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AD

**RDTE PROJECT NO. IX141807D174
USATECOM PROJECT NO. 4-6-0500-01
USAATA PROJECT NO. 66-06**

**ENGINEERING FLIGHT TEST
AH-1G HELICOPTER (HUEYCOBRA)**

PHASE D

**PART 1
HANDLING QUALITIES**

FINAL REPORT

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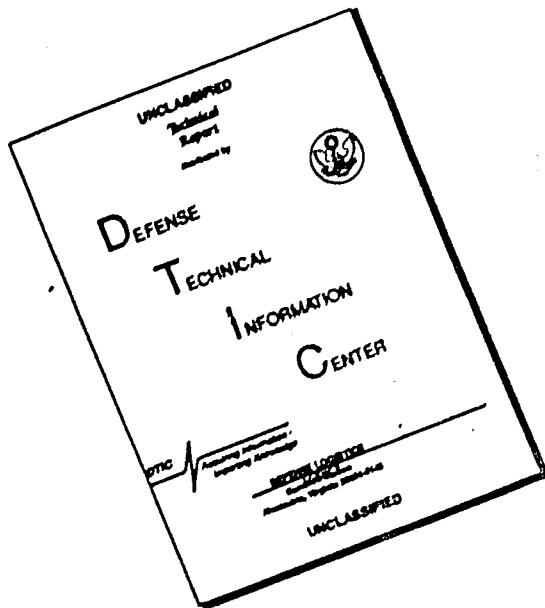
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DECEMBER 1970

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**US ARMY AVIATION SYSTEMS TEST ACTIVITY
EDWARDS AIR FORCE BASE, CALIFORNIA 93523**

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ABSTRACT

The Phase D, Part 1 airworthiness and qualification handling qualities tests of the AH-1G helicopter were conducted at Edwards Air Force Base, California, and auxiliary test sites during the period 13 June 1968 through 29 July 1969. Handling qualities were quantitatively evaluated to determine model specification compliance and to obtain mission suitability information for inclusion in technical manuals and other publications. The AH-1G met all contractual requirements of MIL-H-8501A except for paragraphs 3.2.4 (cyclic force gradients), 3.2.7 (cyclic breakout forces), 3.5.4.1 (take-off and landing in winds), 3.5.5 (autorotational entry) and 3.5.5.1 (aircraft reaction to engine failure). Tests were not conducted to verify compliance with paragraphs 3.5.4.3 (autorotational landings), 3.5.4.4 (autorotational landings) and 3.5.4.5 (autorotational landing with flotation gear) of MIL-H-8501A. By contractual agreement, the handling qualities requirements presented in paragraphs 3.3 (directional and lateral handling qualities) and 3.6 (handling qualities during instrument flight) of MIL-H-8501A were not applicable. The handling qualities of the AH-1G are acceptable throughout the flight envelope except for the four deficiencies for which correction is mandatory for mission accomplishment: excessive cyclic control breakout forces; inadequate directional control; inability to achieve maximum tail rotor blade angle (19 deg) when full left directional control is applied for all conditions with the present directional control/yaw SCAS geometry; and excessive tail rotor horsepower required for hovering and translational flight. In addition, there were five shortcomings for which corrective action is desirable.

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INTRODUCTION

BACKGROUND

1. In October 1965, the Department of the Army directed the US Army Materiel Command (USAMC) to conduct an expedited comparative evaluation of a selected group of three helicopters to fulfill the immediate requirement for an armed helicopter. A flight test program was conducted on the three aircraft by the US Army Aviation Systems Test Activity (USAATA) at Edwards Air Force Base (AFB), California, from 13 November to 1 December 1965. The AH-1G Huey-Cobra was the aircraft selected from the evaluation to meet this requirement.
2. On 17 August 1966, USAATA was directed by the US Army Test and Evaluation Command (USATECOM) to perform Phase B and Phase D testing of the AH-1G helicopter (ref 1, app 1). A test plan for the Phase B engineering test was submitted by USAATA in April 1967 and approved by the US Army Aviation Systems Command (USAAVSCOM). Phase B tests were conducted at different test sites and geographical locations from 3 April 1967 to 3 May 1968 utilizing several aircraft. The results of these tests are contained in references 2 through 8. The test plan for the Phase D program (ref 9) was initially submitted in August 1967 and was approved by USAAVSCOM on 24 October 1968. The Phase D plan of test was amended on 5 November 1968 (ref 10) to include an additional test requested by USAAVSCOM. Two aircraft were used for the Phase D test program to reduce the calendar time. One of the test aircraft was a prototype (aircraft S/N 6615247), and the other was a production model (aircraft S/N 6715695). The results of the Phase D handling qualities tests are presented in this report (Part 1). The Phase D performance capabilities and vibration characteristics are presented in other reports (Part 2 and Part 3). No wing store jettison or armament subsystem firing tests were conducted during the Phase D program since adequate testing had been accomplished in those areas during the AH-1G Phase B program.

TEST OBJECTIVES

3. The objectives of the AH-1G Phase D test program were as follows:
 - a. To provide information for technical manuals and other service publications.

- b. To determine compliance with applicable military specifications.
- c. To determine compliance with contract guarantees.
- d. To evaluate operational suitability for the armed helicopter mission.

DESCRIPTION

4. The AH-1G helicopter manufactured by Bell Helicopter Company (BHC) was designed specifically to meet the US Army requirements for an armed helicopter. Tandem seating is provided for a two-man crew. The main rotor system is a two-bladed, semi-rigid, "door hinge" type with the stabilizer bar removed. A conventional antitorque rotor is located near the top of the vertical stabilizer. The AH-1G is equipped with a three-axis stability and control augmentation system (SCAS) to improve the aircraft handling qualities. The helicopter is powered by a Lycoming T53-L-13 turboshaft engine rated at 1400 shaft horsepower (shp) at sea level (SL) under standard day, uninstalled conditions. The engine is derated to 1100 shp due to the maximum torque limit of the main transmission. Distinctive features of the AH-1G are: the narrow fuselage (36 inches), the stub midwing with four external store stations, the integral chin turret. The flight control system is of the mechanical, hydraulically boosted, irreversible type with conventional helicopter controls in the aft cockpit (pilot station). The controls in the forward cockpit (copilot/gunner station) consist of conventional antitorque pedals and sidarm collective and cyclic controls. An electrically operated force trim system is connected to the cyclic and directional controls to induce artificial feel and to provide positive control centering. The elevator is synchronized with the cyclic stick. The armament configurations are changed by varying the wing stores and chin turret configuration. The pilot operates the wing stores and can fire the chin turret only in the stowed position. The copilot/gunner operates the flexible turret and can also fire the wing stores in an emergency. The wing stores can be jettisoned by either the pilot or gunner in case of emergency. The design gross weight (grwt) for the AH-1G is 6600 pounds, and the maximum grwt is 9500 pounds. More detailed aircraft information and operating limits of the AH-1G are presented in appendix II.

SCOPE OF TEST

5. During the AH-1G Phase D test program, 256 flights were conducted for a total of 368.8 flight hours of which 227.9 hours were productive test hours. Testing was conducted in California, from 12 June 1968 to 29 July 1969, at Shafter Airport (420-ft elevation), Edwards AFB (2300-foot elevation) and at high-altitude test sites near Bishop (4120-, 7010- and 9500-foot elevations). Testing was conducted to determine aircraft performance, handling qualities and vibration characteristics. Two aircraft were utilized during this test program. An early prototype aircraft (S/N 6615247) was utilized primarily for performance tests although a limited amount of stability and control testing was accomplished. A more current production aircraft (S/N 6715695) was utilized for the majority of stability and control testing. This second test aircraft was utilized not only to decrease total calendar time required for testing, but also to comply with USAASTA policy which recognized the desirability of performing handling qualities tests on a production aircraft. A breakdown of flights and flight hours by individual aircraft is presented in table 1. Of these totals, 83 flights (84.5 productive flight hours) were devoted primarily to quantitative stability and control testing. Throughout the test program, qualitative evaluations of handling qualities were made. This report contains only the results of the handling qualities tests. The various aircraft configurations evaluated during the handling qualities portion of the program are listed in table 2.

Table 1. Test Flights and Productive Flight Time.

Test Helicopter	Total Test Flights	Handling Qualities Test Flights	Total Productive Test Hours	Productive Handling Qualities Test Hours
S/N 6615247 (prototype aircraft) ¹	201	28	161.8	18.4
S/N 6715695 (production aircraft) ²	55	55	66.1	66.1
Total (both aircraft)	256	83	227.9	84.5

¹Equipped with TAT-102A turret: one 7.62mm minigun (XM134).

²Equipped with XM28 turret in the hybrid configuration: one 7.62mm minigun (XM134) and one 40mm grenade launcher (XM129).

Table 2. Aircraft Armament Configurations.

Configuration	Armament Subsystems
Clean	TAT-102A or XM28 turret, no external wing stores
Outboard alternate	TAT-102A or XM28 turret, one XM159 outboard each wing
Heavy scout	TAT-102A or XM28 turret, one XM18 inboard each wing, one XM159 outboard each wing
Heavy hog	TAT-102A or XM28 turret, two XM159 each wing

6. The test program was conducted within the limitations established by the AH-1G Safety-of-Flight Release issued by USAAVSCOM (refs 11 and 12, app I).

7. The empty weight of the test aircraft in a clean configuration with test instrumentation installed was 5790 pounds with the center of gravity (cg) at fuselage station (FS) 205.97 for aircraft S/N 6615247 and 5920 pounds with the cg at FS 200.59 for aircraft S/N 6715695.

8. The AH-1G was evaluated as an armed tactical helicopter, capable of day or night operation from prepared or unprepared areas. The handling qualities of the AH-1G helicopter were evaluated to determine compliance with the requirements of paragraph 3.5.2 of the detail specification (ref 13, app I). The Handling Qualities Rating Scale (HQRS) used throughout this report is presented as appendix III. Specific conditions for each test are presented in the Results and Discussion section of this report.

METHOD OF TEST

9. Test methods and data reduction procedures used in these tests are established engineering flight test techniques and are described briefly in appendix IV. All flights were conducted and supported by USAASTA personnel. Tests were conducted in nonturbulent atmospheric conditions.

10. The flight test data were obtained from test instrumentation located on the pilot panel, copilot/gunner panel, photopanel and with oscillograph records. A detailed listing of the test instrumentation is included in appendix V.

CHRONOLOGY

11. The chronology of the AH-1G Phase D, Part 1 test program is as follows:

Phase B flight test completed on aircraft S/N 6615247	3 May	1968
Phase D flight test commenced on aircraft S/N 6615247	13 June	1968
Aircraft S/N 6715695 received	8 August	1968
Flight test commenced on aircraft S/N 6715695	4 September	1968
Flight test completed on aircraft S/N 6715695	10 October	1968
Flight test completed on aircraft S/N 6615247	29 July	1969
Advance copy submitted	15 April	1970

RESULTS AND DISCUSSION

GENERAL

12. This report presents the results of the engineering Phase D handling qualities flight tests of the AH-1G helicopter. The test data obtained during these tests were used for determining compliance with the detail specification (ref 13, app 1), and Military Specification MIL-H-8501A, (ref 14) and to provide information for use in technical manuals and other publications. The AH-1G met all contractual handling qualities requirements of MIL-H-8501A except for paragraphs 3.2.4, 3.2.7, 3.5.4.1, 3.5.5 and 3.5.5.1. Tests were not conducted to verify compliance with paragraphs 3.5.4.3, 3.5.4.4 and 3.5.4.5 of MIL-H-8501A. By contractual agreement, the handling qualities requirements presented in paragraphs 3.3 and 3.6 of MIL-H-8501A were not applicable to the AH-1G (app VI). Aircraft compliance with the vibration characteristics requirement presented in paragraph 3.7 is discussed in Part 3 of this report. There are four deficiencies for which correction is mandatory for adequate mission accomplishment: excessive cyclic control breakout forces; inadequate directional control; inability to achieve maximum tail rotor blade angle (19 degrees) when full left directional control/yaw SCAS geometry; and excessive tail rotor horsepower required for hovering and translational flight. There are five shortcomings for which corrective action is desirable: neutral static longitudinal stability at airspeeds near the limit airspeed (V_L); increase in right directional control displacement with increasing airspeed in a dive; directional instability between 10 and 18 knots at relative wind azimuths between 210 and 230 degrees; deterioration of longitudinal dynamic stability of the AH-1G with the SCAS inoperative; and decrease in lateral-directional damping with the SCAS inoperative.

13. The proposed Military Specification MIL-H-8501B (ref 15, app 1) was used in addition to MIL-H-8501A (ref 14) as a guideline for evaluating and analyzing dynamic stability test results. The contractor was not obligated to comply with any portion of MIL-H-8501B.

AIRCRAFT CONTROL SYSTEM RIGGING

14. Prior to testing, the aircraft flight and engine controls were rigged on both test aircraft in compliance with the appropriate

Army publications (ref 16, app I). Subsequent aircraft flight and engine control rigging changes were coordinated with the contractor technical representatives.

CONTROL SYSTEMS

15. The control system breakout forces and force gradients were determined during ground test with the rotor in a static position. Hydraulic and electrical power were provided by external units. The longitudinal, lateral and directional control systems were evaluated with the cyclic friction at the preset value as stated in the organizational maintenance manual (ref 16, app I). Control forces were measured at the center of the cyclic control grip and at the top of the directional control pedals in the aft cockpit (pilot station). Breakout forces (including friction) were determined by recording the force required to obtain initial movement of the control. The force gradients were obtained by continuously recording the force and control position as each control was displaced from trim. Control forces as a function of control position are presented in figures 1 through 3, appendix VII. The cyclic pitch control pattern is presented in figure 4.

16. Control forces measured in flight agreed with the static ground data except where severe maneuvers exceeded the capability of the hydraulic boost system. Whenever this boost saturation occurred, increased cyclic and collective control forces were noted.

17. The results of the cyclic control evaluation are summarized in table 3. The cyclic force gradients were positive, and there were no discontinuities noted. The magnitudes of both the longitudinal (2.5 pounds per inch) and lateral (1.5 pounds per inch) cyclic force gradients were suitable for the armed helicopter mission even though the longitudinal force gradient exceeded the maximum value stated in para 3.2.4, MIL-H-8501A. The cyclic breakout forces (4.5 pounds longitudinally and 3.5 pounds laterally) exceeded the maximum-allowed values stated in paragraph 3.2.4 of MIL-H-8501A and the approved deviation (ref 13, app I). The high breakout forces made precise aircraft control difficult during hovering flight. This condition was objectionable for lateral control inputs. The high breakout forces were not objectionable during forward flight up to maximum airspeed in level flight (V_{H1}). However, at airspeeds in excess of V_{H1} (diving flight), the longitudinal cyclic force characteristics coupled with the neutral to slightly positive static longitudinal stability gradient, discussed in paragraph 28, made it difficult to maintain airspeed and pitch attitude precisely (HQRS 5). However, the ability to attain adequate mission performance (ie,

target tracking and ordnance delivery) will vary with the competence level of each pilot and the magnitude of turbulence in the atmosphere. These two unknown factors (pilot competence level and atmospheric turbulence) could cause the assigned HQRS to vary from 5 to 7. The magnitudes of cyclic breakout forces and force gradients were unaffected by cyclic trim position. The excessive cyclic control breakout forces are unacceptable for satisfactory operational use and reduction is mandatory for adequate accomplishment of the attack helicopter mission.

Table 3. Cyclic Control Breakout Forces and Force Gradients.

Rotor static Force trim ON			
Test / "	Maximum Allowed by MIL-H-8501A (1b)	Approved Contract Deviation (1b)	Test Results (1b)
Longitudinal breakout force (including friction)	1.5	2.0 (± 0.25)	4.5
Longitudinal force gradient	2.0 lb/in.	None	2.5 lb/in.
Longitudinal force at full throw. ¹	8.0	None	18.0
Lateral breakout force (including friction)	1.5	2.0 (± 0.25)	3.5
Lateral force gradient	2.0 lb/in.	None	1.5 lb/in.
Limit lateral force at full throw. ¹	7.0	None	18.0

¹Control displaced from a 50-percent control trim position in both directions.

18. There was no measurable change in the cyclic control force characteristics with the SCAS inoperative. With the force trim system OFF, the lateral and longitudinal force gradients were essentially zero; and breakout forces were only slightly less than those measured with the force trim ON. Turning off either hydraulic system had no effect on the cyclic breakout forces or force gradients.

19. The cyclic control position pattern, presented in figure A, shows that the available longitudinal control is a function of the lateral control position. Similarly, the lateral control is a function of the longitudinal control position. The position of the collective control has no effect on the cyclic control pattern.

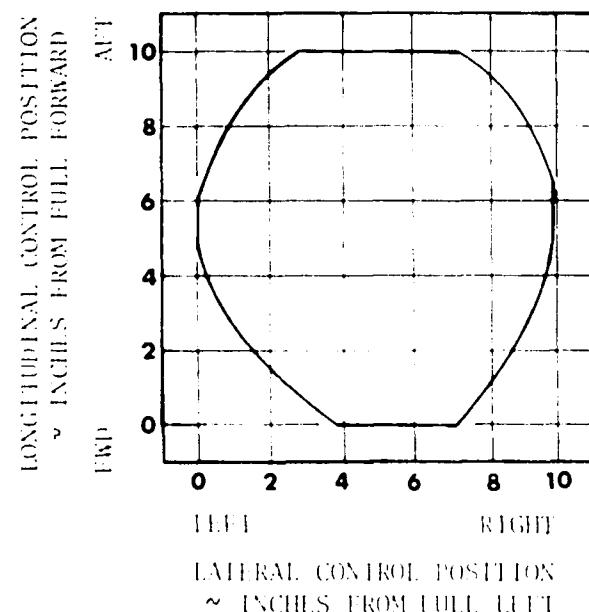


Figure A. Cyclic Pitch Control Pattern.

20. The directional control breakout forces with both boost systems operating and with the number ONE hydraulic boost system inoperative, complied with the requirements of MIL-H-8501A, paragraph 3.5.13, (table 4). The breakout force was 20 pounds with the number TWO hydraulic boost system inoperative. This value (20 pounds) complies with the system failure requirements of MIL-H-8501A, paragraph 3.5.8. At all conditions tested, there were discontinuities in the directional force gradient; thus, the requirement of MIL-H-8501A, paragraph 3.5.11, was not met. These directional force gradient discontinuities occurred at pedal positions not normally encountered in forward flight. The force gradient was zero with the force trim OFF. The directional control system breakout force and force gradient are satisfactory even with the minor discontinuities mentioned above.

Table 4. Directional Control Breakout Forces and Force Gradients.

Rotor static		Force trim ON	
Test	Maximum Allowed by MIL-H-8501A (1b)	Contractor Deviation	Test Results (1b)
Directional breakout force (including friction)	7.0	None	5.0
Directional force gradient	None	None	9.0 lb/in.
Directional force at full throw ¹	15.0	None	20.0 to 25.0

¹Control displaced from a 50-percent control trim position in both directions.

21. Collective control forces were not quantitatively evaluated during this test. However, qualitatively, the collective control forces were satisfactory for operational use.

STATIC TRIM STABILITY

22. Static trim stability characteristics about all three axes were evaluated in climbing, autorotational, diving and level flight. The tests were conducted at each of the configurations and flight conditions listed in appendix VII. The effect of removing the landing gear cross-tube fairings was evaluated in the clean configuration during level flight and dives. The static trim stability of the aircraft was determined by recording the control positions at various stabilized zero-sideslip flight conditions. The summary of the longitudinal trim curves are presented in figures 5 through 7, appendix VII. The static trim curves which present the various control positions as a function of airspeed are shown in figures 8 through 27.

23. At all conditions tested, the remaining longitudinal control displacement was never less than 1.5 inches (15 percent) from the forward control limit and 2.6 inches (26 percent) from the aft control limit (fig. B). A significant change in longitudinal control

position with cg variation was noted. The longitudinal trim curve characteristics were positive (increasing forward control with increasing speed) from approximately 40 to 170 KCAS and are satisfactory for all conditions tested. The longitudinal control gradient was evaluated qualitatively at airspeeds between hover and 40 KCAS in forward flight. This evaluation at low airspeeds revealed a slight discontinuity in the longitudinal control gradient. This discontinuity was not objectionable to the pilot and did not violate the requirements of paragraph 5.2.10 (MIL-H-8501A). The change in longitudinal control position with airspeed is neutral at airspeeds during high-speed dives at airspeeds in excess of 170 KCAS. At speeds above V_H , this is essentially static longitudinal collective-fixed stability, discussed in paragraph 28. This neutral or negative longitudinal trim stability contributed to the increased pilot workload while maintaining selected airspeed and pitch attitude during dives. There was no significant change in the longitudinal control gradient with gross weight and configuration (wing stores) changes.

LEGEND	CONFIG	GRWT (LB)	DEN ALT (FT)	ROTOR SPEED (RPM)	LONG CG (INCH)
— — —	CLEAN	8460	4540	324	201 (AFT)
— - -	CLEAN	7360	4460	324	190 (FWD)

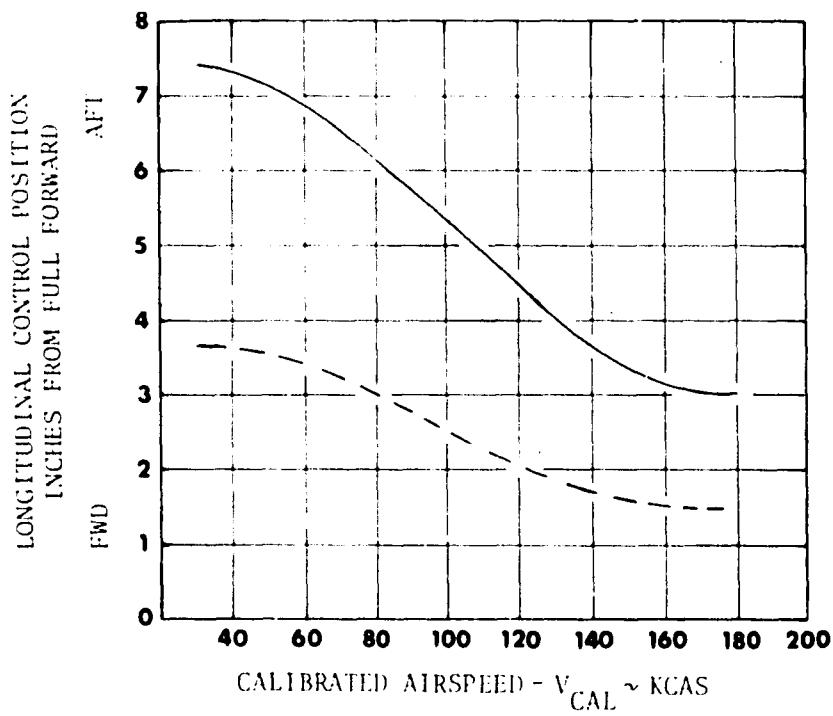


Figure B. Static Trim Stability.

24. There was a significant change in pitch attitude (as much as 10 degrees) between the forward and the aft cg loadings throughout the airspeed range in all flight conditions. This variation in pitch attitude with cg shift was readily apparent to the pilot but was not objectionable. There were slight variations in aircraft pitch attitude at a given airspeed with configuration and gross weight changes. These variations were small and not apparent to the pilot.

25. During zero sideslip stabilized flight at all conditions tested, the remaining lateral control displacement was never less than 4 inches (40.5 percent) from the left control limit and 2.9 inches (29.2 percent) from the right control limit. The lateral cyclic control migration was gradual and was not disconcerting to the pilot as the airspeed was varied between trim points. The lateral control position was farther right at a forward cg loading than at an aft cg loading. Gross weight, symmetrical configuration changes and altitude had no significant effect on lateral control requirements.

26. During stabilized forward flight at airspeeds in excess of 36 KCAS for all conditions tested, the remaining directional control displacement was never less than 1.75 inches (29.3 percent) from full right and 1.3 inches (21.8 percent) from full left. The maximum left directional control displacement occurred at low forward airspeeds (35 KCAS or less). The increasing right directional control was required as airspeed increased from 35 KCAS to the airspeed for minimum power required. Increasing left directional control was then required with increasing airspeed up to V_{H} . As airspeed increased from V_{H} to V_L , the migration of the directional control displacement was to the right. This increasing right directional control with airspeed contributed to the excessive pilot attention required to maintain zero sideslip during dives. Since the amount of sideslip present affects firing accuracy of the weapons, this characteristic is considered to be a shortcoming which detracts from mission effectiveness. For a given airspeed, an increase in left directional control was required for the following: changing longitudinal cg from forward to aft, increasing gross weight, increasing altitude and symmetrically increasing equivalent flat plate area by adding wing stores. Directional control trim position changes attributed to these variations were not noticeable to the pilot. Since an adequate margin was available in all forward flight conditions, this characteristic is acceptable. Qualitatively there was no significant change in the static directional trim stability with the landing gear cross-tube fairings removed.

STATIC LONGITUDINAL COLLECTIVE-FIXED STABILITY

27. The static longitudinal collective-fixed stability characteristics were examined at several different configurations, altitudes and cg loadings. Only the general characteristics noted and significant changes with variations in the above parameters are discussed in this section. These tests were conducted by first trimming the aircraft at the desired airspeed. The aircraft was then stabilized at several airspeeds greater and less than the trim airspeed while maintaining the trim collective control position. The force trim was also maintained at the trim setting. The tests were conducted at each of the configurations and trim conditions listed in appendix VIII. The summary of the longitudinal trim curves are presented in figures 28 through 31, appendix VII. Data were recorded at each stabilized airspeed and are presented in figures 32 through 65.

28. The longitudinal control position gradient was positive (forward cyclic required to maintain an airspeed greater than trim) for all conditions tested at airspeeds from 40 to 170 KCAS. However, the gradient became less positive at higher trim airspeeds and was essentially neutral at airspeeds in excess of 170 KCAS. The neutral static longitudinal collective-fixed stability at airspeeds in excess of 170 KCAS does not meet the requirements of MIL-H-8501A, paragraph 3.2.10. At airspeeds less than 40 KCAS, the static longitudinal collective-fixed stability was similar to the static trim stability discussed in paragraph 23. These data are presented graphically in figure C. The longitudinal control position gradient was more positive at a forward cg loading than at an aft cg loading for a given flight condition. Altitude, gross weight and configuration variations (wing stores) had no significant effect on the longitudinal control position gradient. The high longitudinal friction band masked the longitudinal force gradient, making the measured longitudinal force stability characteristic impractical to evaluate. As a result, the control force data in figures 32 through 65, appendix VII, have had the breakout forces analytically removed. The nearly neutral static longitudinal stability at airspeeds in excess of V_H contributed to the increased pilot effort required to stabilize the aircraft at a desired airspeed and detracted significantly from mission suitability (HQRS 4). This problem was further aggravated by the high longitudinal breakout forces and friction band. The longitudinal control position and force gradients at airspeeds in excess of V_H are minimally acceptable, and an increase of these gradients is desirable for improved service use.

CONFIG	GRWT (LB)	DEN ALT (FT)	ROTOR SPEED, (RPM)	LONG CG (INCH)
OUTB'D ALT	8190	4910	324	201(AFT)

NOTE: POSITIVE LONGITUDINAL STABILITY SIGNIFIES AN INCREASING FORWARD CYCLIC REQUIREMENT WITH INCREASING AIRSPEED

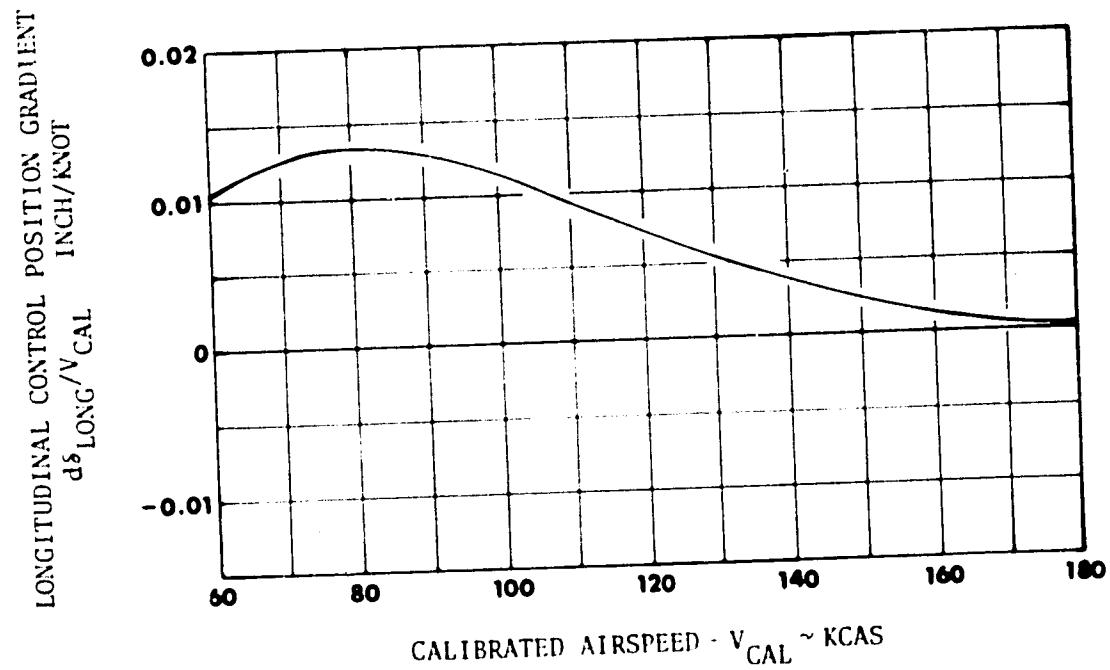


Figure C. Static Longitudinal Collective Fixed Stability.

29. The static longitudinal data presented in the report on the BHC Model 209 helicopter (ref 17, app 1) showed a neutral longitudinal control gradient in a dive. In Part 1 of the AH-1G Phase B report (ref 2), a strong recommendation was made for an increase in the longitudinal stability gradient at high speeds. It was also stated in reference 17, "nominal pilot attention was required to maintain a constant airspeed during high-speed dives."

30. The change in pitch attitude (nose-down attitude change with increased airspeed from trim is defined as positive) with respect to airspeed was neutral in low-speed level flight (60 KCAS trim speed) and became positive with increasing airspeed at a forward cg. These characteristics were similar to those observed during static trim stability testing. The pitch attitude gradient was more positive at an aft cg loading than at a forward cg loading at V_H and V_L . There was no significant change due to the variations in altitude, gross weight or configuration.

31. The changes in lateral cyclic control requirements during these tests were small, and excessive pilot attention was not required to maintain wings-level flight. At airspeeds greater than trim, more right directional control was required. At airspeeds less than trim, more left directional control was required. The directional control trim position changes with varying airspeed required some pilot compensation in order to maintain zero sideslip. This characteristic was most apparent during simulated weapons delivery maneuvers and target tracking tasks. During target tracking, moderate pilot compensation was required in order to achieve desired performance (HQRS 4). This shortcoming detracts from the armed helicopter mission suitability.

32. The longitudinal collective-fixed stability curves with landing gear cross-tube fairings removed are presented in figures 64 and 65 and the summary is presented in figure 31, appendix VII. The removal of these fairings did not significantly affect the longitudinal or lateral control migration characteristics. During flight in this configuration at trim airspeeds approaching V_L , the directional control gradient ($d\alpha_{DIR}/d/V_{CAL}$) did not vary with airspeed as with the fairings installed.

STATIC LATERAL-DIRECTIONAL STABILITY

33. Tests were conducted to determine the static directional stability and dihedral effect throughout the airspeed-sideslip envelope. The static directional stability and dihedral effect

were measured by recording data during stabilized flight at various sideslip angles while maintaining a constant heading at selected trim airspeeds and flight conditions. Tests were conducted at each of the configurations and trim conditions listed in appendix VIII. Summaries of the lateral-directional stability data are presented in figures 66 through 69, appendix VII. The test results are presented in figures 70 through 95, appendix VII.

34. Deviation number 1 (ref 13, app I), states that paragraph 3.3 of MIL-H-8501A shall not be applicable as a design guide for the stability and control characteristics. This deviation was interpreted by USAASTA to include virtually all lateral-directional handling qualities. The deviation should have provided specific guidelines to be used in determining acceptable lateral-directional handling qualities. Since inadequate guidance was provided, MIL-H-8501A was used as the criterion against which all lateral-directional stability characteristics were evaluated.

35. The static directional stability and dihedral effects were positive (increasing right directional control, left bank angle and left lateral control with increasing left sideslip) for all conditions tested except autorotation. The variation in directional and lateral control requirements was essentially linear as sideslip was varied about trim. In autorotation at an airspeed of 60 KCAS, the static directional stability was slightly positive while the dihedral effect was neutral. This characteristic does not comply with the requirements of para 3.3.9, MIL-H-8501A. This neutral dihedral effect in autorotation was apparent to the pilot, since directional control inputs did not establish roll rates (HQRS 3). This characteristic does not detract from mission suitability since acceptable performance could be achieved with minimal pilot compensation.

36. As engine power was increased the static lateral-directional stability gradients increased and were greatest during climbing flight at 60 KCAS. The static directional stability and effective dihedral increased as airspeed increased and reached maximum at V_L . The static directional stability gradient ($d\delta_{pedal}/d\delta$) became more positive as the cg location was changed from aft to forward. An increase in density altitude increased the static directional stability and effective dihedral slightly. There was no significant change in the static lateral-directional handling qualities when the aircraft configuration (wing stores) and gross weight were varied.

37. The static lateral-directional handling qualities are satisfactory for all conditions tested. One undesirable feature which was noted is the excessively high dihedral effect at V_L . The resultant roll rate is high for a small directional control input. This characteristic could cause the pilot to easily over control the aircraft when using directional control. In addition, this also contributes to the excessively high roll rates encountered during engine power loss at high airspeed (para 99).

38. The aerodynamic side-force characteristics as indicated by bank angle during steady sideslips were positive at all conditions tested and increased significantly with increasing airspeed. The side-force characteristics were essentially unchanged at all conditions tested except at high gross weight where a reduction in bank angle for a given amount of sideslip at the high airspeeds (140 to 170 knots) was noted.

39. The static lateral-directional stability characteristics for the landing gear cross-tube fairings removed configuration are presented in figures 94 and 95, appendix VII. A summary plot comparing data with the fairings on and off is presented in figure 69, appendix VII. The directional stability was more positive with the fairings removed. There was no significant difference in dihedral effect between the two configurations.

TRANSLATIONAL FLIGHT HANDLING QUALITIES EVALUATION

40. Translational flight is defined as flight in any direction with relative wind azimuths at any value from zero to 360 degrees (measured clockwise from nose of aircraft) at airspeeds between zero and 35 knots either in ground effect (IGE) or out of ground effect (OGE). The objectives of these tests were to evaluate the handling qualities and to determine control margins in translational flight. Deviation number 1 (app VI) is interpreted as exempting the AH-1G from complying with the lateral-directional handling qualities criteria as stated in MIL-H-8501A. Since no other guidance was provided, test results reported herein, where appropriate, are compared to the above specification to permit a basis for evaluation. A secondary purpose of this test was to determine the amount of tail rotor horsepower required to stabilize the aircraft at various combinations of wind azimuths and wind speeds. A calibrated ground pace vehicle was used as an airspeed reference during these tests. Conditions tested are listed in table 5. Results of the translational flight handling qualities are graphically presented in figures 96 and 125, appendix VII. The dashed portion of the faired curves on these plots indicates extrapolated data.

Table 5. Translational Flight Handling Qualities Evaluation.

Test Condition ¹	Gross Weight (lb)	Density Altitude (ft)	Longitudinal Center of Gravity (in.)	Rotor Speed (rpm)
1	8,240	-40	199.6	324
2	8,060	140	200.4	312
3	8,050	5,270	200.7	324
4	7,210	11,120	195.4	324

¹All tests conducted in the heavy scout configuration with rocket pod fairings removed.

41. Control of skid height, roll attitude and pitch attitude during translational flight was good (HQRS 2) with one exception. This was the abrupt longitudinal trim change for rearward flight in the 10- to 15-knot range for small speed changes. The longitudinal control changes were approximately 1 inch in this speed range (HQRS 5).

42. The directional control capability was significantly less than that required to meet paragraphs 3.3.5 and 3.3.6, MIL-H-8501A. To meet these requirements significantly more tail rotor thrust (directional control), than is presently available, would be required. A directional control margin of 10 percent (0.71 inches for the test aircraft) enabled the pilot to control and maneuver the aircraft in translational flight (HQRS 5). Directional control margins less than 10 percent were inadequate for maneuvering due to the magnitude of average pedal inputs and the control travel limitation problem discussed in paragraph 47 with the yaw SCAS operating.

43. The critical area of insufficient directional control for test condition number 1, table 5, was with wind from 45 to 70 degrees at a velocity of 17 knots. The area (bounded by wind azimuth and velocity) of inadequate directional control increased with combinations of increasing altitude, increasing gross weight and/or decreasing rotor speed. At the most critical condition, number 4 of table 5, the directional control margin was less than 10 percent at all wind azimuths and at velocities from zero to 3 knots. At velocities greater than 3 knots, the area of inadequate directional control was between 30 and 300 degrees. Flight operations

at this gross weight/density altitude condition can not be conducted safely because of inadequate directional control.

44. Directional control of the test aircraft was lost (uncontrolled right yaw) several times during the test at condition number 4, table 5. Recovery of the aircraft was accomplished by reducing power and allowing the skid tubes to lightly contact the ground. The friction between the ground and the skid tubes gradually checked the turning rate of the helicopter. After stopping the turning rate, the collective was lowered and the aircraft landed. The full left directional control pedal was maintained until the yaw rate was arrested.

45. The effect of this major deficiency is well illustrated in the weekly summaries published by the US Army Board for Aviation Accident Research (USABAAR). Between 27 January and 13 July 1969, these summaries noted nine accidents due to loss of left directional control causing major damage (including one accident where flying debris caused major damage to a second aircraft), one accident causing minor damage, one accident in which the damage was not reported and eight incidents.

46. Figure D shows the recommended IGE translational flight envelope. The envelope is based on a directional control margin of 10 percent for any combination of wind velocity and wind azimuth. It is mandatory that the directional control system for the AH-1G be improved to provide better control characteristics.

NOTES: 1. ROTOR SPEED 324 RPM
2. ENVELOPE BASED ON A 10 PERCENT DIRECTIONAL
CONTROL MARGIN AT ALL WIND AZIMUTHS

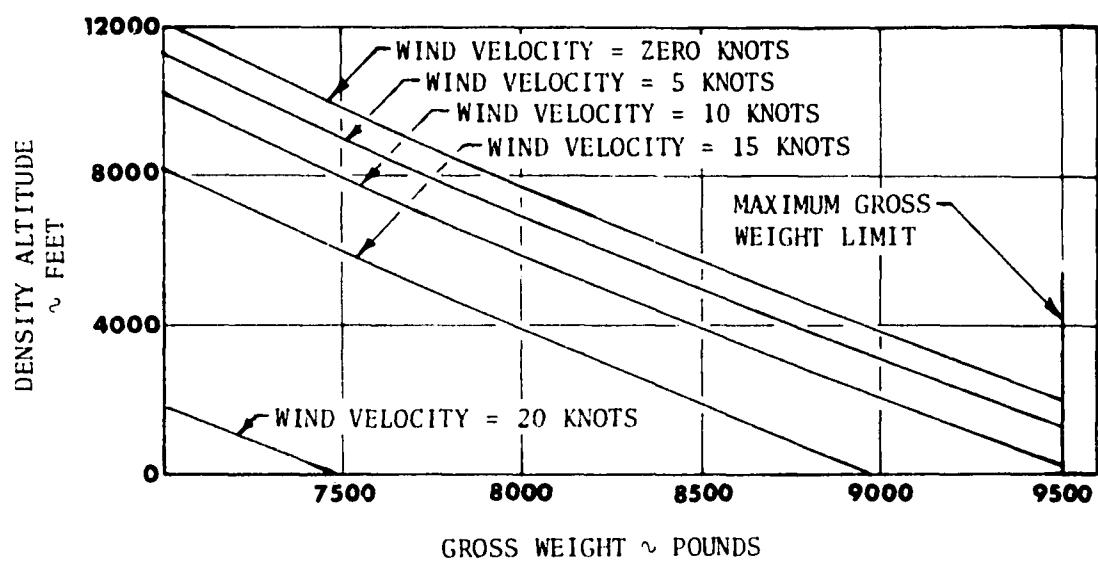


Figure D. Recommended In-Ground-Effect Translational Flight Envelope.

47. The 10-percent directional control position margin is equivalent to a tail rotor blade angle change of 3.0 degrees. Standard rigging of the tail rotor is 19.0 degrees for full left control and -11.0 degrees for full right control with the yaw SCAS actuator centered. Due to a travel limitation in the control linkage between the pedals and the SCAS actuator, the amount of tail rotor blade angle available with full left pedal applied can vary from 19.0 to 16.0 degrees depending on the position of the yaw SCAS actuator. With the yaw SCAS ON, the left pedal margin can be reduced to zero (a tail rotor blade angle of 16.0 degrees) with the yaw SCAS actuator in the most adverse position. This condition is further complicated by the fact that the pilot has no way of knowing how much directional control is available with the yaw SCAS operating. Since the IGE performance is limited by the directional control available, it is mandatory that the directional control be modified so that the maximum tail rotor blade angle of 19 degrees can be achieved regardless of the position of the SCAS actuator.

48. The AH-1G was directionally unstable in wind velocities between 10 and 18 knots at relative wind azimuths between 210 and 330 degrees (clockwise from nose of aircraft) for test conditions 1, 2 and 3, table 5. Rapid and sometimes large directional control excursions were necessary to maintain a heading at these unstable flight conditions (HQRS 6). Also, large changes in longitudinal control were required as the relative wind velocity varied in this area. Pilot recognition and reaction times following small excursions in yaw determined the frequency and magnitude of the directional control inputs. These tests were conducted with the yaw SCAS OFF to provide the pilot with accurate control available information and to insure that a full 19 degrees of tail rotor blade angle was available. Tests were also conducted with the yaw SCAS channel ON to qualitatively evaluate the damping effect. The directional stability was only slightly improved with the directional SCAS operating. This directional instability in translational flight is a shortcoming and detracts from the mission suitability of the aircraft. This instability was encountered under similar conditions and reported in references 3 and 8. Figure E illustrates the area of this instability.

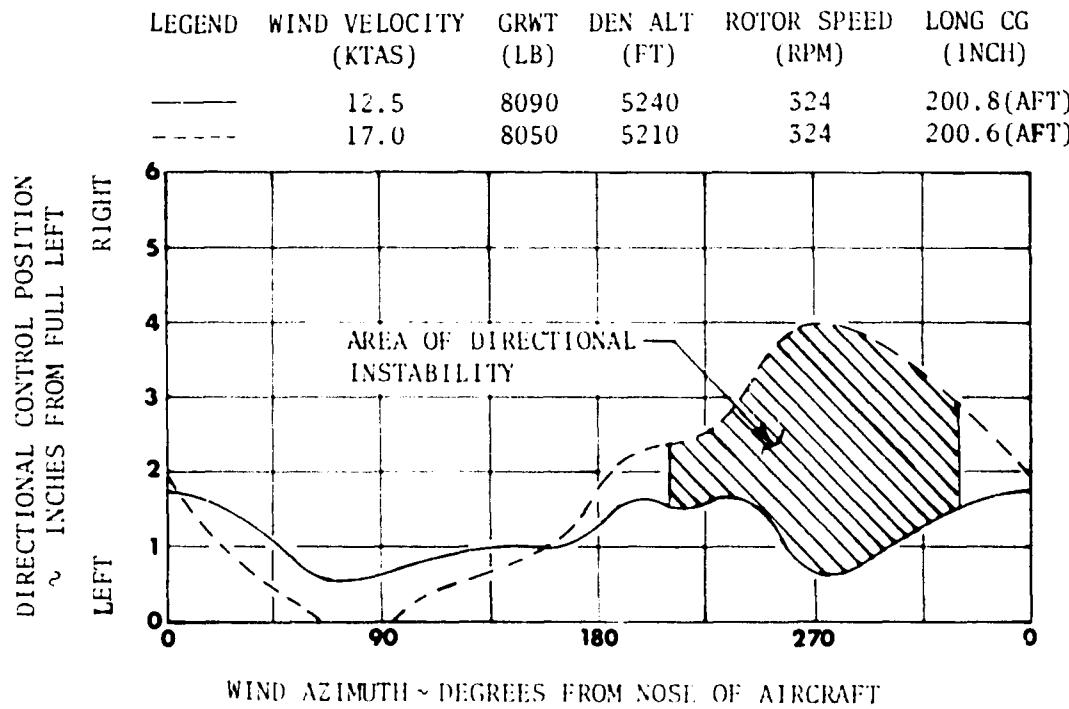


Figure E. Directional Control Position
In-Ground-Effect at Various Wind Azimuths.

49. The AH-1G is further limited by the maximum power transfer capability of the tail rotor drive system. Test results indicate that the tail rotor horsepower required to stabilize the aircraft increased nonlinearly as the directional control approached the left limit. Although a tail rotor drive system torque limit could not be determined, the structural design criteria report (ref 18, app I) for the AH-1G stated that the antitorque drive system design limit was 386 foot-pounds of torque (122 shp at 1654 rpm). Peak tail rotor horsepower encountered during translational flight was 190 horsepower at SL. For a given tail rotor blade pitch angle,

the peak tail rotor horsepower generally decreased as altitude increased. The rapid and sometimes large directional control excursions discussed in paragraph 48 caused large tail rotor torque oscillations. The magnitude of these oscillations were 20 to 160 horsepower for some test conditions. The magnitude of tail rotor horsepower during stabilized hover is presented in reference 19, appendix I. During this test program, *eight* 42-degree gear boxes and *four* 90-degree gear boxes were replaced. Replacement of the 42-degree gear box was required when tail rotor horsepower in excess of 180 horsepower was encountered because of the unacceptable gear wear patterns. The 90-degree gear box required replacement when operated above 180 horsepower for limited periods. The excessive tail rotor horsepower required and resultant antitorque drive system damage are deficiencies and correction is mandatory.

50. Sideward and rearward flights were also conducted with landing gear cross-tube fairings removed. The fairings-off data are presented in figure 125, appendix VII. There was no significant difference in the handling qualities during translational flight as a result of removing the landing gear cross-tube fairings.

DYNAMIC STABILITY

51. The objective of the dynamic stability tests was to evaluate the aircraft short period response characteristics following a gust disturbance. Gust disturbances were simulated by making pulse-type control inputs of 1 inch for 0.5 to 1 second. Following the inputs, the control was returned to trim, and all controls were held fixed until either the aircraft motions damped or recovery action was required. Dynamic stability was evaluated following inputs in both directions for longitudinal, lateral and directional controls. Tests were conducted both with the SCAS ON and OFF. The tests were conducted at each configuration and trim condition listed in appendix VIII.

Longitudinal Dynamic Stability

52. The longitudinal dynamic stability characteristics are summarized in figure 126, appendix VII. The aircraft motions following longitudinal control inputs were analyzed by determining the damping ratios and undamped natural frequencies. Representative time histories are presented for selected trim airspeeds, SCAS ON and for the most critical conditions SCAS OFF in figures 127 through 133.

53. The AH-1G demonstrated strong positive damping of the longitudinal short-period mode with SCAS ON. After the initial response to control input, the pitch attitude, angle of attack and load factor all returned to trim with no overshoot. Correspondingly, pitch rate made one excursion in each direction and then returned to zero. No significant coupling was present in the yaw or the roll axis during or following a longitudinal pulse input. Damping characteristics were similar for both forward and aft pulses. The longitudinal dynamic stability characteristics of the AH-1G with the SCAS ON complied with paragraph 3.2.11 of MIL-H-8501A. These characteristics are highly desirable and enable target-tracking maneuvers for weapon firing to be accomplished with little pilot effort or compensation. The longitudinal stability characteristics SCAS ON significantly enhance the mission suitability (HQRS 1).

54. Longitudinal pulses with SCAS OFF resulted in rapid divergence of pitch rate and pitch attitude for most conditions tested. Recovery action was required in most cases before one complete oscillation. The time history of a longitudinal pulse and resulting oscillating aircraft motions with SCAS OFF are presented in figure 133, appendix VII. In the heavy hog configuration at a gross weight of 7740 pounds and at an aft cg condition, the pitch attitude achieved the double amplitude in less than 10 seconds. There was significant lateral coupling following longitudinal inputs with SCAS OFF. The aircraft rolled to the right during forward inputs and to the left with aft inputs. The lack of positive longitudinal damping and the lateral coupling increased the pilot work load for all forward flight tasks. The aircraft can be safely flown in this condition; and routine maneuvers, such as cruise, approach and landing, can still be preformed with adequate precision (HQRS 4). The suitability for use as a weapons platform and for flight under restricted visibility conditions is significantly reduced (HQRS 6).

Dynamic Lateral-Directional Stability

55. The lateral and directional dynamic stability data are summarized in figures 134 and 142, appendix VII. The aircraft motions following roll and/or yaw inputs were analyzed for damping ratios and undamped natural frequency. Figures 151 and 152 show the lateral-directional damping ratio as a function of both damped natural frequency and calibrated airspeed. Figures 135 through 141 and 143 through 149 show representative time histories of lateral-directional dynamic response characteristics.

56. Damping of the lateral-directional oscillations, commonly referred to as Dutch roll, with SCAS ON was strongly positive. In most cases, the roll and attitude responded to the input and then returned to trim with no overshoot. The heavy hog and clean configurations with SCAS ON demonstrated similar characteristics except during climb where the clean configuration was less damped than the heavy hog configuration. Altitude had no significant effect on damping of the lateral-directional oscillations nor did gross weight or mass distribution, such as the addition of rockets. A summary of the lateral-directional dynamic stability characteristics with SCAS ON is presented in figure F. With SCAS ON, the dynamic lateral-directional stability characteristics comply with the applicable requirements of MIL-H-8501A and are suitable for the intended mission. While the damping was strongly positive it did not limit or degrade the maneuvering capability.

