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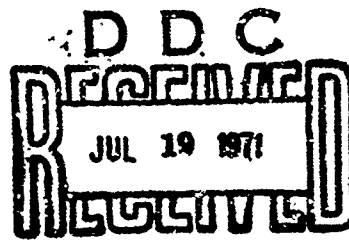
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**THEORETICAL GUN PROPELLANT
THERMOCHEMICAL EVALUATION**

**GUNS AND ROCKETS BRANCH
ADVANCED DEVELOPMENT DIVISION**

TECHNICAL REPORT AFATL-TR-71-11

JANUARY 1971



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13. ABSTRACT A computer program is presented for the computation of chemical equilibrium reaction products associated with gun propellant combustion. The program as developed at the Air Force Armament Laboratory was based on a code used by the NASA Lewis Research Center. The program provides a first approximation of flame temperature, specific heat ratio, impetus, and mean molecular weight of the combustion products. A simplified users manual is presented for thermochemical programs and for the program to generate specific heat polynomials from JANAF tabular data.			

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Theoretical Gun Propellant Thermochemical Evaluation

Otto K. Heiney

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FOREWORD

This report has been generated under the advanced gun propellant evaluation analysis portion of Project 62602F 2560 and is presented as a state of the art advancement that can be applied to gun propellant research efforts. The study was conducted during the period February 1970 to January 1971.

This technical report has been reviewed and is approved.



CHARLES PETRIDES

Chief, Advanced Development Division

ABSTRACT

A computer program is presented for computing the chemical equilibrium reaction products associated with gun propellant combustion. This program will provide a good first approximation of flame temperature, specific heat ratio, impetus, and mean molecular weight of the combustion products. The program as developed at the Air Force Armament Laboratory was based on a code used by the National Aeronautics and Space Administration Lewis Research Center. The minor changes to the program are discussed, some results from advanced solid propellant formulations calculations are presented, and a form of users manual for thermochemical programs and for the program to generate specific heat polynomials from JANAF tabular data is presented.

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LIST OF ABBREVIATIONS AND SYMBOLS

C_p	Specific heat at constant pressure
C_v	Specific heat at constant volume
E	Internal energy
F_p	Propellant impetus
G	Gibbs free energy
H	Enthalpy
K	Gas conductivity
M	Molecular weight
P	Pressure
R	Gas constant
S	Entropy
T	Temperature
T_{FP}	Flame temperature at constant pressure
T_{FV}	Flame temperature at constant volume
V	Volume
X_i	Mole fraction
γ	Specific heat ratio
σ	Leonard-Jones force constant
Ω	Leonard-Jones force constant
μ	Gas viscosity

SECTION I

INTRODUCTION

The field of gun propellant development, which had been relatively static for many years, has recently begun to attract increased attention. The availability of an accurate theoretical thermochemical propellant performance computer program is of central importance to informed research and development efforts in this field. As a formulation screening tool, a few dollars of machine time can save hundreds of dollars of laboratory small-batch-mix effort by eliminating unpromising candidate formulations and providing a good first approximation to the primary important propellant parameters. These would include flame temperature, specific heat ratio, impetus, and mean molecular weight of the combustion products. To most expediently obtain a computer program for computing the chemical equilibrium reaction products, the Air Force Armament Laboratory modified an existing free-energy minimization rocket propellant performance program. The program selected was the one used by the National Aeronautics and Space Administration Lewis Research Center. This code⁽¹⁾ has a background of almost ten years of successful application. In addition, it was readily available and the JANAF specific heat data could be easily applied to the thermodynamic data tape. The program, as modified for gun propellant applications, was checked against established experimental data and other analytic chemical equilibrium computing techniques, with excellent agreement. Additionally, an algorithm was added which computes combustion gas viscosity and thermal conductivity by a Leonard-Jones potential technique.

The following sections of this report discuss the minor changes made to the Lewis approach, give some results from advanced solid propellant formulation calculations, and provide a form of users manual for the thermochemical programs and for the program to generate specific heat polynomials from JANAF tabular data⁽²⁾. Appendix I presents the Lewis program listing and Appendix II presents the polynomial fit program used at the Armament Laboratory.

SECTION II

FREE ENTHALPY EQUATIONS

This report will not discuss the mathematical techniques of chemical equilibrium computations. This task has effectively been accomplished in a recently issued monograph⁽³⁾ which discusses in detail not only the Lewis technique but also several other commonly used approaches. This report will demonstrate only that, at chemical equilibrium, the Gibbs free energy, G , (or free enthalpy) will be a minimum.

From the First Law of Thermodynamics, in an irreversible process:

$$dE + pdv - Tds < 0 \quad (1)$$

or at equilibrium

$$dE + pdv - Tds = 0 \quad (2)$$

For a constant pressure and temperature, equation (2) becomes

$$d(E + pv - Ts) = 0 \quad (3)$$

$$G_T = H_T - T_1 S_1 \quad (4)$$

Equation (4) establishes the relation that the Gibbs free energy will be a minimum at equilibrium, and when coupled with the atomic species mass conservation equations, it provides a sufficient set for solution of the combustion species concentration and flame temperature (if the combustion pressure is specified). Then, to set up a minimization algorithm only requires a value for the heat of formation of the reactant compounds and tabular or polynomial data for the specified heat, C_p , enthalpy, H_T , and entropy, S_T , of the possible combustion products. These thermodynamic data can be obtained from reference 2 for most combustion products of interest: as

$$H_T - H_{298} = \int_{298}^T C_p dT \quad (5)$$

$$\text{and } S_T - S_{298} = \int_{298}^T \frac{C_p}{T} dT \quad (6)$$

Selecting a polynomial form for C_p , the terms H_T and S_T can be conveniently fitted to similar polynomials by performing the indicated integrations

$$\frac{C_p}{R} = a_1 + a_2 T + a_3 T^2 + a_4 T^3 + a_5 T^4 \quad (7)$$

$$\frac{H_T}{RT} = a_1 + 1/2 a_2 T + 1/3 a_3 T^2 + 1/4 a_4 T^3 + 1/5 a_5 T^4 + a_6/T \quad (8)$$

$$\frac{S_T}{R} = a_1 \ln T + a_2 T + 1/2 a_3 T^2 + 1/3 a_4 T^3 + 1/4 a_5 T^4 + a_7 \quad (9)$$

For a more precise fit, the Lewis program utilizes two sets of coefficients for each species, one in the temperature range 0° to $1000^\circ K$ and the other from 1000° to $6000^\circ K$. Limits of species existence can be placed on the propellant data to restrict the range of polynomial applicability.

The primary change made to the Lewis algorithm was to additionally develop an approximate isochoric temperature from the isobaric temperature provided by the program. This requires the assumption that approximately the same species would form either in an isochoric or isobaric process, providing a similar total heat release. If these assumptions are warranted, then:

$$Q_R = C_p T_{FP} \quad (10)$$

$$Q_R = C_v T_{FV} \quad (11)$$

$$T_{FV} = C_p/C_v T_{FP} = \gamma T_{FP} \quad (12)$$

Once the isochoric flame temperature and mean molecular weight of the combustion products are known, the impetus is simply

$$F_p = \frac{R}{M} T_{FV} \quad (13)$$

where $R = 2780 \text{ ft-lbs/lb-mole-}^\circ K$

The program also computes the constitutive products mole fractions as a function of the pressure ratio (or, for a gun system, of the velocity) if quasi-isentropic conditions are assumed.

Equation (13) indicates the importance of developing advanced propellants with lower molecular weight combustion products, if the impetus

of a propellant is to be increased without a corresponding flame temperature increase. High propellant flame temperatures are, of course, the prime limiting factor in developing an acceptable barrel life for automatic aircraft cannon having a high performance and a high rate of fire. Current single-base solid gun propellants display molecular weights in the order of 25. Table I illustrates the distinctive flame temperature advantage of lower molecular weights in obtaining cooler combustion conditions without sacrificing energy output.

TABLE I. FLAME TEMPERATURES AS A FUNCTION OF MOLECULAR WEIGHT AND IMPETUS				
Molecular Weight, Atomic Mass Units	Flame Temperature, °K, at Impetus, Ft-lb/lb			
	325,000	350,000	375,000	400,000
25	2980	2150	3380	3500
22	2570	2770	2970	3170
20	2340	2620	2700	2880
19	2220	2390	2570	2740
18	2110	2270	2430	2590
17	1990	2140	2290	2450

The very favorable performance data indicated by the lower right-hand entries in Table I are responsible for the continued advanced solid gun propellant development efforts. The test cases described in the following sections have resulted from calculations of two of the formulations now under contract investigation and from a comparison of results of two theoretical computations with experimental measurements of inservice propellants. All computations are performed at a standard reference pressure of 5,000 psia.

The first requirement for free energy computations is a reliable list of heats of formations for the constituents to be considered. Table II provides this data for the ingredients in the formulations discussed in this report. Additional tables are available in references 4 and 5.

TABLE II. HEATS OF FORMATION		
CONSTITUENT	EMPIRICAL FORMULA	HEATS OF FORMATION KILOCALORIES PER MOLE
Ammonium Nitrate	H ₄ O ₃ N ₂	-88.1
CTPB	C ₇ H ₁₁ O _{0.2} N _{0.02}	-5.0
Dibutylphthalate	C ₁₈ H ₁₄ O ₄	-200.0
Diphenylamine	C ₁₂ H ₁₁ N ₁	+27.6
DMDTH	C ₆ H ₁₄ O ₆ N ₄	-94.0
Ethyl Acrylate	C ₅ H ₈ O ₂	-87.3
Ethyl Alcohol	C ₂ H ₆ O ₁	-66.3
Ethyl Centralite	C ₁₇ H ₂₀ O ₁ N ₂	-34.2
Ethylene Dihydrazine	C ₂ H ₁₀ N ₄	+31.2
Glycol Dinitrate	C ₂ H ₄ O ₆ N ₂	-58.7
Guanidine Nitrate	C ₁ H ₆ O ₃ N ₄	-79.3
HMX	C ₄ H ₈ O ₈ N ₈	+17.9
Nitrocellulose (12.6 percent N)	C ₂₄ H _{30.2} O _{39.4} N _{9.8}	-655.5
Nitrocellulose (12.7 percent N)	C ₂₄ H ₃₀ O ₄₀ N _{10.0}	-659.3
Nitrocellulose (13.15 percent N)	C ₂₄ H _{29.5} O _{41.3} N _{10.6}	-643.1
Nitrocellulose (13.75 percent N)	C ₂₄ H _{29.3} O _{41.4} N _{10.7}	-639.9
Nitroglycerine	C ₃ H ₅ O ₉ N ₃	-85.3
Nitroguanidine	C ₁ H ₄ O ₂ N ₄	-12.6
Polymethyl Vinyl Tetrazole	C ₄ H ₆ N ₄	+52.4
RDX	C ₃ H ₆ O ₆ N ₆	+14.9
Potassium Sulfate	K ₂ S ₁ C ₄	-338.5
Triacetin	C ₉ H ₁₄ O ₆	-307.0
Triazoethanol	C ₂ H ₅ O ₁ N ₃	+22.5
Triaminoguanidine Nitrate	C ₁ H ₉ O ₅ N ₇	-11.5
Water	H ₂ O ₁	-68.4

SECTION III

COMPUTATION OF VISCOSITY AND CONDUCTIVITY

For gun propellant applications, it is often quite important to determine a theoretical value for the combustion gas conductivity and viscosity. These are particularly necessary if the convective gun barrel heating characteristics of the propellants are to be evaluated. To accomplish this task, the Leonard-Jones potential technique⁽⁶⁾ was applied.

The viscosity for a single constitutive species is given by:

$$\mu_1 = 2.6693 \times 10^{-5} \sqrt{MT} / \sigma^2 \Omega \quad (14)$$

where T is the temperature, M is the molecular weight, and σ and Ω are the Leonard-Jones force constants. The viscosity of the mixture is defined by

$$\mu_{MIX} = \sum_{i=1}^n \left(x_i \mu_i \right) \left(\sum_{j=1}^n x_j \phi_{ij} \right) \quad (15)$$

with n being the number of species considered and x_i being the mole fraction of the species. The value, ϕ_{ij} is defined as

$$\phi_{ij} = \frac{1}{\sqrt{8}} \left(1 + \frac{M_i}{M_j} \right)^{-1/2} \left[1 + \left(\frac{\mu_i}{\mu_j} \right)^{1/2} \left(\frac{M_j}{M_i} \right)^{1/4} \right]^2 \quad (16)$$

The thermal conductivity of a species is given as:

$$K_i = 1.9891 \times 10^{-4} \frac{\sqrt{T/M}}{\sigma^2 \Omega} \quad (17)$$

The mixture value is given as

$$K_{MIX} = \sum_{i=1}^n \left(x_i K_i \right) \left(\sum_{j=1}^n x_j \phi_{ij} \right) \quad (18)$$

This approach is strictly valid for only dilute mixtures of non-polar molecules. Five species are considered, (one of which, H_2O , is polar), and all have a dense gas system. Thus, the results contain only order of magnitude validity, but are none the less of value, considering the state of the art in mathematical modeling of the transient heat convection process in gun bores. Table III gives the species considered which are typically 98 to 99 percent of the combustion gas constituents.

TABLE III. LEONARD-JONES POTENTIAL PARAMETERS (FORCE CONSTANTS)			
Species	Molecular Weight, Atomic Mass Units	Viscosity, Grams/cm-sec	Conductivity, Cal/cm-sec-K
H ₂	2.016	2.915	38.0
N ₂	28.02	3.749	79.8
CO	28.01	3.706	88.
CO ₂	44.01	3.897	213.
H ₂ O	18.0	2.824	230.9

Table IV consists of the $\Omega - \frac{KT}{\epsilon}$ relations needed for the solution of Equations (14) and (17). The first column contains values for the relatively non-polar species such as H₂, N₂, CO, and CO₂, while the second column has a corrected value for the highly polar H₂O.

TABLE IV. REDUCED CROSS SECTION

KT/ε	NON-POLAR	POLAR		KT/ε	NON-POLAR	POLAR
1.0	1.5938	2.6199		7	0.8725	0.8946
1.2	1.4568	2.4257		8	0.8536	0.8422
1.4	1.3557	2.2713		9	0.8378	0.8043
1.6	1.2800	2.1413		10	0.8242	0.7760
1.8	1.2216	2.0263		11	0.8123	0.7544
2.0	1.1751	1.9217		12	0.8017	0.7376
2.2	1.1377	1.8258		13	0.7922	0.7243
2.4	1.1066	1.7373		14	0.7836	0.7134
2.6	1.0803	1.6559		15	0.7756	0.7045
2.8	1.0579	1.5812		16	0.7883	0.6971
3.0	1.0385	1.5126		32	0.6939	0.6462
3.2	1.0214	1.4499		64	0.6262	0.6033
3.4	1.0063	1.3926		128	0.5634	0.5528
3.6	0.9928	1.3401		256	0.5056	0.5006
3.8	0.9807	1.2922		512	0.4528	0.4505
4.0	0.9696	1.2485				
5.0	0.9265	1.0797				
6.0	0.8960	0.9694				

SECTION IV

INPUT FOR GUN PROPELLANT PROGRAM

The input data for the gun propellant program (Appendix I) can be divided into four general groups having code names as follows:

- 1) Thermodynamic data for the reaction products (THERMØ data).
- 2) Data pertaining to the reactants or propellants (REACTANTS data).
- 3) Special options related to chemical species present in the combusted gas (ØMIT/INSERT data).
- 4) Namelist data including the type of problem, pressure ratio and area ratio schedules, various options, etc. (NAMELISTS data).

The required order of the data cards is:

- 1) One card with the code word THERMØ punched in columns 1 to 6.
- 2) THERMØ data.
- 3) REACTANTS card. Number of reactants right adjusted in columns 1 to 3 and number of cases right adjusted in columns 4 to 6.
- 4) ØMIT and/or INSERT data.
- 5) One card containing up to 80 columns of alphanumeric identification data.
- 6) NAMELISTS data.

For any particular problem there may be multiple REACTANTS cards. Each set of REACTANTS cards may be followed by multiple NAMELISTS input cards. Each type of input data is discussed in detail in the following sections.

1. THERMØ DATA

The thermodynamic data for the reaction products may be read either from cards or from magnetic tape. When tape input is used, both the THERMØ code card and all THERMØ data cards must be omitted. It is anticipated that most users will prefer the magnetic tape since this reduces the number of cards which must be handled. The card format for the THERMØ data is described in Section V. Use of the tape input requires no action on the part of the user, once the required data is established on the tape.

2. REACTANTS DATA

REACTANTS data is required for all problems. Following the code card there should follow one card for each reactant species being considered, with a maximum of 15 allowed. Each reactant card, after the code card, contains the following information:

- a. The chemical formula for the species.
- b. Either the number of moles of the reactant or the relative weight. The relative weight is the weight of each fuel or oxidizer expressed as a fraction of the total fuel or oxidizer.
- c. The enthalpy of the species expressed in calories per mole. (This is not required for an assigned temperature problem. See Section IV.4 for description of assigned temperature problem.)
- d. The state of the reactant (gas, liquid, or solid).
- e. The temperature associated with the enthalpy.
- f. Designation of each reactant species as either a fuel or an oxidizer. (The program then combines all fuels into an effective fuel and all oxidizers into an effective oxidizer.)
- g. The reactant species density. (This information is optional and may be omitted. If densities are input for all reactants, the program calculates a density for the overall system.)
- h. Multiple cases with identical reactants are identified by the reactants code card and the preceding data need not be repeated.

The reactant information is arranged on a card. Standard chemical alphabetic symbols are required for the chemical elements (i.e., H for hydrogen, HE for helium, LI for lithium, BE for beryllium, etc.). Each reactant may be composed of no more than five distinct chemical elements. Each chemical element is allowed two columns (columns 1 and 2, 10 and 11, 19 and 20, 28 and 29, and 37 and 38) for its symbol. For those elements whose symbol consists of a single letter, the symbol must be placed in the left-most (left adjusted) of the two columns. The formula number (the number of atoms of each element in a reactant) is to appear in the columns immediately following the chemical symbol (i.e., columns 3 to 9, 12 to 18, 21 to 27, 30 to 36, and 39 to 45). The formula number may appear anywhere within the seven column field, and a decimal point must be used for each number. Note that the exponent numeric form, or E format, may not be used here. Also note that for a given reactant an individual element may appear only once (empirical formula). Thus, a compound such as furfuryl alcohol, whose formula might be written as $C_4H_3O \cdot CH_2OH$ to represent its structure, must be treated as though it were $C_5H_6O_2$ or $O_2H_6C_5$, etc. The order of the elements is immaterial for this program.

The relative weight of each reactant should be placed in columns 46 to 52. The number may appear anywhere in these columns, a decimal point must be used, and the exponent numeric form may not be used. If the number of moles of each species is input in these columns the same restrictions apply, but an additional bit of information, an M in column 53, must

appear on the card. Column 53 is left blank for relative weights. Note that the relative weight and molar designations may not be mixed for any single problem.

The reactant enthalpy is placed in columns 54 to 62, and the units must be calories per mole. The number may appear anywhere in these columns, a decimal point must be used, and the exponent numeric form may not be used. A sign is required only if the enthalpy is negative. Obviously, this enthalpy must be consistent with the enthalpy base used for the THERMØ data. For the JANAF data, the enthalpy base is as follows: For each element, the phase, condensed or liquid, which is most stable at one atmosphere pressure is designated as a reference, or base, state. The heat of formation of this state at 298.15°K is arbitrarily specified as zero. Then all thermodynamic properties for other phases of the element, as well as for any compound containing the element, are referenced to the base state.

The initial state for each reactant is indicated by an S for solid, an L for liquid, or a G for gas in column 63. The initial reactant temperature, in degrees Kelvin, goes in columns 64 to 71. Both the initial state and temperature are used only to label the output printout and if they are omitted or input incorrectly, the calculations are not affected.

For all problem types (see Section IV.4) except a detonation problem, columns 73 to 79 are reserved for the reactant density in grams per cubic centimeter. The inputting of this data is optional, but if it is given, a decimal point must be used. For a detonation problem, columns 73 to 80 are used for the reactant specific heat at constant pressures. This data is required for each reactant for a detonation problem.

3. ØMIT/INSERT DATA

The purpose of the ØMIT/INSERT option is as follows. The program considers as possible products all species in the THERMØ data which are consistent with the chemical system which was input on the REACTANTS cards. Occasionally, it may be desired to eliminate one or more species from consideration as possible products. This may be accomplished by placing the species chemical formula on an ØMIT card. Both gaseous and condensed species may be omitted.

Only the names of condensed species may appear on an INSERT card. The INSERT option has been included for two reasons. The less important of the two is that if it is known beforehand that one or more particular condensed species will be among the final equilibrium composition for the first assigned point (i.e., the combustion chamber for a rocket problem), then a small amount of computer time can be saved by using an INSERT card. The more important reason for the INSERT option is that, in rare instances, it is impossible to obtain convergence without the use of an

INSERT card. This occurs when, by considering gases only, the temperature becomes extremely low. When this happens, the program outputs the following message: "LOW TEMPERATURE IMPLIES CONDENSED SPECIES SHOULD HAVE BEEN INCLUDED ON AN INSERT CARD" and no solution will be obtained. The user should resubmit the problem with one or more appropriate condensed species listed on an INSERT card.

The use of OMIT and INSERT cards is completely optional; however when used, each card must contain either the code word OMIT in columns 1 to 4 or INSERT in columns 1 to 6 and the chemical formulas of from one to four product species. The names of the species must be left-adjusted and begin in columns 16, 31, 46, or 61. In addition, the species name must be punched on the card exactly as it appears in the THERMO data. This means that the order of the chemical elements within the species name, the formula numbers, and the state of the species must all be identical. For example, gaseous ammonia would commonly appear as NH_3 . Because of the alphabetizing scheme used for thermodynamic data, this species is written as H3N1(G).

4. NAMELISTS DATA

The word NAMELIST is a FORTRAN IV statement and provides a convenient way of inputting data. One of the major advantages of the NAMELIST input method is that the data can be placed in any order and need not be placed within pre-specified card columns as is the case for the REACTANTS data. A secondary advantage is that the variable name appears with its numerical value on a card, thus making it easy to tell the purpose of each piece of data without having to refer to a program manual or to the program listing. Even though inputting data by means of NAMELIST is convenient, the following rules must be observed.

All data input by means of a NAMELIST statement must be associated with a NAMELIST name, and for this program there are only two: INPT2 and RKTINP. The first column of all NAMELIST data cards may not be used and must be blank. The second column of the first card only must contain a \$ character. The applicable NAMELIST name must be placed on the first card only. The name must begin in column 3, and must be followed by at least one blank column.

Each NAMELIST name is assigned a group of FORTRAN variables. (The variables belonging to INPT2 and RKTINP are listed in Tables V and VI, respectively.) These variables are assigned to a NAMELIST name within the program, and numeric data can only be input in conjunction with a NAMELIST name.

Although, in general, there are seven forms that input data may take, only three are of interest for this report. These are integer constants,

real number constants, and logical constants. These are defined as follows:

- a. An integer consists of one to eleven digits written without a decimal point.
- b. A real number constant may be written in two ways. The first form is from one to nine digits, including a decimal point, followed by an exponent. The exponent is written as the letter E followed by a sign and a one or two digit integer. For example 12345. could be written as 1.2345E04 or .12345+5, etc. The second form is one to nine digits, including a decimal point, but not followed by an exponent.
- c. A logical constant may be either true or false. There are two forms in which the constant may be written. These are either .TRUE. or T .FALSE. or F. The periods before and after the long forms are mandatory.

Logical constants may be associated only with logical variables. Integer constants may be associated with real variables and vice versa, and the proper conversion is made automatically by the computer. Note that when inputting data without a NAMELIST statement this conversion may cause difficulties and should only be used with great care.

On a NAMELIST card, each piece of data must be written in conjunction with its variable name (e.g., P = 100; or INDEX = 3, or PSIA = .TRUE., etc.). The equal sign is mandatory, and the data items must be separated by commas. If more than one card is required, the last item on each card, except for the last card, must be a constant followed by a comma. A variable name may not be the last item on the card. The end of a group of data is signaled by a \$ character. This may be on the same card as that containing the NAMELIST name if only one card is used or may be on any succeeding card, but it may not be the first character on a succeeding card. Note that it is not necessary to completely fill a card with data before beginning a subsequent card. In fact, the user may want to put each piece of data on separate cards. This facilitates subsequent data changes. One final note, it is not necessary to input data for every variable contained in a NAMELIST; however, each variable has been assigned a value within the program, and this value is used unless superseded by input data. The assigned values for all NAMELIST variables in this program are included in Tables V and VI.

To illustrate the preceding instructions, the following paragraphs discuss the specific NAMELIST data required by this program, what each data bit does, and then some specific examples.

The INPT2 NAMELIST data must be used for all problems. The variables in the INPT2 NAMELIST are listed and defined in Table V along with the type and assigned value of each variable. The type of problem (one of either TP, HP, RKT, or DETN), at least one pressure (P), and the relative amounts of fuel and oxidizer (i.e., one of either EQRAT, OF, FPCT, or FA) are required for each problem. The other variables are either completely optional or may be required only if a particular problem type is requested.

The variable JANF is a flag to indicate which thermodynamic data polynomial should be used. JANF=0 designates a polynomial of the form $C_p = A_1 + A_2T + A_3T^2 + A_4T^3 + A_5T^4$. This is the form used by the Lewis Research Center and is also the form the Armament Laboratory uses after converting the JANAF data.

