IX,IY,I2,I1)
   PHIP = 45.
   PHIPRM = 50.-PHI
   PPRIM = 90.-PHIP
   A3=(16000.-PHIPRM-16000.-PHIPRM**2+400.-PHIPRM**3)/(400.-PHIPRM**3)
   PPRIM=40.-PPRIM**2+PPRIM**3)
   A4=(40.-PPRIM**3)/PHIPRM-1200.-PHIPRM*(PPRIM**2)-(PPRIM**3)/
   PHIPRM**2+1200.-PPRIM*(PHIPRM**2)+(PPRIM**2)*(PHIPRM**3)-40.-
   PPRIM*(PHIPRM**3)/(400.-PHIPRM-40.-PPRIM**2+PPRIM**3)
   RTE = RTBO + A*A3 + B *A4
   GO TO 80
120 RTE = RTEP*SIN(PHIP-.0174532)
   GO TO 80
200 IF(ALPHA .GT. 30.) GO TO 210
   ALF = ALPHA + 10.
   A2=2.07752E-07*ALF**4 + 1.72193E-05*ALF**3 + 6.24467E-04*ALF**2
   + .016458069*ALF + .087604485
   A1 = 4.66769E-07*ALF**4 - 4.22299E-05*ALF**3 + 2.32986E-04*ALF**2
   + .6936E-03*ALF + .98159845
   CALL LOOK1(KTY,KTF,US,KTBD,11,IX,I1)
   RTBO = AC + A1*KTE
   IF(IFLAG .EQ. 1) GO TO 290
   IF(IFLAG .EQ. 1) GO TO 300

```

04/27/78 09:19:41.

FTN 4.2-74355

SUBROUTINE CNTPH1 74/74 OPT=1

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280 GO TO 25
290 ALF = ALPHA + 10.
    A0 = 4.5799E-12*ALF**6 - 2.30809E-09*ALF**5 + 3.96812E-07*ALF**4
    A1 = 2.15272E-05*ALF**3 - 8.10606E-04*ALF**2 + .092902183*ALF
    A2 = -.85855362
    A3 = 1.67133E-11*ALF**6 - 9.5912E-09*ALF**5 + 2.09288E-06*ALF**4
    A4 = 2.19478E-04*ALF**3 + .011664495*ALF**2 - .303221946*ALF
    A5 = 3.0674E-04
295 CALL LOOK1(K15,RTPT,DS,K1PDS,11,1X,1)
    A2 = -2.16611E-11*ALF**6 + 1.21153E-08*ALF**5 - 2.53877E-06*ALF**4
    A3 = -2.4641E-04*ALF**3 + .01114855*ALF**2 + .217380211*ALF
    A4 = -1.28277255
    CALL LOOK2(RTPT2,RTPT2,12,MACH,RTPT2*12,LAMDA,RTPT2*3,1X,1Y,1)
    RTPT2 = RTPT2-LAMDA
    RTPT = A0 + A1*RT + A2*RTPT2
    IF(LFLAG.EQ.1) GO TO 300
    IF(LFLAG.EQ.1) GO TO 290
    GO TO 280
300 ALF = ALPHA + 10.
    A0 = 4.5799E-12*ALF**6 - 2.30809E-09*ALF**5 + 3.96812E-07*ALF**4
    A1 = 2.15272E-05*ALF**3 - 8.10606E-04*ALF**2 + .092902183*ALF
    A2 = -.85855362
    A3 = 1.67133E-11*ALF**6 - 9.5912E-09*ALF**5 + 2.09288E-06*ALF**4
    A4 = 2.19478E-04*ALF**3 + .011664495*ALF**2 - .303221946*ALF
    A5 = 3.0674E-04
310 GO TO 295
320 IF(LFLAG = 1)
    MACH2 = MACH
    MACH = 1.2
    GO TO 290
330 IF(LFLAG = 0)
    RTPT = RTPT
    MACH = 1.75
    LFLAG = 1
    GO TO 290
340 IF(LFLAG = 0)
    MACH = MACH2
    RTPT2 = RTPT
    RTPT = RTPT*((MACH-1.2)/.55)*(RTPT2-RTPT)
    GO TO 25
350 DCP = D/CR
    CALL PHCC(ALPHA,MACH,DCR,PHC1)
    PHC = PHC1*240
    PHI = (PHI-90.)*360
    A = (1.-(1.-(PHC**2))**2)/(PHC**2)/(PI/2.)*2/(PI/2.)*PHI**2
    B = (PHI*(1.-(PHC**2))-PHC*(PI/2.))/(PI/2.)*PHI**2+2*(1.-(PHC
    C = -1.-(PI/2.)/(PI/2.)*PHI**3
    PHI = PHI/360.
    IF(MACH.LT.1.2) GO TO 410
    CALL LOOK3(RPM,APPM,RT,19,10,MACH,RPM,19,ALPHA,APPM,10,LAMDA,
    APPM,19,1X,1Y,1Z,1)
    IF(APPM.LT.1) GO TO 420
    CALL LOOK4(RT,RTPT,19,10,MACH,RTPT,19,ALPHA,RTPT,10,AR,
    RTPT,19,1X,1Y,1Z,1)
    APPM = APPM*RTPT
    GO TO 420