- NOTES:
1. SCAS ON
 2. ALL CONDITIONS ON AIRCRAFT S/N 6715695 FALL WITHIN SOLID LINE
 3. \square DENOTES CONDITIONS TESTED ON AIRCRAFT S/N 6615247 WITH LANDING GEAR CROSS TUBE FAIRINGS REMOVED

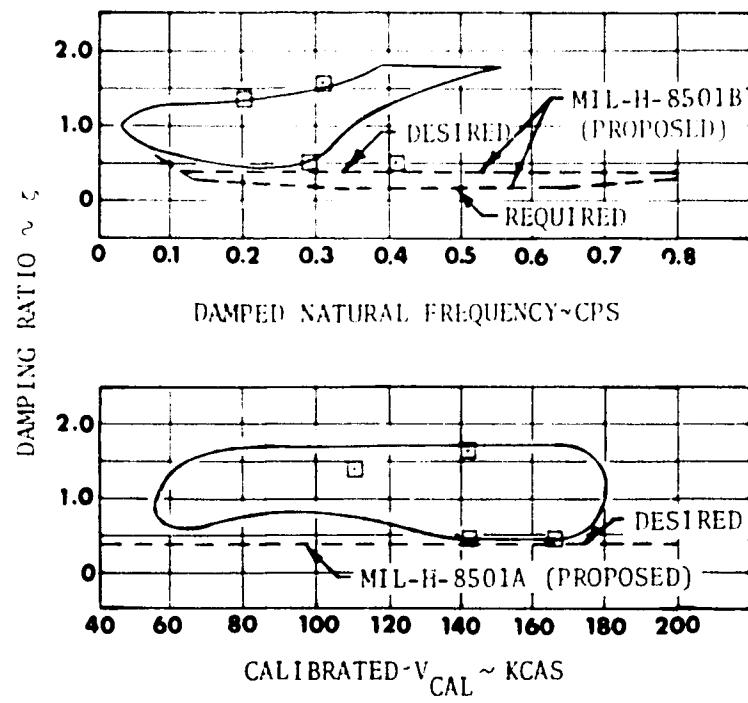


Figure F. Summary of Lateral-Directional Dynamic Stability.

57. In most conditions tested, the lateral-directional dynamic stability with the SCAS OFF was well below that value contained in the proposed specification, MIL-H-8501B (ref 13, app I), for an armed tactical helicopter. The yaw/roll oscillations or dutch roll had a period of approximately 4 seconds. The worst condition was the climb, clean configuration, at a 7210-pound grwt and an aft cg loading. A time history of this condition is presented in figure 141, appendix VII. The aircraft oscillations were divergent in roll and yaw for this test condition. At most conditions tested, damping ratios were less than 0.2. A summary of lateral-directional dynamic stability with SCAS OFF is presented in figure G. This low damping of the lateral-directional motions with SCAS OFF resulted in objectionable, uncomfortable aircraft motions, particularly at higher airspeeds. In addition, this characteristic, aggravated by the excessively high lateral breakout forces discussed in paragraph 17, resulted in a pilot induced oscillation in the roll axis at high speeds. This characteristic seriously detracts from mission suitability and makes satisfactory, effective completion of most missions questionable during SCAS OFF operations. The aircraft can be safely returned to base and landed. However, precise flight tasks are very difficult to perform (HQRS 6).

- NOTES:
1. SCAS OFF
 2. ALL CONDITIONS TESTED ON AIRCRAFT S/N 6715695
FALL WITHIN SOLID LINE
 3. DENOTES CONDITIONS TESTED ON AIRCRAFT S/N
6615247 WITH LANDING GEAR CROSS TUBE FAIRINGS
REMOVED

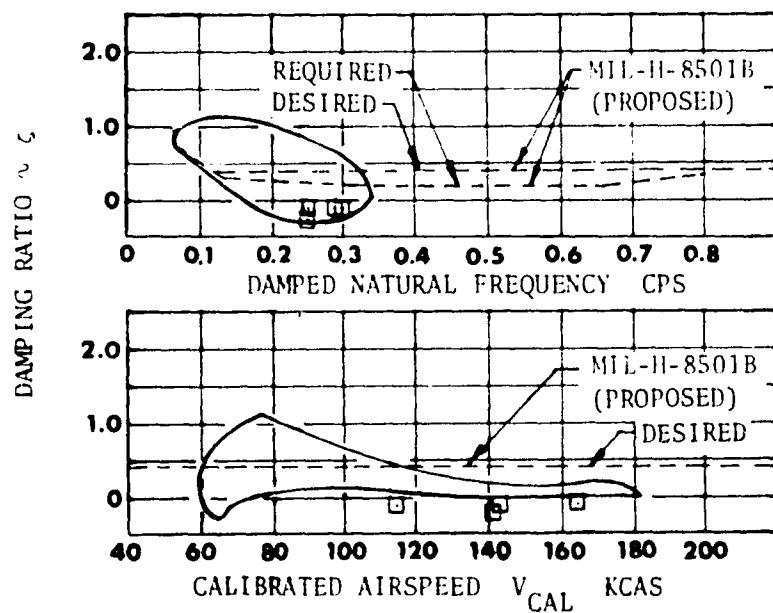


Figure G. Summary of Lateral-Directional Dynamic Stability.

58. The results of these tests agree closely with those described in reference 17, appendix I, with SCAS ON. However, with SCAS OFF, test results indicated a degradation in lateral-directional dynamic stability characteristics from the reference.

59. Lateral-directional dynamic stability characteristics were also evaluated for the clean configuration with the landing gear cross-tube fairings removed, with SCAS ON and OFF. A comparison of the clean configuration with fairings on and off is presented in figure 150, appendix VII. Time histories of lateral and directional pulses SCAS OFF are presented in figures 151 and 152.

60. With SCAS ON, the removal of the fairings had no significant effect on lateral-directional damping at airspeeds less than 160 KCAS (HQRS 2). At airspeeds in excess of 160 KCAS, the lateral-directional coupling increased and damping decreased (para 83). The increased lateral-directional coupling and decreased damping caused the pilot workload to increase beyond a tolerable limit when performing target tracking maneuvers (HQRS 7). An airspeed limit of 160 KCAS is recommended in order to maintain an effective target tracking capability when the landing gear cross-tube fairings are not installed.

61. With SCAS OFF, the removal of the landing gear cross-tube fairings significantly degraded the dynamic lateral-directional characteristics. Dutch roll oscillations were induced by either lateral or directional control inputs. The oscillations for most conditions were divergent and had a period of about 4 seconds and a negative damping ratio of 0.2. The rates in both axes increased rapidly to unacceptable levels (50 deg/sec in roll and 25 deg/sec in yaw). A limit of 115 KCAS is recommended when landing gear cross-tube fairings are not installed, and the SCAS is inoperative. Flight during periods of restricted visibility, such as at night or during instrument conditions with the fairings removed and with SCAS OFF, is not recommended (HQRS 8).

CONTROLLABILITY IN FORWARD FLIGHT

62. Controllability was evaluated in level flight, dive, auto-rotation, climb and hover throughout the flight envelope. The hover tests were performed at several different gross weights, rotor speeds and density altitudes. Controllability tests were also conducted in forward flight with the landing gear cross-tube fairings removed.

63. The objective of these tests was to evaluate the ability to control the aircraft by quantitatively evaluating the aircraft

reaction to a given control input. This was accomplished by measuring the aircraft attitude displacements, rates and angular accelerations that resulted per inch of control input. Step-type control inputs were utilized which consisted of rapidly displacing the control to the desired position (maximum input time of 0.2 seconds) and then holding this position until the maximum rate was reached or recovery action was necessary. The magnitude of the step inputs was varied (usually a minimum of three inputs in each direction). An adjustable, rigid control fixture was used to assist in achieving the desired inputs. The forward flight controllability test data are presented in figures 169 through 243, appendix VII. The forward flight controllability test results are summarized by presenting data for a 1-inch control input at the various flight conditions and airspeeds tested. These summaries are presented in figures 156 through 168. The dashed portion of the faired curves on these plots (figs. 156 through 168) indicates extrapolated data. Typical time histories of step inputs are presented in figures 280 through 286.

64. Controllability characteristics are discussed in terms of control sensitivity, control response and attitude displacement. Control sensitivity is defined as the maximum angular acceleration which results from a 1-inch control step input. Control response is defined as the angular rate which results from a 1-inch control step input. Attitude displacement is discussed in terms of aircraft displacement at 1 second after a control input.

Longitudinal

65. The longitudinal controllability test conditions are presented in table VII, appendix VIII. A portion of these tests were conducted with the SCAS OFF.

66. In the heavy hog configuration the longitudinal sensitivity was essentially constant at $10 \text{ deg/sec}^2/\text{inch}$ at all forward flight speeds up to V_L . In the clean configuration, however, longitudinal sensitivity was a constant $10 \text{ deg/sec}^2/\text{in.}$ at airspeeds up to $0.8 V_H$ and then increased with increasing airspeed to a value of $17 \text{ deg/sec}^2/\text{in.}$ at V_L . The time required to achieve the peak angular acceleration following a 1-inch step input did not exceed 0.5 second. In general, the forward step inputs resulted in slightly greater angular accelerations than did aft step inputs. Longitudinal control sensitivity with SCAS OFF was the same as with SCAS ON and was not a function of altitude. Only minor variations in longitudinal control sensitivity with changes in gross weight and cg were noted. The average value of sensitivity during climb and autorotation was approximately $9 \text{ deg/sec}^2/\text{inch}$. Figure H summarizes longitudinal control sensitivity for all conditions tested.

NOTES: 1. SCAS ON
 2. SHADED ENVELOPE CONTAINS ALL SCAS ON
 FLIGHT TEST DATA

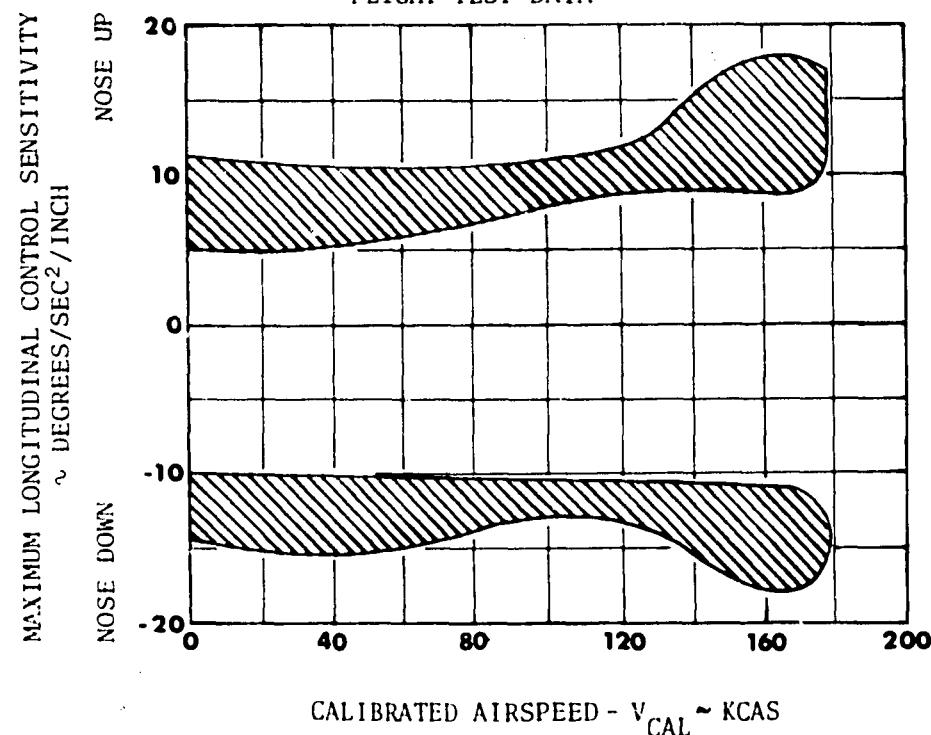


Figure H. Longitudinal Control Sensitivity.

67. The longitudinal controllability characteristics were also evaluated in terms of maximum response as defined in paragraph 64. The longitudinal response of the aircraft was slightly greater for a forward input than for an aft input. With SCAS ON, the longitudinal response averaged 7 deg/sec/in. and was not a function of configuration, gross weight, airspeed or altitude. The time required to achieve maximum rate (SCAS ON) was 1 second or less for all conditions tested. Maximum response was slightly higher at an aft cg than at a forward cg at airspeeds approaching V_L . In figure J, the maximum pitch rate data for all conditions tested are summarized.

NOTES: 1. SCAS ON
 2. SHADED ENVELOPE CONTAINS ALL SCAS ON
 FLIGHT TEST DATA

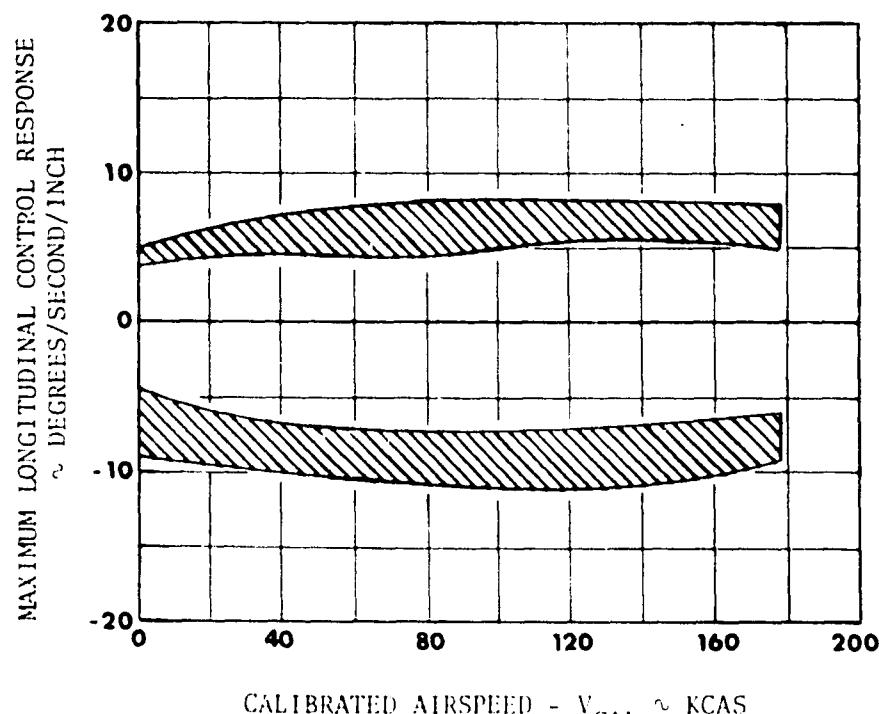


Figure J. Longitudinal Control Response.

68. Pitch rate at 1 second following a 1-inch longitudinal step input is presented for comparison of SCAS ON and SCAS OFF tests. This presentation is necessary because with SCAS OFF the maximum response was not achieved before recovery was necessary. The longitudinal response characteristics with SCAS OFF were similar to those for the SCAS ON condition except for the following differences:

- a. At airspeeds greater than 80 KCAS, the pitch rate at 1 second after the control input was greater with SCAS OFF. (A constant 6 deg/sec/in. with SCAS ON as compared to a maximum of 13 deg/sec/in. at V_L with SCAS OFF).
- b. At V_L and at an aft cg loading, the response was significantly greater with SCAS OFF.
- c. In all cases tested with SCAS OFF, a maximum response was not achieved since rate continued to increase until recovery was necessary.

69. The response resulting from an aft step input is in compliance with paragraph 3.2.11.1, MIL-H-8501A, as shown in figure 155, appendix VII, both the cg normal acceleration and the angular pitch velocity became concave downward in less than 2 seconds. The cg normal acceleration became concave downward at an average time of 1.56 seconds and the pitch rate at an average time of 0.3 second.

70. Pitch attitude displacement characteristics were determined by measuring pitch attitude change from trim at 1 second following a 1-inch step input. This was done both with SCAS ON and OFF. Figure K presents the summary of the SCAS ON data. Generally with SCAS ON, the displacement was a constant 5 degrees/inch and increased slightly between V_H and V_L . There was no change in displacement at 1 second with variations of configuration, gross weight and altitude. With SCAS OFF, the displacement increased with increasing airspeed. The only difference noted with a change in configuration with SCAS OFF was a slightly greater displacement in the clean configuration than in the heavy hog configuration.

NOTES: 1. SCAS ON
2. SHADeD ENVELOPE CONTAINS ALL SCAS ON FLIGHT TEST DATA

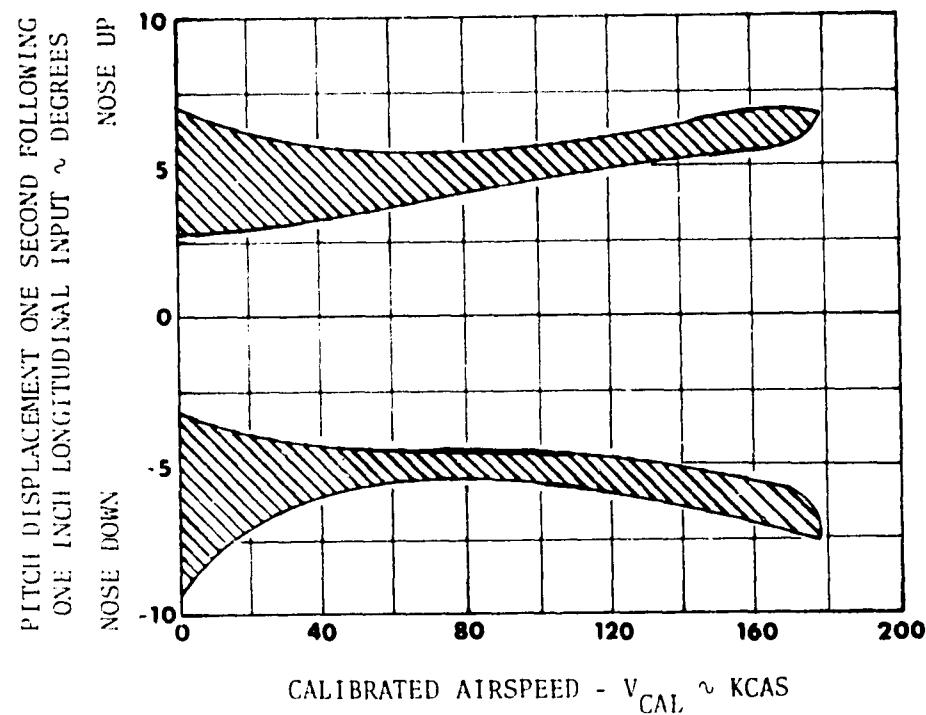


Figure K. Pitch Attitude Displacement.

71. Longitudinal controllability characteristics are considered to be satisfactory. Qualitatively, no objectionable characteristics were observed, and the aircraft reactions to longitudinal control inputs were highly satisfactory. During simulated target tracking maneuvers with SCAS ON, it was determined that a desired pitch attitude could be precisely maintained, and attitude changes could be easily and accurately accomplished (HQRS 2). The high level of pilot effort required to maintain an airspeed during dives was caused by the control force characteristics and the shallow static longitudinal stability gradients. The insensitivity of the longitudinal controllability characteristics to variations in weight, cg, configuration and altitude is highly desirable, and contributes significantly to mission suitability. The characteristics with the longitudinal SCAS OFF are good with little increase in pilot effort required for satisfactory mission accomplishment. A mildly annoying characteristic with SCAS OFF was a slight amount of control cross-coupling. A forward control input resulted in a right roll, and an aft control input resulted in a left roll.

Lateral

72. The lateral controllability characteristics were determined to be satisfactory. The lateral controllability test conditions are presented in table VIII, appendix VIII. A portion of these tests were conducted with the SCAS OFF. In all cases tested, the aircraft reacted in the proper direction with a lateral control step input, and no apparent hesitation nor discontinuities in resultant rates were noted. The sensitivity and response was greater with a left lateral control input than with a right control input. The deviation to MIL-H-8501A discussed in paragraph 34 also applies to this section.

73. The lateral control sensitivity at airspeeds less than 100 KCAS was approximately 16 deg/sec²/in. and was independent of altitude, gross weight or configuration. The time required to reach maximum angular acceleration was in all cases less than 0.5 second. At a given flight condition, the lateral sensitivity in climb was greater than that in level flight, and in autorotation it was less than in level flight. The maximum values of roll acceleration were achieved during climbs and in dives at V_L and were on the order of 25 to 30 deg/sec²/inch. Lateral control sensitivity characteristics with SCAS OFF were similar to those obtained with SCAS ON. Lateral control sensitivity data with SCAS ON are shown in figure I.

NOTES: 1. SCAS ON
 2. SHADED ENVELOPE CONTAINS ALL SCAS ON
 FLIGHT TEST DATA

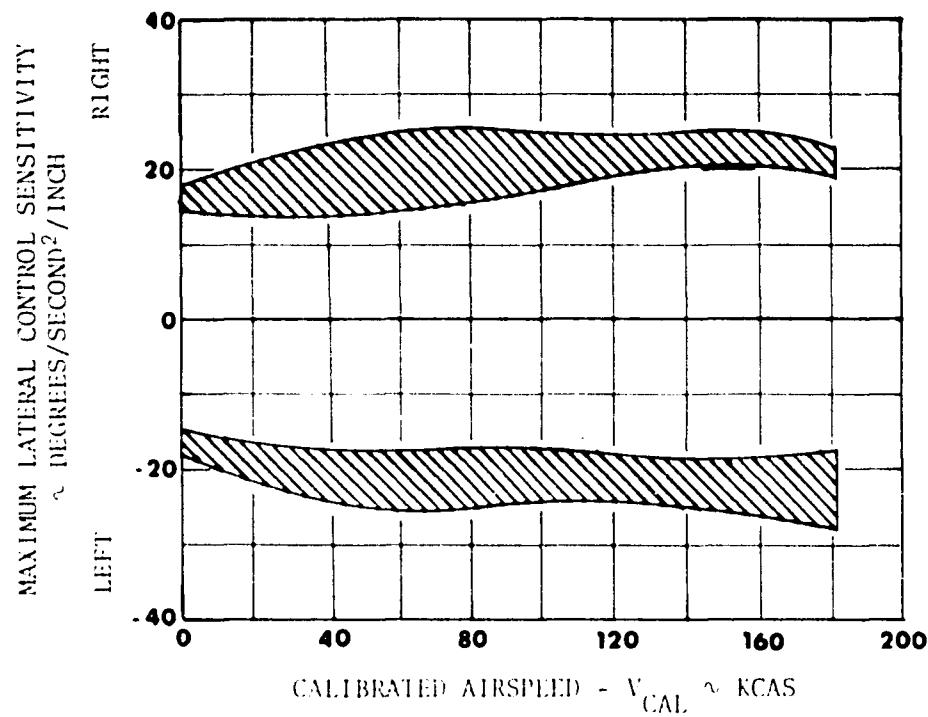


Figure 1. Lateral Control Sensitivity.

74. The maximum lateral control response with SCAS ON varied 10 deg/sec/in. at mid airspeeds (70 to 120 KCAS) to 20 deg/sec/in. at V_L in the clean configuration. Lateral control response was not a function of altitude or gross weight, but in the heavy hog configuration, higher maximum roll rates occurred than in the clean configuration (fig. 157, app VII). The time required to achieve maximum roll rate was approximately 1 second at all conditions tested with SCAS ON.

75. Lateral control response characteristics with SCAS OFF were similar to those observed with SCAS ON, except, as in the case of pitch response, a peak rate could not be achieved prior to initiating recovery due to the high rates and large roll displacements which occurred. Therefore, the SCAS OFF data are presented in terms of rate at 1 second after control input. The lateral control response characteristics are summarized in figure M. With SCAS ON, the AH-1G meets the requirements of paragraph 3.3.15 of MIL-H-8501A except for those areas, as indicated in figure M, where maximum roll rates exceeded 20 deg/sec/inch.

NOTES: 1. SCAS ON
 2. SHADED ENVELOPE CONTAINS ALL SCAS ON
 FLIGHT TEST DATA

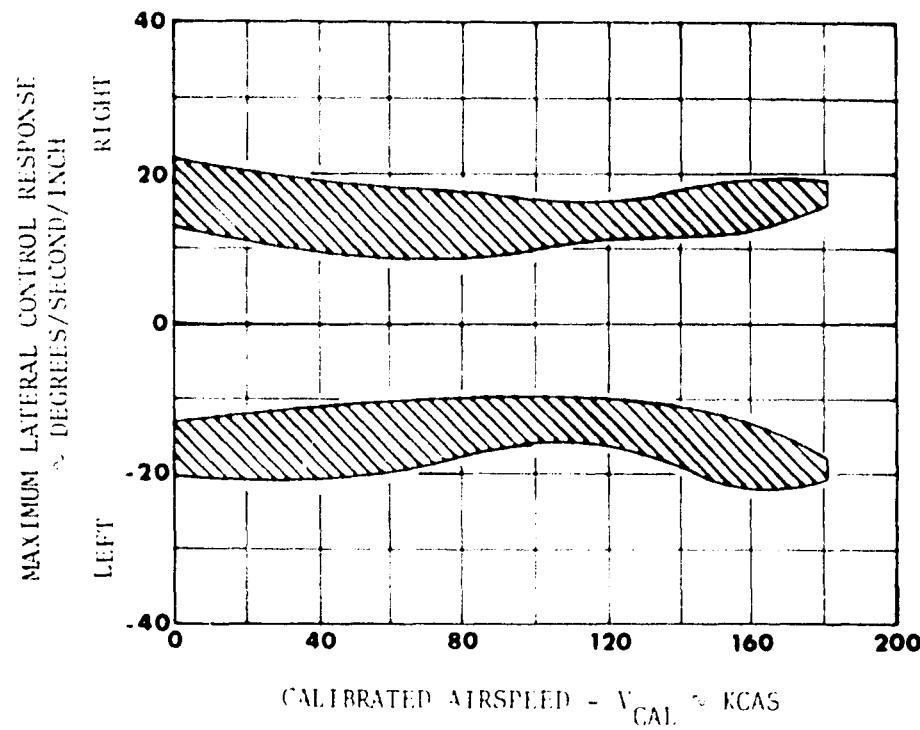


Figure M. Lateral Control Response.

76. The roll attitude displacement at 1 second following a 1-inch control input varied from 7 to 15 deg/inch. In general, the only parameters affecting the displacement were increased gross weight and loaded rocket pods, both of which decreased displacement. Roll attitude displacement characteristics were essentially the same for SCAS ON and SCAS OFF. Data with SCAS ON are summarized in figure N.

NOTES: 1. SCAS ON
2. SHADED ENVELOPE CONTAINS ALL SCAS ON
FLIGHT TEST DATA

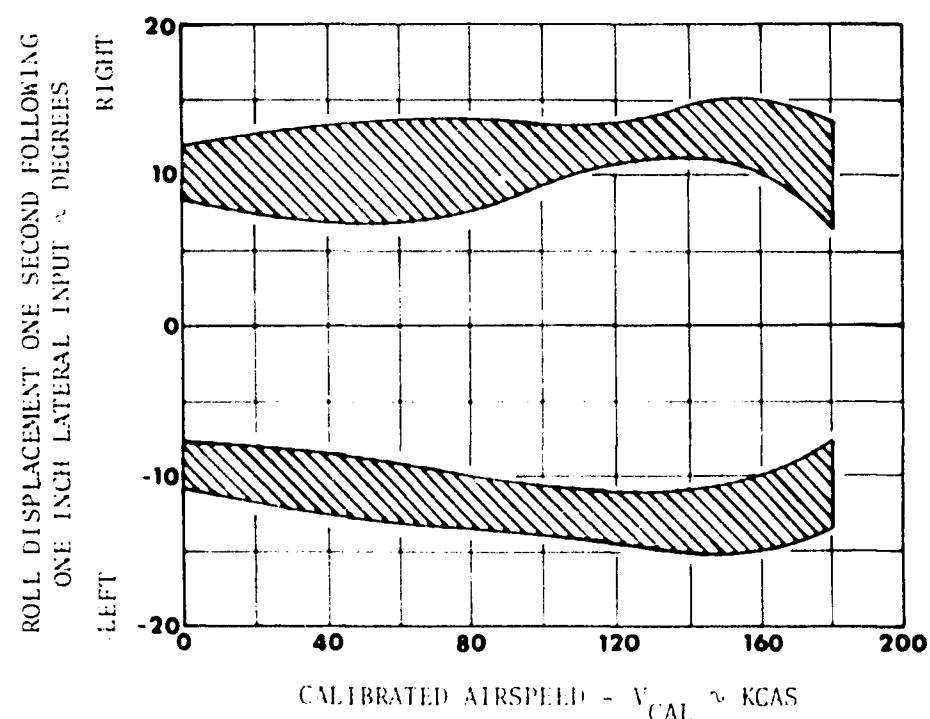


Figure N. Roll Attitude Displacement.

77. Qualitatively, the lateral controllability characteristics of the AH-1G in forward flight are satisfactory with SCAS ON. No objectionable characteristics were noted, and the aircraft reacts rapidly to a control input. The relatively high roll rates and roll accelerations observed, while in some cases exceed the

maximum values stated in MIL-H-8501A, are satisfactory for an attack helicopter. These characteristics contribute to the ability to make rapid turns and minimize time in return-to-target maneuvers (HQRS 2). However, these rates (22deg/sec/in.) are approaching the maximum allowable from a qualitative standpoint. A phenomenon was noted where an increase in engine torque resulted from a left control input, and a decrease in engine torque resulted from a right control input. This is discussed in detail in the Performance portion of the AH-1G Phase B report (ref 19, app 1). No significant control coupling was encountered during the lateral controllability tests.

Directional

78. Directional controllability characteristics were investigated at the same conditions as longitudinal and lateral controllability and were generally satisfactory. The directional controllability test conditions are presented in table IX, appendix VIII. A portion of these tests were conducted with the SCAS OFF. In all cases, the directional inputs resulted in an initial yawing of the aircraft in the proper direction.

79. The directional control sensitivity decreased with increasing airspeed and was minimum at V_L . Sensitivity was greater in the clean configuration than in the heavy hog configuration at all airspeeds. Increasing gross weight and increasing altitude, in a given configuration, resulted in a significant decrease in control sensitivity, particularly at high airspeeds. In all cases tested, the maximum yaw acceleration occurred at 0.5 second or less after the control input. SCAS OFF characteristics were generally the same as SCAS ON. Data are summarized for all conditions tested (SCAS ON) in figure 0.

NOTES: 1. SCAS ON
 2. SHADED ENVELOPE CONTAINS ALL SCAS ON
 FLIGHT TEST DATA

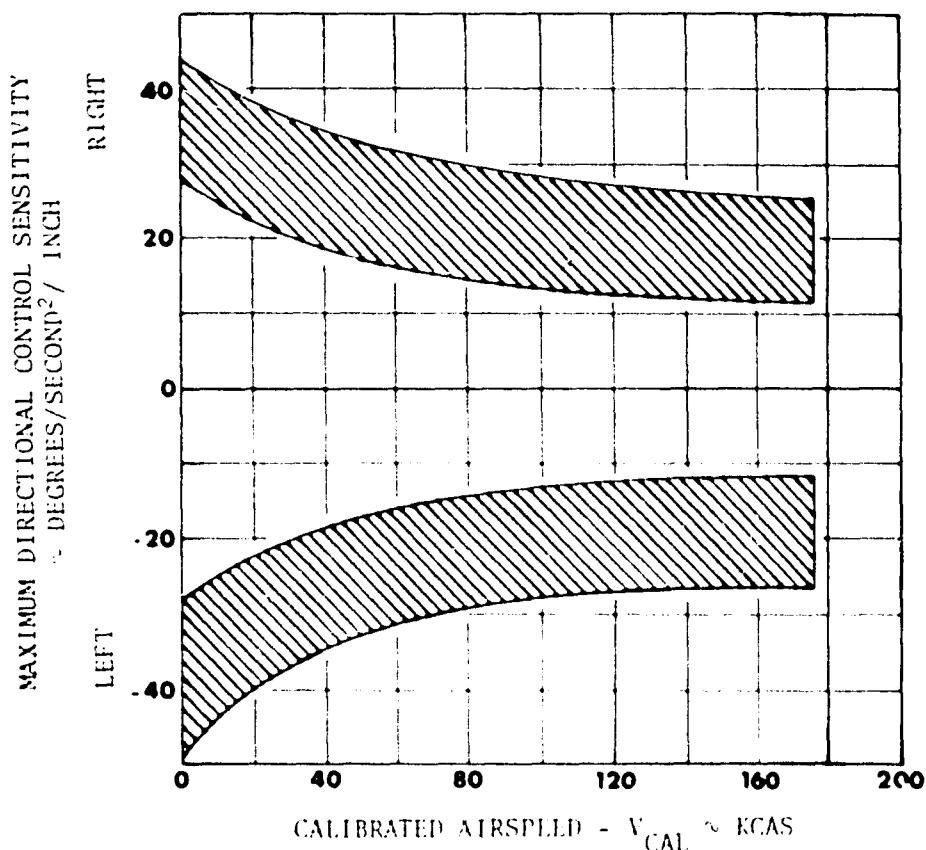


Figure 0. Directional Control Sensitivity.

80. As with sensitivity, the directional control response was maximum at low airspeeds and decreased with increasing airspeed. Time to reach the maximum rate varied from 0.8 second (low altitude, light weight) to 1.5 seconds (high altitude, heavy weight). Differences in gross weight and configuration had no significant effect on the maximum yaw rate. Increasing density altitude resulted in a decreasing response. There was no significant change in directional control response characteristics with SCAS OFF when compared to corresponding SCAS ON condition. A summary of maximum directional control response is presented in figure P.

NOTES: 1. SCAS ON
2. SHADED ENVELOPE CONTAINS ALL SCAS ON
FLIGHT TEST DATA

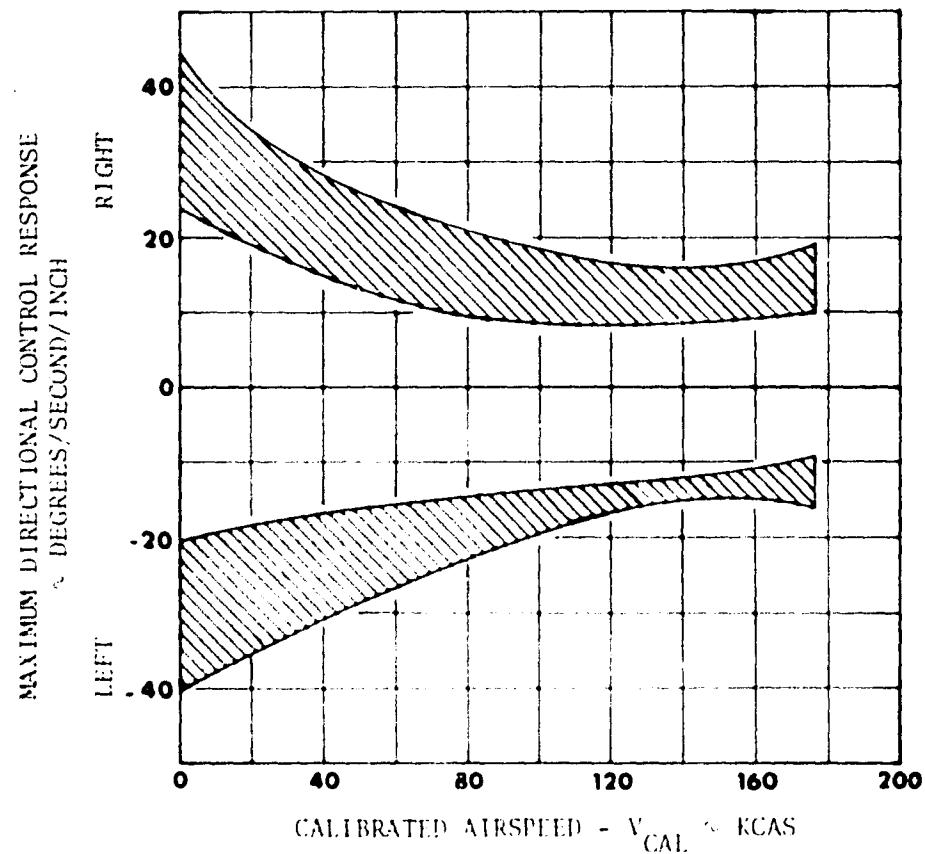


Figure P. Directional Control Response.

81. Yaw attitude displacement was defined at 1 second after a 1-inch pedal input. This displacement was maximum at low airspeeds and minimum at V_L . The heavy hog configuration had a slightly lower yaw displacement than did the clean configuration at all airspeeds. Increased gross weight or altitude also reduced the yaw displacement at 1 second. With SCAS OFF, the yaw characteristics were similar to those with SCAS ON except that all yaw displacements were decreased by 5 to 6 deg/inch. Figure Q presents a summary of the yaw displacement characteristics for all SCAS ON conditions tested.

NOTES: 1. SCAS ON
 2. SHADED ENVELOPE CONTAINS ALL SCAS ON
 FLIGHT TEST DATA

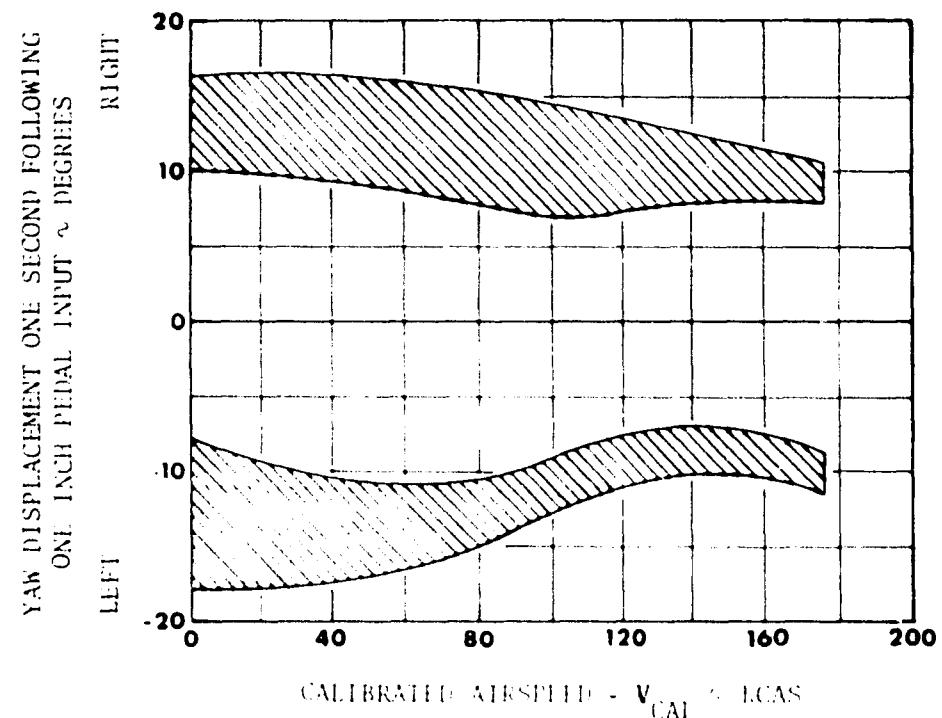


Figure Q. Yaw Attitude Displacement.

82. The directional controllability characteristics were good. During simulated tracking maneuvers, it was determined that, except for the characteristic of changing directional control trim with airspeed discussed in paragraphs 26 and 31, minimal pilot effort was required to maintain an adequate performance level (HQRS 2). One characteristic which was undesirable was the resultant high roll rate which occurred during forward flight at high speeds following a directional control step input. The roll was always in the same direction as the control input and was greater to the right than to the left. This phenomenon is due to the very high effective dihedral at this flight condition and, in fact, prevented the buildup of significant sideslip angle during directional step inputs at high speed. SCAS ON or OFF had no significant effect on this roll-yaw coupling.

LANDING GEAR CROSS-TUBE FAIRINGS EFFECTS

83. Controllability tests were conducted with landing gear cross-tube fairings removed at trim airspeeds of $0.8V_H$, V_H and V_L . Tests were conducted to investigate both lateral and directional characteristics. Only slight variations were noted between the two configurations in the yaw axis; however, a large increase in sensitivity and response was noted in the lateral axis with landing cross-tube fairing removed. With the fairings removed, the lateral sensitivity was more than $20 \text{ deg/sec}^2/\text{in.}$ greater than with fairings installed. The time to achieve maximum acceleration was essentially unchanged. The lateral response was approximately 10 deg/sec/in. greater, and time to maximum rate was 0.7 second as compared to 1 second with the fairings installed. Figure 164, appendix VII, illustrates the comparison between fairings on and off for lateral sensitivity and response. The maximum value of 24 deg/sec/in. lateral control response does not meet the requirement of paragraph 3.3.15 of MIL-H-8501A and is qualitatively determined to be excessive. The excessive roll rate and decrease in lateral-directional damping (para 60) made precise maneuvering of the aircraft extremely difficult when performing normal flight tasks (HQRS 5). However, pilot workload reached an intolerable level when performing maneuvers where precise attitude and coordinate flight were required to accomplish the intended mission for this aircraft (HQRS 7).

HOVER CONTROLLABILITY

84. Hover controllability tests were conducted primarily in the clean configuration. The hover controllability conditions tested are presented in tables X through XII, appendix VIII. A portion of these tests was also conducted with the SCAS OFF. The C_T range flown during these hovering tests was 0.0037 to 0.0052. These tests were conducted IGE at a skid-height range from 5 to 15 feet at mid cg loading. The hover controllability data are presented in figures 247 through 279, appendix VII. These data are summarized as a function of thrust coefficient (C_T) in figures 244 through 246.

Longitudinal

85. With SCAS ON, the longitudinal controllability characteristics varied slightly with C_T . The aircraft reaction was generally greater following a forward control input than with an aft input. The longitudinal sensitivity was approximately $10 \text{ deg/sec}^2/\text{in.}$, and time to reach maximum acceleration was approximately 0.2 second. The maximum response was essentially constant throughout the C_T

range at 5 deg/sec/inch. The time to reach maximum pitch rate varied from 0.8 to 1.0 second depending on the C_T . The longitudinal displacement at 1 second following control input remained relatively constant at 3.5 deg/in. as C_T varied. This exceeded the minimum value (2.05 deg/in.) required by paragraph 3.2.13 of MIL-H-8501A. There was no significant change in the longitudinal controllability characteristics in hover due to configuration change. The longitudinal controllability characteristics with the SCAS OFF were essentially the same as with SCAS ON except that the maximum pitch rate and resultant pitch attitude change were slightly greater.

86. The longitudinal controllability characteristics during hover were satisfactory. In all cases, the helicopter reacted in the desired direction to a cyclic control step input, and the resultant rates and accelerations were satisfactory. Precision hovering required an unnecessarily high amount of pilot effort due to the high cyclic breakout forces discussed in paragraph 17.

Lateral

87. The lateral control sensitivity with SCAS ON was approximately 16.5 deg/sec²/in., and the time required to achieve maximum acceleration was a constant 0.15 second. Maximum roll response varied from 18 to 21 deg/sec/in., and time required to achieve maximum rate varied from 0.75 to 0.9 second. Lateral controllability characteristics were essentially unaffected by variations in C_T store configuration, ordnance loading and sense of the input (left or right).

88. The lateral controllability characteristics changed only slightly when the SCAS was not operating. The maximum acceleration per inch of lateral cyclic control input was less in most cases, and the time to reach peak roll acceleration increased to approximately 0.35 second. The maximum roll rate and resultant roll attitude change were greater with SCAS OFF than with SCAS ON. The time to reach maximum roll rate remained the same (0.75 to 0.9 second).

89. The maximum allowable roll rate stated in paragraph 3.3.15 of MIL-H-8501A was exceeded slightly in some cases; however, no tendency to overcontrol was noted. In addition, the lateral controllability characteristics in hover comply with the requirement stated in paragraphs 3.3.16 and 3.3.18 of MIL-H-8501A.

90. The lateral controllability characteristics in hover were similar to the longitudinal controllability in that the aircraft reacted in the proper direction to a control step input, and the resultant rates and accelerations were satisfactory. The high

control breakout forces had a more detrimental effect on pilot effort required for precise hovering in the lateral axis than in the longitudinal axis (para 86).

91. The maximum tail rotor horsepower recorded during recovery from a left lateral step input during the controllability tests ranged between 200 to 260 horsepower. The magnitude of the tail rotor horsepower depended on the dynamic characteristics of the aircraft as well as the magnitude of the control input during recovery. Tail rotor horsepower was maximum at SL and decreased with altitude for a given control input. The 42- and 90-degree gear boxes were replaced several times during the tests because of unacceptable gear wear patterns. There was insufficient directional control to maintain a constant heading during recovery from a right lateral step input. This problem is related directly to the translational handling qualities discussed in paragraphs 42 through 46.

Directional

92. The directional controllability characteristics in hover varied significantly with variations in main rotor C_T . Figure R presents the results of this test. When hovering at a C_T greater than 0.00465, less than 1 inch of left directional control remained; hence, inputs were limited to the available control travel. The yaw displacement requirement of paragraph 3.3.5 of MIL-H-8501A was not met except within the very limited range of C_T values as indicated in figure R. Directional control margin was inadequate when the average directional control position was less than 10 percent from the control limit. In order to comply with the directional axis requirement of MIL-H-8501A, a significant increase in tail rotor thrust is required. The directional controllability characteristics are considered to be unacceptable, and correction is mandatory. With SCAS OFF, the aircraft reaction to a directional control step input was generally less than with SCAS ON.

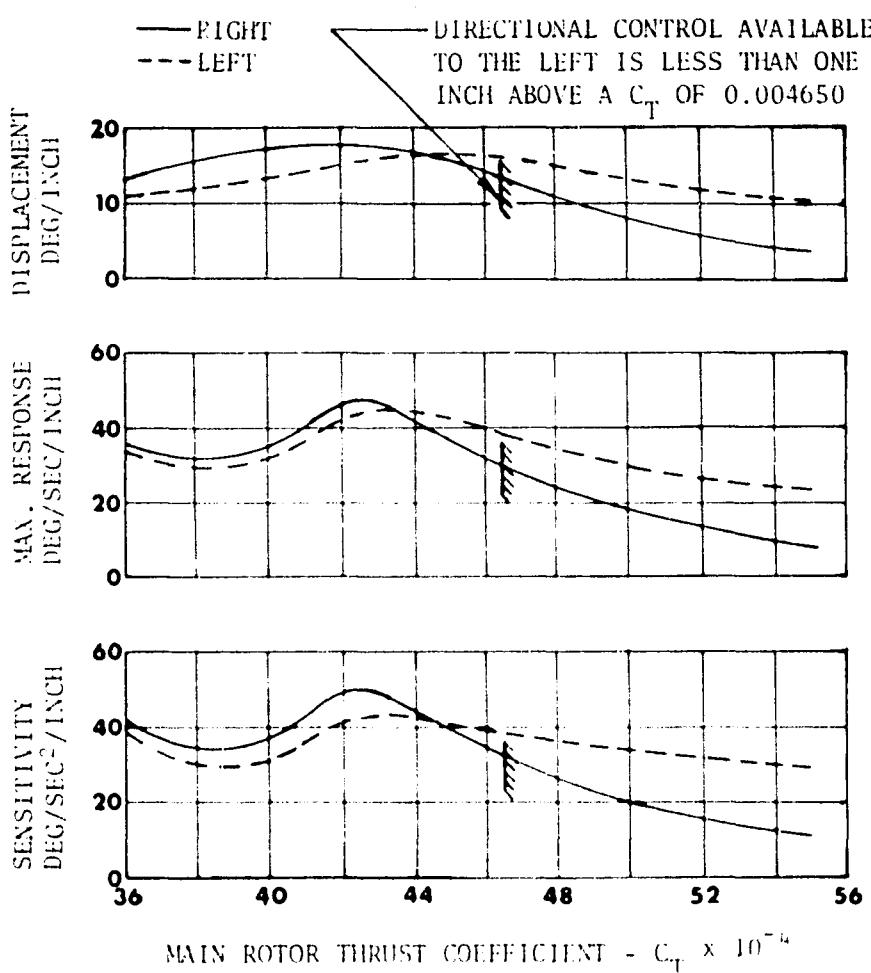


Figure R. Directional Hovering Controllability.

93. A related problem to the insufficient directional control problem is the tail rotor power transfer limitation discussed in paragraph 49. Tail rotor horsepower was measured for directional control inputs during most of the directional controllability testing. The change in tail rotor horsepower required to initiate a directional heading change was generally found to be a function of pedal input magnitude. Peak tail rotor horsepower encountered when arresting turns varied from 210 to 225 horsepower. The tail rotor horsepower required to arrest a turn rate was a function of the following parameters: yaw rate, yaw angular acceleration and rate of pedal control input. These high horsepowers resulted in the unacceptable gear wear patterns of the 42- and 90-degree gear boxes as discussed in paragraph 49. Figures 287 through 289, appendix VII, present the tail rotor horsepower encountered during hover controllability tests.

94. The directional controllability of the AH-1G is poor and jeopardizes safe mission accomplishment where insufficient left directional control exists to either develop an adequate left yaw rate or to satisfactorily arrest a right yaw rate. For the C_T range where more than 10 percent of left directional control remains, an HQRS of 5 is assigned for the directional controllability in hover. For the C_T range where less than 10 percent of left directional control remains, an HQRS of 10 is assigned.

MANEUVERING STABILITY

95. Maneuvering stability tests were conducted to evaluate the longitudinal control characteristics of the AH-1G. The two techniques used during this test were wind-up turns and symmetrical pull-ups. For both techniques, the aircraft was first stabilized at a trim airspeed in level flight, and the collective and force trim settings were maintained throughout the maneuver. During the wind-up turns, the helicopter was stabilized at increasing increments of normal acceleration in a constant-airspeed, coordinated turn. During the symmetrical pull-ups, climbs and dives were performed establishing increasing increments of normal acceleration in a symmetrical pull-up as the helicopter passed through the level flight attitude at the trim airspeed and altitude. The aircraft was evaluated at two airspeeds: 0.8 V_H and V_H . The configurations tested were: clean wing, forward and aft cg loading at 7800 pounds and aft cg loading at 7000 pounds. The average density altitude for these tests was 5000 feet. The results of these tests are presented in figure 291, appendix VII. Also, a summary of the maneuvering stability is presented in figure 290.

96. The helicopter possessed positive maneuvering stability. As the load factor was increased, an increase in aft longitudinal force (pull) and aft longitudinal control position was required. Higher gradients were experienced at the forward cg loading than at the aft cg loading. Extrapolation of these data indicates that both the longitudinal control position gradient and longitudinal force gradient would be stable throughout the cg envelope of the aircraft. Increasing gross weight caused both the control position and force gradients to increase as did decreasing airspeed. No feedback was noticed in the cyclic control as was indicated in references 2 and 17, appendix I.

