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## **PVAST** PROPELLER VIBRATION AND STRENGTH ANALYSIS PROGRAM VERSION 7.3 EXAMPLES MANUAL

Koto, T.S., Palmeter, M.F., Chernuka, M.W. MARTEC Limited 1888 Brunswick Street, Suite 400 Halifax, Nova Scotia, Canada, B3J 3J8

Contract No. W7707-7-4689/001/HAL

### Defence R&D Canada DEFENCE RESEARCH ESTABLISHMENT ATLANTIC

Contractor Report
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# PVAST Propeller Vibration and Strength Analysis Program Version 7.3 Examples Manual

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#### **Abstract**

This report is an examples manual for the finite element analysis code called PVAST (Propeller Vibration And STrength) that is used for prediction of stress and vibration in marine propellers. PVAST can automatically generate propeller finite element models from basic propeller geometry defined by the orientation of 2D "wrapped" blade sections at specified radii. A number of different models can be considered including; a single blade, a single blade with fillet, a blade-fillet-palm model, a blade-fillet-hub segment model, and multiple blade and hub model. The types of structural finite element analyses that can be conducted include; static analysis with user-defined blade pressure distributions and point loads, natural frequency analysis in air and in water, time domain analysis with applied loads and support motion, response spectrum analysis and frequency response analysis. The program provides 2D and 3D plotting of blade geometry, finite element models and postprocessing to provide visualization of predicted finite element model displacements, stresses and mode shapes. The code has been modified recently to include a "Windows" graphical user interface implemented with a combination of GKS and MS Visual C++. This provides a more "friendly" user interface and is a major change in the look and feel of PVAST Version 7.3 compared with earlier versions of the code. This manual provides a number of example problems, considered with PVAST Version 7.3 for a range of model types, analysis options and results.

#### Résumé

Le présent rapport est un manuel d'exemples pour le code d'analyse par éléments finis appelé PVAST (Propeller Vibration And Strength [vibrations et résistance des hélices]) qui sert à prédire les contraintes et les vibrations sur les hélices de navires. Ce logiciel peut générer automatiquement des modèles par éléments finis d'hélices à partir de leur géométrie de base définie par l'orientation des sections de pales en 2 dimensions à des rayons spécifiés. Un certain nombre de modèles peuvent être étudiés : une seule pale, une seule pale avec raccordement de racine, un modèle de pale-raccordement-tourteau, un modèle de paleraccordement-moyeu et un modèle avec pales multiples et un moyeu. Les types d'analyse structuralle par éléments finis qui peuvent être exécutées comprennent les analyses statiques avec les répartitions des pressions sur les pales et les contraintes ponctuelles définies par l'utilisateur, les analyses des fréquences propres dans l'air et dans l'eau, l'analyse dans le domaine temporel avec les contraintes exercées et les déplacements des supports, l'analyse du spectre de réponses et l'analyse des réponses en fréquences. Le programme donne un tracé de la géométrie des pales en 2 D et en 3 D, des modèles par éléments finis et un post-traitement pour obtenir une visualisation des prévisions par éléments finis des mouvements des modèles, des contraintes et des formes de modes. Le code a été modifié récemment pour inclure une interface graphique de l'utilisateur sur système d'exploitation Windows; elle fonctionne avec une combinaison d'un système graphique de base GKS et du logiciel MS Visual C++, ce qui donne une interface plus pratique et constitue un changement majeur dans l'apparence et la présentation de la version 7.3 de PVAST par rapport aux versions précédentes de ce code. Le manuel donne un certain nombre d'exemples de problèmes, basés sur la version 7.3 du PVAST et qu'on prévoit pour une série de types modèles, d'options d'analyses et de résultats.

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#### **Executive summary**

Background: A marine propeller blade has very a complicated geometry. In order to obtain an accurate assessment of propeller strength and vibration characteristics it is necessary to use numerical analysis methods. Methods for structural analysis of marine propellers have been developed at DREA through in-house and contracted research based on the finite element method. A computer code called PVAST (Propeller Vibration And STrength) has been written to automatically generate propeller finite element models from basic propeller geometric data. The code can automatically produce a number of different models including; a single blade, a single blade with fillet, a blade-fillet-palm model, a blade-fillet-hub segment model, and a multiple blade and hub model. The types of structural finite element analyses that can be conducted include; static analyses with user-defined blade pressure distributions and point loads, natural frequency analyses in air and in water, time domain analyses with applied loads and support motion, response spectrum analyses and frequency response analyses. The program provides 2D and 3D plotting of blade geometry, finite element models and post-processing visualization of predicted finite element model displacements, stresses and mode shapes. The code has been modified recently to include a "Windows" graphical user interface implemented with a combination of GKS and MS Visual C++ coding.

**Principal Results:** The principal result arising from the recent work on the code is a user-friendly graphical interface. This is a major change in the look and feel of PVAST Version 7.3 compared with earlier versions of the code. It is easier to use and accessible to more users since it can now be run on PCs with Windows95, 98 and NT operating systems, whereas previously, it could only be run on a mainframe computer or UNIX work station.

**Significance of Results:** Because of their complicated three-dimensional geometry, the generation of propeller finite element models using general purpose finite element modeling programs is very time consuming and prone to errors. The PVAST code allows the user to enter propeller geometry in formats commonly used by propeller designers. It provides a number of graphical tools for checking the input geometry and automatically generating finite element models. It also presents results in many formats, many specialized for propeller geometry. This program will allow DREA scientists and navy engineers to quickly build reliable structural models of propellers to analyze strength and vibration problems in existing designs and also to assess structural characteristics of future designs.

Koko, T.S., Palmeter, M.F., Chernuka, M.W. 2001. PVAST Propeller Vibration and Strength Analysis Program Version 7.3 Examples Manual. DREA CR 2000-153 Defence Research Establishment Atlantic.

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#### Sommaire

**Explication:** Une hélice de navire possède une géométrie très complexe. Pour obtenir une évaluation précise des caractéristiques de résistance et de vibration d'une hélice, il est nécessaire de faire appel aux méthodes d'analyse numériques. Les méthodes d'analyse structurale des hélices de navires ont été développées au CRDA grâce des recherches effectuées sur place ou sous contrat, toutes fondées sur la méthode par éléments finis. Un code informatique appelé PVAST (Propeller Vibration And STrength [vibrations et résistance de hélices]) a été développé pour générer automatiquement des modèles par éléments finis d'hélices à partir de données géométriques d'hélices de base. Ce code peut produire automatiquement un certain nombre de modèles différents : une seule pale, une seule pale avec raccordement de racine, un modèle de pale-raccordement-tourteau, un modèle de paleraccordement-moyeu et un modèle avec pales multiples et moyeu. Les types d'analyse structurale par éléments finis qui peuvent être exécutées comprennent : les analyses statiques avec répartitions des pressions sur les pales et les contraintes ponctuelles définies par l'utilisateur, des analyses des fréquences propres dans l'air et dans l'eau, des analyses dans le domaine temporel appliquées aux contraintes et aux mouvements des supports, des analyses du spectre des réactions et des analyses des réponses en fréquences. Le programme donne un tracé de la géométrie des pales en 2 D et en 3 D par éléments finis, des modèles par éléments finis et une visualisation post-traitement des prédictions des mouvements des modèles, des contraintes et des formes de mode. Le code a été modifié récemment pour comprendre une interface graphique avec l'utilisateur sur Windows, mis en œuvre avec une combinaison d'un système graphique de base GKS et du logiciel MS Visual C++.

**Principaux résultats:** Le principal résultat des travaux récents effectués sur le code est une interface graphique plus pratique. Il s'agit d'un changement important dans l'apparence et la présentation de la version 7.3 de PVAST, par rapport aux versions précédentes de ce code. Il est plus facile à utiliser et est accessible à plus d'utilisateurS car il peut maintenant fonctionner sur des ordinateurs personnels avec les systèmes d'exploitation Windows 95, 98 and NT, alors qu'auparavant il ne pouvait fonctionner que sur un ordinateur central ou un poste de travail UNIX.

Importance des résultats: En raison de leur géométrie tri-dimensionnelle complexe, la génération de modèles d'hélice par des programmes universels de modélisation par éléments finis demande beaucoup de temps et est sujette à des erreurs. Le code PVAST permet à l'utilisateur d'entrer une géométrie d'hélice dans des formats fréquemment exploités par des concepteurs d'hélices. Il fournit un certain nombre d'outils graphiques pour vérifier la géométrie retenue et pour générer automatiquement des modèles par éléments finis. Il présente aussi les résultats en plusieurs formats, beaucoup d'entre eux spécialisés dans la géométrie des hélices. Ce programme permettra aux scientifiques du CRDA et aux ingénieurs maritimes de construire rapidement des modèles de structure d'hélices fiables pour analyser les problèmes de vibration et de résistance des hélices existantes et aussi d'évaluer les caractéristiques structurales des hélices futures.

Koko, T.S., Palmeter, M.F., Chernuka, M.W. 2000. Manuel D'utilisation Du Programme D'analyse Des Vibrations Et De La Résistance Des Hélices PVAST, Version 7.3. CRDA CR 2000-153 Centre pour la Recherche de la D'efence Atlantique.

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#### 1. INTRODUCTION

#### 1.1 Background

This document provides example problems to demonstrate the use of program PVAST version 7.3. PVAST is a computer program for the strength and vibration analysis of marine propellers. It is based on the finite element method of structural analysis and is designed to automatically generate finite element models for a wide variety of propeller shapes. The three-dimensional spatial co-ordinates of the blade geometry are automatically generated from the two-dimensional blade section data format in which the blade geometry is generally described. Finite element meshes of the blade geometry are automatically generated from a choice of shell and solid elements. The program can graphically display the geometry and the finite element model for data checking purposes. Static, natural frequency and dynamic response analyses can be carried out with the program. The analytical results can be processed and displayed in graphic form for ease of interpretation to show stresses, displacements, natural frequency of vibration and dynamic response.

#### 1.2 PVAST Capabilities

PVAST has several capabilities covering the types of structural models, types of analysis and display options. Detailed descriptions of these options are provided in Reference 5 and are summarized below.

#### 1.2.1 Types of Propeller Blade Models

There are eight types of structural models available in PVAST. These include:

- Blade Only
- Blade-Fillet
- Blade-Fillet-Palm (Bolt as Rods)
- Blade-Fillet-Palm (Super Elements)
- Blade-Fillet-Hub
- Multi-Blade Hub
- Key-way
- Air-channel

Figures 1.1 to 1.8 show typical views of the eight structural models.

#### 1.2.2 Analysis Types

PVAST offers the following analysis types:

- Static analysis
- Natural frequency analysis in air
- Natural frequency analysis in water

- Time history dynamic analysis due to applied loading or support motion
- Response spectrum analysis
- Frequency response analysis

#### 1.2.3 Display Options

PVAST provides several plotting options that are categorized into *General Plots* and *Special Plots*. The *General Plots* option utilizes the MGDSA general-purpose pre- and post-processing graphics capabilities for displaying the propeller finite element models and results. The *Special Plots* option utilizes special graphics capabilities for displaying data, models and results that are specific to propeller blades. Table 1.1 shows the display options available in PVAST.

**Table 1.1: PVAST Display Options** 

GENERAL PLOT	SPECIAL PLOTS
Pre-Processing:	Pre-Processing:
Blade, root, substructure and fluid FE	Blade geometry input data
models	Individual section plots
FE loads and boundary condition plots	Magnified nose/tail sections
	Views of single blade sections
	View of assembled blade
	Chordwise pressure plots
	Blade-to-root intersection
	Fluid FE model
Post-Processing:	Post-Processing
Displacements	Chordwise displacements and stresses
Stresses	Blade section displacement and mode
Mode Shapes	shapes
	Displacement/stress time histories at
	selected radial/chordwise positions
	Radial, tangential and normal force
	vectors

#### 1.2.4 Operating System

PVAST is designed to be hardware portable and is available on personal computers (PC) with Windows 95/98 operating system.

#### 1.3 Applicable Documents

The following documents should be consulted to gain familiarity with marine propeller blade geometry, finite element theory, and the MGDSA graphics capabilities:

- T.S. Koko, M.F. Palmeter, M.W. Chernuka, and T. MacFarlane. "PVAST. Propeller Vibration and Stress Analysis by Finite Element Methods Version 7.3 User's Manual." Martec Limited, June 2000.
- M.W. Chernuka, M.E. Norwood and T.S. Koko. "Propeller Vibration and Stress Analysis by Finite Element Methods (PVAST) Version 4 User's Manual." Martec Limited, July 1992.
- D.R. Smith and T.R. MacFarlane. "BLADE: A Propeller Blade Geometry Generator Program User's Manual." DREA Technical Communication 91/302, February 1991.
- J.L. Kerwin and C.S. Lee. "Prediction of Steady and Unsteady Marine Propeller Performance by Lifting Surface Theory." Vol. 86, 1978. (Provides background on lifting surface programs PINV4 and PUF2 for steady and unsteady propeller force predictions, respectively. Distribution of these program is limited.)
- MicroVAST Graphics System User's Manual. Martec Limited, March 1996.
- Vibration and Strength Analysis Program (VAST): User's Manual Version 7.3, Martec Limited, April 1997.

#### 1.4 Organization of This Manual

The remainder of this manual is organized as follows:

- Chapter 2: Provides examples on how to generate the geometry of propeller blades. The DREA propeller blades named TRUMP, NRC45, P5363 and P4388 are used for the demonstrations.
- Chapter 3: Demonstrates how to generate *Blade Only* finite element models, perform natural frequency analysis in air and to display the results, using the NRC45 propeller blade. Finite element models (*Blade Only*) of P5363 and P4388 propeller blades are also presented.
- Chapter 4: Demonstrates how to generate fluid finite element models, perform natural frequency analyses in water and to display the results, using the NRC45 propeller blade. The development of fluid finite elements for the P5363 and P4388 propeller blades is also presented.

#### INTRODUCTION

Chapter 5:	Shows how to perform stress analysis of Blade Only finite element
	models and to display the results, using the P5363 propeller blade.
Chapter 6:	Illustrates how to generate Blade-Fillet-Hub models, using the P5363,
	P4388 and NRC45 propeller blades
Chapter 7:	Demonstrates how to generate Blade-Fillet-Palm models using another
	DREA propeller blade named PD280.
Chapter 8:	Illustrates how to generate a two-dimensional hub model with a Keyway.
Chapter 9:	Demonstrates how to generate air-channel models of the blade and
	perform stress analysis. The P5363 propeller blade is used for this
	purpose.

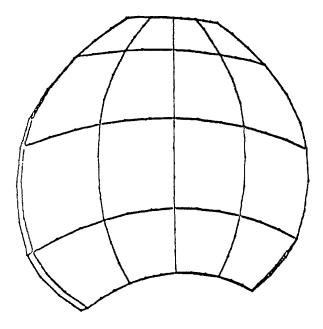


Figure 1.1: Blade Only Model

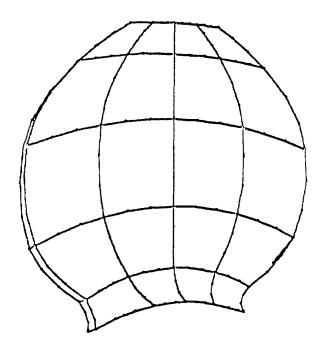


Figure 1.2: Blade-Fillet Model

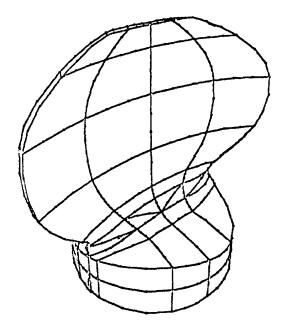


Figure 1.3: Blade-Fillet-Palm (Bolts as Rods) Model (shown without bolts)

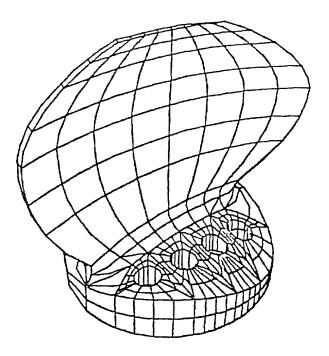


Figure 1.4: Blade-Fillet-Palm (Bolts as Superelements) Model

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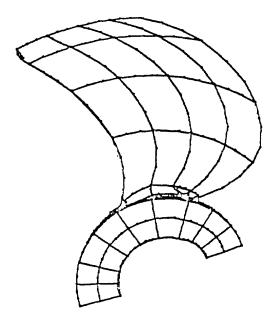


Figure 1.5: Blade-Fillet-Hub Model

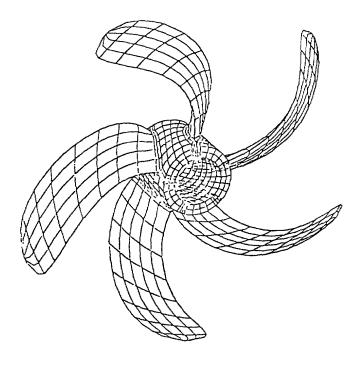


Figure 1.6: Multi-Blade Hub Model

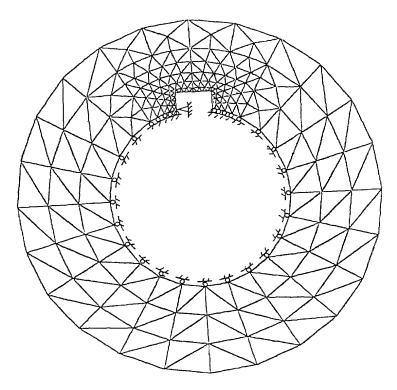


Figure 1.7: Keyway Model

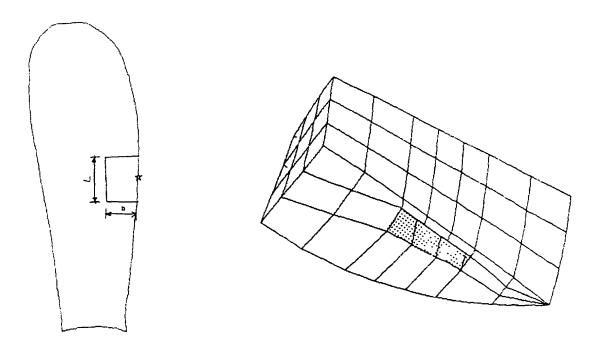


Figure 1.8: Air Channel Model

#### 2. BLADE GEOMETRY GENERATION

#### 2.1 Introduction

This chapter illustrates how to generate the geometry of propeller blades. This is considered to be the first main step of the blade finite element modelling process. This could be a fresh start or the blade geometry definition data may be available on a file called PREFIX.DAT, where PREFIX is the alphanumeric prefix name used to identify files for the current session. When the latter is the case, the data is presented in the PREFIX.DAT according to the format specified in Appendix A, and the user could proceed to edit/modify or graphically view the data as illustrated in this chapter. For a fresh start, the procedure illustrated in this chapter has to be followed.

Figure 2.1 shows the **Blade Geometry** Submenu. The steps involved are:

- Definition of Basic Data;
- Definition of Radial Data;
- Definition of Chordwise Data;
- Definition of Edge Data, if required; and
- Definition of Hub/Palm data, if required.

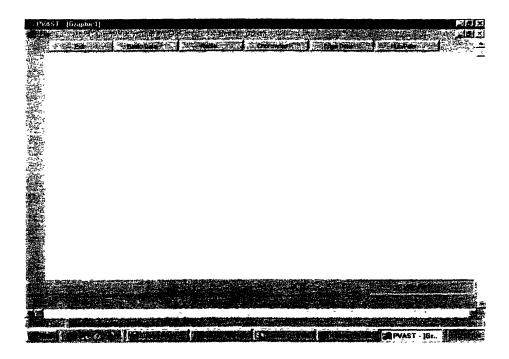


Figure 2.1: Blade Geometry Menu

It is preferable to go through the steps in the order shown. The blade data is defined through several edit tables, and graphical plots of the data and the blade geometric configuration are provided to aid the modelling process. In Section 2.2, details of the edit tables and the significant plots for DREA's TRUMP propeller blade are provided. Then in Sections 2.3 to 2.5, the data entered for generating three other blades, namely DREA's NRC45, P5363 and P4388 propeller blades are presented.

It should be noted that during the blade geometry definition process, the program creates several files that are required for plotting the data or required by other modules of PVAST. One of these files is the PREFIX.T16 file which is required for creating the finite element grid proportions [1]. This file may also serve as a starting point in the PVAST modelling process. When this is the case, the blade geometry definition step is not required, and the user should go directly to the FE grid proportions definition step. The format of the PREFIX.T16 file is also shown in Appendix A.

#### 2.2 Geometry of TRUMP Propeller Blade

#### 2.2.1 Basic Data

Figure 2.2 shows the basic propeller data entered for this blade. The form of data is offsets.

	IC PROPE	LER DATA
Date Tale (25) chas	oriers)	BLADE-PALM MODEL
Unit of Measure		MILLIMETERS
Blade Radiks 1		2159 000
PARKET TO SERVE		RIGHT
Minber of Reduction		11
PAREOLEMAN -		ANGULAR
		LINEAR
		Y
		OFFSETS
		17
		Same
		Not Used
	er, gr	

Figure 2.2: Basic Data for TRUMP Propeller Blade

#### 2.2.2 Radial Data

Figure 2.3 shows the radial data entered for this blade.

2980	775.0810	48 0790	49 8000	5000
3000	779 8310	48 3320	45 8000	3.8000
3500	923 1180	50 0770	-48 9000	78 1000
4000	1059 2050	49 3200	-126 9000	139 9000
5000	1341 1710	45 1310	-196 6000	188 6000
6000	1611 9090	39 2260	-158 3000	155.3000
7000	1763 9030	34 2260	-49.2000	88 1000
8000	1734 1090	29 0150	118 5000	8 6000
9000	1427 9630	22 9970	324 7000	-55 2000
9500	1094 1810	19 4000	431 4000	-68 6000
9750	823 8740	17 3680	485 5000	-68 9000

Figure 2.3: Radial Data for TRUMP Propeller Blade

Figures 2.4 to 2.7 show the variations of the chord length, pitch, skew and rake along the radial direction.