```


PAGE 7

04/27/78 09.19.41.

FIN 4.2*74355

SUBROUTINE CATP=1 74/74 OPT=1

006180
006190
006200
006210

610 RPR = 0.
620 RTR = RYTCOA + RPR**B
GO TO 110
END

345

[illegible]

PAGE 4

04/27/78 09.23.25.

FTN 4.2-7A355

007930
007940

OPT=1

74/74

SUBROUTINE CNTY

GO TO 98
END

49


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115      2.510..505..517..323..326..460..467..501..593..537..330..320..310. 009090
      3.422..406..509..550..485..337..315..360..423..500..560..580..605. 009100
      4000..330..445..475..485..485..485..485..485..485..485..485..485. 009110
      5.465..470..470..165..290..380..475..448..458..467..475..193..300. 009120
      6.390..433..457..470..477..477..200..330..423..465..485..493..496. 009130
      7.495..200..130..423..445..485..493..496..495..200..330..423..465. 009140
      8.485..493..467..465/ 009150
      X=PI*SQRT(45*(1.-Y**2))
      Y=PI*ATAN(SQRT(1.-Y**2))
      Z=PI
      IF(X.GT.7.) WRITE (6,900) X
      IF(Z.GT.1.) WRITE (6,902) Z
      IF(X.GT.1.0) GO TO 1
      CALL LOOK3(CLEAR,PAR1,15,7,X,YT1,15,Y,YT1,7,Z,YT1,4,IX,IV,IZ,1)
      IF(Y.GT.4.) WRITE (6,901) Y
      CALL LOOK3(X(CFCB,PAR2,5,X,YT2,5,Z,YT2,4,IX,IV,IZ,1)
      CLA=CLAR*AP
      RETURN
      1 CALL LOOK3(CLEAR,PAR3,15,7,X,AT1,15,Y,YT1,7,Z,YT1,4,IX,IV,IZ,1)
      IF(Y.GT.4.) WRITE (6,901) Y
      CALL LOOK3(X(CFCB,PAR4,5,X,YT2,5,Z,YT2,4,IX,IV,IZ,1)
      CLA=CLAR*AP
      RETURN
900  FORMAT (IX,*,EXTRAPOLATION REQUIRED, *10HAP*ETA = F10.4)
901  FORMAT (IX,*,EXTRAPOLATION REQUIRED, *11HAP*TANSM = F10.4)
902  FORMAT (IX,*,EXTRAPOLATION REQUIRED, *APER RATIO = *F10.4)
      END

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[illegible]

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115      * (16.0000)/PI.000)*CNP12
      RETURN
120  20 IF(MACH-UT.1.5) GO TO 90
      110 CALL LOG2(CNA*CNAT.13.0,MACH*CNAM.13.0,CNAL.4.0,CNALD.4.0,
      *TIMY.12.1)
      GO TO 100
      30 CNA1=CNA
      IFLAG=0
      MACH=1.5
      JFLAG=1
      GO TO 110
      40 CNA2=CNA
      MACH = MACHT
      JFLAG=0
      CNA=CNA2-(CNA2-CNA1)*(1.5-MACH)/.3
      GO TO 50
      90 IFLAG = 1
      MACHT=MACH
      MACH = 1.2
      GO TO 10
      75 CNA=ALPHA*E2
      CNA=SIGN(.001)*COS(A/2.)*COS(W.0)*COS(SPIFF)*SIN(A)***2
      RETURN
      END
135