97. There was little or no lateral control variation from trim with increasing load factor during the symmetrical pull-ups. However, there was some right displacement of the lateral control from trim in the wind-up turns as load factor was increased. The magnitude of this right lateral control displacement was larger in wind-up turns to the right. The lateral control was approximately 1.0 inch from trim at the highest attained load factor. A summary of lateral control displacement during maneuvering stability tests is presented in figure 292, appendix VII. This lateral control migration with normal acceleration was not noticeable to the pilot. The maximum bank angles attained were 72 degrees (left bank) in a left wind-up turn and 68 degrees (right bank) in a right wind-up turn. These values were obtained at the light gross weight (7000 pounds) and aft cg loading. The maneuvering stability characteristics are rated highly desirable. The control position and force gradients were adequate and displayed no discontinuities. An apparent change in stick force per g caused some concern during high-speed, constant-g pullouts. When normal acceleration was maintained at 2g's or above during the pullout, the rapid decrease in airspeed during the maneuver resulted in a trim change which reduced the stick force noticeably. For trimmed dive conditions, a decrease of 50 to 60 knots in airspeed during a constant-g pullout reduced the stick force to approximately zero. This characteristic should be noted in the KH-1G operator's manual (ref 20, app 1) and should be considered in follow-on control system designs.

AIRCRAFT REACTION TO ENGINE FAILURE

98. The aircraft reactions following a sudden engine failure were evaluated to determine the adequacy of pilot cues, identify the recovery techniques required to establish autorotation and determine MIL-H-8501A compliance. Sudden engine failure was simulated by rapidly rotating the throttle to the ground idle position. All tests were initiated from stabilized wings-level flight. Following the simulated engine failure, all flight controls were held fixed for 2 seconds or until recovery was necessary to evaluate recognition cues, required pilot actions and effect of delay times. All tests were conducted with SCAS ON. Results of these tests are summarized in figures 293 through 297, appendix VII. Time histories of several simulated engine failures are presented in figures 298 through 301. Tests were conducted under conditions as shown in table 13, appendix VIII.

Aircraft Motions Following Simulated Engine Failures

99. The initial reaction of the aircraft following simulated engine failures was, for all cases, an immediate yaw to the left as the rotor rpm began to decrease. This was followed by a left roll. The initial yaw acceleration was a function of the engine torque at the instant of failure. A slight pitch-up tendency was controlled by the SCAS before being sensed by the pilot. The left roll induced by the left yaw reaction (dihedral effect) was slight at low speeds (60 to 80 KCAS) and was controlled by the lateral SCAS so that no roll rates were sensed by the pilot. At airspeeds greater than 80 KCAS, the roll rates saturated the lateral SCAS and resulted in increasing left roll rates with increasing airspeed. At approximately 120 KCAS with a cruise power setting, the roll rate reached 25 to 28 deg/sec in 2 seconds or less. Since the dihedral effect becomes greater with increasing airspeed, the time to reach the maximum acceptable roll rate (25 to 28 deg/sec) was decreased and reduced the time before recovery was initiated. At maximum airspeeds evaluated, the yaw/roll reaction became very severe. Heavy buffeting of the tail boom and vertical stabilizer was encountered at 170 KCAS with a 0.5-second delay.

Engine Failure Cues

100. The reactions and indications sensed by the pilot following sudden engine failure are strong and clear: audible (loss of engine noise, low rpm audio signal, change of rotor sound), visual (engine and rotor instruments, low rpm warning light, attitude change) and kinesthetic (yaw and roll accelerations).

Delay Time Evaluation

101. The time available for pilot recognition and reaction to sudden engine failure (delay time) was evaluated for all conditions. For each condition, the critical control input was determined. For full-power climbs at 65 KCAS, the delay time possible was greater than 2 seconds. Aircraft attitudes and rates were not objectionable during full-power climb, and controlling rotor rpm decay (approximately 27 rpm/sec) with the collective was the critical pilot action. For level flight conditions at, or near, the airspeed for minimum power required (65 to 75 KCAS) delays in excess of 2 seconds for all controls are possible. Aircraft attitude and rotor rpm decay were easily controlled. For all level flight conditions at airspeeds between 60 and 120 KCAS,

a 2-second delay on all controls was achieved. At approximately 120 KCAS, the maximum tolerable left roll rate (25 to 28 deg/sec) was reached and recovery action was required. As the airspeed was further increased, the maximum tolerable delay time on the cyclic and directional controls decreased. At 150 KCAS with the engine developing maximum power, recovery action (aft and right cyclic and right directional control) was required after approximately 1 second for all configurations and gross weights. At V_L (165 to 175 KCAS) for the minimum usable test altitude, the maximum delay time recorded was 0.7 second. Because of the severity of the aircraft reaction following sudden engine failure, the requirement for pilot response of less than 1 second is unacceptable. Qualitative results of other tests (ref 21, app 1) indicated that 1-second delays were acceptable at all airspeeds for engine torque settings less than 35 psi. Additional testing is necessary to quantitatively evaluate the effects of reduced engine power on simulated engine failure maneuvers.

Recovery Technique

102. The recovery technique following sudden engine failure was similar for all conditions. For the lower airspeeds (60 to 100 KCAS), only small cyclic inputs were required to control aircraft attitude, and a smooth lowering of the collective was adequate to control the rotor rpm decay and establish autorotation. At the higher airspeeds (100 KCAS to V_L), prompt control of the aircraft attitude (yaw and roll to the left) followed by a positive cyclic flare was essential. The cyclic flare reduced the rate of descent and checked rotor rpm decay rate while reducing the airspeed to the desired autorotation value. The collective was lowered smoothly after the flare was established so that the rotor rpm was in the normal range when the autorotational airspeed was reached.

Rotor RPM Decay Characteristics

103. The rotor rpm decay rate varied from 17 to 27 rpm/sec depending on the collective setting (or engine torque) at the time of simulated engine failure. Airspeed with R/C had no measurable effect on the decay rate (figs. 293 through 297, app VII). Minimum rotor speeds of 260 to 280 rpm were common for delay times of 2 seconds. The lowest rotor rpm encountered during the tests was 219 rpm for a 1.8-second delay at 120 KCAS at 10,000 feet. The rotor rpm responded quickly to recovery action by the pilot.

Effects of Gross Weight, Center of Gravity, Density Altitude and Wing-Stores Configuration

104. The aircraft reactions following a simulated engine failure were basically similar for all conditions tested. The aircraft reaction to failure at light grwt was quicker than at heavy grwt. The aircraft response to control inputs and susceptibility to control feedback were less during aircraft recovery at light grwt. The aircraft reactions at the medium grwt (8500 pounds) was less objectionable than either the heavy grwt (9500 pounds) or light (7500 pounds) grwt. Maximum rotor loading (gross weight times normal acceleration) was more difficult to attain at light weight; and, consequently, the maximum rotor speeds attainable during aircraft recovery were much lower (300 to 310 rpm). The reactions with forward cg loadings were more objectionable due to the increased nose-down attitude at the high airspeeds and the reduced amount of aft cyclic control available to effect recovery. Density altitude effects were not significant since the more critical high airspeeds were beyond the envelope limits. The external stores configurations tested (clean and four XM159 rocket pods installed) were not noticeably different.

Effects of Landing Gear Cross-Tube Fairings Removed

105. Reactions of the AH 1G following sudden engine failure were also evaluated with landing gear cross-tube fairings removed. No significant differences in the aircraft reactions were observed at airspeeds less than 160 ECAS: the maximum permitted airspeed for this configuration.

Limitations

106. The following characteristics and reactions were encountered which limited the testing and are the basis for operational limitations:

- a. Unacceptable left roll rates encountered at the high-speed, high-power conditions with a marginally acceptable pilot recognition and reaction time of 1 second.
- b. Heavy buffeting of the tail boom and vertical fin, at or near the limit airspeed conditions, following simulated engine failures at high-power settings.
- c. Heavy control feed-back during recovery from high-speed, simulated engine failures where the maximum tolerable aircraft attitudes and rates were recorded.

d. Large main rotor flapping angles (70 percent of total available before hub and mast contact) were recorded during limit condition recoveries. The magnitude of the main rotor flapping angle can be increased to a dangerous level by lowering the collective before a positive flare and a resultant increased normal acceleration is established.

107. To limit the operation of the AH-1G at conditions where the reactions following sudden engine failure are unacceptable, the following should be accomplished:

a. Limit indicated engine torque to 35 psi for dive air-speeds greater than 150 KCAS.

b. Mark all airspeed indicators with yellow caution ARC between 150 and 190 knots.

c. Mark all torqueometers with a yellow caution stripe at 35 psi.

d. Revise paragraphs 4-15 through 4-25, 7-17, 8-26 and 8-38 of the AH-1G pilot's handbook (ref 20, app 1) in accordance with the preceding discussion.

MISCELLANEOUS

Trim Change Accompanying SCAS Disengagement

108. Tests were conducted to evaluate the aircraft reactions following SCAS disengagement. These tests were conducted at trim airspeeds between 55 KCAS and V_L in the heavy hog configuration. In all cases tested, the aircraft reacted with a gradual nose-up pitching motion and a slight right roll when SCAS was disengaged. The rates observed were very small and did not exceed the requirement of paragraph 3.5.9(a), MIL-H-8501A. No significant aircraft reaction was observed during subsequent SCAS reengagement during trimmed, stabilized flight. It is most probable that SCAS disengagement in stabilized flight would initially be undetected by the pilot except for the illumination of the appropriate warning lights and the decrease in aircraft dynamic stability as discussed in paragraph 57. The aircraft reactions following SCAS "hardovers" were not investigated during these tests. The results of the contractor in-flight SCAS qualification tests are presented in reference 22, appendix I.

SCAS Pylon Coupling

109. SCAS pylon coupling was not encountered during the Phase D program. This would indicate that the problem previously encountered during Phase B testing (ref 2, app 1) had been alleviated. However, a small amount of undamped aircraft motion was encountered at maximum power settings (topping power). These small, but annoying aircraft oscillations were probably due to engine oscillation and not SCAS pylon coupling. These oscillations were eliminated by reducing engine output power slightly below topping power.

Airspeed Calibration

110. Airspeed calibration tests were conducted to determine the position error of the standard and test (boom) airspeed systems in climbing, diving, autorotational and level flight. The methods used to calibrate the test airspeed system were a combination of the trailing bomb, paper aircraft and ground speed course. The calibration was conducted in the clean configuration only, and the data are presented in figures 302 through 304, appendix AII.

111. The standard airspeed system was calibrated using the trailing bomb and paper aircraft methods, and the results are presented in figure 299, appendix AII. In addition to the data gathered during this evaluation, the test results include data from the AH-1G Phase B test report (ref 2, 3 and 4, app II). The test configurations were clean, basic and outboard alternate. The position error in climbing and autorotational flight was less than 3 knots from 35 to 100 knots indicated airspeed (KIAS) and was acceptable. This airspeed band includes the airspeed for maximum glide. Higher position errors were present from 30 to 55 KIAS, but these errors are not deemed significant since the helicopter is normally accelerating or decelerating through this airspeed band.

112. The standard airspeed system calibration for level and diving flight was compared to the position errors listed in the operator's manual (ref 18, app I). This comparison is presented in figure 8 and shows essentially the same position error from 40 to 170 KIAS. For the airspeed ranges from 30 to 40 KIAS and 170 to 190 KIAS, there is a difference of 2 knots or less between the two sources of data. The airspeed position errors determined during this test are satisfactory for the aircraft's mission and should be incorporated into the operator's manual.

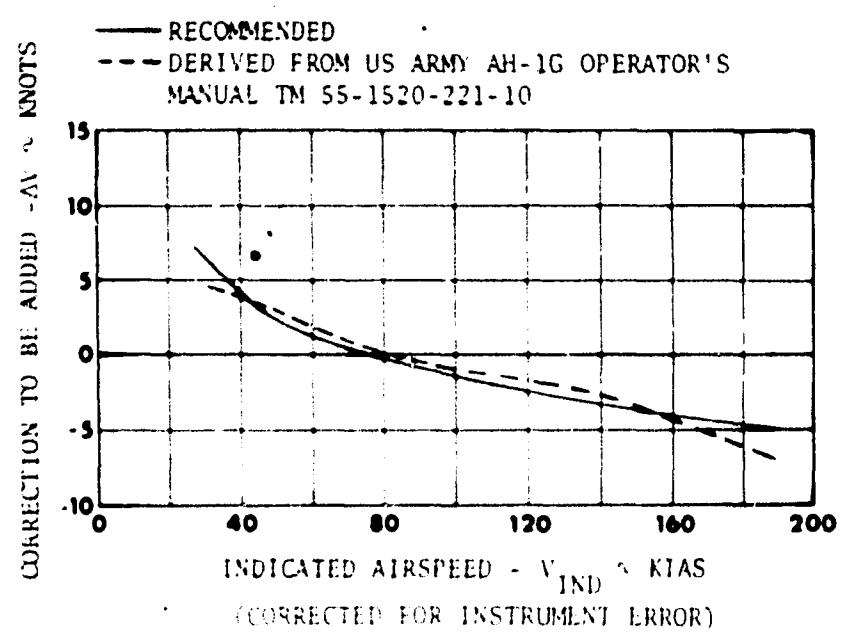


Figure S. Standard Airspeed System Calibration.

CONCLUSIONS

GENERAL

113. The handling qualities of the AH-1G are acceptable throughout the published flight envelope except for the deficiencies as listed in paragraph 118.

114. The deviation from MIL-H-8501A referred to in the AH-1G contract pertaining to the lateral-directional handling qualities does not establish adequate alternate standards for design or evaluation (paras 34 and 40).

115. A directional control margin of 10-percent total pedal travel is the minimum acceptable for operating the AH-1G (para 42).

116. The dynamic stability handling qualities of the AH-1G are unacceptable at airspeeds in excess of 160 KCAS with the landing gear cross-tube fairings removed and with the SCAS OK (paras 60 and 83).

117. The dynamic stability handling qualities of the AH-1G are unacceptable at airspeeds in excess of 115 KCAS with the landing gear cross-tube fairings removed and with the SCAS inoperative (para 61).

DEFICIENCIES AND SHORTCOMINGS AFFECTING MISSION ACCOMPLISHMENT

118. Correction of the following deficiencies is mandatory for successful accomplishment of the intended mission:

- a. The excessive cyclic control breakout forces (para 17).
- b. Inadequate directional control (paras 43 through 46).
- c. Inability to achieve maximum tail rotor blade angle (19 degrees) when full directional control is applied for all conditions with the present directional control/yaw SCAS geometry (para 47).
- d. The excessive tail rotor horsepower required for hovering and translational flight (paras 49, 91 and 93).

119. Correction of the following shortcomings is desirable for successful accomplishment of the intended mission:

- a. Neutral static longitudinal stability at airspeeds approaching V_L (para 28).
- b. Increase in right directional control with increasing airspeed in dive (paras 26 and 31).
- c. Directional instability between 10 and 19 knots at relative wind azimuths between 210 and 230 degrees (para 48).
- d. The poor longitudinal dynamic stability characteristics with the SCAS not operating (para 54).
- e. The decrease in lateral-directional damping with the SCAS OFF (para 57).

MILITARY SPECIFICATION COMPLIANCE

120. All stability and control handling qualities specified in reference 12, appendix I, are complied with except for the following paragraphs of MIL-H-8501A (not including paras 3.3, 3.6 and 3.7).

<u>Paragraph</u>	<u>Item</u>
3.2.10	Neutral static longitudinal stability at airspeeds above 170 KCAS.
3.2.4	Longitudinal breakout force is greater than the force gradient required to produce the first inch of longitudinal control displacement from trim.
3.2.7	Longitudinal breakout forces in excess of approved deviation from MIL-H-8501A.
3.5.4.1	Insufficient directional control to perform vertical climb throughout present flight envelope.
3.5.5 and 3.5.5.1	Insufficient time to recognize and institute corrective action following engine failure within the present flight envelope.
3.5.4.3, 3.5.4.4 and 3.5.4.5	Tests not conducted to check compliance.

121. All portions of paragraph 3.3 of MIL-H-8501A were met except the following. The contractor was not obligated to meet the following portions of MIL-H-8501A:

<u>Paragraph</u>	<u>Item</u>
3.3.2, 3.3.3, 3.3.5 and 3.3.6	Insufficient directional control during translational flight.
3.3.9	Neutral dihedral effect in autorotation.
3.3.11	Lateral breakout forces greater than the force gradient to produce the first inch of longitudinal control displacement from trim.
3.3.13	Lateral breakout forces in excess of approved deviation from MIL-H-8501A.
3.3.15	Angular roll rate is greater than 20 degrees/second/inch for some flight conditions.

RECOMMENDATIONS

122. The handling qualities and flight envelope limitations presented in this report are recommended for inclusion in the operator's manual.
123. Correct deficiencies on a priority basis.
124. Correct shortcomings at the earliest convenience.
125. Restrict the operational flight envelope to conditions which provide a 10-percent directional control margin (para 42).
126. Initiate action to increase directional control margins and improve the torque transfer capability of the tail rotor drive system (paras 46 and 49).
127. Revise deviation 1 of MIL-H-8501A granted in the AH-1G contract, pertaining to the lateral-directional handling qualities, to include adequate standards for design and evaluation (para 34).
128. Incorporate the following flight envelope limitations:
 - a. Limit airspeed to 160 KCAS (SCAS ON) and 115 KCAS (SCAS OFF) when landing gear cross-tube fairings are not installed (paras 60, 61 and 83).
 - b. Mark airspeed indicators (pilot and copilot) with a yellow caution arc between 150 KIAS and limit airspeed (para 107).
 - c. Mark engine torque meters (pilot and copilot) with a yellow stripe at 35 psi (para 107).
 - d. Mark airspeed indicators (pilot and copilot) with a yellow caution arc between 150 KIAS and limit airspeed (para 107).

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14. Military Specification, MIL-H-8501A, *Helicopter Flying and Ground Handling Qualities; General Requirements For*, 7 September 1961, Amended 3 April 1962.
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21. Final Report, USAASTA, Project No. 69-01, *Airworthiness and Flight Characteristics Test, AH-1G Helicopter with Stabilized Night Sight (SNS), Phase II*, August 1970.
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APPENDIX II. BASIC AIRCRAFT INFORMATION AND OPERATING LIMITS

AIRFRAME

Rotor System

The 540 "door hinge" main rotor assembly is a two-bladed, semi-rigid, underslung feathering axis type rotor. The assembly consists basically of two all-metal blades, blade grips, yoke extensions, yoke trunnion, and rotating controls. Control horns for cyclic and collective control input are mounted on the trailing edge of the blade grip. Trunnion bearings permit rotor flapping. The blade grip to yoke extension bearings permit cyclic and collective pitch action.

Tail Rotor

The tail rotor is a two-bladed, delta-hinge type employing pre-coning and underslinging. The blade and yoke assembly is mounted to the tail rotor shaft by means of delta-hinge trunnion. Blade pitch angle is varied by movement of the tail rotor control pedals. Power to drive the tail rotor is supplied by a takeoff on the lower end of the main transmission.

Transmission System

The transmission is mounted forward of the engine and coupled to the engine by a short drive shaft. The transmission is basically a reduction gear box which transmits engine power at reduced rpm to the main and tail rotors by means of a two-stage planetary gear train. The transmission incorporates a free-wheeling unit at the input drive. This provides a disconnect from the engine in case of a power failure to allow the aircraft to make an autorotational landing.

Synchronized Elevator

The synchronized elevator, which has an inverted airfoil section, is located near the aft end of the tail boom and is connected by control tubes and mechanical linkage to the fore and aft cyclic control system. Fore and aft movements of the cyclic control stick produce a change in the synchronized elevator attitude.

Control Systems

A dual hydraulic control system is provided for the cyclic and collective controls. The directional controls are powered by a single servo cylinder which is operated by system No. 1. The hydraulic system consists of two hydraulic pumps, two reservoirs, relief valves, shut-off valves, pressure warning lights, lines, fittings, and manual, dual tandem, servo actuators incorporating irreversible valves. Tandem power cylinders incorporating closed center four-way manual servo valves and irreversible valves are provided in the lateral, fore and aft cyclic and collective control system. A single power cylinder incorporating a closed center four-way manual servo valve is provided in the directional control system. The cylinders contain a straight-through mechanical linkage.

Force Trim

A magnetic brake and force gradient device is incorporated in the cyclic control and directional pedal controls. These devices are installed in the flight control system between the cyclic stick and the hydraulic power cylinders and between the directional pedals and the hydraulic power cylinder. The force trim control can be turned off by depressing the left button on the top of the cyclic stick. The gradient is accomplished by springs and magnetic brake release assemblies which enable the pilot to trim the controls as desired.

Cyclic Control Stick

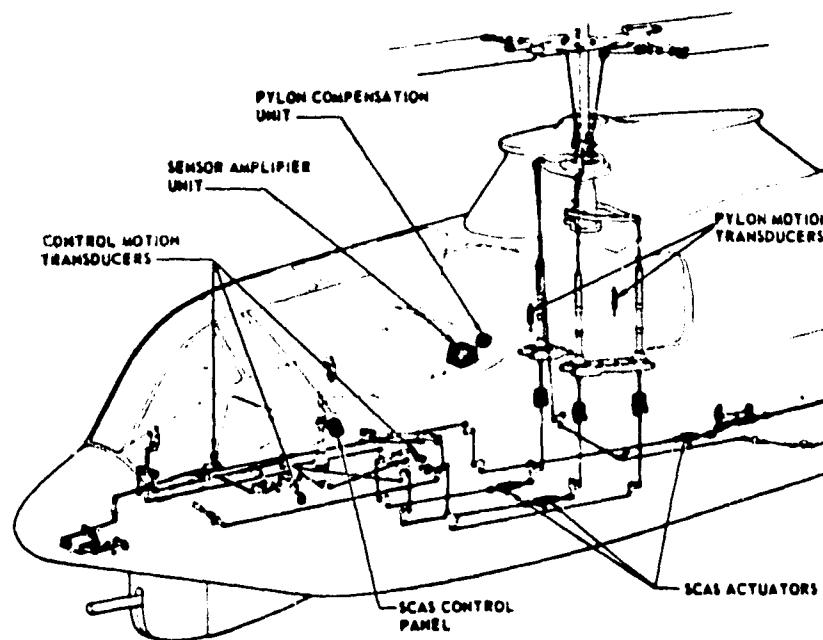
The pilot and gunner cyclic stick grip each have a force trim switch and a SCAS release switch. The pilot's cyclic stick has a built-in operating friction. The cyclic control movements are transmitted directly to the swash plate. The fore and aft cyclic control linkage is routed from the cyclic stick through the SCAS actuator, to the dual boost hydraulic actuator and then to the right horn of the fixed swash plate ring. The lateral cyclic is similarly routed to the left horn.

Collective Pitch Control

The collective pitch control is located to the left of the pilot and is used to control the vertical mode of flight. Operating friction can be induced into the control lever by hand tightening the friction adjuster. The pilot and gunner collective pitch controls have a rotating grip-type throttle.

Tail Rotor Pitch Control Pedals

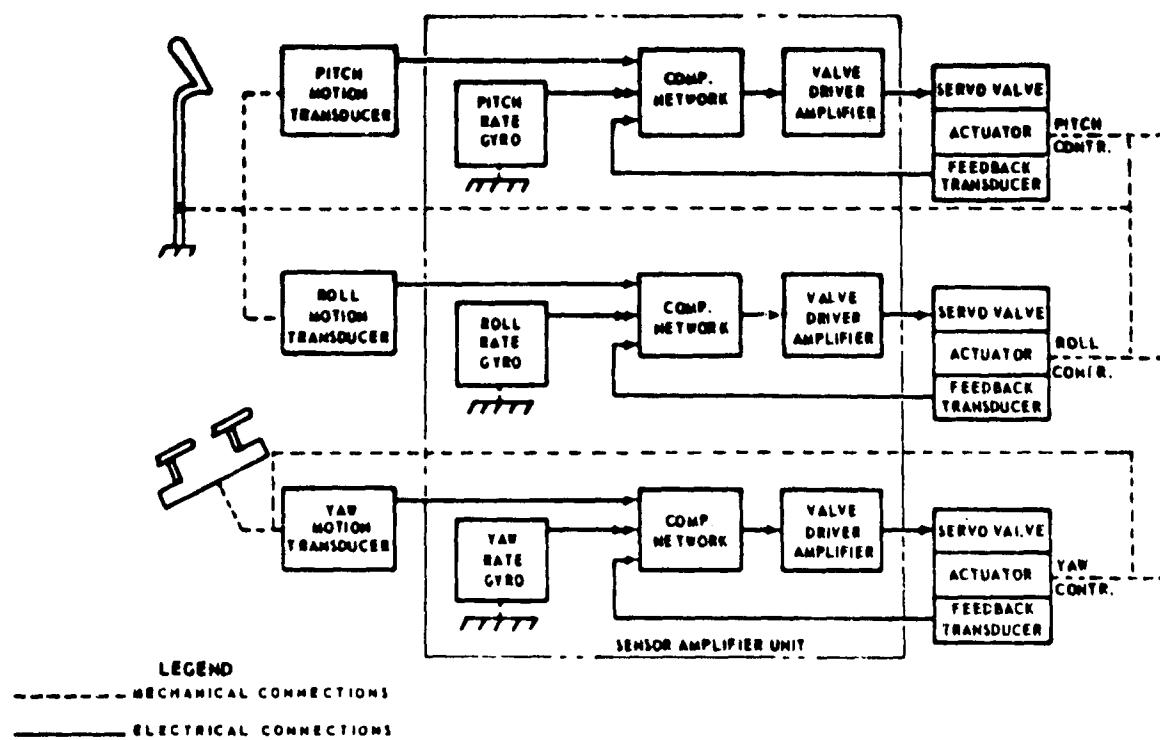
Tail rotor pitch control pedals alter the pitch of the tail rotor blades and thereby provide the means for directional control. The force trim system is connected to the directional controls and is operated by the force trim switch on the cyclic control grip.



Flight Controls Schematic

Stability and Control Augmentation System (SCAS)

The SCAS is a three-axis, limited-authority, rate-referenced stability augmentation system. It includes an electrical pilot input which augments the pilot's mechanical control input. This system permits separate consideration of airframe displacements caused by external disturbances from displacements caused by pilot input. The SCAS is integrated into the fore, aft, lateral and directional flight controls to improve the stability and handling qualities of the helicopter. The system consists of electro-hydraulic servo actuators, control motion transducers, a sensor/amplifier unit and a control panel. The servo actuator movements are not felt by the pilot. The actuators are limited to a 25-percent authority and will center and lock in case of electrical and/or hydraulic failure.



Interrelation of SCAS Components

ENGINE

Engine Description

The T53-L-13 engine, rated at 1400 shp, is a successor to the T53-L-11 engine. The additional power has been achieved with no change in the basic T53-L-11 engine envelope mounting and connection points and with a 6-percent increase in basic engine weight.

The performance gain is accomplished thermodynamically by the mechanical integration of a modified axial compressor, a two-stage compressor turbine and a two-stage power turbine into the T53-L-11 engine configuration.

Replacement of the first two compressor stators and changing of the first two stages of compressor rotor blades and disks results in an approximate 20-percent increase in mass air flow through the engine. This is accomplished without the use of inlet guide vanes.

An inlet flow fence, located on the outer wall of the inlet housing in the area of the previously used inlet guide vanes, provides the desired inlet conditions for the transonic compressor during acceleration at low speeds. At compressor speeds up to 70 percent, the

fence is in the extended position. Above 70 percent, the flow fence is retracted into the outer wall of the inlet housing. Similar to a piston ring, the circumference of the flow fence is changed by the action of a piston actuator powered by compressor discharge pressure.

The specification for this engine allows the use of JP-4 or JP-5 type fuel for satisfactory operation throughout the engine's operating envelope. During this program, JP-4 fuel was used.

Engine Power Control System

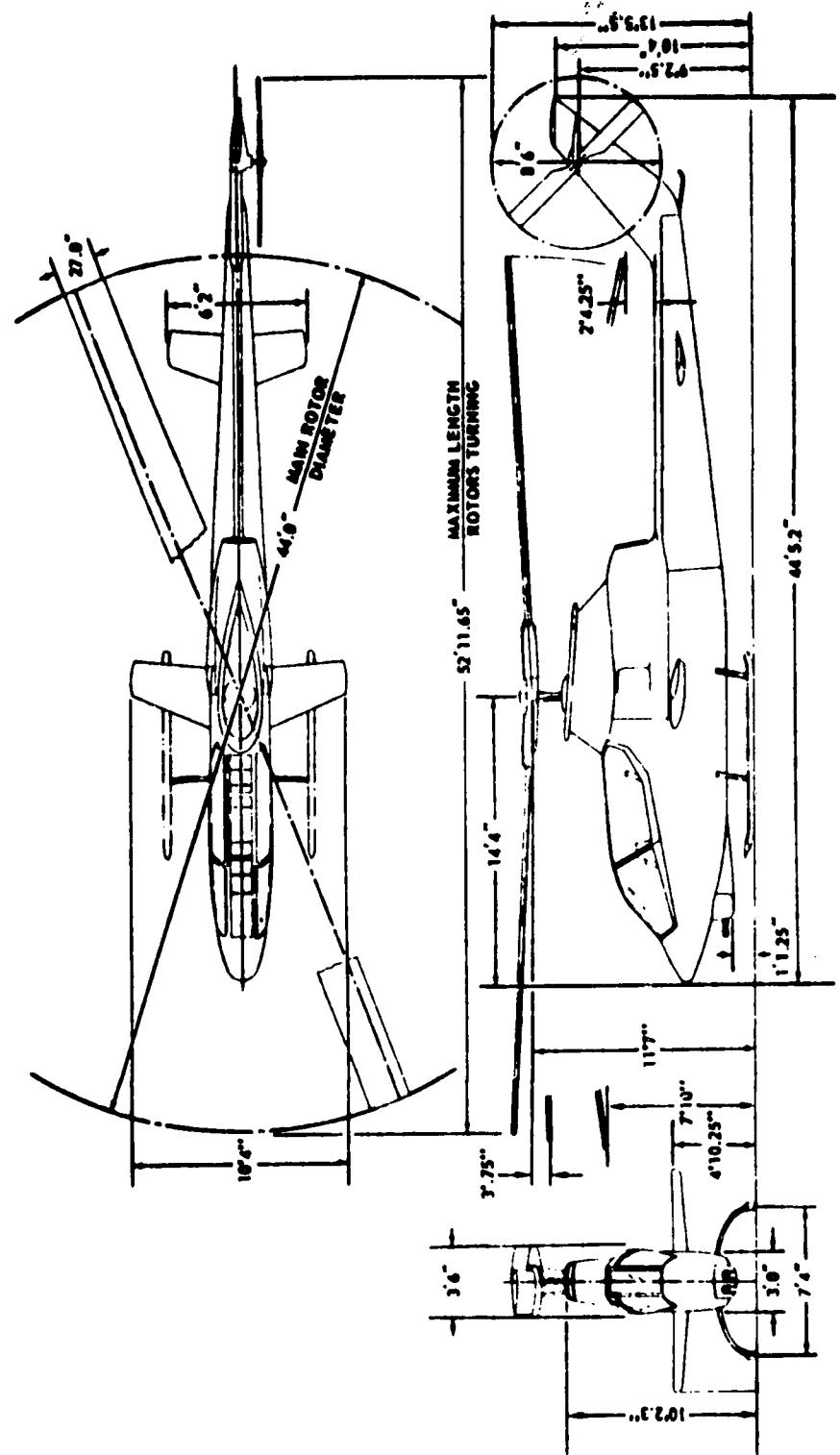
The fuel control for the T53-L-13 engine is a hydro-mechanical type of fuel control. It consists of the following main units:

- a. Dual-element fuel pump.
- b. Gas producer speed governor.
- c. Power turbine speed topping governor.
- d. Acceleration and deceleration control.
- e. Fuel shut-off valve.
- f. Transient air bleed control.

An air bleed control is incorporated within the fuel control to provide for opening and closing the compressor interstage air bleed in response to the following signals present in the power control:

- a. Gas producer speed.
- b. Compressor inlet air temperature.
- c. Fuel flow.

The fuel control is designed to be operated either automatically or in an emergency mode. In the emergency position, fuel flow is terminated to the main metering valve and is routed to the manual (emergency) metering and dump valve assembly. While in the emergency mode, fuel flow to the engine is controlled by the position of the manual metering valve which is directly connected to the power control (twist grip). During the emergency operation, there is no automatic control of fuel flow during acceleration and deceleration; thus, EGT and engine acceleration must be pilot-monitored.



Three-view drawing - AH-1G

BASIC AIRCRAFT INFORMATION

Airframe Data

Overall length (rotor turning)	637.2 inches
Overall width (rotor trailing)	124.0 inches
Center line of main rotor to center line of tail rotor	320.7 inches
Center line of main rotor to elevator hinge line	198.6 inches
Elevator area (total)	15.2 square feet
Elevator area (both panels)	10.9 square feet
Elevator airfoil section	Inverted Clark Y
Vertical stabilizer area	18.5 square feet
Vertical stabilizer airfoil section	Special camber
Vertical stabilizer aerodynamic center	FS 499.0
Wing area:	
Total	27.8 square feet
Outboard of BL 18.0 (both sides)	18.5 square feet
Wing span	10.33 feet
Wing airfoil section:	
Root	NACA 0030
Tip	NACA 0024
Wing angle of incidence	14 degrees

Main Rotor Data

Number of blades	2
Diameter	44 feet
Disc area	1520.5 square feet
Blade chord	27 inches
Rotor solidity	0.0651
Blade area (both blades)	99 square feet
Blade airfoil	9.33 percent symm special section
Linear blade twist	-0.455 deg/ft
Hub precone angle	2.75 degrees
Main rotor inertia	2900 slugs-ft ²

Antitorque Rotor Data

Number of blades	2
Diameter	8.5 feet
Disc area	56.74 square feet
Blade chord	8.41 inches
Rotor solidity	0.105
Blade airfoil	NACA 0010 modified
Blade twist	Zero degrees

For this test, the AH-1G with skid gear fairings removed: same as standard configurations (Normal limit for operational use: 160 KCAS)

All other configurations: 190 KCAS below a 4000-foot density altitude; decrease 8 KCAS per 1000 feet above 4000 feet

Gross Weight/Center of Gravity Envelope

Forward center of gravity limit: Below 7000 pounds, FS 190.0; linear increase to FS 192.1 at 9500 pounds

Aft center of gravity limit: Below 8270 pounds, FS 201.0; linear decrease to FS 200 at 9500 pounds

Sideslip Limits

Five degrees at V_L with linear increase to 20 degrees at 60 KCAS

Rotor and Engine Speed Limits (Steady State)

Power on:

Engine rpm	6400 to 6600
Rotor rpm	314 to 324

Power off:

Rotor rpm	294 to 339
Rotor rpm transient lower limit	250

Power on during dives and maneuvers:

Rotor rpm	314 to 324
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Temperature and Pressure Limits

Engine oil temperature	93°C
Transmission oil temperature	110°C
Engine oil pressure	25 to 100 psi
Transmission oil pressure	30 to 70 psi
Fuel pressure	5 to 20 psi

T53-L-13 Engine Limits

Normal rated EGT (maximum continuous)	625°C
Military rated EGT (30-minute limit)	645°C
Starting and acceleration EGT (5-second limit)	675°C
Maximum EGT for starting and acceleration	760°C
Torque pressure limit	50 psi

Transmission Drive System Ratios

Engine to main rotor	20.383:1.0
Engine to antitorque rotor	3.990:1.0
Engine to antitorque drive system	1.535:1.0

Test Aircraft (S/N 6615247) Control Displacements

Longitudinal cyclic control:

Full forward to full aft with SCAS nulled 9.07 inches

Lateral cyclic control:

Full left to full right with SCAS nulled 10.00 inches

Directional (pedal) control:

Full left to full right with SCAS nulled 7.07 inches

Collective control:

Full up to full down with SCAS nulled 9.30 inches

Test Aircraft (S/N 6615247) SCAS Authority

Longitudinal SCAS authority:

±12.5 percent or ±1.13 inches of longitudinal
cyclic control displacement

Lateral SCAS authority:

±12.5 percent or ±1.25 inches of lateral
cyclic control displacement

Directional SCAS authority:

±12.5 percent or ±0.88 inch of directional
(pedal) control displacement

Test Aircraft (S/N 6715695) Control Displacements

Longitudinal cyclic control:

Full forward to full aft with SCAS nulled 10.08 inches

Lateral cyclic control:

Full left to full right with SCAS nulled 9.90 inches

Directional (pedal) control:

Full left to full right with SCAS nulled 5.97 inches

Collective control:

Full up to full down with SCAS nulled 8.98 inches

Test Aircraft (S/N 6715695) SCAS Authority

Longitudinal SCAS authority:

± 12.5 percent or ± 1.26 inches of longitudinal
cyclic control displacement

Lateral SCAS authority:

± 12.5 percent or ± 1.24 inches of lateral
cyclic control displacement

Directional SCAS authority:

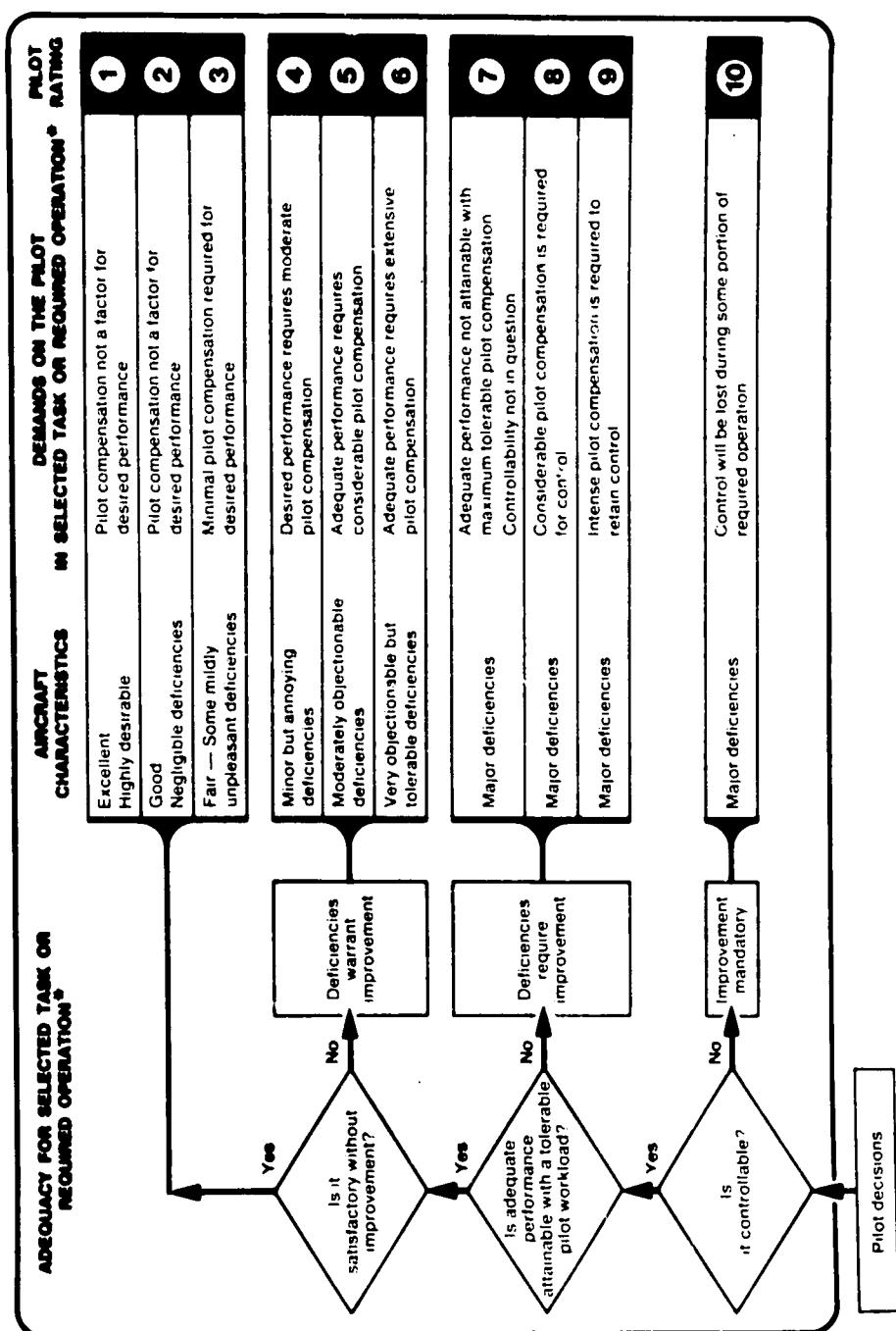
± 12.5 percent or ± 0.75 inch of directional
(pedal) control displacement

OPERATING LIMITATIONS

Limit Airspeed (V_L)

Any configuration with XM159 rocket pods: 180 KCAS below a 3000-foot density altitude; decrease 8 KCAS per 1000 feet above 3000 feet

APPENDIX III. HANDLING QUALITIES RATING SCALE



APPENDIX IV. TEST TECHNIQUES AND DATA REDUCTION PROCEDURES

INTRODUCTION

Nondimensional Method

1. Tests were flown at different combinations of gross weight and density altitude to determine if variation in these parameters caused a change in handling qualities. Correlation of these data were accomplished by summarizing the data as a function of main rotor thrust coefficient where applicable. Each individual test flight was flown at a constant main rotor thrust coefficient (C_T). A constant C_T was maintained by either increasing altitude as fuel was consumed (for flights conducted at altitude) or adding ballast to the aircraft as fuel was consumed (for flights conducted in ground effect). The equation used to determine the nondimensional main rotor thrust coefficient was:

$$\text{Thrust coefficient} = C_T = \frac{\text{GRWT}}{A \cdot R^2} \quad (1)$$

Instrumentation

2. All instrumentation in both aircraft was calibrated prior to commencing the test program. All quantitative data obtained during this flight test program were derived from special sensitive instrumentation. A detailed tabulation of the instrumentation is given in appendix V. Data were obtained from four aircraft sources and two ground support sources. The aircraft sources were: oscillograph, photopanel, pilot's panel (hand recorded), and engineer's panel (hand recorded). The ground support sources were: ground station and ground speed reference vehicle.

Weight and Balance

3. A high degree of control was maintained on weight and balance of the test helicopter. Variations in empty weight and cg, because of changes in helicopter component instrumentation, were defined by periodically weighing the helicopter.

4. The empty weight of test aircraft, S/N 615247, in the clean configuration without instrumentation installed could not be determined since the aircraft was partially instrumented when it was delivered to USAASTA at the beginning of the program. In addition, the aircraft

was not a production model and was not representative of a standard AH-1G. The empty weight of test aircraft, S/N 715695, in the clean configuration without instrumentation installed was 5805 pounds, and the longitudinal cg was 201.4 inches. This aircraft is considered to be representative of the production model aircraft. This weighing was performed with following conditions prevailing: engine and transmissions full of oil, trapped fuel not drained, ammunition boxes with covers and ammunition chutes installed for chin turret, four wing store pylon stations installed, air conditioning system not installed and weight and center of gravity adjusted for removal of jack pads. The fuel load of the aircraft was defined by measuring the fuel specific gravity and temperature after each fueling and by using an external sight gage on the calibrated fuel cell to determine fuel volume. Fuel used in flight was recorded by a calibrated fuel-used system, and the results were cross-checked with the sight gage reading following each flight. Helicopter loading and cg were controlled by using ballast.

Flight Control Systems

5. Control breakout forces, control force gradients and control force friction band were measured on the ground with the rotor in a static position. Hydraulic pressure and electrical power were supplied by ground support equipment during these tests. Breakout forces and control force characteristics were determined by using an electrical strain gage bridge mounted in the appropriate location on each control. The control was displaced from the trim condition at a rate of 0.1 to 0.2 inch/second. A continuous record of control position and control force was made during the test. The breakout forces and control force friction band were also checked during flight.

STATIC STABILITY CHARACTERISTICS

Static Trim Stability

6. The static trim stability was investigated using the following technique. The helicopter was trimmed at various airspeeds (minimum of 5 points) over an airspeed range. The range of the airspeed flown for each flight condition depended on density altitude, gross weight and cg. While the aircraft was stabilized at each trim airspeed, all control forces, control positions and aircraft attitudes were recorded. Altitude was varied during each test flight to maintain a constant thrust coefficient for each trim airspeed.

Static Longitudinal Collective-Fixed Stability

7. The static longitudinal collective-fixed stability was investigated using the following method. The aircraft was first stabilized at the desired trim conditions. The helicopter was then stabilized at several airspeeds greater and less than the trim airspeed in ascending or descending flight. The airspeed was then varied by use of the longitudinal control. The trim collective control position, control trim force position and trim engine power were maintained as airspeed was varied about each trim airspeed. At each stabilized point the control positions, control forces and aircraft attitudes were recorded. Altitude was varied as fuel was consumed during each test flight to maintain a constant thrust coefficient for each trim airspeed.

Static Directional Stability and Effective Dihedral

8. The static directional stability and effective dihedral tests were conducted using the following technique. The aircraft was first stabilized at a trim airspeed at or near zero angle of sideslip. Sideslip angle was then varied and stabilized at different values (left or right of trim) until the limits of the sideslip envelope were achieved. The trim collective control position, control trim force position and trim airspeed were held constant as angle of sideslip was varied about each trim condition. At each stabilized point control positions, control forces and attitudes were recorded. Altitude was varied as fuel was consumed during each test flight to maintain a constant thrust coefficient for each trim airspeed.

Translational Flight Handling Qualities Evaluation

9. The translational handling qualities were investigated by conducting tests at various combinations of wind azimuth and airspeed. When the aircraft was stabilized in translational flight, parameters necessary to determine gross weight, ambient air conditions, azimuth, airspeed and directional control (pedal) with SCAS in nulled position were recorded. A ground vehicle with a calibrated speedometer was used as a reference when attempting to stabilize the helicopter at the desired airspeed and azimuth. Ambient wind velocity and direction were incorporated into the analysis when determining the airspeed and wind azimuth. Tests were conducted with wind velocities less than 4 knots. A constant thrust coefficient was maintained for each test condition by adding ballast as fuel was consumed.

Dynamic Stability

10. Dynamic stability characteristics of the AH-1G were tested by using the following techniques. The aircraft was first trimmed at the desired flight condition and airspeed. Gust disturbances were then simulated by making pulse-type control inputs of 1 inch for 0.5 to 1.0 second. The control was then returned to trim at which time all controls were held fixed until the aircraft motions damped out or recovery action was required. All resulting aircraft motions, as well as the control input, were recorded on the oscillograph. Altitude was varied as fuel was consumed during each test flight to maintain a constant thrust coefficient for each trim airspeed. Oscillations were evaluated by determining the resultant damping ratio and damped natural frequency. Times for the aircraft oscillations to damp were obtained from the timing lines on the oscillograph. The damped natural frequency and the damping ratio were derived for all conditions tested by two methods. These were the logarithmic decrement method and time ratio method.

11. The logarithmic decrement method was used for lightly damped to unstable aircraft motion. The range of damping ratios determined by this method was from -0.5 to +0.5. The damping ratio is a function of the amplitude and the damped natural frequency is a function of the period.

$$\ln \frac{x_m}{x_0} = -\frac{\pi m \zeta}{\sqrt{1 - \zeta^2}} \quad (2)$$

$$\omega_d = \frac{2\pi}{P} \quad (3)$$

12. The time ratio method was used to analyze the heavily damped aircraft motion which was usually characterized by one excursion from trim. The range of damping ratios determined by this method was from 0.5 to 1.8. Anything more heavily damped than 1.8 was considered "deadbeat," and no accurate means was available to determine either damping ratio or undamped natural frequency. When using the time ratio method, the undamped natural frequency was determined by the damping ratio and the damped natural frequency by means of the following formula:

$$\omega_d = \omega_n \sqrt{1 - \zeta^2} \quad (0 < \zeta < 1) \quad (4)$$

$$\omega_d = \omega_n \sqrt{\zeta^2 - 1} \quad (\zeta > 1) \quad (5)$$

13. Each flight condition was given a description as far as the kind of damping characteristic that it represented. These descriptions along with the damping ratio range are listed below:

<u>Description</u>	<u>Damping Ratio Range</u>
Negatively damped	$\zeta < 0$
Neutrally damped	$\zeta = 0$
Lightly damped	$\zeta = 0.1$ to 0.4
Heavily damped	$\zeta = 0.5$ to 1.8
Dead beat	$\zeta > 1.8$

Controllability

14. Aircraft controllability characteristics were investigated using the following technique. The aircraft was first stabilized at the desired flight condition and airspeed. Step-type control inputs were then initiated and held until the maximum rate was reached or recovery action was necessary. The magnitude of these step-type control inputs was varied (usually a minimum of 2 inputs in each direction) until a maximum control displacement of approximately 1.0 inch was realized. An adjustable, rigid control fixture was used to assist in achieving the desired inputs. Resultant aircraft motions as well as the control input were recorded on the oscilloscope. The maximum angular accelerations were derived by differentiating the rate trace at the inflection point.

Airspeed Calibration

15. The test airspeed indicator system (boom) and standard airspeed system were calibrated by comparing readings to a known reference. A calibrated trailing bomb was suspended from the helicopter with a cable approximately 50 feet in length. The aircraft was then stabilized at various airspeeds in level flight, climb and autorotation. By comparing the airspeed, corrected for instrument errors, of both systems to the bomb system, the error was defined.

16. The test boom airspeed indicator system was calibrated at higher airspeeds, both in level flight and dive using a T-28 pacer aircraft. The test and pacer aircraft were stabilized at the same airspeed, and data were recorded in each aircraft simultaneously. Since the position error of the pacer was known, the calibrated airspeed of the aircraft was readily computed.

17. The test boom airspeed indicator system was calibrated in level flight over a measured ground course. Two passes were flown on reciprocal headings at each airspeed to average wind effects. This method provided a cross-check on the trailing bomb method described in paragraph 15.

18. The test airspeed system consisted of a boom with a non-swiveling pitot-static head mounted just aft and below the nose of the aircraft. This pitot-static system was connected to the sensitive airspeed and altimeter indicators on various instrument panels. This system was used in place of the standard pitot-static system since the standard system was not accurate when both systems were installed on the aircraft.

APPENDIX V. TEST INSTRUMENTATION

USA S/N 6715695

All instrumentation was installed in the test helicopter prior to the start of the test program. This instrumentation provided data from three sources: pilot panel, copilot/engineer panel and a 50-channel oscilloscope. All instrumentation was calibrated. The flight test instrumentation was installed and maintained by the Instrumentation Branch, Logistics Division, USAASTA. The following test parameters were presented.