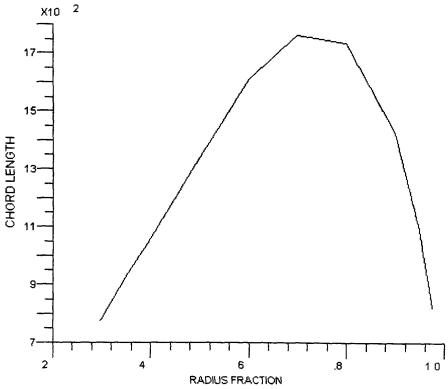


Figure 2.4 Plot of Chord Length vs Radial Fraction for TRUMP Propeller Blade

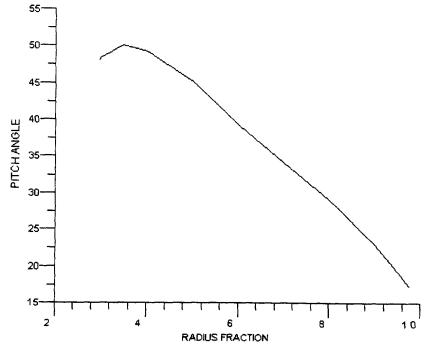


Figure 2.5: Plot of Pitch Angle vs Radial Fraction for TRUMP Propeller Blade

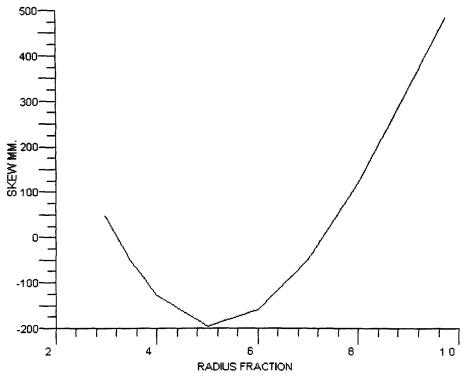


Figure 2.6: Plot of Skew vs Radial Fraction for TRUMP Propeller Blade

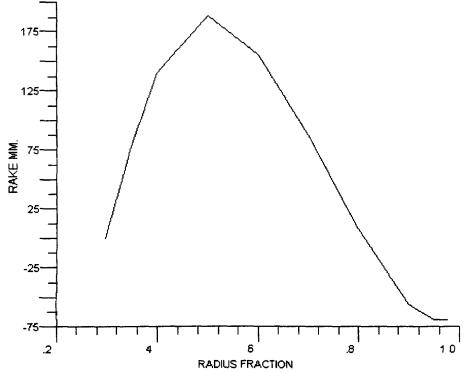


Figure 2.7: Plot of Rake vs Radial Fraction for TRUMP Propeller Blade

#### 2.2.3 Cross Section Data

Figures 2.8 (a) to (k) show the cross section data at the 11 radial positions entered for this blade.

0000	0000	0000	6000	-80 1000	85 9640
0100	-15 9000	17 5010	7000	-69 6000	74 4780
0250	-25 0000	27 3530	8000	-53 7000	57 3720
0500	-35 3000	38 4600	9000	-32 3000	34 7390
1000	-49 8000	54 0000	9500	-19 6000	21 2370
2000	-68 5000	74 1520	9750	-12 8000	13 9520
3000	-79 7000	85 8710	9900	-8 6000	9 5410
4000	-85 2000	91 6300	1 0000	-5 6000	6 2780
5000	-85 4000	91 7540			

(a)

IORO FRACTIO	SACK DESCRIPTION	CROSS SECTION	The state of the s		FACEORISET
0000	0000	0000	6000	-79 4100	85 1580
0100	-15 8850	17.4060	7000	-69 8420	73 7560
0250	-24 9940	27 1770	8000	-53 8710	56 8030
0500	-35 3260	38 1960	9000	-32 3630	34 4370
1000	-49 8620	53 5820	9500	-19 5970	21 0790
2000	-68 8120	73 5380	9750	-12 7500	13 8650
3000	-79 8940	85 1260	9900	-8 6170	9 4910
4000	-85 4150	90 8190	1 0000	-5 5990	6 2620
5000	-85 6640	90 9130			
BADI		OK	Cancel 1		SHELD.

torne il sere di sis					<b>FLEXIBLE</b>
0000	0000	0000	6000	-87 0470	70 6330
0100	-15.6300	15.2510	7000	-72 2950	60 9030
0250	-24 8340	23 5510	8000	-55 8710	46 7870
0500	-35 4140	32 7820	9000	-33 1610	28 8040
1000	-50 4150	45 5410	9500	-19 7750	17 9470
2000	-70 0890	61.9550	9750	-12 6850	12 0010
3000	-81 7110	71 3630	9900	-8 4100	8 3910
4000	-87 6010	75 8680	1 0000	-5 3270	5 6590
5000	-88 1000	75 7010	1		1

(c)

0000	0000	0000	6000	-84 5990	56 9320
0100	-15 1150	13 1660	7000	-73 2330	48 7980
0250	-24 2660	20 0610	8000	-56 6890	37 3580
<b>)500</b>	-34 8800	27 5920	9000	-33 2910	23 4830
1000	-50 0260	37 8880	9500	-19 5950	14 9670
2000	-70 0030	50 9580	9750	-12 4030	10 2210
3000	-81 8980	58 3200	9900	-8 0820	7 3090
4000	-88 0200	61 7310	1 0000	-5 0100	5 0740
5000	-88 7190	61 3280			

(d)

0000	0000	0000	6000	-79 8130	31 5170
0100	-13 0500	9.3350	7000	-70 2100	26 3270
0250	-21 4450	13 6260	8000	-54 5450	19 8630
0500	-31 4100	18 0250	9000	-31 3030	13 5990
1000	-45 8410	23 7120	9500	-17 9050	9 4420
2000	-65 1140	30 5920	.9750	-10 9840	6 9200
3000	-76 7820	34 1600	9900	-6 8530	5 3380
4000	-82 9650	35 51 40	1.0000	-3 9830	3 9830
5000	-84 0380	34 6830			

#### **BLADE GEOMETRY GENERATION**

HICERAGNON	Core				
0000	0000	0000	6000	-74 0670	13 0890
0100	-10 1230	7.6080	7000	-66 0240	12 6860
0250	-16 5700	10 3810	8000	-51 6780	11 0420
0500	-24 7750	12 7020	9000	-30 2230	7 3660
1000	-37,2350	14 3780	9500	-16 6030	4 5300
2000	-55 1430	14 5070	9750	-9 0110	2 8210
3000	-67 1360	13 7820	9900	-4 1010	1 8860
4000	-74 2130	13 2340	1 0000	- 9030	9030
5000	-76 5660	13 0570			

(f)

0000	0000	0000	6000	-63 3060	- 0180
0100	-7 7440	5 1 3 3 0	7000	-56 2860	8820
0250	-13 0000	6 5790	8000	-43 8860	1 6580
0500	-19 8790	7 3380	9000	-25 5240	1 7810
1000	-30 6210	6 8790	9500	-13 9350	1 4110
2000	-46 4080	4 1810	9750	-7 5140	1 0760
3000	-57 0970	1 6760	9900	-3 5810	9700
4000	-63 41 20	- 0880	1 0000	- 6530	6530
5000	-65 5290	4410			

(g)

0000	0000	0000	6000	-47 9830	-3 6240
100	-5 5840	3 4510	7000	-42 6070	-2 5490
250	-9 4860	4 2310	8000	-33 1560	-1.2490
500	-14 6360	4 4220	9000	-19 2490	- 1040
000	-22 8030	3 4510	9500	-10 4910	2780
2000	-34 9250	5200	9750	-5 6360	3820
3000	-43 1620	-1 9940	9900	-2 6530	5380
1000	-48 0520	-3 5550	1 0000	- 4510	4510
5000	-49 6820	-4 0750			

(h)

0000	0000	0000	6000	-27 1880	.5860
0100	-3 3700	2 2850	7000	-24 1750	9000
0250	-5 6410	2 9420	.8000	-18 8630	1 1280
0500	-8 5960	3 3410	9000	-10 9810	1 0000
1000	-13 2090	3 2410	9500	-5 9970	7280
2000	-19 9630	2 2280	9750	-3 2410	5280
3000	-24 5320	1 2570	9900	-1 5420	4570
4000	-27 2310	6430	1 0000	- 2860	2860
5000	-28 1310	4280			

(i)

0000	0000	0000	6000	-15 6800	4 3330
100	-2 2650	1 8050	7000	-13 9950	4 0700
0250	-3 6650	2 5170	8000	-10 9750	3 4140
500	-5 4270	3 1730	9000	-6 445D	2 1880
000	-8 0530	3 7970	9500	-3 5450	1 3020
2000	-11 7730	4.2130	9750	-1 9370	<b>77</b> 70
3000	-14 2460	4 3220	9900	- 9520	4810
1000	-15 71 20	4 3660	1 0000	- 2080	2080
5000	-16 1940	4 3770			

(j)

0000	0000	0000	77 (GRB REACTO) 6000	-9 3590	6 9860
0100	-1 7140	1 6150	7000	-8 4200	6 3440
0250	-2 6450	2 4060	8000	-6 6730	5 0910
0500	-3 7490	3 2790	9000	-3 9710	3 0810
1000	-5 2890	4 3990	9500	-2 2160	1 7470
2000	-7 3240	5 7420	9750	-1 2280	9890
3000	-8 6260	6 5500	9900	- 6340	5360
4000	-9 3840	7 0110	1 0000	- 1650	1650
5000	-9 6390	7 1680			

(k)

Figure 2.8: Cross-section Data for TRUMP Propeller Blade

Figures 2.9 and 2.10 show plots of the back and face offsets at the first radial position (radial fraction = 0.298).

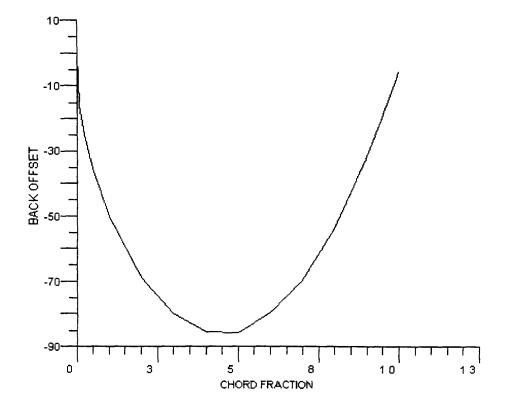


Figure 2.9: Variation of Back Offsets with Chord Fractions for TRUMP Propeller Blade

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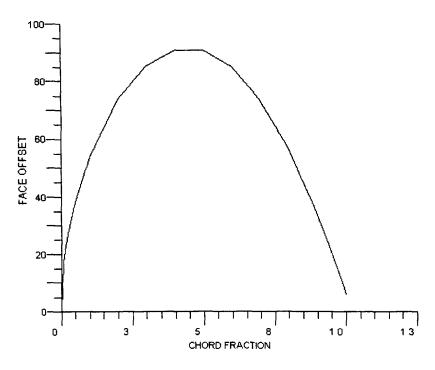


Figure 2.10: Variation of Front Offsets with Chord Fractions for TRUMP Propeller Blade

#### 2.2.4 Edge Data

Figure 2.11 shows the blade edge data entered for the TRUMP blade.

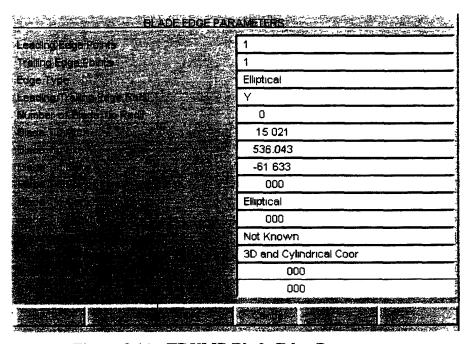
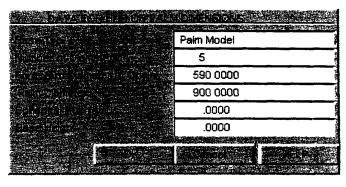


Figure 2.11: TRUMP Blade Edge Parameters

#### 2.2.5 Hub/Palm Data

Figure 2.12 shows the hub/palm data entered for this blade.



(a)

eti.	1082 0000	0000
	1198 0000	210.0000
	1410 0000	590 0000
	1363.0000	1050.0000
	300 0000	2462 0000
	THINK THE COM	

Figure 2.12: Hub/Palm Data for TRUMP Propeller Blade

This completes the blade geometry data definitions. By clicking **EXIT** on the blade geometry submenu (Figure 2.1), the program generates the complete blade geometry.

#### 2.2.6 Plots of TRUMP Blade Geometry

Several options are provided for plotting the blade geometry including the blade data. These options are available under the **Special Plots (Model)** option and are accessed by clicking **Display** on the PVAST main menu, **Special Plots (Model)** and then **Blade Geometry**. The available options are shown in Figure 2.13.

TI

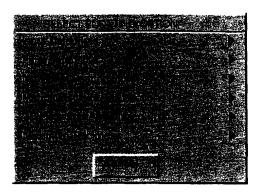


Figure 2.13: Blade Geometry Plotting Options

Final Data Plots

Figures 2.14 and 2.15 show plots of the maximum camber and maximum thickness versus the section radii plotted through the **Final Data Plots** option (Figure 2.13).

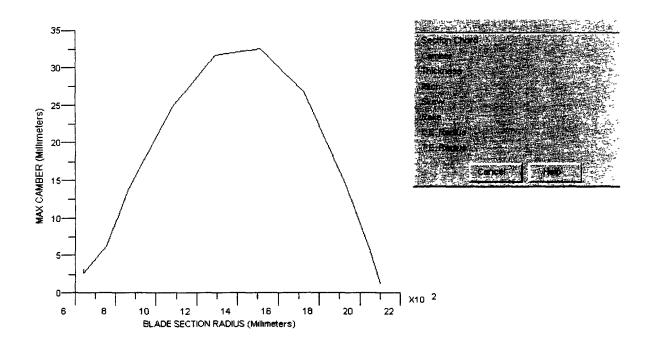


Figure 2.14: Maximum Camber vs Section Radius of TRUMP Blade

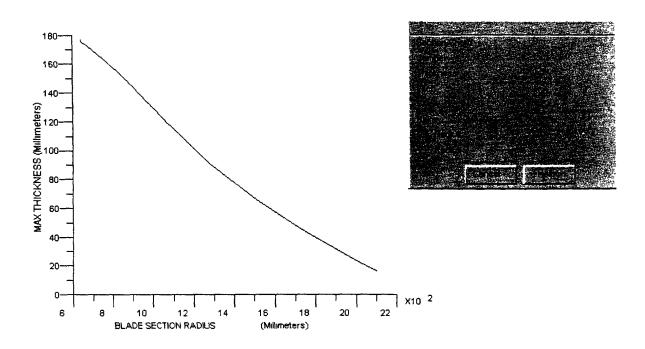


Figure 2.15: Maximum Thickness vs Section Radius of TRUMP Blade

Individual Section Plots

Figure 2.16 shows a typical section plot (at radial fraction 0.4) plotted through the **Individual Section Plots** option (Figure 2.13).

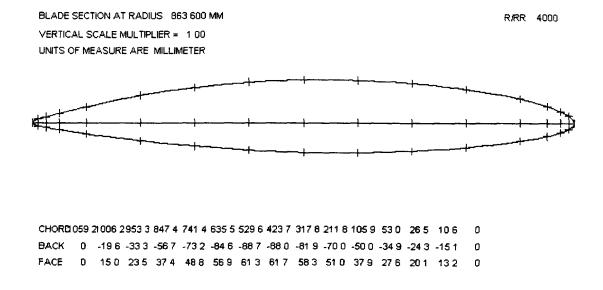


Figure 2.16: Individual Section Plot for TRUMP Propeller Blade

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Magnified Nose/Tail Sections

Figure 2.17 shows the magnified leading edge section (at 0.4 radial fraction) plotted through the **Magnified Nose/Tail Sections** plotting option (Figure 2.13).

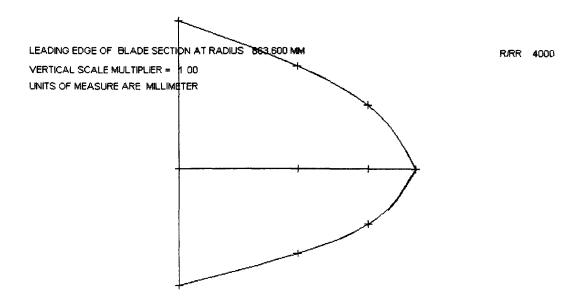


Figure 2.17: Magnified Leading Edge of TRUMP Propeller Blade

### 3-D Plots and Assembled Prop

Figures 2.18 to 2.28 show views of a single blade of the TRUMP propeller.

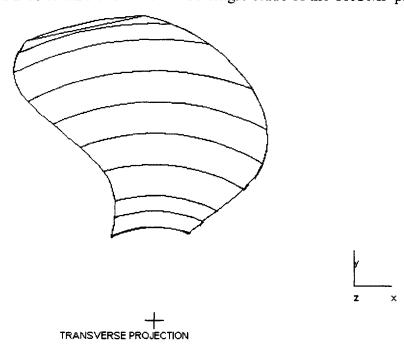


Figure 2.18: Transverse Projection of TRUMP Propeller Blade

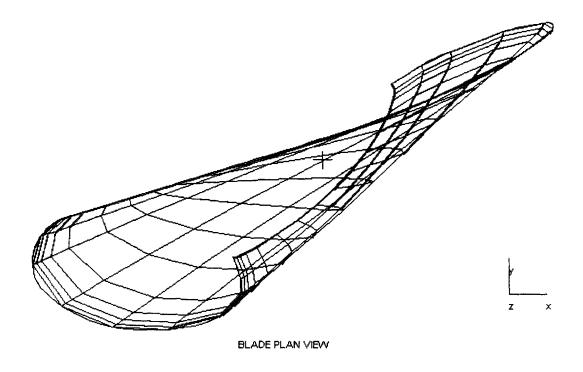


Figure 2.19: Plan View of TRUMP Propeller Blade

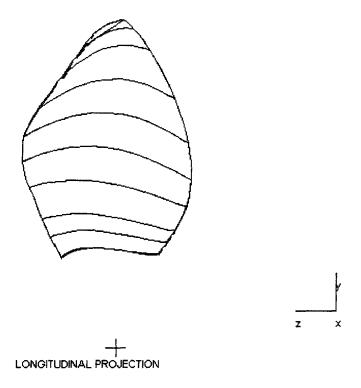


Figure 2.20: Longitudinal Projection of TRUMP Propeller Blade

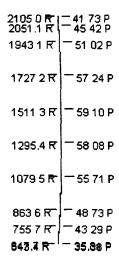


Figure 2.21: Pitch Diagram of TRUMP Propeller Blade

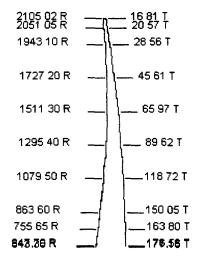




Figure 2.22: Blade Thickness at 50% Chord for TRUMP Propeller Blade

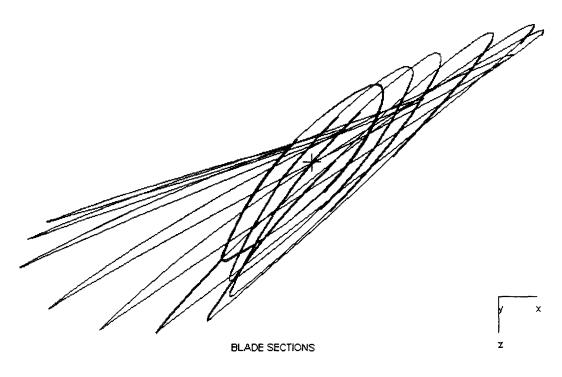


Figure 2.23: Plan View of Blade Sections for TRUMP Propeller Blade

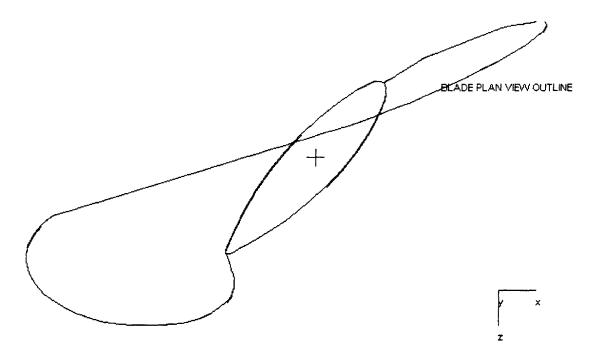


Figure 2.24: Plan View Outline of TRUMP Propeller Blade

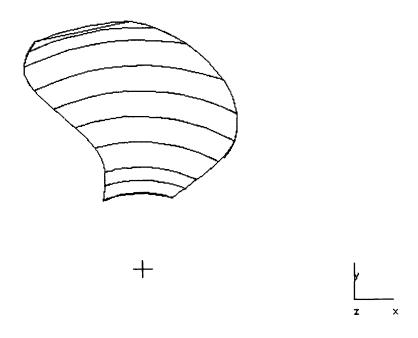


Figure 2.25: Developed Outline of TRUMP Propeller Blade

DEVELOPED OUTLINE

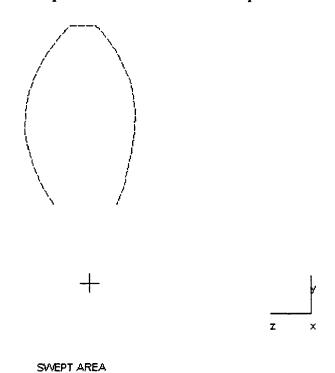


Figure 2.26: Swept Area of TRUMP Propeller Blade

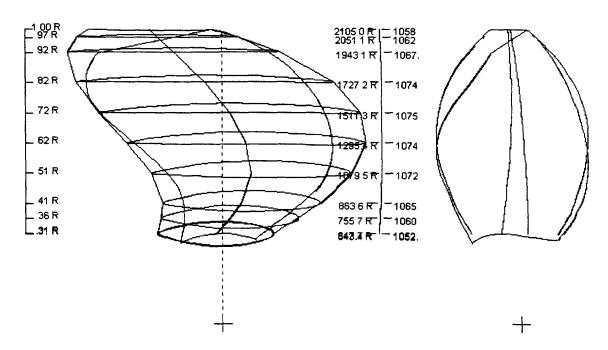
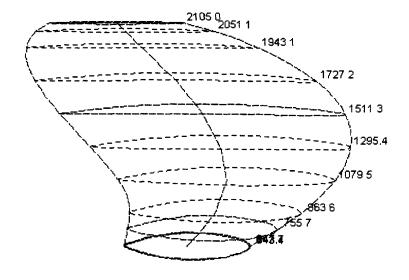


Figure 2.27: Combined Drawing of TRUMP Propeller Blade (3rd Angle Projection)



EXPANDED SECTIONS

Figure 2.28: Expanded View of TRUMP Propeller Blade

- T T

Figure 2.29 shows a view of an assembled propeller with 3 blades.