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140 CALL LOG10(CELX,CFLXT,WACHCDELX**23,X**3)
      DELX = CELX*LDL
      X20 = XC*DELX
      A = ALPHA
      A0 = 1+((A**2)/26000)-((1+A**2)/24000.)
      A1 = ((A**2)/26000)-(A**2)/(240000.)
      A2 = ((A**2)/26000.-2*A**2)/26000.
      LN = LND*O
      LA = LAD*O
      LB = LBD*LN*O*F
      SCN = LN*(SGRT(-(LA**2)+24000))-((A**2)*ASIN(LN/(A**2-((R-D/2)))*LN
      *SCN*SGRT(-(LN**2)+(LB**2)))-(LB**2)/2)*ASIN(LN/A))-((R-D/2)*LN**2
      CSA = LAC*O
      XPAR = (LN**2/LZ/2)*LN*O
      XPAR = ((XPAR*XPAR)/(LSPN*CP2)
      XP12 = XPAR*F
      IF(ALPHA*.GT..20.) GO TO 20
      XPE = A0*X0 + A1*X20+A2*XP12
      70 CONTINUE
      RETURN
10 IF(WACH*.LT..1E-3) GO TO 50
120 CALL LOG10(X0*XC*Y2*7+A*WACH*XC*Y2*7*LAC*XC*Y2*L*4*LWD*XC*Y2*L*3*
      *Y1*Y12*1)
      GO TO 30
20 IF(WACH*.GE..1.) GO TO 40
      APRIM = 50.
      GO TO 50
40 APRIM = 20.
50 AM = (X2-U*XP12)/(APRIM-90.)
      IF(ALPHA*.LT..APRIM) GO TO 60
      IF(ALPHA*.LE..160.) GO TO 60
      X10 = 70+AM*XP12
      R0 = (-51640000.+900000.*ALPHA-5200.*ALPHA**2+10.*ALPHA**3)/
      *4000.
      R1 = (4854000.-86400.*ALPHA+310.*ALPHA**2-ALPHA**3)/4000.
      R2 = (-48560000+86400.*ALPHA-510.*ALPHA**2+ALPHA**3)/4000.
      XCR = R0*AN + F1*(L4D*LND) + 52*X10
      GO TO 70
60 XCP6 = X20
      GO TO 70
80 XCP6 = F1*(ALPHA-APRIM)*X20
      GO TO 70
90 IF(LAG = 1
      WACHT = WACH
      WACH = 1+2
      GO TO 120
100 X01 = X0
      IF(LAG = 0
      JFLAG = 1
      WACH = 1+A
      GO TO 120
110 X02 = X0
      JFLAG = 0
      WACHT = WACH
      X0 = X02+(X02-X01)*(1-A-WACHT)/A3
      GO TO 140

```

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CPT-1

74/74

SUBROUTINE XCPEDC

011000

FAC

115