Pilot Panel

(Boom system) airspeed
(Boom system) altitude
Rate of climb
Rotor speed
Gas producer speed
(Standard system) torque pressure
Longitudinal control position
Lateral control position
Pedal control position
Collective control position
Center of gravity normal acceleration
Angle of sideslip



Photo 1. Pilot Panel for Aircraft S/N 6715695

Engineer Panel

(Boom system) airspeed
(Boom system) altitude
Outside air temperature
Rotor speed
Fuel used total
Oscillograph correlation counter

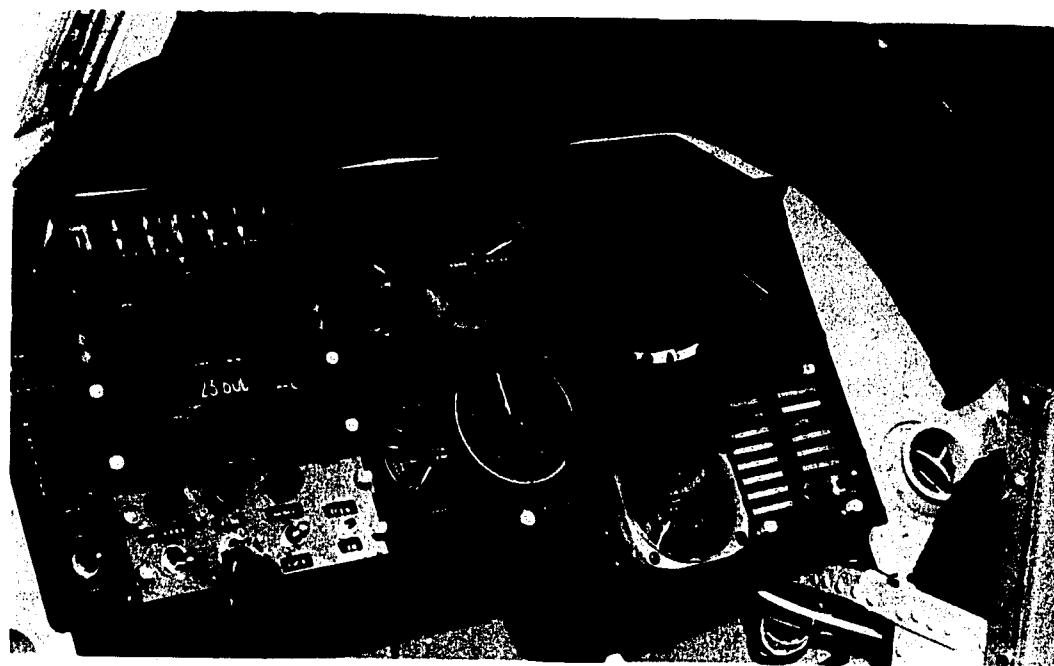


Photo 2. Engineer Panel for Aircraft S/N 6715695.

Oscillograph

Longitudinal control position
Lateral control position
Directional control position
Collective control position
Pitch attitude
Roll attitude
Yaw attitude
Pitch rate
Roll rate
Yaw rate
Angle of attack
Angle of sideslip
CG normal acceleration
Longitudinal SCAS position
Lateral SCAS position
Directional SCAS position
Rotor blip
Lateral and vertical vibration sensors (pilot seat)
Lateral and vertical vibration sensors (copilot/gunner seat)
Lateral and vertical vibration sensors (copilot/gunner site mounting)
Pilot event
Engineer event

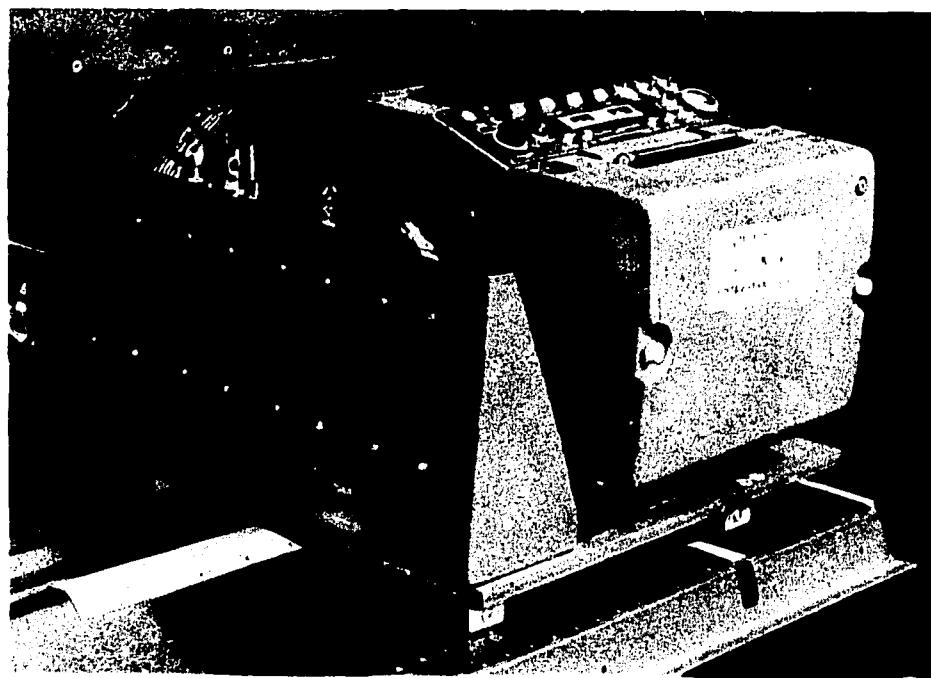


Photo 3. 50-Channel Oscillograph Installed in Aircraft S/N 6715695.

USA S/N 6615247

Flight test instrumentation was installed in the test helicopter prior to the start of this evaluation. This instrumentation provided data from four sources: pilot panel, copilot/engineer panel, photopanel and a 24-channel oscillograph. All instrumentation was calibrated. Some of the instrumentation was used for only a portion of the test program. The flight test instrumentation was installed and maintained by the Instrumentation Branch, Logistics Division, USAASTA. The following test parameters were presented:

Pilot Panel

(Standard system) airspeed
(Boom system) airspeed
(Boom system) altitude
Rate of climb
Gas producer speed
(Standard system) torque pressure
Exhaust gas temperature
Longitudinal control position
Lateral control position
Pedal control position
Collective control position
CG normal acceleration
Angle of sideslip



Photo 4. Pilot Panel for Aircraft S/N 6615247.

Engineer Panel

(Boom system) altitude
Outside air temperature
Rotor speed
Gas producer speed
Fuel used total
Torque pressure (high)
Torque pressure (low)
Exhaust gas temperature
Oscillograph correlation counter
Photopanel correlation counter
Fuel temperature
Engine fuel flow

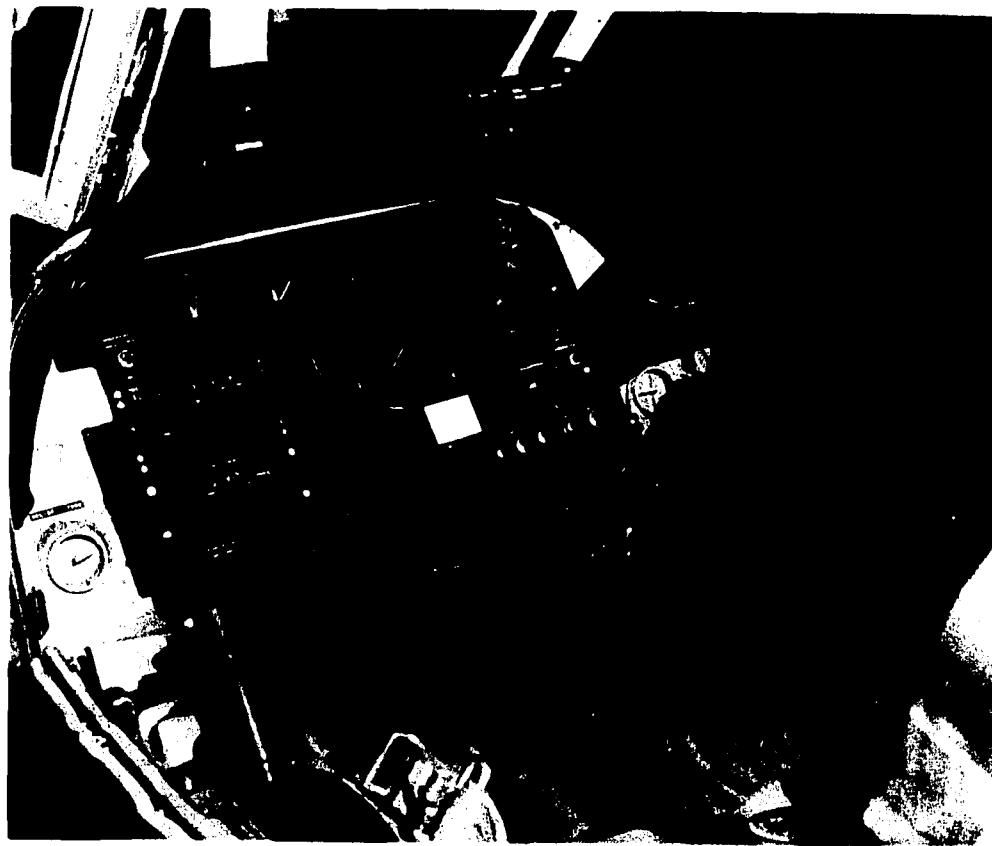


Photo 5. Engineer Panel for Aircraft S/N 6615247.

Photopanel

(Boom system) airspeed
(Standard system) airspeed
(Boom system) altitude
Rotor speed
Gas producer speed
Fuel used total
Torque pressure (high)
Torque pressure (low)
Exhaust gas temperature
Compressor inlet temperature
Compressor inlet total pressure
Inlet guide vane position
Bleed band position (light)
Fuel pressure at nozzle
Time (10-second stopwatch)
Oscillograph correlation counter
Photopanel correlation counter
Engineer event
Pilot event



Photo 6. Photopanel Installed in Aircraft S/N 6615247.

Oscillograph

Longitudinal control position
Lateral control position
Directional control position
Collective control position
Pitch attitude
Roll attitude
Yaw attitude
Pitch rate
Roll rate
Yaw rate
CG normal acceleration
Angle of sideslip
Angle of attack
Tail rotor torque
Main rotor flapping angle
Linear rotor speed
Photopanel correlation flip
Engineer event
Pilot event

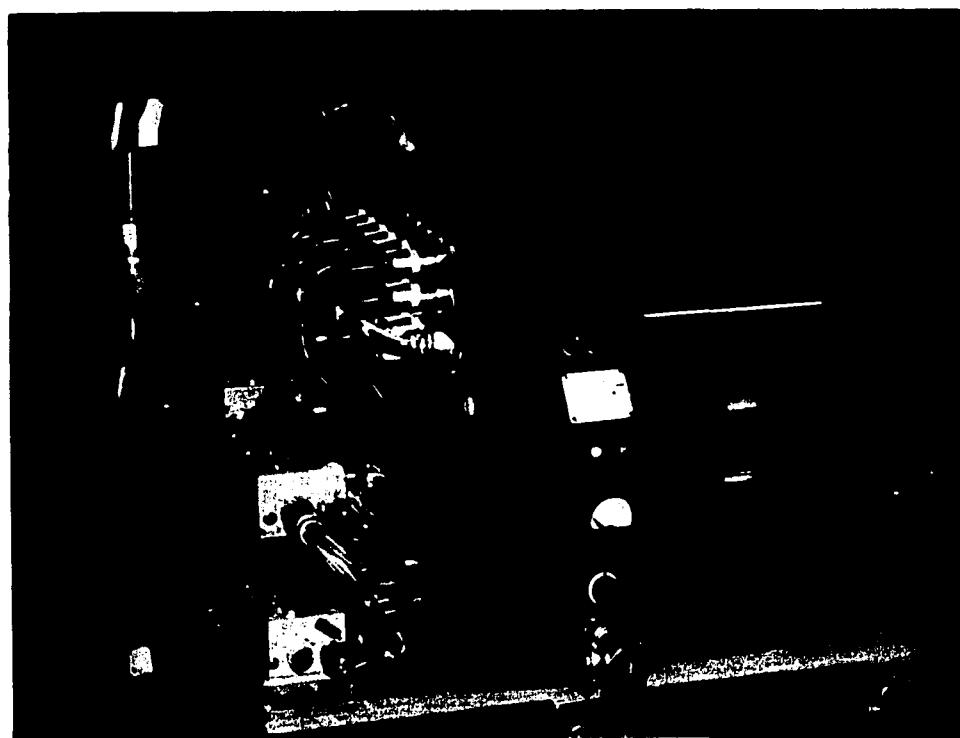


Photo 7. 24-Channel Oscillograph Installed in Aircraft S/N 6615247.

APPENDIX VI. APPROVED HANDLING QUALITIES DEVIATION FROM MIL-H-8501A

1. The model specification states that MIL-H-8501A shall be used as a design guide for the stability and control characteristics for the AH-1G aircraft, except for paragraph 3.6 "Instrument Flight Conditions".
2. The deviations from MIL-H-8501A are presented in the following statements:

Contractor Deviation Number	Model Specification Paragraph Number (ref 13, app I)	Subject
42	3.3.2.1	<u>Cyclic Breakout Force</u>

Requirement: Paragraphs 3.2.4, 3.2.7 and 3.3.11 specifies that the cyclic breakout force shall be not less than 0.5 pounds nor more than 1.5 pounds. Also, the breakout force shall not be greater than the force produced by the trim force gradient in the first inch of stick travel.

Deviation: The breakout force for the pilot cyclic shall be 2.0 ±0.25 pounds.

Reason: The design values of the aircraft cyclic breakout force are such that: (1) to prevent stability augmentation system feedback and (2) cyclic stick flop. The aircraft handling qualities test conducted by ATA pilots have shown that the aircraft performed in accordance with MIL-H-8501 as defined in BHC Specification 209-947-042, Handling Qualities Demonstration.

1	3.3.2.1	<u>Control Characteristics</u>
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Requirement: Specification MIL-H-8501 shall be used as a design guide for the stability and control characteristics for this aircraft, except for paragraph 3.6 (Instrument Flight Conditions).

Deviation: Those requirements of MIL-H-8501, paragraph 3.3 pertaining to control continuity shall not be applicable.

Reason: Aerodynamic discontinuities due to airflow pattern affect tail rotor thrust during some phases of sideward and rearward flight. Increased tail rotor rigging to compensate for the disturbance results in over torque of the tail rotor drive system.

APPENDIX VII. TEST DATA

FIGURE NO. 1
LONGITUDINAL CYCLIC CONTROL FORCES
AH-1G USAF 1970

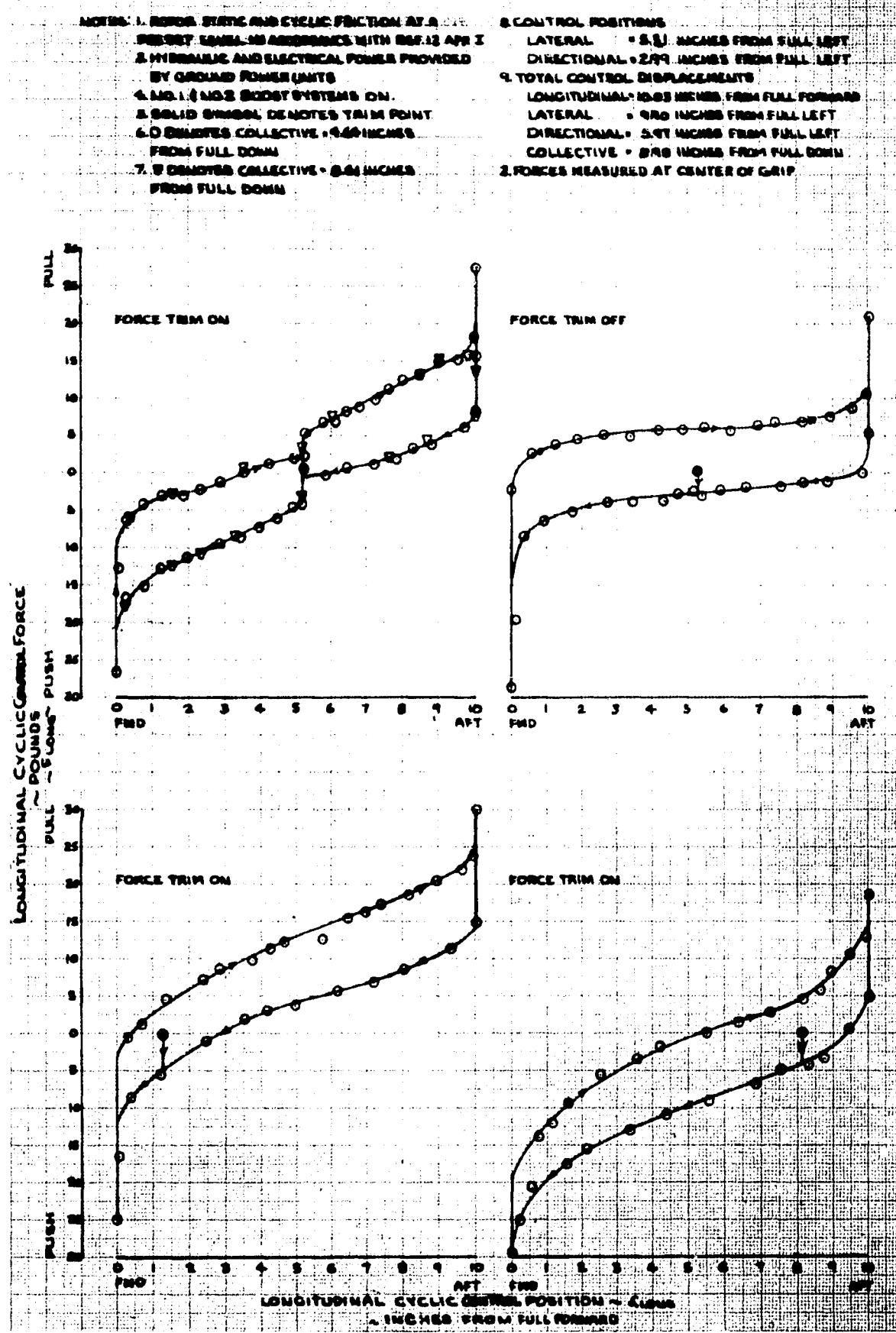


FIGURE NO. 2
LATERAL CYCLIC CONTROL FORCES
AH-1G USAF 25565

NOTES: 1. ROTOR STATIC AND CYCLIC FUNCTION AT A
 PRESET LEVEL IN ACCORDANCE WITH EER 12 APR 1
 3. HYDRAULIC AND ELECTRICAL POWER PROVIDED
 BY GROUND POWER UNITS
 4. NO. 1 & NO. 2 BOOST SYSTEMS ON
 5. SOLID SYMBOLS DENOTE TRIM POINT
 6. O DENOTES COLLECTIVE + 9.61 INCHES
 FROM FULL DOWN
 7. □ DENOTES COLLECTIVE + 8.80 INCHES
 FROM FULL DOWN

8. CONTROL POSITIONS:
 LONGITUDINAL = 4.64 INCHES FROM FULL FWD.
 DIRECTIONAL = 2.99 INCHES FROM FULL LEFT
 9. TOTAL CONTROL DISPLACEMENTS:
 LONGITUDINAL = 10.03 INCHES FROM FULL FWD.
 LATERAL = 9.90 INCHES FROM FULL LEFT
 DIRECTIONAL = 5.91 INCHES FROM FULL LEFT
 COLLECTIVE = 0.88 INCHES FROM FULL DOWN
 10. FORCES MEASURED AT CENTER OF GRIP

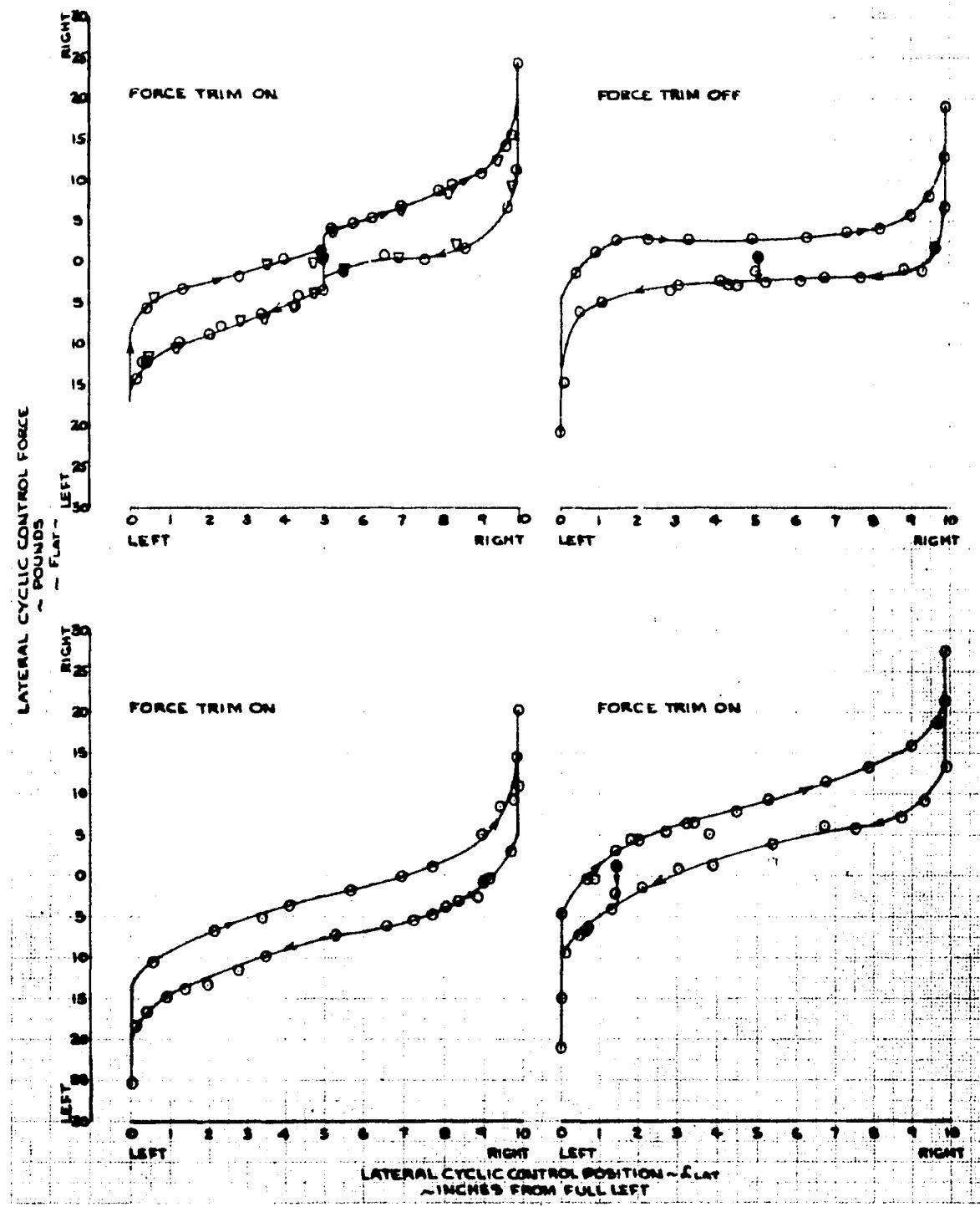


FIGURE NO. 3
DIRECTIONAL CONTROL FORCES
AH-1G USA#715695

NOTES:
 1. MOTOR STATIC AND CYCLIC FRICTION MAYA
 PRE SET LEVEL IN ACCORDANCE WITH REF. 12 APP J
 2. HYDRAULIC AND ELECTRICAL POWER PROVIDED
 BY GROUND POWER UNITS
 3. SOLID SYMBOLS DENOTES TRIM POINT
 4. O DENOTES COLLECTIVE = 4.61 INCHES
 FROM FULL DOWN.
 5. □ DENOTES COLLECTIVE = 8.80 INCHES
 FROM FULL DOWN.

7. CONTROL POSITIONS:
 LONGITUDINAL = 0.66 IN. FROM FULL FWD.
 LATERAL = 5.31 IN. FROM FULL LEFT

8. TOTAL CONTROL DISPLACEMENTS:
 LONGITUDINAL = 10.03 IN. FROM FULL FWD.
 LATERAL = 9.90 IN. FROM FULL LEFT
 DIRECTIONAL = 5.97 IN. FROM FULL LEFT
 COLLECTIVE = 6.9 IN. FROM FULL DOWN

2. FORCES MEASURED AT THE TOP OF THE PEDAL

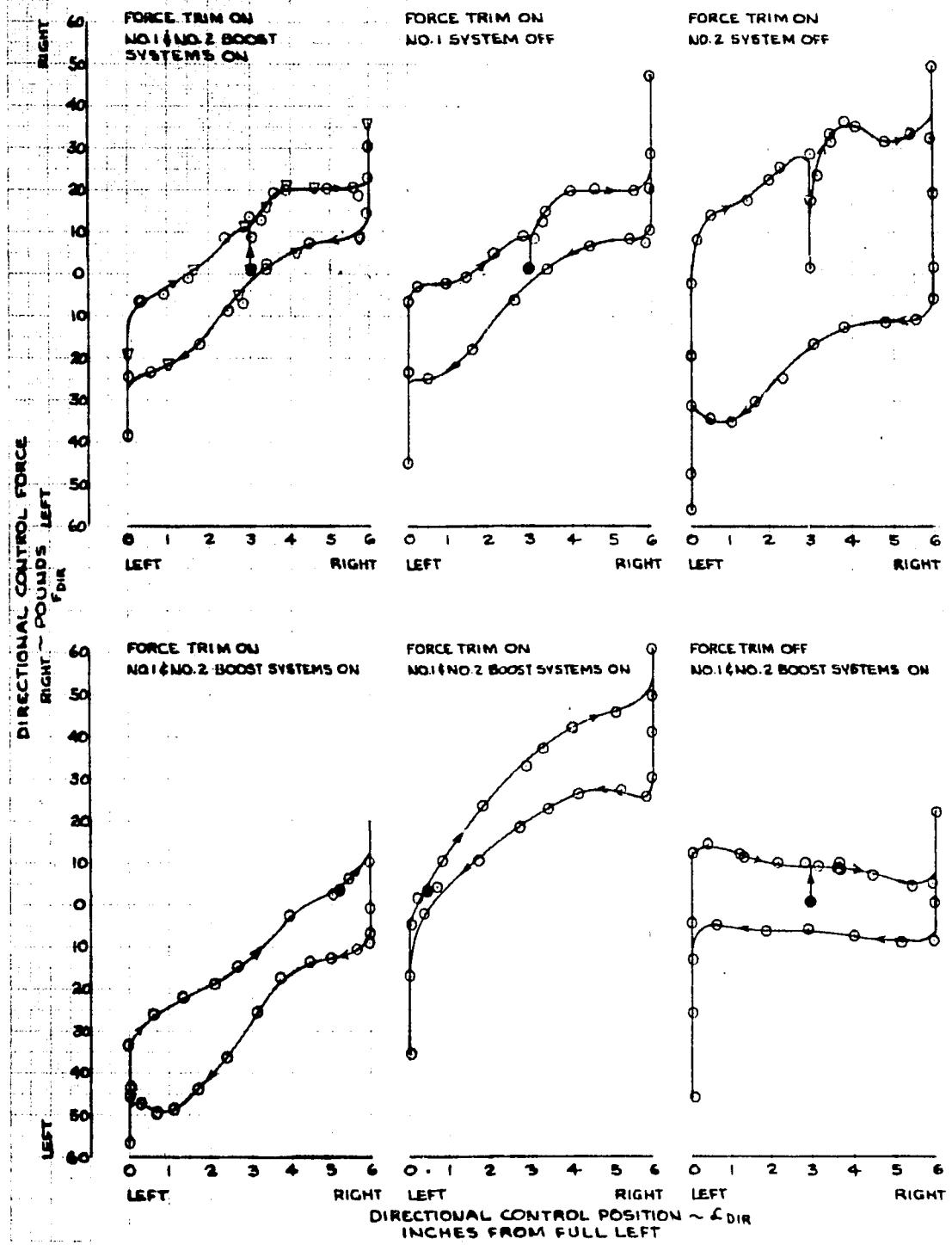


FIGURE NO. 4
CYCLOIC PITCH CONTROL PATTERN
 AH-1G USAF/TIGERS

NOTES: 1. ROTOR STATIC
 2. HYDRAULIC AND ELECTRICAL POWER PROVIDED
 BY GROUND POWER UNITS
 3. NO. 1 & NO. 2 BOOST SYSTEMS ON
 4. 10 DENOTES COLLECTIVE - 9.64 INCHES FROM FULL DOWN
 5. 0 DENOTES COLLECTIVE - 8.50 INCHES FROM FULL DOWN
 6. CONTROL POSITION
 DIRECTIONAL - 2.96 INCHES FROM FULL LEFT
 7. TOTAL CONTROL DISPLACEMENTS:
 LONGITUDINAL - 10.08 INCHES FROM FULL FORWARD
 LATERAL - 9.90 INCHES FROM FULL LEFT
 DIRECTIONAL - 5.97 INCHES FROM FULL LEFT
 COLLECTIVE - 8.98 INCHES FROM FULL DOWN

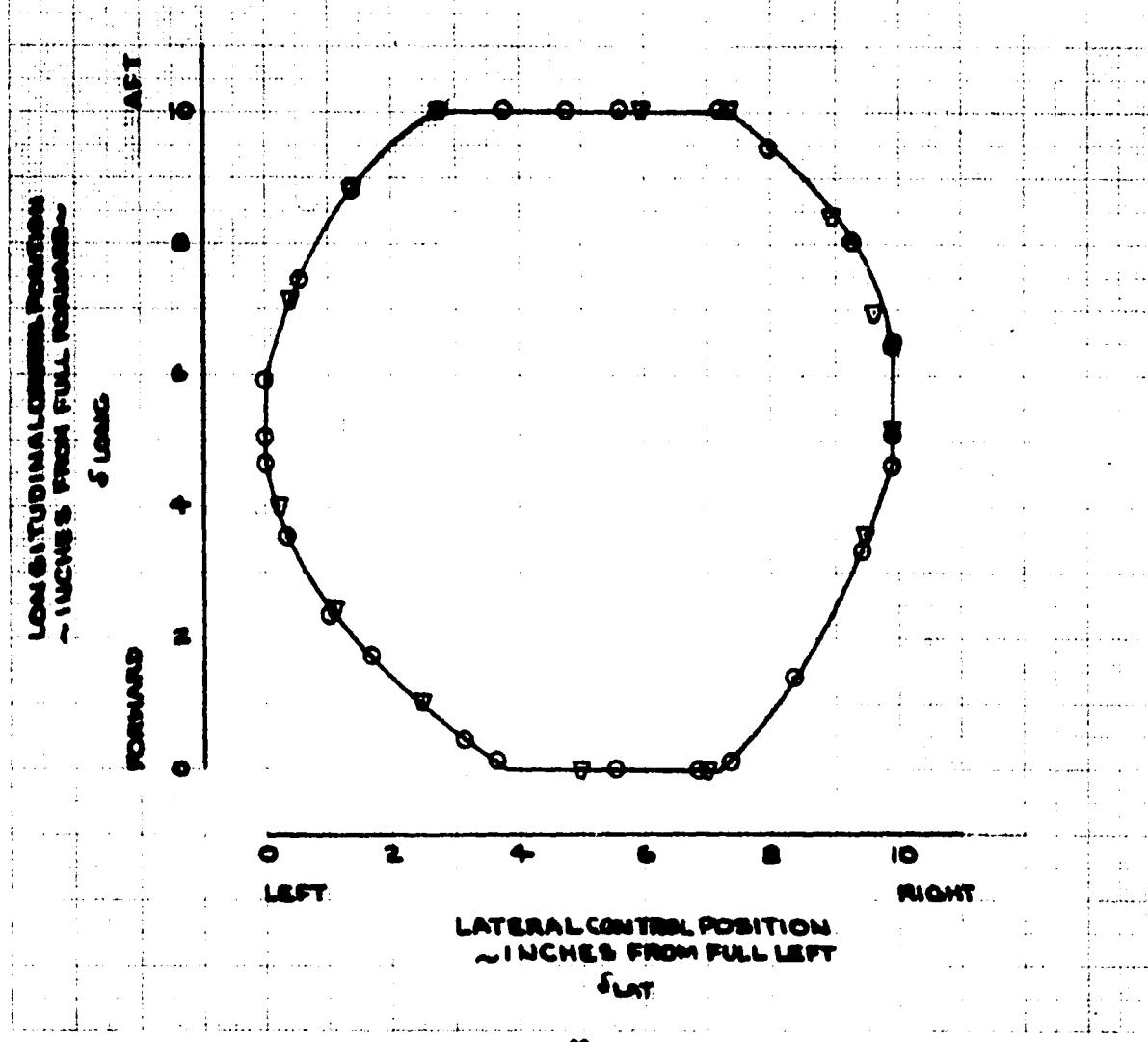


FIGURE No. 5
SUMMARY OF CONTROL POSITIONS IN FORWARD FLIGHT
AM-1G USAF 715693

SYM.	AVE ALT. H ₂ -FT.	AVG. GND ANG. CG-WIN.	AVG. LONG. ROTOR RPM	CONFIG.	FLT. COND.	THRUST COEFF. ~C _T
○	5360	8530	200.0(AFT)	323.5	HVV. HOG LEVEL FLT/DIVE	0.004985
△	6510	8460	200.0(AFT)	324.0	CLEAN	0.004801
□	4440	9580	200.0(AFT)	326.0	HVV. HOG	0.005894
○	4460	8620	191.8(FWD)	329.0	HVV. HOG	0.004961
○	4750	8470	191.4(FWD)	329.0	CLEAN	0.004978
○	3720	8200	200.0(AFT)	324.0	OUTBD ALT.	0.004912
○	4040	8570	201.0(AFT)	324.5	HVV. SCOUT	0.004671
○	3500	9555	200.0(AFT)	324.5	HVV. SCOUT	0.005246
▽	6480	9480	200.0(AFT)	326.0	OUTBD ALT.	0.005650
○	14100	8420	200.9(AFT)	323.0	CLEAN	0.006948
○	14760	8600	200.7(AFT)	323.0	HVV. HOG	0.006775
○	15200	8410	200.4(AFT)	324.0	OUTBD ALT.	0.006383

NOTES: 1. POINTS DERIVED FROM FIGURES 8 THROUGH 20 APPENDIX VIII
 2. POSITIVE LONGITUDINAL STABILITY SIGNIFIES AN INCREASING FORWARD CYCLE REQUIREMENT WITH INCREASING AIRSPEED

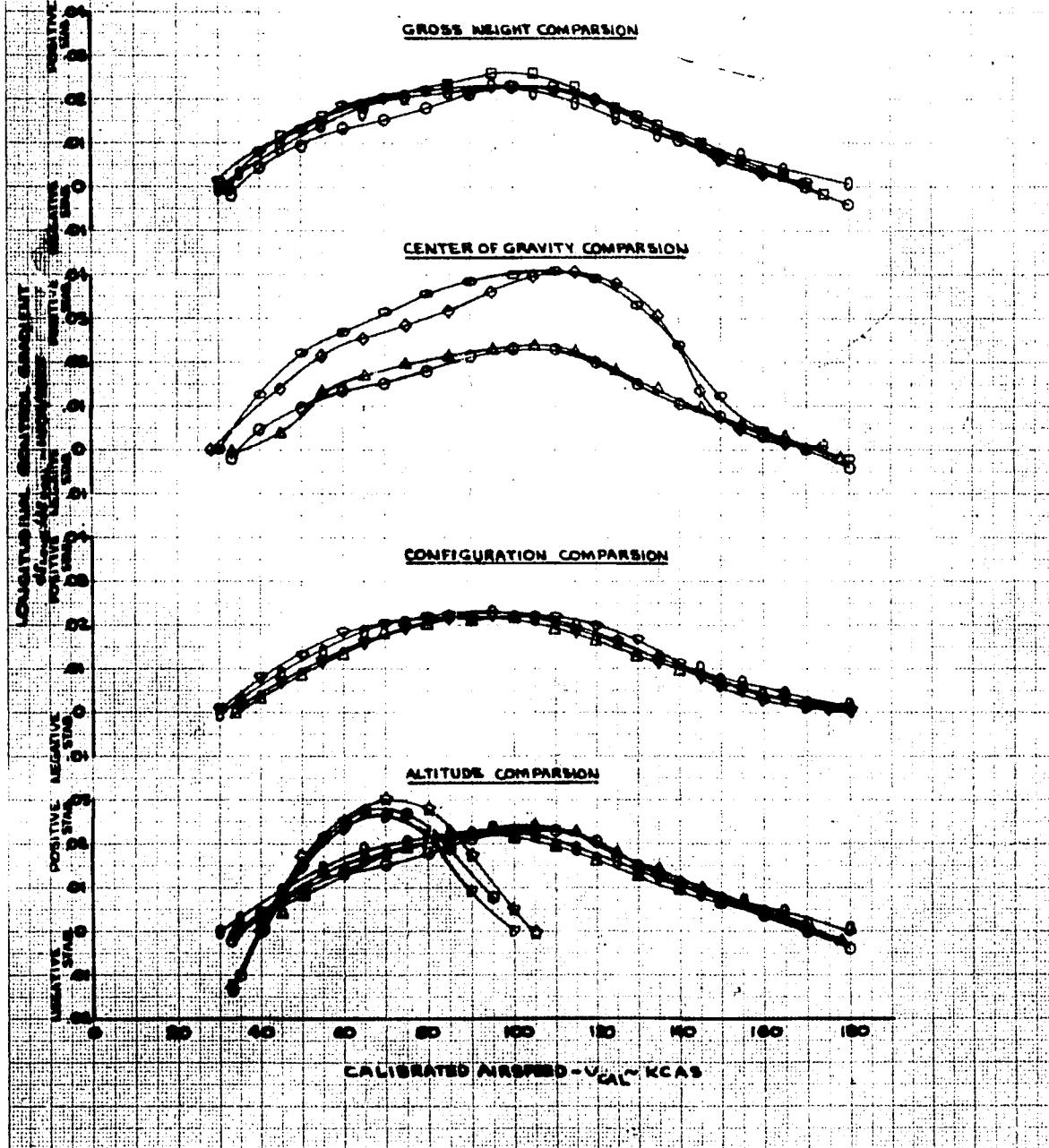


FIGURE NO 6
SUMMARY OF CONTROL POSITIONS IN CLIMB & AUTO ROTATION
AH-1G LIBAS/TIGER

SYN.	AVG. ALT. HO.-FT.	AVG. GENT. -LB.	AVG. LOAD. C.G.-IN.	MOTOR RPM	COMB. FLYING. THRU	CRASH -CT
○	5470	9320	200.2(AFT)	324.0	WV4.MOB	0.005448
△	4450	9240	200.1(AFT)	321.0	AUTO.	0.005121
○	6000	9280	201.0(AFT)	324.0	CLIMB	0.004919
□	5920	9310	201.0(AFT)	322.0	AUTO.	0.005019
△	5650	8350	191.5(FWD)	324.0	CLIMB	0.004908
○	5770	8140	191.5(FWD)	324.0	AUTO.	0.004980
△	6470	8170	201.1(AFT)	323.5	CLEAN	0.004740
○	4450	8170	201.1(AFT)	317.0	AUTO.	0.004910
□	5000	8260	191.2(FWD)	328.0	CLIMB	0.004778
○	5000	8290	191.2(FWD)	329.0	AUTO.	0.004771

NOTES: 1. POINTS DERIVED FROM FIGURES 21 THROUGH 26, APPENDIX III.
2. POSITIVE LONGITUDINAL STABILITY SIGNIFIES AN INCREASING FORWARD CYCLIC REQUIREMENT WITH INCREASING AIRSPEED.

GROSS WEIGHT COMPARISON IN CLIMBING FLIGHT

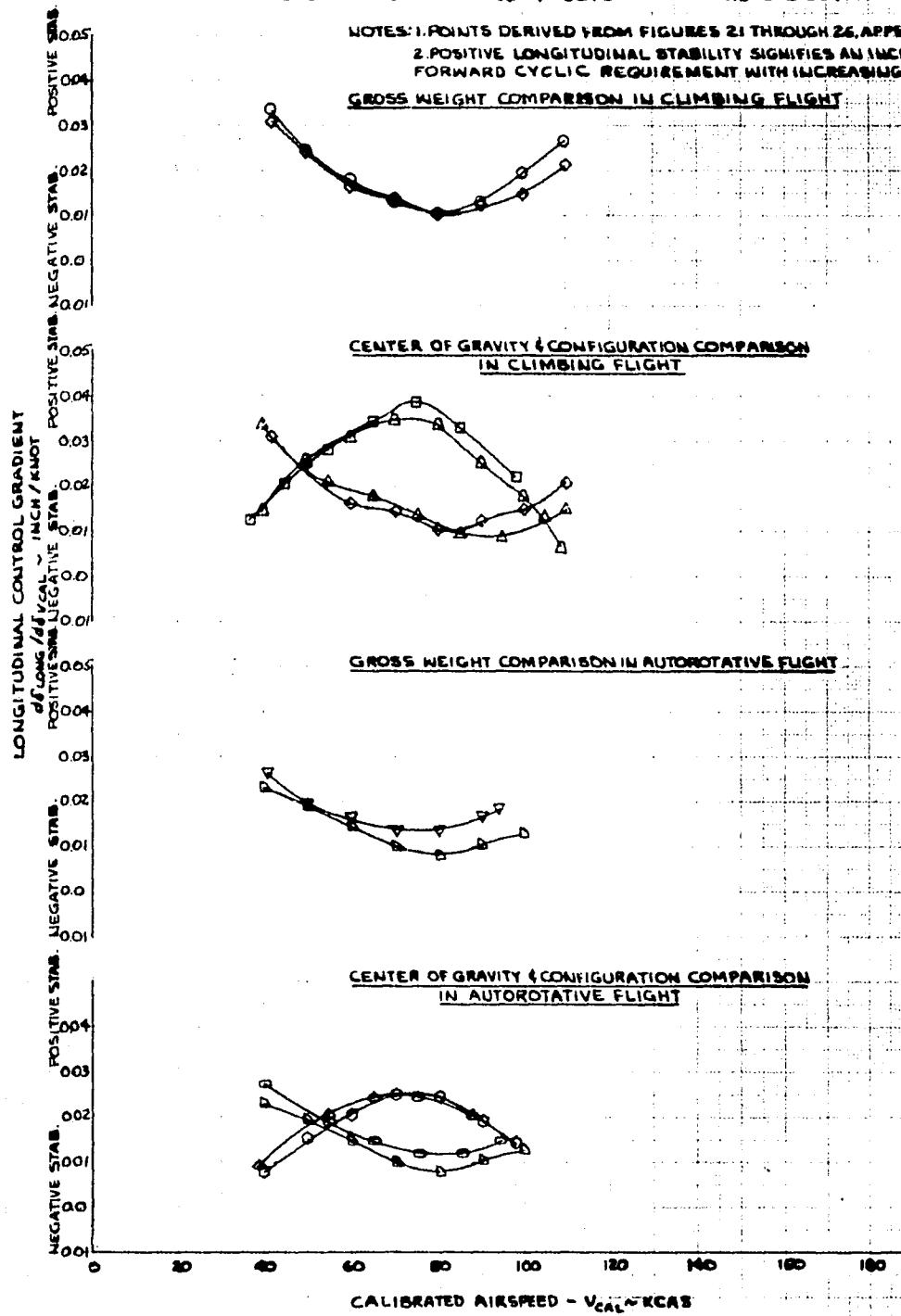


Figure No. 7
SUMMARY OF CONTROL POSITIONS IN FORWARD FLIGHT

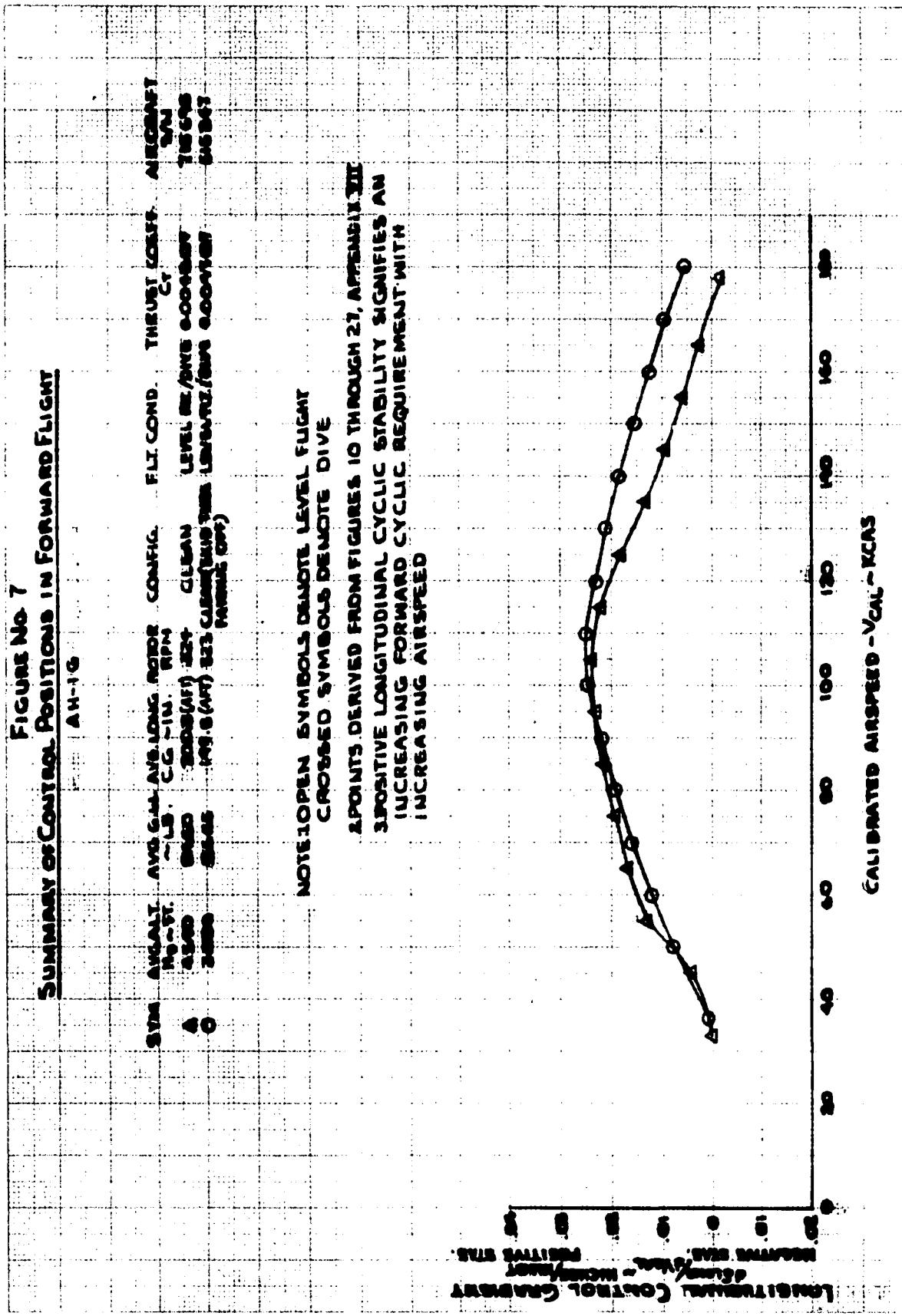


FIGURE NO. 8
STATIC TRIM STABILITY
AM-1G USAF/TIGERS
CLEAN CONFIGURATION

SYM AND ALT.	AVG. G.W. LBS.	Avg. LONG. RPM	THROTTLE POS.	THRUST COEF.	FLT. CRD.
O 6460	7860	190.3 (FWD)	323.5	0.000488	LEVEL FLT.
D 5220	7210	190.2 (FWD)	321.0	0.000481	DIVE

NOTE: 1. KM-90 CHIN TURRET INSTALLED (STOWED POSITION).