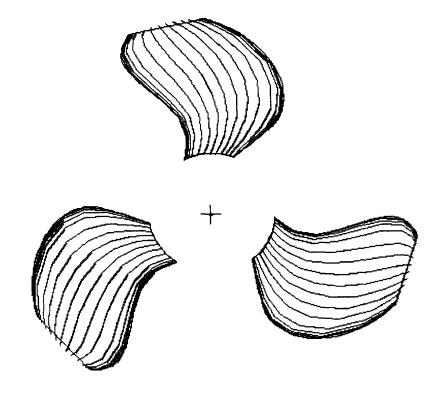
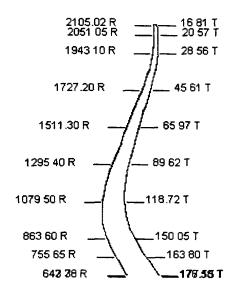


Figure 2.29: View of Assembled TRUMP Propeller Blade

# Maximum Thickness

Figure 2.30 shows plots of the maximum thickness with and without rake, plotted through the **Maximum Thickness** plotting option.



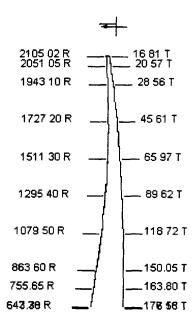


Figure 2.30: Maximum Thickness of TRUMP Propeller Blade With and Without

Rake

T T

Following the above proceedings, the geometries of other blades can be defined and plotted.

# 2.3 Geometry of NRC45 Propeller Blade

The blade geometry data for this propeller blade is shown in the NRC45.DAT file presented in Appendix A.

# 2.4 Geometry of P5363 Propeller Blade

The blade geometry data for this propeller blade is shown in the P5363.DAT file presented in Appendix A.

# 2.5 Geometry of P4388 Propeller Blade

The blade geometry data for the P4388 propeller blade is shown in the P4388.DAT file presented in Appendix A.

The blade geometry definition step generates PREFIX.T16 files which are used for developing models in Chapters 3 to 9.

#### 3. BLADE ONLY MODEL FOR VIBRATION ANALYSIS IN AIR

### 3.1 Introduction

In this chapter, we shall demonstrate how to generate a propeller blade finite element model, perform a natural frequency analysis of the model; and to view the results. It is assumed that the blade geometry data has been entered and geometry defined, as described in Chapter 2. Thus, a PREFIX.T16 file is now available in the working directory, where, "PREFIX" is the alphanumeric prefix of the file name. The narrow blade (NRC45) propeller blade shall be used for this demonstration. With the blade geometry already defined, the remaining steps are:

- (i) To generate the finite element model
- (ii) To perform the finite element analysis using the VAST program; and
- (iii) To post process and view the results

These steps are described in Sections 3.2 to 3.4.

In Sections 3.5 and 3.6 the generation of *Blade Only* finite element models for two other blades, namely the P5363 and P4388 propeller blades, respectively, are presented.

#### 3.2 Finite Element Model Generation

This step involves the development of the finite element model of the propeller blade. This step involves the following sub-tasks:

- Selection of model type;
- Generation of FE grid proportions;
- Generation of the blade FE mesh; and
- Generation of boundary conditions.

These subtasks are described in the following subsections.

#### 3.2.1 Select Model Type

Click **Model** on the main menu and ensure that the **Blade Only** model is highlighted, as shown in Figure 3.1.

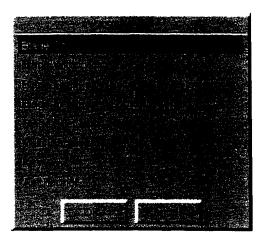


Figure 3.1: Model Submenu

# 3.2.2 Generate Finite Element Grid Proportions

Click the **Create/Modify** on the main menu and select the **FE Grid Proportions** option on the **CREATE/MODIFY** submenu (Figure 3.2).

The **FE Grid Proportions** submenu appears as shown in Figure 3.3. This submenu also provides capability for editing the blade geometry data available on the PREFIX.T16.

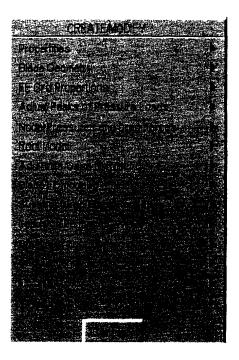


Figure 3.2: Create/Modify Submenu

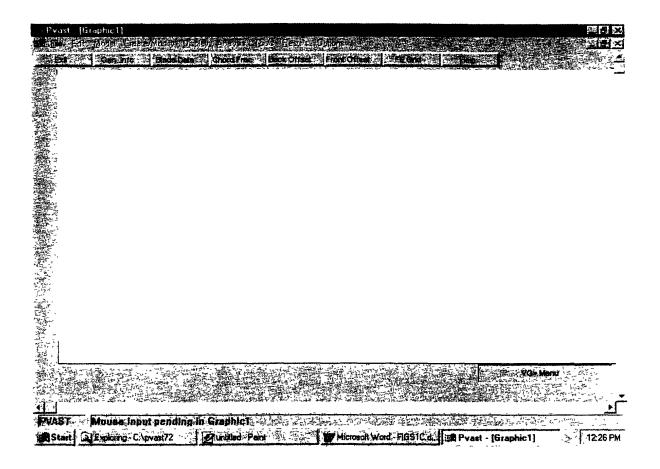


Figure 3.3: FE Grid Proportions Submenu

If it is of interest to view the data, as in the case when the PREFIX.T16 file is the starting point of the modeling, click on

Gen. Info: To view general information about the blade data

Blade Data To view the radii, chord, pitch, skew and rake data

Chord Frac: To view chord fraction data Back Offset: To view back offset data Front Offset: To view front offset data

If the PREFIX.T16 file is not the starting point the above reviews may not be necessary and you should go directly and click **FE Grid**. Figure 3.4 shows the grid proportion data entered for this analysis.

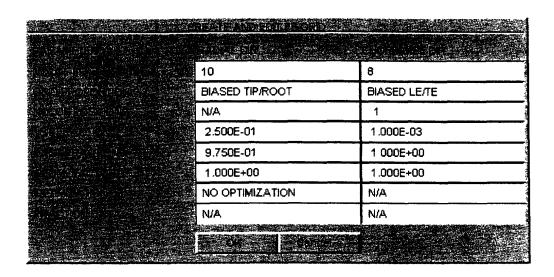


Figure 3.4: Edit Table for FE Grid Proportion

Click **OK** (Figure 3.4), when finished

Click Exit on the FE Grid Proportion submenu (Figure 3.3).

The FE grid proportions are now generated and a message is displayed at the bottom left corner of the PVAST window.

To display the FE grid proportions

Click Display on the main menu

Click Special Plots on the MODEL DISPLAY submenu

Click Blade Grid Proportions on the Special Plots (Model) submenu

Then select Grid Proportions, as shown in Figure 3.5

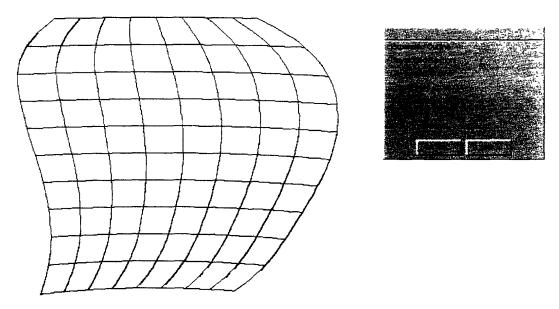


Figure 3.5: FE Grid Proportion for NRC45 Propeller Blade

### 3.2.3 Generate Finite Element Model

Click the Create/Modify on the main menu and select the FE Model option on the CREATE/MODIFY submenu (Figure 3.2).

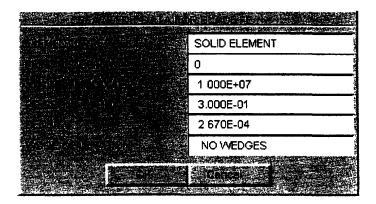


Figure 3.6: Edit Table for Finite Element Model Data

Figure 3.6 shows the edit table for entering the finite element model data. In this example, solid elements have been selected to model the blade, and no wedges are formed at the leading and trailing edges of the blade.

Click **OK** (Figure 3.6), when finished

The FE model is now generated and a message is displayed at the bottom left corner of the PVAST window.

To display the FE model:

Click Display on the main menu

Click Blade FE Model on the MODEL DISPLAY submenu

Then the blade finite element model is displayed as shown in Figure 3.7, using the general purpose plotting capability.

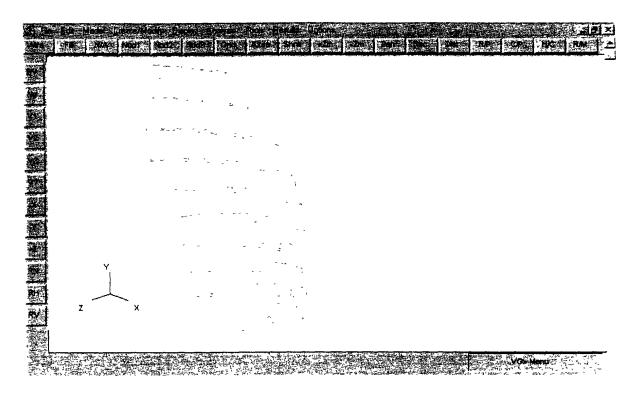


Figure 3.7: Finite Element Model of NRC45 Propeller Blade Using General Plotting Capability

In Figure 3.7, the finite element model has been plotted using the wire mesh plotting option. A fill plot can be made by clicking the Fill button near the top right corner. Similarly, other views can be plotted by clicking on V1, V2, V3, X, Y, Z, etc. For a complete description of the general display capabilities, see the MGDSA manual [2].

#### 3.2.4 Generate Boundary Conditions

With the blade finite element model displayed as shown in Figure 3.7,

Click the Create/Modify on the main menu and select the Boundary Conditions option on the CREATE/MODIFY submenu (Figure 3.2).

At this point the user is required to respond to question: Should default boundary conditions serve as starting point? The default boundary conditions are automatically generated during the finite element model generation. These are usually reasonable boundary conditions, and in most cases they are all the boundary conditions needed for the model. For instance, for the Blade Only model, all the nodes at the base of the blade are fixed automatically.

Click Yes to accept the default boundary conditions as starting point for the boundary condition definition. Then the default boundary conditions will be displayed as shown in Figure 3.8.

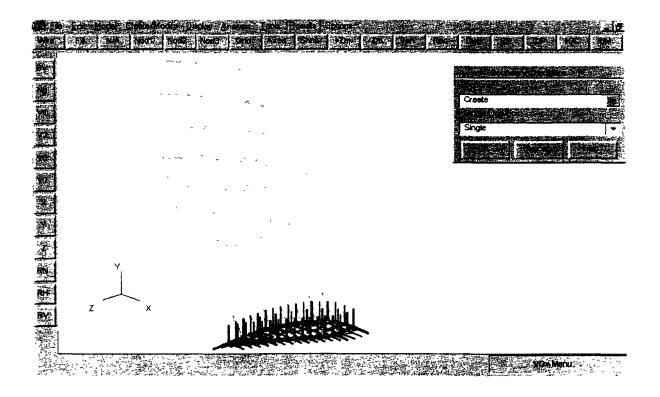


Figure 3.8: Default Boundary Conditions for Blade Only Model

If it is desired to add or edit any of the existing boundary conditions, click on the appropriate boxes on the **Boundary Conditions** submenu, using single, line or box selection of nodes, shown in Figure 3.8.

For the present model, the default boundary conditions shown in Figure 3.8 are the required boundary conditions. So click **Cancel** to end the boundary conditions generation option. The boundary conditions are now defined.

# 3.3 VAST Finite Element Analysis

This step involves the performance of the finite element analysis using the VAST finite element code. This is accomplished by the following processes:

### 3.3.1 Generate VAST Input File

This step involves generating the input file for a VAST finite element analysis.

Click the Create/Modify on the main menu and select the VAST Input File option on the CREATE/MODIFY submenu (Figure 3.2).

Select Natural Frequency analysis as shown in Figure 3.9. Click OK.

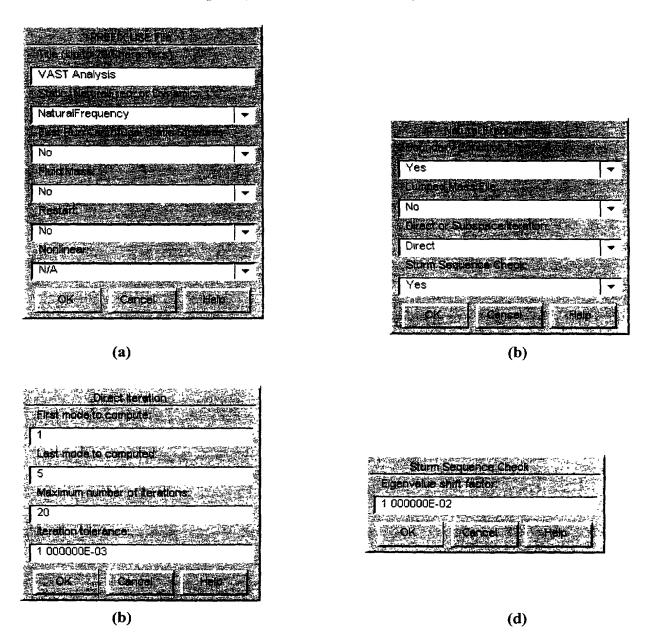


Figure 3.9: Generating VAST Input File for Natural Frequency Analysis

# 3.3.2 Natural Frequency Analysis

Click Analysis on the main menu. Then Click Start VAST Analysis on the Analysis submenu as shown in Figure 3.10. When the analysis has completed, enter a carriage return to return to the PVAST main menu.

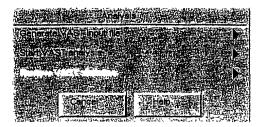


Figure 3.10: Start VAST Analysis

# 3.3.3 Post Processing of Results

To plot the dry mode results using the general plotting capability, the following steps should be followed:

Click Results on the main menu.

Click **Deformation** on the **Results** submenu.

Click Vibration mode.

Enter the desired mode number. Now...

Click **Options** on the main menu.

Click Plotting on the Options submenu.

Click Contour on the Plotting submenu.

Click **Deformation** on the **Contour** submenu

Select Fringe Plotting.

Figures 3.11(a) - (c) show the contours of mode shapes 1-3, respectively.

The capability of plot using the special plotting option is available for dry mode results.

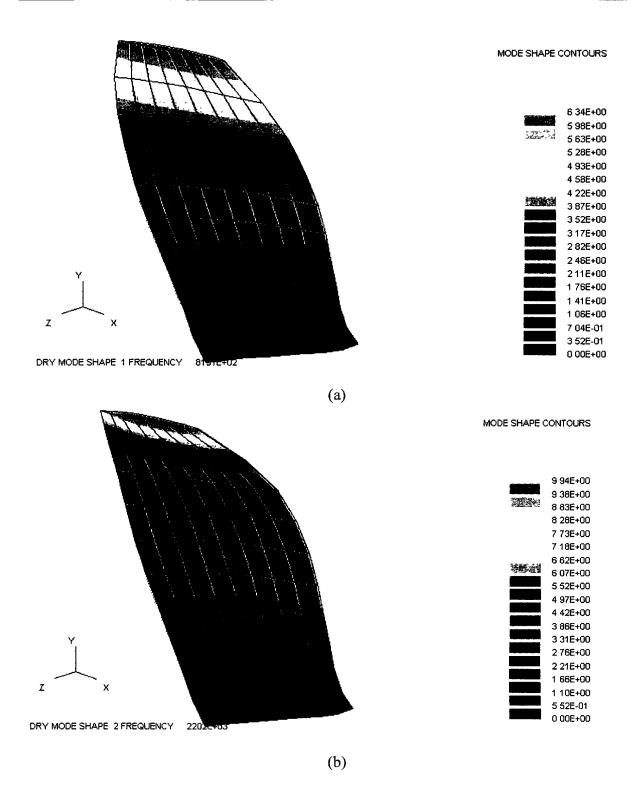
Click Results on the main menu.

Click Special Plots.

Click Blade Section Mode Shape.

Select a radial position.

1 1



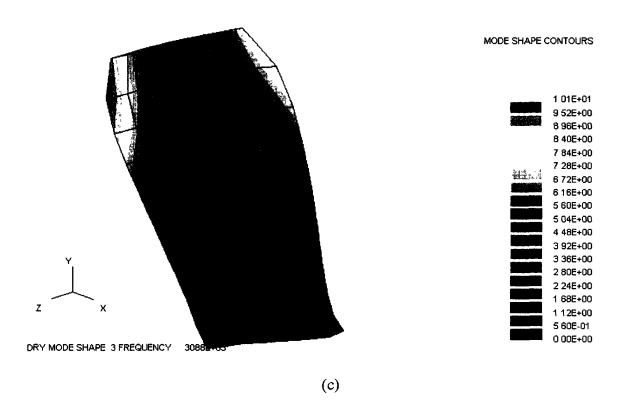
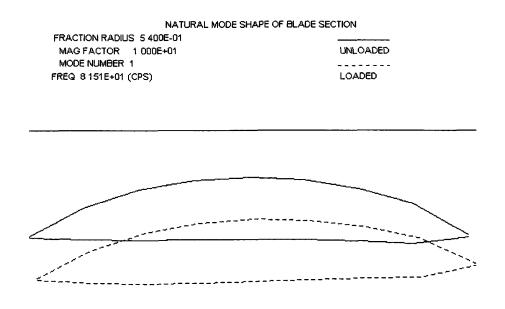


Figure 3.11: Contours of Mode Shapes of NRC45 Propeller in Air: (a) Mode 1; (b) Mode 2; and (c) Mode 3

The resulting plot is shown in Figure 3.12.



# Figure 3.12: Blade Section Mode Shape (Mode 1, at 0.5400 Radial Fraction)

The blade section mode shape for other modes and radial positions can be plotted in a similar manner.

# 3.4 Blade Only Model of P5363 Propeller Blade

In this section, the generation of finite element models of the *Blade Only* model of the skewed propeller blade (P5363 propeller) is presented. It is assumed that the blade geometry has been generated as described in Chapter 2 and that a PREFIX.T16 file of the blade now exists, where PREFIX is the prefix of the filename for identifying the model. The remaining steps for defining the finite element model include:

- (a) selection of model type
- (b) generation of finite element grid proportions;
- (c) generation of the finite element mesh; and
- (d) generation of boundary conditions.

These are presented below.

#### Model Type

The model type selected is **Blade Only** (see Figure 3.1)

#### Finite Element Grid Proportions

Figure 3.13 shows the grid proportion data entered and Figure 3.14 shows the FE grid proportions obtained.

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ntventolalez-ry	N/A	N/A
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Figure 3.13: FE Grid Proportions Data for P5363 Propeller Blade

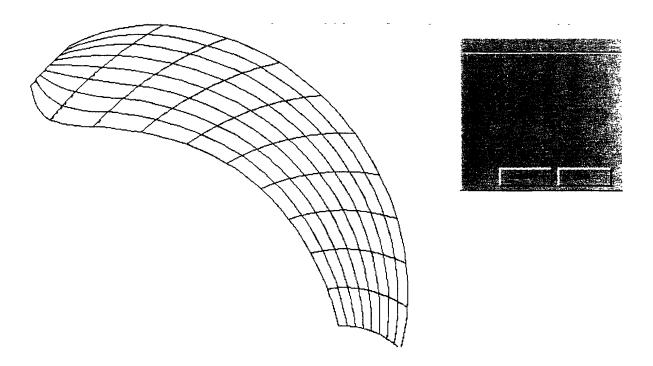


Figure 3.14: FE Grid Proportions for P5363 Propeller Blade

#### FE Mesh Generation

Figure 3.15 shows the finite element data entered. Figure 3.16 shows a wire frame mesh of model, using the general plotting capability. Figure 3.17 shows the default boundary conditions generated automatically by the program.

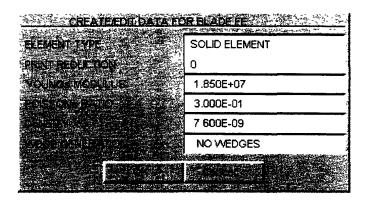


Figure 3.15: Finite Element Mesh Data for P5363 Propeller Blade



Figure 3.16: Finite Element Model of P5363 Propeller Blade

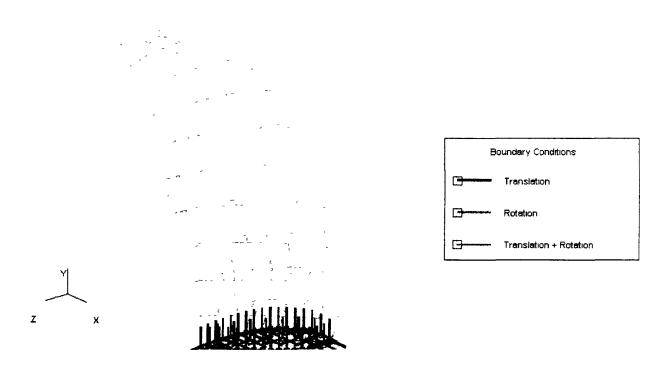


Figure 3.17: Boundary Conditions for P5363 Blade Only Model

# 3.5 Blade Only Model of P4388 Propeller Blade

In this section, the generation of finite element models of the *Blade Only* model of the highly skewed propeller blade (P4388 propeller) is presented. It is assumed that the blade geometry has been generated as described in Chapter 2 and that a PREFIX.T16 file of the blade now exists, where PREFIX is the prefix of the filename for identifying the model. The remaining steps for defining the finite element model include:

- (e) selection of model type
- (f) generation of finite element grid proportions;
- (g) generation of the finite element mesh; and
- (h) generation of boundary conditions.

These are presented below.

Model Type

The model type selected is **Blade Only** (see Figure 3.1)

Finite Element Grid Proportions

Figure 3.18 shows the grid proportion data entered and Figure 3.19 shows the FE grid proportions obtained.