```

C.....
C SUBROUTINE IRTT(LAMDA,MACH,AR,ALPHA,PHI,S,O,IBT) 011890
C..... 011900
C THIS SUBROUTINE CALCULATES BODY NORMAL CARRYOVER FORCE COEFF. 011910
C..... 011920
C..... 011930
C LAMDA = TAIL TAPER RATIO 011940
C MACH = MACH NUMBER 011950
C AR = TAIL ASPECT RATIO 011960
C ALPHA = ANGLE OF ATTACK 011970
C PHI = BODY ROLL ANGLE 011980
C S = BODY SEMI SPAN(INCLUDING BODY 011990
C O = BODY DIAMETER 012000
C IBT = BODY CARRY OVER FORCE COEFF. (RETURNED VALUE) 012010
C..... 012020
C..... 012030
C REAL LAMDA,MACH,IABAS,IABST,IABT,ICBAS,ICBAS,I13AS,I2BAS, 012040
C I13AS,MACHT,I1,I2,I3,I5,I1,I2,I4FOR,IPTAR,ICBAS,I13O,I8ST,IA,IC 012050
C I13TM 012060
C DIMENSION YDIBT(6,3,3),DIBTAF(6),DIBTLM(3),DIBSTAR(3), 012070
C I8ST(5,3),I8TM(5),I8TAR(3), 012080
C FCART(6),FCATT(6), 012090
C ICPAST(2),ICBAS(2), 012100
C FAMT(5,3),FAMAC(5),FAMAR(3), 012110
C FAAPT(11),FAAPT(11), 012120
C IABST(2),IABST(2), 012130
C IFAR(10),IFAR(10), 012140
C IF2OR(13),IF2OR(13), 012150
C IF2M(2),IF2MACH(2), 012160
C IF2P(5,11),IF2P(5,11), 012170
C IFIDR(13),IFIDR(13), 012180
C IFIEAS(2),IFIEAS(2), 012190
C DATA ((TOIBT(I,J,K)=1.5),J=1,6),J=1,3,K=1,3)/0.0,0.18,0.106,0.05,0.04, 012200
C 11.53,0.02,0.119,0.332,0.649,1.117,0.0,0.023,0.109,0.299,0.557,0.768,0. 012210
C 2.015,0.066,0.219,0.408,0.646,0.0,0.018,0.081,0.167,0.296,0.446,0.0,0.071, 012220
C 3.149,0.254,0.304,0.0,0.013,0.043,0.139,0.218,0.271,0.0,0.013,0.051,0.109,0.155, 012230
C 0.205,0.0,0.15,0.043,0.059,0.13,0.122, 012240
C DATA ((IETAR(I)=1.5),I=1,6)/0.0,0.10,0.15,0.20,0.25, 012250
C DATA ((IETLM(I)=1.5),I=1,6)/0.0,0.5,1.0, 012260
C DATA ((IETAR(I)=1.5),I=1,6)/5.1,0.2, 012270
C DATA ((IETLM(I)=1.5),I=1,6)/J=1,3/I=1,6,K=1,3)/1.484,-1.13,-2.339,0.73,1.006,0.252, 012280
C 1-4.91,-0.805,-0.252,0.403,0.491,-2.26,-0.491,-3.9,0.415, 012290
C DATA ((IPTM(I)=1.5),I=1,6)/5.1,0.2, 012300
C DATA ((IETAR(I)=1.5),I=1,6)/5.1,0.2, 012310
C DATA ((FCART(I)=1.5),I=1,6)/2.496,1.941,1.462,1.109,1.0,1.1, 012320
C DATA ((FCATT(I)=1.5),I=1,6)/5.1,0.2, 012330
C DATA ((ICBAS(I)=1.5),I=1,6)/5.1,0.2, 012340
C DATA ((ICBAS(I)=1.5),I=1,6)/J=1,3,I=1,6)/1.76,1.668,1.494,1.332,1.0,2.0, 012350
C 12.0,2.0,3.0,3.0,3.0,3.0, 012360
C DATA ((FAMT(I)=1.5),I=1,6)/5.1,0.2, 012370
C DATA ((FAMAC(I)=1.5),I=1,6)/5.1,0.2, 012380
C DATA ((FAMAR(I)=1.5),I=1,6)/5.1,0.2, 012390
C DATA ((FAAPT(I)=1.5),I=1,6)/2.597,2.118,1.714,1.311,1.134,1.0,1.0,1.0, 012400
C 11.0,1.1, 012410
C DATA ((FAAPT(I)=1.5),I=1,6)/.487,.564,.628,.731,.808,.911,1.03,1.295,0.12420 012420
C 11.5,2.1, 012430
C DATA ((IABST(I)=1.5),I=1,6)/1.5,1.1, 012440
C DATA ((IABST(I)=1.5),I=1,6)/J=1,3,I=1,6)/3.0,5.1, 012450

```


[illegible]

```

115      RETURN
      80 IFLAG = 0
      JFLAG = 1
      IBT1=IBT
      MACH = 2.0
      GO TO 90
120      JFLAG = 0
      IBT2 = IBT
      MACH = MACHT
      IBT = IBT2-(2.0-MACH)*((IBT2-IBT1)/.7
      RETURN
125      IF (MACH .GE. 2.) GO TO 90
      IFLAG = 1
      MACHT = MACH
      MACH = 1.3
      GO TO 30
130      CALL LOOK1(I1BAS,I1BAS,LAMDA,I1BLM,2,IX,1)
      CALL LOOK1(I1BAS,I1BAS,LAMDA,I1BLM,1,IX,1)
      I1 = I1BAS+1
      CALL LOOK1(I2BAS,I2BAS,LAMDA,I2BLM,1,IX,1)
      CALL LOOK1(I2M,I2M,MACH,I2MACH,2,IX,1)
      CALL LOOK1(I2DB,I2DB,IF2DB,2,IX,1)
      I2 = I2BAS+I2M+I2DB
      CALL LOOK1(I3AR,I3AR,IF3AR,10,IX,1)
      I3 = -5*IF3AR
      IF (ALPHA .GT. 90.) GO TO 105
      IBTO = I1-SIN(ALPHA*PI)
      GO TO 110
105      IF (ALPHA .GT. 115.) GO TO 120
      IBTO = I1-(I1-I2)*SIN((ALPHA-90.)/25.)
      GO TO 110
110      IBTO = -19.325*I3+11.926*I2+115.816*I3-8.362*I2*(ALPHA*PI)
      IF (JFLAG .EQ. 1) GO TO 100
      RETURN
150      20 WRITE(6,500)
      500 FORMAT(1X,'MACH NUMBER OUTSIDE ALLOWABLE LIMITS')
      RETURN
      END

```