2. TOTAL CONTROL DISPLACEMENT:

LONGITUDINAL = 10.08 INCHES FROM FULL FORWARD

LATERAL = 4.90 INCHES FROM FULL LEFT

DIRECTIONAL = 8.97 INCHES FROM FULL LEFT

COLLECTIVE = 6.98 INCHES FROM FULL DOWN

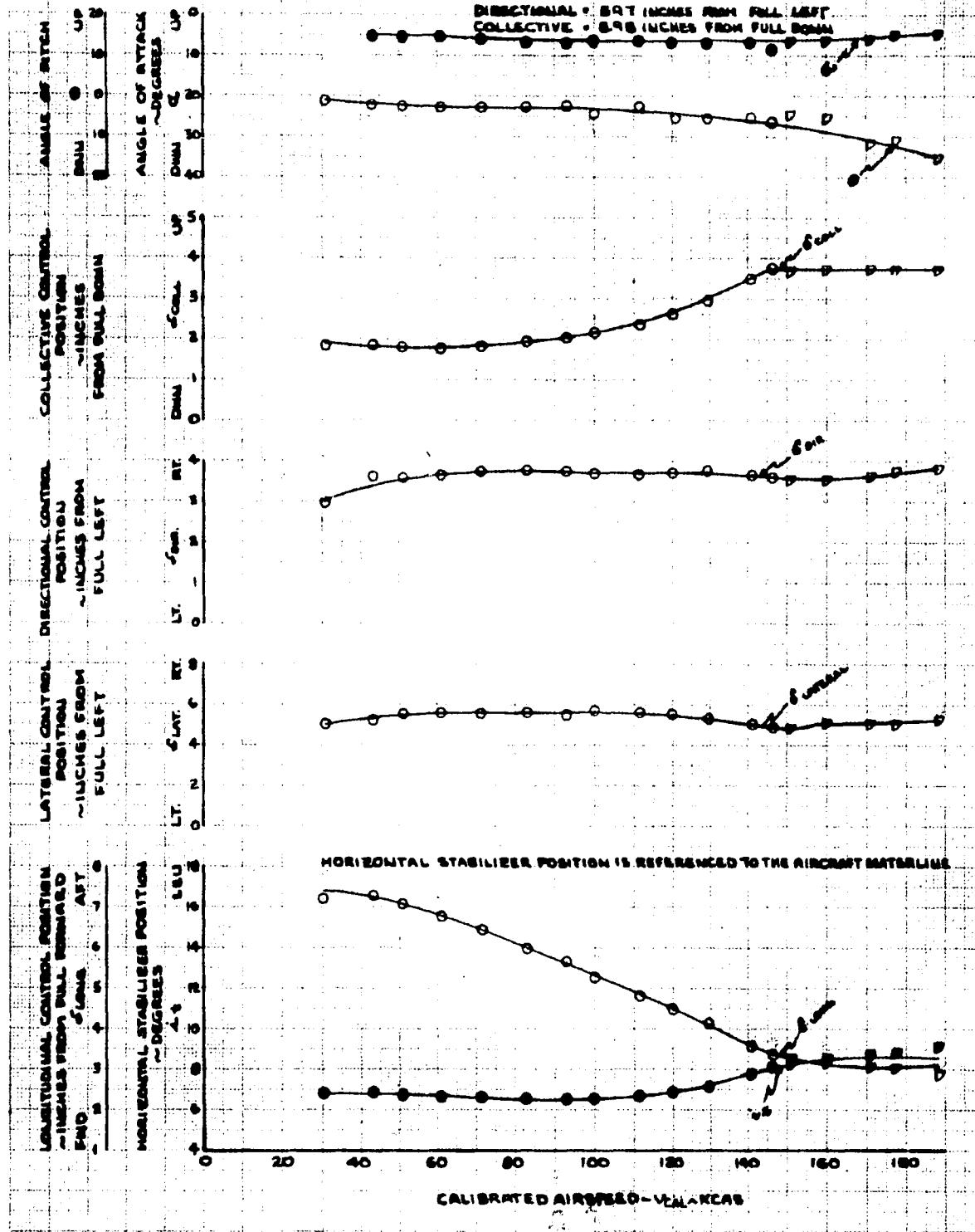


FIGURE NO. 9
STATIC TRIM STABILITY
AM-1G USA 64715695
CLEAN CONFIGURATION

GYM AVERAGE AVG.LONG. MOTOR THRUST COEFF. FLT. COND.
 $H_0 \sim 10000$ ft. ~1.8 C.G. ~1.0 in. RPM ~CT
 4480 8470 101.4 (FWD) 324 0.004818 LEVEL FLT.
 5440 8240 101.3 (FWD) 324 0.004812 DIVE

NOTES: 1. XM-20 CANN TURBET INSTALLED (STOWED POSITION)

2. TOTAL CONTROL DISPLACEMENT

LONGITUDINAL = 100 IN. FROM FULL FORWARD

LATERAL = 19.0 IN. FROM FULL LEFT

DIRECTIONAL = 5.97 IN. FROM FULL LEFT

COLLECTIVE = 8.98 INCHES FROM FULL DOWN

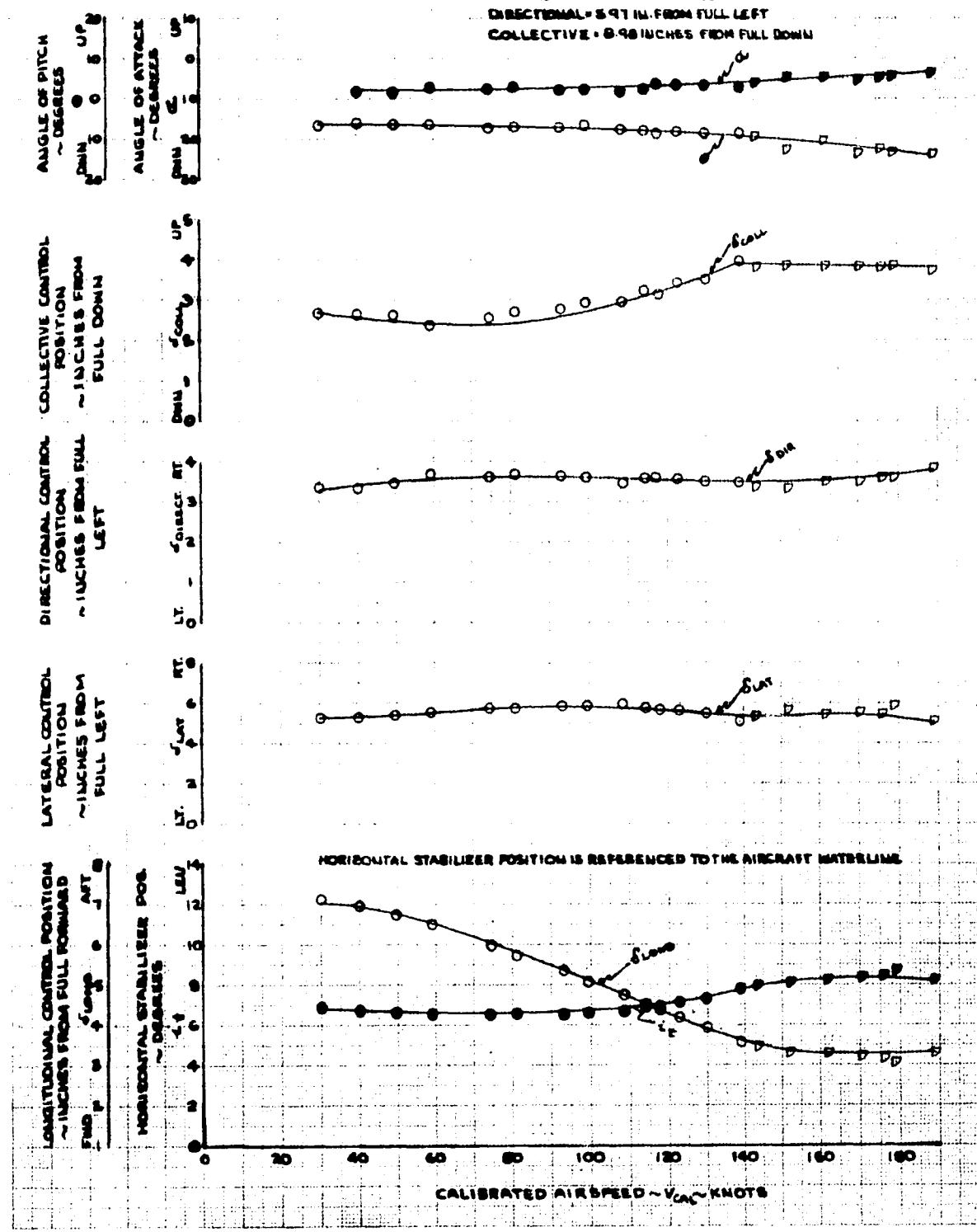


FIGURE NO. 10
STATIC TRIM STABILITY
AH-6 USAUTISER
CLEAN CONFIGURATION

SYM	Avg. Alt.	Avg. GM	Avg. Angle	MOTOR	THRUST GROSS	FLT. COND.
N ₀ -ST	~50	~10	~10	~10	~10	~10
O	4540	6460	2000.0(AFT)	324	0.0004801	LEVEL-FLT.
D	4520	6320	201.0(AFT)	324	0.0004725	SHAKE

NOTES: 1. AH-6B CLEA TAILORING INSTALLED (TRIM POSITION).

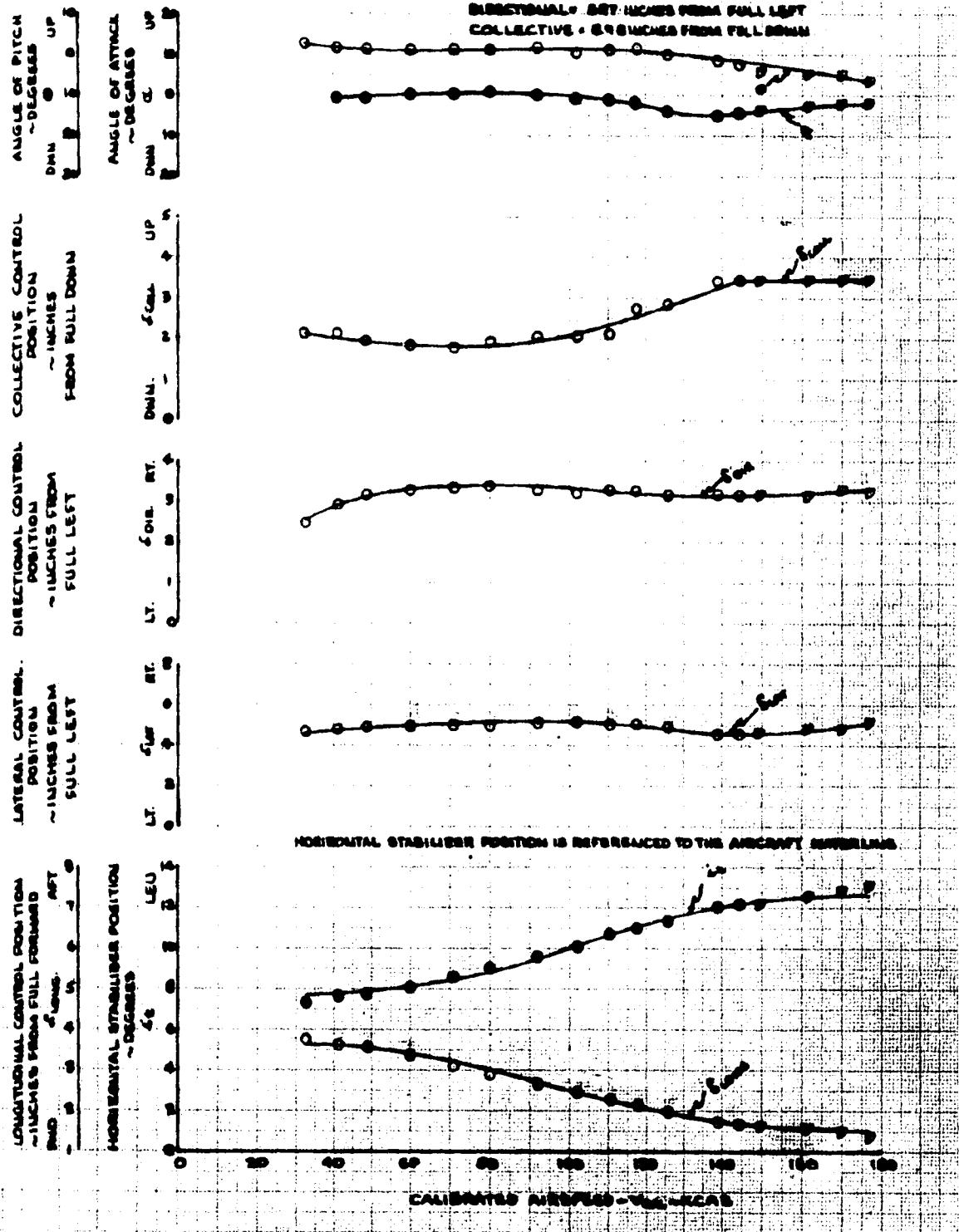
2. TOTAL CONTROL DISPLACEMENT

LONGITUDINAL 10.00 INCHES FROM FULL FORWARD

LATERAL - 1.00 INCHES FROM FULL LEFT

DIRECTIONAL - 0.75 INCHES FROM FULL LEFT

COLLECTIVE - 0.9 INCHES FROM FULL DOWN



HORIZONTAL STABILIZER POSITION IS REFERENCED TO THE AIRCRAFT SURVEY LINE

2

FIGURE NO. 11
STATIC TRIM STABILITY
AH-1S USAF 67-13665
CLEAN CONFIGURATION

DATA: AVG ALT. AVG GLL. AVG. IOD. MOTOR THRUST COEFF. FLT. COND.
HGT-FT. ~10. C.G.-IN. RPM ~CT
O 16100 8420 3000(M) 523.0 0.006448 LEVEL FLT.

MOTOR 1, 1.5M-200 CHM TURBET INSTALLED (STOWED POSITION)

2. TRIM CONTROL DISPLACEMENT
LONGITUDINAL: 10.08 INCHES FROM FULL FORWARD
LATERAL: +9.90 INCHES FROM FULL LEFT
DIRECTIONAL: +8.97 INCHES FROM FULL LEFT
COLLECTIVE: +8.98 INCHES FROM FULL DOWN

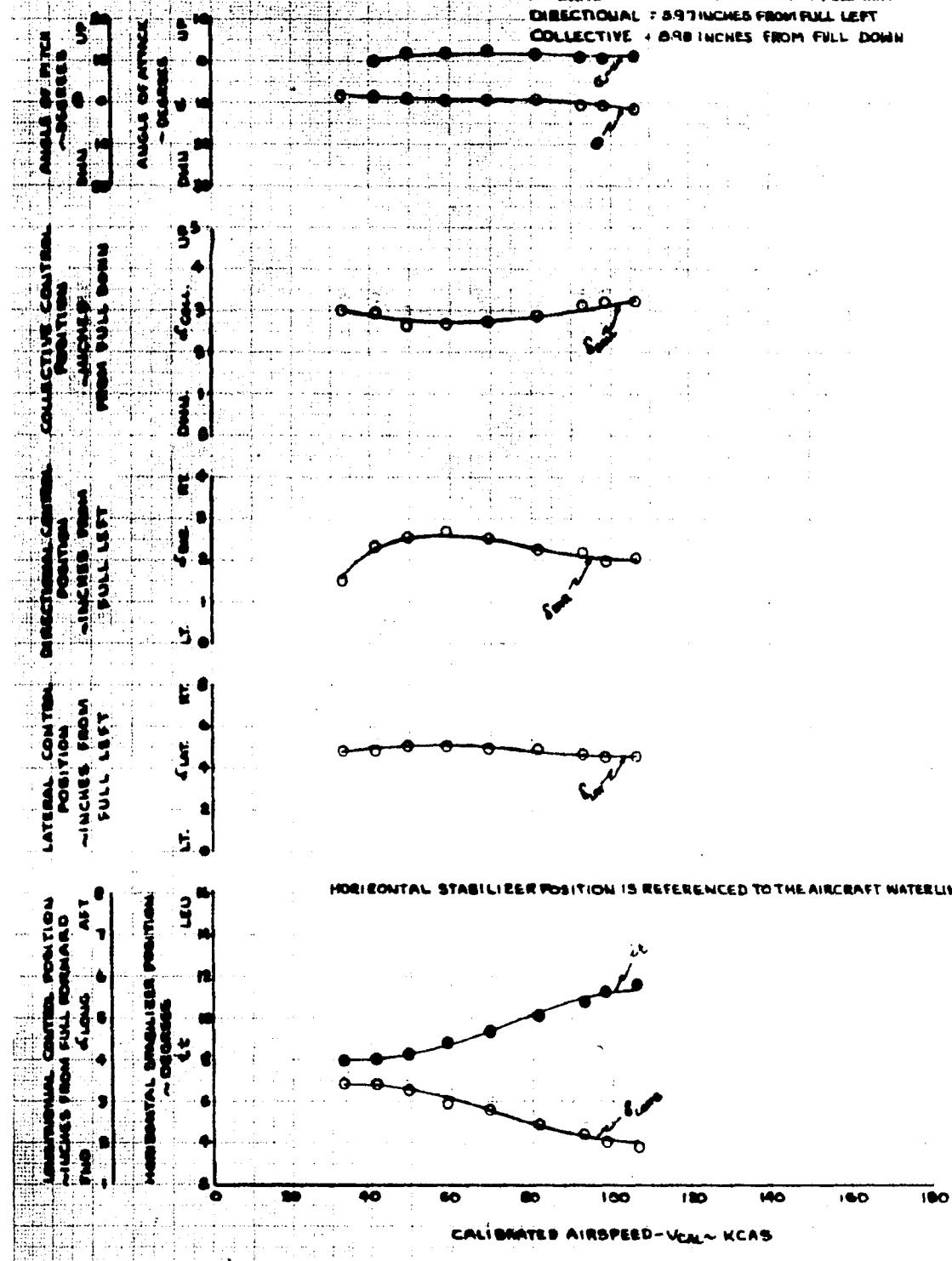


FIGURE NO. 12
STATIC TRIM STABILITY
AN-100 URGENTUS
CUT 80 ALTERNATE CONFIGURATION: WING SPOILERS REMOVED.

SYM	ANGLE AFT	ANGLE LATERAL	ANGLE LONG.	ROTATE	THROTTLE CRANK	FL. GEAR
H-100	-1.0	0.0	0.0	0.0	0.0	0.0
O	BT80	0.000	0.001 (APT)	0.000	0.000712	LEVEL FLT
U	GO80	0.050	0.001 (APT)	0.035	0.000607	DIVE

NOTES: 1. AN-100 CHIN TURBINE INSTALLED (STRAIGHT POSITION)

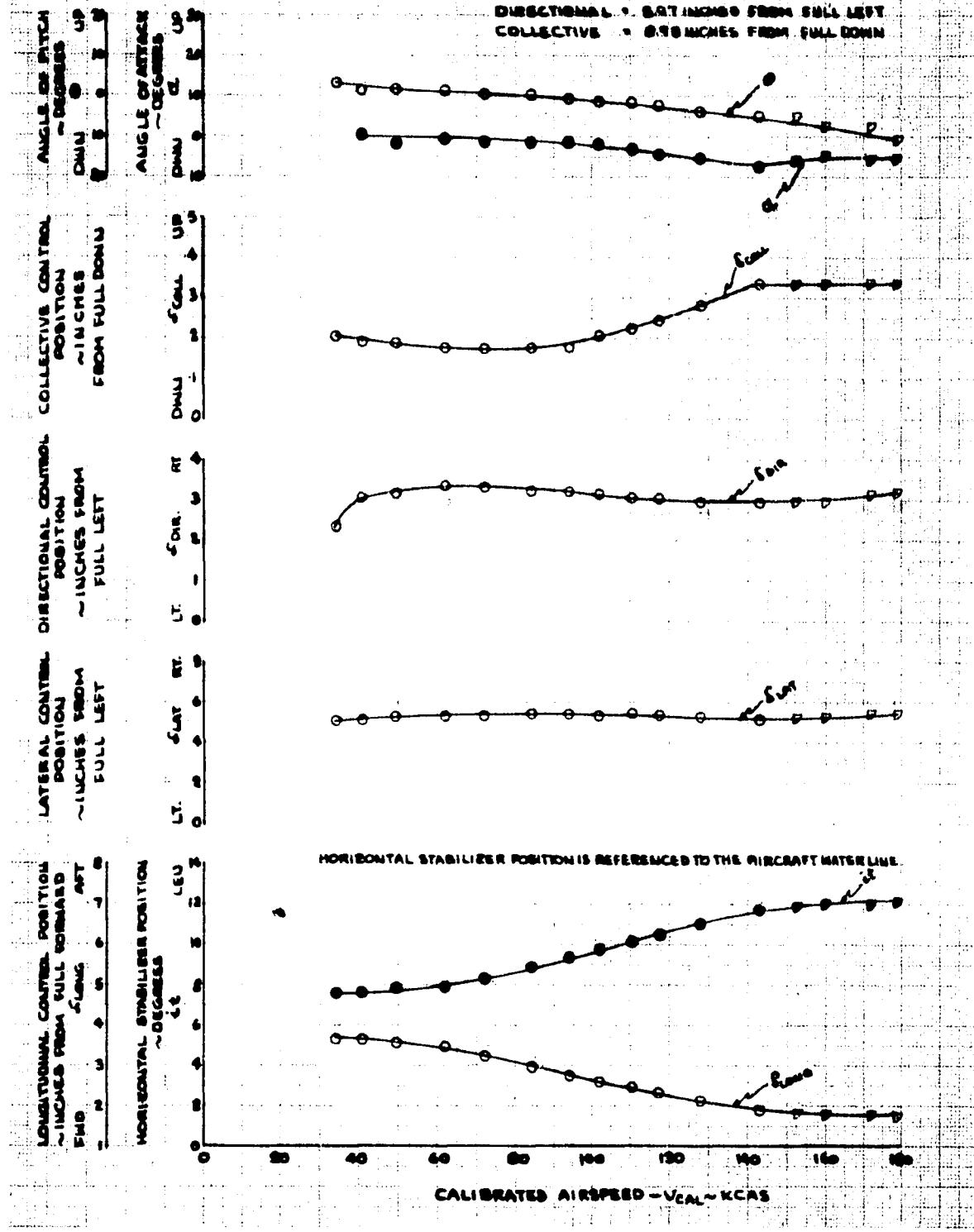
2. TOTAL CONTROL DISPLACEMENT

LONGITUDINAL .100 INCHES FROM FULL FORWARD

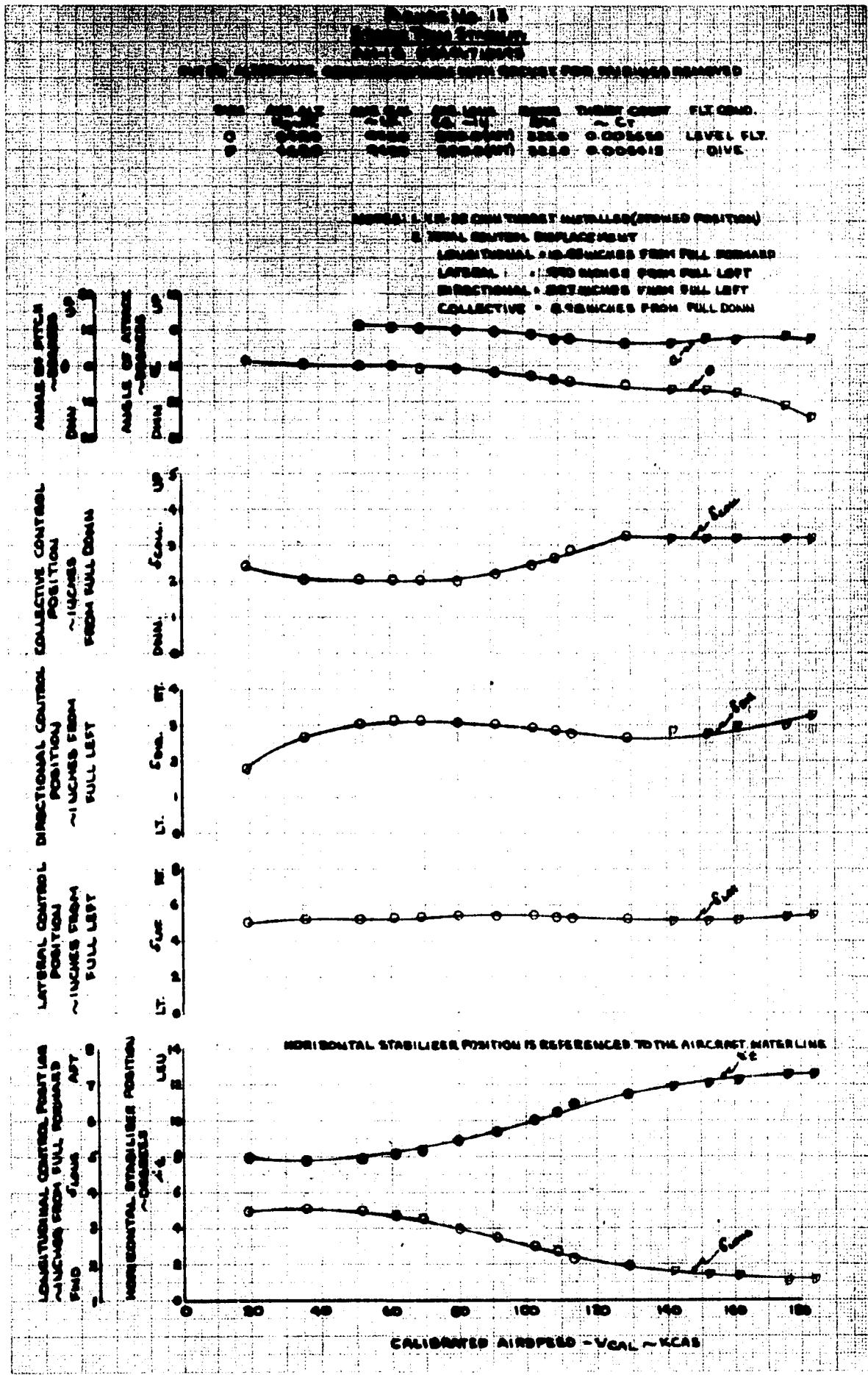
LATERAL .90 INCHES FROM FULL LEFT

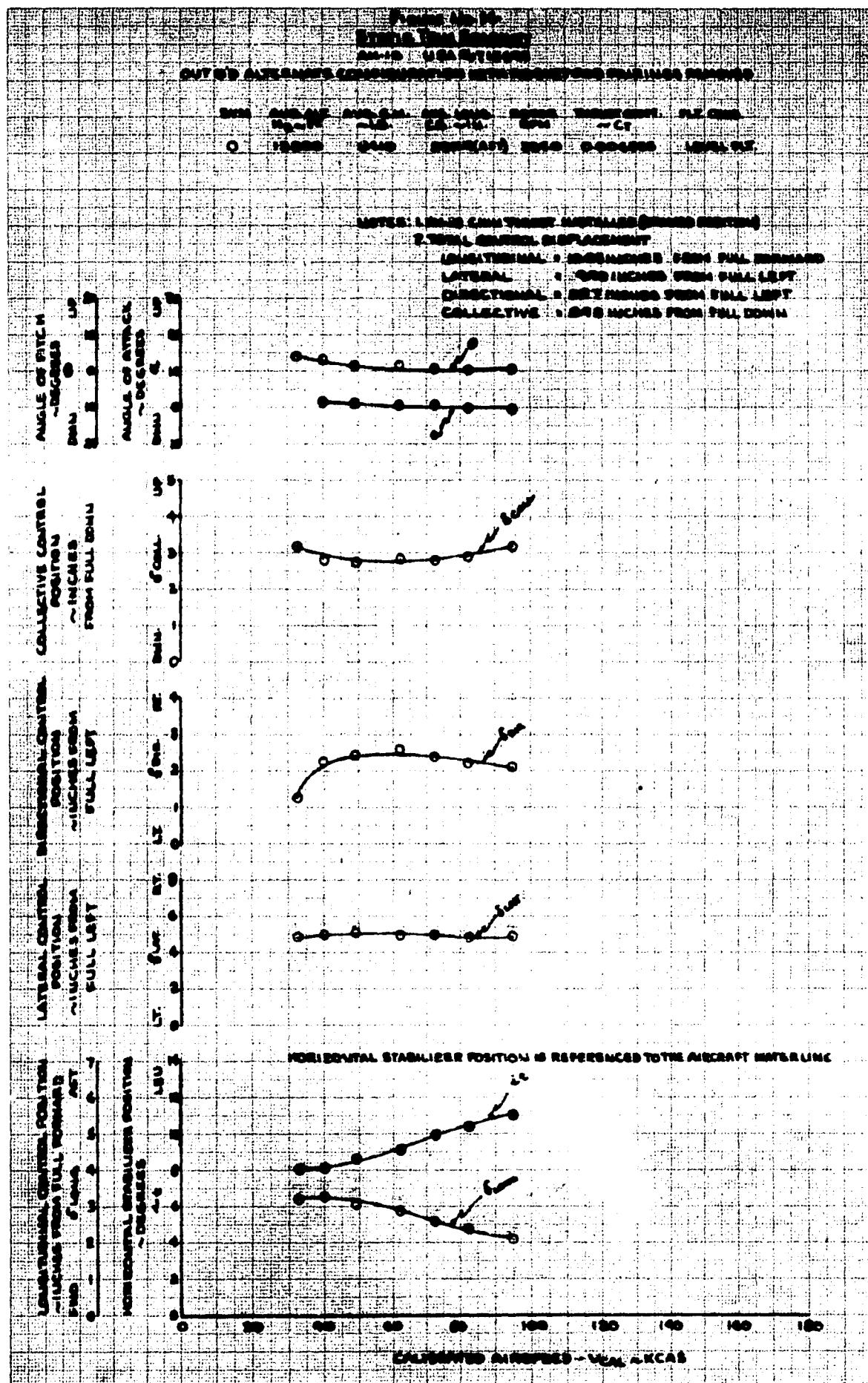
DIRECTIONAL .90 INCHES FROM FULL LEFT

COLLECTIVE .050 INCHES FROM FULL DOWN



CALIBRATED AIRSPEED - V_{CAL} - KCAS





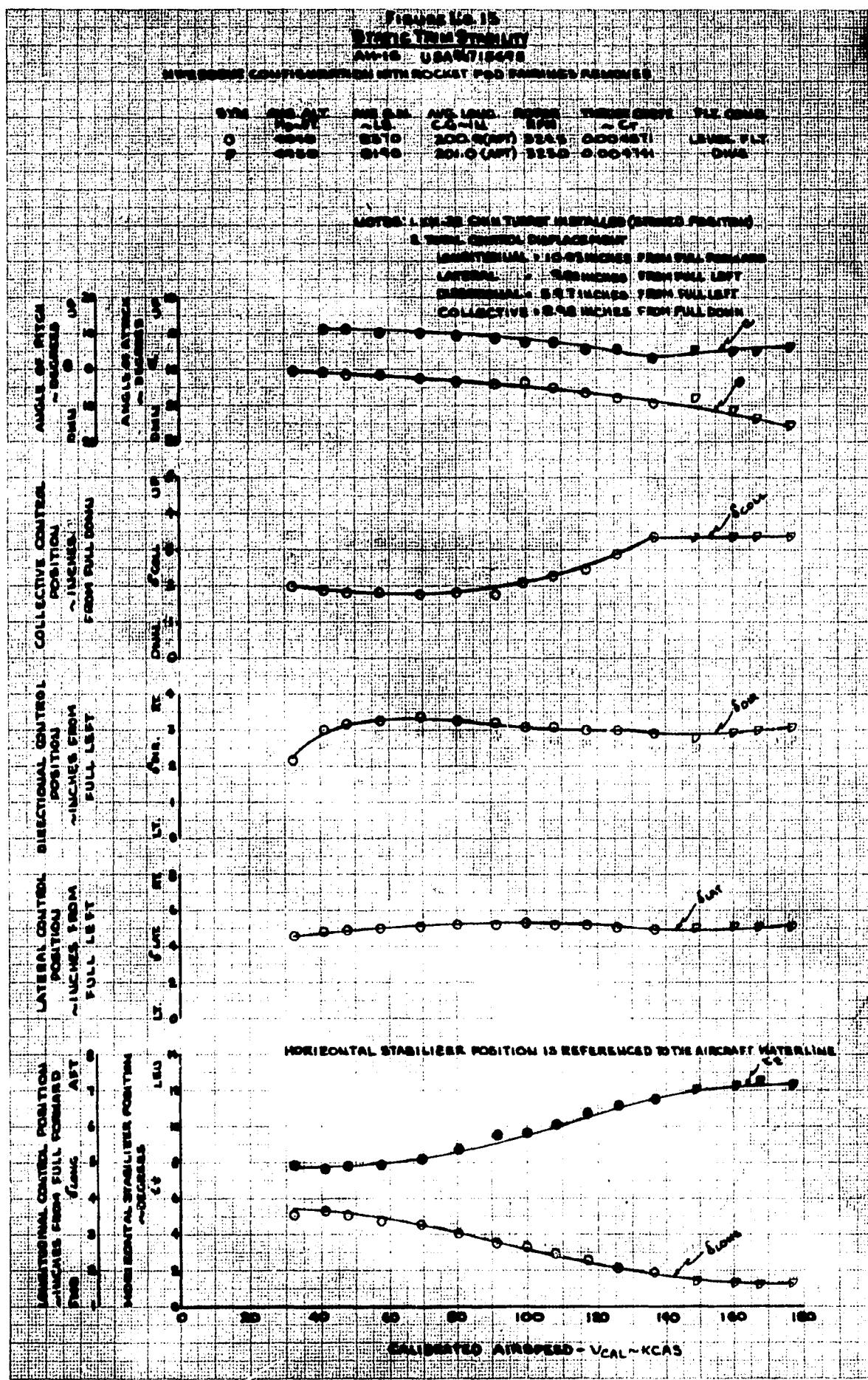


FIGURE NO 16
STATIC TRIM STABILITY
AM-1G USAF AIRCRAFT
HVV SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

STATE	AVG ALT. IN FT.	AVG S. I. IN FT.	AVG LOAD. IN FT	ROT. THRUST COEF.	FLT. QMD.
0	3500	4355	200.0 (FT)	0.245	0.005246
0	5260	4355	200.1 (FT)	0.240	0.005461

NOTES: 1. XM-20 CHIN TURRET (INSTALLED/ARMED POSITION)

2. TOTAL CONTROL DISPLACEMENT

LONGITUDINAL = 10.0 INCHES FROM FULL FORWARD

LATERAL = 6.90 INCHES FROM FULL LEFT

DIRECTIONAL = 8.47 INCHES FROM FULL LEFT

COLLECTIVE = 0.18 INCHES FROM FULL DOWN

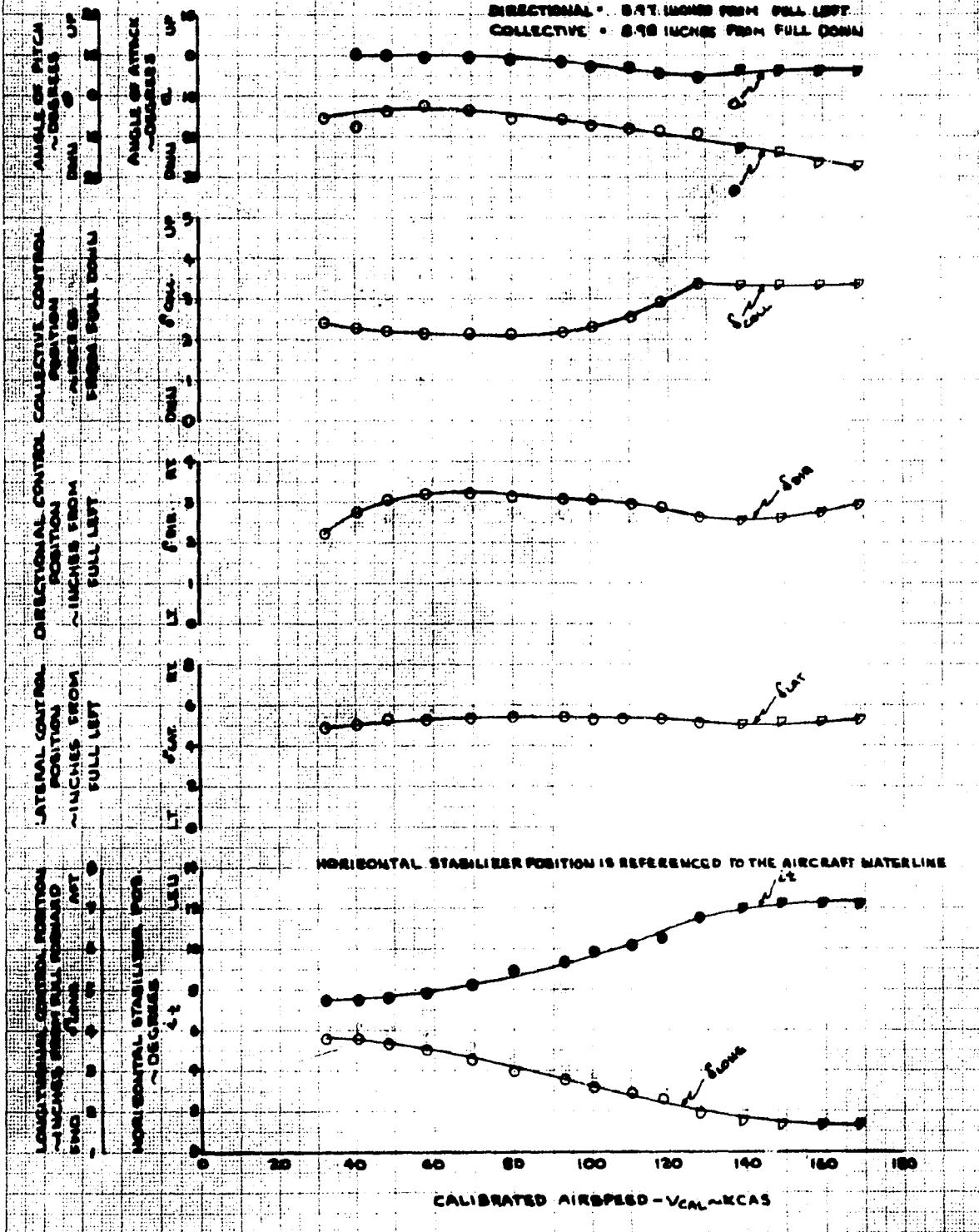


FIGURE No. 17
 STATIC TRIM STABILITY
 AH-1G USAF 6715678
 HUV. HOG CONFIGURATION WITH ROCKET POD RACKINGS REMOVED

SYM AVE. ALT. AVE. GAN. AVE. LONG. ROTOR THRUST COEFF. FLT. COND.
 $M_0 = 1.1$ ~10 CG ~14 RPM ~CT
 O .4960 .6620 191.6(FWD) 324.0 0.004961 LEVEL FLT.
 P .6760 .6620 191.6(FWD) 323.6 0.004961 IN DIVE

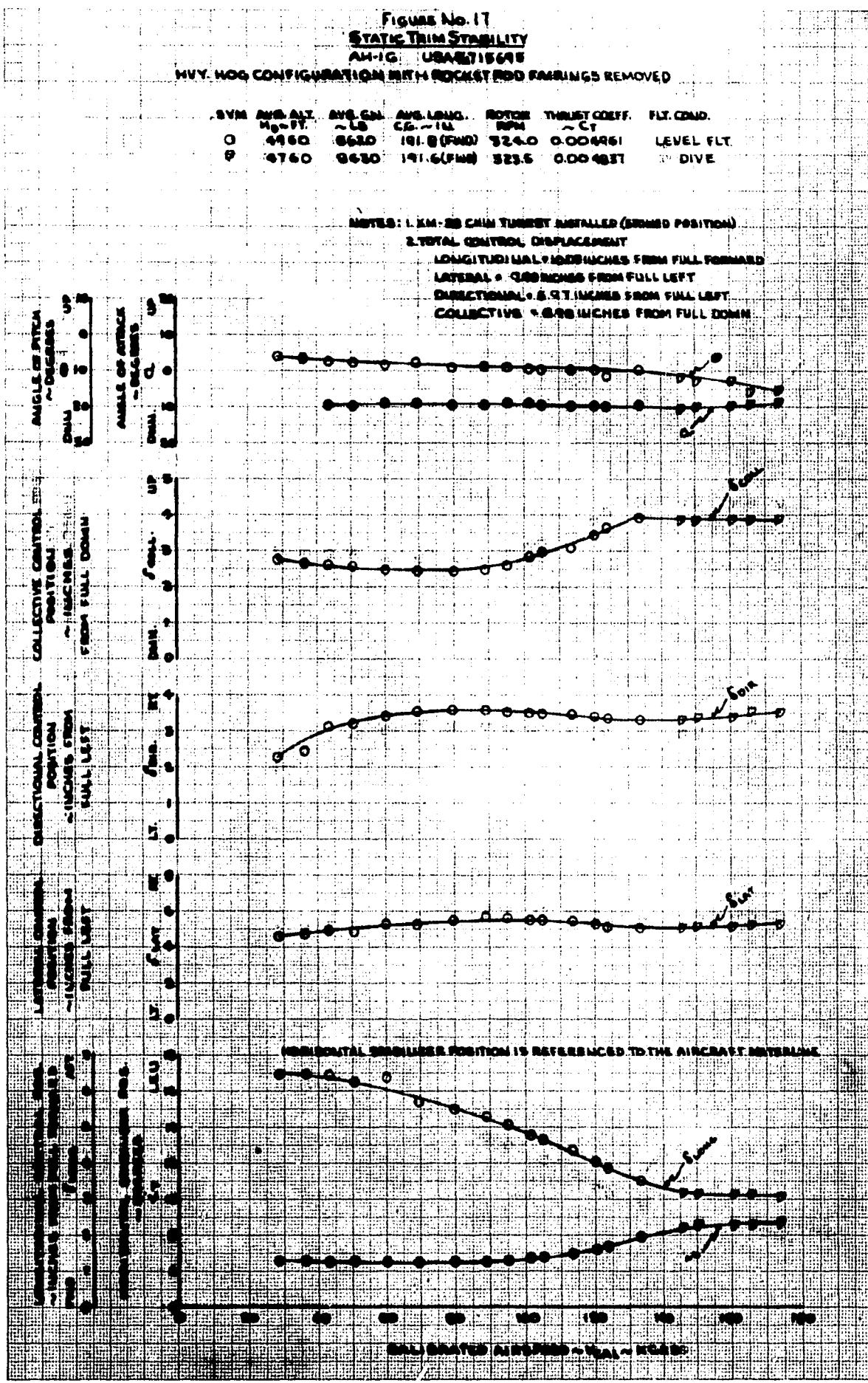
NOTES: 1. KM-30 CANNON TURRET INSTALLED (ARMED POSITION)

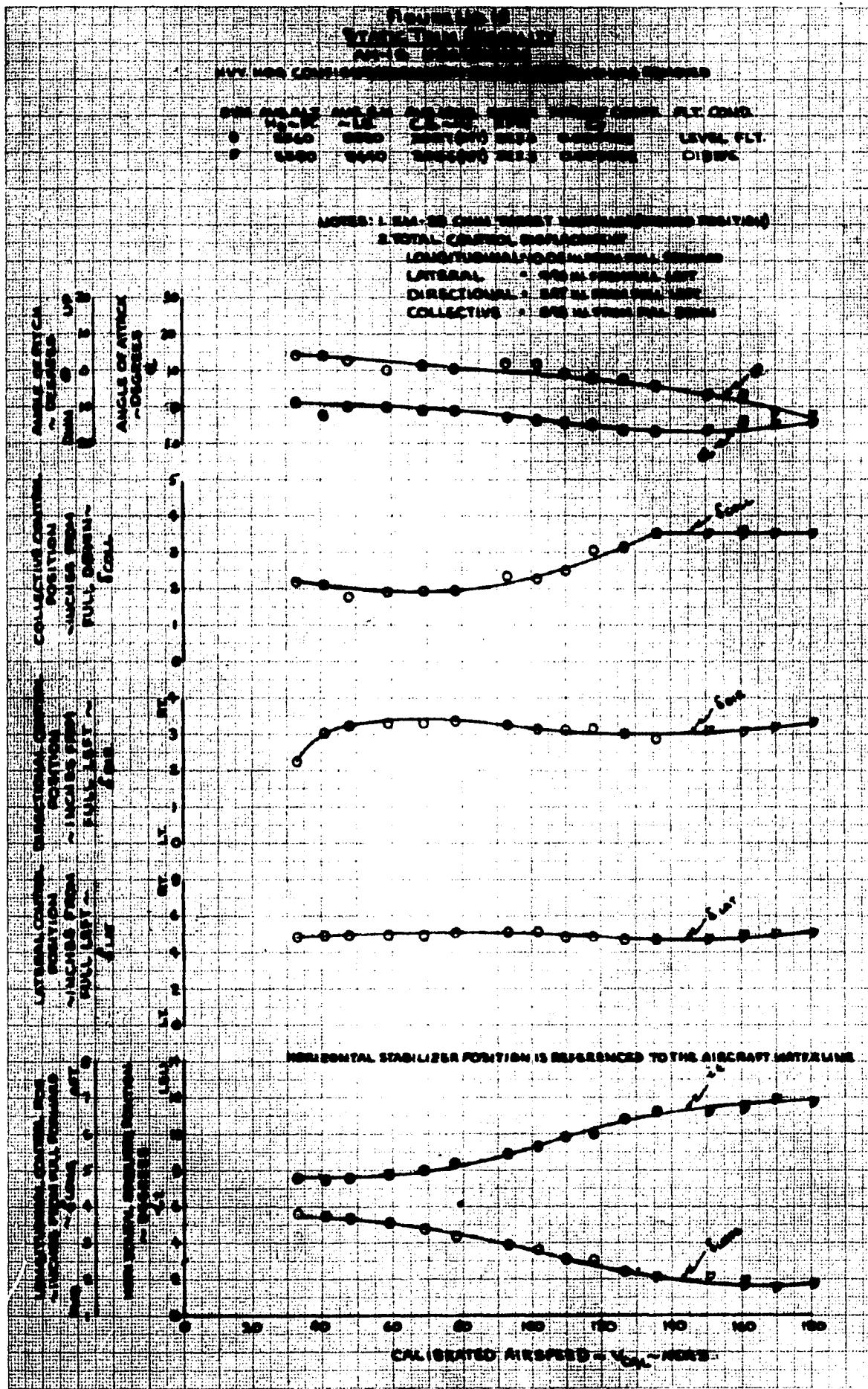
2. TOTAL CONTROL DISPLACEMENT

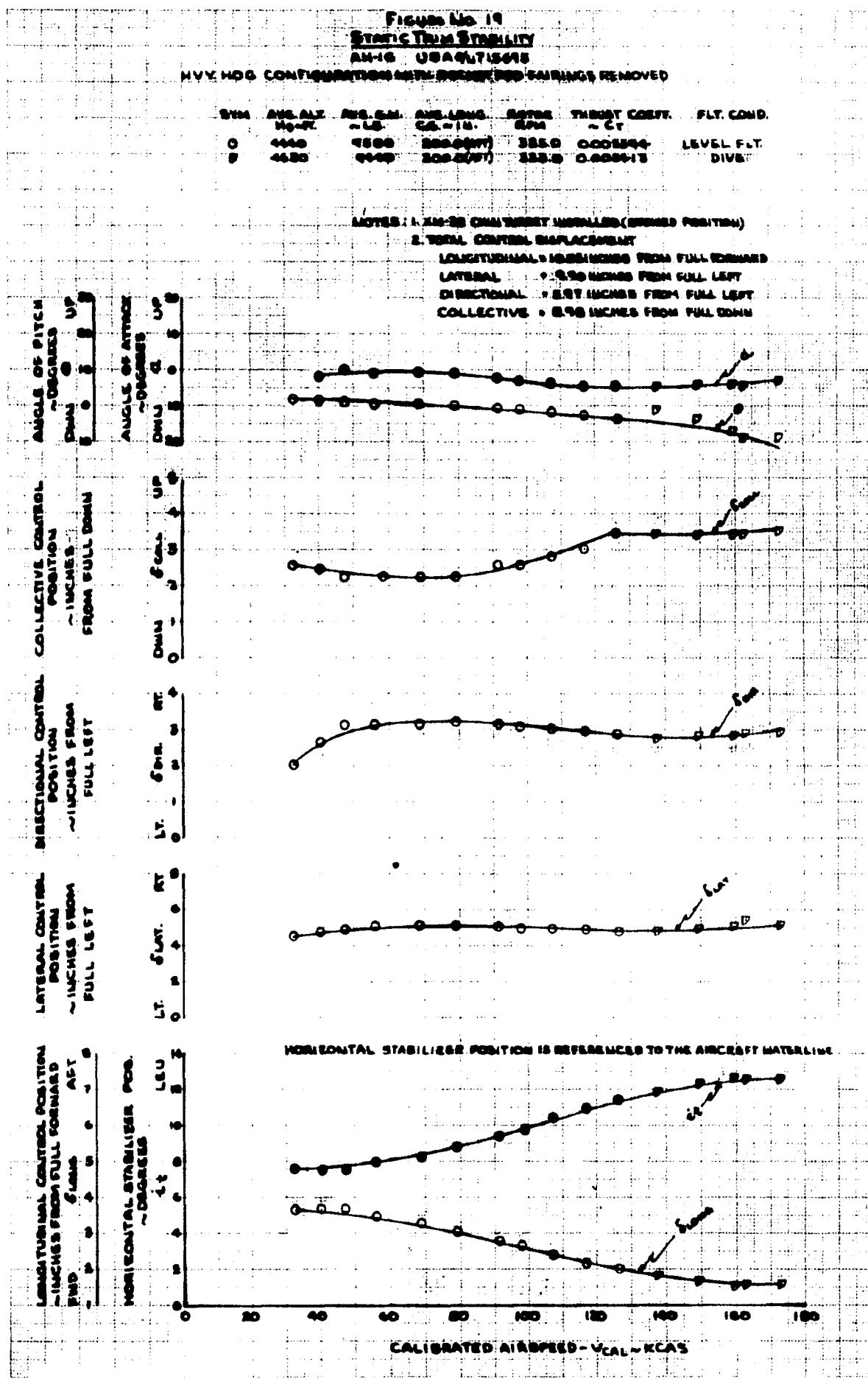
LATERAL = 1.00 INCHES FROM FULL FORWARD

DIRECTIONAL = 0.50 INCHES FROM FULL LEFT

COLLECTIVE = 0.50 INCHES FROM FULL DOWN







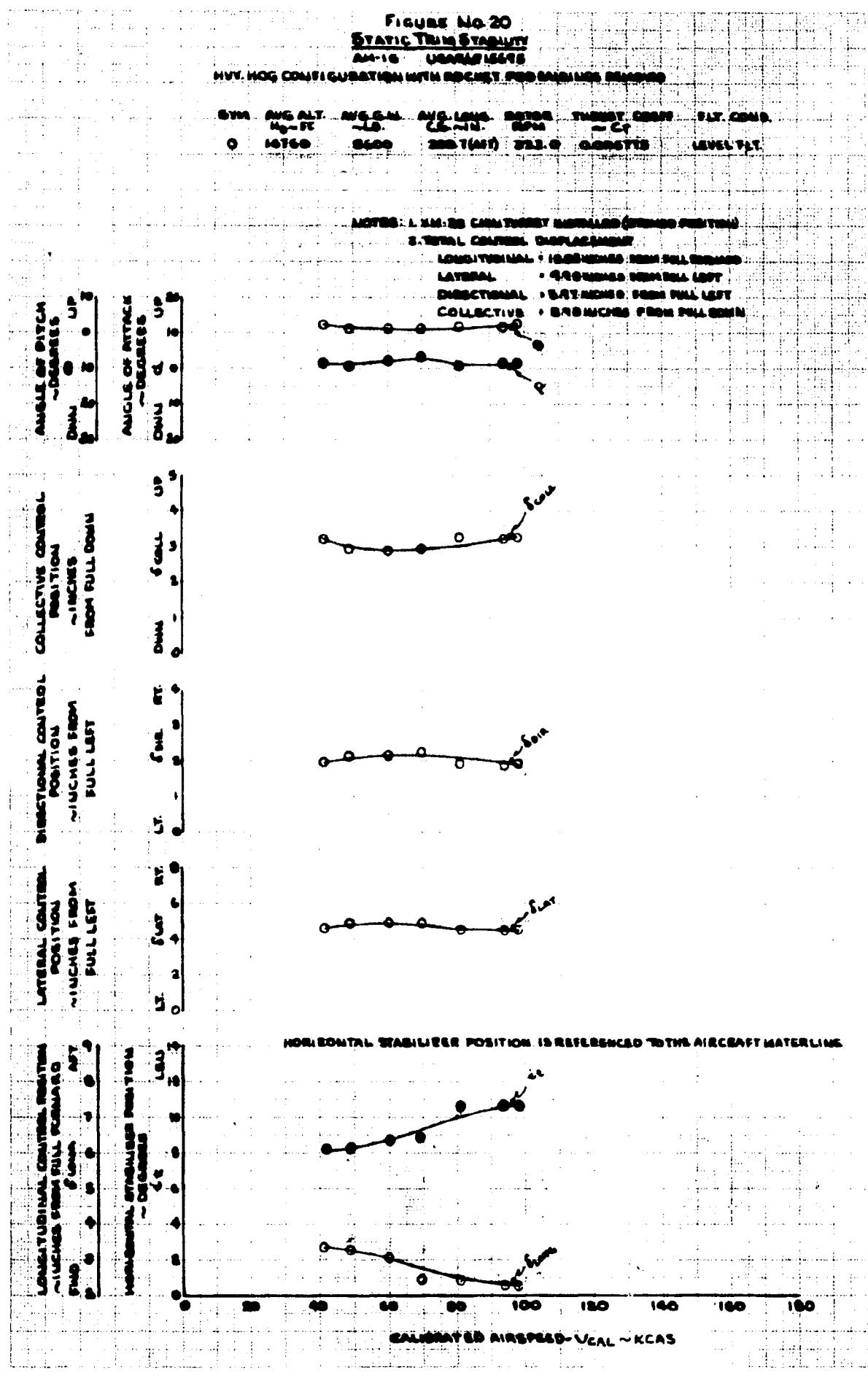


FIGURE UG-21
STATIC TRIM STABILITY
 AH-1G USAFT 15698
 CLEAN CONFIGURATION

STM AVG ALT. 14000 FT. AVG LONG. ROTOR THRUST CREST. FLT. COND.
 $H_0 = 14000$ FT. CG = 1M. RPM = 51% CLIMB
 ▲ 6850 6790 190.0 (FW) 323.0 0.004288 AUTOROTATION
 □ 6660 7040 190.1 (FW) 321.0 0.004378