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	1 000E+00	1.000E+00	
	NO OPTIMIZATION	N/A	
	N/A	N/A	

Figure 3.18: FE Grid Proportions Data for P4388 Propeller Blade

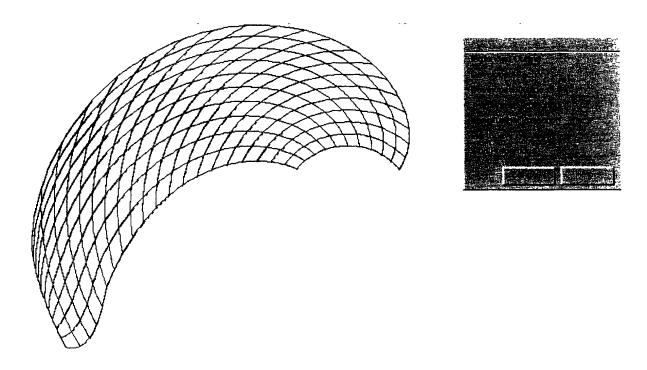


Figure 3.19: FE Grid Proportions for P4388 Propeller Blade

### FE Mesh Generation

Figure 3.20 shows the finite element data entered. Figure 3.21 shows a fill plot of the model, using the general plotting capability. Figure 3.22 shows the default boundary conditions generated automatically by the program.

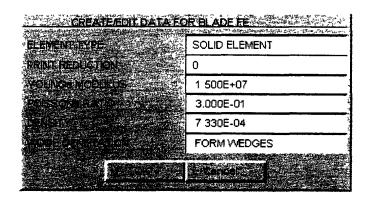


Figure 3.20: Finite Element Mesh Data for P4388 Propeller Blade

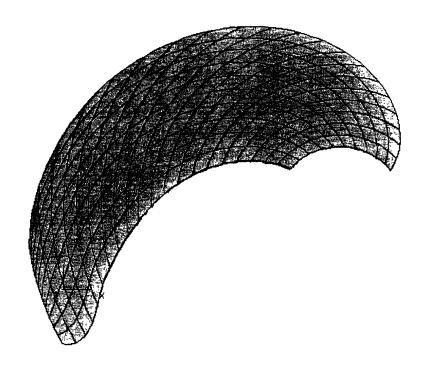


Figure 3.21: Finite Element Model of P4388 Propeller Blade

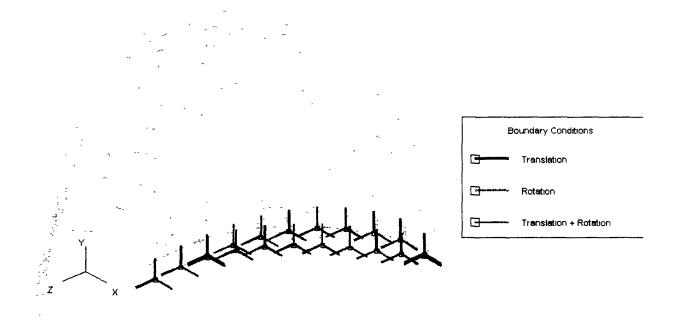


Figure 3.22: Boundary Conditions for P4388 Blade Only Model

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BLADE ONLY MODEL FOR VIBRATION ANALYSIS IN AIR

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#### 4. BLADE ONLY MODEL FOR VIBRATION ANALYSIS IN WATER

#### 4.1 Introduction

In this chapter, we shall demonstrate the how to generate a propeller blade finite element model, including the fluid finite element model, perform a natural frequency analysis of the model that includes the fluid the added mass; and to view the results. The narrow blade (NRC45) propeller blade shall be used for this demonstration. A natural frequency analysis of this blade in air was considered in the Chapter 3. Thus the blade finite element is available at this point, and the user can refer to Chapter 3 for a description of the steps necessary to generate the finite element model. The steps involved in this analysis are:

- (i) To select the model type (Blade Only)
- (ii) To generate the blade geometry
- (iii) To generate the finite element grid proportions
- (iv) To generate the blade finite element model
- (v) To generate the boundary conditions
- (vi) To generate the fluid finite element model
- (vii) To perform the finite element analysis using the VAST program; and
- (viii) To post-process and view the results

With the blade finite element model already defined, only the last three steps are required for the present analysis. These steps are described in sections 4.2 to 4.4.

There are two types of fluid models that can be generated. These include the full 3D-fluid finite element model and the surface panel fluid model. While reasonable surface panel fluid models can be generated for any propeller blade, the full 3-D fluid model option has to be used with care especially for highly skewed propeller blades to avoid the generation of distorted fluid elements. To illustrate the applicability of the PVAST algorithm for various blade configurations, fluid finite element models are also generated for two other blades – one a skewed blade (P5363 propeller), and the other a highly skewed blade (P4388 propeller) – in Section 4.5

#### 4.2 Fluid Finite Element Model Generation

There are two types of fluid finite element models that can be generated. The first is a full 3-D fluid finite element model, and the other is a surface panel model. These are discussed below.

### 4.2.1 Full 3-D Fluid Finite Element Model

### 4.2.1.1 Generating the Fluid FE Model

The 3-D fluid finite element model can be generated according to the following steps:

Click the Create/Modify on the main menu and select the Fluid FE option on the CREATE/MODIFY submenu (Figure 3.2).

Figure 4.1(a) shows the edit table for creating/editing fluid model data. In the table, the type of fluid model is set to **Finite Element Model**, and the original finite element grid of the blade is used as the fluid-structure interface grid. Default values are entered for all the other required data.

Click the Create/Edit box to enter the fluid layer depth data, as shown in Figure 4.1(b). These are provided as fractions of the full blade radius.

Click **OK** when finished.

At this point, a pick menu (Figure 4.2) is presented for selecting the kind of fluid model to plot. Click **Thin Fluid Model** to generate the thin fluid model. This is a model of the full 3-D fluid model, with the fluid layer thickness reduced to zero. This is used to first check the outline of the full 3-D model, before it is actually generated. Once the selection is made, the program generates the thin fluid model and provides the message *Finished Generating Fluid FE Model* at the bottom left corner of the screen.

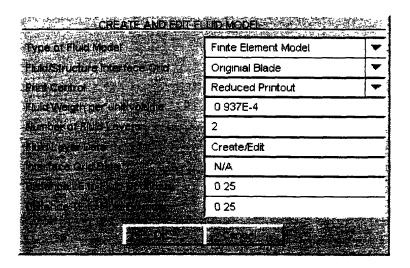


Figure 4.1(a): Blade Geometry Menu

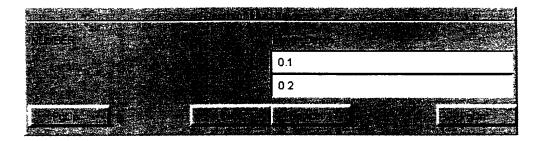


Figure 4.1(b): Entering Fluid Layer Depth Data

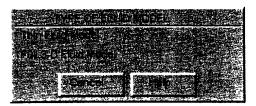


Figure 4.2: Selecting the Kind of Fluid FE Model

After generating the thin fluid model, the model can be viewed as described in Section 4.2.1.2. If the thin blade outline is satisfactory, proceed to generate the full 3-D fluid finite element model by selecting the **Full 3-D Fluid Model** option on Figure 4.2. Again, the program generates the fluid model and provides the message *Finished Generating Fluid FE Model* when finished. The fluid model can now be viewed as described below.

# 4.2.1.2 Displaying the Fluid FE Model

From the PVAST main menu, click **Display**.

### 4.2.1.3 For Special Plotting Option

Click **Special Plots** on the **MODEL DISPLAY** submenu. Click **Fluid Model** on the **SPECIAL PLOTS** submenu

The fluid FE model will then be displayed as shown in Figure 4.3(a).

The thin fluid model (if available) can also be displayed by clicking the options button on this screen (not shown in figure), and selecting the **Thin Model** option. The thin fluid model is shown in Figure 4.3(b).

For general plotting option Click Fluid Model on the MODEL DISPLAY submenu.

The fluid model will be generated using the MGDSA general purpose plotting capabilities, as shown in Figure 4.4.

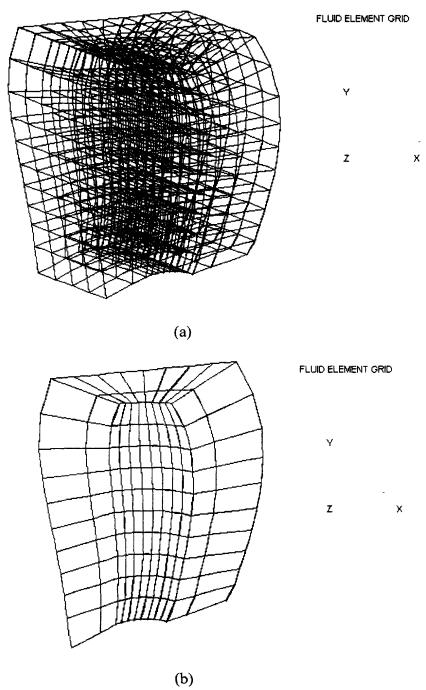


Figure 4.3: Fluid Finite Element Models Using Special Plotting Option: (a) Full 3-D Model, (b) Thin Fluid Model

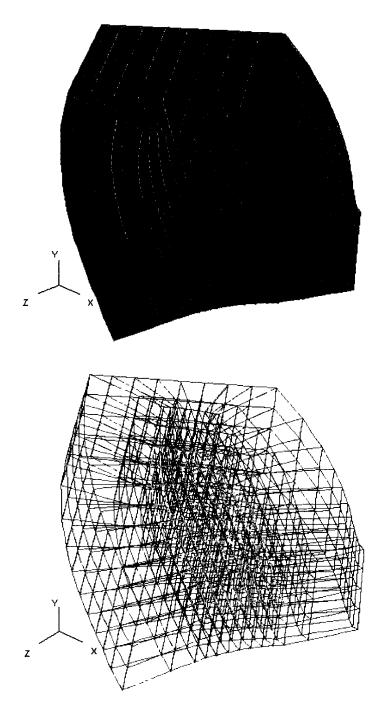


Figure 4.4: Fluid Finite Element Models Using General Plotting Option: (a) Fill Plot, (b) Wire Mesh

# 4.2.2 Surface Panel Fluid Model

# 4.2.2.1 Generating the Surface Panel Fluid Model

The surface panel fluid model can be generated according to the following steps:

Click the Create/Modify on the main menu and select the Fluid FE option on the CREATE/MODIFY submenu (Figure 3.2). Click Type of Fluid Model and select Surface Panel Model.

Figure 4.5 shows the edit table for creating/editing fluid model data. In the table, the type of fluid model is set to **Surface Panel Model**, and free surface effects are ignored in this model. Default values are entered for all the other required data.

Click **OK** when finished.

At this point, the program generates the surface panel fluid model and provides the message *Finished Generating Fluid FE Model* at the bottom left corner of the screen.

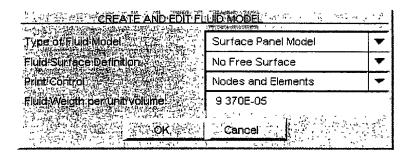


Figure 4.5: Edit Table for Creating/Editing the Surface Panel Fluid Model

#### 4.2.2.2 Displaying the Fluid FE Model

From the PVAST main menu, click **Display**.

Click Fluid Model on the MODEL DISPLAY submenu.

The fluid surface panel model will then be displayed as shown in Figure 4.6.

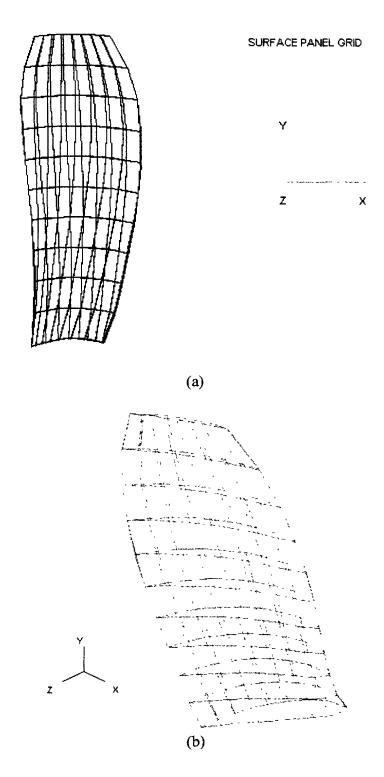


Figure 4.6: Fluid Surface Panel Model of NRC45 Blade: (a) Special Plot Option, (b) General Plot Option

### 4.3 VAST Finite Element Analysis

This step involves the performance of the finite element analysis using the VAST finite element code. This is accomplished by the following processes:

## 4.3.1 Generate VAST Input File

(b)

This step involves generating the input file for a VAST finite element analysis. Click the Create/Modify on the main menu and select the VAST Input File option on the CREATE/MODIFY submenu (Figure 3.2).

Select **Natural Frequency** analysis, and include **Fluid Mass** as shown in Figure 4.7. Click **OK**.

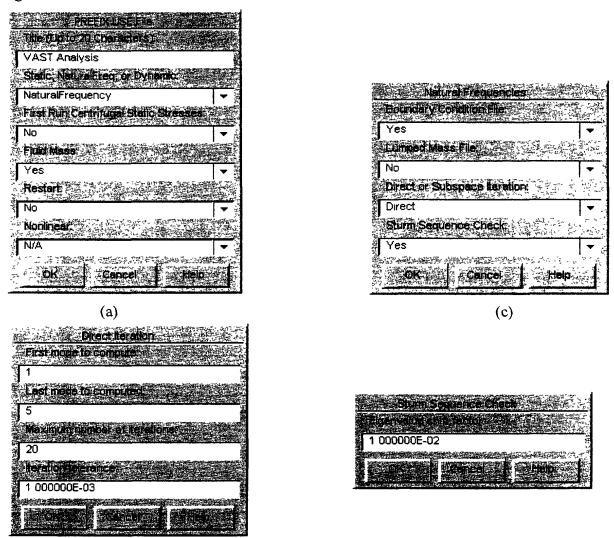


Figure 4.7: Generating VAST Input File for Natural Frequency Analysis in Water

(d)

## 4.3.2 Natural Frequency Analysis

The procedure is exactly the same as described in Section 3.3.2.

Click **Analysis** on the main menu. Than Click **Start VAST Analysis** on the **Analysis** submenu as shown in Figure 4.8.

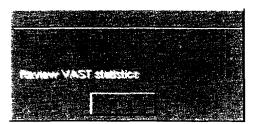


Figure 4.8: Analysis Submenu

The VAST analysis status, shown in Figure 4.9 will now be displayed. Click **Start** to start the VAST natural frequency analysis. The progress of the analysis will be shown in the dialog box, and a message will be provided when the analysis is completed. Click **OK** and return to the PVAST main menu.

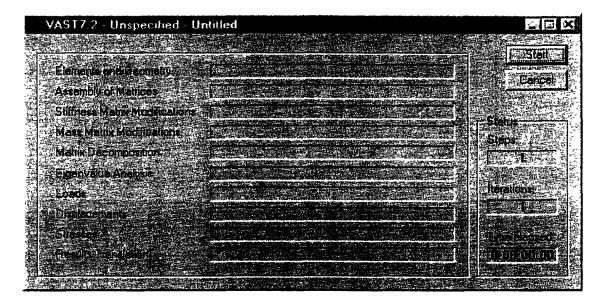


Figure 4.9: VAST Analysis Status Dialog Box

## 4.4 Post-Processing of Results

The plotting of results is similar to that described in Section 3.4. However, in this case mode shapes of *dry* and *wet* modes are available for plotting. The dry modes are

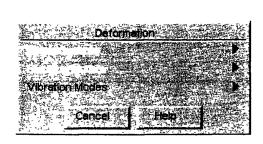
plotted exactly as described in Section 3.4, and since the results are similar to those in obtained in Section 3.4, they are not repeated here. For wet modes, only the general plotting capability is used as the special plotting capability is not available for this case. To plot the wet modes using the general plotting capability, the following steps should be followed:

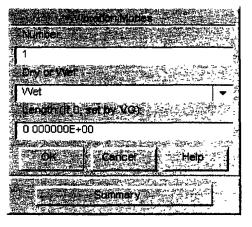
Click Results on the main menu (Figure 3.12 (a) appears).

Click **Deformation** on the **Results** submenu (Figure 4.10(a) appears).

Click Vibration Modes, (Figure 4.10 (b) appears).

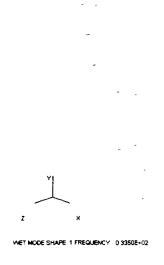
Enter the desired mode number. Select Wet mode and enter a scale factor (Length) as shown. The corresponding mode shape (using wire mesh plotting) is shown in Figure 4.11.



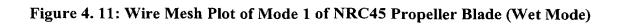


(a) (b)

Figure 4.10: Menus for General Plots (Wet Mode Results)



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## Plotting Contours of Mode Shapes

Plotting wet mode shape contours involves the following steps:

Click Options on the main menu

Click Plotting on the Options submenu

Click Contour on the Plotting submenu

Click **Deformation** on the **Contour** submenu

Select Fringe plotting

Figures 4.12 (a)-(c) show the contours of wet modes 1-3, respectively.

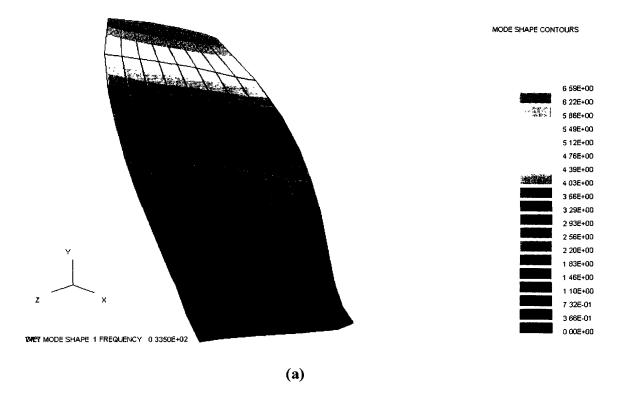


Figure 4.12: Contours of Mode Shapes of NRC45 propeller in Water: (a) Mode 1

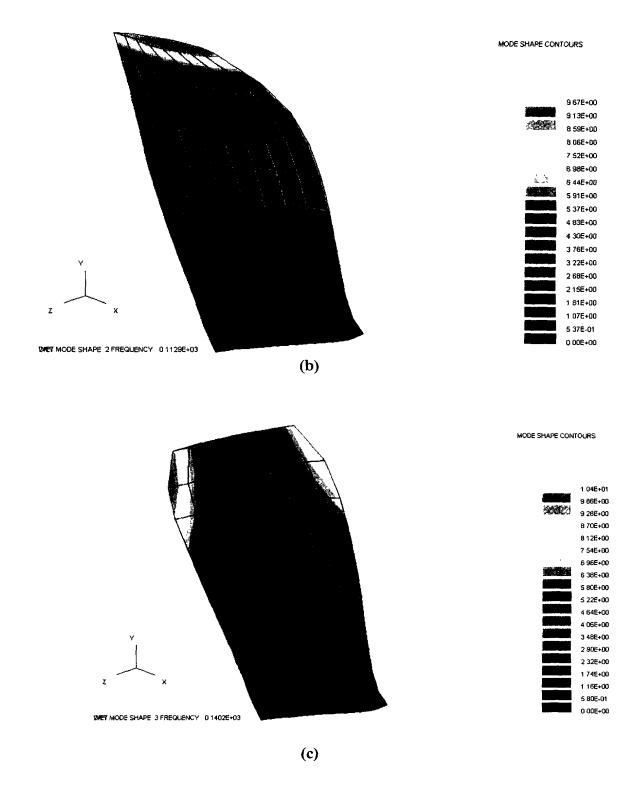


Figure 4.12: Contours of Mode Shapes of NRC45 propeller in Water: (a) Mode 1; (b) Mode 2; and (c) Mode 3

# 4.5 Fluid Models for P5363 Propeller Blade

In this section, the generation of fluid finite element models of the *Blade Only* model of the skewed propeller blade (P5363 propeller) is presented. It is assumed that the blade geometry and the finite element model of the blade have been generated as described in Chapters 2 and 3. Only the fluid finite element model generation step is considered here.

Figure 4.13 shows the data entered for the fluid model generation.

·····································	
Type of Fluid Models	Finite Element Model
Fluid/Structure Interface Grid:	Originial Blade
Print Control	Reduced Printout
Fluid Weight per unit yol/g	0.937E-4
Number of Fluid Layers	2
Fluid Layer Date	Create/Edit
Interface Orid Data	N/A
Distance LEto Fluid Boundary	0.25
Distance TE to Fluid Boundary	0 25
©K. Caricel	

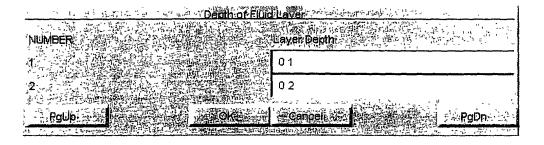


Figure 4.13: Fluid Model Data for P5363 Propeller Blade

Figure 4.14 shows the thin fluid finite element model using the special plotting option. Figure 4.15(a) shows a wire mesh of the 3-D fluid finite element model superimposed on the blade model, and Figure 4.15(b) shows a fill plot of the fluid model.