The Lewis program is quite flexible in the type of problems it will consider or the thermodynamic variables which may be fixed. For gun propellant problems, it is most advantageous to assign the enthalpy and pressure which, in system nomenclature, constitutes an RKT problem.

a. RKT Problem

If RKT = .TRUE. or T, then a rocket problem is solved. A rocket problem is one for which the combustion takes place at an assigned enthalpy (REACTANTS cards) and assigned pressure (single value in the P variable), followed by an isentropic expansion. The combustion temperature, the thermodynamic properties and rocket performance are calculated for the chamber, the throat, and assigned exit points. The exit points desired are specified in the RKTINP namelist. If a temperature is assigned (T variable), then combustion will be assumed to occur at that temperature and not at the assigned enthalpy. The RKT problem type combines the H,S and T,S problems of the earlier program version. Note that, when this option is selected, the second set of NAMELIST data, RKTINP, is then required. The combustion gas conductivity and viscosity are computed for this option only.

b. DETN Problem

If DETN = .TRUE. or T, then the program solves a Chapman-Jouget detonation problem. The thermodynamic properties and composition downstream of the detonation wave are calculated for an assigned pressure and temperature upstream of the wave. This detonation calculation is primarily oriented for gas phase detonations. It is of limited utility for computation of detonations in solids, as the specific heat polynomial of the reactants must be on the data tape, which will not, in general, be the case for a typical solid explosive constituent ingredient.

c. P, PSIA, and MMHG Variables

The value P may be either the combustion pressure of a rocket engine (RKT problem) or a pressure at which composition and thermodynamic properties (TP or HP problem) are desired. Up to 26 values may be input, but only one is permitted for an RKT problem. The program assumes that the units of the pressures are in atmospheres unless either PSIA or MMHG are set true. If PSIA = .TRUE. or T then the pressure units are assumed to be in psia units. If MMHG = .TRUE. or T then the pressure units are assumed to be in millimeters of mercury. PSIA and MMHG may not both be set true in the same problem.

d. T Variable

Values for the T variable should be input only if TP is set true or if an assigned chamber temperature is desired for RKT problem. The temperature units must be degrees Kelvin.

e. EQRAT, ØF, FPCT, and FA Variables

The relative amounts of total fuel and total oxidizer may be expressed in one (and only one for each problem) of four ways. The mixture ratio (ØF) and percent fuel (FPCT) are self evident. The fuel-to-air weight ratio (FA) and equivalence ratio (EQRAT) are new to this version of the program and are not of use for gun propellant calculations.

f. IDEBUG Variable

If IDEBUG = .TRUE. or T then a printout of the intermediate calculation details is obtained. This is intended primarily as a debugging aid in the event there are problems. The output is extensive and is explained on page 34 of Reference 1.

g. IØNS Variable

If IØNS = .TRUE. or T then the program will consider ionized species. The earlier Lewis program version could not handle ionic species although provision was made in one of the subroutines for future consideration of ions. This capability is included in the newer program and thermodynamic data for ionized species are available as well as a sample problem which uses IØNS = T.

h. EQL, FRØZ, PCP, SUBAR, and SUPAR Variables

The five RKTINP variables (EQL, FRØZ, PCP, SUBAR, and SUPAR) in the RKTINP namelist are listed in Table VI. Of these, only PCP is required. The RKTINP namelist is required only if RKT is set true in the INPT2 namelist.

(1) PCP Variable

The value PCP is the ratio of the chamber pressure to the exit pressure. This is one of the independent variables (along with the entropy) for the nozzle portion of a rocket problem, and as such, at least one value must be input. As many as 22 values may be input; however, unlike the older program, values for the chamber and throat should not be input. Pressure ratios for the subsonic portion of the nozzle may be used. Values must be ordered so that the magnitudes increase monotonically.

(2) SUBAR and SUPAR Variables

Gun propellant performance at specific area ratios corresponding to a given gas velocity, either subsonic or supersonic, may be requested. Subsonic ratios are read as SUBAR and supersonic as SUPAR. When assigned area ratios are requested, the range of PCP values should be large enough to include the assigned area ratios. If the range is not large enough, extrapolation may be performed. SUBAR values should be ordered such that the values decrease and the SUPAR data should increase. Thirteen of each variable are permitted. Note that the use of this program feature is completely optional.

(3) EQL and FRØZ Variables

The program will calculate performance for both equilibrium and frozen expansions unless instructed otherwise. If EQL = .FALSE. or F then the equilibrium expansion is omitted and only frozen performance is calculated. If FRØZ = .FALSE. or F then the frozen expansion is omitted and only equilibrium performance is calculated.

TABLE V. VARIABLES IN INPT2 NAMELIST			
Variable Name	Variable Type	Value (Unless Set Differently)	Definitions
JANF	Integer	1.	Thermodynamic data polynomial indicator
P	Real	0.	Assigned pressures
T	Real	0.	Assigned temperatures
EQRAT	Real	0.	Equivalence ratio
ØF	Real	0.	Oxidant-to-fuel weight ratio
FPCT	Real	0.	Percent fuel by weight
FA	Real	0.	Fuel-to-air weight ratio
TP	Logical	False	Assigned temperature and pressure problem
HP	Logical	False	Assigned enthalpy and pressure problem
RKT	Logical	False	Rocket problem
DETN	Logical	False	Detonation problem
PSIA	Logical	False	Assigned pressure-to be in psia units
MMHG	Logical	False	Assigned pressures in millimeter of mercury units
IØNS	Logical	False	Consider ionic species
IDDEBUG	Logical	False	Print intermediate output

TABLE VI. VARIABLES IN RKTNP NAMELIST			
Variable Name	Variable Type	Value Unless Set Differently	Definition
EQL	Logical	True	Gun propellant performance assuming equilibrium composition to be calculated
FRQZ	Logical	False	Gun propellant performance assuming frozen composition to be calculated
PCP	Real	0.	Ratio of chamber pressure to exit pressure
SUBAR	Real	0.	Subsonic area ratios
SUPAR	Real	0.	Supersonic area ratios

Table VII contains the input data for several propellant performance cases, and the output is listed on Tables VIII through XI. These cases are respectively M-10 (Case 100), M-9 (Case 101), an HMX-rubber propellant system (Case 102), and an RDX-triamino-guanidine nitrate formulation (Case 106). A comparison of these data with experimental or independent theoretical solutions gives the following results.

	Case 100			
	Tv	Fp	γ	Mw
Lewis	3312	366,548	1.22	25.1
Experimental	3034	346,180	1.23	24.2
	Case 101			
Lewis	3853	394,180	1.17	27.2
Experimental	3840	396,840	1.20	26.5
	Case 102			
Lewis	2566	377,584	1.28	18.9
Other Theoretical	2545	373,000	(--)	18.9
	Case 106			
Lewis	2637	390,870	1.29	18.8
Other Theoretical	2647	391,000	(--)	18.8

The input data (Table VII) are discussed in the program writeup except that no OMIT or INSERT cards are used.

TABLE VII. INPUT DATA FOR SAMPLE GUN PROPELLANT PROBLEMS

3 1									
C 24.0	H 29.5	O 41.3	N 10.6	1.0	-643100.	298.	F		
C 12.0	H 11.0	N 1.0		.33	27600.	298.	O		
C 2.0	H 14.0	O 6.0	N 4.0	.67	-66300.	298.	O		
CASE 100 PROPELLANT IS M-10									
\$INPT2 JANF=0,P(1)=5000.,RKT=TRUE.,FPCT=98.,PSIA=TRUE.,\$									
\$RKTINP PCP(1)=1.2,1.4,1.6,2.0,3.0,4.0,5.0,10.0,68.0,FROZ=FALSE,\$									
4 1									
C 24.0	H 29.5	O 41.3	N 10.6	1.0	-643100.	298.	F		
C 3.0	H 5.0	O 9.0	N 3.0	.96	-85300.	298.	O		
C 12.0	H 11.0	N 1.0	N 4.0	.02	27600.	298.	O		
C 3.0	H 14.0	O 6.0		.02	-66300.	298.	O		
CASE 101 PROPELLANT IS M-9									
\$INPT2 JANF=0,P(1)=5000.,RKT=TRUE.,FPCT=58.,PSIA=TRUE.,\$									
\$RKTINP PCP(1)=1.2,1.4,1.6,2.0,3.0,4.0,5.0,10.0,68.0,FROZ=FALSE,\$									
2 1									
C 4.0	H 8.0	O 8.0	N 8.0	1.0	17900.	298.	O		
C 7.0	H 11.0	O .2	N .02	1.0	-5000.	298.	F		
CASE 102 PROPELLANT IS HMX RUBBER									
\$INPT2 JANF=0,P(1)=5000.,RKT=TRUE.,FPCT=15.,PSIA=TRUE.,\$									
\$RKTINP PCP(1)=1.2,1.4,1.6,2.0,3.0,4.0,5.0,10.0,68.0,FROZ=FALSE,\$									
3 1									
C 4.0	H 8.0	O 8.0	N 8.0	1.0	17900.	298.	O		
C 7.0	H 11.0	O .2	N .02	.88	-5000.	298.	F		
T 11.0				.12	0.	298.	F		
CASE 103 PROPELLANT IS HMX-RUBBER WITH TITANIUM ADDED									
\$INPT2 JANF=0,P(1)=5000.,RKT=TRUE.,FPCT=17.,PSIA=TRUE.,\$									
\$RKTINP PCP(1)=1.2,1.4,1.6,2.0,3.0,4.0,5.0,10.0,68.0,FROZ=FALSE,\$									
4 1									
C 2.0	H 5.0	O 1.0	N 3.0	.83	22500.	298.	F		
C 4.0	H 6.0	N 4.0		.17	52400.	298.	F		
C 3.0	H 6.0	O 6.0	N 6.0	.60	14900.	298.	O		
C 1.0	H 9.0	O 3.0	N 7.0	.40	-11500.	298.	O		
CASE 106 PROPELLANT IS RDX-TAG NITRATE									
\$INPT2 JANF=0,P(1)=5000.,RKT=TRUE.,FPCT=16.,PSIA=TRUE.,\$									
\$RKTINP PCP(1)=1.2,1.4,1.6,2.0,3.0,4.0,5.0,10.0,68.0,FROZ=FALSE,\$									

TABLE VIII. OUTPUT FOR CASE 100, M-10 PROPELLANT

THEORETICAL GUN PROPELLANT PERFORMANCE ASSUMING EQUILIBRIUM COMPOSITION DURING EXPANSION														
PC = 5000.0 PSIA														
CASE 100 PROPELLANT IS M-10														
CHEMICAL FORMULA														
FUEL	C 24.00000	H 29.50000	O 41.30000	N 10.60000										
OXIDANT C	12.00000													
OXIDANT C	2.00000													
O/F= .0204 PERCENT FUEL= 98.0000 EQUIVALENCE RATIO= 1.5547 DENSITY= 0.0000														
WT FRACTION ENTHALPY STATE TEMP DENSITY														
(SEE NOTE) CAL/MOL DEG K G/CC														
1.0000	1.788	1.200	1.400	1.800	2.000	3.000	4.000	5.000	10.000	18.000	34.02	58.000		
340.2	190.3	283.5	243.0	212.5	170.1	113.4	85.06	68.05	34.02	5.003				
2713	2443	2625	2553	2491	2391	2217	2101	2015	1766	1227				
-562.7	-681.0	-601.2	-632.7	-659.3	-702.4	-776.2	-825.3	-861.6	-965.0	-1189.2				
2.2442	2.2442	2.2442	2.2442	2.2442	2.2442	2.2442	2.2442	2.2442	2.2442	2.2442				
25.125	25.137	25.130	25.133	25.135	25.138	25.141	25.143	25.143	25.144	25.148				
-1.00052	-1.00022	-1.00040	-1.00032	-1.00026	-1.00019	-1.00010	-1.00007	-1.00005	-1.00003	-1.00003				
1.0096	1.0040	1.0074	1.0058	1.0047	1.0033	1.0017	1.0010	1.0007	1.0003	1.0037				
.4447	.4313	.4398	.4362	.4334	.4294	.4239	.4209	.4191	.4152	.4239				
1.2206	1.2263	1.2226	1.2241	1.2253	1.2272	1.2300	1.2316	1.2320	1.2352	1.2307				
1046.8	995.0	1030.5	1016.7	1004.8	985.1	949.7	925.1	906.2	849.4	786.6				
0.000	1.000	.951	.753	.895	1.098	1.408	1.603	1.745	2.168	3.240				
0.0	3264.4	1061.8	2511.7	2950.7	3547.5	4385.6	4863.7	5188.8	6819.9	7512.1				
.000795	.000738	.000777	.000762	.000749	.000727	.000690	.000665	.000656	.000591	.000468				
.000300	.000281	.000294	.000289	.000285	.000278	.000266	.000256	.000251	.000234	.000201				
3312														
36654.8.														
GSTAR, FT/SEC														
CF	4760	4760	4760	4760	4760	4760	4760	4760	4760	4760				
AE/AT	.686	.391	.528	.528	.820	.745	.921	1.022	1.090	1.265				
IVAG, LB-SEC/LB	1.000	1.266	1.065	1.011	1.008	1.134	1.292	1.452	2.194	8.385				
I, LB-SEC/LB	184.2	213.9	190.5	185.1	184.8	192.3	199.0	204.2	219.2	251.5				
	101.5	57.9	78.1	78.1	91.7	110.3	136.3	151.2	161.3	187.1				

TABLE VIII. Concluded

MOLE FRACTIONS													
CH ₄	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000
CO	.40188	.39739	.40060	.39943	.39834	.39637	.39229	.38996	.38611	.37568	.33827	.00000	.00000
CO ₂	.13746	.14238	.13868	.14019	.14130	.14339	.14339	.13991	.13978	.16431	.20966	.00000	.00000
H	.00104	.00046	.00082	.00066	.00054	.00039	.00020	.00012	.00000	.00002	.00000	.00000	.00000
H ₂	.00001	.00001	.00001	.00001	.00001	.00001	.00001	.00001	.00000	.00000	.00000	.00000	.00000
H ₂ O	.00016	.00066	.00013	.00011	.00009	.00007	.00004	.00002	.00002	.00001	.00000	.00000	.00000
NH ₃	.10392	.10883	.10739	.10664	.10781	.10990	.11415	.11753	.12044	.13101	.17615	.00000	.00000
N ₂	.23507	.23088	.23392	.23283	.23180	.22989	.22585	.22253	.21968	.20916	.16394	.00000	.00000
NO	.00003	.00003	.00003	.00003	.00003	.00003	.00002	.00002	.00002	.00002	.00002	.00002	.00002
N ₂ O	.00005	.00001	.00004	.00002	.00002	.00001	.00000	.00000	.00000	.00000	.00000	.00000	.00000
OH	.11974	.11983	.11978	.11980	.11982	.11984	.11986	.11987	.11987	.11987	.11989	.00000	.00000
ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN .00005 FOR ALL ASSIGNED CONDITIONS	.00061	.00019	.00043	.00032	.00024	.00015	.00006	.00003	.00001	.00000	.00000	.00000	.00000
C													
C ₂ H ₄	C ₂ H ₆	C ₂ H ₂	C ₂ H ₄	C ₂ H ₆	C ₂ H ₂	C ₂ H ₄	C ₂ H ₆	C ₂ H ₂	C ₂ H ₄	C ₂ H ₆	C ₂ H ₂	C ₂ H ₄	C ₂ H ₆
NH ₂	N ₂	N ₂ O	N ₂ O	N ₂ O	N ₂ O	N ₂ O	N ₂ O	N ₂ O	N ₂ O	N ₂ O	N ₂ O	N ₂ O	N ₂ O
NOTE: WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS													
VISCOSITY AND CONDUCTIVITY VALUES BASED ON 99.8 PERCENT OF GAS MIXTURE													

THEORETICAL GUN PROPELLANT PERFORMANCE ASSUMING EQUILIBRIUM COMPOSITION DURING EXPANSION

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TABLE X. OUTPUT FOR CASE 102, HMX-RUBBER

THEORETICAL GUN PROPELLANT PERFORMANCE ASSUMING EQUILIBRIUM COMPOSITION DURING EXPANSION															
PC = 5000.0 PSIA															
CASE 102 PROPELLANT IS HMX-RUBBER															
CHEMICAL FORMULA															
OXIDANT C		4.00000		H		8.00000		O		8.00000		N		8.00000	
FUEL C		7.00000		H		11.00000		O		.20000		N		.02000	
O/F= 5.5667 PERCENT FUEL= 15.0000 EQUIVALENCE RATIO= 2.7550 DENSITY= 0.0000															
WT FRACTION ENTHALPY STATE TEMP DENSITY															
(SEE NOTE) CAL/MOL DEG K G/CC															
1.00000 17900.000 298.00 -0.0000															
1.00000 -5000.000 298.00 -0.0000															
CHAMBER															
PC/P	1.000	THROAT	EXIT	EXIT	EXIT	EXIT	EXIT	EXIT	EXIT	EXIT	EXIT	EXIT	EXIT	EXIT	EXIT
P, ATM	340.2	187.0	1.019	1.200	1.400	2.000	3.000	4.000	5.000	10.000	60.000	60.000	60.000	60.000	60.000
T, CP, DEG K	1995	1758	1918	263.5	243.0	212.6	170.1	113.4	68.05	34.02	5.003	5.003	5.003	5.003	5.003
H, CAL/G	43.8	-73.8	6.3	-24.2	-49.8	-91.0	-160.9	-207.0	-241.0	-337.8	-557.9	-557.9	-557.9	-557.9	-557.9
S, CAL/(G)(K)	2.4686	2.4686	2.4686	2.4686	2.4686	2.4686	2.4686	2.4686	2.4686	2.4686	2.4686	2.4686	2.4686	2.4686	2.4686
M, VOL WT															
(OLV/DLP) T	18.902	19.006	18.925	18.950	18.976	19.030	19.163	19.284	19.392	19.796	21.091	21.091	21.091	21.091	21.091
(OLV/DLP) P	-1.01474	-1.02159	-1.01644	-1.01815	-1.01982	-1.02299	-1.02975	-1.03507	-1.03932	-1.05817	-1.07938	-1.07938	-1.07938	-1.07938	-1.07938
CP, CAL/(G)(K)	1.0946	1.1603	1.1127	1.1309	1.1409	1.1639	1.2631	1.3303	1.3876	1.7060	2.2655	2.2655	2.2655	2.2655	2.2655
GAMMA (S)															
1.2863	1.2791	.3452	.5607	.5769	.6103	.6929	.8383	1.3712	2.3570	2.3570	2.3570	2.3570	2.3570	2.3570	2.3570
SON VEL, M/SEC	991.7	1.040.8	1.2854	1.2837	1.2817	1.2769	1.2642	1.2531	1.2438	1.1.103	1.1394	1.1394	1.1394	1.1394	1.1394
MACH NUMBER	0.000	1.000	.538	.738	.879	.980.7	934.5	903.3	880.2	809.4	693.4	693.4	693.4	693.4	693.4
VEL, FT/SEC	0.0	3253.6	1837.3	2476.8	2903.8	3484.2	4293.7	4752.8	5084.5	5862.5	7351.1	7351.1	7351.1	7351.1	7351.1
VISC, G/CM-SEC	.000604	.000555	.000588	.000576	.000565	.000548	.000521	.000504	.000493	.000469	.000416	.000416	.000416	.000416	.000416
C, CAL/G-SEC-K	.000391	.000357	.000380	.000371	.000364	.000351	.000331	.000317	.000307	.000285	.000249	.000249	.000249	.000249	.000249
T, CV, DEG K	2566														
IMPETUS															
377584.															
CSLAR, FT/SEC															
CF	.703	.397	.535	.628	.753	.928	1.027	1.095	1.267	1.267	1.591	1.591	1.591	1.591	1.591
AT/AT	1.000	1.290	1.072	1.014	1.006	1.123	1.279	1.431	1.584	1.584	1.907	1.907	1.907	1.907	1.907
IVAC, LB-SEC/LB	180.2	210.6	187.0	181.4	180.6	187.3	193.6	198.6	213.6	213.6	248.0	248.0	248.0	248.0	248.0
I, LB-SEC/LB	101.1	97.1	76.9	90.3	108.3	135.5	147.7	157.4	162.2	162.2	228.8	228.8	228.8	228.8	228.8

TABLE X. Concluded

MOLE FRACTIONS													
C(S)	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
CH3	.00003	.00001	.00002	.00002	.00001	.00001	.00001	.00000	.00000	.00000	.00000	.00000	.07542
CH4	.00418	.00735	.00494	.00571	.00649	.00605	.01175	.01508	.01030	.00000	.00000	.00000	.00000
CO	.00002	.00490	.00000	.00395	.00348	.00443	.00101	.00000	.00000	.00000	.00000	.00000	.00000
CO2	.00566	.00741	.00608	.00650	.00693	.00780	.00992	.01194	.01263	.00000	.00000	.00000	.02120
C2H2	.00002	.00001	.00002	.00001	.00001	.00001	.00001	.00001	.00001	.00000	.00000	.00000	.00000
C2H4	.00002	.00001	.00001	.00001	.00001	.00001	.00001	.00001	.00001	.00001	.00001	.00001	.00001
H	.00005	.00001	.00003	.00002	.00001	.00001	.00001	.00001	.00001	.00001	.00001	.00001	.00001
HCN	.00136	.00074	.00114	.00098	.00085	.00067	.00043	.00030	.00023	.00000	.00000	.00000	.00000
HCO	.00007	.00002	.00005	.00004	.00003	.00002	.00001	.00000	.00000	.00000	.00000	.00000	.00000
H2	.34336	.33076	.34237	.34127	.34009	.33764	.33162	.32616	.32141	.30765	.28640	.25793	.00000
H2O	.02193	.02248	.02165	.02105	.02210	.02266	.02413	.02545	.02656	.03329	.05793	.00000	.00000
NH3	.00065	.00056	.00062	.00060	.00057	.00054	.00049	.00045	.00042	.00033	.00015	.00000	.00000
N2	.21627	.21702	.21600	.21704	.21742	.21814	.21902	.22129	.22259	.22518	.22400	.00000	.00000
ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN .00005 FOR ALL ASSIGNED CONDITIONS													
C	CH	CH2	CN	CN2	C2	C2H	C2H2	C2N	C2N2	C2O	N2O	N2O2	N2O3
C3	H2O2	H2O2(l)	H2O2(s)	N	NH	NH2	NH3	NO	NO2	NO3	NO4	NO5	NO6
N2H4	N2O	N2O3	O	OH	O2								
NOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS													
VISCOSITY AND CONDUCTIVITY VALUES BASED ON 99.4 PERCENT OF GAS MIXTURE													

TABLE XI. OUTPUT FOR CASE 106, RDX-TRIAMINO GUANIDINE NITRATE

~~THEORETICAL GUN PROPELLANT PERFORMANCE ASSUMING EQUILIBRIUM COMPOSITION DURING EXPANSION~~

PC = 500.0 PSIA

CASE 136 PROPELLANT IS ROX-TAG NITRATE

CHEMICAL FORMULA	G	N	H	O	M	W	MI FRACTION (SEE NOTE)	ENTHALPY CAL/MOL	STATE	TEMP DEG K	DENSITY G/CC
FUEL C	2.00000	H	5.00000	O	1.00000	N	3.00000			298.00	-0.00000
FUEL C	4.00000	H	6.00000	O	4.00000	N				298.00	-0.00000
OXYLANT C	3.00000	H	6.00000	O	6.00000	N	6.00000			298.00	-0.00000
OXYDANT C	1.00000	H	9.00000	O	3.00000	N	7.00000			298.00	-0.00000
							.40000	-15000.000		298.00	-0.00000
							.60000	14000.000		298.00	-0.00000
							.17000	52000.000		298.00	-0.00000
							.83000	22500.000		298.00	-0.00000
										298.00	-0.00000

0/F=	2.3333	PERCENT FUEL=	30.0000	EQUIVALENCE RATIO=	2.6026	DENSITY=	0.0000
------	--------	---------------	---------	--------------------	--------	----------	--------

CHAMBER	THROAT	EXIT	EXIT	EXIT	EXIT	EXIT	EXIT
PC/P	1.003	1.826	1.000	1.000	2.000	3.000	4.000
P, ATM	340.2	186.4	283.5	243.3	212.6	170.1	113.4
T, CP, DEG K	2051	1795	1970	1904	1848	1759	1610
H, CAL/G	9.5	-24.9	58.7	27.1	.8	-42.0	-114.2
S, CAL/(G)(K)	2.5166	2.5166	2.5166	2.5166	2.5166	2.5166	2.5166
M, MOC WT (DLV/DLP) I	18.777	18.763	18.766	18.77	18.783	18.823	18.934
(DLV/DLT) P	-1.00316	-1.00507	-1.00393	-1.00443	-1.00561	-1.00943	-1.01395
CP, CAL/(G)(K)	1.0171	1.0359	1.0217	1.0249	1.0412	1.0794	1.1274
GAMA (S)	4.866	4.956	4.871	4.987	4.995	5.033	5.083
SON VEL, M/SEC	1.2855	1.2888	1.2871	1.2881	1.2886	1.2837	1.2748
MACH NUMBER	1081.0	1012.0	1063.0	1042.3	1001.7	915.6	822.7
VEL, FT/SEC	0.0	3320.3	3538	3737	3877	4093	4293
F/FSC, G/CM-SEC	0.00624	0.00568	0.00616	0.00592	0.00561	0.00528	0.00508
LAL/G-SEC-K	0.00401	0.00366	0.00390	0.00381	0.00361	0.00340	0.00326
I, CV, DEG K	2637	2637	2637	2637	2637	2637	2637
APETUS	390870.						