NOTES: 1. XM-20 CHIN TURRET INSTALLED (STOWED POSITION)
 2. TOTAL CONTROL DISPLACEMENT
 LONGITUDINAL = 10.5 INCHES FROM FULL FORWARD
 LATERAL = 5.5 INCHES FROM FULL LEFT
 DIRECTIONAL = 5.5 INCHES FROM FULL LEFT
 COLLECTIVE = 6.0 INCHES FROM FULL DOWN

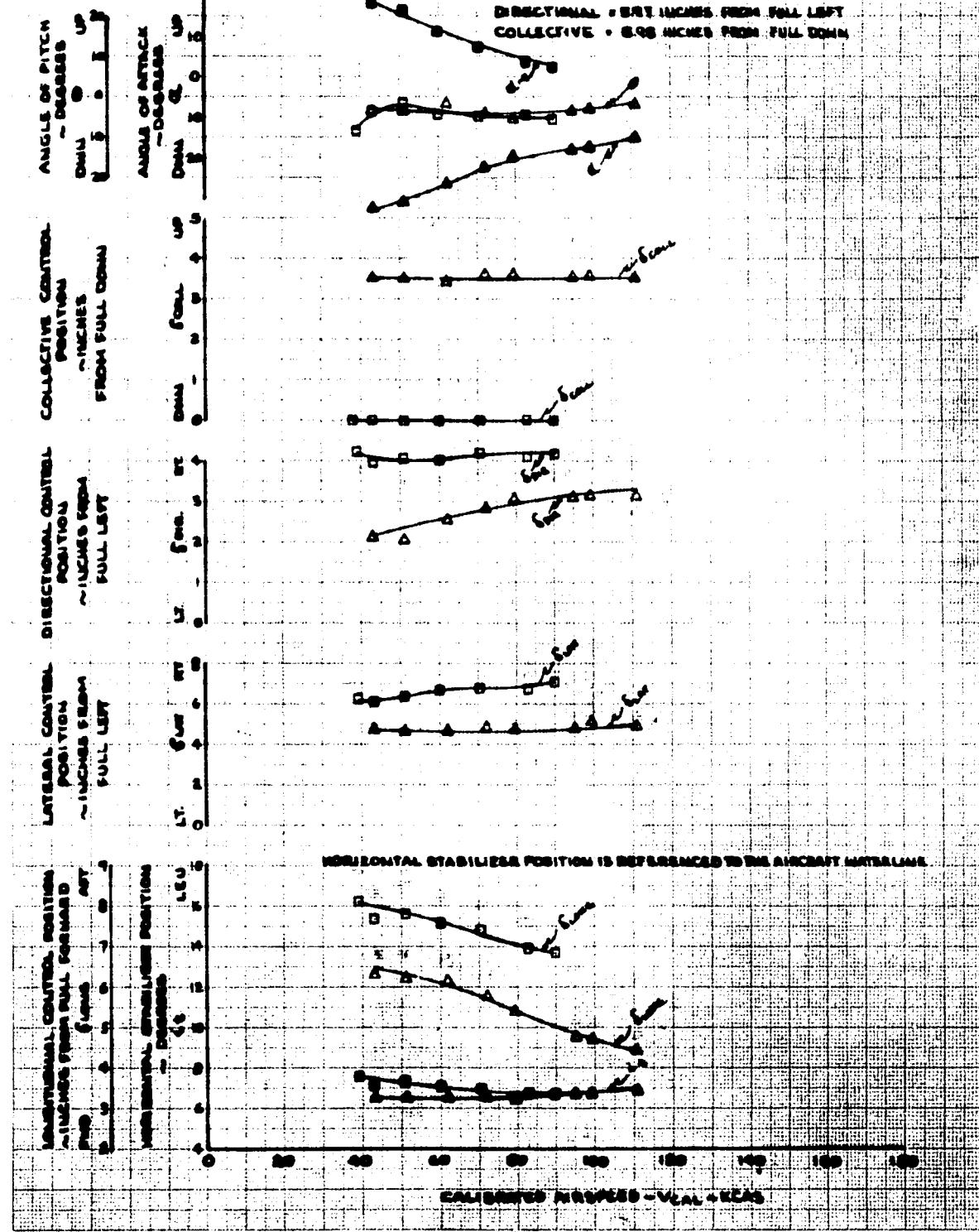


FIGURE NO 22
STATIC TRIM STABILITY
AH-1G USA 66715645
CLEAN CONFIGURATION

SYN	Avg Alt. ft.	Avg G.W. lb.	Avg Long. C.G. ~ in.	MOTOR RPM	THRUST COEF.	FLT. COND.
▲	8200	820	1911 (FWD)	323.0	0.004118	CLIMB
●	8200	820	1912 (FWD)	324.0	0.004117	AUTOROTATION

NOTE: 1. KMA-20 CHM THRUST INSTALLED (STIMED POSITION)

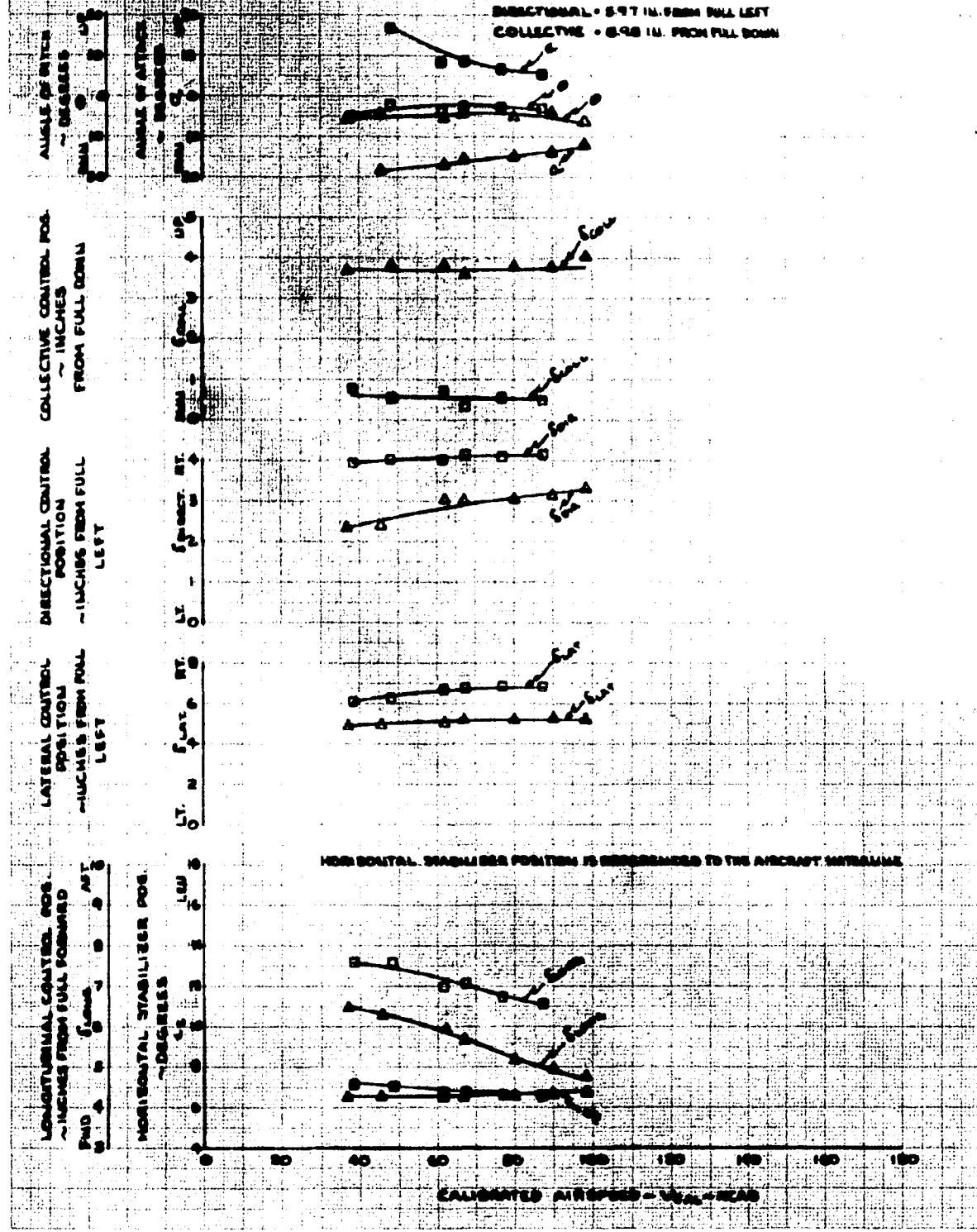
2. TOTAL CONTROL DISPLACEMENT

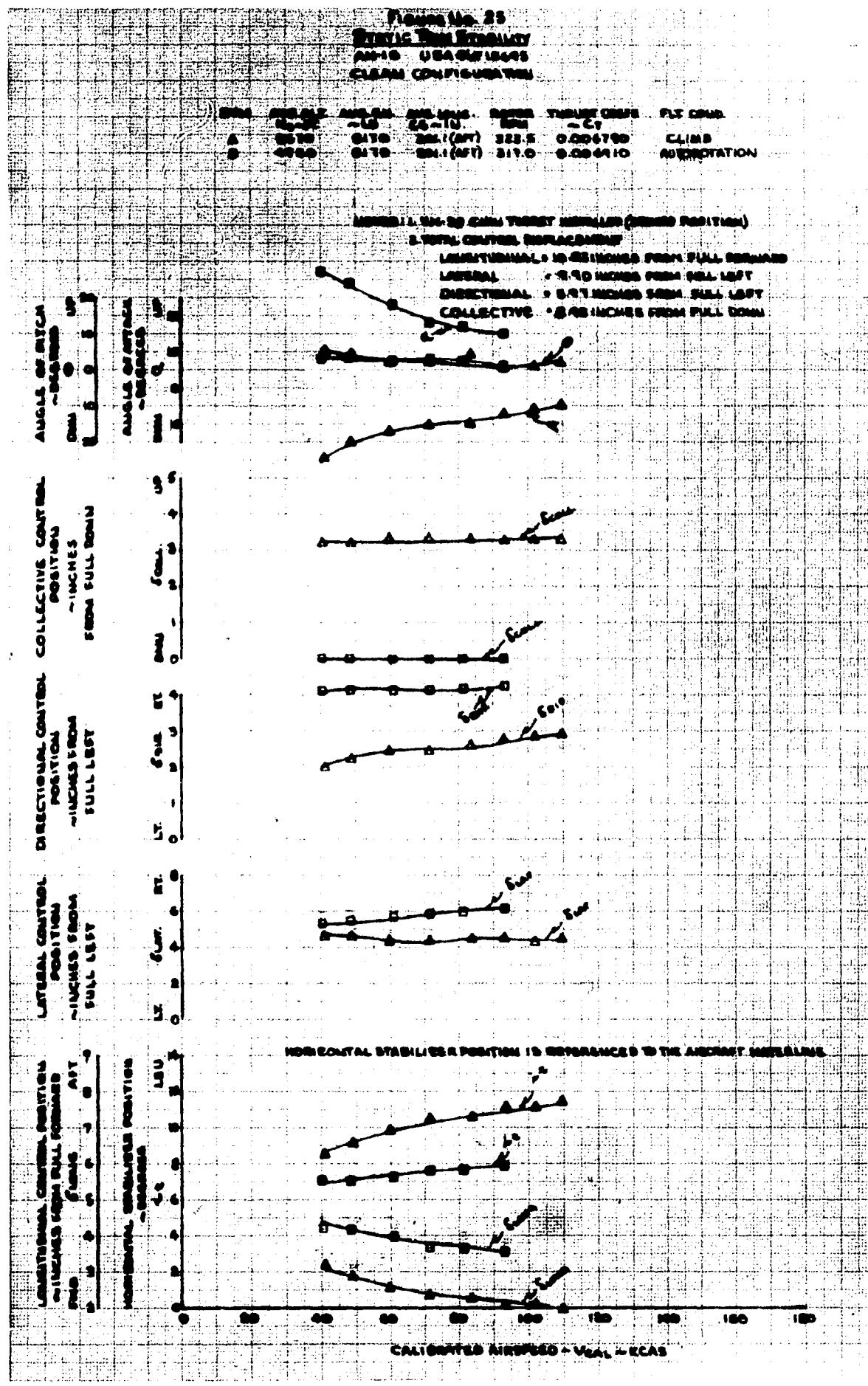
LONGITUDINAL = 10.00 IN. FROM FULL FORWARD

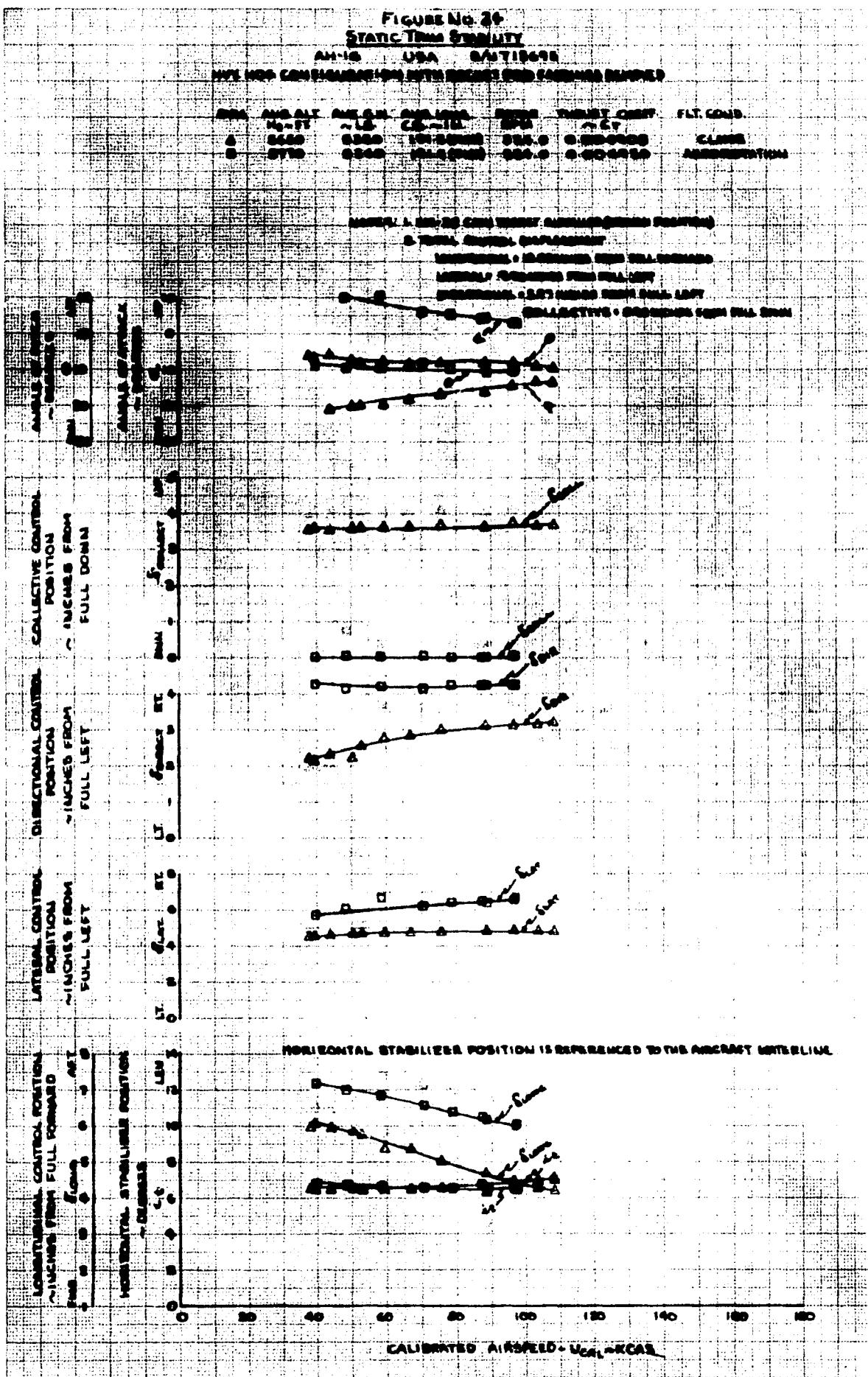
LATERAL = 4.70 IN. FROM FULL LEFT

DIRECTIONAL = 5.77 IN. FROM FULL LEFT

COLLECTIVE = 6.98 IN. FROM FULL DOWN







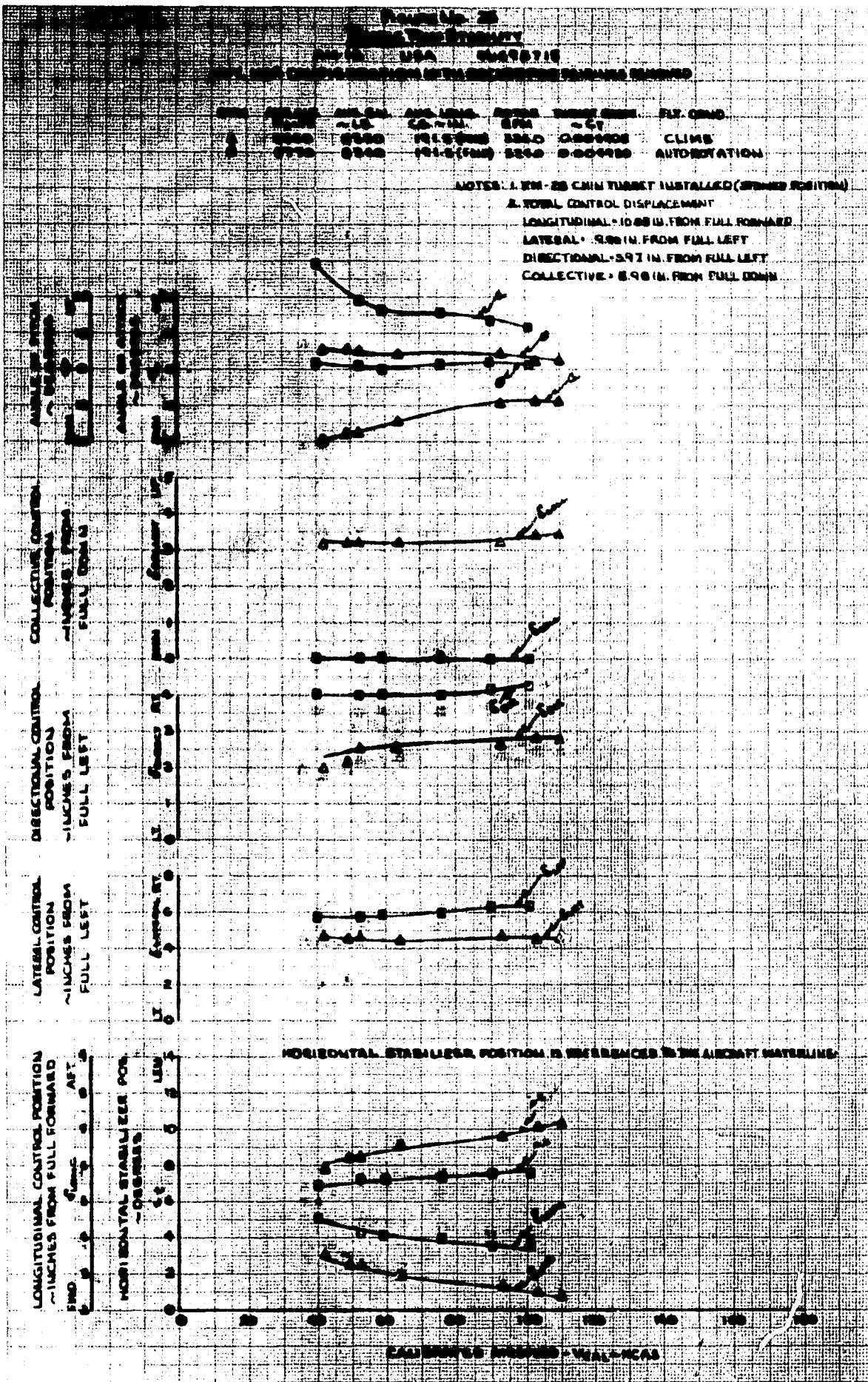


FIGURE NO. 26
 STATIC TRIM STABILITY
 AIRCRAFT WEIGHTS
 MVN. MOG. CONFIGURATION WITH BOOMET POD FAIRINGS REMOVED

DATA AND GND. WING CHG. AND LOADS. MOTOR: THURST CENTER
 $\text{M}_0 = 0.7$ CL₀ = 1.0 EPM ~ C_T
 ▲ 6010 4820 200(140) 324.0 0.005446 FLT. CGND
 ◆ 4950 4820 200(240) 331.0 0.005181 CLMAX AUTOROTATION

NOTES: 1. XM-28 CANN TURRET INSTALLED (STANDARD POSITION)
 2. TOTAL CENTER DISPLACEMENT:

- LONGITUDINAL - 10 INCHES FROM FULL FORWARD
- LATERAL - +0.98 INCHES FROM FULL LEFT
- DIRECTIONAL - +0.7 INCHES FROM FULL LEFT
- COLLECTIVE - +0.48 INCHES FROM FULL DOWN

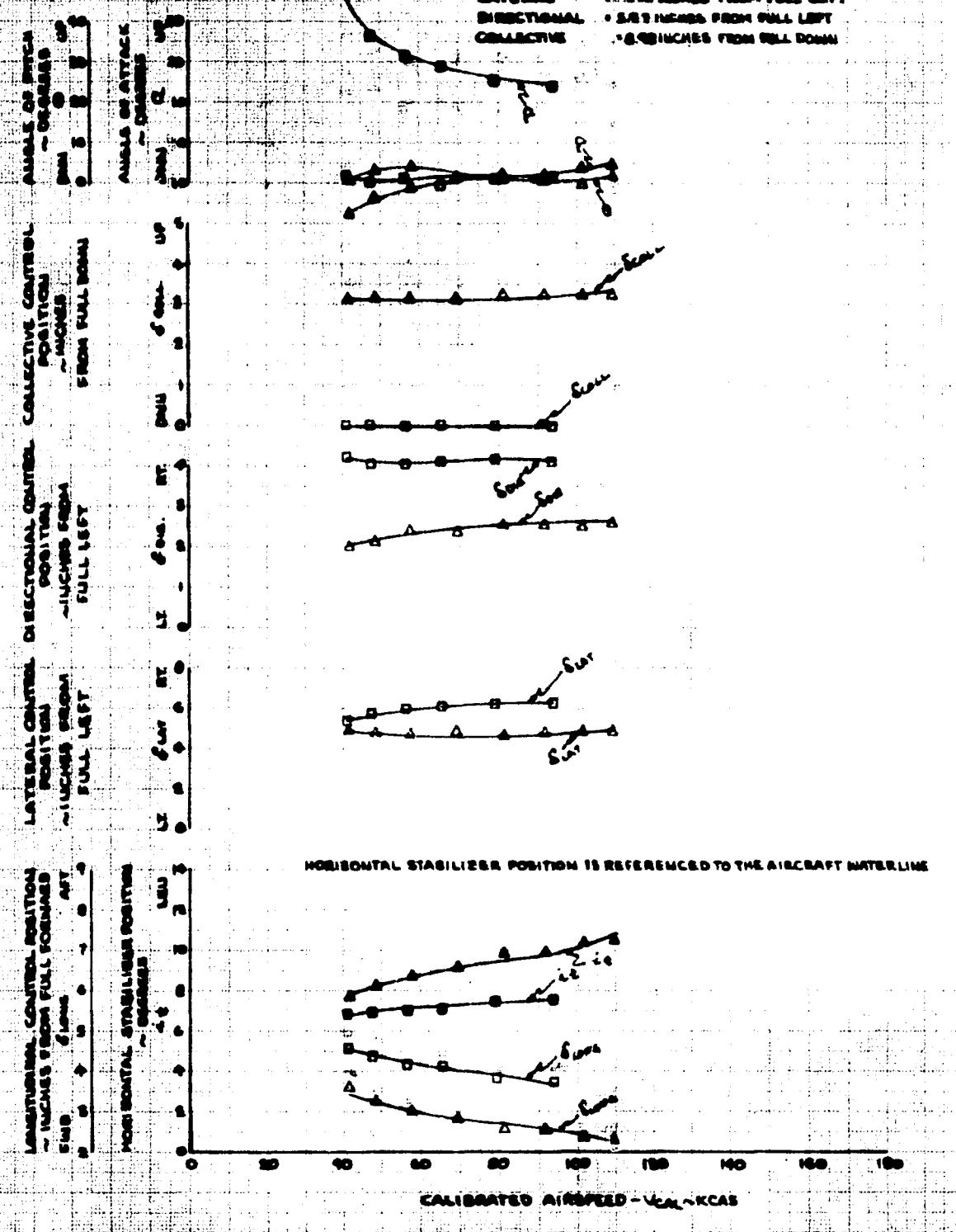


FIGURE NO. 27
 STATIC TIRM STABILITY
 AM-1G USA 8C15247
 CLEAN CONFIGURATION SKID TUBE FAIRINGS OFF

SYM AND ALT. AVG.G.H. AND LONG. MOTOR THRUST COEFF. FLT. COND.
 Hs ~5° ~LR C.G. ~IN. RPM ~CT
 0 3600 5540 199.9(FT) 3220 0.00480 LEVEL FLT.
 0 3140 5665 199.8(FT) 3220 0.00481 DIVE

NOTES: 1. TAT 102 CHIN TUBE INSTALLED (STOWED POSITION).

2. TOTAL CONTROL DISPLACEMENT

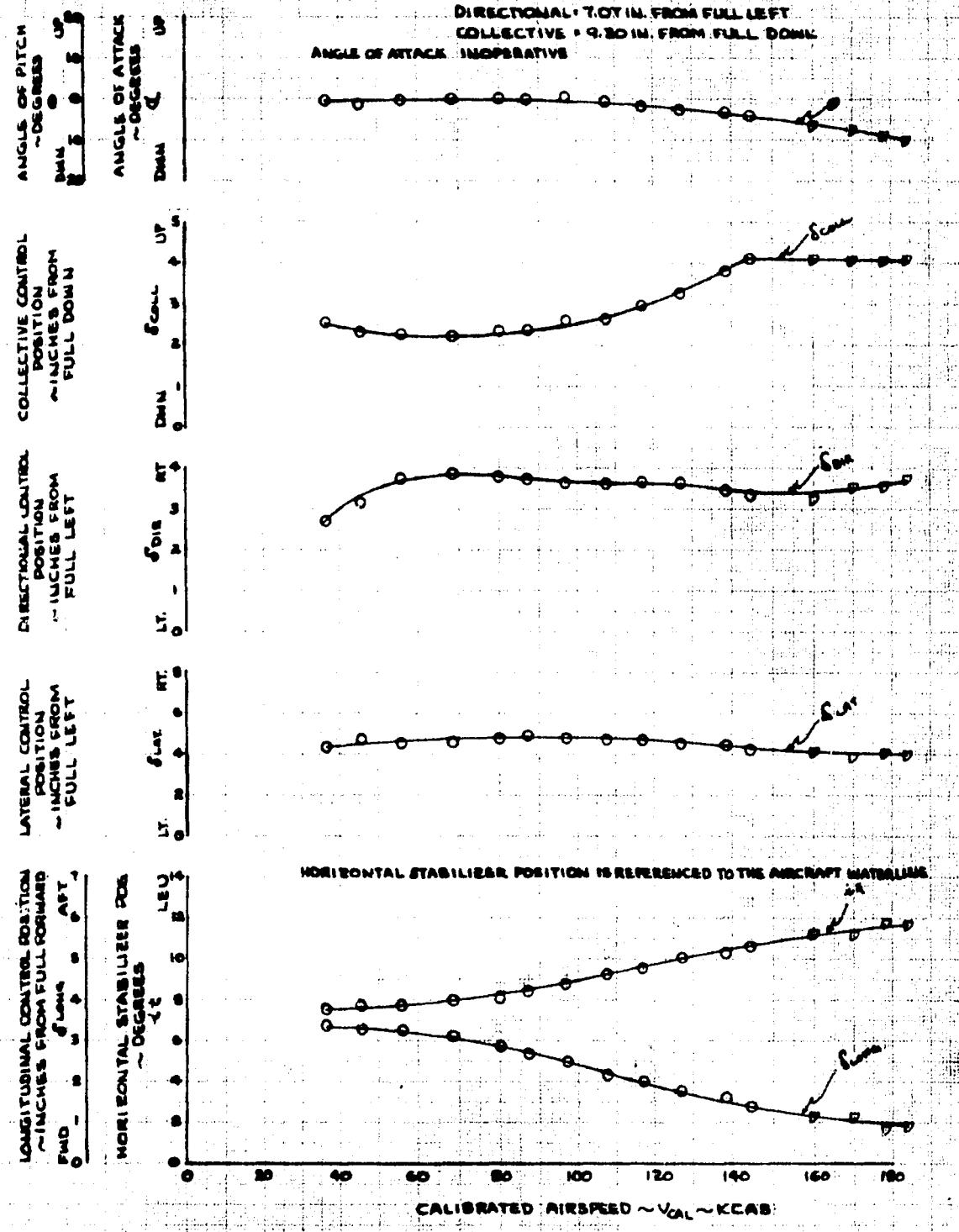
LONGITUDINAL = 9.0 IN. FROM FULL FORWARD

LATERAL = 10.00 IN. FROM FULL LEFT

DIRECTIONAL = 7.0 IN. FROM FULL LEFT

COLLECTIVE = 9.20 IN. FROM FULL DOWN

ANGLE OF ATTACK INOPERATIVE



HORIZONTAL STABILIZER POSITION IS REFERENCED TO THE AIRCRAFT WATERLINE.

FIGURE NO. 28
SUMMARY OF STATIC LONGITUDINAL COLLECTIVE FIXED STABILITY
 AH-1G USA 4718695
 GROSS WEIGHT COMPARISON

SYM.	ANG ALT. H _g -FT.	Avg. GROSS WT. LB.	ANGLE OF ARIE. deg. -10 deg. / sec.	ROTOR CONFIG.	THRUST COEFF. C.G.-IN. RPM	CYCLE
0	5510	6460	200.0(0)	202.0	0.003002	C
0	6020	7140	200.0(0)	202.0	0.003079	C
0	6530	7820	200.0(0)	202.0	0.003166	C
0	7140	8500	200.0(0)	202.0	0.003443	C
0	7650	9180	200.0(0)	202.0	0.003713	C

NOTES: 1. POINTS DERIVED FROM FIGURES 43 THROUGH 48, 50 THROUGH 55,
 AND 56 THROUGH 61, APPENDIX XII.

2. OPEN SYMBOLS DENOTE LEVEL FLIGHT.

3. CROSSED SYMBOLS DENOTE DIVE.

4. FLAGGED SYMBOLS DENOTE CLIMB.

5. TAILED SYMBOLS DENOTE AUTOROTATION.

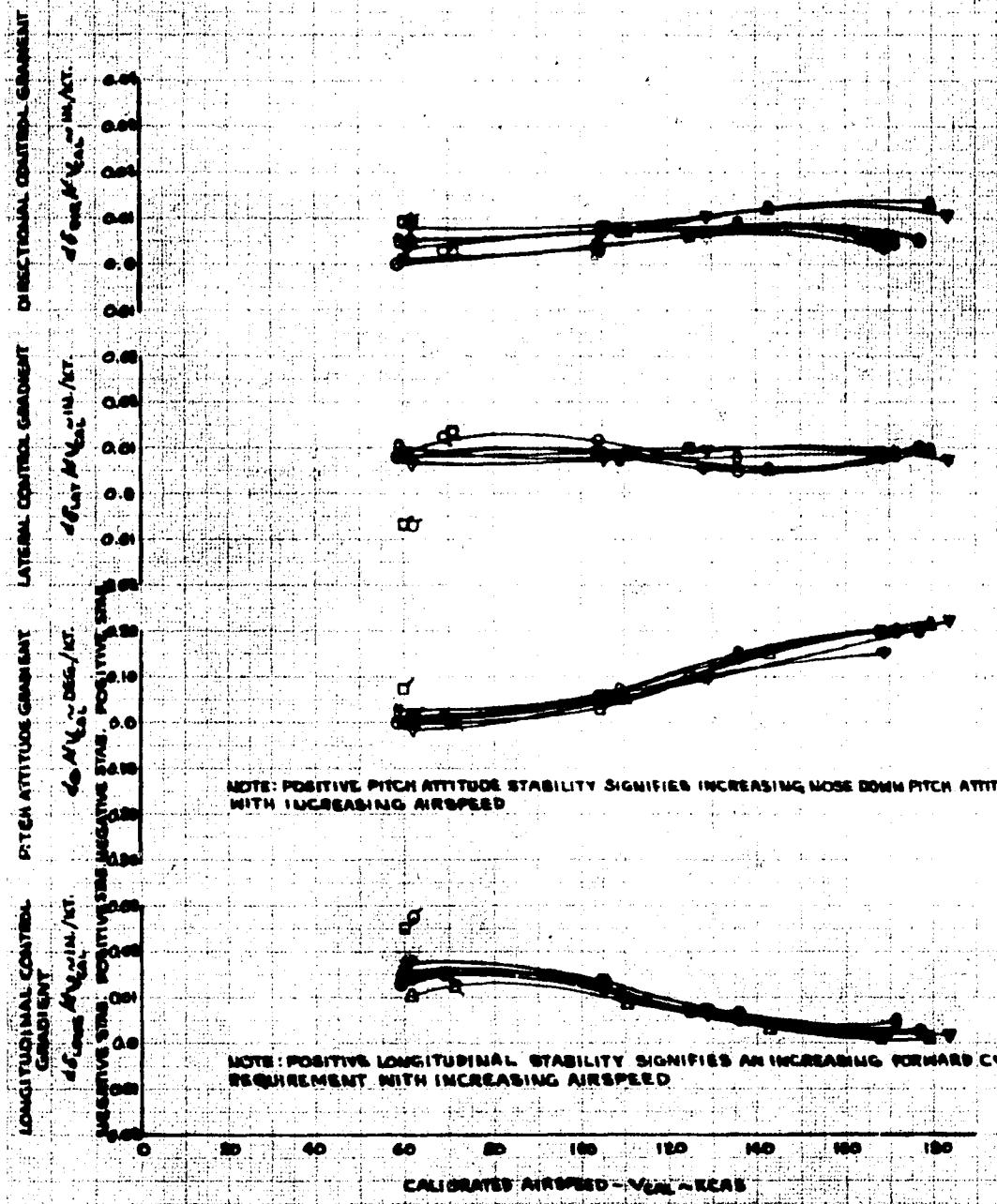


FIGURE No. 29
SUMMARY OF STATIC LONGITUDINAL COLLECTIVE FIXED STABILITY
AH-1G USA #715693
CENTER OF GRAVITY COMPARISON

SYM.	Avg. Alt. H ₀ ~FT.	Avg. Grav. Wt. ~LB.	Avg. Long. C.G.~IN.	RPM	CONFIG.	THRUST COEFF.
○	2810	8460	200.0(AFT)	3220	HVV.HDG	0.0004982
△	5730	8100	201.0(AFT)	3225	CLEAN	0.0004917
○	6766	8100	191.0(FWD)	3225	HVV.HDG	0.0004961
○	5760	8220	191.1(FWD)	3220	CLEAN	0.0004874

- NOTES: 1. POINTS DERIVED FROM FIGURES 22 THROUGH 40 AND 53
 THROUGH 59, APPENDIX III
 2. OPEN SYMBOLS DENOTE LEVEL FLIGHT
 3. CROSSED SYMBOLS DENOTE DIVE
 4. FLAGGED SYMBOLS DENOTE CLIMB
 5. TAILED SYMBOLS DENOTE AUTOROTATION

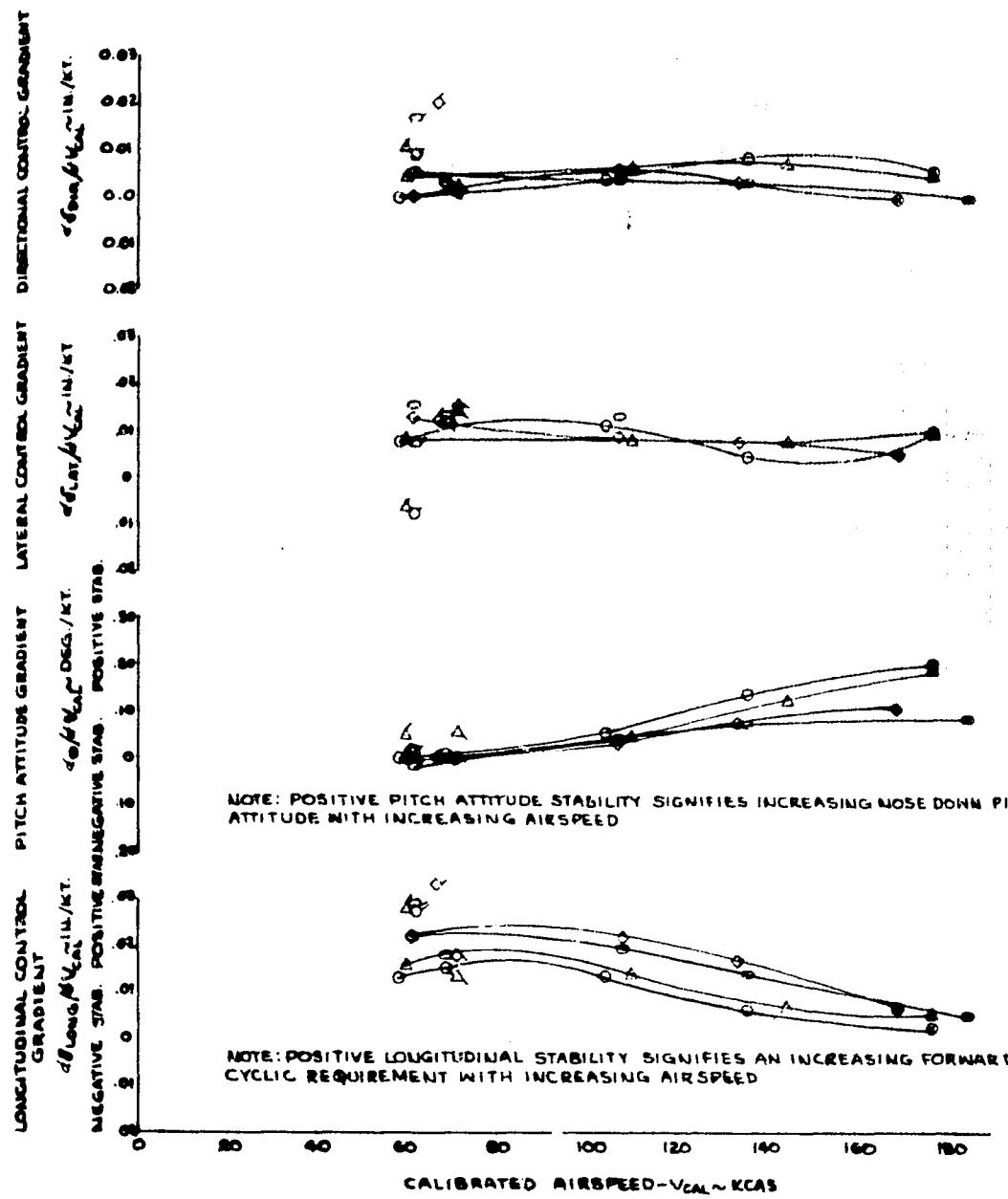


FIGURE NO. 50
SUMMARY OF STATIC LONGITUDINAL COLLECTIVE FIXED STABILITY
AH-1G USA #NTIS 695
ALTITUDE COMPARISON

SYM.	ANG ALT. HO ~ FT.	Avg. Gross WT. ~ LB	Avg. Long. C.G. ~ IN.	ROTOR RPM	CONFIG.	THRUST COEFF. ~ CT
▲	5700	8400	201.1(AFT)	322.5	CLEAN	0.004817
●	5820	8415	201.0(AFT)	324.5	HVV. HOG	0.004644
○	5810	8460	200.8(AFT)	322.0	HVV. HOG	0.004982
△	4970	8150	201.0(AFT)	324.0	OUTED ALT.	0.004773
◎	15620	8150	201.1(AFT)	322.5	CLEAN	0.006881
■	14660	8570	201.7(AFT)	323.5	HVV. HOG	0.006700
○	14650	8180	201.7(AFT)	323.5	OUTED ALT	0.006402

NOTES: 1. POINTS DERIVED FROM FIGURES 38 THROUGH 43, 45 THROUGH 50,
 56 THROUGH 58, 62 AND 63, APPENDIX III
 2. OPEN SYMBOLS DENOTE LEVEL FLIGHT
 3. CROSSED SYMBOLS DENOTE DIVE
 4. FLAGGED SYMBOLS DENOTE CLIMB
 5. TAILED SYMBOLS DENOTE AUTOROTATION

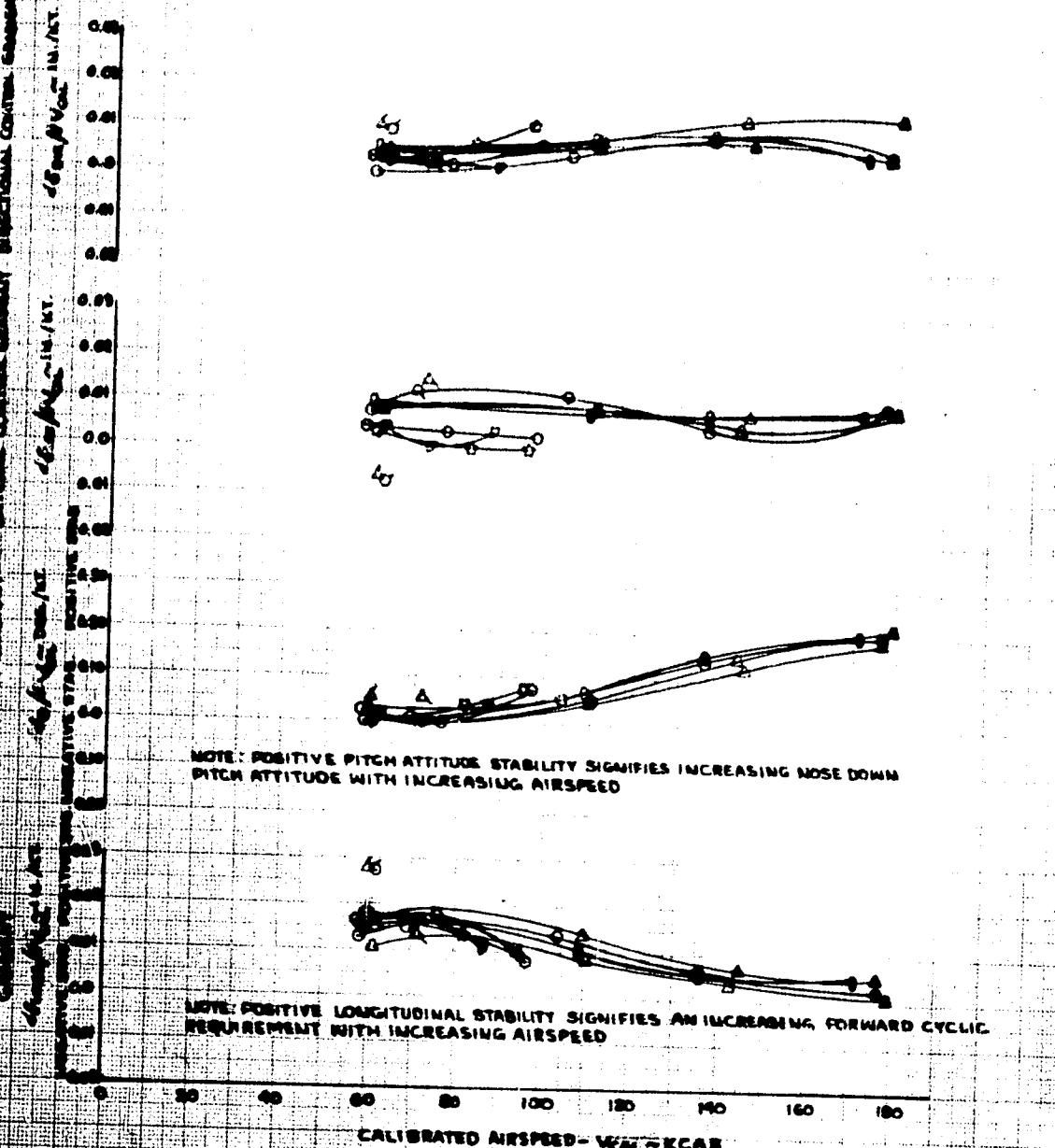


FIGURE NO. 31
Summary of Static Longitudinal Collective Fixed Stability
AH-1S

DATA ANG. ATT. AND G.L. AND LOAD. FOR 20 TON CHIN. CARGO. 8/64
 NO. OF C.G. = 10. C.G. = 10. 100% MAX. LOAD. ~11° CARGO
 O 6000 6000 199.7 (MFT) 352.0 CARGO 20 TON CHIN. CARGO
 A 6750 6000 200.4 (MFT) 353.5 CARGO 20 TON CHIN. CARGO

LOCATES DERIVED FROM FIGURES IN THE MAN 20, 21 AND 22.