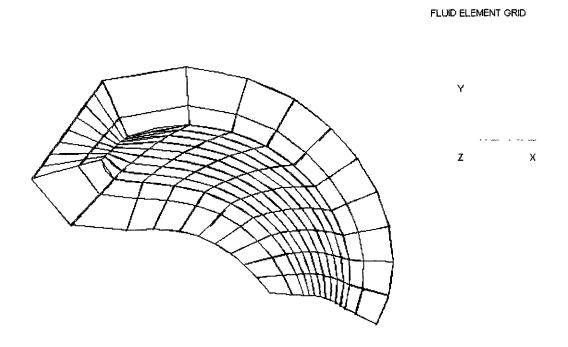


Figure 4.14: Thin Fluid Model of P5363 Propeller Blade

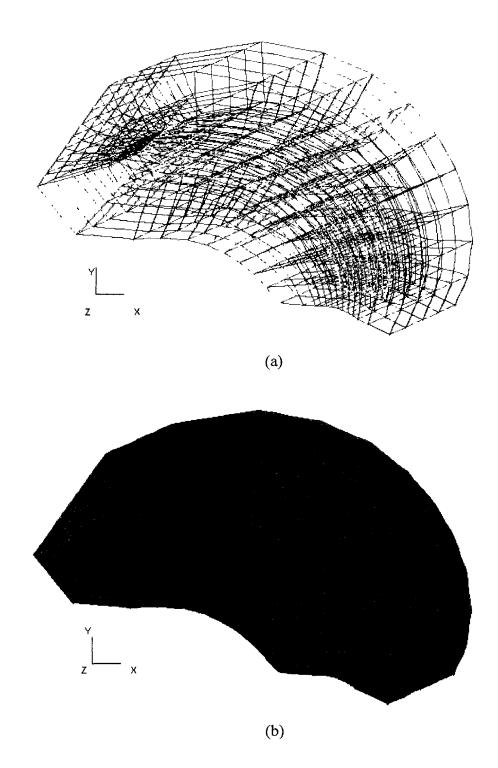


Figure 4.15: Full 3-D Finite Element Meshes of P5363 Propeller Blade; (a) Wire mesh of fluid superimposed on Blade; and (b) Fill Plot of Fluid Model

## 4.6 Fluid Models for P4388 Propeller Blade

In this section, the generation of fluid finite element models of the *Blade Only* model of the highly skewed propeller blade (P4388 propeller) is presented. It is assumed that the blade geometry and the finite element model of the blade have been generated as described in Chapters 2 and 3. Only the fluid finite element model generation step is considered here.

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Finite Element Model

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Finite Element Model

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Figure 4.16 shows the data entered for the fluid model generation.

Figure 4.16: Fluid FE Data for P4388 Propeller

Figure 4.17 shows the thin fluid finite element model using the special plotting option. Figure 4.18(a) shows a wire mesh of the 3-D fluid finite element model superimposed on the blade model, and Figure 4.18(b) shows a fill plot of the fluid model.

Due to the highly skewed nature of this blade, care had to be exercised in generating the fluid model. Some of the measures taken to avoid problems are highlighted below.

- The distance from the blade trailing edge to the fluid boundary (**Distance TE to Fluid Boundary**) should not be too largen otherwise, the fluid elements may cross over each other.
- A fairly fine mesh is used to have better distribution of the element, especially toward the tip. In this example a 20x10 blade FE mesh is used. An earlier model involving a 10x10 grid did not produce well shaped fluid elements near the tip.

Similar corrective measures might be required for other complex shaped propeller blade geometries.

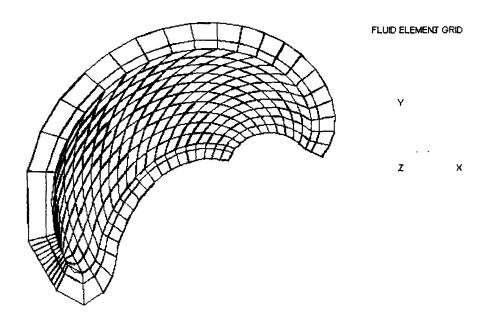


Figure 4.17: Thin Fluid Model of P4388 Propeller Blade

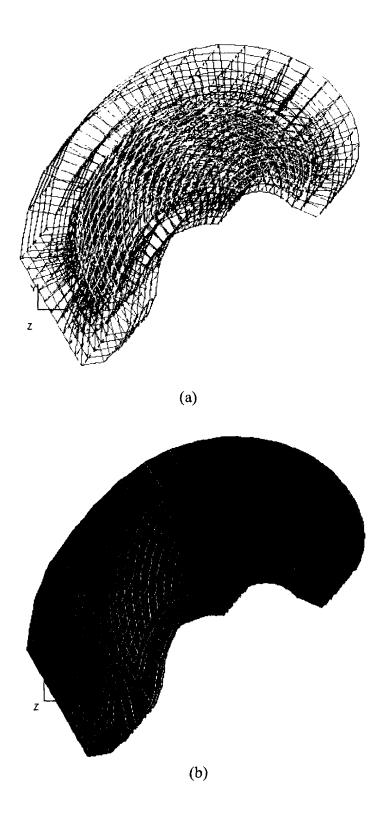


Figure 4.18: Full 3-D Finite Element Meshes of P4388 Propeller Blade; (a) Wire mesh of fluid superimposed on Blade; and (b) Fill Plot of Fluid Model

A surface panel fluid model was also generated for this blade. Figure 4.19 shows the data entered to generate the surface panel model. Figure 4.20 shows the surface panel model using the general plotting option.

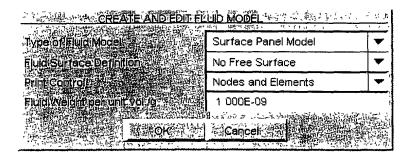


Figure 4.19: Surface Panel Data for P4388 Propeller Blade

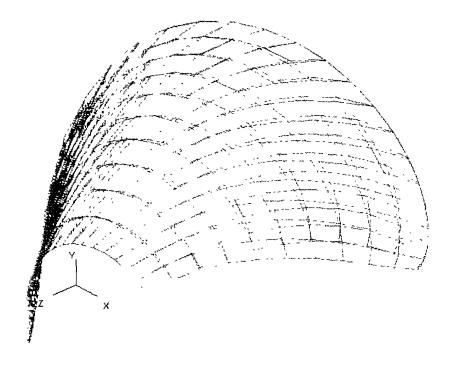


Figure 4.20: Surface Panel Fluid Model for P4388 Propeller Blade

## 5. BLADE ONLY MODEL FOR STRESS ANALYSIS

#### 5.1 Introduction

In this chapter, we shall demonstrate how to generate a propeller blade finite element model, perform a static stress analysis of the model; and to view the results. It is assumed that the blade geometry data has been entered and geometry defined, as described in Chapter 2. Thus, a PREFIX.T16 file is now available in the working directory, where, "PREFIX" is the alphanumeric prefix of the file name. It is also assumed that the hydrodynamic loads are available on the PREFIX.LIN file. The skewed blade (P5363) propeller blade shall be used for this demonstration. With the blade geometry already defined, the remaining steps are:

- (i) To generate the finite element model. This includes the selection of the model type, generation of finite element grid proportions; adjusting peak pressure loads; defining nodal pressures and drag pressures; generation of the finite element mesh; generation of loads on the finite element mesh; and generation of boundary conditions.
- (ii) To perform the finite element analysis using the VAST program; and
- (iii) To post process and view the results

These steps are described in the following sections.

#### 5.2 Finite Element Model Generation

## 5.2.1 Definition of Model Type

Click **Model** on the main menu and ensure that the **Blade Only** model is highlighted, as shown in Figure 3.1.

# 5.2.2 Finite Element Grid Proportions

The finite element grid proportions for the P5363 propeller blade were previously defined in Section 3.5. The same grid proportions are used here and the data entered are presented in Figures 3.18 and 3.19. Refer to Section 3.5.

# 5.2.3 Adjust Peaks of Pressure Loads

The blade pressure load is assumed to be available on a file called P5363.LIN. The contents of the file are shown in Appendix B. The purpose of this step is to adjust the applied load to reduce pressure spikes along the leading and trailing edges from which loading errors could develop. The adjustment is carried out such that the smoothed chordwise pressure distributions produce the same thrust and spindle thrust as the original pressure distribution. The procedure is as follows:

Click the Create/Modify on the main menu and select the Adjust Peaks of Pressure Loads option on the CREATE/MODIFY submenu (Figure 3.2).

The **Adjust Peaks of Pressure Loads** submenu appears as shown in Figure 5.1. The options selected are as shown in the figure.

Click **OK** when finished.

In this demonstration, both the leading edge (LE) and trailing edge (TE) loads are adjusted with no limits, as shown in Figure 5.1.

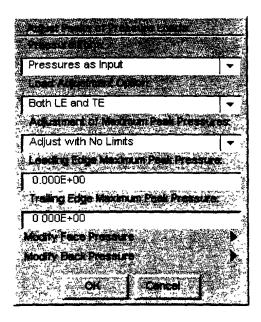


Figure 5.1: Submenu for Adjusting Peaks of Pressure Loads

To display the loads:

Click Display on the main menu

Click Special Plots

Click Adjusted Chordwise Pressure

The pressure loads are displayed as shown in Figures 5.2 to 5.4. Figure 5.2 shows a graph of the pressure load versus fraction chord. This **Load Graph**. Similarly, Figure 5.3 shows an expanded plot showing the pressure superimposed on the expanded outline of the blade.

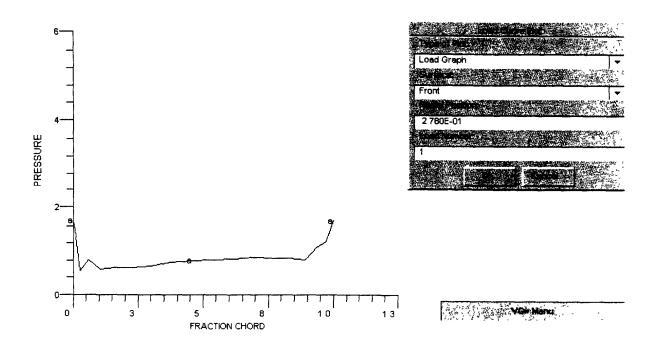


Figure 5.2: Load Graph of Pressure Distribution

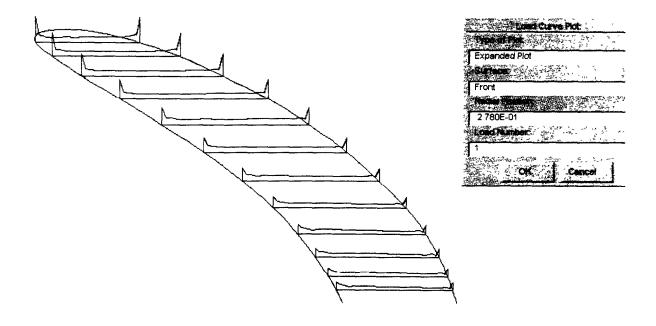


Figure 5.3: Expanded Plot of Pressure Distribution

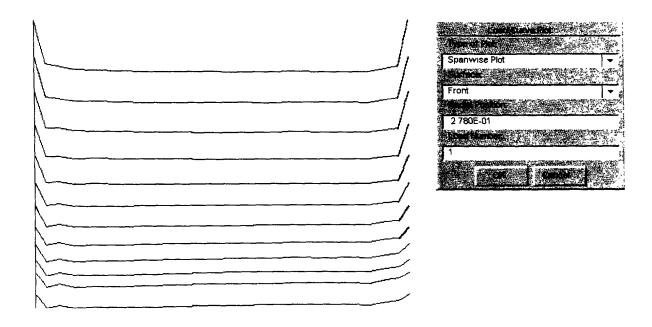


Figure 5.4: Spanwise Plot of Pressure Distribution

## 5.2.4 Nodal Pressures and Drag Forces

This step is performed to transform the propeller blade pressure data into a form that is acceptable by the module for generating the **Loads on FE Model.** If the adjusted pressure (PREFIX.LAD) file is available, it will be used for the computations, otherwise the data on the PREFIX.LIN file will be used. The procedure is as follows:

Click Create/Modify on the main menu. Click Nodal Pressures and Drag Forces

At this point, a pick menu appears for selecting the print option. Select Yes or No and click OK when finished.

A message indicating the transformation has been completed will be displayed when finished.

### 5.2.5 Finite Element Mesh

This step is performed to generate the finite element mesh. The procedure is as follows:

Click Create/Modify on the main menu.

Click **Blade FE Model** on the **Create/Modify** submenu. Figure 5.5 shows the data entered and Figure 5.6 shows a fill plot of the finite element mesh using the general plotting capability.

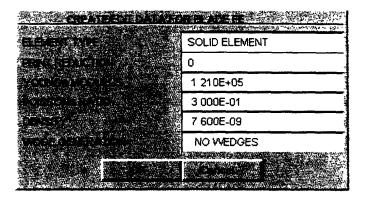


Figure 5.5: FE Model Data for P5363 Propeller Stress Analysis

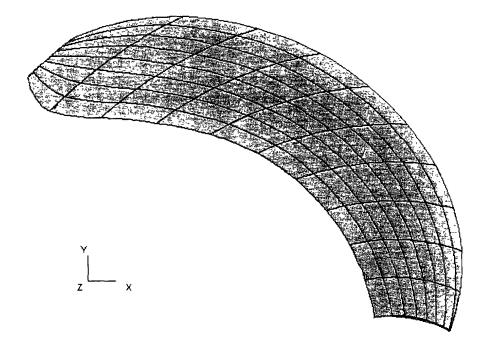


Figure 5.6: FE Mesh of P5363 Propeller Stress Analysis

### 5.2.6 Loads on Finite Element Model

This step involves the generation of loads on the finite element mesh. No additional data is required. The following procedure is followed:

Click Create/Modify on the main menu and then Click Loads on FE Model on the Create/Modify submenu.

The program will generate the loads and provide a message when finished.

## 5.2.7 Boundary Conditions

Click Create/Modify on the main menu and then Click Boundary Conditions on the Create/Modify submenu.

The default boundary conditions, as shown in Figure 3.22, are used for the analysis.

## 5.2.8 VAST Input File Generation

This step involves generating the input file for a VAST finite element analysis.

Click Create/Modify on the main menu and select the VAST Input File on the Create/Modify submenu. (Figure 5.7).

Select **Static** analysis, as shown in Figure 5.7. Click **OK**.

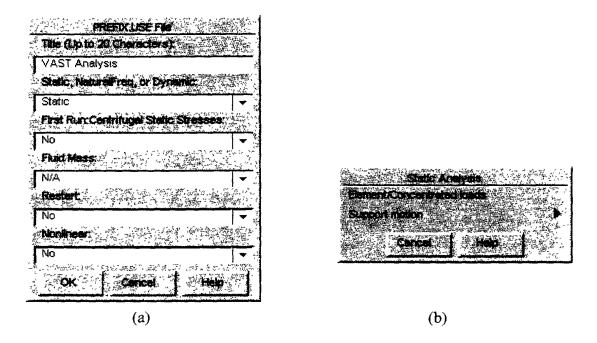


Figure 5.7: Generating VAST Input File for Stress Analysis

## 5.3 Static Stress Analysis

The steps for performing the VAST stress analysis are the same as those described in Section 3.3.

Click Analysis on the main menu. Then click Start VAST Analysis on the Analysis submenu as shown in Figure 5.8.



Figure 5.8: Analysis Submenu

The VAST analysis status, shown in Figure 5.9, will now be displayed. Click **Start** to start the VAST stress analysis. The progress of the analysis will be shown in the dialog box, and a message will be provided to signify the end of the analysis. Click **OK** to return to the PVAST main menu.

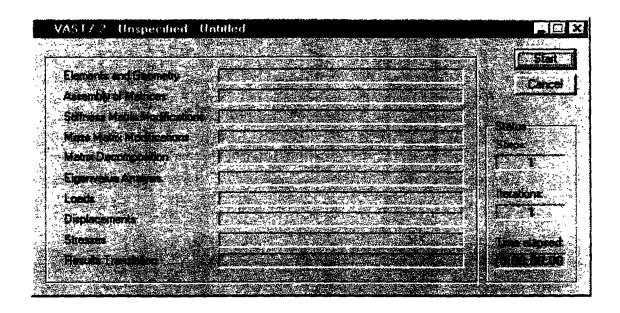


Figure 5.9: VAST Analysis Status Dialog Box

## 5.4 Post-Processing of Results

## 5.4.1 Special Plots

Click **Results** on the main menu (Figure 5.10 (a) appears). Click **Special Plots** on the **Results** submenu (Figure 5.10 (b) appears).

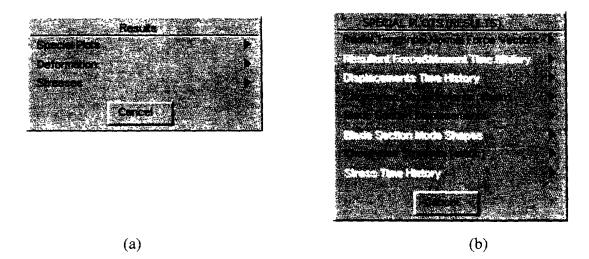


Figure 5.10: Menus for Selecting Special Plots Stress (Results)

To plot the radial, tangential and normal force vectors, click **Radial**, **Tangential**, **Normal Force Vectors**. Figure 5.11 shows the radial force vectors at the front.

PRESSURE LOADING (STATIC ANALYSIS) RADIAL NODAL FORCE (FRONT FACE)

Figure 5.11: Radial Force Vectors at Front Face of P5363 Propeller Blade

To plot other components, click **Options** at the top right hand corner and toggle through the options under **Component** and **Face** to select the component and the face, as shown in Figure 5.12. Following this procedure, other components have been plotted. Figures 5.13 and 5.14 show the front face tangential and normal force vectors, respectively.

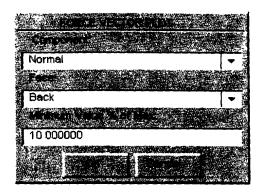


Figure 5.12: Selecting Force Components for P5363 Propeller

PRESSURE LOADING (STATIC ANALYSIS) TANGENTIAL NODAL FORCE (FRONT FACE)

Figure 5.13: Tangential Force Vectors at Front Face of P5363 Propeller Blade

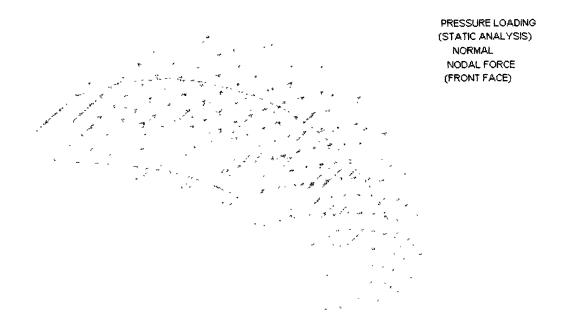


Figure 5.14: Normal Force Vectors at Front Face of P5363 Propeller Blade

To plot the chordwise displacements, click **Chordwise Displacements (Static)**. A list of the radial fractions is then presented. Select the radial function at which displacement plotting is desired by clicking on the radial fractions, and click **OK**. Figure 5.15 shows plot at radial fraction 0.9155 displacement components and radial. Other positions can be plotted by clicking **Options** at the top right hand corner and using the data boxes shown in Figure 5.16.

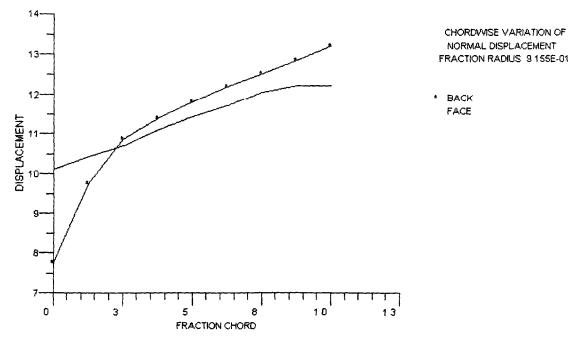


Figure 5.15: Chordwise variation of Normal Displacement of P5363 Propeller

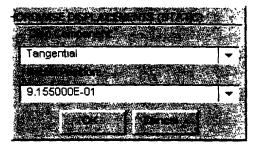


Figure 5.16: Selecting Components and Radial Positions for Plotting Chordwise Displacements in P5363 Blade

To plot the blade section displacements, click **Blade Section Displacements**. A list of the radial positions will now be displayed. Click on the appropriate radial position to select the radial position. Figure 5.17 shows the blade section displacement at radial position 0.836. Other positions can be selected by clicking options on the top right hand corner.

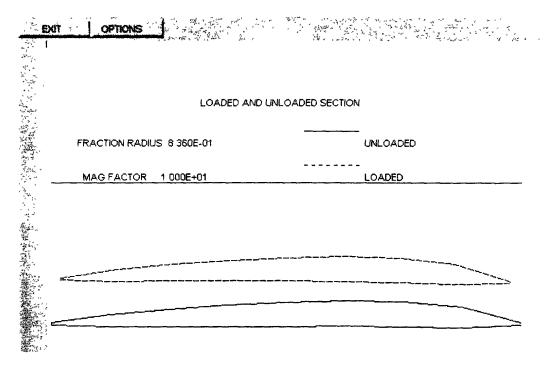


Figure 5.17: : Blade Section Displacement at 0.836 Radial Fraction in P5363 Propeller Blade

To plot the chordwise variation of stresses, click **Chordwise Stresses (Static)** on the **Special Plots (Results)** submenu. Again, the radial positions are displayed. Click the desired radial position. Figure 5.18 shows the chordwise variation of the primary principal stresses at radial function of 0.518. Other stress components and radial positions can be selected as described above.

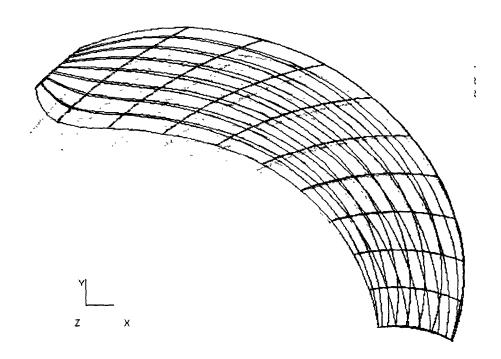


Figure 5.21: Deformed Shape Superposed with the Undeformed Shape

# Plotting Contours of Mode Shapes

Plotting mode shape contours involves the following steps:

Click Options on the main menu

Click Plotting on the Options submenu

Click Contour on the Plotting submenu

Click **Deformation** on the **Contour** submenu

Select Fringe plotting

Figure 3.22 shows the contours of deformed shape.

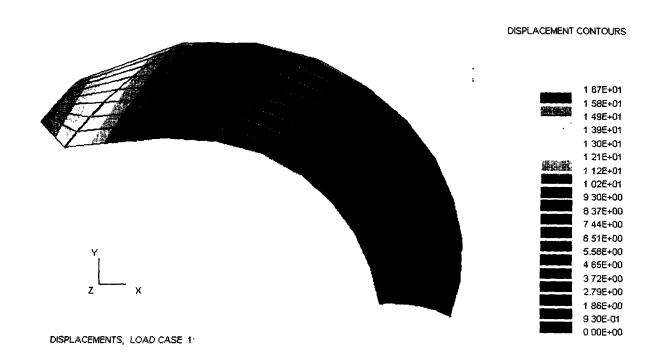


Figure 5.22: Deformation Contours of P5363 Propeller Blade

## Plotting Stresses:

Click Results on the main menu.

Click Stresses on the Results submenu (Figure 5.19 (a)).