[illegible]

TABLE XI. Concluded

[illegible]

TABLE XII. THERMO DATA INPUT FORMAT FOR TITANIUM DIOXIDE

-62000.0	9	51	TITANIUM DIOXIDE (TiO2) IDEAL GAS									
298	300	400	500	600	700	800	900	1000				
10.838	10.858	11.820	12.548	13.079	13.464	13.746	13.957	14.117				
0.000	.020	1.156	2.376	3.659	4.987	6.348	7.734	9.138				
56.146	56.213	59.474	62.194	64.531	66.578	68.395	70.027	71.506				
1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	2000	2100	2200
3000	3100	3200	3300	3400	3500	3600	3700	3800	3900	4000	4100	4200
5000	5100	5200	5300	5400	5500	5600	5700	5800	5900	6000		
14.117	14.211	14.339	14.417	14.480	14.532	14.575	14.611	14.641	14.667			
14.690	14.709	14.725	14.741	14.754	14.765	14.776	14.785	14.793	14.800			
14.807	14.813	14.819	14.824	14.828	14.832	14.836	14.840	14.843	14.846			
14.849	14.852	14.854	14.856	14.858	14.860	14.862	14.864	14.866	14.867			
14.869	14.870	14.871	14.872	14.874	14.875	14.876	14.877	14.878	14.878			
14.879												
9.138	10.556	11.985	13.423	14.868	16.319	17.774	19.234	20.696	22.162			
23.630	25.099	26.571	28.045	29.519	30.995	32.472	33.950	35.429	36.909			
38.389	39.870	41.352	42.834	44.317	45.800	47.283	48.767	50.251	51.736			
53.220	54.705	56.191	57.676	59.162	60.648	62.134	63.620	65.107	66.593			
68.080	69.567	71.054	72.541	74.029	75.516	77.004	78.491	79.979	81.467			
82.955												
71.506	72.858	74.101	75.252	76.323	77.324	78.263	79.147	79.948	80.776			
81.529	82.246	82.931	83.586	84.213	84.816	85.395	85.953	86.491	87.010			
87.512	87.997	88.468	88.924	89.336	89.796	90.214	90.621	91.017	91.402			
91.778	92.145	92.503	92.852	93.194	93.528	93.854	94.174	94.487	94.794			
95.094	95.383	95.677	95.960	96.238	96.511	96.779	97.043	97.301	97.556			
97.806												

TABLE XIII. THERMO DATA OUTPUT FORMAT FOR TITANIUM DIOXIDE

TITANIUM DIOXIDE (TiO2) IDEAL GAS

HO = -62000.0

VALUES OF G
COEFFICIENTS ARE

~~36725340E+01~~ ~~10003020E-01~~ ~~11120307E-04~~ ~~49403359E-08~~ ~~67934354E-12~~ ~~32580921E+05~~ ~~79567663E+01~~
~~-33589155E-02~~ ~~54917462E-02~~ ~~15152376E-01~~

T CP CCP HT CHT ST CST DCP DHT DST

298. 10.838 10.838 0.000 0.100 56.146 56.146 .000 0.000 .000
 300. 10.850 10.866 .020 .022 56.213 56.219 .002 .002 .006
 400. 11.820 11.816 1.156 1.158 59.474 59.480 .004 .002 .006
 500. 12.540 12.540 2.376 2.377 62.194 62.194 .008 .001 .004
 600. 13.079 13.076 3.659 3.659 64.531 64.534 .003 .000 .003
 700. 13.464 13.465 4.987 4.987 66.578 66.581 .001 .000 .003
 800. 13.746 13.746 6.348 6.349 68.395 68.398 .000 .001 .003
 900. 13.957 13.958 7.734 7.734 70.027 70.030 .004 .000 .002
 1000. 14.117 14.118 9.138 9.138 71.506 71.509 .001 .000 .003

VALUES OF G
COEFFICIENTS ARE

.62406076E+01 .12046967E-02 -.50104624E-06 .85525393E-10 -.53125222E-14 -.32336518E+05 -.01070897E+01
 .95760211E-01 .22837632E-01 .10773479E+00

T CP CCP HT CHT ST CST DCP DHT DST

1000. 14.117 14.117 9.138 9.138 71.506 71.506 .000 .000 .000
 1100. 14.241 14.214 10.556 10.555 72.858 72.856 .027 .001 .002
 1200. 14.339 14.301 11.985 11.981 74.101 74.097 .038 .004 .004
 1300. 14.417 14.379 13.423 13.415 75.252 75.245 .038 .004 .002
 1400. 14.480 14.447 14.868 14.856 76.323 76.313 .033 .012 .010
 1500. 14.532 14.508 16.319 16.304 77.324 77.312 .024 .015 .012
 1600. 14.575 14.561 17.774 17.757 78.263 78.250 .014 .017 .013
 1700. 14.611 14.607 19.234 19.216 79.147 79.134 .004 .018 .013
 1800. 14.641 14.646 20.696 20.678 79.948 79.970 .005 .018 .022
 1900. 14.667 14.681 22.162 22.145 80.776 80.763 .014 .017 .013
 2000. 14.690 14.709 23.630 23.614 81.529 81.516 .019 .016 .013
 2100. 14.709 14.734 25.099 25.086 82.246 82.235 .025 .013 .011
 2200. 14.726 14.754 26.571 26.561 82.931 82.921 .028 .010 .010
 2300. 14.741 14.771 28.046 28.037 83.586 83.577 .030 .008 .009
 2400. 14.754 14.784 29.515 29.515 84.213 84.206 .030 .004 .007
 2500. 14.766 14.796 30.986 30.984 84.816 84.809 .030 .001 .007
 2600. 14.776 14.803 32.472 32.474 85.395 85.390 .027 .002 .005
 2700. 14.785 14.808 33.968 33.964 85.953 85.949 .024 .004 .004
 2800. 14.793 14.814 35.429 35.435 86.491 86.487 .021 .006 .004
 2900. 14.800 14.817 36.909 36.917 87.010 87.007 .017 .008 .003
 3000. 14.807 14.819 38.389 38.399 87.512 87.510 .012 .010 .002
 3100. 14.813 14.821 39.870 39.881 87.997 87.995 .008 .011 .002
 3200. 14.819 14.821 41.352 41.363 88.468 88.466 .002 .011 .002
 3300. 14.824 14.822 42.834 42.845 88.924 88.922 .002 .011 .002
 3400. 14.828 14.823 44.317 44.327 89.336 89.365 .005 .010 .029
 3500. 14.832 14.823 45.800 45.810 89.796 89.794 .009 .010 .002
 3600. 14.836 14.824 47.283 47.292 90.214 90.212 .012 .009 .002
 3700. 14.840 14.826 48.767 48.775 90.621 90.618 .015 .008 .003
 3800. 14.843 14.827 50.251 50.257 91.017 91.013 .016 .006 .004
 3900. 14.846 14.829 51.736 51.740 91.402 91.399 .017 .004 .003
 4000. 14.849 14.832 53.220 53.220 91.778 91.774 .017 .003 .004
 4100. 14.852 14.836 54.705 54.706 92.145 92.140 .017 .001 .005
 4200. 14.854 14.839 56.191 56.190 92.503 92.498 .015 .001 .005
 4300. 14.856 14.844 57.676 57.674 92.852 92.847 .012 .002 .005
 4400. 14.858 14.848 59.162 59.159 93.194 93.188 .010 .003 .006
 4500. 14.860 14.854 60.644 60.644 93.528 93.522 .006 .001 .006
 4600. 14.862 14.859 62.134 62.130 93.854 93.849 .003 .004 .005
 4700. 14.864 14.865 63.620 63.616 94.174 94.168 .001 .004 .006
 4800. 14.866 14.871 65.107 65.103 94.487 94.481 .005 .004 .006
 4900. 14.867 14.876 66.593 66.590 94.794 94.788 .009 .003 .006
 5000. 14.869 14.881 68.080 68.078 95.094 95.089 .012 .002 .005
 5100. 14.870 14.886 69.567 69.566 95.388 95.383 .016 .001 .005
 5200. 14.871 14.889 71.054 71.055 95.677 95.672 .018 .001 .005
 5300. 14.872 14.892 72.541 72.544 95.960 95.956 .020 .003 .004
 5400. 14.874 14.893 74.029 74.033 96.238 96.235 .019 .004 .003
 5500. 14.876 14.892 75.516 75.523 96.511 96.508 .017 .002 .003
 5600. 14.876 14.889 77.004 77.012 96.779 96.776 .013 .008 .003
 5700. 14.877 14.883 78.491 78.500 97.043 97.040 .006 .009 .003
 5800. 14.878 14.875 79.979 79.988 97.301 97.298 .003 .009 .003
 5900. 14.878 14.862 81.467 81.475 97.556 97.553 .016 .008 .003
 6000. 14.875 14.847 82.955 82.960 97.806 97.802 .032 .005 .004

TABLE XIV. DATA TAPE FORM FOR THERMØ DATA OUTPUT

T102	J 6/70T1	10	200	000	06	299.000	6000.000	1
C.62406876E+01	0.12846967E-02	-0.50184624E-06	0.85525393E-10	-0.53125222E-14				2
-0.3336518E+05	0.81878897E+01	0.30725348E+01	0.10883020E-01	-0.11120307E-04				3
0.49483359F-08	-0.67934354F-12	-0.32508921E+05	0.79567663F+01					4

SECTION V

THERMO DATA PROGRAM

The program (Appendix II) to fit the tabular JANAF thermochemical data to the Lewis polynomial is relatively simple and straightforward. JANAF data for Cp, H, and S is read in the tabular form for two temperature ranges 298° to 1,000°K and 1,000° to 6,000°K. The format is as shown in Table XII for the gas TiO₂. The first line consists of the reference heat of formation to 298°K in calories per mole, the number of points in the first temperature range and the number of points in the second temperature range, followed by a species identifier. The tabular temperature references for the first interval are then listed followed by the appropriate Cp, H, and S values. This sequence is then repeated for the second temperature range. Subsequent to data input, the program establishes a matrix which it solves by an inversion procedure to obtain the required polynomial constants. These constants are then output in the form suitable for inclusion on the Lewis program thermodynamic data tape.

The output is as shown on Table XIII for the TiO₂ species which is also shown on the input. The coefficients required on the data card for the first temperature range are shown on the first line followed by a comparison between the tabular data and the generated polynomials for the three functions of interest. It can be seen that the data fit is quite good. These data are followed by the required constants for the second temperature range and a similar comparison of polynomial and tabular results.

These results are read onto the data tape in the form shown on Table XIV. There are four cards per species. The first line consists of the empirical formula in columns 1 to 12. A gaseous species has no subscript, a liquid, has subscript L, and a solid, has subscript S. Columns 19 to 21 contain a code for the data source, in this case, a J for the JANAF tables. Columns 22 to 24 are the month and year of polynomial computation. The first through the fourth atoms in the species are inserted in columns 25 and 26, 30 and 31, 35 and 36, 40 and 41, while the respective number of atoms are placed in columns 27 to 29, 32 to 34, 37 to 39, and 42 to 44. Column 45 is used for the phase of the species G, L, or S. Columns 46 through 55 have the lower temperature bound at which the species exists with the upper temperature bound being placed in columns 56 through 65.

Cards 2, 3, and 4 contain the 14 polynomial constants, five each on cards 2 and 3 and four on card 4.

APPENDIX I
LEWIS PROGRAM LISTING

35
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		PROGRAM P1712 INPUT, OUTPUT, TAPES=INPUT, TAPES=OUTPUT, TAPES=4, TAPES=9	P1712	00002
	C	I E R P G REFERENCE PROGRAM ODE	P1712	00003
	C	DECK SEQUENCED BY SUBROUTINE	P1712	00004
	C	THERMODYNAMIC DATA FOLLOWS SOURCE DECK	P1712	00005
05	C	DATA FOR TEST CASES FOLLOWS THERMODYNAMIC DATA	P1712	00006
	C	PROGRAM USES TAPE UNIT 4 FOR THERMO DATA	P1712	00007
	C	ODE ICRPG REFERENCE PROGRAM	P1712	00008
	C	MAIN PROGRAM	P1712	00009
	C	UCUBLE PRECISION G.X	P1712	00010
	C	INTEGER DATA, ORIT, ENSERT, REAC, BLANK, THRM, END, SUB	P1712	00011
15	C	LOGICAL HP, SP, TP, IDEBUG, NEMR, IONS, MOLES, FROZ, E3L, PSIA, RKT	P1712	00012
	C	LOGICAL SHOCK, MPMG, PASCAL, EV, IC, DETN, CPCVFR, CPCVEG, SIUNIT, EUNITS	P1712	00013
	C	DIMENSION OMIT(2,3), NCD(4), ENSERT(13,3), LH(2), LVP(2), LVM(2)	P1712	00014
	C	COMMON/POINTS/HSUT(13), SSUM(13), CPR(13), DVTP(13), DULVPT(13)	P1712	00015
20	C	1, GAMHAS(13), P(26), T(26), V(13), PPP(13), MM(13), SONVEL(13), TIT(13)	P1712	00016
	C	2, TOTN(13)	P1712	00017
	C	COMMON/SPECES/CDEF(2,7,150), S(150), EN(150,13), ENLN(150), H3(150)	P1712	00018
	C	1, CELN(150), A(15,150), SUB(150,3), IUSE(150), TEMP(50,2)	P1712	00019
	C	COMMON/MISC/ENNSUMN, IT, SO, ATOM(3,101), LLMT(15), 80P(15,2)	P1712	00020
25	C	1, TM, TLOW, THIU, TH15H, PP, CPSUM, OF, EQRT, FPCT, R, R, RSUBU, AG(2), AM(2)	P1712	00021
	C	2, HPP(2), RHU(2), VMIN(2), VPLS(2), MP(2), DATA(22), NAME(15,5)	P1712	00022
	C	3, ANUM(15,5), PECHT(15), ENTH(15), FAZ(15), RTEHP(15), FOX(15), DENS(15)	P1712	00023
	C	4, RHOP, KYM(15), LCN, JANF	P1712	00024
	C	COMMON/DOUBLE/ G(20,21), X(20)	P1712	00025
30	C	COMMON/INDEX/ IDEBUG, CONVG, TP, HP, SP, HPSP, TPSP, MOLES, NP, NT, NPI, L, NS, XMAT, INAT, IGIN, J, NMOT, IP, NEMR, NSUB, NSUP, ITN, CPCVFR, CPCVEU	P1712	00026
	C	2, IONS, NC, NSERT, JSOL, JULIQ, KASE(14), NREAC, IC, IO2	P1712	00027
	C	COMMON/PERF/PCP(26), VRQC(13), SPIH(13), VAGI(13), SUBAR(13), SUPAR(13)	P1712	00028
35	C	1, CPRF(13), AEAT(13), CSTR, EGL, FROZ, SSO	P1712	00029
	C	EQUIVALENCE (OMIT, ENLN), (ENSERT, EN(1,3))	P1712	00030
	C	DATA MIT/4HOMIT/, BLANK/1H /, PSIA/4HPSIA/, REAC/4HREAC/.	P1712	00031
40	C	1 INPUT/4HINPU/, IE/1HE/, INSERT/4HINSE/, THRM/4HTHER/, END/3HEND/	P1712	00032
	C	DATA LH/4HL/, CA, 4HL/G /, LVP/2HJV+, 1H /, LVM/2HVM-, 1H /, NMLT/4HNAME/	P1712	00033
	C	NAMELIST/INPT2/JANF, P, T, EQRT, OF, FPGI, FA, TP, HP, SP, RKT	P1712	00034
	C	1, PSIA, MPMG, SHOCK, IONS, EV, V, DETN, CPCVFR, CPCVEG, IDEBUG	P1712	00035
	C	2, SIUNIT, EUNITS	P1712	00036
45	C	TLOW = 0.	P1712	00037
	C	NEMR = .FALSE.	P1712	00038
	C	DO 399 I=1,15	P1712	00039
50	C	DO 398 J=1,150	P1712	00040
	C	A(I,J) = 0.0	P1712	00041
	C	398 CONTINUE	P1712	00042
	C	399 CONTINUE	P1712	00043
	C		P1712	00044
	C		P1712	00045
	C		P1712	00046
	C		P1712	00047
	C		P1712	00048
	C		P1712	00049
	C		P1712	00050
	C		P1712	00051
	C		P1712	00052
	C		P1712	00053
	C		P1712	00054

55	1 WRITE(6,100) 1712 00555
	400 FORMAT(1P1) 1712 00556
	READ(5,1204) NREAC,NCASE,NSRT,NMIT 1712 00557
	1204 FORMAT(1P1) 1712 00558
	IF(NREAC.LE.1.OR.NCASE.LE.3) WRITE(6,1023) NREAC,NCASE 1712 00559
	1023 FORMAT(1H,'NO REACTANTS OR NO CASES SPECIFIED ON TYPE 1 DATA CARD 1712 00560
60	1, NREAC=1,13, NCASE=1,13) 1712 00561
	11 NMIT = 0 1712 00562
	NSRT = 0 1712 00563
	MOLES = .FALSE. 1712 00564
	CALL REACT 1712 00565
65	IF(L.CO.0) WRITE(6,52) 1712 00566
	52 FORMAT(1H,'ERROR IN REACTANT CARDS') 1712 00567
	C 1712 00568
	C 1712 00569
	C 1712 00570
70	IF(NSRT.LE.0) GO TO 205 1712 00571
	180 DO 195 K=1,NSRT 1712 00572
	READ(5,204) (DATA(J),J=1,15) 1712 00573
	WRITE(6,2045) (DATA(J),J=1,15) 1712 00574
	2045 FORMAT(1P1,3X) 1712 00575
75	2045 -OR-MAT(1X,5(3A4,3X)) 1712 00576
	DO 185 I=1,15,3 1712 00577
	IF (DATA(I).EQ.8LANK) GO TO 185 1712 00578
	NSRT = NSRT+1 1712 00579
80	INSERT(1,NSRT) = DATA(I) 1712 00580
	INSERT(2,NSRT) = DATA(I+1) 1712 00581
	INSERT(3,NSRT) = DATA(I+2) 1712 00582
	185 CONTINUE 1712 00583
	C 1712 00584
	C 1712 00585
85	C CHECK OMIT CARDS 1712 00586
	205 IF(NMIT.LE.0) GO TO 210 1712 00587
	DO 208 K=1,NMIT 1712 00588
	READ(5,204) (DATA(J),J=1,15) 1712 00589
	WRITE(6,2045) (DATA(J),J=1,15) 1712 00590
90	DO 208 I=1,15,3 1712 00591
	IF (DATA(I).EQ.8LANK) GO TO 208 1712 00592
	NMIT = NMIT+1 1712 00593
	OMIT(1,NMIT) = DATA(I) 1712 00594
	OMIT(2,NMIT) = DATA(I+1) 1712 00595
95	OMIT(3,NMIT) = DATA(I+2) 1712 00596
	208 CONTINUE 1712 00597
	NEWIR = .TRUE. 1712 00598
	C 1712 00599
	C 1712 00600
100	C BEGIN NAMELIST INPT2 1712 00601
	210 DO 300 NCS=1,NCASE 1712 00602
	DO 300 I=1,15 1712 00603
	CP(I) = 0. 1712 00604
	F(I) = 0. 1712 00605
105	T(I) = 0. 1712 00606
	V(I) = 0. 1712 00607

```

300 CONTINUE
V1 = 0.
V2 = 0.
RHOP = 0.
KASE = 0
IP = .FALSE.
HP = .FALSE.
SP = .FALSE.
RKT = .FALSE.
CPCVR = .FALSE.
CPCVEJ = .FALSE.
SHOCK = .FALSE.
DETN = .FALSE.
EV = .FALSE.
PASCAL = .FALSE.
MHG = .FALSE.
PSIA = .FALSE.
R = 1.987165
TR = 418.7
SIUNIT = .FALSE.
EUNITS = .FALSE.
IONS = .FALSE.
IDBUG = .FALSE.
FA = 0.
UF = 0.
EGRAT = 0.
FPCT = 0.
EGL = .TRUE.
READ(5,303)KASE
303 FORMAT(13A5,A2)
C20(5,INPT2)
DO 305 I=1,25
IF(P(I).EQ.0.) GO TO 322
NP = I
IF (MHG) P(NP) = P(NP)/760.
IF (PASCAL) P(NP) = P(NP)/101325.
IF PSCIA
P(NP) = P(NP)/14.696056
305 CONTINUE
322 IF (FA.NE.0.) OF = 1./FA
IF (EORAT.EQ.0.) GO TO 725
OF = (-EORAT*VMIN(2)-VPLS(2))/(VPLS(1)+EGRAT*VHIN(1))
GO TO 727
725 IF (OF.NE.0.) GO TO 727
IF (FPCT.EQ.0.) GO TO 9051
OF = (1.-FPCT)/FPCT
GO TO 727
9051 WRITE(6,724)
724 FORMAT(48HNO INPT2 VALUE GIVEN FOR OF, EGRAT, FA, OR FPCT )
727 WP(1) = OF
WP(2) = 1.
SUM = WP(1)+WP(2)
FPCT = 100.*WP(2)/SUM