APPENDIX III

1. OPEN SYMBOLS INDICATE LEVEL FLIGHT.

2. CROSSED SYMBOLS INDICATE CLIMB.

3. SOLID SYMBOLS INDICATE DESCENT.

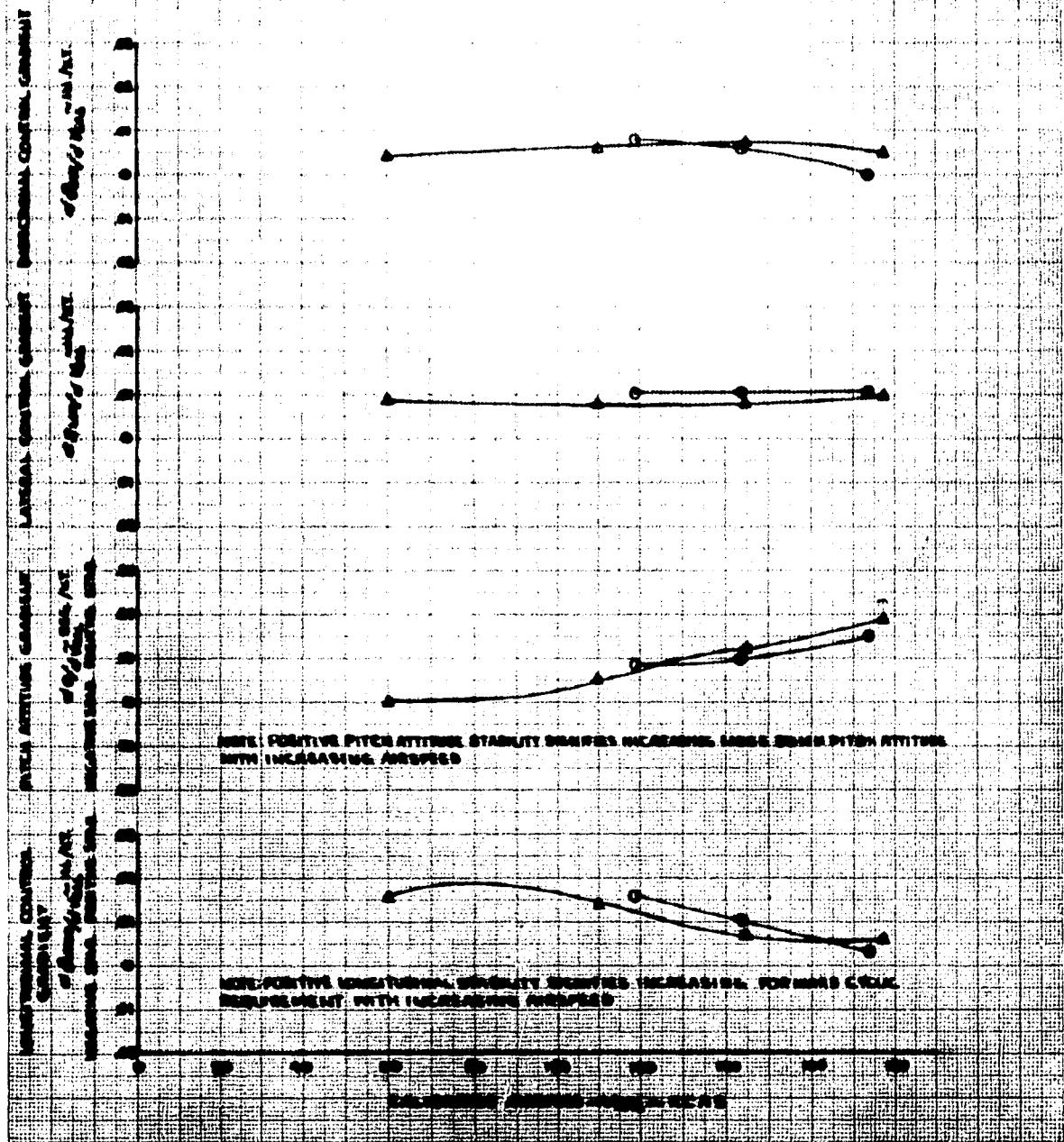


FIGURE NO. 32
 STATIC LONGITUDINAL COLLECTIVE FIXED STABILITY
 AH-1G USAF 718695
 CLEAN CONFIGURATION

SYM	Avg. Alt. ft	Avg. G-M ~Lb	Avg. Lndg. C.G. ~IN.	Rot. deg/sec	Flt. Cond.	Thrust Coeff.
0	4380	7440	140.6(FWD)	2240	LEVEL FLT.	0.0004800
0	5160	7828	140.3(PWD)	2230	LEVEL FLT.	0.0004873

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINTS

2. AH-1G CMM TURBET INSTALLED (ARMED POSITION)

3. TOTAL CONTROL DISPLACEMENT

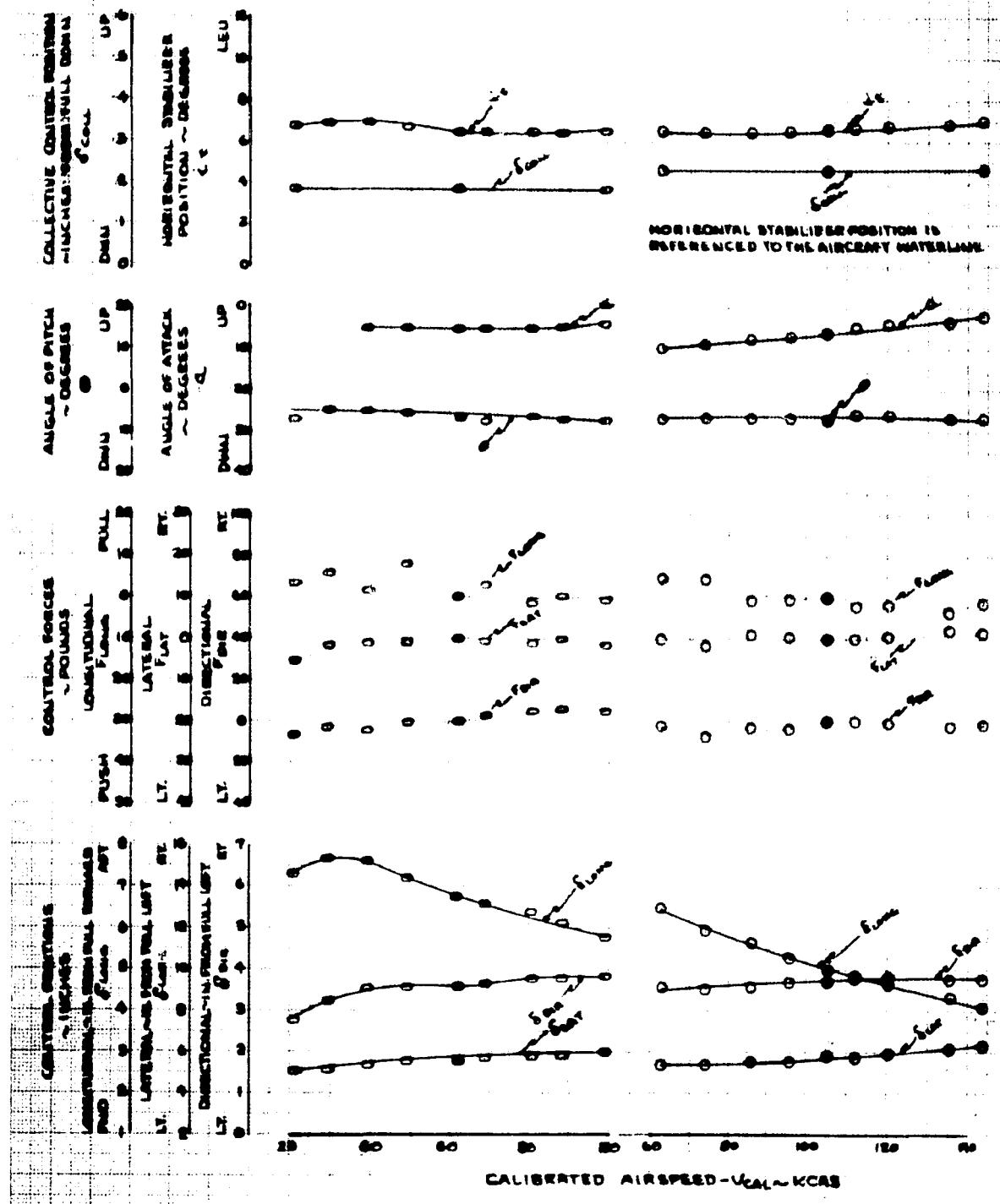
LONGITUDINAL = 10 INCHES FROM FULL FORWARD

LATERAL = 9 INCHES FROM FULL LEFT

DIRECTIONAL = 8.97 INCHES FROM FULL LEFT

COLLECTIVE = 8.98 INCHES FROM FULL DOWN

4. BREAKOUT FORCES HAVE BEEN ANALYTICALLY REMOVED
 FROM ALL CONTROL FORCE DATA



Project No. 202
TURBINE LOADING AND COLLECTIVE FORCE SURVEY

AN-26 USAF/NASA

DATA SHEET NO. 1

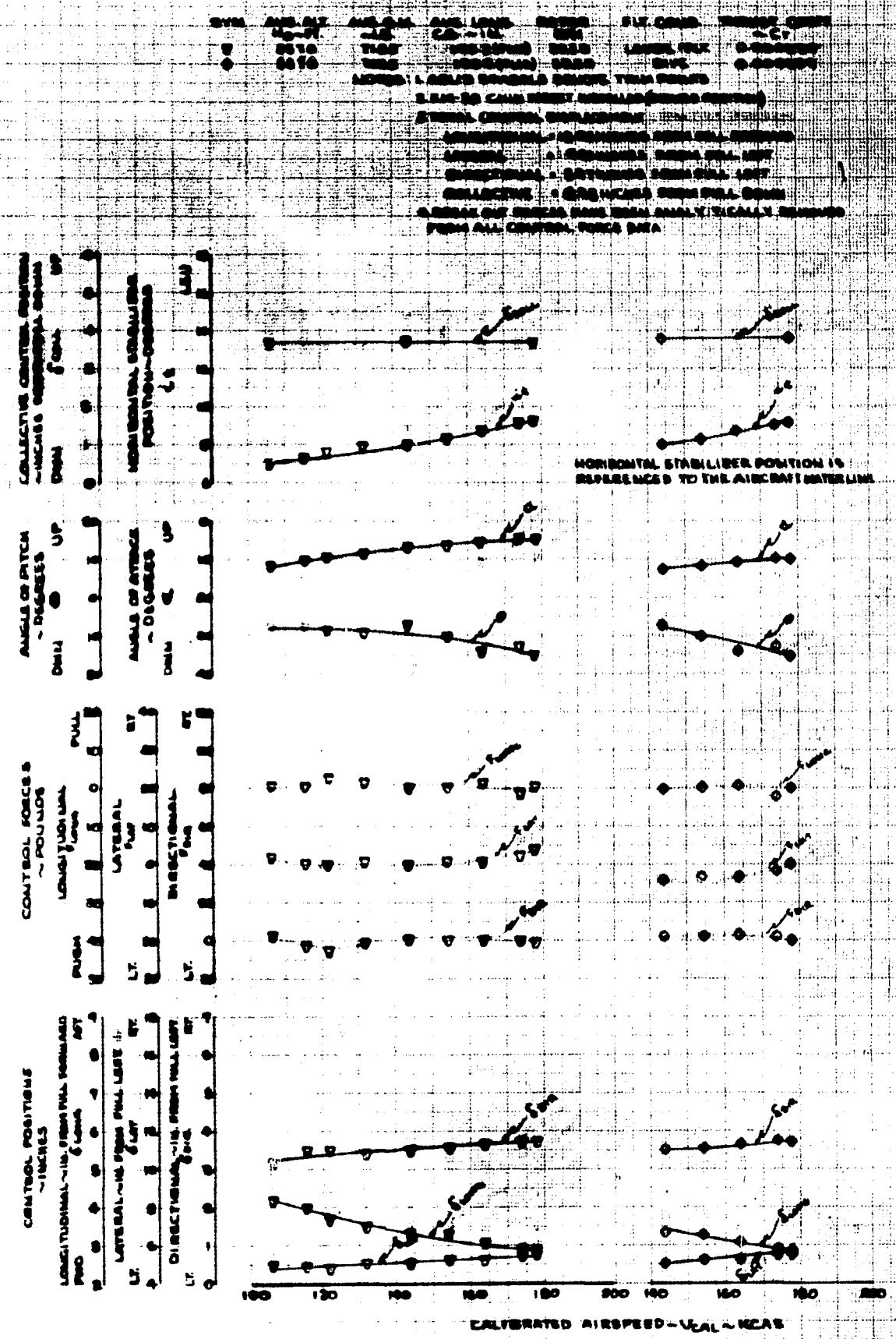


FIGURE NO. 50
 STATIC LONGITUDINAL COLLECTOR FINED STABILITY
 AN-10 U.S. AIR FORCE
 CLEAN Configuration

DATA SOURCE: ANGUS AND MCGEE, 1960
 TEST NUMBER: 1000
 DATE: 10-10-60
 ALTITUDE: 10,000 FEET
 WIND: 10 MPH STRAIGHT FROM THE NORTH
 2.500 G CHIN UP AT MINIMUM OPERATING ALTITUDE
 D. TAIL CENTER LINE POSITION
 LATERAL: 10 INCHES FROM CHIN POSITION
 LATERAL: + 10 INCHES FROM CHIN LEFT
 DIRECTIONAL: - 5 INCHES FROM CHIN LEFT
 COLLECTIVE: + 10 INCHES FROM CHIN DOWN
 AVERAGE ONE STANDARD DEVIATION ANALYTICALLY DERIVED
 FROM ALL CONTROL FORCE DATA

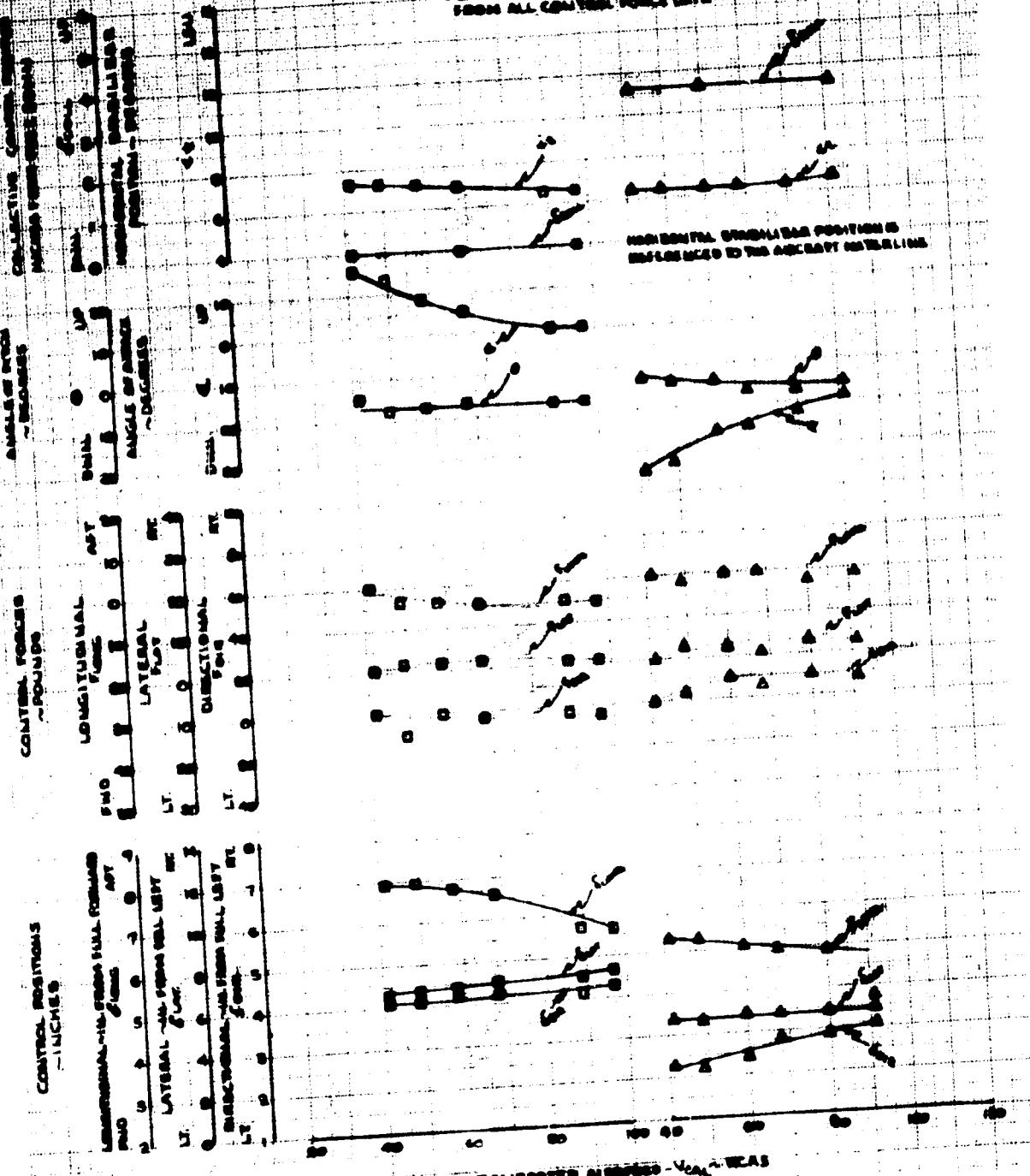


FIGURE NO. 10
STATIC LONGITUDINAL COLLECTIVE FIXED STABILITY
AN-12 MACH 0.75
CABIN COMPARTMENT

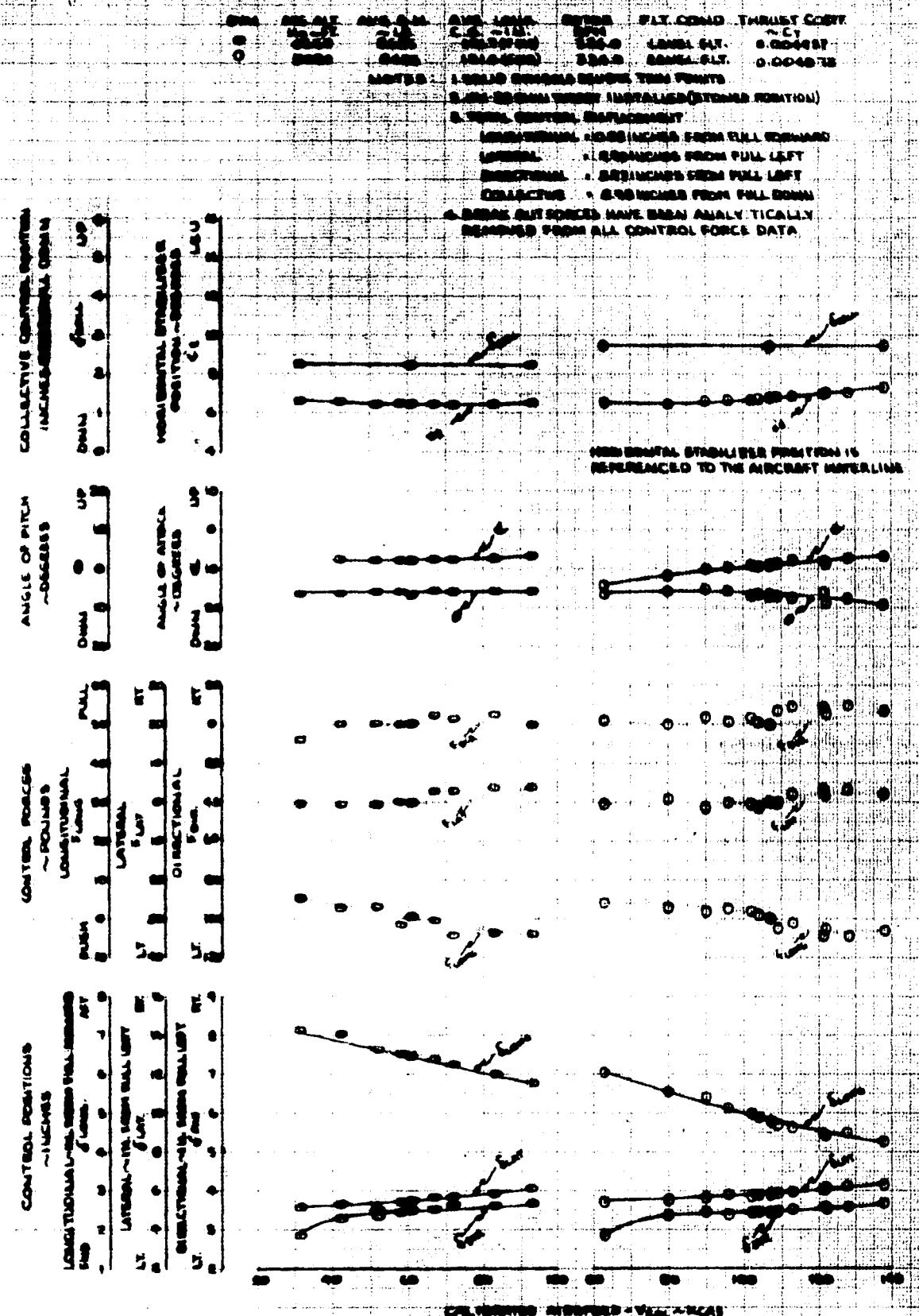


FIGURE NO. 36
STATIC LONGITUDINAL COLLECTIVE FRICTION STABILITY
AM-1G - USAF/HOPS
CLEAN CONFIGURATION

DATA: MAX AND MIN. ANG. LOADS. DRAFT: 0.1200. THRUST: 0.90.
 HORIZONTAL - 1.0 C.G. - 1.0. 0.0000. ~C_T
 STAB: 0.000 190.0 (MAX) 0.000 LEVEL FLT: 0.0047E-1
 0.000 190.0 (MIN) 0.000 0.0000E-1

NOTES: 1. SOLID SYMBOLS INDICATE TEST POINTS
 2. X-SYMBOLS INDICATE INTERPOLATED POINTS
 3. TOTAL CENTRAL DISPLACEMENTS
 LONGITUDINAL = 100 INCHES FROM FULL FORWARD
 LATERAL = 100 INCHES FROM FULL LEFT
 DIRECTIONAL = 59.7 INCHES FROM FULL LEFT
 COLLECTIVE = 500 INCHES FROM FULL DOWN
 4. BREAK OUT POINTS HAVE BEEN ANALYTICALLY REMOVED
 FROM ALL CONTROL FORCE DATA

HORIZONTAL STREAMER POSITION TO
 IMBALANCE TO THE AIRCRAFT CENTERLINE

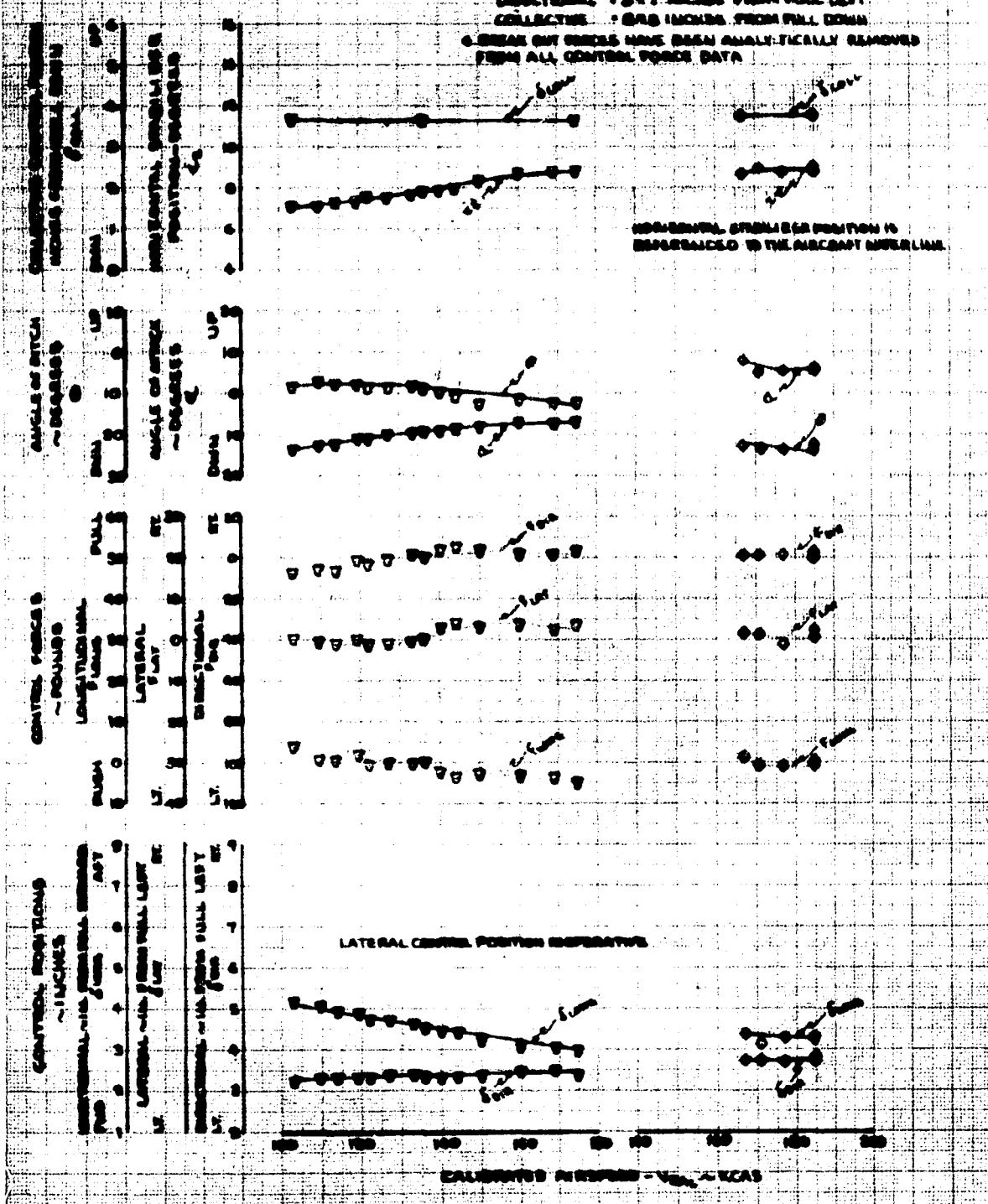


FIGURE NO. 37
 STATIC LONGITUDINAL COLLECTIVE FIN STABILITY
 AH-1G - U20A715649
 CLEAN CONFIGURATION

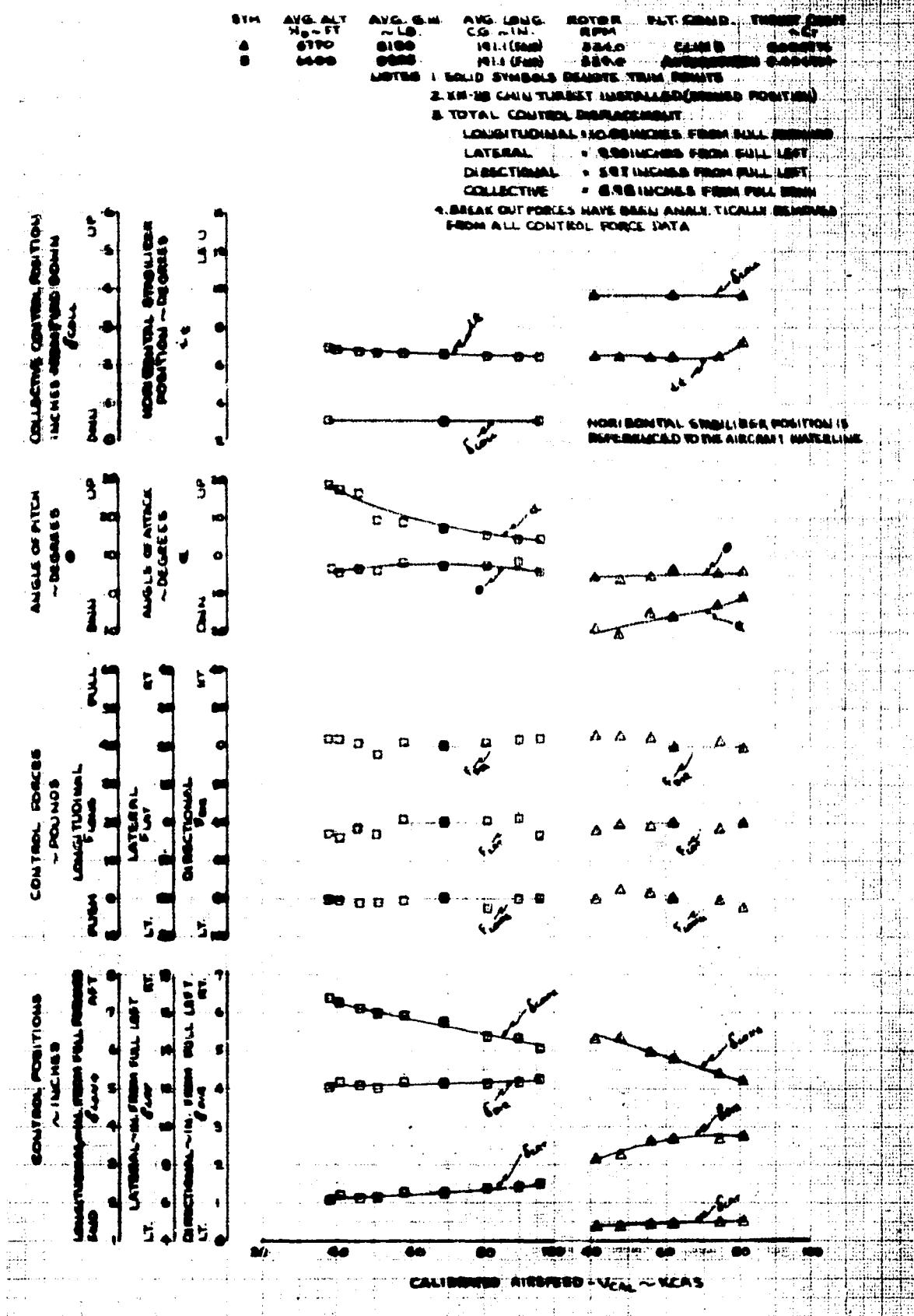


FIGURE NO. 38
 STATIC LONGITUDINAL COLLECTIVE FIXED STABILITY
 AMIG USAF 15698
 CLEAN CONFIGURATION

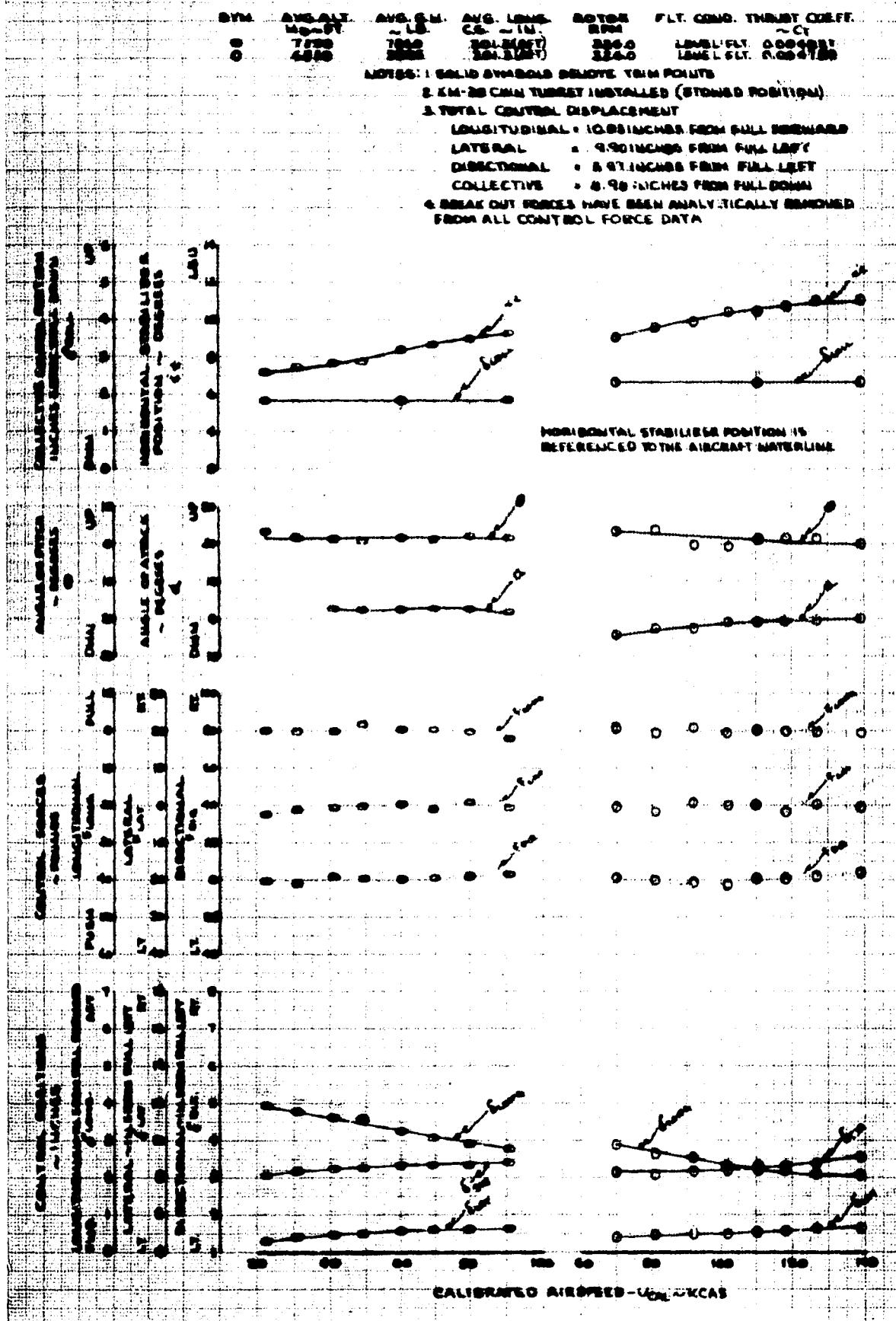


FIGURE NO. 59
STATIC LONGITUDINAL COLLECTIVE FLYER STABILITY
AH-1G USAF 74-16000
CLEAN CONFIGURATION

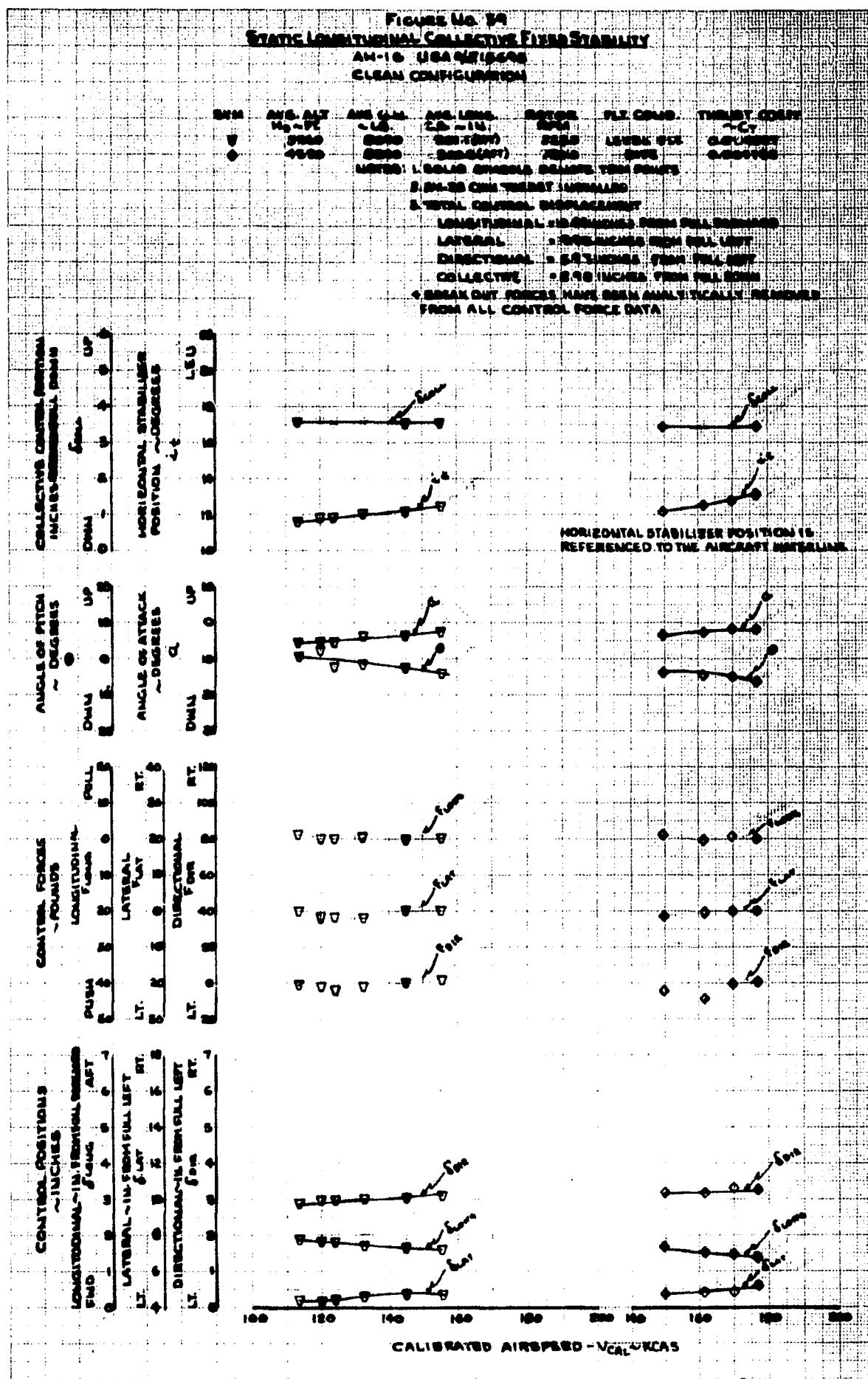


FIGURE NO. 40
 STATIC LONGITUDINAL COLLECTIVE FIN POSITION
 AND HORIZONTAL STABILIZER POSITION
 CLEAN CONFIGURATION

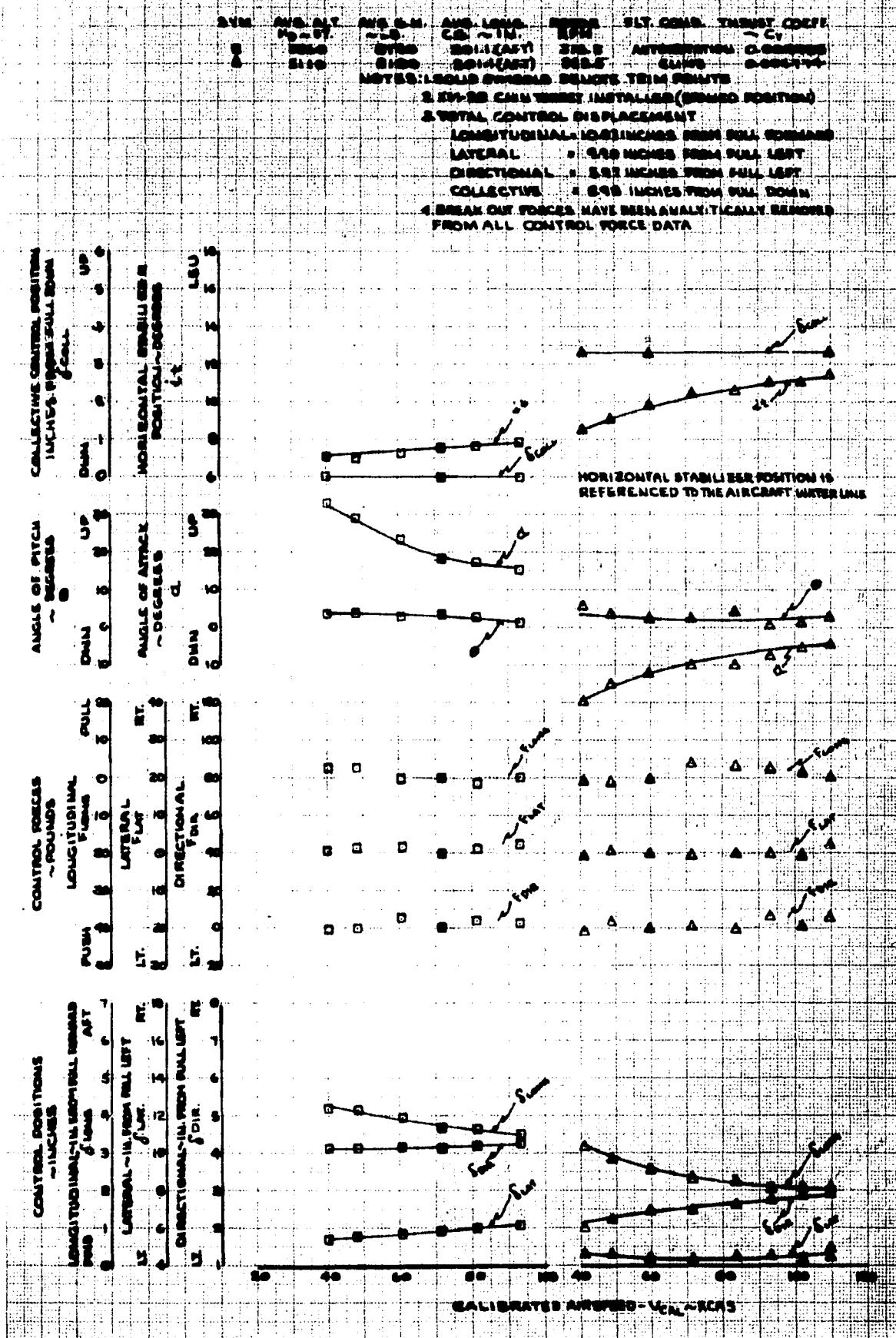


FIGURE No. 41
STATIC LONGITUDINAL COLLECTIVE FIXED STABILITY
AH-1G - HEAVY LOADS
CLEAN CONFIGURATION

AVM AVG. ALT AVG. RPM AVG. LONG. ROTOR FL. C.G. THRUST (OZ)
 M₂ = 10000 2000 1201.0 (RPT) 334.0 LEVEL FLT. 0006666
 16400 2000 1201.1 (RPT) 335.0 LEVEL FLT. 0006672
 MOTORS 1. SOLID SYMBOLS INDICATE TRIM POINTS
 2. KH-28 CHAIN TURRET INSTALLED (STORM POSITION)

3. TOTAL CONTROL DISPLACEMENT

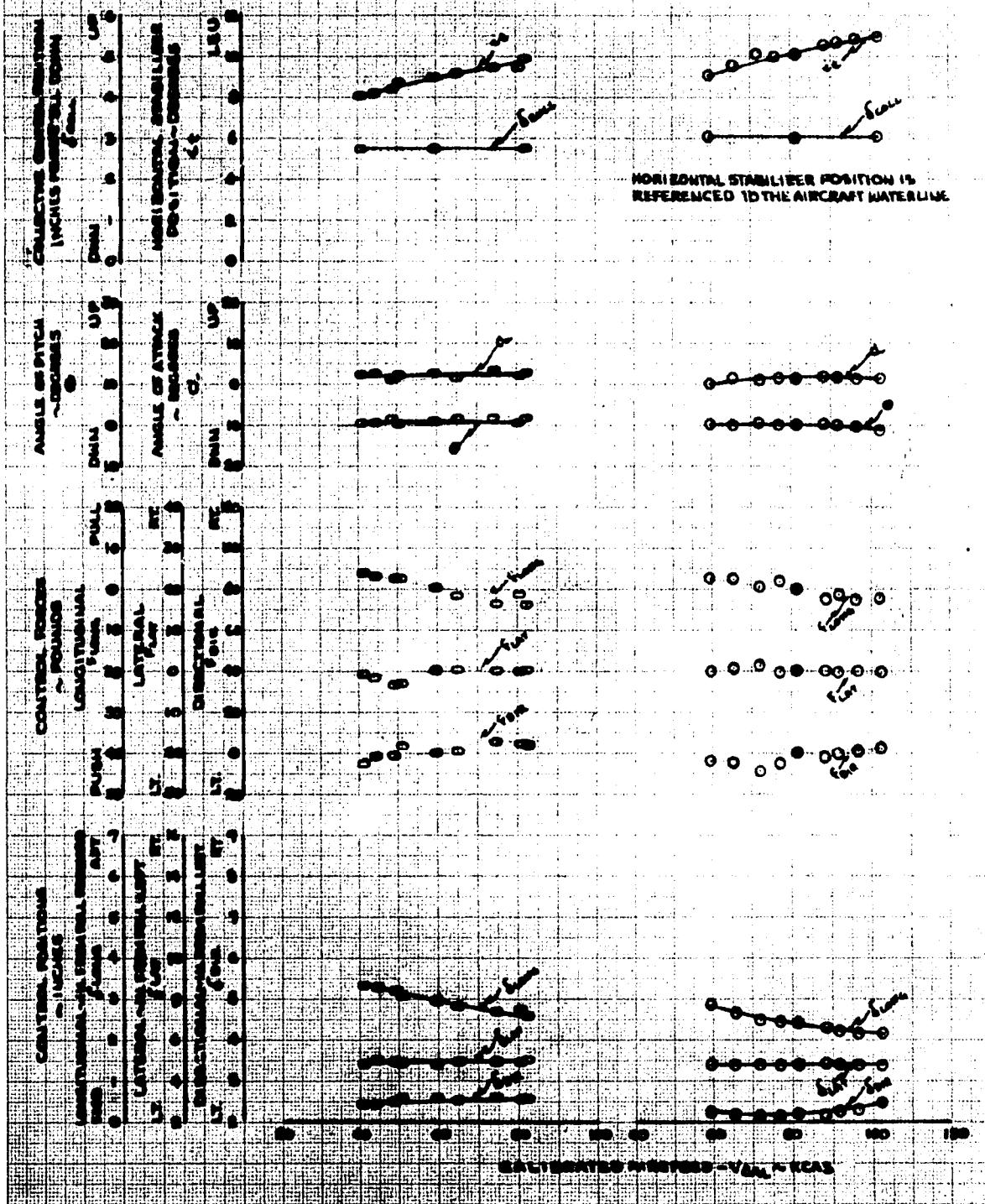
LATERAL: 1.00 INCHES FROM FULL FORWARD

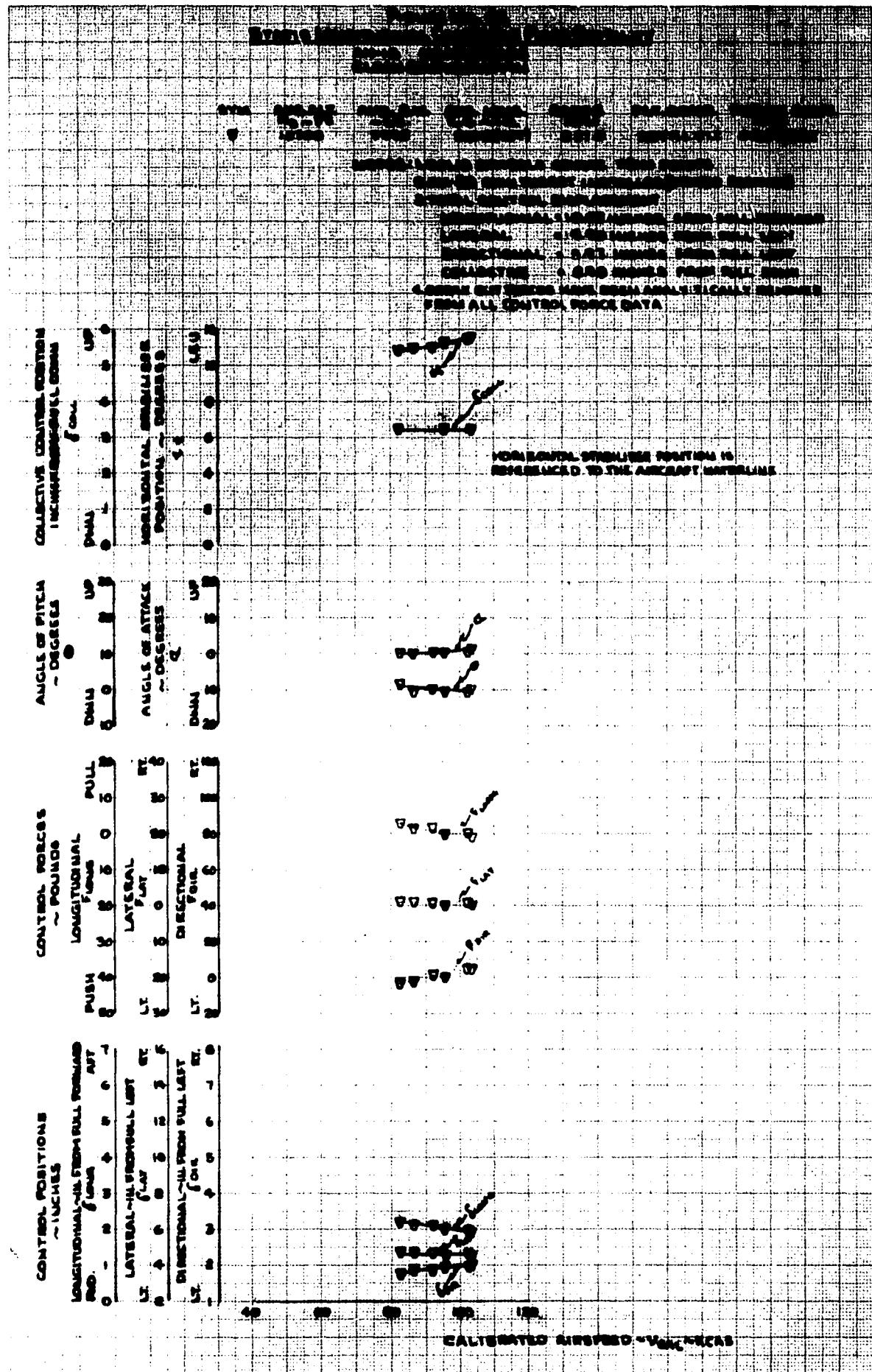
LATERAL: 1.00 INCHES FROM FULL LEFT

DIRECTIONAL: 5.0 INCHES FROM FULL LEFT

COLLECTIVE: 0.08 INCHES FROM FULL DOWN

4. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED
FROM ALL CONTROL FORCE DATA