```

RAD = PI/180.
DP = 0/12.5)
IF(ALPHA.GT.50.) GO TO 10
IF(MACH.GT. 1.) GO TO 20
BETA = SQR(1.-MACH**2)
PAR = BETAPAR
CALL LOOK3(XCPC0,TCP1,P,4,PAR,TEAR,5,DE,TDP,4,LAMDA,TLAM,3,IX,IV,
.12.1)
40 A = ALPHA*RAU
DIF = (2.0**3)/(PI/2.0)**3-(3.0**2)/(PI/2.0)**2
XCPC1 = XCPC0+DIF*(XCPC0-5)
RETURN
70 IF(MACH.GT. 1.) GO TO 30
BETA = SQR(1.-MACH**2)
PAR = BETAPAR
CALL LOOK3(XCPC0,TCP2,P,4,PAR,TEAR,5,DE,TDP,4,LAMDA,TLAM,3,IX,IV,
.12.1)
50 A = (180.-ALPHA)*RAD
DIF = (2.0**3)/(PI/2.0)**3-(3.0**2)/(PI/2.0)**2
XCPC1 = XCPC0 + DIF*(XCPC0-5)
RETURN
80 BETA = SQR(MACH**2-1.)
PAR = BETAPAR
CALL LOOK3(XCPC0,TCP3,P,4,PAR,TEAR,5,DE,TDP,4,LAMDA,TLAM,3,IX,IV,
.12.1)
GO TO 40
30 BETA = SQR(MACH**2-1.)
PAR = BETAPAR
CALL LOOK3(XCPC0,TCP4,P,4,PAR,TEAR,5,DE,TDP,4,LAMDA,TLAM,3,IX,IV,
.12.1)
GO TO 50
END
014000
014010
014020
014030
014040
014050
014060
014070
014080
014090
014100
014110
014120
014130
014140
014150
014160
014170
014180
014190
014200
014210
014220
014230
014240
014250
014260
014270
014280
014290
014300
014310

```


SUBROUTINE XCPTEH 76/76 OPT=1

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60
GO TO 30
40 CONTINUE
XCPTEU = XCPTEA
XCPTEL = XCPTEU
30 CONTINUE
RETURN
END

014890
014900
014910
014920
014930
014940
014950