```

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160 IF (EORAT.NE.0.) GO TO 745
    V2 = (WP(1)*VMIN(1)+WP(2)*VMIN(2))/SUM
    V1 = (WP(1)*VPLS(1)+WP(2)*VPLS(2))/SUM
    IF (V2.NE.0.) EORAT=ABS(V1/V2)
    745 DO 747 I=1,L
        80(I) = (WP(1)*BOP(I,1)+WP(2)*BOP(I,2))/SUM
    747 CONTINUE
    IF (EORAT.EQ.1.) EORAT= 1.000005
    IF (.NOT.(IONS.OR.L.NI(L).EQ.1E) GO TO 748
    L = L+1
    LL*1(L) = IE
    80(L) = 0.
    748 HSUB0 = (WP(1)*HPP(1)+WP(2)*HPP(2))/SUM
    WRITE (6,10PT2)
    WRITE (6,752)KASE
    752 FORMAT(1H0,13A6,A2/)
    WRITE (6,770)
    770 FORMAT(1H0,17X,4HFUEL,13X,7HOXIDANT,12X,7HMIXTURE //)
    780 FORMAT(1H0,24X,SEIS-87)
    WRITE (6,730) LH,HPP(2),HPP(1),HSUB0,LVP,VPLS(2),VPLS(1),V1,
    1LVM,VMIN(2),VMIN(1),V2
    HSUB0 = HSUB0/R
    WRITE (6,785)
    785 FORMAT(8H ATOMS/G )
    RHOP = WP(2)*RH0(1)+WP(1)*RH0(2)
    IF (RHOP.NE.0.) RHOP = (WP(1)+WP(2))*RH0(1)*RH0(2)/RHOP
    795 IF (NEWR) CALL SEARCH
    701 = L+1
    IF (NC.EQ.0) GO TO 790
    80 302 J=1,MS
    IF (IUSE(J).EQ.0) GO TO 302
    IF (IUSE(J).GT.0) IUSE(J) = -IUSE(J)
    IF (INSERT.EQ.0) GO TO 302
    00 301 I=1,MSERT
    IF (SUB(J,1).NE.INSERT(1,I)) GO TO 301
    IF (SUB(J,2).NE.INSERT(2,I)) GO TO 301
    IF (SUB(J,3).NE.INSERT(3,I)) GO TO 301
    INSERT(1,I) = 0.
    IQ1= I01+1
    IUSE(J) = -IUSE(J)
    301 CONTINUE
    302 CONTINUE
    NSERT = 1
    790 IIN= 35
    IC = .FALSE.
    PP = NS
    NPT = 1
    ENN = 1
    SUPN = ENN
    XI = NS - NC
    XI = ENN/XI
    XLN = AL9G(XI)
```

	00 432 J=I,NS	P1712 00214
	IF(IUSE(J),50,-10000) IUSE(J)=0	P1712 00215
215	EN(J,1) = 0,	P1712 00216
	ENLN(J)=0.	P1712 00217
	IF (IUSE(J),NE.0) GO TO 432	P1712 00218
	EN(J,1) = XI	P1712 00219
	ENLN(J) = XLN	P1712 00220
220	432 CONTINUE	P1712 00221
	JSL = 0	P1712 00222
	JLIQ = 0	P1712 00223
	IF(OETN) CALL DETON	P1712 00224
	IF(RKT) CALL ROCKET	P1712 00225
225	IF (TP) CALL HOLIER	P1712 00226
	IF (WP) CALL CMBSN	P1712 00227
	500 CONTINUE	P1712 00228
	GO TO 1	P1712 00229
	END	P1712 00230

[illegible]

SUBROUTINE CMO3YN

C

COMMON/POINTS/MSUM(13),SSUM(13),CPR(13),OLVTP(13),OLVPI(13)

1,CAM4AS(13),P(26),T(26),V(13),PPP(13),N(13),SONVEL(13),ITT(13)

2,TTN(13)

COMMON/SPFGES/CGEF(2,7,150),S(150),EV(150,13),ENLN(150),P(150)

1,TELT(150),TA(15,150),SUB(150,3),IUSE(150),TEPR(50,2)

COMMON/MISC/ENN,SUIN,TT,S0,ATOM(3,101),LLMT(15),BU(15),BOP(15,2)

1,TH,TLOW,THIO,THIEM,PP,CPSUM,OF,EORAT,EPT,R,RR,HSUB0,AC(2),AM(2)

2,PPP(2),R4U(2),VMIN(2),VPLS(2),NP(2),DATA(22),NAME(15,5)

3,ANUM(15,5),PECT(15),CNTH(15),FAZ(15),ATENP(15),FOX(15),DEMS(15)

4,RHOP,R4W(15),TLN,JANF

COMMON/INDX/IDEBUG,CONVG,IP,WP,SP,HPSP,TPSP,MOLES,NP,NT,NPT,LLNS,

1,KMAT,IMAT,ICI,N,J,NOMIT,IP,NEMR,NSUB,NSUP,ITA,CPCVFR,CPCVEG

2,IONS,NG,NSERT,JSOL,JLIG,KASE(14),NREAC,IC,I02

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SUBROUTINE CPHS

COMMON/SPECES/COEF(2,7,150),S(150),EN(150,13),ENLN(150),HQ(150)

1 .GELN(150),A(15,150),SUB(150,3),IUSE(150),TEMP(50,2)

COMMON/SC/ENN,SUMN,TT,S0,ATOM(3,101),LLMT(15),80(15),80P(15,2)

1 .TM, .OK,THID,THIGH,PP,CPSUM,OF,FORA,FPCT,R,R,HSUB0,AC(2),AM(2)

2 .PPPT(27),RHOT(27),VPLST(27),VPLST(27),DATA(27),NAME(15,5)

3 .ANUM(15,5),PECTH(15),FZ(15),RTEMP(15),FOX(15),DENS(15)

4 .RHOP,RMH(15),TLN,JANF

COMMON/INDX/ IDEBUG,CONVG,TP,HP,SP,HPSP,TPSP,MOLES,NP,NT,NPT,L,NS,

1 .KMAT,THAT,IQ1,N,J,NOHIT,IP,NEHR,NSUB,NSUP,ITN,CPCVFR,CPCVEQ

2 .IONS,NC,NSERT,JSOL,JIQ,ICASE(14),NREAG,IC,IQ2

K = 1

IF (TT.LF.TMID)K = 2

KK = 0

CPSUM=0.

90 IF (COEF(K,1,J).NE.0.)GO TO 97

IF (IUSE(J).LT.0) GO TO 100

KK = K

K = 1

IF (KK.EQ.1) K = 2

97 CONTINUE

IF (JANF.EQ. 0)GO TO 98

S(J)=COEF(K,1,J).TLN+COEF(K,7,J)=COEF(K,5,J)/2./TT/TT

1+(COEF(K,4,J)/3.0+TT+COEF(K,3,J)/2.0)*TT+COEF(K,2,J))*TT

HQ(J)=((COEF(K,4,J)/4.0)*TT+COEF(K,3,J)/3.0)*TT+COEF(K,2,J))*TT

1TT+COEF(K,1,J)-(COEF(K,5,J)/TT-COEF(K,6,J))/TT

CPSUM=CPSUM ((COEF(K,4,J)*TT+COEF(K,3,J))*TT+COEF(K,2,J))*TT

1+COEF(K,1,J)-COEF(K,5,J)/TT/TT)*EN(J,NPT)

GO TO 99

98 S(J) = (((COEF(K,5,J)/4.)*TT+ COEF(K,4,J)/3.)*TT+ COEF(K,3,J)/2.

1)*TT+COEF(K,2,J))*TT+ COEF(K,1,J)*TLN + COEF(K,7,J)

HQ(J) = (((COEF(K,5,J)/5.)*TT+ COEF(K,4,J)/4.)*TT+ COEF(K,3,J)/3.

1)*TT+ COEF(K,2,J)/2.)*TT+ COEF(K,1,J) + COEF(K,6,J)/TT

CPSUM= CPSUM+(((COEF(K,5,J)*TT+ COEF(K,4,J))*TT+ COEF

1)*TT+COEF(K,2,J))*TT+COEF(K,1,J))*EN(J,NPT)

99 CONTINUE

IF (KK.EQ.0) C. TO 100

K = KK

KK = 0

100 IF (J.EQ.NS) GO TO 200

J=J+1

GO TO 90

200 RETURN

ENC

SUBROUTINE DETON		P1712	00401
C		P1712	00402
C		P1712	00403
C	CHAP4AN-JOUUGUET DETONATIONS	P1712	00404
C		P1712	00405
05	LOGICAL HP,SP,TF,IOEBUG,NENR,IONS,MOLES,FROZ,EGL,PSIA,RKT	P1712	00406
	LOGICAL CPCVEG,CPCVFR,CALCH	P1712	00407
C		P1712	00408
	DIMENSION GM(13),CP(13),H1(13),PU3(13),TUB(13),GM1(13),RRHO(13)	P1712	00409
C		P1712	00410
10	COMMON/POINTS/HSUM(13),SSUM(13),CPR(13),OLYTP(13),OLVPT(13)	P1712	00411
	,GAMMA(13),PR26,T(26),V(13),PPP(13),MH(13),SONVEL(13),ITT(13)	P1712	00412
	,TOTN(13)	P1712	00413
	COMMON/SPECES/COEF(2,7,150),S(150),EN(150,13),ENLN(150),H0(150)	P1712	00414
15	1,CELN(150),A(15,150),SUB(150,3),TUSE(150),TEMP(50,2)	P1712	00415
	COMMON/MISC/EN,SUMN,IT,S0,ATOM(3,101),LLMT(15),80(15),80P(15,2)	P1712	00416
	1,TM,TLOM,THID,THIGH,PP,CPSUM,OF,EGRAT,FPCT,R,AR,MSUB0,AC(2),AM(2)	P1712	00417
	2,HRP(2),RHO(2),VHIN(2),VPLS(2),WP(2),DATA(22),NAME(15,5)	P1712	00418
	3,TRUM(15,5),RECMT(15),ENTH(15),FAZ(15),RTEMP(15),FOX(15),DEMS(15)	P1712	00419
20	4,RHOP,RMH(15),TLN,JANF	P1712	00420
	COMMON/INDX/ IDEBUG,CCNGV,TF,HP,SP,HPSP,TPSP,MOLES,NP,NT,NPT,L,NS,	P1712	00421
	1,KRAT,IRAT,IQI,N,J,NOMIT,IP,NENR,NSUB,NSUP,ITN,CPCVFR,CPCVEO	P1712	00422
	2,IONS,NC,INSERT,JSL,JLIG,KASE(14),NREAC,IC,I02	P1712	00423
	COMMON/PCRF/PCP(26),VMOC(13),SPIN(13),VAGI(13),SUBAR(13),SUPAR(13)	P1712	00424
25	4,CP2F(13),ALAT(13),CSIK,EGL,FROZ,SSU	P1712	00425
46	COMMON/CUPT/FRT(30),FP(4),FI(4),FH(4),FS(4),FV(4),FO(4)	P1712	00426
	1,FC(4),FG(4),FB,FMT13,F1,F2,F3,F4,F5,F(4),FMT19,FA1,FA2	P1712	00427
	2,FR1,FC1,FN(4),FR(4),FA(4),FI(4),FMT9X,F0	P1712	00428
		P1712	00429
30	EQUVALENCE(CP,DATA),(GM,SPIH),(H1,VAG1),(PUB,SUBAR),(TUB,SUPAR)	P1712	00430
	EQUVALENCE(GMI,AEAT),PCP(14),RRHO	P1712	00431
		P1712	00432
	DATA FT1/4HT1,0/,FP1/4HP1,A/,FH1/4HH1,C/,FM1/4HH1,M/	P1712	00433
35	1,FCP1/4HCP1,I/,FG1/4HA1,I/,FPP/4HP/P1/,FTT/4HT/T1/	P1712	00434
	2,FUG/4HDET,I/,FHM/4HR/M1/,FRA/4HRHD/I/,FRE/4HRH01/	P1712	00435
	3,FMA/4HHACH/I/,FMS/4H NO/I/,IZERO/2H00/	P1712	00436
		P1712	00437
	O(3)=A11*A22-A21*A12	P1712	00438
40	XX(7)=(B1*A22-E2*A12)/D(C)	P1712	00439
	YY(2)=(B2*A11-E1*A21)/D(C)	P1712	00440
C		P1712	00441
	NT=1	P1712	00442
	MSUB0=MSUB0*K	P1712	00443
	CALCH=.TRUE.	P1712	00444
45	IT=0.	P1712	00445
	IF(T(1).EQ.0.)T(1)=RTEMP(1)	P1712	00446
	DO 2 N=1,NREAC	P1712	00447
	IF(NAME(N,5).EQ.IZERO)CALCH=.TRUE.	P1712	00448
		P1712	00449
50	2 CONTINUE	P1712	00450
	OC 3 IT=1,26	P1712	00451
	IF (ITT).EQ.0.) GO TO 7	P1712	00452
	NT=IT	P1712	00453
	3 CONTINUE	P1712	00454

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55 7 IF (AM(1).NE.0.0) AND. AM(2).NE.0.0) GO TO 4
    AM1 = AM(2)
    IF (AM(2).EQ.0.0) AM1 = AM(1)
    GO TO 9
    4 AM1 = (MP(1)+MP(2))*AM(1)*AM(2)/(MP(2)*AM(1)+MP(1)*AM(2))
    3 CONTINUE
    60 DO 902 IT=1,N1
        TI = T/IT
        IF (CALCH) CALL HCALC
        CP1 = (MP(1)*AC(1)+MP(2)*AC(2))/(MP(1)+MP(2))
        DO 902 IP=1,NP
            PI = P/IP
            H1(NPI) = HSUB0
            TUB(NPI)=TI
            PUR(NPI)=PI
            CP(NPI) = CP1*P
            ITR= 0
            IT= 3600.
            PP1= 15.
            PP= PP1*PI
            HSUB0 = H1(NPI)/R + .75*TI*PP1/AM1
            TP = .FALSE.
            HP = .TRUE.
            CALL EOLDRM
            HSUB0 = H1(NPT)
            MP= .FALSE.
            IF (TI.EQ.0.) GO TO 1000
            GAP= GAMMAS(NPT)
            TI1= TI/TI
            II= 0
            TEM=TI1-.75*PP1/(CPR(NPT)*AM1)
            AMH=MH(NPT)/AM1
            IF (IDEBUG) WRITE(6,190)
            190 FORMAT(33HDETONATION VELOCITY CALCULATIONS /11X,4HP/PI,17X,4HT/11
                1)
            IF (IDEBUG) WRITE(6,203) II,PP1,TI1
            C
            200 DO 202 II=1,4
                ALFA=AMH/TI1
                PP1= (1.+GAM)* (1.+(1.-G.*GAM*ALFA/(1.+GAM))*2)**.5)/(2.*GAM*.LFA)
                RK=PP1*ALFA
                TIT= TEM+.5*PP1*GAM*(RK*RK-1.)/(AM1*CPR(NPT)*RK)
                IF (IDEBUG) WRITE(6,203) II,PP1,TI1
                203 FORMAT(15,2E20.8)
                202 CONTINUE
                TP= .TRUE.
                IT= TI*TI1
                AM1 = PP1*AMH/TI1
            C
            205 ITR= ITR+1
            PP= PP1*PP1
            CALL EOLDRM

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IF (NPT.EQ.0) GO TO 1000
*F (TT.EQ.0) GO TO 860
GAM= GAMAS(NPT)
IF (CP(CVFR)GAM= CP(RF(NPT)) / (CP(RF(NPT))-1./WM(NPT))
C IF (CP(CVEU)GAM= -GAMAS(NPT)*DLVPT(NPT)
AMP= AM(NPT)/AM1
KRI= PP1*AM/TT1
A11= 1./PP1 + GAM*RR1*DLVPT(NPT)
A12= GAM*RR1*DLVPT(NPT)
A21= .5*GAM*(RR1**2-1.-DLVPT(NPT)*(1.+RR1**2))*DLVPT(NPT)-1.
A22= -.5*GAM*DLVPT(NPT)*(RR1**2+1.)-WM(NPT)*CPR(NPT)
B1= 1./PP1-1.*GAM*(RR1-1.)
B2= WM(NPT)*(RSUM(NPT)-HI(NPT)/R)/TT-.5*GAM*(RR1*RR1-1.)
X1= XX(Y)
X2= YY(Z)
ALAM= 1.
TE4= X1
IF (TEM.LI.0.) TEM= -TEM
IF (X2.GT.TEN) TEN=X2
IF (-X2.GT.TEN) TE4= -X2
IF (TEM.GT.0.4) ALAM=.4/TEM
PP1= PP1*EXP(X1*ALAM)
TT1= TT1*EXP(X2*ALAM)
TT= TT1
US= (RR*GAM*TT/WM(NPT))**.5
UD= RR1*UG
IF (IDERUG) WRITE(6,10) ITR
10 FORMAT (21H0 ITERATION NUMBER=I2 )
IF (IDERUG) WRITE(6,30) PP1,TT1,RR1,X1,X2,US
30 FORMAT (6X,4HP/PI,10X,1H= E20.8/6X,4HT/TT, 10X,1H= E20.8/6X,8HRH0/R0
101.6X,1H= E20.8/6X,11HDEL IN P/PI,3X,1H=E20.8/6X,11HDEL IN T/TT,3X
2.1H=E20.8/6X,2HUS,12X,1H=E20.8)
C CONVERGENCE TEST
IF (ITR.LE.10 .AND. TEM.GT.0.5E-04) GO TO 205
KRM(NPT)=RR1
IF (CP(NPT).EQ.0.) GO TO 40
GM1(NPT)= CP(NPT) / (CP(NPT)-R/AM1)
VMCC(NPT)= UD/RR*GM1(NPT)*T1/AM1**.5
GO TO 41
40 GM1(NPT)= 0.
VMCC(NPT)= 0.
GO TO 150
C DERIVATIVES
41 IF (IDERUG) WRITE(5,55)
55 FORMAT (17H0 DERIVATIVE OF:13X,AMEN P,10X,AMEN T,10X,2H0D,
1 /9X,2HBY )
B1= 1./PP1-GAM*RR1
B2= GAM*RR1**2
X1= XX(Y)
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160 X2 = YY(2)
    AA = .5*(1.-OLVPT(NPT))
    88 = .5*OLVPT(NPT)
    OUC = UD*(AA*X1+BB*X2-1.)
    X1 = X1-1.0
    165 IF(IDERUG) WRITE(6,81) X1,X2,DUO
    81 FORMAT(6X,13HUNPT AT T1,M1,6X,M1=,3E17.8)
    B1 = GAM*RR1
    82 = -B1*RR1-MM(NPT)*CP(NPT)/(R*TT1)
    X1 = XX(Y)
    X2 = YY(Z)
    170 DUO = UD*(AA*X1+BB*X2+1.)
    X2 = X2-1.
    IF(IDERUG) WRITE(6,84) X1,X2,DUO
    84 FORMAT(6X,16HUNPT1 AT P1,M1,M1,3X,1H=3E17.8)
    B1 = 0.
    81 = -MM(NPT)/(R*TT1)
    X1 = XX(Y)+1000.
    X2 = YY(Z)+1000.
    DUO = UD*(AA*X1+BB*X2)
    180 IF(IDERUG) WRITE(6,85) X1,X2,DUO
    85 FORMAT(6X,20HUNPT1 AT T1,P1,M1 =3E17.8)
    C
    150 K = 0
    185 IF(17P.EQ.NPT.ND.IF-K-2.NF-OR-IT.EQ.0.) GO TO 830
    K = NPT
    IF(NPT.NE.13) GO TO 870
    C
    C OUTPUT
    C
    190 868 WRITE(6,5)
    5 FORMAT(1H1,42X,46HDETONTATION PROPERTIES OF AN IDEAL REACTING GAS )
    CALL OUT1
    WRITE(6,46)
    195 46 FORMAT(13H UNBURNED GAS//)
    FMT(4)=FMT13
    FMT(5)=F8
    FMT(7)=F4
    WRITE(6,FMT)FP1,FP(2),FB,FB,(PUB(J),J=1,NPT)
    FMT(7)=F2
    WRITE(6,FMT)FT1,FT(2),FB,FB,(TUB(J),J=1,NPT)
    WRITE(6,FMT)FM1,FM(2),FB,FB,(H1(J),J=1,NPT)
    80-56 I=.NPT
    V(I)=AM1
    SONVEL(I) = (RR*GM1(I)*TUB(I)/AM1)**.5
    205 56 CONTINUE
    FMT(7)=F3
    WRITE(6,FMT)FN1,F1(2),FM(3),FB,(V(J),J=1,NPT)
    FMT(7)=F4
    WRITE(6,FMT)FCP1,FC(2),FC(3),FC(4),(CP(J),J=1,NPT)
    WRITE(6,FMT)FG(1),FG1,FB,FB,(GM1(J),J=1,NPT)
    FMT(7)=F1
    WRITE(6,FMT){FL(I),I=1,4},{SONVEL(J),J=1,NPT}
```



```

215      WRITE(6,55)
55      FORMAT(11HBOURNED GAS//)
      FMT(4)=FMT(6)
      CALL OUT2
      WRITE(6,56)
68      FORMAT(22HDETENTIONATION PARAMETERS //)
      FMT(7)=F4
220      DO 70 I=1,NPT
          V(I)=PPF(I)/PUB(I)
          PCP(I)=IT(I)/TUB(I)
          SONVEL(I)=SONVEL(I)*RRHO(I)
70      CONTINUE
225      WRITE(6,FMT)FPP,FB,FB,FB,IV(I),J=1,NPT)
      WRITE(6,FMT)FIT,FB,FB,FB,PCP(J),J=1,NPT)
      DO 73 I=1,NPT
          V(I)=MM(I)/AM1
73      CONTINUE
      FMT(7)=F4
230      WRITE(6,FMT)FPM,FB,FB,FB,IV(I),J=1,NPT)
      WRITE(6,FMT)FRA,FR3,FB,FB,RRHO(J),J=1,NPT)
      WRITE(6,FMT)FMA,FMB,FB,FB,VMOC(J),J=1,NPT)
      FMT(7)=F1
235      WRITE(6,FMT) FUD,FL(2),FL(3),FL(4),(SONVEL(J),J=1,NPT)
          EQL=.TRUE.
      CALL OUT3
865      IF(K.EQ.0) GO TO 1000
      WRITE(6,865)
240      865      FORMAT(1M1)
          NPT = 0
          870      NPT = NPT + 1
      C
      C      SAVE COMPOSITIONS FOR ESTIMATES OF NEXT POINT
      C
245      DO 880 I = 1,NS
          EN(I,NPT) = EN(I,K)
880      CONTINUE
902      CONTINUE
250      1000      TP = .FALSE.
          RETURN
          ENC

```

P1712 00613
P1712 00614
P1712 00615
P1712 00616
P1712 00617
P1712 00618
P1712 00619
P1712 00620
P1712 00621
P1712 00622
P1712 00623
P1712 00624
P1712 00625
P1712 00626
P1712 00627
P1712 00628
P1712 00629
P1712 00630
P1712 00631
P1712 00632
P1712 00633
P1712 00634
P1712 00635
P1712 00636
P1712 00637
P1712 00638
P1712 00639
P1712 00640
P1712 00641
P1712 00642
P1712 00643
P1712 00644
P1712 00645
P1712 00646
P1712 00647
P1712 00648
P1712 00649
P1712 00650
P1712 00651
P1712 00652

55	IF(IQ1) GO TO 171 IF (.NOT. CONVG. OR .JSOL.EQ.0) GO TO 62 ENSOL = EN(JSOL,NPT) EN(JSOL,NPT) = EN(JSOL,NPT) + EN(JLQ,NPT) IUSE(JLQ) = -IUSE(JLQ) IQ1 = IQ1 - 1 DLVTP(NPT) = 0. CP(NPT) = 0. GAPAS(NPT) = 0. LOGV = .TRUE. 62 CALL MATRIX 65 NUMB = IEN - IENUMB + 1 IF(.NOT. CONVG) GO TO 67 IF (LOGV.AND. JSOL.EQ.0) GO TO 63 DO 182 I=1,L PRCH(I) = G(IQ1,I) 70 182 CONTINUE IF (.NOT. LOGV) GO TO 67 C C LCGV = .TRUE. -- SET UP MATRIX TO SOLVE FOR DLVPT C 75 63 G(IQ1,IQ2) = ENN IG = IQ1 - 1 DO 777 I = 1, IQ G(I,IQ2) = G(I,IQ1) 777 CONTINUE 80 67 IF (.NOT. IOEBUG) GO TO 72 WRITE(6,772) NUMB 772 FORMAT (11H0 ITERATION ,I3.6X,7HMATRIX //) DO 911 I=1,IMAT 911 WRITE (6,73) (G(I,K),K=1,KMAT) 72 IF (CONVG) IMAT=IMAT-1 ITST = IMAT CALL MGAUSD IF (ITST.NE.IMAT) GO TO 774 IF (.NOT. IOEBUG. OR. CONVG) GO TO 773 90 WRITE (6,73) (G(I,I),I=1,L) 373 FORMAT (7H0PI ,9(A4.10X)) WRITE (6,73) (X(I),I=1,IMAT) 73 FORMAT (9E14.0) 773- IF (.NOT. CONVG) GO TO 85 95 IF (LOGV) GO TO 171 174 SUM = 0. DO 175 J=1,L SUM = SUM + PRCH(J)*X(J) 175 CONTINUE DLVTP(NPT) = 1.4*G(IQ2,IQ1)/ENN - SUM/ENN - X(IQ1) CP(NPT) = G(IQ2,IQ2) DO 176 J=1,IQ1 CP(NPT) = CPR(NPT) - G(IQ2,J)*X(J) 176 CONTINUE LOGV = .TRUE. GO TO 62 105	P1712 00706 P1712 00707 P1712 00708 P1712 00709 P1712 00710 P1712 00711 P1712 00712 P1712 00713 P1712 00714 P1712 00715 P1712 00716 P1712 00717 P1712 00718 P1712 00719 P1712 00720 P1712 00721 P1712 00722 P1712 00723 P1712 00724 P1712 00725 P1712 00726 P1712 00727 P1712 00728 P1712 00729 P1712 00730 P1712 00731 P1712 00732 P1712 00733 P1712 00734 P1712 00735 P1712 00736 P1712 00737 P1712 00738 P1712 00739 P1712 00740 P1712 00741 P1712 00742 P1712 00743 P1712 00744 P1712 00745 P1712 00746 P1712 00747 P1712 00748 P1712 00749 P1712 00750 P1712 00751 P1712 00752 P1712 00753 P1712 00754 P1712 00755 P1712 00756 P1712 00757 P1712 00758
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C
C SINGULAR MATRIX
C
110      774 IF(.NOT.CONVG) GO TO 775
        WRITE(6,172)
172      FORMAT(23HDERIVATIVE MATRIX SINGULAR )
        IC = .TRUE.
        GO TO 171
115      775 IF (.NOT.HP.OR.NPT.NE.1.OR.NC.EQ.0.OR.IT.GT.100.) GO TO 371
        WRITE(6,874)
174      FORMAT(96HLOW TEMPERATURE IMPLIES CONDENSED SPECIES SHOULD HAVE
        196EN INCLUDED ON AN INSERT CARD, RESTART )
        GO TO 873
120      971 WRITE (6,74)
        74      FORMAT(16HOSINGULAR MATRIX)
        IF (IC) GO TO 973
        IF (ISING) GO TO 937
        NTZERO = 0
125      965 DC 970 JJ = 1, NS
        IF (IUSE(JJ)) 97C,968,967
        967 IF (EN(JJ,NPT).EQ.0.) GO TO 873
        GO TO 969
        969 IF (EN(JJ,NPT).NE.0.) GO TO 969
        EN(JJ,NPT) = SHALNC
        EN(JJ) = SHALC
        GO TO 970
        969 NTZERO = NTZERO+1
        970 CONTINUE
        IF (.NOT.IC) GO TO 971
        IC = .FALSE.
        GO TO 43
130      971 ISING = .TRUE.
        WRITE (6,776)
        776      FORMAT (9HORESTART)
        GO TO 43
        997 IF (NTZERO.NE.(I-1)) GO TO 873
        IF (FORMAT,67,1,00001,00K,ERROR,T,T,0.99999) GO TO 873
        EN=0.
        NEN = 0
        DO 83 I=1,L
        JEN=0
        DO 80 J=1,NS
        IF (EN(I,NPT).EQ.0.) GO TO 88
        IF (A(I,J).EQ.0.) GO TO 83
        IF (JEN.NE.0) GO TO 83
        JEN = J
        80      CONTINUE
        NEN = NEN+1
        EN(JEN,NPT) = 0.06447413JEN)
        83      CONTINUE
        IF (NEN.LT.NTZERO) GO TO 373
        CONVG = .TRUE.
        IC = .TRUE.

```

167	HSUM(NPT) = J. DO 84 J=1,NS IF (CN(J,NPT).EQ.0.) GO TO 84 ENN = EN(J,NPT)+ENH TEP = EN(J,NPT) ENLN(J) = ALOG(TEM) HSUM(NPT) = HSUM(NPT) + EN(J,NPT)*HU(J)	P1712 00612 P1712 00613 P1712 00614 P1712 00615 P1712 00616 P1712 00617 P1712 00618
165	84 CONTINUE TM = ALOG(PP/ENN) GO TO 43	P1712 00619 P1712 00620 P1712 00621 P1712 00622 P1712 00623
170	85 ITNUM8= ITNUM8-1 C C C OBTAIN CORRECTIONS TO THE ESTIMATES	P1712 00624 P1712 00625 P1712 00626 P1712 00627 P1712 00628 P1712 00629
175	KK = L + 1 OLNT= X(I02) IF (TP) OLNT=0. DO 101 J=1,NS IF (IUSEV(J)) I01=98,I00 9% DELN(J) = HQ(J)*OLNT-HC(J)+S(J)-ENLN(J)-TM*X(IG1) DO 99 K=1,L DELN(J)= DELN(J)+A(K,J)*X(K)	P1712 00630 P1712 00631 P1712 00632 P1712 00633 P1712 00634 P1712 00635
180	99 CONTINUE GO TO 101 100 DELN(J) = X(KK) KK = KK + 1 101 CONTINUE AMEDA= 1. AMBDAL= 1. SUM = X(I01)	P1712 00636 P1712 00637 P1712 00638 P1712 00639 P1712 00640 P1712 00641
185	IF (SUM.LT.0.) SUM=SUM IF (OLNT.GT.SUM) SUM=OLNT IF (-OLNT.GT.SUM) SUM=-OLNT DO 917 J=1,NS IF (IUSEV(J).NE.0) GO TO 917 IF (EN(J,NPT).GT.0.) AND DELN(J).GT.SUM SUM = DELN(J) IF (EN(J,NPT).NE.0.) OR DELN(J).LE.0.) GO TO 917 SUM1 = (-9.212-ENLN(J)+ENNL)/(DELN(J)-X(I01)) IF (SUM1.LT.0.) SUM1=-SUM1 IF (SUM1.LT.AMBDA1) AMBDAL = SUM1	P1712 00642 P1712 00643 P1712 00644 P1712 00645 P1712 00646 P1712 00647 P1712 00648 P1712 00649 P1712 00650 P1712 00651 P1712 00652 P1712 00653
190	917 CONTINUE IF (SUM.GT.2.) AMBDA=2./SUM IF (AMBDAL.LT.AMBDA1) AMBDA = AMBDAL IF (.NOT.IDE9UG) GO TO 111 WRITE(6,923) TT,ENN,ENNL,PP,PPLN,AMBDAL 923 FORMAT (3HJ1=E15.3,6H ENN=E15.3,7H ENNL=E15.3,5H PP=E15.3,7H PPLN=E15.3,8H AMBDA=E15.3) 1 7H PPLN=E15.3,8H AMBDA=E15.3) WRITE (6,924) 924 FORMAT (10H,18X,2HNT,12X,2HNLN,18X,9HDEL LN,10X,4HMT,RT,9X,4HMS07	P1712 00654 P1712 00655 P1712 00656 P1712 00657 P1712 00658 P1712 00659 P1712 00660 P1712 00661 P1712 00662 P1712 00663 P1712 00664
195	12,12X,6H-G0/RT,9X,5H-G/RT) DO 926 J=1,NS FNEG1 = S(J)-H0(J) FNEG2 = FNEG1	
200		
205		
210		

215	IF (IUSE(J).EQ.0) FNEG2=FNEG2-ENLN(J)*TH WRITE (6,325) SUB(J,1),SUB(J,2), 1SUB(J,3),EN(J,NPT),ENLN(J),DELN(J),H3(J),S(J),FNEG1,FNEG2 925 FORMAT (1X,3A4,7E15.5) 926 CONTINUE WRITE (6,110) 110 FORMAT (1H0)	P1712 00885 P1712 00866 P1712 00867 P1712 00868 P1712 00869 P1712 00870 P1712 00871 P1712 00872 P1712 00873 P1712 00874 P1712 00875 P1712 00876 P1712 00877 P1712 00878 P1712 00879 P1712 00880 P1712 00881 P1712 00882 P1712 00883 P1712 00884 P1712 00885 P1712 00886 P1712 00887 P1712 00888 P1712 00889 P1712 00890 P1712 00891 P1712 00892 P1712 00893 P1712 00894 P1712 00895 P1712 00896 P1712 00897 P1712 00898 P1712 00900 P1712 00901 P1712 00902 P1712 00903 P1712 00904 P1712 00905 P1712 00906 P1712 00907 P1712 00908 P1712 00909 P1712 00910 P1712 00911 P1712 00912 P1712 00913 P1712 00914 P1712 00915 P1712 00916 P1712 00917
220	C C C 111 SUM = 0. DO 113 J=1,NS 112 ENLN(J)=ENLN(J)+AMBDA*DELN(J) EN(J,NPT) = 0. IF (ENLN(J)-ENLN+SIZE).LE.0.) GO TO 113 EN(J,NPT) = EXP(ENLN(J)) SUM = SUM+EN(J,NPT) GO TO 113	
225	114 EN(J,NPT) = EN(J,NPT) + AMBDA * DELN(J) 115 CONTINUE SUMN = SUM IF (TP) GO TO 115 TLN= TLN+4130A*DLNT TLN = EXP(TLN) 115 ENLN = ENLN+AMBDA*X(IG1) ENN = EXP(ENLN) IF (LLHT(L).NE.1E) GO TO 116	
235	C C C CHECK ON REMOVING IONS DO 1116 J = 1,NS IF (A(L,J).EQ.0.) GO TO 1116 IF (EN(J,NPT).GT.0.) GO TO 116 1116 CONTINUE DO 1118 J=1,NS IF (A(L,J).NE.0.) IUSE(J) = -10000 1118 CONTINUE L = L-1 IG1 = IG1-1 GO TO 43	
245	C C C TEST FOR CONVERGENCE 116 IF (ITNU*8.EQ.0) GO TO 13 IF (AMBDA.LT.1.) GO TO 43 SUM = (ENN-SUMN)/ENN IF (SUM.LT.0.) SUM = -SUM IF (SUM.GT.0.5E-5) GO TO 43 DO 130 J=1,NS IF (IUSE(J).LT.0) GO TO 139 AA= DELN(J)/SUMN IF (AA.LT.0.) AA=-AA	
255		
260		
265		