Accept Transfer to Database (for first time).

Click Static.

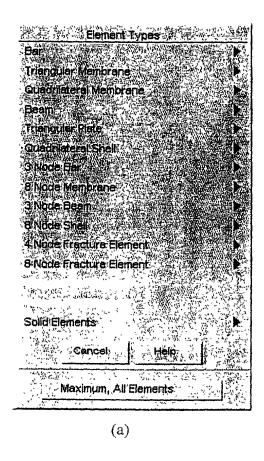
Enter load case (equal to 1 in this case)

Click **Solid Elements** on the **Element Types** submenu (Figure 5.23 (a)) and select 20-node brick (Figure 5.23 (b).

Select von Mises on **the 20-node Solid** element stress component submenu (Figure 5.24).

Click Plot Stresses, to plot the element stresses, as shown in Figure 5.25.

Following the procedure outlined above for plotting displacement contours, the von Mises stress contours can be plotted as shown in Figure 5.2 (b).



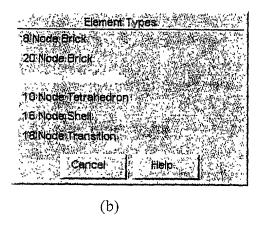


Figure 5.23: Element Types Submenu

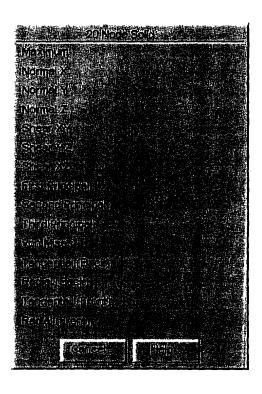


Figure 5.24: Stress Components for 20-node Solid

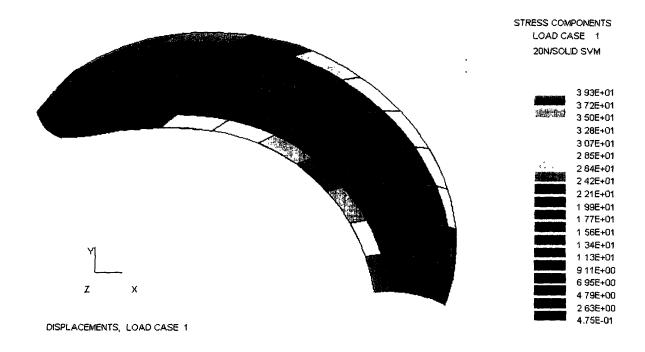


Figure 5.25: von Mises Stresses in P5363 Propeller Blade

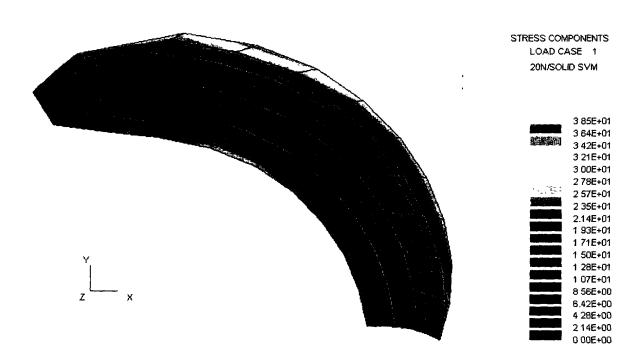


Figure 5.26: von Mises Stress Contours in P5363 Propeller Blade

#### 6. BLADE-FILLET-HUB MODEL

#### 6.1 Introduction

In this chapter we shall demonstrate how to generate blade-fillet-hub models. It is assumed that the blade geometry has been defined in Chapter 2. Thus a PREFIX.DAT file is available in the working directory, where PREFIX is the alphanumeric prefix of the file name. The P5363, P4388 and NRC45 propeller blades shall be used for this demonstration. Finite element grid proportions of these blades have been generated in Chapter 3. With the grid proportions already defined, the remaining steps are to:

- (a) Generate the blade model;
- (ii) Generate the blade finite element mesh; and
- (iii) Generate the sub-structural models of the blade, fillet and hub.

It should be noted that the model type bust be set to **Blade Fillet Hub** or **Multi Blade Hub**. The **Multi-Blade Hub** model is selected for this demonstration.

## 6.2 Blade-Fillet-Hub Model of P5363 Propeller Blade

#### 6.2.1 Root Model Generation

Click Create/Modify on the main menu.

Click Root Model on Create/Modify submenu.

Figure 6.1 appears for defining the root data.



Figure 6.1: Root Model Data Generation Submenu

Figure 6.2 shows the data entered under Gen Info.

Figure 6.3(a) shows the data entered under **Palm/Hub Data**. Selection of the option **Create** coordinate points results in the display shown in Figure 6.3(b).

Figure 6.4 shows the data entered under Fillet Data

For the type of model selected, no data under FBI (fillet-blade-interface) points and FHI (fillet-hub-interface) points are required.

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**BLADE-FILLET-HUB MODEL** 

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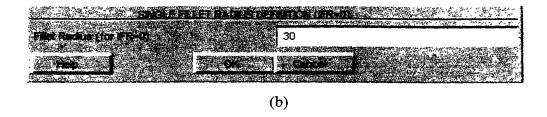


Figure 6.5: Correcting an Error in the P5363 Root Data (a) Error Message; (b) Revised Fillet Radius

It should be noted that the PVAST, root model generation algorithms assume that the data supplied is reasonable, and provide guidance on how to resolve some cases of incorrect or unreasonable data. As PVAST is designed as an analysis tool, it might not be possible to detect all kinds of inappropriate data during design iterations which might lead to the generation of badly shaped elements in the fillet and hub finite element models, or even program crashes. To avoid these situations, reasonable root data obtained by measurements from actual blades may be required.

Plotting Blade-to-Root Intersection

Click Display on the main menu.

Click Special Plots (Model) on the Model Display submenu.

Click Blade-to-Root Intersection on the Special Plots Model option.

Figure 6.6 shows the blade-to-root intersection. This figure aids in determining if the blade is well positioned on the hub. In the present example, the blade is seen to be positioned properly on the hub.

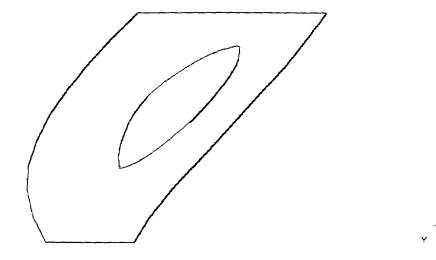


Figure 6.6: P5363 Blade-to-Root Intersection Plot

Plotting Fillet and Hub Models

Click Display on the main menu.

Click Root FE Model on the Model Display submenu.

Click Fillet on the Root Model submenu to plot the fillet or hub model.

Figures 6.7 (a) and (b) show the wire frame and fill plot models of the fillet finite element model.

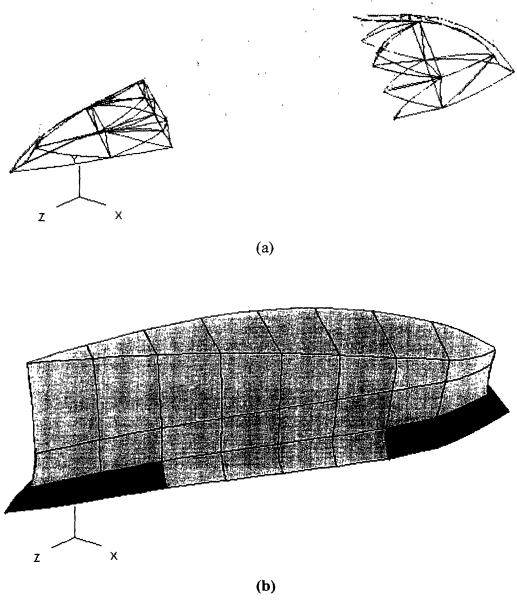


Figure 6.7: P5363 Fillet Finite Element Models, (a) Wire Frame, (b) Fill Plot

1 1

Figure 6.8 shows a fill plot of the hub model.

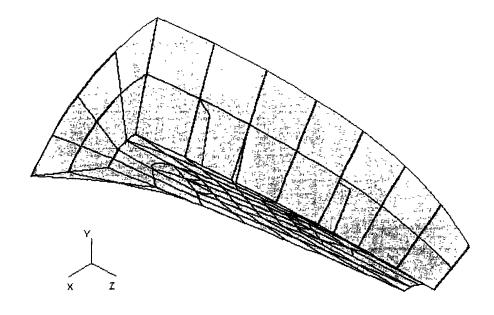


Figure 6.8: P5363 Hub Finite Element Model

## 6.2.2 Blade Mode Generation

This step is required to generate the finite element model of the blade. The procedure is similar to that described in Chapters 3 and 5. The data entered for the blade finite element generation is shown in Figure 6.9. The blade's finite element mesh is shown in Figure 6.10, appended to the fillet and hub model models.

CREATEEDT DATA FO	R BLADE FE
ELEMENT TYPE	SOLID ELEMENT
PRINT REDUCTION	0
YOUNGS MODULUS	1 210E+05
POISSONS RATIO	3 000E-01
DENSITY	7 600E-09
WDGE GENERATION	NO WEDGES
OK L	Cancel

Figure 6.9: Blade FE Data for P5363 Blade-Fillet-Hub Model

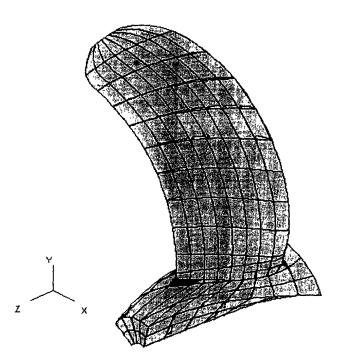


Figure 6.10: P5363 Blade FE Model Appended to Fillet and Hub Models

### 6.2.3 Substructured Blade-Root-FE Model

Click Create/Modify on the main menu.

Click **Substructured Blade-Root FE** on the **Create/Modify** submenu. The substructured data entry submenu now appears as shown in Figure 6.11.

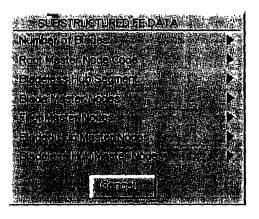


Figure 6.11: Defining Substructured FE Data

Click **Number to Blades** to define the number of blades. For this demonstration, the number of blades is 5.

Click Root Master node Code to define how the root master nodes are defined. The Interface and Side Nodes option is selected.

Click **Bladeless Hub Segment** to specify if a bladeless hub segment is to be used. Select **No**.

Click Blade Master nodes to define master nodes for each of the five blades. Select **No Additional Nodes** for each of the five blades. This is the default option in which the blade master nodes are automatically defined by PVAST.

Click **Fillet Master Nodes** to define master nodes for the five fillets. Again the default option (No Additional Nodes) is selected.

Click **Bladed Hub Master Nodes** to define master nodes for the five hubs. Again the default nodes are used (**No Additional Nodes**).

Since no bladeless hub was selected, it is not necessary to define data for the **Bladeless Hub Master Nodes.** 

Note that the other options of master node generation (i.e. Create Additional Nodes and Use Previous Additional Nodes are not functional in this current version of PVAST.

Click Cancel to exit the substructure data generation. The program now generates the substructured model of the blade-fillet and hub. Figure 6.12 shows the five bladed substructured model.

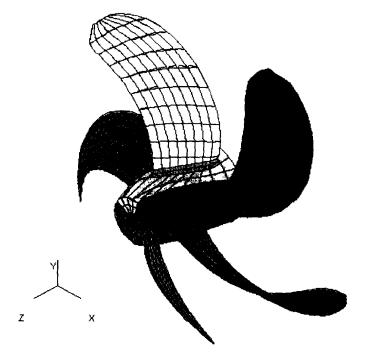


Figure 6.12: Five-Bladed Substructural Model of P5363 Propeller Blade

#### 7. BLADE-FILLET-PALM MODEL

#### 7.1 Introduction

This chapter illustrates how to develop a blade-fillet-palm model. Another DREA propeller blade designated as TRUMP is used for the demonstration because some reasonable palm root model data exists for the blade. The starting point is the PREFIX.DAT file containing the blade geometric data. The steps for generating the blade-fillet-palm model involve:

- Selection of blade geometry;
- Generation of blade geometry
- Definition of FE grid proportions
- Generation of the root model;
- Generation of the blade finite element model; and
- Generation of substructured model.

However, emphasis is placed on the last three steps, as other steps have been described in detail in previous sections.

## 7.2 Generation of the Blade-Fillet-Palm Model

## 7.2.1 Selection of Model Type

Click model on the main menu

Select Blade Fillet Palm (Bolts as Rods) or Blade Fillet Palm (Superelements) on the main PVAST Model submenu.

In this demonstration the Blade Fillet Palm (Superelements) option is selected as shown in Figure 7.1. For this type of model, the bolt holes are treated as bolt hole superelements. For the Blade Fillet Palm (Bolt as Rods) model, the bolts are treated as rods. It should, however, be noted that the options to generate the bolts and bolt hole superelements have not been available in this version of PVAST.

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## **BLADE-FILLET-PALM MODEL**

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Type of root geom	PALM GEOM	e dit i saar	No. LE overhang elem	0
Fillet rad parameter	1		No. TE overhang elem	0
Continuous function	NO	▼	Young's modulus	1 210E+05
No. of chord points	3	**************************************	Poisson's ratio	3 000E-01
Print reduction	NO	-	Density	7 610E-09
No. of elems at edge	2 ELEMENTS		Rad, frac increament	1 000E-02
Root model	PALM MODEL		Angle increament	1 000E+00
	•		Iteration tolerance	1 000E-03
Help		<b>*</b> ;	Cancel	•

Figure 7.4 (a):

Chord #	Chord Fraction	Fillet Radius (Face)	Fillet Radius (Back)
	1 000E-01	3 000E+01	3 000E+01
2	5 000E-01	5 000E+01	5 000E+01
	9 000E-01	3 000E+01	0 000E+01
Help	OK	Cancel	•

Figure 7.4 (b)

PALM GEOMETRY DATA DEFINITION								
Spherical Palm Radius	0 000E+00							
Palm Base Height	5 000E+02							
Palm Coordinate Offset	0 000E+00							
Palm Diameter	9 500E+02							
Coordinate Points	CREATE							
Help OK	Cancel							

Figure 7.4 (c):

eccilia.	X (Giold)	v Gradi	7 ( again an an an an an an an
	3 520E+02	5 800E+02	-4 300E+02
	1 540E+02	5 800E+02	-5 280E+02
	-1.540E+02	5 800E+02	-5 280E+02
	-3 520E+02	5 800E+02	-4 300E+02
	5 280E+02	5 800E+02	-1 540E+02
	1 760E+02	7 620E+02	-1 760E+02
	-1 760E+02	7 620E+02	-1 760E+02
	-5 280E+02	5 800E+02	-1 540E+02
	5 280E+02	5 800E+02	1 540E+02
	1 760E+02	7.620E+02	1 760E+02
	-1 760E+02	7 620E+02	1 760E+02
	-5 280E+02	5 800E+02	1 540E+02
	3 520E+02	5 800E+02	4 300E+02
	1 540E+02	5 800E+02	5 280E+02
	-1 540E+02	5 800E+02	5 280E+02
	-3 520E+02	5 800E+02	4 300E+02
Help 1	N. OK.	Cencel	

Figure 7.4 (d):

Figure 7.5 shows the blade-to-root intersection which is plotted through Display/Special Plots (Model); Blade-to-Root Intersection.

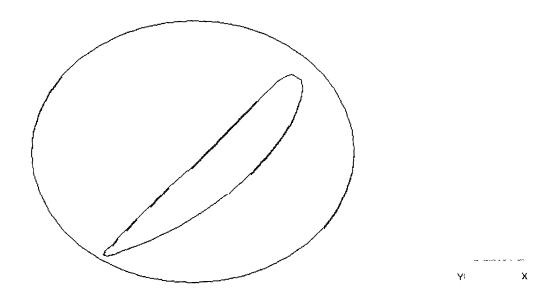


Figure 7.5: Blade-to-Root Intersection of TRUMP Propeller

Figure 7.6 shows the fillet model using the general purpose wire frame and fill plot options.

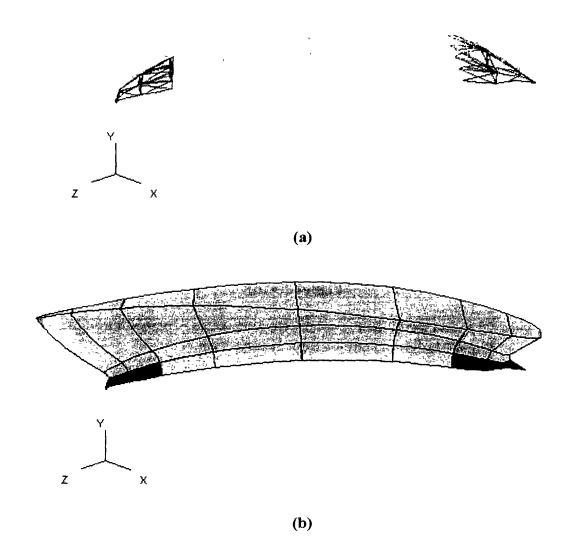


Figure 7.6: Finite Element Model of Fillet of TRUMP Propeller, (a) Wire Frame Plot and (b) Fill Plot

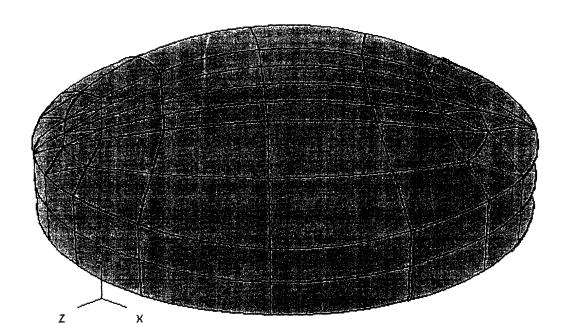


Figure 7.7 shows the palm model using the general purpose fill plot options.

Figure 7.7: Finite Element Model of Palm of TRUMP Propeller

#### 7.2.5 Blade Model Generation

Figure 7.8 shows the submenu for generating the blade finite element model, and Figure 7.9 shows the finite element mesh generation using the general purpose plotting option.

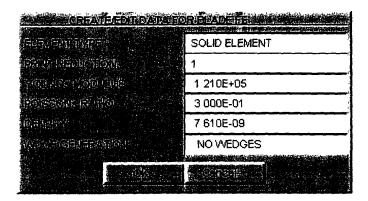


Figure 7.8: Submenu for Generating Blade Finite Element Model

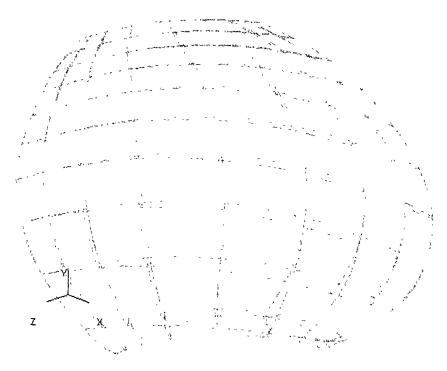


Figure 7.9: Blade FE Model of TRUMP Propeller

## 7.2.6 Generation of Substructured Model

To generate the substructured model click **Create/Modify** and then **Substructured Blade Root FE** and enter the required data. in the present examples, no additional data was entered and the default values have been used throughout. The model generated is displayed in Figure 7.10.

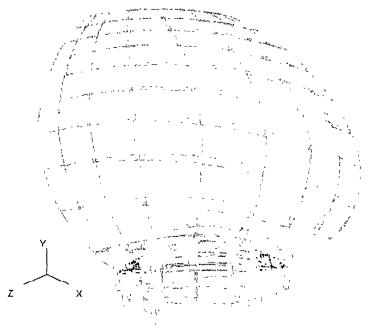


Figure 7.10

#### 8. TWO-DIMENSIONAL HUB MODEL WITH KEYWAY

#### 8.1 Introduction

This chapter demonstrates how to generate a keyway model. The TRUMP propeller blade is used for the demonstration. The blade geometry, finite element and root models have been presented in Chapters 2 and 7. The steps involved include:

- Generation of the keyway model,
- Performance of the analysis, and
- Post processing of results.

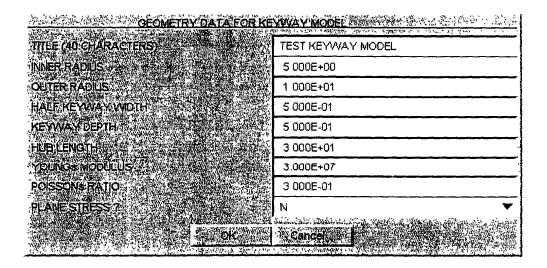


Figure 8.1: Keyway Model Data

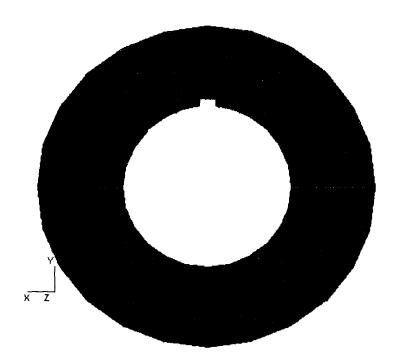


Figure 8.2: Keyway Finite Element Model

#### 8.2 Finite Element Model Generation

Figure 8.1 shows the data entered for generation of the keyway model for this blade, and Figure 8.2 shows the keyway finite element model generated. Figure 8.3 shows the keyway load data.. Figure 8.4 shows the skew coordinates.

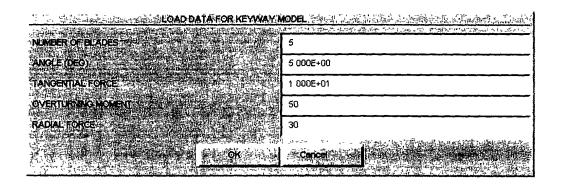


Figure 8.3: Keyway Load Data

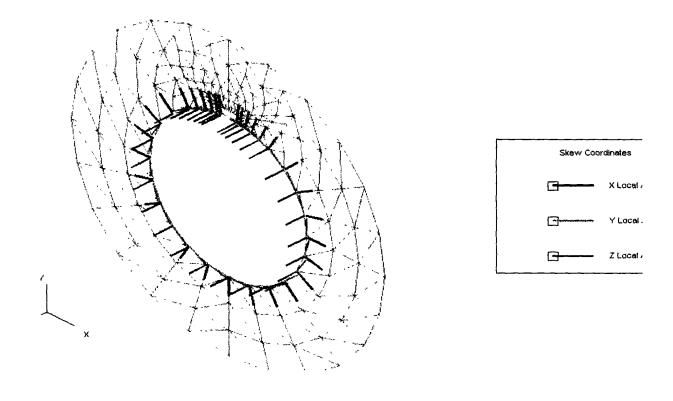


Figure 8.4: Skew Coordinates

## 8.3 Post-Processing Results

Figure 8.5 shows contours of the displaced shape.