```
7593.774532.57.4452.36.403.92.367.77.382.54.386.02.389.53.396.66.
8407.4418.83.434.34.446.27.458.59.466.97.479.84.488.62.499.82.
9705.3866.64.5618.49.518.28.468.86.448.3.442.25.444.26.452.38.
469.09493.07.506.97.523.534.99.544.77.552.23.559.79.564.89.
1570.04.815.46.775.82.702.19.610.14.537.42.508.97.495.51.499.82.
2520.633548.74.585.75.610.14.622.81.636.43.644.25.650.11.650.11.
3528.626.46/
DATA (PCIM2(I),I=1,19),I=1,19)/J=1,63)/58.04.57.26456.23.54.47.52.3.
149.06.45.23.42.65.41.541.54.1.88.42.65.43.23.44.02.44.42.44.83.
245.02.45.23.45.65.90.92.90.1.88.08.84.56.60.44.74.46.67.41.63.84.
341.20.59.37.59.1.59.64.59.91.60.46.61.01.61.85.62.69.63.64.13.130017190
4.06.128.69.126.121.51.115.08.102.29.92.58.84.56.79.74.14.70.53.
568.02.66.20.65.1.65.766.570.21.77.23.85.71.177.02.177.02.171.49.
5160.95.147.1331.25.118.25.116.25.116.25.116.25.116.25.116.25.116.25.
780.44.80.74.82.29.66.49.94.27.105.11.831.29.232.34.220.04.196.26.
4177.02.160.95.146.33.135.48.126.119.87.117.19.117.19.118.79.
9122.07.126.57.133.05.139.85.145.01.149.69.294.1.287.51.269.83.
1166.13.174.63.185.23.197.36.203.73.204.65.199.16/
DATA (PCIM2(I),I=1,19),I=1,19)/J=1,121)/363.93.356.97.326.42.287.51.
1253.24.232.34.215.11.207.45.205.58.207.45.211.25.217.07.227.14.
2236.64.247.57.255.55.264.98.260.22.239.84.434.54.18.83.389.53.
3336.94.298.13.274.77.262.59.256.71.257.88.262.59.271.06.279.8.
4291.45.330.56.314.79.324.94.332.39.323.47.296.78.518.26.504.37.
5460.66.399.08.350.97.332.39.323.47.322.01.322.01.326.42.333.9.
5344.66.357.35.372.27.386.02.396.66.403.92.407.66.400.27.612.91.
7596.47.4534.05.458.58.405.75.389.53.384.27.387.77.391.3.398.45.
8405.75.4416.94.432.34.446.27.456.54.466.97.479.84.490.84.499.82.
9715.04.692.71.621.3.625.37.466.97.448.3.442.25.444.26.456.5.469.1.
488.62.504.37.520.63.532.57.544.77.552.23.559.79.564.89.572.83.
1819.19.742.49.708.58.612.91.539.86.506.86.495.51.499.82.520.83.
2549.74.583.1.604.63.624.13.4635.55.4644.25.647.17.647.17.641.33.
3628.96/
DATA (PCIM2(I),I=1,19)/J=1,19)/0.02.5.5.7.5.10.12.5.15.17.5.20.22.25017420
1.427.5.30.32.5.35.37.5.40.42.5.45./
DATA (PCIM2(I),I=1,12)/J=1,12)/.81.1.2.1.4.1.6.1.8.2.0.2.2.2.4.2.6.2.8.
13.0/
DATA (PCIM20(I),I=1,31)/J=5.75.1./
IF(DCR.GE.1.) DCR=1.
IF(DCR.LE.-5) DCR=-5
CALL LOOK3(PCIM2,PCIM2,15,12,ALPHA,PCIM2A,19,MACH,PCIM2M,12,DCR,
*PCIM20,3,14,15,12,1)
PHC1 = PHC1M2/MACH**2
RETURN
END
```



```

        IF(ALPHA-GE. 160.) GO TO 15
        CA = CAO-(CAO-CAPI)*SIN(ALPHAP/57.2957)
        GO TO 40
    15 CONTINUE
        CA = CAPI
        GO TO 40
    70 IF(ALPHA-GT.90.) GO TO 50
        CAW =(-0.0008 + 0.1501*(MACH/LND) + 0.3641*(MACH/LND)**2 + 0.0928*(MACH/LND)**3
        SMACH/LND)**3 - 0.0409*(MACH/LND)**4 + 0.004*(MACH/LND)**5)/(0.7*
        SMACH**2)
        CALL CSF(RN,MACH,CF)
        CASF = (4.0/5.0)*CFSWOR
        CAO = CAW + CASF +CDH
        CA = CAO
        GO TO 40
    50 IF(ALPHA-GE. 160.) GO TO 60
        CAPI = -(2.9217-9.1867*(MACH)+14.0023*(MACH)**2-8.7943*(MACH)**3+
        12.4985*(MACH)**4-0.2658*(MACH)**5)
        CA = CAO-(CAO-CAPI)*SIN(ALPHAP/57.2957)
        GO TO 40
    60 CAPI = -(2.9217-9.1867*(MACH)+14.0023*(MACH)**2-8.7943*(MACH)**3+
        12.4985*(MACH)**4-0.2658*(MACH)**5)
        CA = CAPI
    40 CONTINUE
        RETURN
        END
    