```

129 IF (IUSE(J).EQ.0) XE= XEN(J,NPT)
130 CONTINUE
131 CONVG= .TRUE.
270 IF (IT.LT.1000000) WRITE(6,336) IT,NPT
306 FORMAT(17H) THE TEMPERATURE=12.4,26H IS OUT OF RANGE FOR PCINT,15)
IF (IT.NGT.1000000) GO TO 167
WRITE(6,973) IT,NPT
973 FORMAT(17H) 12,59H ITERATIONS DID NOT SATISFY CONVERGENCE REQUIRE
METS FOR THE POINT
15)
IF (.NOT.HP.OR.APV.NE.1.0) NC.EQ.0.0R.IT.GT.1000000 GO TO 873
WRITE(6,874)
IT= IT+1
RETURN
C
280 C CONVERGENCE TESTS ARE SATISFIED, TEST CONDENSED SPECIES.
C
C
160 IF (NC.EQ.0) GO TO 143
SIZE= N.
INC= 0
DO 170 J= 1,N5
IF (IUSE(J).EQ.0 .OR. IUSE(J).EQ.-10000) GO TO 170
INC= INC + 1
IF (IDERUG) WRITE(6,144) (SU3(J,I),I=1,3),TEMP(INC),TEMP(INC+2),
IUSE(J),TEMP(INC,NPT)
144 FORMAT (10H,144,2F10.3,3X,5H) IUSE=,14,215.7)
IF (TEMP(INC,NPT)) 146,146,159
146 IF (J.NE.JSOL .AND. J.NE.JLIQ) GO TO 147
JSOL= 0
JLIQ= 0
147 TOL= TOL - 1
EN(J,NPT)= 0.
GO TO 166
148 KC= 1
IF (IUSE(J).EQ.-1) IUSE(J+1) GO TO 154
IF (J.EQ.1.0R.IUSE(J).NE.-IUSE(J-1)) GO TO 153
KC= -1
154 JAG= J + KC
IF (CENTXG(NPT).LT.0.) GO TO 170
TKELT= TEMP(INC,1)
TMP= INC + KC
IF (TKELT.EQ.TEMP(IMP,2)) GO TO 154
TKELT= TEMP(IMP,2)
IF (TKELT.EQ.TEMP(IMP,1)) GO TO 157
WRITE (6,156)
156 FORMAT (50H) 3 PHASES OF A CONDENSED SPECIES ARE OUT OF ORDER )
C
C JTM SPECIES A SOLID (EN=0), (J+KC)TH SPECIES A LIQUID (EN IS +)
C
157 IF (IT.GT.1000000) GO TO 169
IF (P.AND.IT.EQ.TMELT) GO TO 165
IF (TP) GO TO 1165
IF (IT.LE.TMELT-150.) GO TO 1165

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320      JSQ = J
      JLIQ = JKG
      GO TO 159

      C
      C JTH SPECIES A LIQUID(EN=0), (J*KG)TH SPECIES A SOLID (EN IS +)
      C
325      IF (TT.LT.TMELT) GO TO 169
      IF (TP.AND.TT.EQ.TMELT) GO TO 169
      IF (TP) GO TO 1165
      IF (TT.GE.TMELT+150.) GO TO 1165
      JSOL = JKG
      JLIQ = J
330      TTN = ALOG(TMELT)
      TT = TMELT
      EN(JKG,NPT) = .5 * EN(JKG,NPT)
      EN(J,NPT) = EN(JKG,NPT)
      GO TO 165

335      C
      C WRONG PHASE INCLUDED FOR T INTERVAL, SWITCH EN
      C
340      1165 EN(J,NPT) = EN(JKG,NPT)
      IUSE(J) = -IUSE(J)
      IUSE(JKG) = -IUSE(JKG)
      EN(JKG,NPT) = 0.
      GO TO 160

345      153 IF (TT.LT.TEMP(INC,1) .AND. TEMP(INC,1) .NE. TLON) GO TO 169
      IF (TT.GT.TEMP(INC,2)) GO TO 169

      C
      C
      SUM = 0.
      DO 167 I = 1, L
      SUM = SUM + A(I,J)*X(I)
350      167 CONTINUE
      DELF = H1(J)-S(J)-SUM
      IF (IDEBUG) WRITE(6,168)DELF,SIZEF
      168 FORMAT (17H GO-SUM(AIJ*PI) =E15.7,10X,18HPREVIOUS DELTA G =,E15.7)
      IF (DELF.GE.SIZEF)FOR=DELF.GE.0. GO TO 169
      SIZEF = DELF
      JOELF = J
355      169 IF (INC.EQ.NC) GO TO 1160
      170 CONTINUE
      1160 IF (SIZEF.EQ.0.) GO TO 143
      J = JOELF

360      165 IC1 = IC1 + 1
      166 IUSE(J) = - IUSE(J)
      167 CONVG = .FALSE.
      163 TN = NUM9
      IF (IDEBUG) WRITE(6,771) NPT, (X(IIL),IL=1,L), TN
      771 FORMAT (13,14F9.3)
      ITNUM9 = ITN
      GO TO 143

370      C
      C CALCULATE EQUILIBRIUM PROPERTIES

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P1712 00971
P1712 00972
P1712 00973
P1712 00974
P1712 00975
P1712 00976
P1712 00977
P1712 00978
P1712 00979
P1712 00980
P1712 00981
P1712 00982
P1712 00983
P1712 00984
P1712 00985
P1712 00986
P1712 00987
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P1712 01000
P1712 01001
P1712 01002
P1712 01003
P1712 01004
P1712 01005
P1712 01006
P1712 01007
P1712 01008
P1712 01009
P1712 01010
P1712 01011
P1712 01012
P1712 01013
P1712 01014
P1712 01015
P1712 01016
P1712 01017
P1712 01018
P1712 01019
P1712 01020
P1712 01021
P1712 01022
P1712 01023

171	SSUM(NPT) = 0.	P1712	01024
	IF(JLIO.NE.0) EN(JSOL,NPT)=ENSOL	P1712	01025
375	DO 183 J=1,NS	P1712	01026
	IF (NPT.EQ.1) SS0 = SS0 + EN(J,1)*S(J)	P1712	01027
	SS = S(J)	P1712	01028
	IF(IUSEVJT.EQ.UJ) SS=SS-EN(N(J)-1)	P1712	01029
	SSUM(NPT) = SSUM(NPT)+SS*EN(J,NPT)	P1712	01030
380	183 CONTINUE	P1712	01031
	IF(.NOT.IC) GO TO 176	P1712	01032
	GLVPT(NPT) = -1.	P1712	01033
	OLVPT(NPT) = 1.	P1712	01034
	CPR(NPT) = CPSUM	P1712	01035
385	GO TO 199	P1712	01036
	SUM = 0.	P1712	01037
178	DO 179 J = 1,L	P1712	01038
	SUM = SUM + PROK(J)*X(J)	P1712	01039
179	CCATINUE	P1712	01040
	OLVPT(NPT) = -2.*SUM/ENN*X(IQ1)	P1712	01041
390	184 IF(JLIC.EQ.0) GO TO 199	P1712	01042
	IUSE(JLIC) = -IUSE(JLIC)	P1712	01043
	HSUM(NPT) = HSUM(NPT)+EN(JLIO,NPT)*(40(JLIO)-40(JSOL))	P1712	01044
	IQ1 = IQ1+1	P1712	01045
395	GAMMAS(NPT) = -1./OLVPT(NPT)	P1712	01046
	GO TO 185	P1712	01047
	199 GAMMAS(NPT) = -1./ (OLVPT(NPT)+(OLVPT(NPT)**2)*ENN/CPR(NPT))	P1712	01048
50	186 ITT(NPT) = TT	P1712	01049
	PPR(NPT) = PP	P1712	01050
400	CPR(NPT) = CPSUM	P1712	01051
	SSUM(NPT) = HSUM(NPT)*TT	P1712	01052
	MM(NPT) = 1./ENN	P1712	01053
	200 IF (.NOT.IDEBUG) RETURN	P1712	01054
405	WRITE(6,201) NPT,PCPINPT),PP,TT,HSUM(NPT),SSUM(NPT),MM(NPT),CPR(NP	P1712	01055
	1),OLVPT(NPT),OLVPT(NPT),GAMMAS(NPT)	P1712	01056
	201 FORMAT (7HOPINT=I3,X,4HPCP=E13.6,X,2HP=E13.6,X,2HT=E13.6,X,4H	P1712	01057
	1H/R=E13.6,X,4H5/R=E13.6//3X,3HMM=E13.6,X,5HCP/R=E13.6,X,6HDI.VPT	P1712	01058
	2=E13.6,X,6HOLVPT=E13.6,X,9MGAMMA(S)=E13.6)	P1712	01059
	GO TO 1000	P1712	01060
410	C	P1712	01061
	C	P1712	01062
	C	P1712	01063
873	TT=0.	P1712	01064
	NPT = NPT-1	P1712	01065
415	1000 RETURN	P1712	01066
	END	P1712	01067
		P1712	01068

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PAGE NO. 1

SUBROUTINE FROZEN

C

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05

{FROZEN COMPOSITION EXPANSION ONLY}

LOGICAL EQL,FROZ,CONVG

10

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COMMON/POINTS/RSUM(13),SSUN(13),CPR(13),OLVTP(13),OLVPT(13)
1  GAMMAS(13),PI26),Y(26),V(13),PPF(13),WM(13),SONVEL(13),YTT(13)
2  TCTN(13)
COMMON/SPECIES/COEF(2,7,150),S(150),EN(150,13),ENLN(150),H0(150)
1  DELN(150),A(15,150),SUB(150,3),IUSE(150),TEMP(50,2)
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COMMON/RTSC/ENN,SUMN,TT,SH,ATGR(13,101),LLRT(15),BU(15,2)
1  TM,TLCH,TMIO,THIGH,PF,SH,UN,OF,EORAT,FPCT,R,RR,HSUB90,AC(2),AM(2)
2  HPP(2),RHO(2),VMIN(2),LS(2),MP(2),DATA(22),NAME(15,5)
3  ANUM(15,5),PECHT(15),ENTH(15),FAZ(15),RTEMP(15),FOX(15),DENS(15)
4  RHOP,RHM(15),TLN,JANF
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COMMON/INDEX/IOEBUG,CONVG,IP,HP,SP,HPSP,TPSP,MOLES,MP,NT,NPT,L,NS,
1  KHAT,INAT,TOL,N,J,NOMIT,IP,NEWK,NSUB,NSUP,ITR,GPCVFR,CPCEVO
2  IONS,AC,NSERT,JSOL,JLIO,KASE(14),NREAC,IC,IQ2
COMMON/PERF/PCP(26),VMOC(13),SPIN(13),VAGI(13),SUBAR(13),SUPAR(13)
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1  CPRF(13),AEAT(13),CSTR,EQL,FROZ,SSO
COMMON/OUP/FT(30),FP(4),FT(4),FH(4),FS(4),FM(4),FV(4),FD(4)
1  FG(4),FG(4),FB,FHT13,F1,F2,F3,F4,F5,FL(4),FMT19,FA1,FA2
2  FRI,FCI,FN(4),F(4),FA(4),FI(4),FMT9X,F0
```

30

```
ITROT = 3
EQL = .FALSE.
NPT = 2
TT = TTT(1)
TLN=ALOG(TT)
```

35

```
GAMMAS(I) = CPRF(I)/CPRF(I)*1.7MN(1)
CPR(1) = CPRF(1)
PCP(2) = ((GAMMAS(1)+1.)/2.)*((GAMMAS(1)/(GAMMAS(1)-1.))
DATA(1) = 2./(GAMMAS(1) + 1.)
TLN = TLN + ALOG(DATA(1))
DO 902 IP=2,NP
```

40

```
IF(NPT.EQ.2) GO TO 45
PCP(NPT) = P(1)/P(IP)
CONVG = .FALSE.
PCPLH=ALOG(PCP(NPT))
S0 = SSO -PCPLN/NM(1)
SUMH = 0.
```

45

```
51 TT=EXP(TENT)
SUNS=0.
J = 1
NNA = NPT
NPT = 1
CALL GPHS
NPT = NM
```

50

```
DO 60 J=1,NS
IF(EN(J,1).EQ.0.) GO TO 63
SUMS = SUMS + S(J)*EN(J,1)
IF(CONVG) SUMH=SUMH+H0(J)*EN(J,1)
```

55	60 CONTINUE	P1712 01122
	IF (CONVG) GO TO 81	P1712 01123
	ULNT=(SUMS-50)/CPSUM	P1712 01124
	TUA=TLN-DLNT	P1712 01125
	IF (DLNT.LT.0.) DLNT=-DLNT	P1712 01126
	IF (DLNT.LT.U.5E-4) CONVG=.TRUE.	P1712 01127
60	GO TO 51	P1712 01128
	81 ITI(NPT)= IT	P1712 01129
	SSUM(NPT)= SSUM(1)	P1712 01130
	HSUM(NPT)= IT*SUM	P1712 01131
	GAMMAS(NPT)= CPSUM/(CPSUM-1./NM(1))	P1712 01132
65	IF (IP.GT.2) GO TO 90	P1712 01133
	GO TO 51	P1712 01134
	C	P1712 01135
	C	P1712 01136
	C	P1712 01137
70	OH = HSUM(1)-HSUM(2)	P1712 01138
	OHSTAR = OH-(GAMMAS(2)*TT/(2.*NM(1)))	P1712 01139
	OH = OHSTAR/OH	P1712 01140
	IF (OH.LT.0.) OH=-OH	P1712 01141
	IF (OH.L. 0.4E-4.OR. ITROT.EQ.0) GO TO 90	P1712 01142
75	PCP(2) = PCP(2)/(1.+2.*OHSTAR*NM(1)/(IT*(GAMMAS(2)+1.)))	P1712 01143
	P(2) = P(1)/PCP(2)	P1712 01144
	ITROT = ITROT-1	P1712 01145
	GO TO 45	P1712 01146
	90 NP(NPT)= NM(1)	P1712 01147
	PP(NPT) = P(IP)	P1712 01148
80	CP(NPT)= CPSUM	P1712 01149
	K = 0	P1712 01150
	IF (IT.LT.(TLOW-150.)) GO TO 903	P1712 01151
	IF (NC.EQ.0) GO TO 700	P1712 01152
	INC = 1	P1712 01153
85	DO 901 I=1,N5	P1712 01154
	IF (IUSE(I).EQ.0.OR.IUSE(I).EQ.-10000) GO TO 901	P1712 01155
	INC = INC+1	P1712 01156
	IF (EM(I).EQ.0.) GO TO 901	P1712 01157
	IF (IT.LT.(TEMP(INC)-50.))OR.IT.GT.(TEMP(1.2)+50.))GO TO 903	P1712 01158
90	901 CONTINUE	P1712 01159
	700 IF (IP.EQ.NP) GO TO 863	P1712 01160
	K = NPT	P1712 01161
	IF (NPT.NE.13) GO TO 870	P1712 01162
	GO TO 863	P1712 01163
95	903 NP1 = NPT - 1	P1712 01164
	863 CALL RKROUT	P1712 01165
	IF (NSUB+NSUP.NE.0) CALL RATIO	P1712 01166
	865 IF (K.EQ.0) GO TO 1002	P1712 01167
	NPT = 2	P1712 01168
100	870 NPT = NPT + 1	P1712 01169
	902 CONTINUE	P1712 01170
	1000 RETURN	P1712 01171
	END	

	C	SUBROUTINE HCALC	P1712 01172
	C	CALCULATE ENTHALPY FOR PROPELLANT USING COEFFICIENTS	P1712 01173
05	C	LOGICAL MOLES	P1712 01174
		DIMENSION NUM(15),S(2)	P1712 01175
			P1712 01176
			P1712 01177
	C	COMMON/SPACES/COEF(2,7,150),S(150),EN(150,13),ENLN(150),M0(150)	P1712 01178
		1,DELN(150),A(15,150),SUB(150,3),IUSE(150),TEMP(50,2)	P1712 01179
10		COMMON/MISC/ENH,SUMN,IT,S0,ATOM(1,10),LLMT(15),30(15),80P(15,2)	P1712 01180
		1,FM,7LCM,THIO,THIGH,PP,CPSUM,OF,EGRAT,FPST,R,RR,MSUB0,AC(2),AM(2)	P1712 01181
		2,HP(12),RH0(12),VMIN(2),VPLS(12),MP(2),DATA(22),NAME(15,5)	P1712 01182
		3,ANUM(15,5),PECHT(15),ENTH(15),FAZ(15),RTMP(15),FOX(15),DENS(15)	P1712 01183
15		4,RHOP,RHM(15),TLN,JANF	P1712 01184
		COMMON/INCH/ IDEBUG,CONVG,TP,HP,SP,HPSP,TPSP,MOLES,NP,NT,NPT,L,NS,	P1712 01185
		1,KHAT,IMAT,IQI,N,J,NOMIT,IP,NEWQ,NSUB,NSUP,IIN,CPCVFR,CPCVED	P1712 01186
		2,IONS,NC,INSERT,JSOL,JLIQ,KASE(14),NREAC,IC,IQ2	P1712 01187
20		EQUIVALENCE(ANUM,NUM)	P1712 01188
	C	DATA AG/1HG/,IZERO/2H00/,OX/1H0/	P1712 01189
25	C	IS IT IN RANGE	P1712 01190
		IF(IT.LI.(TLOW-100.).OR.IT.GT.(THIGH+1000.))GO TO 80	P1712 01191
		NS(1) = 0.	P1712 01192
		NS(2) = 0.	P1712 01193
		HP(1) = 0.	P1712 01194
30		HP(2) = 0.	P1712 01195
		AC(1) = 0.	P1712 01196
		AC(2) = 0.	P1712 01197
		DO 900 N=1,NREAC	P1712 01198
		K=2	P1712 01199
35		IF(FOX(N).EQ.OX)K=1	P1712 01200
		PCNT=PECHT(N)	P1712 01201
		IF(THOLES)PCNT=PCNT+RHM(N)	P1712 01202
		WS(K) = WS(K) + PCNT	P1712 01203
		J = NUM(N,5)	P1712 01204
40		IF (J.NE.3) GO TO 90	P1712 01205
		DO 11 J=1,L	P1712 01206
		DATA(J)=0.	P1712 01207
		10 CONTINUE	P1712 01208
		DO 40 I=1,4	P1712 01209
45		IF(ANUM(N,I).EQ.0.)GO TO 50	P1712 01210
		DO 20 J=1,L	P1712 01211
		IF(ILLMT(J).EQ.NAME(N,I)) GO TO 30	P1712 01212
		20 CONTINUE	P1712 01213
		30 DATA(J)=ANUM(N,I)	P1712 01214
50		40 CONTINUE	P1712 01215
		50 IS=0	P1712 01216
		DO 70 J=1,NS	P1712 01217
		IF(IUSE(J).EQ.0)GO TO 55	P1712 01218
			P1712 01219
			P1712 01220
			P1712 01221
			P1712 01222
			P1712 01223
			P1712 01224

```

55      IS = IS+1
      IF (FAZ(N).EQ.AG) GO TO 70
      IF (IT.LY.TEMP(IS,1).OR.IT.JT.TEMP(IS,2)) GO TO 70
      GO TO 56
56      IF (FAZ(N).EQ.AG) GO TO 70
58      DO 60 I=1,L
      IF (ATIT,JT.NE.DATA(IT)) GO TO 70
      60 CONTINUE
      NUM(N,5) = J
      GO TO 90
      70 CONTINUE
      GO TO 80
59      NSS = NS
      NS = J
      CALL CP+S
      GPSUM = GPSUM/EN(J,HPT)
      NS = NSS
      IF (H0(J).GT.-.01 .AND. H0(J).LT..01) H0(J) = 0.
      RTEMP(N) = IT
      ENTH(N) = HU(J)*RT
      AC(N) = AC(K)+GPSUM*PCHT/RMW(N)
      HPP(K) = HPP(K)+ENTH(N)*PCWT/RMW(N)
      75      HPP(K) = HPP(K)
      900 CONTINUE
      DO 950 K=1,2
      IF (HPT(K).EQ.0) GO TO 955
      HPP(K) = HPP(K)/WS(K)
      AC(K) = AC(K)/WS(K)
      950 CONTINUE
      HSUB9 = (HP(1)*HPP(1)+HP(2)*HPP(2))/(HP(1)+HP(2))
      GO TO 1000
      80 WRITE(955) N
      85 FORMAT(1H0,12,34HITH REACTANT IS NOT IN THERMO DATA )
      1300 RETURN
      END

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P1712 01225
 P1712 01226
 P1712 01227
 P1712 01228
 P1712 01229
 P1712 01230
 P1712 01231
 P1712 01232
 P1712 01233
 P1712 01234
 P1712 01235
 P1712 01236
 P1712 01237
 P1712 01238
 P1712 01239
 P1712 01240
 P1712 01241
 P1712 01242
 P1712 01243
 P1712 01244
 P1712 01245
 P1712 01246
 P1712 01247
 P1712 01248
 P1712 01249
 P1712 01250
 P1712 01251
 P1712 01252
 P1712 01253
 P1712 01254
 P1712 01255
 P1712 01256
 P1712 01257
 P1712 01258

		P1712	U1259
	SUBROUTINE MATRIX	P1712	U1259
		P1712	U1260
	DOUBLE PRECISION G,X	P1712	U1261
05	LOGICAL HP,SP,IF,IOEBUG,CONVG,NEWK	P1712	U1262
		P1712	U1263
		P1712	U1264
	COMMON/POINTS/HSUB(13),SSUM(13),CPR(13),OLVTP(13),ULVPT(13)	P1712	U1265
	1, GANVAS(13),P(26),T(26),V(13),PPP(13),WM(13),SONVEL(13),TTT(13)	P1712	U1266
	2,TCIN(13)	P1712	U1267
10	COMMON/SPECES/COEF(2,7,150),S(150),EN(150,13),ENLN(150),M0(150)	P1712	U1268
	1, BELN(15),A(15,150),SUB(15,3),IUSE(150),TEMP(50,2)	P1712	U1269
	COMMON/MISC/ENN,SUMN,TT,SU,ATON(3,14),LLMT(15),BO(15),BOP(15,2)	P1712	U1270
	1,TR,TLCK,TNID,THIGH,PF,CPSUM,OF,EORAT,FPCT,R,PR,HSUB0,ACT2),AM(2)	P1712	U1271
	2,PPP(2),RMO(2),VMIN(2),VPLS(2),MP(2),DATA(22),NAME(15,5)	P1712	U1272
15	3, ANUM(15,7),PECHT(15),ENTH(15),FAZ(15),RIEMP(15),FOX(15),DENS(15)	P1712	U1273
	4, RHOP, RMH(15),TLN,JANF	P1712	U1274
	COMMON /DOUBLE/ G(20,21), X(20)	P1712	U1275
	COMMON/INDEX/ IOEBUG,CONVG,TP,HP,SP,HPSP,TPSP,HOLES,NP,NT,NPT,L,NS,	P1712	U1276
	1, KMAT,IMAT,IOI,N:J,NOMIT,IP,NEWK,NSUB,NSUP,ITN,CPCVFR,CPCVED	P1712	U1277
20	2, IONS,AC,NSERT,JSOL,JLJO,KASE(14),NREAC,IO,IO2	P1712	U1278
	IO2 = IO1 + 1	P1712	U1279
	IO3 = IO2 + 1	P1712	U1280
	KMAT = IO3	P1712	U1281
25	IF(.NOT.CONVG.AND.TP) KMAT = IO2	P1712	U1282
	IMAT = KMAT - 1	P1712	U1283
	CLEAR MATRIX STORAGES TO ZERO	P1712	U1284
	DO 211 I=1,IMAT	P1712	U1285
30	DO 211 K=1,KMAT	P1712	U1286
	G(I,K) = 0.000	P1712	U1287
	G(I,K) = 0.0	P1712	U1288
35	211 CONTINUE	P1712	U1289
	SSS = 0.	P1712	U1290
	HSUM(NPT) = 0.	P1712	U1291
	BEGIN SET UP OF ITERATION MATRIX	P1712	U1292
40	KK = L	P1712	U1293
	DO 65 J=1,NS	P1712	U1294
	HSUB(J)*EN(J,NPT)	P1712	U1295
	IF (IUSE(J)) 65,11,70	P1712	U1296
45	1) F = (H0(J)-S(J)+ENLN(J)+IN)*EN(J,NPT)	P1712	U1297
	SS = M-F	P1712	U1298
	TERM1 = H	P1712	U1299
	IF (KMAT.EQ. IO2) TERM1 = F	P1712	U1300
	DO 55 I = 1, L	P1712	U1301
	CALCULATE THE ELEMENTS R(I,K)	P1712	U1302
50	IF (A(I,J).EQ. 0.) GO TO 55	P1712	U1303
	TERM = A(I,J)*EN(J,NPT)	P1712	U1304
		P1712	U1305
		P1712	U1306
		P1712	U1307
		P1712	U1308
		P1712	U1309
		P1712	U1310
		P1712	U1311

31/12/70

FORTRAN EXTENDED VERSION 2.0

SUBROUTINE MATRIX

08.09.56.