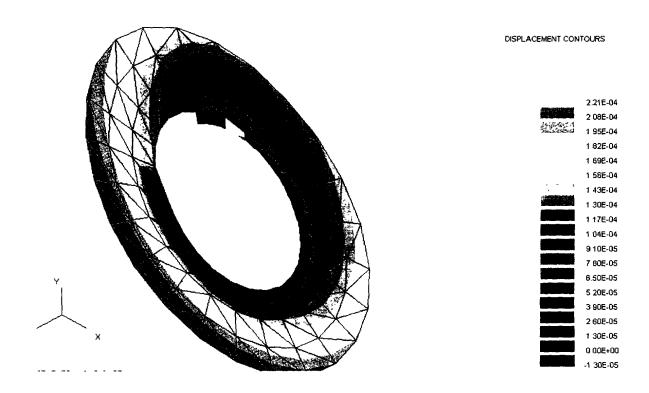


Figure 8.5: Contours of Displaced Shape

#### 9. BLADE AIR CHANNEL STRESS ANALYSIS

#### 9.1 Introduction

This chapter demonstrates how to generate an air channel model from a blade model and to perform a detailed stress analysis of the air channel model, using a top-down approach. The method adopted is that the blade be first modeled and analyzed, ignoring the effects of the air channel and then a detailed model of a portion of the blade containing the air channel is then developed. Thus, to generate this model, it is required that a Blade Only finite element stress analysis be performed first. The P5363 propeller blade will be used for this demonstration. A stress analysis of this blade was performed in Chapter 5, and the results will be used in the development of the air channel model. With the stress analysis of the blade already completed the remaining steps are:

- To generate the air-channel finite element model;
- To perform a stress analysis of the model; and
- To post-process the results.

These steps are described in the following sections.

#### 9.2 Generation of Finite Element Model of Air Channel

#### 9.2.1 Select Model Type

Click **Model** on the main menu and ensure click on the **Air Channel** model, as shown in Figure 9.1.

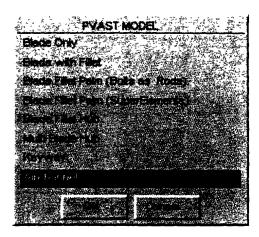


Figure 9.1: Selection of Air Channel Model

#### 9.3 Generate Air Channel Geometric and FE Data

Click the Create/Modify on the main menu and select the Generate Air ('hannel option on the CREATE/MODIFY submenu as shown in Figure 9.2, to generate the air channel data..

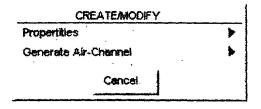


Figure 9.2: Air Channel Create/Modify Submenu

Figure 9.3 shows the air channel data generated. Click **OK** in Figure 9.3(a), when finished.

AIR-CHANNEL DATA							
DEPTH OF AIR-CHANNEL	200						
LENGTH OF AIR-CHANNEL	100						
DIMENSION D1	20						
DIMENSION DEG	0						
DIMENSION A1	70						
DIMENSION B1	15						
DIMENSION C1	35						
DIMENSION E1	10						
NO. OF ELEMS ALONG BLADE EDGE	5						
PRINTING RESULTS	ALL NODES						
NSTEPS FOR AIR-CHANNEL PRESSURE	1						
AIR-CHANNEL PRESSURE DATA	CREATE						
ок	Cancel						

(a)

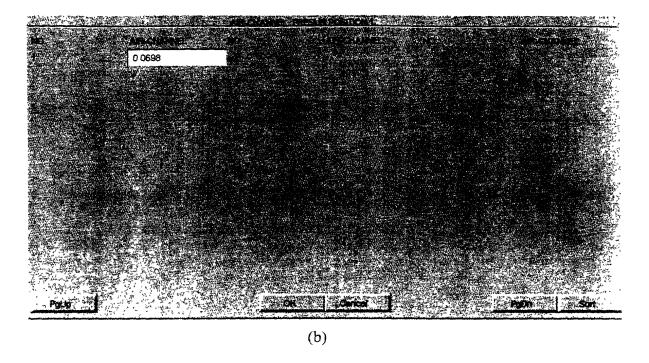


Figure 9.3: Air Channel Data (a) Geometry and FE Data; (b) Air Pressure Data

At this time, an outline of the blade is drawn on the screen (see Figure 9.4) to enable the selection of the point along the leading edge where the air channel model is to be located. The desired location is at a radial fraction of about 0.7. When a point on the leading edge is selected, the program computes and displays its radial position as shown in Figure 9.4. If the point is far away from radial position 0.7, then click on **Not Close Enough** to pick another point. If the point is close enough to the desired (as in this case, because the point select had a radial fraction of 0.6987), click on **This is Close Enough** on the menu at the upper right hand side of the blade outline. Then the program will use the data entered earlier to generate the air channel model at this point, with a message displayed to signify that the air channel model has been generated.



Figure 9.4: Blade Outline for Selecting Location of Air-Channel Model

To display the air channel model Click **Display** on the main menu and then select **Air-Channel FE Model** on the **MODEL DISPLAY** submenu (Figure 9.5)



Figure 9.5: Air-Channel Model Display Options

Figure 9.6 shows the finite element mesh of the air-channel model. The boundary conditions can be displayed by clicking on Air-Channel Boundary Conditions on the MODEL DISPLAY submenu (Figure 9.5). The air channel model with the default boundary conditions are shown in Figure 9.6.

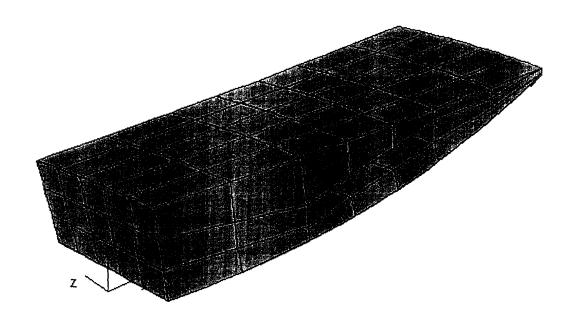


Figure 9.6: Finite Element Mesh of Air-Channel Model

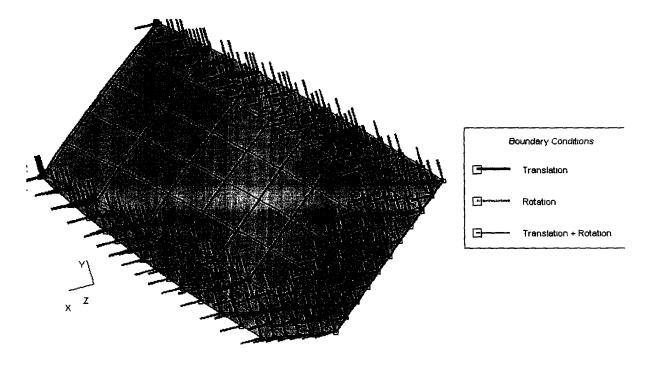


Figure 9.7: Finite Element Mesh of Air-Channel Model Showing Boundary Conditions

#### 9.4 Finite Element Stress Analysis of Air Channel Model

This step involves the performance of the finite element analysis using the VAST finite element code. This is accomplished by the following procedure.

#### 9.4.1 Generate VAST Input File

This step involves generating the input file for a VAST finite element analysis.

Click the Analysis on the main menu and select the Generate VAST Input File option on the ANALYSIS submenu.

During the air-channel model generation, the program generates a file named PREFIX.CHL, which is a complete VAST input deck. Therefore, in this step, all that is done is to copy the PREFIX.CHL file into another file called PREFIXC.USE, which is used for the VAST analysis. This way, any existing VAST files with the original PREFIX name are maintained and not over written. It should be noted that the air-channel data is still retained in the original prefix name.

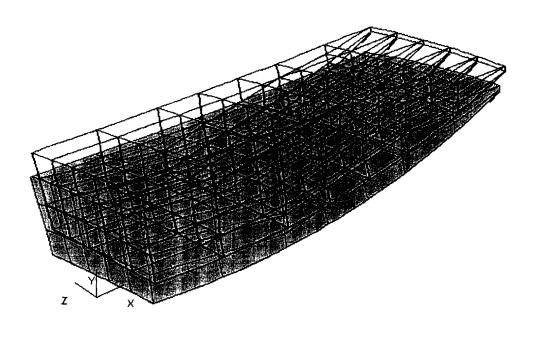
### 9.4.2 Finite Element Stress Analysis

The process of performing the finite element stress analysis is similar to the one described in Section 3.3.2.

Click **Analysis** on the main menu, then click **Start VAST Analysis** on the **Analysis** submenu (see Figure 3.10). When the VAST analysis status screen is shown (Figure 3.11) click **Start** to start the VAST stress analysis. Click **OK** when the analysis is complete and return to the PVAST main menu.

#### 9.5 Post-Processing Stress Results

Only the general-purpose plotting options are available for the air-channel model. The procedure for displaying results is similar to that described in Section 5.3.2. Following that procedure, displacement and stress responses from the air-channel model analysis have been plotted. Figure 9.7 (a) shows the deformed shape superimposed on the undeformed air-channel configuration, and Figure 9.7(b) shows contours of the model displacements. Contours of the von-Mises stresses are plotted in Figure 9.8 (a) and (b) using the contour fringe and line plotting options, respectively.



DISPLACEMENTS, LOAD CASE 1

Figure 9.8

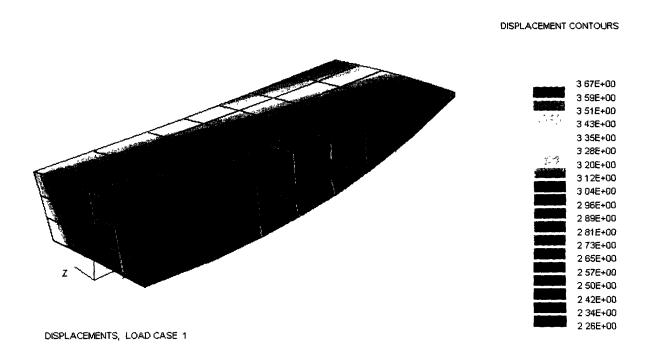


Figure 9.9: Air-Channel Displacement Responses (a) Deformed Shape Superimposed on Undeformed Configuration; (b) Displacement Contours

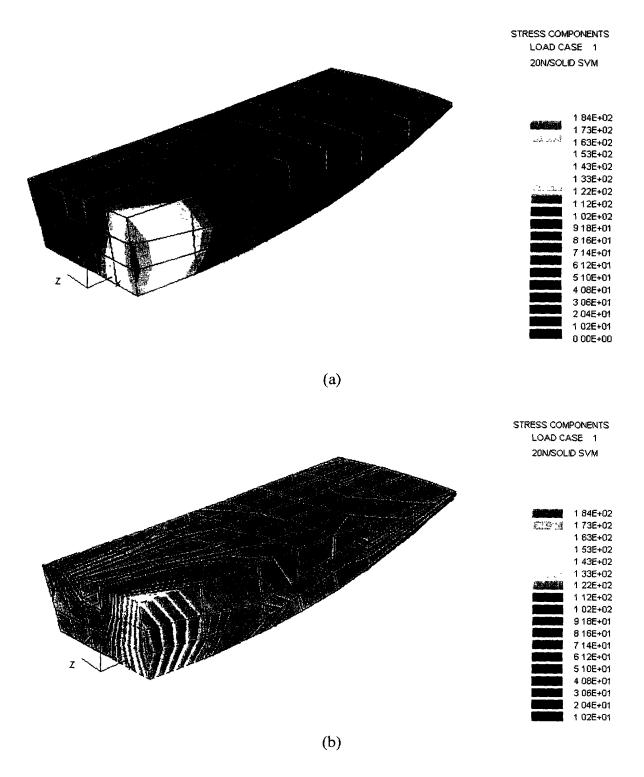


Figure 9.10: Air-Channel von-Mises Stresses (a) Fringe Plot; (b) Contour Line Plot

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## APPENDIX A:

BLADE GEOMETRY FILE FORMATS AND SAMPLE FILES

#### 1. A.1 Format of PREFIX.DAT File

Headers are used to distinguish various sections of the blade geometry data.

#### 2. A. Basic Data

**BASIC** Header Card 1 (A40) TITLE 40 character title Card 2 (A\$) 4 character description of length units **UNIT** - IN. for length in inches - MM. for length in millimeters Card 3 (F10.3) full radius RR Card 4 (I5) **IHAND** parameter for describing the divertion of rotation of the propeller — (1) for right hand rotation (clockwise looking forward) — (-1) for left hand rotation (anticlockwise looking forward) Card 5 (15) K number of radial sections Card 6 (A1) PITCH pitch type - A for pitch defined as angles - P for pitch defined as distance travelled in one rotation — D for pitch as pitch diameter ratio Card 6 (A1) **SKEW** = skew type - A for skew defined as angle - D for skew defined as linear measure Card 7 (I5) 1FORMAT =section data format

— 1 for non-dimensional ratios of maximum thickness

- 2 for NACA section data

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- 3 for section offsets Card 8 (15) number of chord stations Card 9 (I5) 1CHORD - 1 same chord fractions used throughout - 2 different chord fractions are used В. **Radial Data RADIAL** Header Repeat Card 1 for K Sections Card 1 (F10.3) R section radius as fraction of full radius. Repeat Card 2 for K Sections Card 2 (F10.3) chord length Repeat Card 3 for K Sections Card 3 (F10.3) pitch Repeat Card 4 for K Sections Card 4 (F10.3) skew Repeat Card 5 for K Sections Card 5 (F10.3) RK rake C. **Chordwise Data** Header **CHORDWISE** Repeat Card 1 for K Radial Stations

D.

Card 2 (I5)

Card 1 (F10.3) MAXTHK =maximum thickness/chord ratio Repeat Card 2 for K Radial Stations Card 2 (F10.3) MAXCAM =maximum camber/chord ratio Repeat Card 3 for L Chord Stations Card 3 (F10.3) PERCHORD= chord station as percentage of the chord length Repeat Card 4 for L Chord Stations Card 4 (F10.3) HLFTHK half thickness as percentage of chord length Repeat Card 5 for L Chord Stations Card 5 (F10.3) camber offset as percentage of chord length **CAMB** Card 6 (I5) IMOD modification option - O for no modification of chordwise data - I for modification of chord data Card 7 (I5) NCHORD = number of existing chord stations Card 8 (I6) NCOS number of COS function generated stations **Edge Data** Header **EDGES** Card 1 (I5) **NLEP** number of additional leading edge points

NTEP = number of additional trailing edge points

Card 3 (15)

IELLIP = type of edge generated

-1 for elliptical

- 2 for radial

E. Base Data

Header = BASE

Card 1 (15)

IBASE = base type

— 1 for hub

-2 for palm

Card 2 (I5)

NDIAM = number of hub diameters

Repeat Card 3 for NDIAM Diameters

Card 3 (2F10.3)

DIA = diameter

LOC = location at which diameter is measured along the shaft axis

Card 4 (F10.3)

FDIA = forward diameter to origin

#### A.2 FORMAT OF PREFIX.T16 FILE

Card 1 (A40)

TITLE = 40 character title

Card 2 (15)

ICHORD = code for specifying chordwise positions for defining face and

back offsets. If =1, chordwise positions for the first section are provided, and those for the remaining sections are assumed to be identical. If =2, chordwise positions are provided for

each section.

Card 3 (215)

K = number of radial positions where data are provided (3=K=43)

L = number of chordwise positions where data are provided

(3=L=41)

Card 4 (F10.4)

RR = propeller full radius (length)

Card 5 (see Figure A-1) (SE10.3)

R section radial location as fraction of full radius

P = pitch angle (degrees), positive counter clockwise

S = section chord length

SK = skew (length), positive for section shifted in direction of

trailing edge

RK = rake (length), positive aft

Card 6 ( $C_{ii}$ , j=1,L) (8F10.4)

 $C_{(1,1)}$  = the chord fractions for the face and back surface offsets for the

? first section (see Figure A.1)

 $C_{(1,L)}$ 

## Repeat Card 7 for i=2,K

Card 7 ( $C_{ij}$ , j=1,L) (Omit if ICHORD=1) (8F10.4)

 $C_{i,1}$  = the chord fractions for the face and back surface offsets for

? sections 2 to K

 $C_{i,L}$ 

## Repeat Cards 8 and 9 for j=1,L

Card 8 (TB<sub>ji</sub>, i=1,K) (8F10.4)

TB<sub>(j,1)</sub> = back surface offsets (length), i.e. the z' coordinate in the developed sections (see Figure A.1) (negative value for -z' TB<sub>(j,K)</sub>

Card 9 (TF<sub>ji</sub>, i=1,K) (8F10.4)

TF<sub>(j,1)</sub> = face surface offsets
?

TF<sub>j,K)</sub>

#### A.3 NRC45.DAT Sample File

```
BASIC
QUEST PROPELLER BLADE #45 REF.DWG, CFHQ. #
IN.
    60.000 FULL RADIUS
        HAND
      NO OF SECTIONS
D
    2
       SECTION DATA FORMAT
   17
       NUMBER OF CHORD STATIONS
    1 SAME FRACTIONS THROUGHOUT
RADIAL
      .250
            R
      .300
            R
      .400
            R
      .500
            R
      .600
            R
      .700
      .800
      .900
            R
      .950
            R
      .975
            R
     1.000
            R
    18.000
            CHORD
    17.560
            CHORD
    17.240
            CHORD
    17.840
            CHORD
    18.500
           CHORD
    18.720
            CHORD
    17.940
            CHORD
    15.300
            CHORD
    12.860
            CHORD
    10.840
            CHORD
     5.300
            CHORD
    57.000
            P ANGLE
    52.900
           P ANGLE
    46.930 P ANGLE
    42.400 P ANGLE
    37.980 P ANGLE
    33.450 P ANGLE
    28.630 P ANGLE
    24.120
           P ANGLE
    22.370 P ANGLE
    21.650
           P ANGLE
    21.050
            P ANGLE
     1.638
            SKEW
      .285
            SKEW
    -1.030
            SKEW
    -1.602
            SKEW
    -1.781
            SKEW
    -1.624
            SKEW
    -1.198
            SKEW
     -.607
            SKEW
     -.256
            SKEW
     -.069
            SKEW
      .000
            SKEW
      .658
            RAKE
     2.711
            RAKE
```

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```
5.517
           RAKE
     7.757
            RAKE
     9.675
            RAKE
    11.382
            RAKE
    12.872
            RAKE
    14.312
           RAKE
    15.007
            RAKE
    15.368
            RAKE
    15.728
            RAKE
CHORDWISE
            MAX TH/CHORD
      .256
      .239
            MAX TH/CHORD
            MAX TH/CHORD
      .207
           MAX TH/CHORD
      .167
           MAX TH/CHORD
      .127
      .092
           MAX TH/CHORD
      .065
           MAX TH/CHORD
      .049 MAX TH/CHORD
      .050 MAX TH/CHORD
      .057
           MAX TH/CHORD
      .113 MAX TH/CHORD
      .025
           MAX CAM/CHORD
      .046 MAX CAM/CHORD
      .068
           MAX CAM/CHORD
      .072
           MAX CAM/CHORD
      .065
            MAX CAM/CHORD
      .052
            MAX CAM/CHORD
            MAX CAM/CHORD
      .033
      .015
            MAX CAM/CHORD
      .006 MAX CAM/CHORD
           MAX CAM/CHORD
      .002
     -.006 MAX CAM/CHORD
     .000 % CHORD
1.250 % CHORD
     2.500
           % CHORD
     5.000
           % CHORD
     7.500 % CHORD
    10.000
           % CHORD
    15.000
           % CHORD
    20.000
           % CHORD
    30.000
           % CHORD
    40.000
            % CHORD
    50.000
            % CHORD
    60.000
            % CHORD
    70.000
            % CHORD
            % CHORD
    80.000
    90.000
            % CHORD
    95.000
           % CHORD
   100.000
           % CHORD
      .000
           HALF THICK % CHORD
     1.292
           HALF THICK % CHORD
     1.805
           HALF THICK % CHORD
     2.509 HALF THICK % CHORD
     3.032
           HALF THICK % CHORD
     3.457
            HALF THICK % CHORD
     4.135
           HALF THICK % CHORD
     4.664
            HALF THICK % CHORD
            HALF THICK % CHORD
HALF THICK % CHORD
     5.417
     5.885
     6.000 HALF THICK % CHORD
```

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```
HALF THICK % CHORD
     5.835
           HALF THICK % CHORD
     5.269
     4.199 HALF THICK % CHORD
           HALF THICK % CHORD
     2.517
    1.415 HALF THICK % CHORD
      .120 HALF THICK % CHORD
      .000 CAMBER OFFSET % CHORD
      .296 CAMBER OFFSET % CHORD
      .585 CAMBER OFFSET % CHORD
     1.140 CAMBER OFFSET % CHORD
     1.665 CAMBER OFFSET % CHORD
     2.160
           CAMBER OFFSET % CHORD
     3.060
           CAMBER OFFSET % CHORD
     3.840
           CAMBER OFFSET % CHORD
     5.040
           CAMBER OFFSET % CHORD
     5.760
           CAMBER OFFSET % CHORD
           CAMBER OFFSET % CHORD
     6.000
           CAMBER OFFSET % CHORD
     5.760
     5.040 CAMBER OFFSET % CHORD
     3.840 CAMBER OFFSET % CHORD
     2.160 CAMBER OFFSET % CHORD
     1.140 CAMBER OFFSET % CHORD
      .000 CAMBER OFFSET % CHORD
    O MODIFICATION OPTION
   17 NO OF EXISTING CHORD STATIONS
    O NO. OF COS FUNCTION GENERATED STATIONS
EDGES
    3 NO. OF ADDITIONAL LEADING EDGE PTS.
    0 NO. OF ADDITIONAL TRAILING EDGE PTS.
    1 ELLIPTICAL TYPE LEADING EDGE
      NO. OF ADDITIONAL TIP RADII
      .000 BLADE TIP PITCH
      .000 BLADE TIP SKEW
           BLADE TIP RAKE
      .000
           BLADE TIP POINT OF MAX THICK.
      .000
            TIP GENERATION BY RADIAL METHOD
      .000 RADIUS OF TIP PROFILE
      DISTANCE NOT KNOWN FROM REF TO CENTER OF BLADE TIP
      .000 DIST FROM REF AXIS TO CENTER OF BLADE TIP
      COORINATE DATA PRINT OPTION
      .COO ROTATION ANGLE FOR BLADE SURFACE MEASUREMENT
      .000 SHIM THICKNESS FOR BLADE MEASUREMENT
   .5500
          .4900
                   .3600
                           .2400
                                   .1500
                                           .0800
                                                    .0630
                                                            .0630
           .0630
   .0630
                   .0630
   .0000
           .0000
                  .0000
                           .0000
                                   .0000
                                           .0000
                                                            .0000 LE
                                                   .0000
          .0000
   .0000
                   .0000
      .000
                 .000
                            .000
                                       .000
                                                   .000
                                                              .000
                                                                         .000
.000
     ANTISING ANG.
                          .000
      .000
                .000
      .000
                 .000
                            .000
                                       .000
                                                   .000
                                                              .000
                                                                         .000
.000
     ANTISING LENGTH
      .000
               .000
                          .000
BASE
      BLADE BASE TYPE
    3 NUMBER OF HUB DIAMETERS
    26.500
               .000 DIA. AND LOCATION
              12.750 DIA. AND LOCATION
    24.800
    19.000
              28.125 DIA. AND LOCATION
    12.750FWD. DIA. TO ORIGIN
```