```

```

SUBROUTINE CSF(RN,MACH,CF)
C.....
C THIS PROGRAM CALCULATES THE SKIN FRICTION COEFFICIENT ON THE BODY
C.....
C RN = REYNOLDS NUMBER
C MACH = MACH NUMBER
C CF = SKIN FRICTION COEFFICIENT
C.....
REAL MACH,LAM
G = 1.4
LAM = 1.0/SORT((2.0/((G-1.0)*MACH**2))*1.0)
CF1 = 0.074*((1.0/RN**2))*1.0/((G-1.0)/2.0)*MACH**2)***.44
FCF1 = (ASIN(LAM)/LAM)*1.0/SORT(1.0/((G-1.0)/2.0)*MACH**2))*(-.242/019530
SSORT(CF1))-ALOG10(CF1)*RN)*1.26*(ALOG10(1.0/((G-1.0)/2.0)*MACH**2))
CF2 = CF1 * 0.00001
FCF2 = (ASIN(LAM)/LAM)*1.0/SORT(1.0/((G-1.0)/2.0)*MACH**2))*(-.242/019560
SSORT(CF2))-ALOG10(CF2)*RN)*1.26*(ALOG10(1.0/((G-1.0)/2.0)*MACH**2))
N = 1
10 DCF0DF = ((CF2-CF1)/(FCF2-FCF1))
CF3 = CF2 - DCF0DF*FCF2
IF(FCF2*LT-0.0) GO TO 15
CF3 = CF1 - DCF0DF*FCF1
15 N = N + 1
FCF3 = (ASIN(LAM)/LAM)*1.0/SORT(1.0/((G-1.0)/2.0)*MACH**2))*(-.242/019640
SSORT(CF3))-ALOG10(CF3)*RN)*1.26*(ALOG10(1.0/((G-1.0)/2.0)*MACH**2))
IF(ABS(FCF3)-LE-0.000001) GO TO 20
CF1 = CF2
FCF1 = FCF2
CF2 = CF3
FCF2 = FCF3
IF(M*GT-50.0) GO TO 30
GO TO 10
20 CF = CF3
30 WRITE(6,35)
35 FORMAT(1MO** THE ITERATION HAS GONE THROUGH 50 CYCLES*)
50 CONTINUE
RETURN
END

```

```

SUBROUTINE LOOK1(F,FT,X,XT,NX,IX,MULT)
C.....
C ONE-DIMENSIONAL TABLE LOOKUP ROUTINE (* = RETURNED VALUES)
C *F = FT(IX)
C *FT FUNCTION TABLE FT(NR)
C *NR NO. OF ROWS IN FT-TABLE
C *NC NO. OF COLUMNS IN FT-TABLE
C *X WORKING VALUE OF INDEPENDENT VARIABLE
C *XT INDEPENDENT VARIABLE TABLE
C *NX DIMENSION OF XT TABLE
C *IX X INDEX ON PREVIOUS LOOKUP (UPDATED ON EACH CALL)
C *MULT *0= USE PREVIOUS X
C *1= LOOKUP NEW X
C.....
C DIMENSION FT(1),XT(1)
C IF(MULT-1)2,1,2
C 1 CALL INDEX(X,XT,NX,IX,KEEP,RX)
C 2 F=FT(IX)
C 3 IF(KEEP-1)3,4,3
C 4 RETURN
C END

```


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SUBROUTINE LOOK2 74/74 OPT=1

```

C..... SUBROUTINE LOOK2(FT,NR,X,XT,NX,Y,YT,NY,IX,IY,MULT) 018320
C..... TWO-DIMENSIONAL TABLE LOOKUP ROUTINE (* = RETURNED VALUES) 018330
C..... F=FT(X,Y) 018340
C..... 018350
C..... FUNCTION TABLE FT(NR,NC) 018360
C..... NO. OF ROWS IN FT-TABLE 018370
C..... NC NO. OF COLUMNS IN FT-TABLE 018380
C..... X,Y WORKING VALUES OF INDEPENDENT VARIABLES 018390
C..... XT,YT INDEPENDENT VARIABLE TABLES 018400
C..... NX,NY DIMENSION OF XT,YT-TABLES 018410
C..... *IX,IY X,Y INDEXES ON PREVIOUS LOOKUP (UPDATED ON EACH CALL) 018420
C..... MULT =0, USE PREVIOUS X,Y 018430
C..... =1, LOOKUP NEW X,Y 018440
C..... 018450
C..... DIMENSION FT(1),XT(1),YT(1) 018460
C..... IF(MULT-1)2 018470
C..... 1 CALL INDEX(YT,NY,IY,KEEP,RY) 018480
C..... I = 1+(IY-1)*NR 018490
C..... II = 1+NR 018500
C..... 2 CALL LOOK1(F,FT(I),X,XT,NX,IY,MULT) 018510
C..... IF(KEEP-1)3,4,3 018520
C..... 3 CALL LOOK1(F2,FT(II),X,XT,NX,IX,1) 018530
C..... F=(F2-F)*RY+F 018540
C..... 4 RETURN 018550
C..... END 018560

```