55	DC 15 K=1, C	P1712 01312
	G(I,K) = G(I,K) + A(I,J)*TERM	P1712 01313
	15 CONTINUE	P1712 01314
	C	P1712 01315
	G(I,IQ1)=G(I,IQ1)+TERM	P1712 01316
60	G(I,IQ2)=G(I,IQ2)+A(I,J)*TERM1	P1712 01317
	IF (CONVG=.OR. F) GO TO 55	P1712 01318
	G(I,IQ3) = G(I,IQ3)+A(I,J)*F	P1712 01319
	IF (SP) G(IQ2,I) = G(IQ2,I) + A(I,J)*SS	P1712 01320
	55 CONTINUE	P1712 01321
65	IF (KNAT .EQ. IC2) GO TO 64	P1712 01322
	IF (CONVG.OR.HP) GO TO 59	P1712 01323
	G(IQ2,IQ1) = G(IQ2,IQ1) + SS	P1712 01324
	G(IQ2,IQ2)=G(IQ2,IQ2)+H0(J)*SS	P1712 01325
	G(IQ2,IQ3) = G(IQ2,IQ3)+(S(J) - EMLN(J)-TM)*F	P1712 01326
	GO TO 62	P1712 01327
70	59 G(IQ2,IQ2)=G(IQ2,IQ2)+H0(J)*H	P1712 01328
	IF (CONVG) GO TO 64	P1712 01329
	G(IQ2,IQ3)=G(IQ2,IQ3)+H0(J)*F	P1712 01330
	62 G(IQ1,IQ3)=G(IQ1,IQ3)+F	P1712 01331
75	64 G(IQ1,IQ2)=G(IQ1,IQ2)+TERM	P1712 01332
	GO TO 65	P1712 01333
	C	P1712 01334
	C CONDENSED SPECIES	P1712 01335
	70 KK = KK + 1	P1712 01336
80	00 75 I = 1, L	P1712 01337
	G(I,KK) = A(I,J)	P1712 01338
2	G(I,KK) = G(I,KK) - A(I,J)*EN(J,NPT)	P1712 01339
	75 CONTINUE	P1712 01340
	G(KK,IQ2) = H0(J)	P1712 01341
85	G(KK,KK) = H0(J) - S(J)	P1712 01342
	MSUM(NPT) = MSUM(NPT) + M	P1712 01343
	IF (.NOT.SP) GO TO 55	P1712 01344
	SSS = SSS + S(J)*EN(J,NPT)	P1712 01345
	G(IQ2,KK) = S(J)	P1712 01346
90	65 CONTINUE	P1712 01347
	SSS = SSS + G(IQ2,IQ1)	P1712 01348
	MSUM(NPT) = MSUM(NPT) + G(IQ1,IQ2)	P1712 01349
	G(IQ1,IQ1) = SUM - ENN	P1712 01350
95	C	P1712 01351
	C REFLECT SYMMETRIC PORTIONS OF THE MATRIX	P1712 01352
	ISYM = IQ1	P1712 01353
	IF (HP.OR.CONVG) ISYM=IQ2	P1712 01354
100	00 102 I=1, ISYM	P1712 01355
	00 102 J=I, ISYM	P1712 01356
	G(J,I)=G(I,J)	P1712 01357
	102 CONTINUE	P1712 01358
	C	P1712 01359
	C COMPLETE THE RIGHT HAND SIDE	P1712 01360
105	C	P1712 01361
	C IF (CONVG) GO TO 175	P1712 01362
		P1712 01363
		P1712 01364

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110      DC 165 I=1,L
          X(I)=30(I)-G(I,IQ1)
          G(I,KMAT) = G(I,KMAT)+X(I)
          145 CONTINUE
          G(IQ1,KMAT) = G(IQ1,KMAT)+ENN-SUMN
          C
          C COMPLETE ENERGY ROW AND TEMPERATURE COLUMN
          C
          IF (KMAT.EQ. IC2) GO TO 105
          IF (SP)ENERGY = S0+ENN-SUMN - SSS
          IF (HP)ENERGY=HSUR0/TT - HSUM(NPT)
          G(IQ2,IC3)=G(IQ2,IC3)+ENERGY
          175 G(IQ2,IC2)=G(IC2,IC2)+CPSUM
          105 RETURN
          ENC
120

```

P1712 01365
 P1712 01366
 P1712 01367
 P1712 01368
 P1712 01369
 P1712 01370
 P1712 01371
 P1712 01372
 P1712 01373
 P1712 01374
 P1712 01375
 P1712 01376
 P1712 01377
 P1712 01378
 P1712 01379


```

55      28 IF (NN-I) 29,31,29
      29 DO 30 J=NN,IUSE1
      30 Z=G(I,J)
      31 G(I,J)=G(NN,J)
      32 G(NN,J)=Z
      33 CONTINUE
      34 DIVIDE A11 ROW BY NTH DIAGONAL ELEMENT AND ELIMINATE THE NTH
      35 VARIABLE FROM THE REMAINING EQUATIONS
      36 K = NN + 1
      37 DO 38 J = K, IUSE1
      38 IF (G(NN,J) .EQ. 0.) GO TO 23
      39 G(NN,J) = G(NN,J) / G(NN,NN)
      40 CONTINUE
      41 IF (K-IUSE1) 46,45,38
      42 DO 44 I = K,IUSE1
      43 DO 44 J = K, IUSE1
      44 G(I,J) = G(I,J) - G(I,NN)*G(NN,J)
      45 CONTINUE
      46 CONTINUE
      47 BACKSOLVE FOR THE VARIABLES
      48 K = IUSE1
      49 J = K + 1
      50 X(K) = 0.000
      51 X(K) = 0.3
      52 SUM = 0.0
      53 IF (IUSE - J) 51,49,48
      54 DO 56 I = J,IUSE1
      55 SUM = SUM + G(K,I)*X(I)
      56 CONTINUE
      57 X(K) = G(K,IUSE1) - SUM
      58 K = K - 1
      59 IF (K) 67,151,67
      60 IUSE = IUSE - 1
      61 RETURN
      62 END

```

P1712 01438
 P1712 01439
 P1712 01440
 P1712 01441
 P1712 01442
 P1712 01443
 P1712 01444
 P1712 01445
 P1712 01446
 P1712 01447
 P1712 01448
 P1712 01449
 P1712 01450
 P1712 01451
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 P1712 01460
 P1712 01461
 P1712 01462
 P1712 01463
 P1712 01464
 P1712 01465
 P1712 01466
 P1712 01467
 P1712 01468
 P1712 01469
 P1712 01470
 P1712 01471

05	C	SUBROUTINE MOLIER	P1712 01472
		COMMON/POINTS/MSUM(13),SSUM(13),CPR(13),OLVFP(13),JLVFP(13)	P1712 01473
		1 ,GAMMAS(13),P(26),T(26),V(13),PPP(13),MM(13),SONVEL(13),TTT(13)	P1712 01474
		2 ,TCFN(13)	P1712 01475
		COMMON/SPECIES/DOEF(2,7,150),S(150),EN(150,13),EALN(150),MO(150)	P1712 01476
		1 ,TENT(150),A(15,150),SU(150,3),IUSE(150),TEMP(150,2)	P1712 01477
		COMMON/MISC/ERN,SUMM,II,SU,ATOM(13,10),LLMT(15),BU(15),BDP(15,2)	P1712 01478
		1 ,TK,TLOM,THIO,THIGH,PP,CPSUM,OF,EGRAI,FPC,R,R,M,MSUBO,AC(2),AM(2)	P1712 01479
		2 ,MP(12),AMO(12),VMI(12),VPLS(12),MP(12),DATA(22),NAME(15,5)	P1712 01480
		3 ,ANUM(15,5),FCMF(15),ENTH(15),FAZ(15),RTCMP(15),FOX(15),DEMS(15)	P1712 01481
		4 ,RHOP,R4M(15),ILN,JANF	P1712 01482
		COMMON/INIT/IDCRUG,CONVG,IP,NP,SP,NDSF,TPSP,MOLES,NP,NT,L,NS,	P1712 01483
		1 ,KHA7,I7AT,I3I,N,J,NOMIT,IP,NEWZ,NSUB,ASUP,ITN,OPCVFR,CPCVE3	P1712 01484
		2 ,IONS,NC,INSERT,J,SOL,JULIQ,KA5E(14),NREAC,IC,JO2	P1712 01485
		DO 91 IT = 1,26	P1712 01486
		IF (IT) EQ. 0.7 GO TO 95	P1712 01487
		NT = IT	P1712 01488
		91 CONTINUE	P1712 01489
20	C	SET ASSIGNED P	P1712 01490
	C	92 DO 902 IP = 1,NP	P1712 01491
		PP = P(IP)	P1712 01492
	C	SET ASSIGNED :	P1712 01493
	C	DO 902 I3=1,NT	P1712 01494
		IT = (IT)	P1712 01495
		CALL EQLDRM	P1712 01496
30		IF (IT) EQ. 0 GO TO 302	P1712 01497
		IF (NP) EQ. 1 GO TO 1000	P1712 01498
		IF (IP) EQ. 0 GO TO 860	P1712 01499
		K = NP	P1712 01500
		IF (NP) EQ. 1 GO TO 870	P1712 01501
35		5 FORMAT(1M1,41X,6HTHERMODYNAMIC EQUILIBRIUM PROPERTIES AT ASSIGNED	P1712 01502
		1 ,/43X,28H TEMPERATURES AND PRESSURES ///	P1712 01503
		CALL OUT1	P1712 01504
		WRITE (6,863)	P1712 01505
		FORMAT (25HTHERMODYNAMIC PROPERTIES//)	P1712 01506
		CALL OUT2	P1712 01507
		CALL OUT3	P1712 01508
45		865 IF (K) EQ. 0 GO TO 1000	P1712 01509
		WRITE (6,866)	P1712 01510
		FORMAT (1M1)	P1712 01511
		NP = 0	P1712 01512
		970 NP = NP + 1	P1712 01513
		971 NP = NP + 1	P1712 01514
		CALL OUT3	P1712 01515
		WRITE (6,868)	P1712 01516
		FORMAT (1M1)	P1712 01517
		NP = 0	P1712 01518
		970 NP = NP + 1	P1712 01519
		971 NP = NP + 1	P1712 01520
50	C	SAVE COMPOSITIONS FOR ESTIMATES OF NEXT POINT	P1712 01521
	C	DO 880 I = 1,NS	P1712 01522
			P1712 01523
			P1712 01524

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FORTAN EXTENDED VERSION 2.0

SUBROUTINE HOLIER

EN(I,NFY) = EN(I,K)

880 CONTINUE

962 CONTINUE

1000 RETURN

END

P1712 01525
P1712 01526
P1712 01527
P1712 01528
P1712 01529

SUBROUTINE OUT1		FORTRAN EXTENDED VERSION 2.0		SUBROUTINE OUT1	
C	C	DOUBLE PRECISION G,X		P1712	01530
C	C	LOGICAL EUL,FROZ ,TP,HP,SP,H2SP,T2SP,MOLES		P1712	01531
05	C	DIMENSION NV(13),Z(10,3),HEAD(15),YX(5),YM(5)		P1712	01532
	C			P1712	01533
	C			P1712	01534
	C			P1712	01535
	C			P1712	01536
10		COMMON/POINTS/MSUB(13),SSUM(13),CPR(13),OLVTP(13),OLVPT(13)		P1712	01537
		1 ,GAMMAS(13),P(26),T(26),V(13),PPP(13),MM(13),SCNVEL(13),FIT(13)		P1712	01538
		2 ,TOTN(13)		P1712	01539
		COMMON/SPECIES/CCEP(2,7,150),S(150),EN(150,13),ENLN(150),H0(150)		P1712	01540
		1 ,CELN(150),A(15,150),SUB(150,3),TUSE(150),TEMP(50,2)		P1712	01541
		COMMON/MISC/ENR,SUNN,TT,ST,ATOM(3,101),LLMT(15),BT(15),BOP(15,2)		P1712	01542
		1 ,TM,TIOM,TIIO,THIGH,PP,CPSON,OF,EQRAT,FCPT,N,RR,MSUBJ,AL(2),AM(2)		P1712	01543
15		2 ,MPP(2),RHO(2),VMIN(2),VPLS(2),NR(2),DATA(22),NAME(15,5)		P1712	01544
		3 ,ANUM(15,5),PCENT(15),ENTH(15),FAI(15),RTEMP(15),FOX(15),DENS(15)		P1712	01545
		4 ,RHCP,FMW(15),TLN,JANF		P1712	01546
		COMMON/DOUBLE/ G(20,21), X(20)		P1712	01547
		COMMON/INDEX/ IDEBUG,CORVG,TP,HP,SP,H2SP,T2SP,MOLES,NP,NT,NFI,1,NS,		P1712	01548
20		1 ,KMAT,IMAT,IOI,N,J,NHMT,IP,NEHR,NSUB,NSUP,ITN,QPCVFR,QPCVEQ		P1712	01549
		2 ,IONS,NC,NSERT,JSOL,JLIQ,KASE(14),NREAC,IC,IQ2		P1712	01550
		COMMON/PERF/PCP(26),VMOC(13),SPIM(13),VACI(13),SUBAR(13),SUPAR(13)		P1712	01551
		1 ,CPRF(13),AEAT(13),CSTR,EQL,FROZ,SSG		P1712	01552
		COMMON/OUT/FFMT(30),FPI(4),FI(4),FHI(4),FS(4),FV(4),FO(4)		P1712	01553
25		1 ,FCIT,FG(4),FB,FMT13,F1,F2,F3,F4,F5,F6,F7,F8,F9,F10,F11,F12,F13,F14,F15,F16,F17,F18,F19,F20		P1712	01554
		2 ,FRI,FCI,FN(4),FA(4),FA(4),FI(4),FNT9,FA1,FA2		P1712	01555
		COMMON/CVOLUM/ VOLUMC,IMPETUS,IFLGGG		P1712	01556
		COMMON/PERCENT/ PMULE		P1712	01557
30		REAL IMPETUS		P1712	01558
		EQUIVALENCE (V,NV1,IZ,NO)		P1712	01559
		HEAD=(1H ,2A4.5 (A2,F8.5,3X)5 X,F7.5,F13.3,4X,A1,F10.2,F9.4)		P1712	01560
35		DATA HEAD/4H(1H ,4H,2A4.2H,5.4H)2,4HF8.5 ,4H,3X)2H,5 .2HX,		P1712	01561
		1 ,4HF7.5 ,4H,F13 ,4H,3.4 ,4HX,A1 ,4H,F10 ,4H,2.F ,4H,9.4)/		P1712	01562
		DATA FUEL/7H(FUEL/7OXID/4HOXID/ANT/3HANT/1OX/1MO/		P1712	01563
		1 ,YN/2H,1 ,2H,2 ,2H,3 ,2H,4 ,2H,5 /		P1712	01564
		2 ,YX/3H,57,3H,44,3H,31,3H,18,2H,5 /		P1712	01565
40		WRITE(6,4) KASE		P1712	01566
		4 FORMAT(1H0,13A6,A2)		P1712	01567
		5 FORMAT(9H CASE NO. ,13)		P1712	01568
45		IF(.NOT.MOLES) WRITE(6,5)		P1712	01569
		5 FORMAT(77X,46HNT FRACTION ENTHALPY STATE TEMP DENSITY/		P1712	01570
		1 10X,16HCHEMICAL FORMULA,51X,21H(SEE NOTE: CAL/MOL,10X,5HDLG K,		P1712	01571
		2 4X,4HCVOL)		P1712	01572
		IF(MOLES) WRITE(6,6)		P1712	01573
		6 FORMAT(10X,5HMOLES,2X,33HENTHALPY STATE,10X,13HDEG K		P1712	01574
50		1 10X,16HCHEMICAL FORMULA,67X,7HCVOL/MOL,10X,13HDEG K		P1712	01575
		DO 15 N=1,NREAC		P1712	01576
		IF (FOX(N).EQ.FOX(N-1))GO TO 11		P1712	01577
		IF (FOX(N).NE.OX)GO TO 10		P1712	01578
				P1712	01579
				P1712	01580
				P1712	01581

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SUBROUTINE OUT1

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55      HD1 = C*10
      HD2 = ANT
      GO TO 11
      10 HD1 = FUEL
      HD2 = FB
      11 DO 13 J=1,5
      13 CONTINUE
      14 J=J-1
      HD3(3)=YN(J)
      HD3(7)=YX(J)
      WRITE(6,HEAD)HD1,HD2,(NAME(N,J),ANUM(N,J),PECHT(N),ENTHT
      1N),FAZ(N),RTMP(N),DENS(N)
      15 CONTINUE
      WRITE(6,20) OF,FCPT,EGRAT,RHOP
      20 FORMAT (1H0,15X, 4H0/F=, F8.4,4X,13HPERCENT FUEL=F8.4,4X,
      1 19HEQUIVALENCE RATIO=, F7.4,4X,8HDENSITY=F8.4//)
      C
      AGV = 9.80665
      DO 25 I = 1,NPT
      TOTN(I) = 0
      DO 25 J = 1,MS
      TOTN(I) = TOTN(I) + EN(J,I)
      25 CONTINUE
      FMT(4) = FMT(6)
      RETURN
      C
      ENTRY OUT2
      C
      C-----PRESSURE
      C
      DO 55 I=1,NPT
      K= 2*I+3
      FMT(K) = F4
      IF (PPP(I).GE.1.) FMT(K)=F3
      IF (PPP(I).GE.10.) FMT(K)=F2
      IF (PPP(I).GE.100.) FMT(K)=F1
      55 CONTINUE
      WRITE (6,FMT) (FP(I),I=1,4), (PPR(J),J=1,NPT)
      C
      C-----TEMPERATURE
      C
      DO 65 I=1,NPT
      NV(I) = TTI(I)*.5
      65 CONTINUE
      FMT(4) = FMT13
      FMT(5) = FMT19
      WRITE (6,FMT) (FI(I),I=1,4), (NV(J),J=1,NPT)
      C
      C-----ENTHALPY
      C
      DO 75 I=1,NPT

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P1712 01582
 P1712 01583
 P1712 01584
 P1712 01585
 P1712 01586
 P1712 01587
 P1712 01588
 P1712 01589
 P1712 01590
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 P1712 01600
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 P1712 01629
 P1712 01630
 P1712 01631
 P1712 01632
 P1712 01633
 P1712 01634

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      V(I) = HSUM(I) * R
      75 CONTINUE
      FMT(5) = F9
      FMT(7) = F1
      WRITE (6,FMT) (FH(I), I=1,4), (V(J), J=1,NPT)
      C
      C ENTROPY
      C
      C
      FMT(7) = F4
      DO 78 I = 1,NPT
      V(I) = SSUM(I) * R
      78 CONTINUE
      WRITE (6,FMT) (FS(I), I=1,4), (V(J), J=1,NPT)
      WRITE (6,80)
      80 FORMAT ( 1H )
      C
      C MOLECULAR WEIGHT
      C
      FMT(7) = F3
      WRITE (6,FMT) (FM(I), I=1,4), (WM(J), J=1,NPT)
      C
      C (DLV/DLP) T
      C
      FMT(7) = F5
      IF (EQL) WRITE (6,FMT) (FV(I), I=1,4), (DLVPT(J), J=1,NPT)
      C
      C (DLV/DLT) P
      C
      FMT(7) = F4
      IF (EQL) WRITE (6,FMT) (FO(I), I=1,4), (DLVTP(J), J=1,NPT)
      C
      C HEAT CAPACITY
      C
      DO 85 I = 1,NPT
      V(I) = CPR(I) * R
      85 CONTINUE
      WRITE (6,FMT) (FG(I), I=1,4), (VT(J), J=1,NPT)
      C
      C GAMMA(S)
      C
      WRITE (6,FMT) (FG(I), I=1,4), (GAMMAS(J), J=1,NPT)
      C
      C SONIC VELOCITY
      C
      FMT(7) = F1
      DO 95 I = 1,NPT
      SONVEL(I) = SORT(R3 * GAMMAS(I) * TTT(I) / WM(I))
      95 CONTINUE
      WRITE (6,FMT) (FL(I), I=1,4), (SONVEL(J), J=1,NPT)
      VOLUME = GAMMAS(1) * TTT(1)
      IMPETUS = VOLUME * 2781.0 / WM(1)
      RETURN
      C

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P1712 01635
 P1712 01636
 P1712 01637
 P1712 01638
 P1712 01639
 P1712 01640
 P1712 01641
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 P1712 01681
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 P1712 01683
 P1712 01684
 P1712 01685
 P1712 01686
 P1712 01687

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160  ENTRY OUT1
    IF (.NOT.EOL) GO TO 331
    C  MOLE FRACTIONS - EQUILIBRIUM
    C
165  WRITE (6,80)
    PRINT*,F5
    WRITE(6,310)
    310 FORMAT(15HMOLE FRACTIONS //)
    DO 330 K=1,NS
    330 K=1,NS
    DO 315 I=1,NPT
    315 I=1,NPT
    V(I) = EN(K,I) /TOTN(I)
    319 CONTINUE
    DO 316 I=1,NPT
    316 I=1,NPT
    IF (V(I).GE.(5.E-6)) GO TO 320
    320 CONTINUE
    320 WRITE (6,FMT) SUB(K,1),SUB(K,2),SUB(K,3),FB,(V(I),I=1,NPT)
    321 CONTINUE
    331 WRITE(6,335)
    335 FORMAT(11SHADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MO
    1LE FRACTIONS WERE LESS THAN .00005 FOR ALL ASSIGNED CONDITIONS//)
    LINE= 0
    DO 340 K=1,NS
    340 K=1,NS
    IF ((EN(K,1)/TOTN(1)).GE.(5.E-6)) GO TO 343
    341 CONTINUE
    LINE= LINE+1
    Z(LINE,1) = SUB(K,1)
    Z(LINE,2) = SUB(K,2)
    Z(LINE,3) = SUB(K,3)
    343 IF ((LINE.NE.10) .AND. K.NE.NS) GO TO 350
    IF (LINE.EQ.6) GO TO 1800
    WRITE(6,345) (Z(LN,1),Z(LN,2),Z(LN,3),LN=1,LINE)
    345 FORMAT (10(1X,3A4))
    LINE= 0
    350 CONTINUE
    IF (.NOT.MOLES) WRITE(6,360)
    360 FORMAT(78HNOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXI
    2DANT IN TOTAL OXIANTS )
    WRITE(6,1100) MOLE
    1100 FORMAT(1H0.*VISCOSITY AND CONDUCTIVITY VALUES BASED ON *.F5.1.* PE
    ARGENT-OF GAS MIXTURE*)
    1000 RETURN
    END

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P1712 01888
 P1712 01889
 P1712 01890
 P1712 01891
 P1712 01892
 P1712 01893
 P1712 01894
 P1712 01895
 P1712 01896
 P1712 01897
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 P1712 01899
 P1712 01900
 P1712 01901
 P1712 01902
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 P1712 01920
 P1712 01921
 P1712 01922
 P1712 01923
 P1712 01924
 P1712 01925
 P1712 01926
 P1712 01927
 P171201 00002
 P171201 00003
 P171201 00004
 P1712 01928
 P1712 01929

SUBROUTINE	RATIO	FORTRAN EXTENDED VERSION 2.0	31/12/70	08.09.56.	PAGE NO. 2
55		IFV(LL).GE.AEAT(J) GO TO 56 38 CONTINUE GO TO 56 40 IF(NPT-NBLO.LE.3) GO TO 1100 V(LL) = SUPAR(I) K=4*NBLO DO 42 JJ=K,NPT J=JJ IF(V(LL).LE.AEAT(J)) GO TO 56 -2 CONTINUE IF(V(LL).GE.AEAT(J)*3.) GO TO 85 56 KJ = J-1 K = KJ DO 64 JJ=1 2 IF(OPR(K).NE.0.) GO TO 63 WRITE(6,62)K 62 FORMAT(17H0CANNOT USE POINT,I2.3X,4HCP=0) GO TO 1100 61 PER(JJ,I)=-1.7CPR(K)*WM(K) IF (EQL) PER(JJ,1) = PER(JJ,1)*DLVTP(K) PER(JJ,2) = TTT(K)/E.*WM(K)*(HSUM(1)-HSUM(K)) RP(JJ) = 1./(1./GAMMAS(K)-PER(JJ,2)) IF(EQL)RPP(JJ) = 1.*DLVTP(K)+(1.-DLVTP(K))*PER(JJ,1) K = KJ + 1 64 CONTINUE 75 80 AMAT(LL) = WM(1) CALL SET(PCP(KJ),RP(1),AEAT(KJ),V(LL), APCP(LL)) CALL SET(TTT(KJ),PER(1,1),PCP(KJ),APCP(LL),AT(LL)) IF(EQL)CALL SET (WM(KJ),RPP(1),PCP(KJ),APCP(LL),AMNT(LL)) K = KJ DO 74 JJ=1,2 G(JJ,7)=SPIM(K)*2 G(JJ+2,7)=2.*G(JJ,7)*PER(JJ,2) G(JJ+4,7)=(1.-GAMMAS(K))/GAMMAS(K)*G(JJ+2,7) G(JJ,1)=1. G(JJ+2,1)=0 G(JJ+4,1)=0 G(JJ,2)=ALOG(PCP(K)) G(JJ+2,2)=1. G(JJ+4,2)=0 DO 70 P=3,5 MXG=M-1 G(JJ,M)=G(JJ,2)*MXP NXP=NXP-1 G(JJ+2,M)=G(JJ,2)*MXP*FLOAT(M-1) G(JJ+4,M)=G(JJ+2,M)/G(JJ,2)*FLOAT(M-2) 70 CONTINUE K = KJ + 1 74 CONTINUE INAT = 6 CALL MGAUSS AI(LL) = X (1) DO 84 JJ=2,6 100 105	P1712 01783 P1712 01784 P1712 01785 P1712 01786 P1712 01787 P1712 01788 P1712 01789 P1712 01790 P1712 01791 P1712 01792 P1712 01793 P1712 01794 P1712 01795 P1712 01796 P1712 01797 P1712 01798 P1712 01799 P1712 01800 P1712 01801 P1712 01802 P1712 01803 P1712 01804 P1712 01805 P1712 01806 P1712 01807 P1712 01808 P1712 01809 P1712 01810 P1712 01811 P1712 01812 P1712 01813 P1712 01814 P1712 01815 P1712 01816 P1712 01817 P1712 01818 P1712 01819 P1712 01820 P1712 01821 P1712 01822 P1712 01823 P1712 01824 P1712 01825 P1712 01826 P1712 01827 P1712 01828 P1712 01829 P1712 01830 P1712 01831 P1712 01832 P1712 01833 P1712 01834 P1712 01835		

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      A1(11)=A1(11)*X*(J1)*ALOG(APCP(LL))*((J1-1)
110      IF(A1(LL).LE.0.)GO TO 85
      A1(LL)=A1(LL)*.5
      GO TO 86
115      LL=LL-1
      IF(LL.GE.15.DR.1.GZ.NARY) GO TO 90
      LL=LL+1
      GO TO 110
      C
      C OUTPLY
      C
120      IF(TECL)WRITE(6,87)
125      87 FORMAT(1H1/20X,* THEORETICAL GUN PROPELLANT PERFORMANCE ASSUMING E
      EQUILIBRIUM COMPOSITION DURING EXPANSION*//)
      IF (.NOT.EQL) WRITE (6,88)
130      88 FORMAT(1H1/20X,* THEORETICAL GUN PROPELLANT PERFORMANCE ASSUMING F
      10ZEN COMPOSITION DURING EXPANSION*//)
      IF (.NOT.SF) WRITE (6,89)
135      89 FORMAT (52X,20HAT AN ASSIGNED TEMPERATURE
      WRITE (6,91)
140      91 FORMAT (52X,20HFOR ASSIGNED AREA RATIOS
      PC= P(1)*14.696C96
      WRITE(6,191)PC
145      191 FORMAT(5M1,*,(P8.1,9M PSIA)
      CALL OUT1
      IF(ISONIC.EQ.1) WRITE(6,33)
150      33 FORMAT(18H0SUBSONIC FLOW
      IF (ISONIC.EQ.2) WRITE (6,35)
155      35 FORMAT(18H0SUPERSONIC FLOW
      C
      C AREA RATIO
      C
160      FMT(6)= FMT(6)
      FMT(4)= FMT(4)
      DO 92 M=1,LL
165      FMT(K)= F3
      IF(V(M).GE.10.) FMT(K)=F2
      IF(V(M).GE.100.) FMT(K)=F1
      92 CONTINUE
      WRITE(6,FMT) FA1,FA2,FB,FB,V(M),M=1,LL)
      C
      C VACUUM SPECIFIC IMPULSE AND SPECIFIC IMPULSE
      C
170      DO 93 M=1,LL
      V(M)=AI(M)+CSTR*V(M)/(32.174* APCP(M))
175      93 CONTINUE
      FMT(4)= FMT(3)
      FMT(5)= F8
      FMT(7)= F1
      WRITE(6,FMT) (FA(M),M=1,4), (V(M),M=1,LL)
      WRITE(6,FMT) (FI(M),M=1,4), (AI(M),M=1,LL)

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```

160      C      C*
      C
      FMT(5) = FMT19
      DO 94 M=1,LL
      NV(M)=CSIR+.5
94 CONTINUE
      WRITE(6,FMT) (FR(I),N=1,4), (NV(M),M=1,LL)
      C
      CF = THRUST COEFFICIENT
      C
      DO 95 M=1,LL
      V(PJER(I)*32.1747/CSIR
95 CONTINUE
      FMT(5) = F3
      FMT(7) = F3
      WRITE(6,FMT) FC1,F8,FD,FB,(V(M),M=1,LL)
      WRITE(6,96)
96 FORMAT(' ')
      C
      C      PRESSURE RATIO
      C
      FMT(4) = FMT(6)
      DO 97 M=1,LL
      K=2*M+3
      FMT(K) = F3
      IF(APCP(M).GE.1000.) FMT(K)=F2
      IF(APCP(M).GE.10000.) FMT(K)=F1
97 CONTINUE
      C
      C      PRESSURE
      C
      WRITE(6,FMT) FR1,F8,FB,FB,(APCP(M),M=1,LL)
      DO 98 M=1,LL
      K=2*M+3
      V(M)=P(1)/APCP(M)
      FMT(K) = F3
      IF(V(M).GE.1.) FMT(K)=F3
      IF(V(M).GE.10.) FMT(K)=F2
      IF(V(M).GE.100.) FMT(K)=F1
98 CONTINUE
      WRITE(6,FMT) (FF(N),N=1,4), (V(M),M=1,LL)
      C
      C      TEMPERATURE
      C
      DO 101 M=1,LL
      NV(M)=AT(M)+.5
101 CONTINUE
      FMT(5) = FMT19
      WRITE(6,FMT) (FT(N),N=1,4), (NV(M),M=1,LL)
      C
      C      ENTHALPY
      C