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#### APPENDIX A

#### A.4 P5363.DAT Sample File

```
BASIC
QUEST SKEWED PROPELLER NO.5363 DWG.5561-6
  1524.000 FULL RADIUS
       HAND
   12 NO OF SECTIONS
      SECTION DATA FORMAT
   13 NUMBER OF CHORD STATIONS
      SAME FRACTIONS THROUGHOUT
       PMT IS CHORD DATUM
RADIAL
     0.200
            R
     0.250
     0.300
            R
     0.400
            R
     0.500
            R
     0.600
            R
     0.700
            R
     0.800
            R
     0.850
            R
     0.900
            R
     0.950
            R
     C.975
            R
   475.000
            CHORD
   491.000
            CHORD
   507.000
            CHORD
   535.000
            CHORD
   558.000
            CHORD
   581.000
            CHORD
   605.000
            CHORD
   615.000
            CHORD
   598.000
            CHORD
   560.000
            CHORD
   477.000
            CHORD
   370.000
            CHORD
    60.681 P ANGLE
    56.647 P ANGLE
    53.157 P ANGLE
    47.398 P ANGLE
    42.401 P ANGLE
    37.553 P ANGLE
    32.359 P ANGLE
    26.862 P ANGLE
    24.440 P ANGLE
    22.462 P ANGLE
    20.879 P ANGLE
    20.200 P ANGLE
D
  -200.000
            SKEW
  -173.000
            SKEW
  -139.000
            SKEW
   -59.000
            SKEW
    45.000
            SKEW
   171.000
            SKEW
   337.000
            SKEW
   542.000
            SKEW
   670.000
            SKEW
```

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1	808.000 967.000 059.000 -53.744 -67.181 -80.617 107.489 -134.361 -161.233 -188.106 -214.978 -228.414 -241.850 -255.286 -262.004 DRDWISE	SKEW SKEW SKEW RAKE RAKE RAKE RAKE RAKE RAKE RAKE RAKE						
	0.4968 0 0.2993 0	.3000	0.4892	0.3000	0.4301			8073 PMT
CHE	D.FRC	.9500	0.9000	0.8000	0.6000	0.4000	0.2000 0.0	0000 CHD FRC
TB	0.2000 0 -52.300	.4000 -69.		0.8000 7.000	1.0000 -87.600	-102.900	-112.800	-117.900TB
-	-119.600 -45.100	-115. -62.		5.700 9.200	-91.500 -79.800	-73.800 -95.300	-46.400 -105.100	-110.400TB
TB -	-112.000 -37.700	-108.: -54.:		8.500 1.200	-84.200 -71.900	-66.500 -87.400	-38.800 -97.200	-102.700TB
	-104.300 -23.300	-100.8 -38.		1.300 5.800	-77.300 -56.400	-59.600 -72.100	-31.700 -82.100	-87.700TB
ТВ	-89.300 -11.400	-86. -25.		8.000 2.000	-64.800 -42.400	-47.500 -57.600	-19.600 -67.500	-73.000TB
TB	-74.600 -3.600	-72. -15.		5.000 1.600	-53.200 -31.300	-36.900 -45.200	-10.300 -54.300	-59.500TB
TB	-61.000 -0.800	-59. -10.		2.800 5.400	-42.500 -23.600	-27.700 -35.400	-3.600 -43.100	-47.600TB
TB	-48.900 -2.300	-47. -9.		2.100	-33.400 -19.400	-21.000 -28.300	-0.800 -34.100	-37.300TB
TB	-38.300 -4.100	-37. -9.		3.300 3.100	-26.800 -18.100	-17.700 -25.400	-2.300 -30.100	-32.800TB
TB	-33.500 -6.300	-32. -11.		9.400	-24.200 -17.500	-16.900 -23.100	-4.100 -26.600	-28.600TB
TB	-29.200 -8.700	-28. -12.		6.100	-22.100 -17.200	-16.600 -21.200	-6.300 -23.700	-25.000TB
TB	-25.400 -9.900	-24. -13.		3.100 4.600	-20.400 -17.000	-16.800 -20.300	-8.700 -22.300	-23.400TB
TB	-23.700 -52.300	-23.1 -35.		1.900 9.700	-19.700 -21.200	-16.900 -10.200	-9.900 -4.000	-0.90CTF
ΤF	0.000	-1.	700 -	6.100	-13.300	-24.500	-46.400	

API	PENDIX A						Page 12	
TF	-45.100	-29.700	-24.200	-16.900	-7.800	-3.000	-0.600TF	
TE	0.000 -37.700	-1.100 -23.600	-4.200 -18.700	-9.900 -12.700	-19.100 -5.400	-38.800 -1.900	-0.300TF	
TF	0.000 -23.300	-0.700 -11.900	-2.800 -8.500	-7.200 -4.800	-14.400 -1.200	-31.700 -0.100	0.200TF	
TF	0.000 -11.400	-0.200 -2.500	-1.100 -0.500	-3.300 1.200	-7.200 1.900	-19.600 1.200	0.500TF	
	0.000 -3.600	0.000 3.000	-0.200 4.200	-0.900 4.600	-2.300 3.500	-10.300 1.900	0.600TF	
TF	0.000	0.100 4.100	0.500 4.900	0.800 5.000	1.200 3.600	-3.600 1.900	0.600TF	
TF TF	0.000 -2.300	0.200 1.600	0.800 2.300	1.600 2.800	2.500 2.100	-0.800 1.100	0.400TF	
TF	0.000 -4.100	0.100 -0.600	0.400 0.100	0.700 0.900	1.100 1.000	-2.300 0.600	0.200TF	
TF	0.000 -6.300	0.000 -3.100	0.000 -2.200	-0.200 -1.100	0.000 -0.200	-4.100 0.100	0.1007F	
	0.00C -8.700	-0.100 -5.600	-0.500 -4.700	-1.200 -3.200	-1.900 -1.400	-6.300 -0.500	-0.100TF	
TF	0.000 -9.900	-0.200 -6.800	-0.900 -5.800	-2.100 -4.200	-3.500 -2.000	-8.700 -0.700	-C.100TF	
ΤF	0.000	-0.300	-1.200	-2.600	-4.200	-9.900		
DOUBLE DECES  5 NO. OF ADDITIONAL LEADING EDGE PTS. 5 NO. OF ADDITIONAL TRAILING EDGE PTS. 1 ELLIPTICAL TYPE LEADING EDGE 3 NO. OF ADDITIONAL BLADE TIP RADII 19.607 BLADE TIP PITCH ANGLE 1168.000 BLADE TIP SKEW -270.000 BLADE TIP PT OF MAX THK 0 TIP GENERATION BY RADIAL METHOD 10.000 RADIUS OF TIP PROFILE 1 DISTANCE KNOWN FROM REF TO CENTER OF BLADE TIP .000 DISTANCE FROM REF AXIS TO CENTER OF BLADE TIP 3 COORDINATE DATA PRINT OPTION .000 ROTATION ANGLE FOR BLADE SURFACE MEASUREMENT .000 SHIM THICKNESS FOR DREA MEAS MACHINE 7.0000 6.9000 6.7500 6.5000 6.0000 3.0000 2.5000 2.2500 LE								
7	.0000 6.	0000 2.00 9000 6.75 0000 4.00	00 6.5000	6.0000	5.5000 5	.0000 4.50	000 lE	
BAS		BASE TYPE						

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#### A.5 P4388.DAT Sample File

```
BASIC
 HIGHLY SKEWED PROPELLER NO.4388
IN.
     6.000 FULL RADIUS
        HAND
       NO OF SECTIONS
Α
D
    3
      SECTION DATA FORMAT
   17
       NUMBER OF CHORD STATIONS
    1 SAME FRACTIONS THROUGHOUT
    1 50% CHORD DATUM
RADIAL
      .200
            R
      .300
            R
      .400
            R
      .500
            R
      .600
            R
      .700
            R
      .800
            R
      .900
            R
      .950
     3.840
            CHORD
     4.362
            CHORD
     4.858
            CHORD
     5.270
            CHORD
     5.532
            CHORD
     5.546
            CHORD
     5.216
            CHORD
     4.336
            CHORD
     3.330
            CHORD
    55.813
            P ANGLE
    44.664
            P ANGLE
    37.214
            P ANGLE
            P ANGLE
    32.237
            P ANGLE
    28.626
    25.967
            P ANGLE
    24.029
            P ANGLE
    22.662
            P ANGLE
            P ANGLE
    22.069
       .000
            SKEW
      .471
            SKEW
     1.256
            SKEW
     2.356
            SKEW
     3.770
            SKEW
     5.498
            SKEW
     7.540
            SKEW
     9.896
            SKEW
    11.090
            SKEW
      .000
            RAKE
      .000
            RAKE
      .000
            RAKE
      .000
            RAKE
      .000
            RAKE
       .000
            RAKE
      .000
            RAKE
      .000
            RAKE
```

.000

RAKE

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CHORDWISE .0000 .4000 1.0000	.0125			.0750 .7000	.1000			CHD.FF	
.000 258 105	0 2 0	79	074 284 013	106 283	132 269	15 23		219 188	
.000 300 123	0 3 0	54 28	078 334 011	116 334	147 320	17 28		252 222	
.000 295 121	0 3 0	23 65	074 329 010	111 331	142 318	16 28		246 222	
.000 274 114	0 3 0	03 60	067 310 008	102 311	131 299	15 26	8	230 210	TB
.000 254 104	0 2 0	78 55	060 285 006	092 286	119 276	14 24	7	210 194	TB
.000 228 094 .000	0 2 0 0	51 48	052 256 005 043	081 258 068	105 250 088	12 22	4	188 176	TB
193 080	2 0 0	13 40	043 218 004 030	219 048	088 212 063	10 19 07	1	159 150 114	TB
139 058 .000	1 0 0	53 29	157 002 022	158 034	153 045	05	8	114 108 084	TB
099 041 .000	1 0 .0	09 21	112 002 .046	113	109	09	8	077	TB
.107 .042 .000	.1 .0 .0	30 24	.111 .013 .025	.108	.098	.08	1	.061	TF
.013 .004 .000	.0	10 16	.005 .011 .014	.002	.005	.01		.012 017	
030 014 .000	0 .0 .0	01 10	043 .010 .006	046 003	051 010	05 01	7	043 040	
054 025 .000	0 0 .0	06 05	072 .008 001	075 011	078 021	07 03	0	062 056	TF
076 032 .000 089	0 0 .0 1	11 00	092 .006 006 106	095 018 109	097 029	09 03	8	074 068	TF
038 .000 092	0 0 1	14 02	.005 010 108	022 110	110 .000 110	10: 04: 10:	2	082 071 082	TF
039 .000 072	01 01 01	16 03	.004	018 087	026 086	03 08	4	082 057 064	TF
030 .000 049	01 01	12 02 56	.002 006 058	012 059	018 059	023 059	3	036 044	TF
+.021 EDGES	00	) <del>9</del>	.002						

EDGES
5 NO. OF ADDITIONAL LEADING EDGE PTS.

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```
0 NO. OF ADDITIONAL TRAILING EDGE PTS.
   1 ELLIPTICAL TYPE LEADING EDGE
   3 NO. OF ADDITIONAL TIP RADII
   21.591 BLADE TIP PITCH
   12.564 BLADE TIP SKEW
     .000 BLADE TIP RAKE
     .000 BLADE TIP POINT OF MAX THICK.
           ELLIPTICAL TIP GENERATION
     .040 SEMITHICKNESS OF ELLIPTICAL PROFILE
   1 DISTANCE KNOWN FROM REF TO CENTER OF BLADE TIP
    -.040 DIST FROM REF AXIS TO CENTER OF BLADE TIP
   1 COORINATE DATA PRINT OPTION
      .000 ROTATION ANGLE FOR BLADE SURFACE MEASUREMENT
      ,000 SHIM THICKNESS FOR BLADE MEASUREMENT
   .0260
          .0168
                  .0108
                           .0068
                                   .0044
                                           .0028
                                                   .0028
                                                           .0028 LE
   .0028
   .0000
           .0000
                 .0000
                           .0000
                                   .0000 .0000
                                                  .0000
                                                           .0000 LE
   .0000
      .000
                .000
                           .000
                                       .000
                                                  .000
                                                             .000
                                                                         .000
.000
    ANTISING ANG.
     .000
                            .000
                                       .000
                                                  .000
                                                             .000
      .000
                 .000
                                                                         .000
.000 ANTISING LENGTH
      .000
BASE
    O BLADE BASE TYPE
```

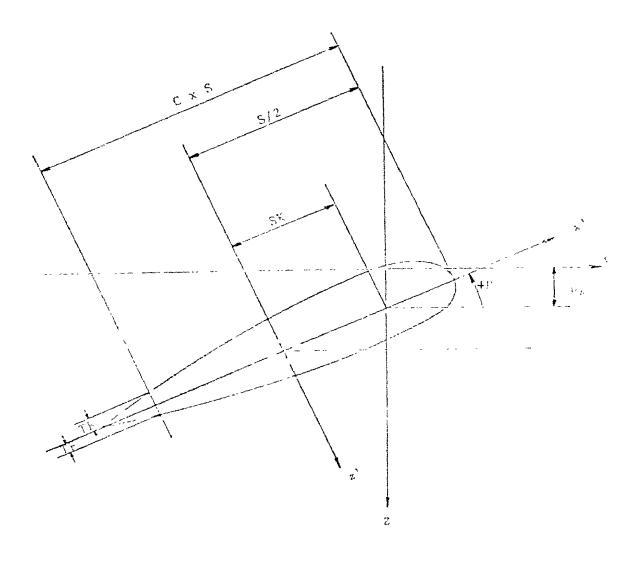


Figure A.1: Diagramatic Explanation of Parameters Used to Describe Blade Section Geometry

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## APPENDIX B:

**P5363.LIN SAMPLE FILE** 

APPENDIX B Page 1

## P5363.LIN Sample File

1 0 NSMB 2 1 12 19	5363 0	MODEL OF	QUEST NEW	DESIGN PROPEI	LER -	
	0.2782	0.3338	0.4011	0.4771	0.5584	0.6416
0.7989 0.0000 0.2998	0.8662 0.0085	0.9218 0.0287		0.1068	0.1625	0.2275
	0.4589	0.5411	0.6223	0.7002	0.7725	0.8375
	0.9713 0.1427	1.0000 0.0650	0.0827	0.0577	0.0572	0.0525
0.0583	0.0581	0.0572	0.0570	0.0623	0.0617	0.0641
0.0929 0.1714 0.0684	0.1080 0.1489	0.1714 0.0566	0.0812	2 0.0599	0.0637	0.0639
0.0759 0.0813	0.0798	0.0825	0.0831	0.0874	0.0844	0,0840
0.1093 0.1804 0.0439	0.1226 0.1460	0.1714 0.0619	0.0781	0.0508	0.0489	0.0434
	0.0479	0.0474	0.0483	0.0556	0.0568	0.0617
0.0964 0.1804 0.0683	0.1131 0.1480	0.1804 0.0565	0.0802	2 0.0589	0.0628	0.0630
0.0768 0.0857	0.0814	0.0844	0.0853	0.0896	0.0869	0.0874
	0.1275 0.1573	0.1804 0.0541	0.0710	0.0424	0.0398	0.0337
0.0380	0.0379	0.0382	0.0403	0.0491	0.0515	0.0577
0.0960 0.1947 0.0724	0.1146 0.1571	0.1947 0.0612	0.0839	0.0628	0.0667	0.0670
0.0811 0.0913	0.0857	0.0887	0.089	0.0944	0.0923	0.2932
0.1195 0.2156 0.0220	0.1321 0.1633	0.1947 0.0438	0.0614	0.0325	0.0294	0.0221
0.0268	0.0280	0.0300	0.0333	0.0428	0.0459	0.0529
0.0942 0.2156 0.0805	0.1154 0.1722	0.2156 0.0712	0.092	0.0708	0.0748	0.0755
0.0887	0.0926	0.0949	0.0960	0.1013	0.0996	0.1006
0.1261 0.2437 0.0079	0.1378 0.1554	0.2156 0.0324	0.0494	0.0197	0.0158	0.0076
0.0145	0.0185	0.0230	0.0275	0.0377	0.0413	0.0492
0.0934 0.2437 0.0917	0.1168 0.1937		0.1050	0.0832	0.0867	0.0872

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0.0987 0.1063	0.1012	0.1026	0.1035	0.1093	0.1080	0.1090
0.1330 0.2792	0.1436 0.1413	0.2437 0.0195	0.0357	0.0041	0.0008	0.0008
0.0008 0.0041 0.0559	0.0119	0.0189	0.0246	0.0353	0.0398	0.0488
0.0949 0.2792	0.1193 0.2280	0.2792 0.1016	0.1194	0.0992	0.1020	0.1018
0.1051 0.1099 0.1136	0.1104	0.1108	0.1115	0.1172	0.1160	0.1167
0.1384 0.3213	0.1477 0.1082	0.2792 0.0066	0.0229	0.0008	0.0008	0.0008
0.0008 0.0008 0.0607	0.0103	0.0185	0.0254	0.0369	0.0426	0.0527
0.0987 0.3213	0.1226 0.2646	0.3213 0.1184	0.1331	0.1146	0.1166	0.1155
0.1172 0.1191 0.1180	0.1177	0.1175	0.1178	0.1226	0.1212	0.1213
0.1405 0.3682	0.1488 0.0584	0.3213 0.0008	0.0119	0.0008	0.0008	0.0008
0.0008 0.0014 0.0662	0.0145	0.0229	0.0301	0.0420	0.0483	0.0582
0.1022 0.3682	0.1250 0.3032	0.3682 0.1322	0.1426	0.1247	0.1265	0.1246
0.1242 0.1237 0.1190	0.1210	C.1205	0.1202	0.1237	0.1217	0.1217
0.1400 0.4170	0.1478 0.0008	0.3682 0.0008	0.0062	0.0008	0.0008	0.0008
0.0008 0.0110 0.0693	0.0228	0.0304	0.0368	0.0478	0.0534	0.0623
0.1036 0.4170	0.1252 0.3394	0.4170 0.1426	0.1474	0.1290	0.1303	0.1273
0.1248 0.1231 0.1170	0.1200	0.1190	0.1184	0.1212	0.1190	C.1190
0.1382 0.4643 0.0059	0.1470 0.0008	0.4170 0.0008	0.0052	0.0008	0.0008	0.0008
0.0039 0.0214 0.0711	0.0317	0.0385	0.0438	0.0535	0.0580	0.0657
0.1053 0.4643 0.1206	0.1265 0.3733	0.4643 0.1532	0.1505	0.1301	0.1284	0.1238
0.1206 0.1188 0.1129	0.1159	0.1147	0.1140	0.1168	0.1145	0.1146
0.1360 0.5064	0.1471 0.0008	0.4643 0.0008	0.0028	0.0008	0.0008	0.0069
0.0179 0.0317 0.0730	0.0406	0.0469	0.0515	0.0603	0.0632	0.0695
0.1098 0.5064 0.1143	0.1321 0.4071	0.5064 0.1623	0.1519	0.1272	0.1225	0.1172

APPENDIX B	<del> </del>					Page 3
0.1132 0.1075	0.1106	0.1092	0.1083	0.1113	0.1090	0.1092
0.1351	0.1495	0.5064				
0.5395	0.0008	0.0008	0.0014	0.0009	0.0071	0.0148
0.0279						
0.0406 0.0715	0.0474	0.0530	0.0573	0.0653	0.0662	0.0707
0.1062	0.1258	0.5395				
0.5395 0.1096	0.4226	0.1735	0.1543	0.1273	0.1186	0.1128
0.1091	0.1067	0.1043	0.1021	0.1051	0.1028	0.1032
0.0996						
0.1299	0.1450	0.5395				

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This report is an examples manual for the finite element analysis code called PVAST (Propeller Vibration And STrength) that is used for prediction of stress and vibration in marine propellers. PVAST can automatically generate propeller finite element models from basic propeller geometry defined by the orientation of 2D "wrapped" blade sections at specified radii. A number of different models can be considered including; a single blade, a single blade with fillet, a blade-fillet-palm model, a blade-fillet-hub segment model, and multiple blade and hub model. The types of structural finite element analyses that can be conducted include; static analysis with user-defined blade pressure distributions and point loads, natural frequency analysis in air and in water, time domain analysis with applied loads and support motion, response spectrum analysis and frequency response analysis. The program provides 2D and 3D plotting of blade geometry, finite element models and post-processing to provide visualization of predicted finite element model displacements, stresses and mode shapes. The code has been modified recently to include a "Windows" graphical user interface implemented with a combination of GKS and MS Visual C++. This provides a more "friendly" user interface and is a major change in the look and feel of PVAST Version 7.3 compared with earlier versions of the code. This manual provides a number of example problems, considered with PVAST Version 7.3 for a range of model types, analysis options and results.

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