```

SUBROUTINE INDEX(X,XT,NX,IH,KEEP,RATIO)
C.....018010
C TABLE INDEX LOOKUP ROUTINE (O = RETURNED VALUES) 018030
C X WORKING VALUE OF INDEPENDENT VARIABLE 018040
C XT INDEPENDENT VARIABLE TABLE XT(NX) 018050
C NX DIMENSION ON X-TABLE 018060
C IH INDEX OF PREVIOUS LOOKUP (UPDATED EACH CALL) 018070
C *KEEP = 0 X-NE-ANY XT. INTERPOLATION WAS REQUIRED. 018080
C          = 1 X-FO-AT(IH). INTERPOLATION NOT REQUIRED. 018090
C *RATIO INTERPOLATION RATIO 018100
C.....018110
C DIMENSION XT(1) 018120
C RATIO = 0. 018130
C KEEP = 0 018140
      IF(NX-IH).EQ.1,2
        1 IX = NX-1 018150
        2 IF(IH-1).EQ.3,4
          3 IX = 1 018170
          4 IF(NX-1).EQ.10,5
            5 IF(NT(IH)-NX).EQ.10,7 018180
            6 IF(NT(IH+1)-IX).EQ.9,11 018190
            7 IX = IX-1 018200
              IF(IH-1).EQ.5,5
                8 IX = IX+1 018210
                9 IF(IH-NX).EQ.10
                  9 IX = IX+1 018220
                  10 KEEP = 1 018230
                  10 RETURN 018240
                  11 RATIO = (X-XT(IH))/(XT(IH+1)-XT(IH)) 018250
                  11 RETURN 018260
                  END 018270
                  30

```


Appendix B. DESCRIPTION OF SUBROUTINES AND PROGRAM LISTING

Table B-1 lists the subroutines and gives their basic function.

A detailed description of each subroutine will not be included in this report. The logic and procedures required of each included method are discussed in detail in Reference 1. The applicable section of Reference 1 for each of the Methodology Program Subroutines is listed in Table B-1.

TABLE B-1. LIST OF PROGRAM ELEMENTS

SUBPROGRAM NAME	REF. 1 SECTION	FUNCTION OF SUBPROGRAM
MAIN		Controls input and output to the program. Uses various subroutines to calculate aerodynamic coefficients and centers of pressure for total missile and isolated components.
CNTPHI	SEC.5.2.1	Calculates tail normal force coefficient in presence of a cylindrical body as a function of roll angle. (Angle of attack limited to 0 to 45 degrees).
CNTT	SEC.5.1.4	Calculates tail normal force coefficient of an isolated tail (angle of attack 0 to 180 degrees).
BRIT		Contains data required by several other Methodology subroutines. Data is taken from British Data Sheets. (Reference 3).
CNBOD	SEC.5.1.1	Calculates body alone normal force coefficient (angle of attack 0 to 180 degrees).
XCPBOD	SEC.5.1.2	Calculates body alone center of pressure measured in calibers from the nose. (Angle of attack 0 to 180 degrees).
IBTT	SEC.5.2.4	Calculates body normal carry over force coefficient.
XCPBTT	SEC.5.2.5	Calculates tail-to-body carry over normal force center of pressure.
XCPTBB	SEC.5.2.2	Calculates the tail chordwise center of pressure (upper and lower bound)/ tail root chord, measured aft from root chord leading edge.

SUBPROGRAM NAME	REF. 1 SECTION	FUNCTION OF SUBPROGRAM
YCPTS	SEC.5.2.3	Calculates tail spanwise center of pressure for isolated tail.
XCPTT	SEC.5.1.5	Calculates chordwise center of pressure for isolated tail for roll angle = 0.
PHCC		Required by several other Methodology Subroutines.
AXIAL	SEC.5.1.3	Calculates the axial force coefficient for the missile body.
CSF	SEC.5.1.3	Calculates the skin friction coefficient for the missile body.
LOOK1		One-dimensional table look-up subroutine.
LOOK2		Two-dimensional table look-up subroutine.
LOOK3		Three-dimensional table look-up subroutine.
INDEX		Required for subroutines LOOK1, LOOK2, and LOOK3.

A complete program listing follows.

REFERENCES

1. Aiello, G.F., "Aerodynamic Methodology (Bodies With Arbitrary Roll Angles, Transonic and Supersonic)", Final report on USAMICOM Contract DAAH01-74-C-0621, OR 14,145, April 1976.
2. Spring, D.J., Derrick, J.N., and Winn, G.C., "An Assessment of the Martin-Marietta High Angle of Attack Aerodynamic Methodology for Body-Tail Missiles", TR RD-76-33, US Army Missile Command, June 1976.
3. Royal Aeronautical Society, Data Sheets, Wings 5.01.03.03, 5.01.03.04, 5.01.03.05, and 5.01.03.06.

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