```

08.09.56.

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SUBROUTINE RATIO FORTRAN EXTENDED VERSION 2.0

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C
      FMT(5)=F8
      FMT(7)=F1
      DO 104, M=1,LL
      V(M)=MSUM(1)*R-1000.*(AI(M)/294.38)**2
104 CONTINUE
      WRITE(6,FMT) (P(M),M=1,N), (V(M),M=1,LL)
C
220  C      ENITROPY
C
      FMT(7)=F4
      V(1)=SSUM(2)*R
      DO 106, M=1,LL
      V(M)=V(1)
106 CONTINUE
      WRITE(6,FMT) (FS(M),M=1,4), (V(M),M=1,LL)
C
230  C      MOLECULAR HEIGHT
C
      FMT(7)=F3
      WRITE(6,FMT) (FM(M),M=1,4), (AMT(M),M=1,LL)
110 CONTINUE
120 CONTINUE
      RETURN
      END

```

SUBROUTINE REACT FORTRAN EXTENDED VERSION 2.0 31/12/70 06:09.56. PAGE NO. 1

```

SUBROUTINE REACT
C
C
C DOUBLE PRECISION G,X
C LOGICAL HP,SP,TP,IOEBUG,CONVG,NEMR,IONS,MOLES,EOL,PROZ
C
C DIMENSION NAME(15),J,T,N,JANE
C
COMMON/HISC/ENN,SUMN,TT,S0,ATOM(3,101),LLMT(15),80(15),80P(15,2)
1  * TM,TLCH,TMID,THIGH,PP,CPSON,OF,EQAT,FCPT,R,RR,HSUB0,AC(2),AK(2)
2  * HPP(2),RHO(2),VWIN(2),VPLS(2),MPI(2),DATA(22),NAME(15,5)
3  * ANUM(15,5),PECHT(15),ENTH(15),FAZ(15),RTMP(15),FOX(15),DENS(15)
4  * HOP,MM(15),TEN,JANE
COMMON/INDX/ IOEBUG,CONVG,IP,HP,SP,HPSP,TPSP,MOLES,NP,NT,NPT,L,NS,
15 1  * KMAT,IMAT,IG1,N,J,NORIT,IP,NEMR,NSUB,NSUP,ITN,CPCVFR,CPCVEQ
2  * IONS,NC,NSERT,JSOL,JLIQ,KASE(14),NREAC,IG,IQ2
C
C EQUIVALENCE (NAME,ANAME)
C
C DATA MOL/1HM/,OX/1HO/,LANK/1H /,IZERO/2H00/
C
WRITE(6,3000)
9000 FORMAT(1H,'*REACTANTS*')
DO 10 K=1,2
  NP(K)=0
  HPP(K)=0
  RHC(K)=0
  VPLS(K)=0
  VWIN(K)=0
  AC(K)=0
  AN(K)=0
  DO 8 J=1,15
    LLMT(J)=0
    BOP(J,K)=0
  8 CONTINUE
  10 CONTINUE
  N=1
  L=1
  NREACS=NREAC
  IF (NREAC.GT.16) NREAC=16
  DO 200 N=1,NREAC
    20 READ(5,21) (NAME(N,I),ANUM(N,I),I=1,5),PECHT(N),MOLE,ENTH(N),FAZ(N)
    1  * RTMP(N),FOX(N),DENS(N)
    21 FORMAT(5(A2,F7.5),F7.5,A1,F9.5,A1,F8.5,A1,F8.5)
    IF (L.EQ.0) GO TO 20
    IF (NAME(N,1).EQ.LANK) GO TO 200
    WRITE (6,31) (NAME(N,I),ANUM(N,I),I=1,5),PECHT(N),MOLE,ENTH(N),FAZ
    1  * (N),RTMP(N),FOX(N),DENS(N)
    31 FORMAT(1X,5(A2,1X,F7.5),F7.5,2X,F9.5,2X,F9.5,2X,F8.5,2X,F8.5,2X)
    1A1,3X,F8.5)
    35 IF (MOLE.EQ.MOL) MOLES=.TRUE.
    K=2
    IF (FOX(N).EQ.OX) K=1
  200 CONTINUE

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SUBROUTINE REACT FORTRAN EXTENDED VERSION 2.0

```
55      DO 38 J=1,15
          DATA(J) = 0.
          38 CONTINUE
          RM=0.
          GO 100 JJ=1,5
          IF (ANUM(N,JJ).EQ.0.) GO TO 101
          DO 41 J=1,15
              NJ = J
              IF (LLMT(J).EQ.0) GO TO 45
              IF (NAME(N,JJ).EQ.LLMT(J)) GO TO 46
              41 CONTINUE
              45 L = NJ
              LLPT(J)=NAME(N,JJ)
              46 DO 48 KK=1,101
                  IF (ATOM(1,KK).EQ.ANAME(N,JJ)) GO TO 50
                  48 CONTINUE
                  L=0
                  GO TO 20
              50 RM=RM+AMU(N,JJ)*ATOM(2,KK)
                  V(J)=ATOM(3,KK)
                  DATA(J)=ANUM(N,JJ)
              100 CONTINUE
              101 PCMT=PECHT(N)
                  IF (MOLES) PCMT=PCMT*RM
                  MP(NT=MP(T)+PCMT
                  IF (NAME(N,5).NE.1ZER0) HPP(K)=HPP(K)+ENTH(N)*PCMT/RM
                  AM(K)=AM(K)+PCMT/R4
                  DO 110 J=1,L
                      80 F(J,K)=DATA(J)*PCMT/RM +90P(J,K)
                  110 CONTINUE
                  IF (DENSE*NE.0.) GO TO 115
                      GO TO 117
                  115 RHQ(K)=RHQ(K)+PCMT/DENS(N)
                  117 RMK(N) = RM
                  200 CONTINUE
                  IF (NREAGS.LE.16) GO TO 1205
                      NRAM=NREAGS-16
                      DO 1200 I=1,NRAM
                          1200 READ(5,21) JUNK
                          1205 IF (L.EQ.0) GO TO 1000
                              IF (L.EQ.0) GO TO 1000
                              DO 220 K=1,2
                                  IF (MP(K).EQ.0.) GO TO 220
                                  HPP(K)=HPP(K)/NF(K)
                                  AM(K) = MP(K)/AM(K)
                                  IF (RHO(K).NE.0.) RHQ(K)=MP(K)/RHO(K)
                                  DO 215 J=1,L
                                      80 P(J,K)=80P(J,K)/MP(K)
                                  IF (V(J).GT.0.) VPM(K)=VPM(K)+80P(J,K)*V(J)
                                  IF (V(LJ).GT.0.) VPLS(K)=VPLS(K)+80P(J,K)*V(J)
                                  215 CONTINUE
                                  IF (MOLES) GO TO 220
                                  DO 216 N=1,NREAL
```

SUBROUTINE REACT		FORTRAN EXTENDED VERSION 2.0		31/12/70	06:09:56	PAGE NO. 3
110	IF (FOX(N) = 0.0X.AND.N.EQ.2) GO TO 218	P1712	02073			
	IF (FOX(N) .NE. 0X.AND. L.EQ.1) GO TO 218	P1712	02074			
	PECMT(N) = PECMT(N)/WP(K)	P1712	02075			
	218 CONTINUE	P1712	02076			
	220 CONTINUE	P1712	02077			
	NEWR = TRUE.	P1712	02078			
	DO 230 N = 1,NREAC	P1712	02079			
	IF (DENS(N) .NE. C.) GO TO 230	P1712	02080			
115	RHC (1) = 0.	P1712	02081			
	GO TO 1800	P1712	02082			
	230 CONTINUE	P1712	02083			
	1000 RETURN	P1712	02084			
	END	P1712	02085			

SUBROUTINE RKTOU1		
C	ROCKET PERFORMANCE PARAMETERS	P1712 02086
		P1712 02087
		P1712 02088
		P1712 02089
05	C	P1712 02090
		P1712 02091
		P1712 02092
		P1712 02093
10	C	P1712 02094
		P1712 02095
		P1712 02096
		P1712 02097
15	C	P1712 02098
		P1712 02099
		P1712 02100
		P1712 02101
20	C	P1712 02102
		P1712 02103
		P1712 02104
		P1712 02105
25	C	P1712 02106
		P1712 02107
		P1712 02108
		P1712 02109
30	C	P1712 02110
		P1712 02111
		P1712 02112
		P1712 02113
35	C	P1712 02114
		P1712 02115
		P1712 02116
		P1712 02117
40	C	P1712 02118
		P1712 02119
		P1712 02120
		P1712 02121
45	C	P1712 02122
		P1712 02123
		P1712 02124
		P1712 02125
50	C	P1712 02126
		P1712 02127
		P1712 02128
		P1712 02129
55	C	P1712 02130
		P1712 02131
		P1712 02132
		P1712 02133
60	C	P1712 02134
		P1712 02135
		P1712 02136
		P1712 02137
65	C	P1712 02138
		P1712 02139
		P1712 02140
		P1712 02141

55	C	PRESSURE RATIOS	P1712 02139
	C		P1712 02140
	C	DO 45 I=1,NPT	P1712 02141
	C	K=2*I+3	P1712 02142
	C	FMT(K)=F3	P1712 02143
	C	IF (PCP(I).GE.1000.) FMT(K)=F2	P1712 02144
	C	IF (PCP(I).GE.1000.) FMT(K)=F1	P1712 02145
	C	IF (PCP(I).GE.10000.) FMT(K)=F1	P1712 02146
	C	IF (PCP(I).GE.100000.) FMT(K)=F1	P1712 02147
	C	IF (PCP(I).GE.1000000.) FMT(K)=F1	P1712 02148
	C	IF (PCP(I).GE.10000000.) FMT(K)=F1	P1712 02149
	C	IF (PCP(I).GE.100000000.) FMT(K)=F1	P1712 02150
	C	IF (PCP(I).GE.1000000000.) FMT(K)=F1	P1712 02151
	C	IF (PCP(I).GE.10000000000.) FMT(K)=F1	P1712 02152
	C	IF (PCP(I).GE.100000000000.) FMT(K)=F1	P1712 02153
	C	IF (PCP(I).GE.1000000000000.) FMT(K)=F1	P1712 02154
	C	IF (PCP(I).GE.10000000000000.) FMT(K)=F1	P1712 02155
	C	IF (PCP(I).GE.100000000000000.) FMT(K)=F1	P1712 02156
	C	IF (PCP(I).GE.1000000000000000.) FMT(K)=F1	P1712 02157
	C	IF (PCP(I).GE.10000000000000000.) FMT(K)=F1	P1712 02158
	C	IF (PCP(I).GE.100000000000000000.) FMT(K)=F1	P1712 02159
	C	IF (PCP(I).GE.1000000000000000000.) FMT(K)=F1	P1712 02160
	C	IF (PCP(I).GE.10000000000000000000.) FMT(K)=F1	P1712 02161
	C	IF (PCP(I).GE.100000000000000000000.) FMT(K)=F1	P1712 02162
	C	IF (PCP(I).GE.1000000000000000000000.) FMT(K)=F1	P1712 02163
	C	IF (PCP(I).GE.10000000000000000000000.) FMT(K)=F1	P1712 02164
	C	IF (PCP(I).GE.100000000000000000000000.) FMT(K)=F1	P1712 02165
	C	IF (PCP(I).GE.1000000000000000000000000.) FMT(K)=F1	P1712 02166
	C	IF (PCP(I).GE.10000000000000000000000000.) FMT(K)=F1	P1712 02167
	C	IF (PCP(I).GE.100000000000000000000000000.) FMT(K)=F1	P1712 02168
	C	IF (PCP(I).GE.1000000000000000000000000000.) FMT(K)=F1	P1712 02169
	C	IF (PCP(I).GE.10000000000000000000000000000.) FMT(K)=F1	P1712 02170
	C	IF (PCP(I).GE.100000000000000000000000000000.) FMT(K)=F1	P1712 02171
	C	IF (PCP(I).GE.1000000000000000000000000000000.) FMT(K)=F1	P1712 02172
	C	IF (PCP(I).GE.10000000000000000000000000000000.) FMT(K)=F1	P1712 02173
	C	IF (PCP(I).GE.100000000000000000000000000000000.) FMT(K)=F1	P1712 02174
	C	IF (PCP(I).GE.1000000000000000000000000000000000.) FMT(K)=F1	P1712 02175
	C	IF (PCP(I).GE.10000000000000000000000000000000000.) FMT(K)=F1	P1712 02176
	C	IF (PCP(I).GE.100000000000000000000000000000000000.) FMT(K)=F1	P1712 02177
	C	IF (PCP(I).GE.1000000000000000000000000000000000000.) FMT(K)=F1	P1712 02178
	C	IF (PCP(I).GE.10000000000000000000000000000000000000.) FMT(K)=F1	P1712 02179
	C	IF (PCP(I).GE.100000000000000000000000000000000000000.) FMT(K)=F1	P1712 02180
	C	IF (PCP(I).GE.1000000000000000000000000000000000000000.) FMT(K)=F1	P1712 02181
	C	IF (PCP(I).GE.100.) FMT(K)=F1	P1712 02182
	C	IF (PCP(I).GE.1000.) FMT(K)=F1	P1712 02183
	C	IF (PCP(I).GE.100.) FMT(K)=F1	P1712 02184
	C	IF (PCP(I).GE.1000.) FMT(K)=F1	P1712 02185
	C	IF (PCP(I).GE.100.) FMT(K)=F1	P1712 02186
	C	IF (PCP(I).GE.1000.) FMT(K)=F1	P1712 02187
	C	IF (PCP(I).GE.100.) FMT(K)=F1	P1712 02188
	C	IF (PCP(I).GE.1000.) FMT(K)=F1	P1712 02189
	C	IF (PCP(I).GE.100.) FMT(K)=F1	P1712 02190

110	C	FMT(4) = FMT9X FMT(5) = FMT13 FMT(6) = FMT19 FMT(7) = F3 WRITE(6,FMT)(FR(I),I=1,4),(NV(J),J=2,NPT)	P1712 02191 P1712 02192 P1712 02193 P1712 02194 P1712 02195 P1712 02196 P1712 02197
115	C	CF = THPST COEFFICIENT FMT(6) = FMT(8) FMT(7) = F3 DO 212 I=2,NPT	P1712 02196 P1712 02196 P1712 02199 P1712 02200 P1712 02201 P1712 02202
120	C	212 V(I)=32.174*SPIK(I)/CSTR WRITE(6,FMT)FC1,FB,FB,FB,(V(J),J=2,NPT)	P1712 02203 P1712 02204 P1712 02205 P1712 02206 P1712 02207 P1712 02208
125	C	AREA RATIO FMT(5) = F3 DO 214 I = 2,NPT K = 2*1+3 FMT(K) = F4 IF (AEAT(I).GE.1.) FMT(K) = F3 IF (AEAT(I).GE.10.) FMT(K) = F2 IF (AEAT(I).GE.100.) FMT(K) = F1	P1712 02209 P1712 02210 P1712 02211 P1712 02212 P1712 02213 P1712 02214 P1712 02215 P1712 02216 P1712 02217 P1712 02218 P1712 02219 P1712 02220
130	C	214 CONTINUE WRITE(6,FMT)FA1,FA2,FB,FB,(AEAT(J),J=2,NPT)	P1712 02221 P1712 02222 P1712 02223 P1712 02224 P1712 02225 P1712 02226
135	C	VACUUM IMPULSE FMT(5) = FMT13 FMT(7) = F1 WRITE(6,FMT)(FA(I),I=1,4),(VAGI(J),J=2,NPT)	P1712 02227 P1712 02228 P1712 02229 P1712 02230 P1712 02231 P1712 02232
140	C	SPECIFIC IMPULSE WRITE(6,FMT)(F1(I),I=1,4),(SPIM(J),J=2,NPT)	P1712 02233 P1712 02234 P1712 02235 P1712 02236 P1712 02237 P1712 02238
145	C	WRITE(6,208) FMT(4) = F3 FMT(5) = FMT13 FMT(7) = F5 IF(COL) GO TO 312 WRITE(6,310)	P1712 02239 P1712 02240 P1712 02241 P1712 02242 P1712 02243
150	C	310 FORMAT(15H0MOLE FRACTIONS //)	
155	C	MOLE FRACTIONS - FROZEN LINE = 0 DO 431 K=1,MS V(LINE+1) = EN(K,1)/TOTN(1) IF (V(LINE+1).LT.(9.E-6)) GO TO 424 LINE = LINE+1 241LINE,1) = SUB(K,1)	

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160	Z(LINE,2) = 1.3(K,2) Z(LINE,3) = SUB(K,3) Z(LINE,4) = V(LINE)		P1712 02244 P1712 02245 P1712 02246	
424	IF (LINE.NE.4.AND.K.NE.NS) GO TO 430 IF (LINE.EQ.0) GO TO 312 WRITE (6,426) (Z(LN,1),Z(LN,2),Z(LN,3),Z(LN,4),LN=1,LINE)		P1712 02247 P1712 02248 P1712 02249	
165	426 FORMAT (1H,4TSAN,9.5,7X) LINE = 0		P1712 02250 P1712 02251	
	430 CONTINUE		P1712 02252	
	712 CALL OUT3		P1712 02253	
170	1000 RETURN END		P1712 02254 P1712 02255	

SUBROUTINE ROCKET FORTRAN EXTENDED VERSION 2.0		31/12/70	08:09.56:	PAGE NO. 2
55	GO TO 311 309 NP = 2 DO 310 I=1,24 IF (I.GT.2) GO TO 309 IF ((PCP(I).EQ.0.)OR.PCP(I).EQ.1.) GO TO 310 309 IF (PCP(I).EQ.0.) GO TO 311 NP = NP + 1 P(NP) = P(1)/PCP(I) 310 CONTINUE 311 NSUB=0 NSUP = 0 DO 320 I=1,13 IF (SUBART(I).NE.0.) NSUB=NSUB+1 IF (SUPART(I).NE.0.) NSUP=NSUP+1 320 CONTINUE WRITE (6,RTINP) SS0 = 0. ITROT = 3 IT = 1 C C C SET ASSIGNED P DO 902 IP = 1, NP PP = P(IP) CALL EQLORN T(NPT) = IT IF (IT.NE.0.) GO TO 333 IF (NPT.EQ.0) GO TO 1000 GO TO 900 333 PCP(NPT) = P(1)/PP IF (IP.GT.1) GO TO 199 C C C COMBUSTION CHAMBER TP = .FALSE. MP = .FALSE. SP = .TRUE. S0 = SSUM(1) PCP(2) = ((GAMMAS(1)+1.) / 2.) * ((GAMMAS(1) / (GAMMAS(1)-1.)) P(2) = P(1) / PCP(2) IT = 2 * IT / (GAMMAS(1)+1.) GO TO 900 199 IF (IP.GT.2) GO TO 900 C C C THROAT 190 IF (ITH.NE.2) GO TO 191 ITH = 2 GAMMAS(2) = 0. GO TO 900 191 OH = HSUM(1)-HSUM(2) DHSTAR = OH-GAMMAS(2) * IT * ENN / 2. IF (IDEPUG) WRITE (6,923) DHSTAR, HSUM(1), HSUM(2), PCP(2)	P1712 02309 P1712 02310 P1712 02311 P1712 02312 P1712 02313 P1712 02314 P1712 02315 P1712 02316 P1712 02317 P1712 02318 P1712 02319 P1712 02320 P1712 02321 P1712 02322 P1712 02323 P1712 02324 P1712 02325 P1712 02326 P1712 02327 P1712 02328 P1712 02329 P1712 02330 P1712 02331 P1712 02332 P1712 02333 P1712 02334 P1712 02335 P1712 02336 P1712 02337 P1712 02338 P1712 02339 P1712 02340 P1712 02341 P1712 02342 P1712 02343 P1712 02344 P1712 02345 P1712 02346 P1712 02347 P1712 02348 P1712 02349 P1712 02350 P1712 02351 P1712 02352 P1712 02353 P1712 02354 P1712 02355 P1712 02356 P1712 02357 P1712 02358 P1712 02359 P1712 02360 P1712 02361		

923 FORMAT(4E25.8)

CH = OMSTAR/DM

IF (DM.LT.0.) OH=OH

IF (DM.LT.0.4E-04) IFROT.EQ.0) GO TO 900

IF (JSOL.NE.0) ITH = 1

IF (JSOL.EQ.0) ITH=2

IF (ITH.EQ.0) GO TO 192

C
C SPECIAL THROAT INTERPOLATION IF ITH = 2
C

115

OLNI = .5*TT*ENN/(HSUM(1)-HSUM(2))

AA(ITH) = .5*OLNI*(2.*OLNI*(54*HMAS(2)-1.)/GAMMAS(2))

XX = ALOG(PCP(2))

98(ITH) = 1./GAMMAS(2)-OLNI-2.*XX*AA(ITH)

GC(ITH) = ENW*TT/(PP*(HSUM(1)-HSUM(2))*0.5)

CC(ITH) = ALOG(CC(ITH))-XX*(38(ITH)+AA(ITH)*XX)

IF (ITH.EQ.1) GO TO 192

H8(1)=8E(1)-88(2)

H8(2)=8E(2)-88(2)

H8(3)=8E(3)-88(2)

PCP(2) = (-39(1)+(88(1)*88(1)-4.*AA(1)*(CC(1)-CC(2))*0.5)/(2.*AA(1))

1) PCP(3)=EXP(PCP(2))

GO TO 193

192 PCP(2) = PCP(2)/(1.+2.*DHSTAR/(ENN*TT*(GAMMAS(2)+1.)))

193 P(2) = P(1) / PCP(2)

PP = P(2)

IFROT = ITROT-1

CALL EOLBRN

IF (TT.EQ.0.) GO TO 1000

GO TO 190

88 K = 0

IF (.NOT.EQ.0.AND. FROZ) GO TO 990

IF (IP.EQ.NP.OR.TT.EQ.0.) GO TO 860

K = NPT

IF (NPT.NE.13) GO TO 870

860 CALL RK70T

IFLGG=1

IF ((NSUB + NSUP).NE.0) CALL RATIO

IF (K.EQ.0) GO TO 930

WRITE(6,865)

865 FORMAT(1H1)

NPT = 2

870 NPT = NPT + 1

C
C SAVE COMPOSITIONS FOR ESTIMATES OF NEXT POINT
C

DO 880 I = 1,NS

ENTINPT) = ENTINPT

880 CONTINUE

902 CONTINUE

990 IF (FROZ) CALL FROZEN

1000 RETURN

199

P1712 02362

P1712 02363

P1712 02364

P1712 02365

P1712 02366

P1712 02367

P1712 02368

P1712 02369

P1712 02370

P1712 02371

P1712 02372

P1712 02373

P1712 02374

P1712 02375

P1712 02376

P1712 02377

P1712 02378

P1712 02379

P1712 02380

P1712 02381

P1712 02382

P1712 02383

P1712 02384

P1712 02385

P1712 02386

P1712 02387

P1712 02388

P1712 02389

P1712 02390

P1712 02391

P1712 02392

P1712 02393

P1712 02394

P1712 02395

P1712 02396

P1712 02397

P1712 02398

P1712 02399

P1712 02400

P1712 02401

P1712 02402

P1712 02403

P1712 02404

P1712 02405

P1712 02406

P1712 02407

P1712 02408

P1712 02409

P1712 02410

P1712 02411

P1712 02412

P1712 02413

P1712 02414

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160 ~~END~~ ~~P1712~~ 02419


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55      DO 168 I=1,L
          IF (LLMT(I).EQ.MT(K)) GO TO 820
          168 CONTINUE
          DO 819 J=1,L
              819 A(I,J,NS) = 0.
              GO TO 7
          820 A(I,NS) = 819
          825 IF (NS.EQ.HAXNS) GO TO 870
              IUSE(NS) = 0
              IF (PHAZ.EQ.GAS) GO TO 170
              NC = NC+1
              TEMP(NC,1) = T1
              TEMP(NC,2) = T2
              IX = IX+1
              IF (IUSE(NS-1).EQ.0 .OR. NC.EQ.1) GO TO 145
              DO 830 I=1,L
                  830 CONTINUE
                  IF (A(I,NS).NE.A(I,NS-1)) GO TO 145
                  IX = IX+1
                  145 IUSE(NS) = -IX
                  170 NS = NS+1
                  GO TO 7
              870 WRITE(6,871) (SUB(NS,J),J=1,3)
                  871 FORMAT (45H0DIMENSIONS IN/SPECIES/100 SHALL TO CONSIDER ,3A4)
                  GO TO 7
              171 NS = NS-1
                  NEWR = .FALSE.
                  WRITE(6,172)
                  172 FORMAT (42H0SPECIES BEING CONSIDERED IN THIS SYSTEM )
                  DO 174 I=1,NS,5
                      174 IF (NS.LT.I5) I5=NS
                          174 WRITE (6,176) (DATE(1,J),DATE(2,J),SUB(J,1),SUB(J,2),SUB(J,3),J=I,
                              1 I5)
                          176 FORMAT (5(5X,2A3,2X,3A4))
                          RETURN
                  END
          90

```

P1712 02469
 P1712 02470
 P1712 02471
 P1712 02472
 P1712 02473
 P1712 02474
 P1712 02475
 P1712 02476
 P1712 02477
 P1712 02478
 P1712 02479
 P1712 02480
 P1712 02481
 P1712 02482
 P1712 02483
 P1712 02484
 P1712 02485
 P1712 02486
 P1712 02487
 P1712 02488
 P1712 02489
 P1712 02490
 P1712 02491
 P1712 02492
 P1712 02493
 P1712 02494
 P1712 02495
 P1712 02496
 P1712 02497
 P1712 02498
 P1712 02499
 P1712 02500
 P1712 02501
 P1712 02502
 P1712 02503
 P1712 02504
 P1712 02505

```

SUBROUTINE SET(ONE,TWO,THREE,ARG,MAL)
C
C   USED FOR AREA RATIO INTERPOLATION ONLY
C   SETS UP ALL 4 BY 5 MATRICES
05  C   DOUBLE PRECISION A,ANS,G,X
C
C   DIMENSION ANS(6),ONE(2),TWO(2),THREE(2),A(20,21)
C
C   COMMON/DOUBLE/G(20,21),X(20)
C   COMMON/INDEX/ IDEBUS,CONVG,TP,HP,SP,HPSP,TPSP,MOLES,MP,NT,NPT,I,ANS,
1   KMAT,IMAT,IC1,N,J,NOMIT,IF,NEWR,NSUB,NSUP,ITN,CPCVFR,CPCVEQ
2   TIONS,TNO,INSEF,JSOI,JIU,KASE(14),NREAC,IC,IO2
C
C   EQUIVALENCE (G,A),(X,ANS)
C
DO 8 J=1,2
A(J,5)=ALOG(ONE(J))
A(J,2)=TWO(J)
A(J,1)=1.0
A(J,2,1)=0.0
A(J,2,2)=1.0
DO 1 J=2,3
A(I,J+1)=A(I,2)**J
NXP=J-1
A(I+2,J+1)=A(I,2)**NXP*FLOAT(J)
1 CONTINUE
IMAT=4
CALL HGAUSD
MAL=ANS(1)
SUM=ALOG(ARG)
DO 10 J=1,3
MAL=MAL+SUM**J*(ANS(J+1))
10 CONTINUE
MAL=EXP(MAL)
RETURN
END
40

```

P1712 02506
 P1712 02507
 P1712 02508
 P1712 02509
 P1712 02510
 P1712 02511
 P1712 02512
 P1712 02513
 P1712 02514
 P1712 02515
 P1712 02516
 P1712 02517
 P1712 02518
 P1712 02519
 P1712 02520
 P1712 02521
 P1712 02522
 P1712 02523
 P1712 02524
 P1712 02525
 P1712 02526
 P1712 02527
 P1712 02528
 P1712 02529
 P1712 02530
 P1712 02531
 P1712 02532
 P1712 02533
 P1712 02534
 P1712 02535
 P1712 02536
 P1712 02537
 P1712 02538
 P1712 02539
 P1712 02540
 P1712 02541
 P1712 02542
 P1712 02543
 P1712 02544
 P1712 02545

SUBROUTINE VISCON(NS,NPT,SUB,EN,TOTN,I)

C
C THIS SUBROUTINE COMPUTES THE VISCOSITY AND THE CONDUCTIVITY
C OF A GAS MIXTURE CONSISTING OF 5 GASEOUS SPECIES.
C GASEOUS SPECIES TO BE CONSIDERED ARE H2O,CO,H2,CO2,AND N2.

05

COMMON/PROCENT/FMOLE

C
C DIMENSION SUB(150,3),EN(150,13),TOTN(13),T(13),SPECES(5),EK(5),
C 1SIG(5),MGTH(5),TE(33),OMEG(33),FMOLE(15),VIS(5),COND(5),
C 2VISNIX(13),CONMIX(13)

10

C
C DATA (SPEC(I),I=1,5)/2.024,3.706,2.915,3.897,3.749/
C DATA (SIG(I),I=1,5)/2.024,3.706,2.915,3.897,3.749/
C DATA (TE(I),I=1,5)/230.9,89.0,38.0,213.0,79.87

15

C
C DATA (MGTH(I),I=1,5)/16.28,0.12,0.16,4.4,0.28,0.2/
C DATA (OMI,CON2,CONS/ 0.090026593,0.37019891,0.3535539059/
C DATA (TE(I),I=1,3)/1.0,1.2,1.4,1.6,1.8,2.0,2.2,2.4,2.6,2.8,3.0,
C 13.2,1.4,3.6,3.8,4.3,5.0,6.0,7.0,8.0,9.0,10.0,11.0,12.0,13.0,14.0,
C 215.8,16.0,32.0,64.0,128.0,256.0,512.0/
C DATA (OMEG(I),I=1,33)/1.5918,1.4588,1.3557,1.2900,1.2216,1.1791,
C 11.1377,1.1066,1.0803,1.0579,1.0385,1.0214,1.0063,0.9928,0.9807,
C 20.9696,0.9265,0.8960,0.8725,0.8536,0.8378,0.8282,0.8123,0.8017,
C 30.7922,0.7836,0.7736,0.7683,0.7639,0.7622,0.7614,0.7606,0.7600,
C 30.7922,0.7836,0.7736,0.7683,0.7639,0.7622,0.7614,0.7606,0.7600

C

C
C VALUES FOR VISCOSITY AND CONDUCTIVITY WILL BE COMPUTED AT THE
C CHARGER, THE THROTT, AND AT THE ASSIGNED EXITS.

C

WRITE(6,9999) NS,NPT

9999 FORMAT(2I10)

FMOLE=0.0

DO 1000 M=1,NPT

93

C
C COMPUTE THE MOLE FRACTIONS OF THE 5 GASEOUS SPECIES.

DO 20 I=1,5

DO 10 J=1,NS

35

C
C SEARCH THE ARRAY SUB(J,I) FOR THE 5 NEEDED SPECIES. WHEN ONE OF THE
C NEEDED SPECIES IS FOUND, COMPUTE THE MOLE FRACTION.

C

IF (SPEC(I),NE,SUB(J,I)) GO TO 10

FMOLE(I)=EN(J,M)/TOTN(M)

WRITE(6,9000) SPEC(I),SUB(J,I),EN(J,M),TOTN(M),FMOLE(I),I,J,M

9000 FORMAT(1X,2A10,3F15.8,3I5)

IF (M.EQ.1) FMOLE=FMOLE/FMOLE(I)*100.

GO TO 20

10 CONTINUE

C
C IF THE SPECIE CANNOT BE LOCATED IN THE ARRAY SUB(J,I), SET THE MOLE
C FRACTION TO MINUS ONE.

C

FMOLE(I)=-1.0

20 CONTINUE

50

C
C COMPUTE THE VISCOSITY AND THE CONDUCTIVITY FOR EACH OF THE 5 SPECIES

C

P171201 00010
P171201 00011
P171201 00012
P171201 00013
P171201 00014
P171201 00015
P171201 00016
P171201 00017
P171201 00018
P171201 00019
P171201 00020
P171201 00021
P171201 00022
P171201 00023
P171201 00024
P171201 00025
P171201 00026
P171201 00027
P171201 00028
P171201 00029
P171201 00030
P171201 00031
P171201 00032
P171201 00033
P171201 00034
P171201 00035
P171201 00036
P171201 00037
P171201 00038
P171201 00039
P171201 00040
P171201 00041
P171201 00042
P171201 00043
P171201 00044
P171201 00045
P171201 00046
P171201 00047
P171201 00048
P171201 00049
P171201 00050
P171201 00051
P171201 00052
P171201 00053
P171201 00054
P171201 00055
P171201 00056
P171201 00057
P171201 00058
P171201 00059
P171201 00060
P171201 00061
P171201 00062

31/12/78

00.09.56.

PAGE NO. 3

C-----CONDUCTIVITY OF MIXTURE

```
110      C
          C CONMIX(N)=CONMIX(M)+FMOLE(I)*CONM(I)/SUM
          WRITE(6,9009) VISMIX(M),CONMIX(M),M
          9009 FORMAT(1X,2F15.11,3X,15)
          200 CONTINUE
          1000 CONTINUE
          WRITE(6,2010) (VISMIX(I),I=1,NPT)
          2010 CONTINUE
          WRITE(6,2100) (CONMIX(I),I=1,NPT)
          2000 FORMAT(1H ,*VISC, 5/CM-SEC*,13F9.6)
          2100 FORMAT(1H ,*C, 6AL/6-SEC-K*,13F9.6)
          RETURN
          END
```

P171201 00116
P171201 00117
P171201 00118
P171201 00119
P171201 00120
P171201 00121
P171201 00122
P171201 00123
P171201 00124
P171201 00125
P171201 00126
P171201 00127
P171201 00128

APPENDIX II
POLYNOMIAL FIT PROGRAM

```

PROGRAM SLSCF(INPUT,OUTPUT)
  DIMENSION TT(100),CPR(100),HTR(100),STR(100)
  DIMENSION CCPR(100),CHTR(100),CSTR(100)
  DIMENSION NPT(2),NAME(6)
  COMMON/PATRIX/ G(10,11),X(10),IMAY
  R=1-99726
  ASSIGN 500 TO MEOF
  IF(EOF(MEOF)) 500,500,1
  1 READ 40,MO,NPT,NAME
  40 FORMAT(F10.1,2I3,4X,6A10)
  PRINT 112,NAME,MO
  112 FORMAT('111,29X,6A10//1P',5NH0 = ,F10.1//)
  KPT=0
  111 KPT=KPT+1
  NVAL=NPT(KPT)
  READ 6,(ITT(K),K=1,NVAL)
  READ 7,(CPR(K),K=1,NVAL)
  READ 7,(HTR(K),K=1,NVAL)
  DC 22 I=1,NVAL
  22 HTR(I)=HTR(I)+1000.*MO
  READ 7,(STR(K),K=1,NVAL)
  6 FORMAT(20F4.0)
  7 FORMAT(10F8.3)
  DC 16 I=1,10
  DC 15 J=1,11
  G(I,J)=0.
  15 CONTINUE
  16 CONTINUE
  SLT=0.
  SLT2=0.
  SLT3=0.
  SLT4=0.
  SLT5=0.
  SLT6=0.
  SLT7=0.
  SLT8=0.
  SLT9=0.
  DO 100 K=1,NVAL
  Y=TT(K)
  CP=CPR(K)/R
  HT=HTR(K)/(R*T)
  ST=STR(K)/R
  TLOG=ALOG(T)
  T2=T**2
  T3=T**3
  T4=T**4
  T5=T**5
  T6=T**6
  T7=T**7
  T8=T**8
  T9=T**9
  TREC=1.0/T
  TM2=1.0/T2
  SUMT=SUMT+Y

```


15.40.00.

05/01/71

FURTRAN EXTENDED VERSION 2.0

SLSQF

PROGRAM

```

55      SUMT2=SUMT2+T2
        SUMT3=SUMT3+T3
        SUMT4=SUMT4+T4
        SUMT5=SUMT5+T5
        SUMT6=SUMT6+T6
        SUMT7=SUMT7+T7
        SUMT8=SUMT8+T8
60      SUMT2=SUMT2+TM2
        G(1,1)=G(1,1)+2.*TLOG**2
        G(1,2)=G(1,2)+(1.5+TLOG)*T
        G(1,3)=G(1,3)+(4./3.+5.*TLOG)*T2
        G(1,4)=G(1,4)+(1.25+TLOG/3.)*T3
        G(1,5)=G(1,5)+(1.2+TLOG/4.)*T4
        G(1,6)=G(1,6)+TREC
        G(1,7)=G(1,7)+TLOG
        G(1,11)=G(1,11)+(CP+HT+ST+TLOG
70      G(2,11)=G(2,11)+(CP+.5*HT+ST)*T
        G(3,11)=G(3,11)+(CP+HT/3.+5*ST)*T2
        G(4,11)=G(4,11)+(CP+HT/4.+ST/3.)*T3
        G(5,11)=G(5,11)+(CP+HT/5.+ST/4.)*T4
        G(6,11)=G(6,11)+HT*TREC
        G(7,11)=G(7,11)+ST
75      IF(X.GT.1) GO TO 50
        G(1,8)=1.0
        G(1,9)=1.0
        G(1,10)=TLOG
        G(2,6)=FLOAT(INVAL)/2.0
        G(2,8)=T
        G(2,9)=1/2.0
        G(2,10)=1
        G(3,8)=12
        G(3,9)=12/3.
        G(3,10)=1/2.
        G(4,8)=13
        G(4,9)=13/4.
        G(4,10)=13/3.
        G(5,8)=14
        G(5,9)=14/5.
        G(5,10)=1/4.
        G(6,9)=TREC
        G(7,7)=FLOAT(INVAL)
95      G(7,10)=1.0
        G(8,11)=CP
        G(9,11)=HT
        G(10,11)=ST
        50 CONTINUE
        100 CONTINUE
        G(2,2)=G(2,2)+G(1,1)*SUMT2
        G(2,3)=G(2,3)+G(1,3)*SUMT3
        G(2,4)=G(2,4)+G(1,4)*SUMT4
        G(2,5)=G(2,5)+G(1,5)*SUMT5
        G(2,7)=SUMT
        G(3,3)=G(3,3)+G(1,3)*SUMT4
105

```

```

110      G(3,4)=(5./4.)*SUMT5
          G(3,5)=(143./120.)*SUMT6
          G(3,6)=SUMT7/3.
          G(3,7)=SUMT2/2.
          G(4,4)=(169./144.)*SUMT6
          G(4,5)=(117./15.)*SUMT7
          G(4,6)=SUMT2/4.
          G(4,7)=SUMT3/3.
          G(5,5)=(441./400.)*SUMT6
          G(5,6)=SUMT3/5.
          G(5,7)=SUMT4/4.
          G(6,6)=SUMT2
          DO 200 I=1,10
            DO 210 J=1,10
              IF(I.EQ.J) GO TO 210
              G(I,J)=G(I,J)
            GO 210 CONTINUE
          210 CONTINUE
          100 CONTINUE
          PRINT 92
          IF(ORIG(1).NE.0.0) GO TO 190
          92 FORMAT(1H ,VALUES OF G*)
          DO 90 I=1,10
            PRINT 91,(G(I,J),J=1,11)
          91 FORMAT(1X,15E11.5)
          90 CONTINUE
          190 IMAT=10
          CALL HGAUSS
          PRINT 94
          94 FORMAT(1H ,COEFFICIENTS ARE*)
          PRINT 192,X
          192 FORMAT(1X,7E15.8/1X,3E15.8)
          DO 401 I=1,NVAL
            T=TT(I)
            T2=T*T
            T3=T2*T
            T4=T3*T
            T5=T4*T
            T6=T5*T
            T7=T6*T
            T8=T7*T
            T9=T8*T
            T10=T9*T
            TLOG=ALOG(T)
            CCPA(I)=X(1)+X(2)*T+X(3)*T2+X(4)*T3+X(5)*T4
            CCPB(I)=CCPR(I)*R
            CSTR(I)=(X(1)+X(2)*T/2.+X(3)*T2/3.+X(4)*T3/4.+X(5)*T4/5.)*T+X(6)
          100 R
            CSTR(I)=CSTR(I)-H01/1000.
            CSTR(I)=(X(1)+TLOG+X(2)*T+X(3)*T2/2.+X(4)*T3/3.+X(5)*T4/4.+X(7)
          1R
          400 CONTINUE
          PRINT 401
          401 FORMAT(1H , , T CP CCP HT CHT T JST
          1 DCF QMT DST//)
          DO 410 I=1,NVAL
            DCPR=ABS(CPR(I)-CCPR(I))
            DTR=(HT(I)-H01)/1000.
            DMS=ABS(DIR-CMTR(I))
            DSTR=ABS(STR(I)-CSTR(I))

```

PROGRAM	SLSQF	FURTRAN EXTENDED VERSION 2.0	05/01/71	15.40.08.	PAGE NO. 4
160	411	FORMAT(1H,1X,F5.0,9F8.3) PRINT 411,IT(1),CPR(1),CCPR(1),DIR,CHTR(1),STR(1),CSIR(1),DCPR, 1CHTR,OSTR			
165	410	CCTINUE GC 10 (111,1),KPT 500 CONTINUE END			

SUBROUTINE MGAUSD

C SOLVE ANY LINEAR SET OF UP TO 20 EQUATIONS

C DOUBLE PRECISION G,X,COEFX(20),SUM,Z
C DIMENSION COEFX(20)

C COMMON/MATRIX/ G(10,10),X(10),IMAT

C EQUIVALENCE (IUSE,IMAT)

C DATA SIGNO/1.E+38/
C DATA SIGNO/1.E+320/

C BEGIN ELIMINATION OF NTH VARIABLE

C IUSE1=IUSE+1

C DO 45 NN=1,IUSE

C IF (NN-IUSE) 8,83,8
C IF (G(NN,NN)) 31,23,31

C SEARCH FOR MAXIMUM COEFFICIENT IN EACH ROW

C DO 10 I=NN,IUSE

C COEFX(I) = SIGNO

C IF (G(I,NN).EQ.0.) GO TO 18

C COEFX(I) = 0.

C DO 10 J=NN,IUSE1

C SUM = G(I,J)

C IF (SUM-11.11) SUM=-SUM

C IF (J.NE.NN) GO TO 9

C Z = SUM

C GO TO 10

C 9 IF (SUM.GT.COEFX(I)) COEFX(I)=SUM

C 10 CONTINUE

C COEFX(I) = COEFX(I)/Z

C 18 CONTINUE

C TEMP = BIGNC

C I=0

C 20 DO 22 J=NN,IUSE

C IF (COEFX(J)-TEMP) 87,22,22

C 27 TEMP=COEFX(J)

C I=J

C 22 CONTINUE

C IF (I) 20,23,28

C INDEX I LOCATES EQUATION TO BE USED FOR ELIMINATING THE NTH

C VARIABLE FROM THE REMAINING EQUATIONS

C INTERCHANGE EQUATIONS I AND NN

C 28 IF (NN-I) 29,31,29

C 29 DO 30 J=NN,IUSE1

```

55      Z=G(I,J)
      G(I,J)=G(MN,J)
      G(MN,J)=Z
      30 CONTINUE
C
60      C-----DIVIDE MTH ROW BY MTH DIAGONAL ELEMENT AND ELIMINATE THE MTH
      C      VARIABLE FROM THE REMAINING EQUATIONS
      C
      31 K = MN + 1
      DO 36 J = K, IUSE1
      IF((I(MN,MN).EQ.0.) GO TO 23
      G(MN,J) = G(MN,J) / G(MN,MN)
      36 CONTINUE
      IF(K-IUSE1) 88,45,88
      88 DC 44 I = K,IUSE
      40 DO 44 J = K, IUSE1
      G(I,J) = G(I,J) - G(I,MN)*G(MN,J)
      44 CONTINUE
      45 CONTINUE
C
75      C      BACKSOLVE FOR THE VARIABLES
      C
      47 J = K - 1
      K = IUSE
      X(K) = 0.000
      X(K) = 0.0
      SUM = 0.0
      IF(IUSE = J) 51,48,48
      48 DC 50 I = J,IUSE
      SUM = SUM + G(K,I)*X(I)
      50 CONTINUE
      51 X(K) = G(K,IUSE1) - SUM
      K = K - 1
      IF (K) 47,151,47
      23 IUSE = IUSE-1
      151 RETURN
      END
90

```

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