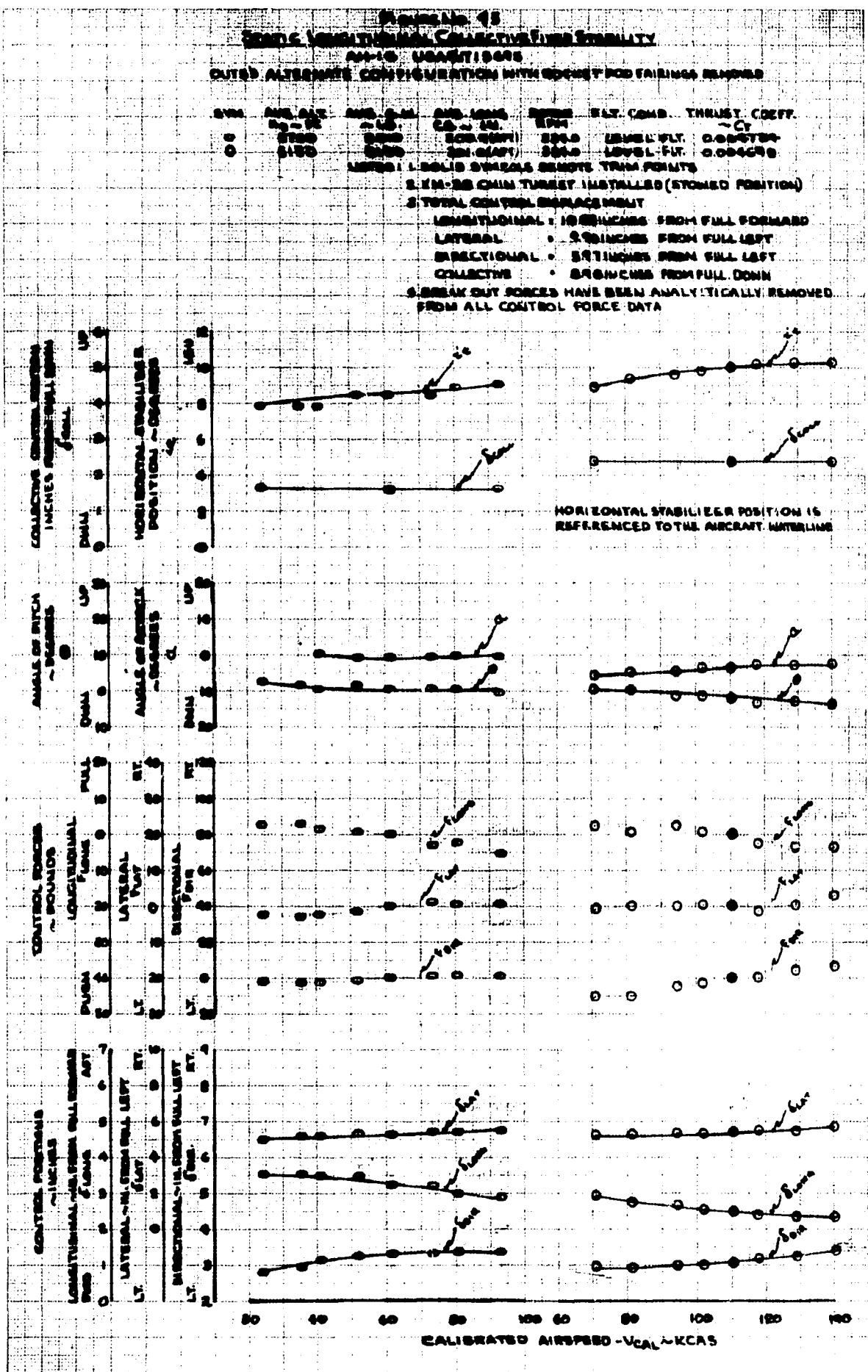


FIGURE NO. 44
STATIC LONGITUDINAL COLLECTIVE FLEXIBILITY
AH-1G USAF TIGER

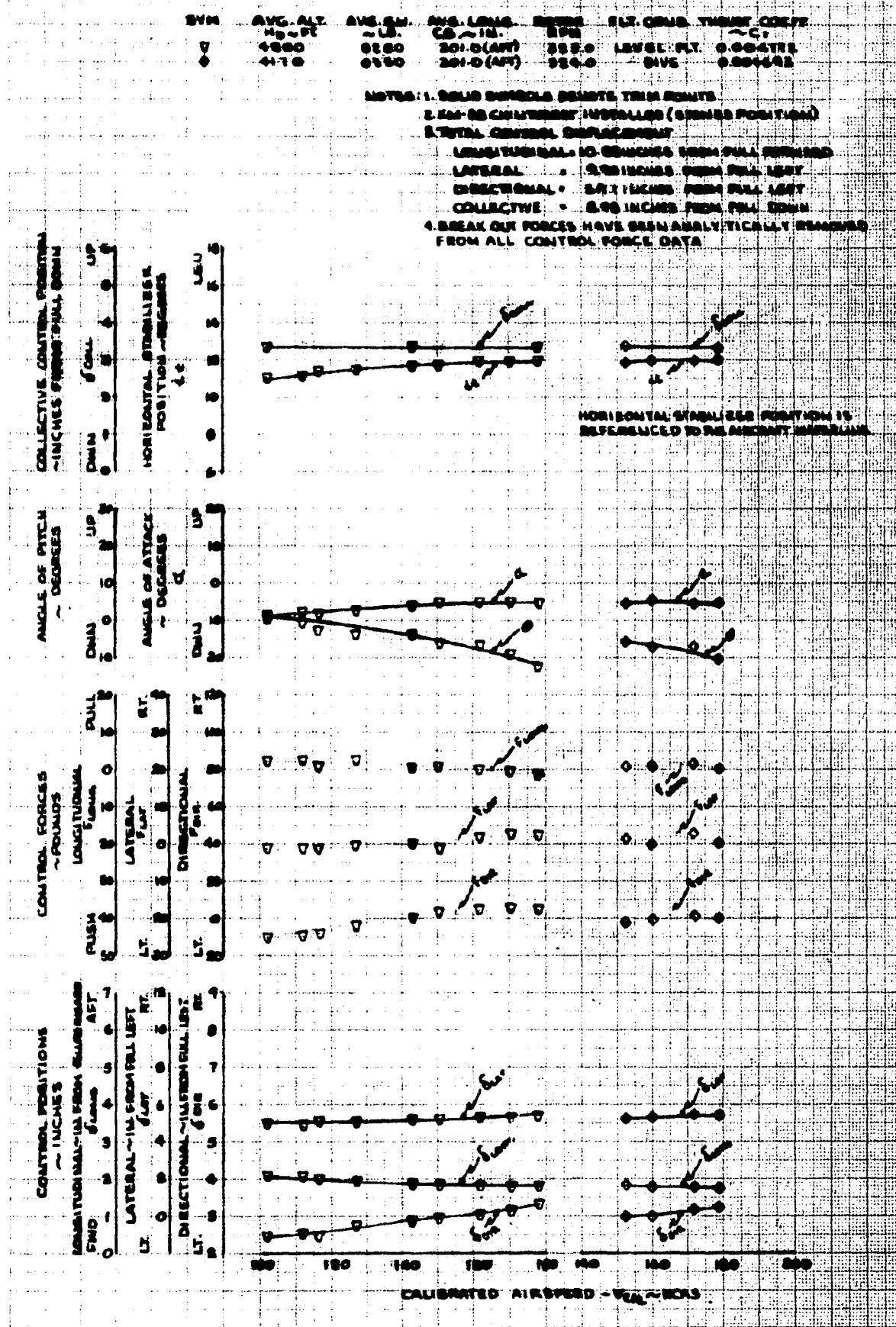


FIGURE NO. 45
STATIC LONGITUDINAL COLLECTIVE THROTTLE STABILITY

AH-1G - USES LOAD
 GUTTED ALTERNATIVE CONFIGURATION WITH BLADE PROFAIRINGS REMOVED

BVM	Avg Alt.	Avg. GM	Avg. Long.	Notes	Flt. Cond.	Thrust - GROSS
Hd - PL	-15	66.4 - 11.0	22.4	-CT		
PL	15	66.4 - 11.0	22.4	350.0	LOWR FLT. 0.00000	
PL	15	66.4 - 11.0	22.4	350.0	LOWR FLT. 0.00001	

NOTES: 1. SOLID DIAMOND = Remote Trim Points

2. FM-20 CHIN TURBINE INSTALLED (OPENED POSITION)

3. TOTAL CONTROL DISPLACEMENT

LONGITUDINAL = 10 INCHES FROM FULL FORWARD

LATERAL = 10 INCHES FROM FULL LEFT

DIRECTIONAL = 6.7 INCHES FROM FULL LEFT

COLLECTIVE = 1.65 INCHES FROM FULL DOWN

4. GRAY BOX FORCES HAVE BEEN ANALYTICALLY REMOVED
 FROM ALL CONTROL FORCE DATA

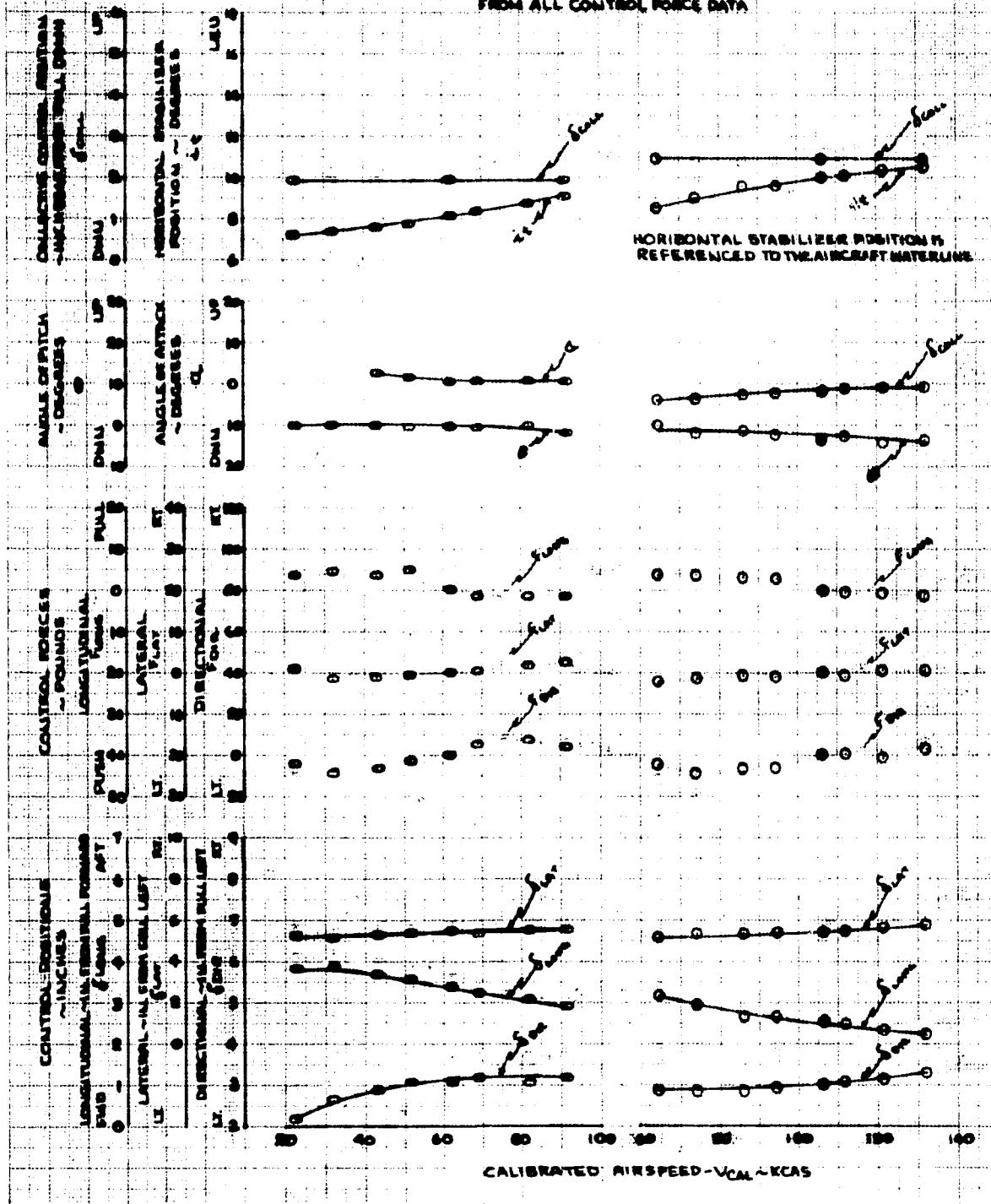


FIGURE NO. 48
STATIC LONGITUDINAL COLLECTIVE FLYING STABILITY
AM-10 USAF 94668
OUT OF ALTITUDE CONFIGURATIONS WITH SOVIET PROPELLERS REMOVED

SIM	Avg. Alt.	Avg. GM	Avg. Long.	Rotors	P.L. Comm.	Thrust Comm.
NO-10	~100	C.G. - 1.0	0.000	2000	0.000	~0.7
6786	1000	0.000	0.000	2000	0.000	0.000
9130	9100	0.000	0.000	2000	0.000	0.000

NOTES:
 1. SOLID SYMBOLS DENOTE TEST POINTS
 2. AM-10 CHIN TURRET INSTALLED (STEADY POSITION)
 3. TOTAL CONTROL DISPLACEMENT
 LONGITUDINAL = 1.0 INCHES FROM FULL FORWARD
 LATERAL = 0.900 INCHES FROM FULL LEFT
 DIRECTIONAL = 0.93 INCHES FROM FULL LEFT
 COLLECTIVE = 0.70 INCHES FROM FULL DOWN
 4. BREAK OUT FORCES HAVE BEEN ANALYTICALLY DEDUCED
 FROM ALL CONTROL FORCE DATA.

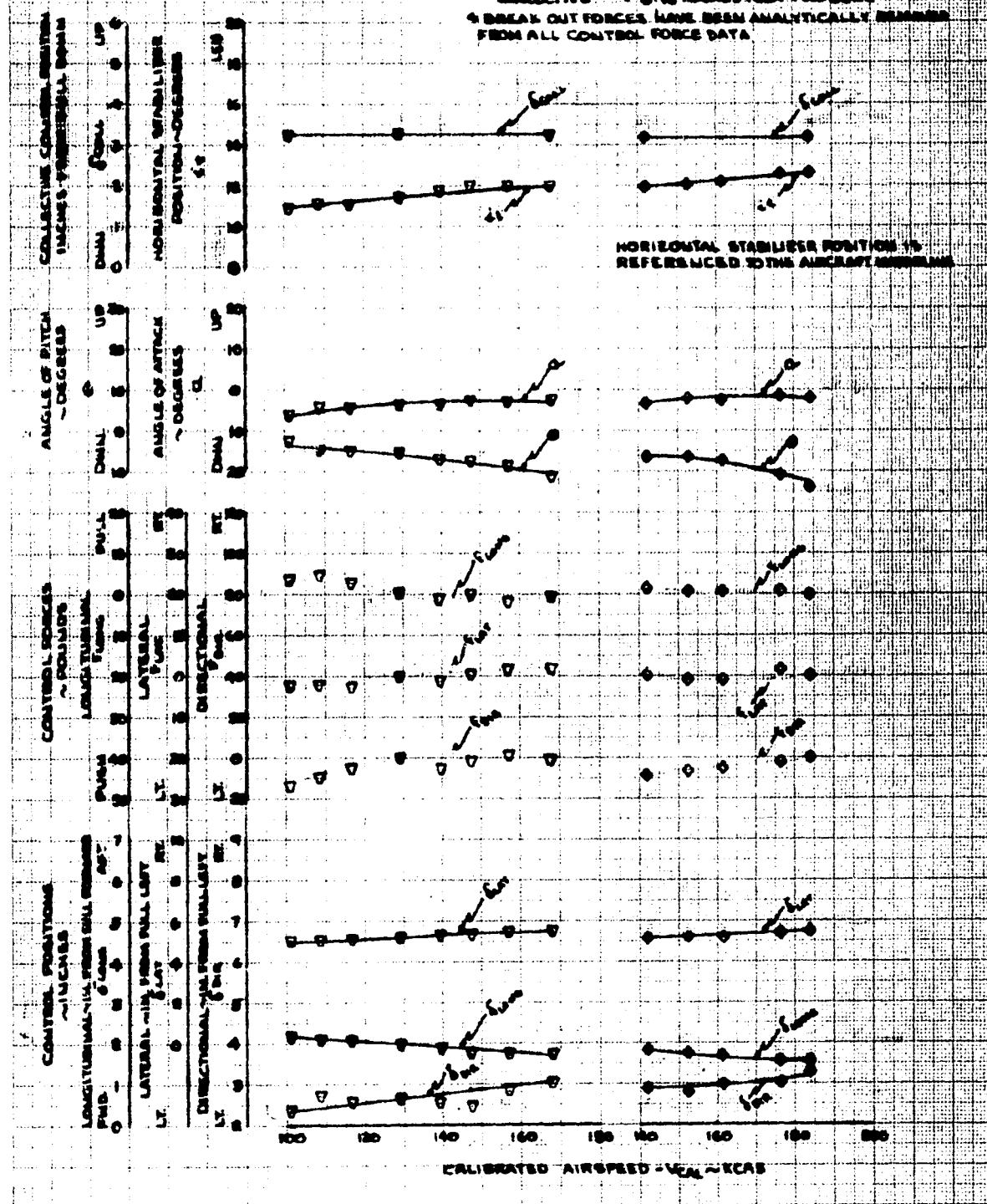


FIGURE A-6
STATIC LONGITUDINAL COLLECTIVE FIXED STABILITY

AH-1G USAF 71-6768
 OUTTED ALTERNATE CONFIGURATION WITH TURBO POD SCAFFOLDS REMOVED

DATA: AVG. ALT. AND GM. AND LONG. ROLLING FLT. COEFF. THRUST COEF.
 $M_0 = 10$ FT. ~1.5 C_T = 1.0. 0.001
 10300 0.020 0.000000 LEVEL-FL. 0.000000
 10350 0.020 0.011(10%) 0.000000 LEVEL-FL. 0.000000
 NOTES: 1. SOLID CIRCLE INDICATE TRIM POINTS
 2. 54-20 CM. TURBINE INSTALLED (SWIMMED POSITION)

3. TOTAL CONTROL DISPLACEMENT

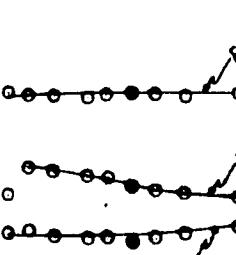
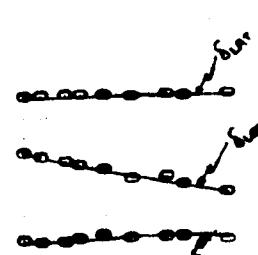
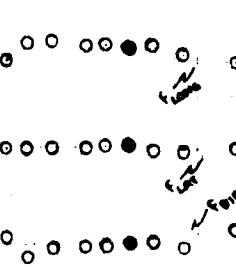
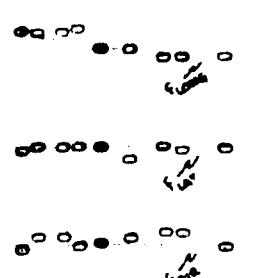
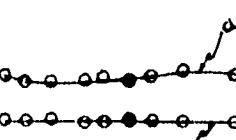
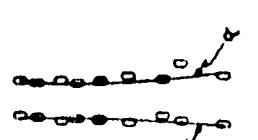
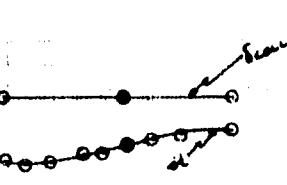
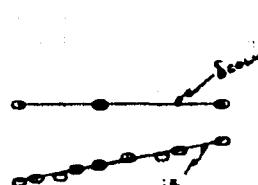
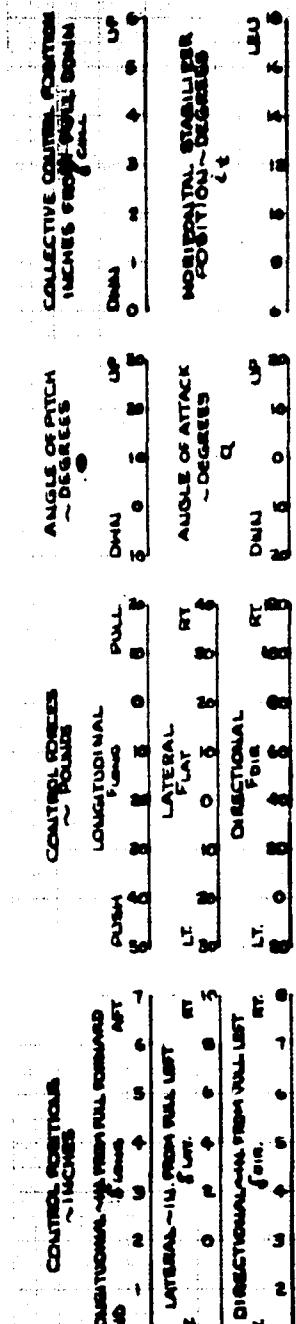
LONGITUDINAL = 10.0 INCHES FROM FULL FORWARD

LATERAL = 1.0 INCHES FROM FULL LEFT

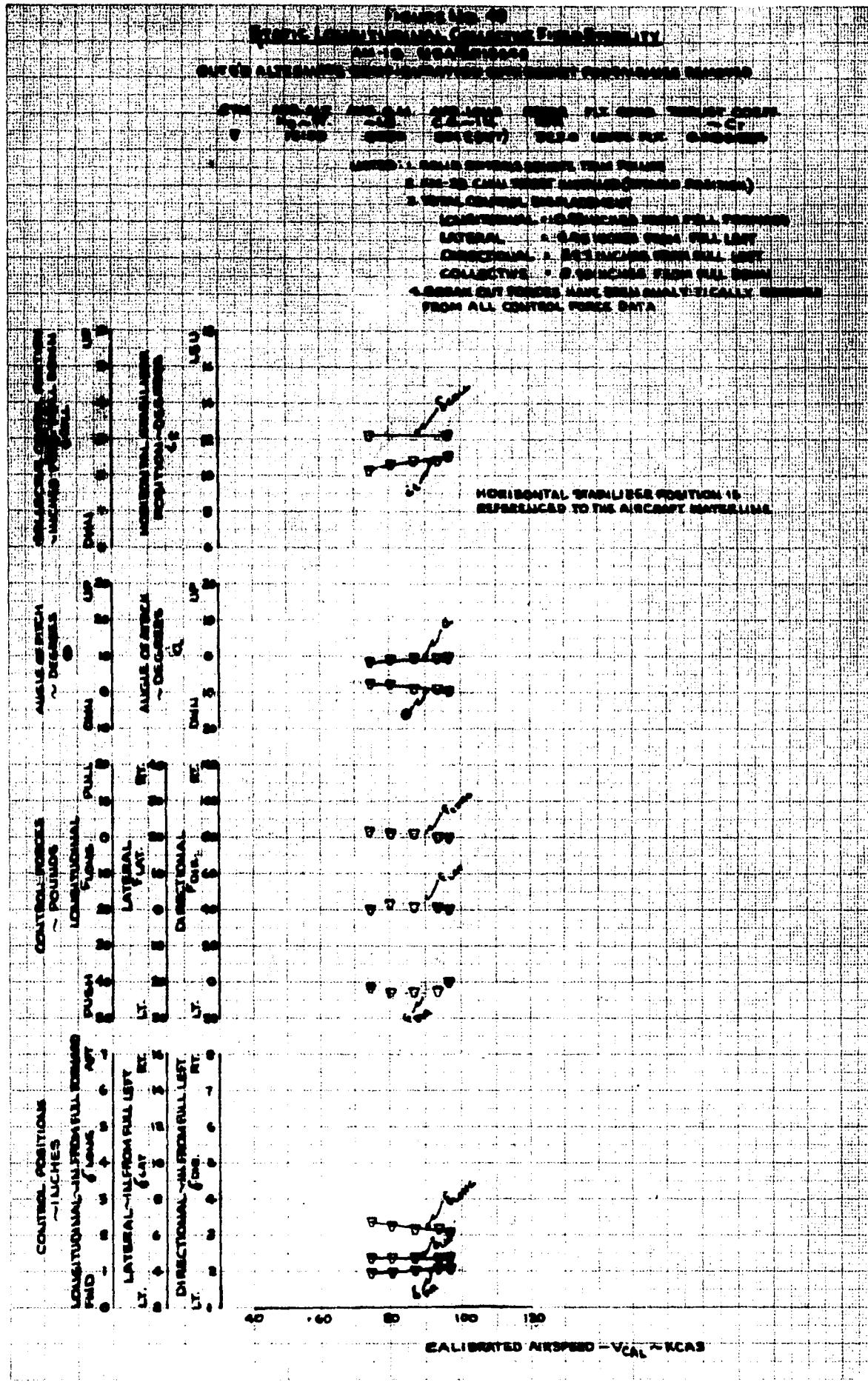
DIRECTIONAL = 5.5 INCHES FROM FULL LEFT

COLLECTIVE = 0.9 INCHES FROM FULL DOWN

4. BREAK AWAY FORCES HAVE BEEN ANALYTICALLY REMOVED
 FROM ALL CONTROL FORCE DATA



CALIBRATED AIRSPEED - V_{CAL} ~ KCAS



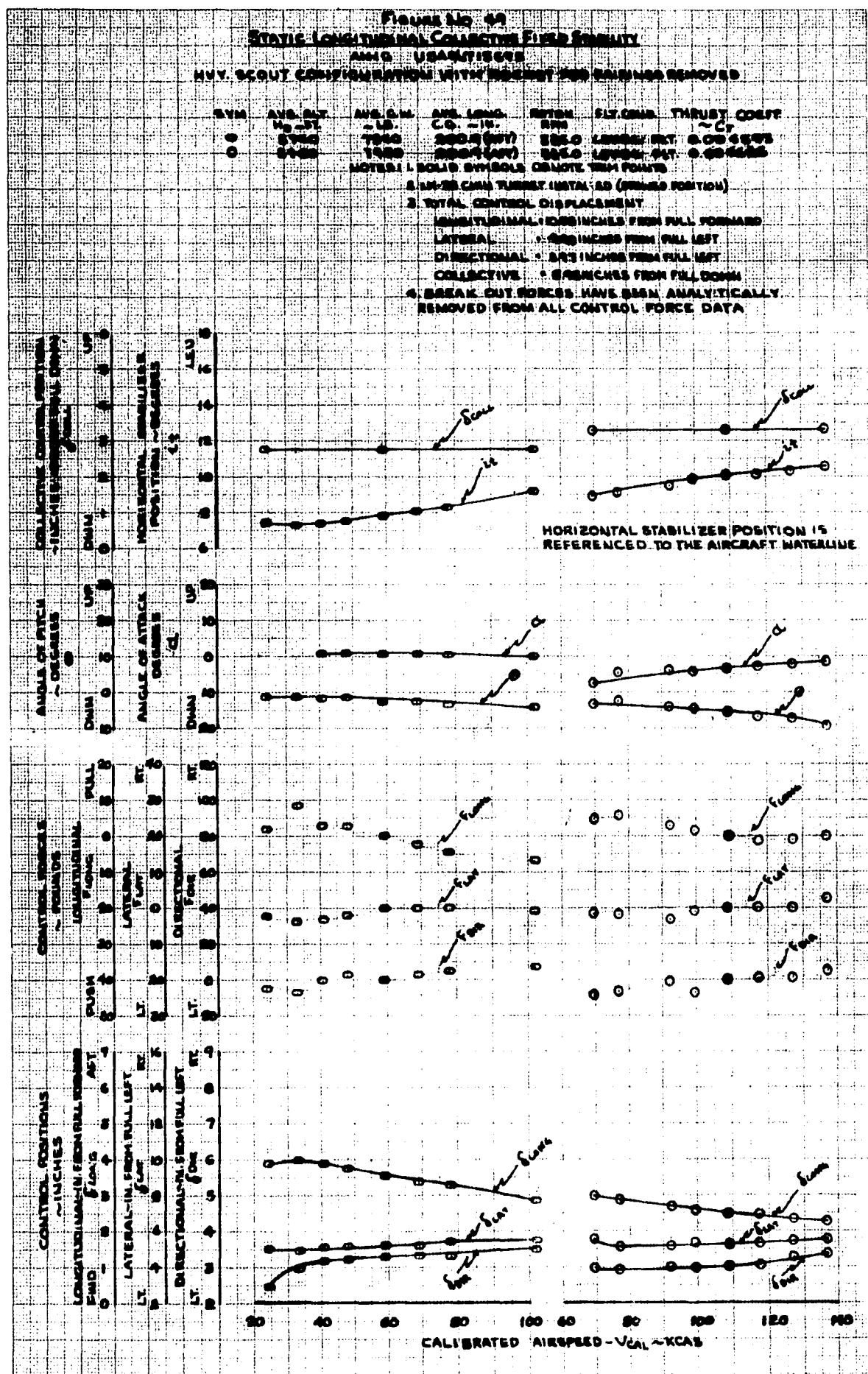


FIGURE No. 50
 STATIC LONGITUDINAL COLLECTIVE FUSELAGE STABILITY
 AN-10 USA SCOUTS
 HVY SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

DATA AVERAGE AVE. LWT. ~18. C.G. ~12.
 50% 8100 201.0(ATT) 826.0 LEVER. FWT. 0.0004641
 50% 8110 201.0(ATT) 834.0 CHME. 0.004624
 NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINTS.

2. XM-20 CHIN TURRET INSTALLED (STOWED POSITION).

3. TOTAL CONTROL DISPLACEMENT

LONGITUDINAL: 1.10 INCHES FROM FULL FORWARD

LATERAL: 1.90 INCHES FROM FULL LEFT

DIRECTIONAL: 2.97 INCHES FROM FULL LEFT

COLLECTIVE: 1.65 INCHES FROM FULL DOWN

4. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED
 FROM ALL CONTROL FORCE DATA

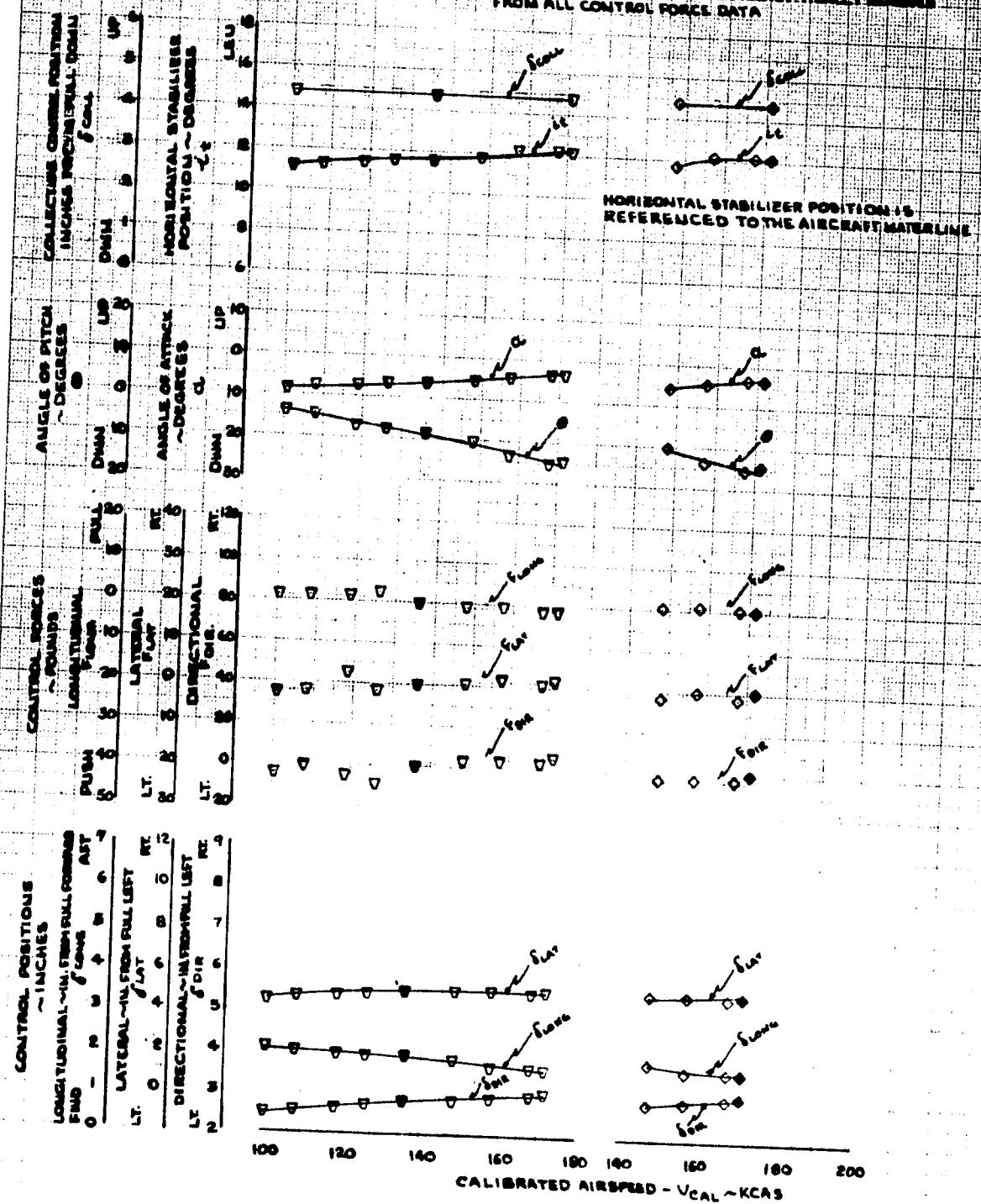


FIGURE NO. 51
STATIC LONGITUDINAL COLLECTIVE FIXED STABILITY
 AH-1G USA 60715695
 HVY. SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM	Avg. Alt. H ₀ ~ FT.	Avg. G.W. ~ LB.	Avg. Long. CG. ~ IN.	Motor RPM	Flt. Cond.	Thrust Coeff.
0	7230	9670	2003(AFT)	324.0	LEVEL FLT.	0.005545
0	6680	9190	2003(AFT)	324.0	LEVEL FLT.	0.005569

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINTS

2. KM-28 CHIN TURRET INSTALLED (STOWED POSITION)

3. TOTAL CONTROL DISPLACEMENT

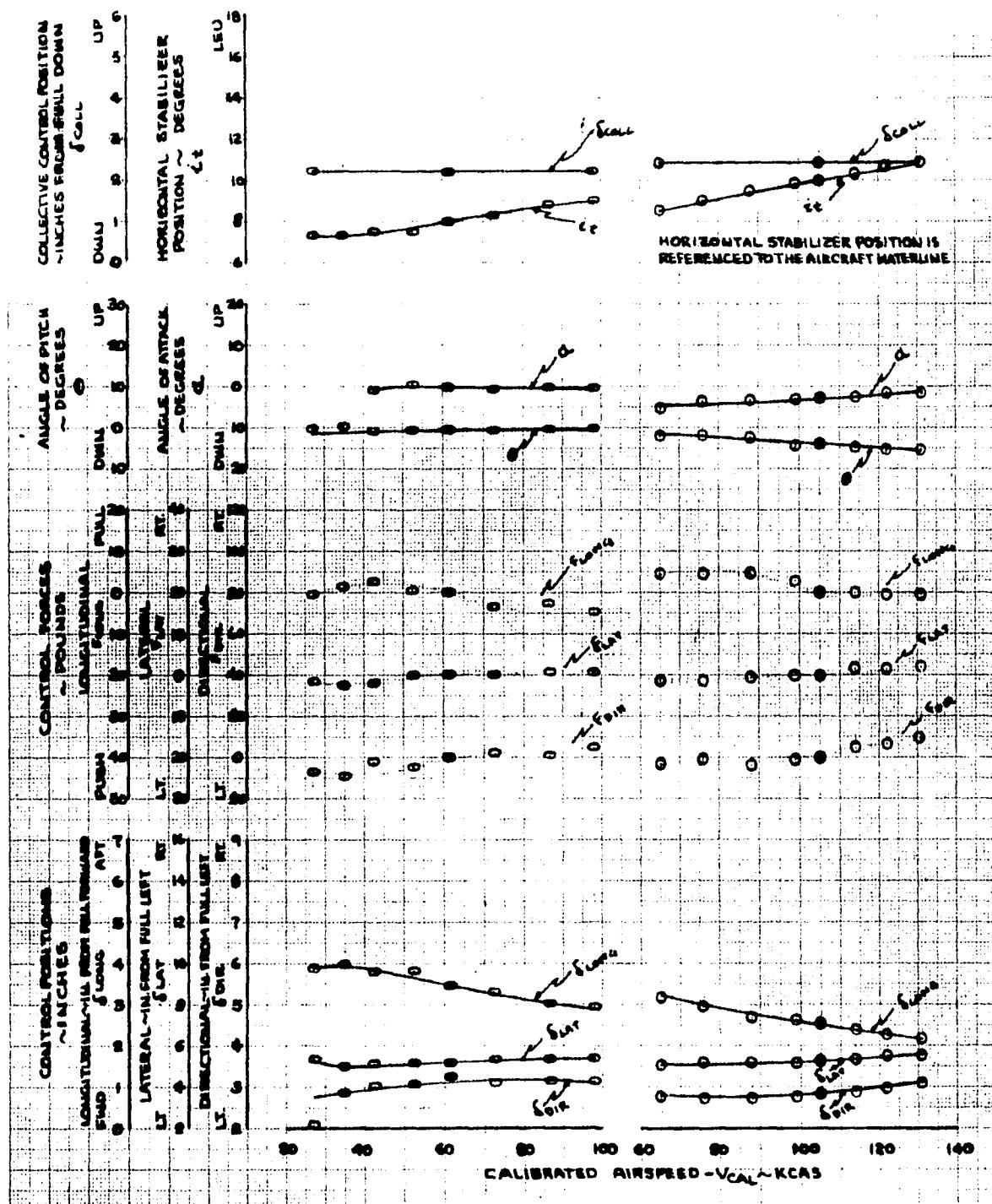
LONGITUDINAL = 100.5 INCHES FROM FULL FORWARD

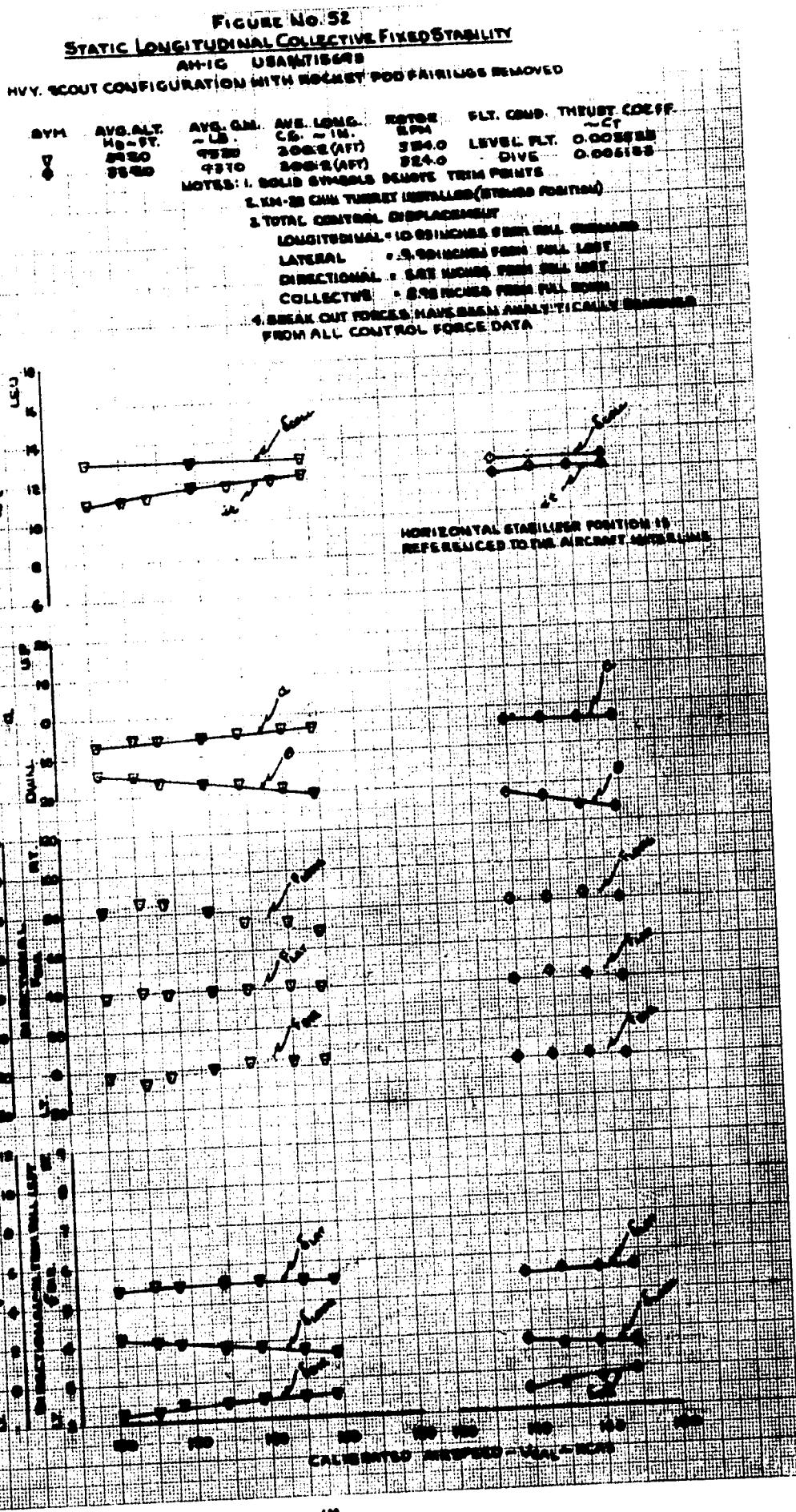
LATERAL = 9.9 INCHES FROM FULL FORWARD

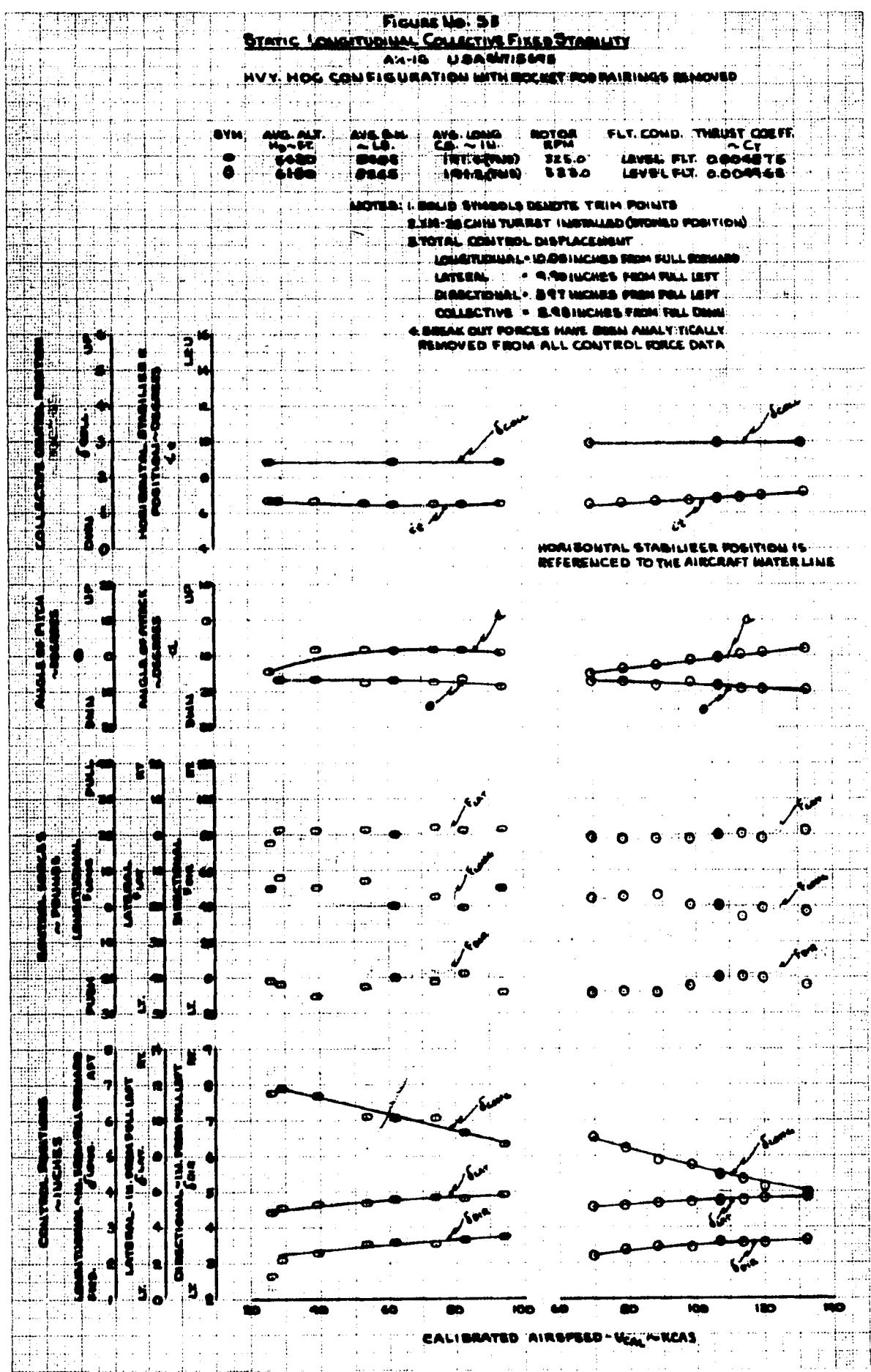
DIRECTIONAL = 5.7 INCHES FROM FULL FORWARD

COLLECTIVE = 8.9 INCHES FROM FULL DOWN

4. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED
 FROM ALL CONTROL FORCE DATA







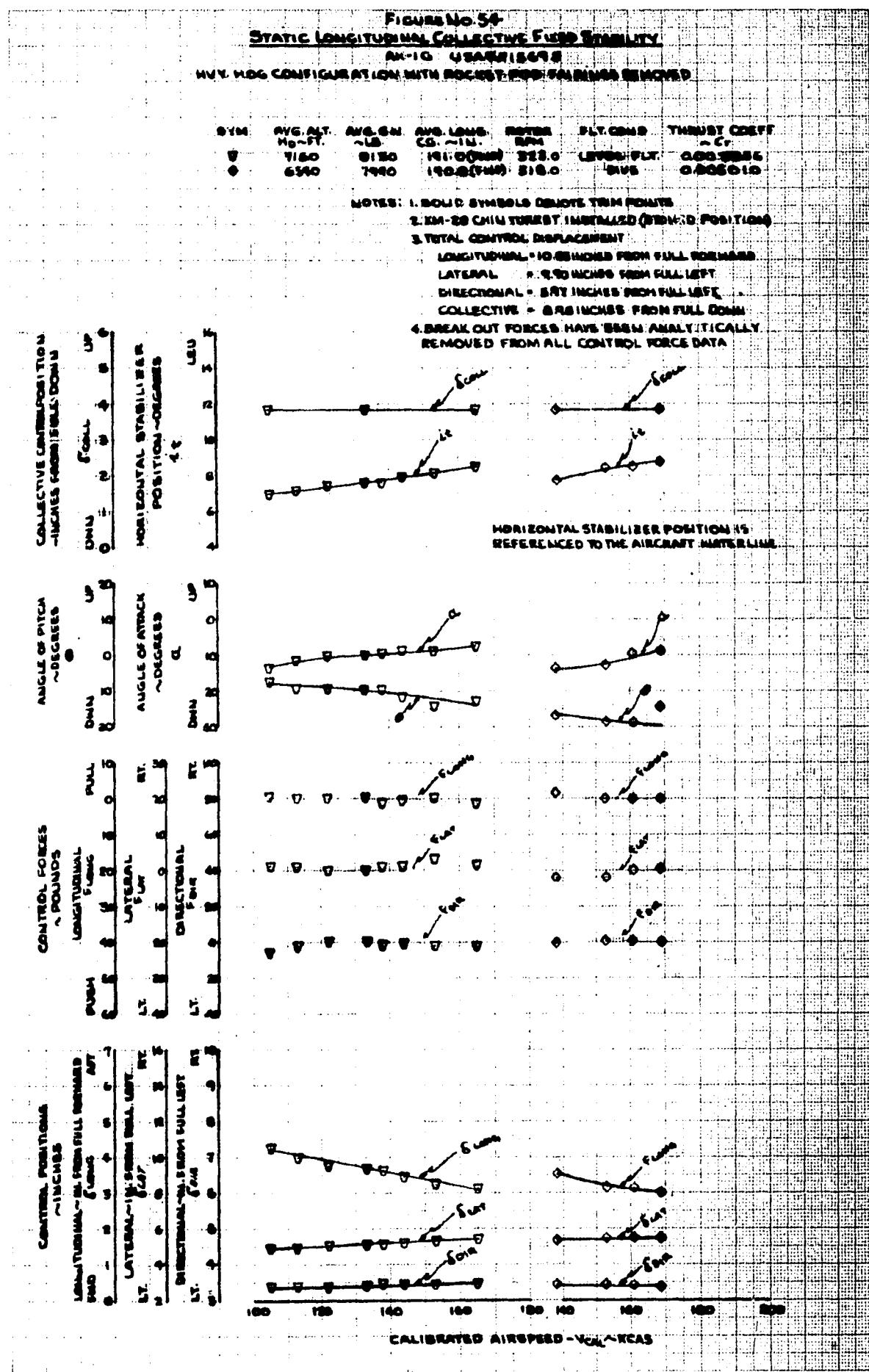
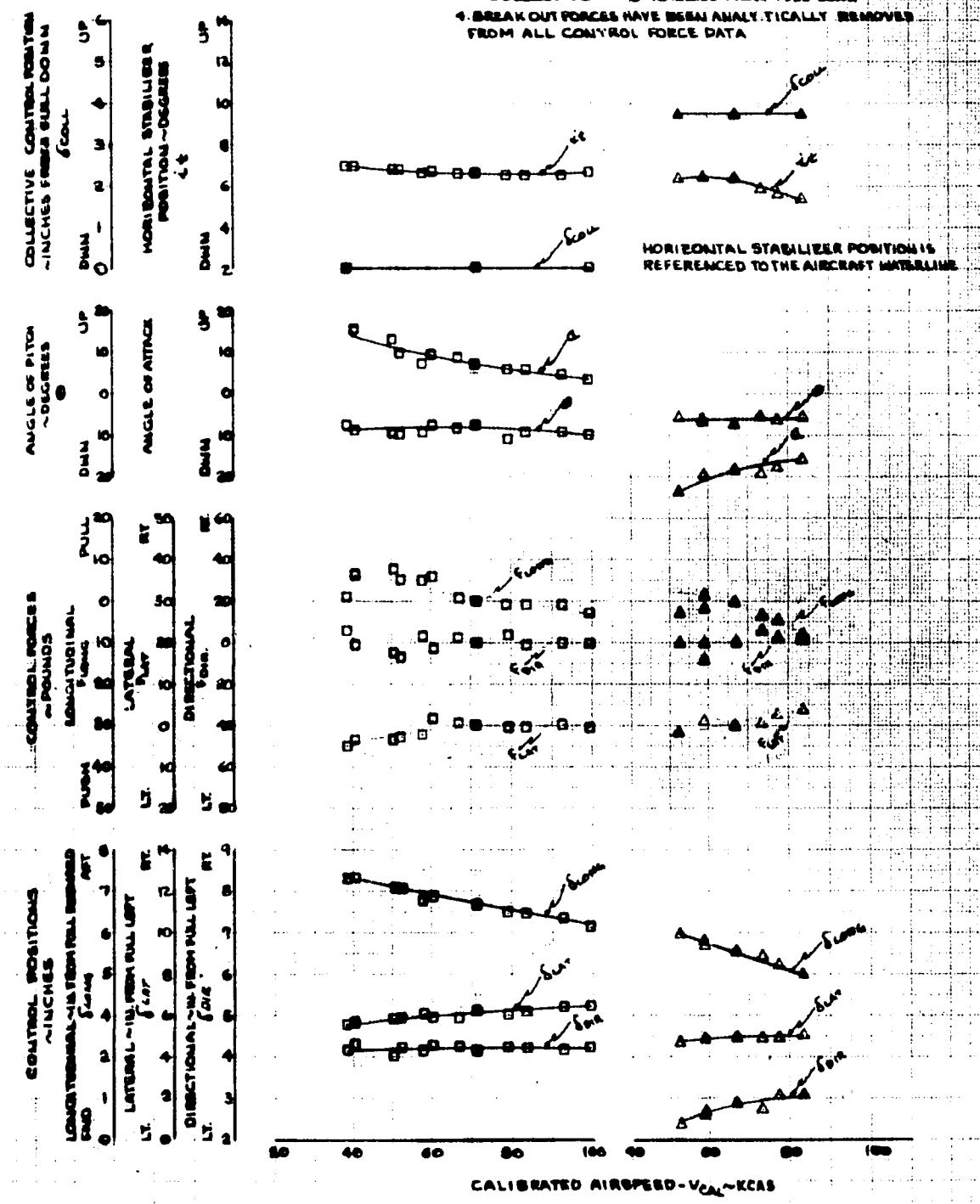


FIGURE NO. 55
STATIC LONGITUDINAL COLLECTIVE FIXED STABILITY
AH-1G USAF 671569S
HUV. HOG CONFIGURATION WITH BOOMET POD FAIRINGS REMOVED

SYM	Avg. Alt. Hd.-FT.	Avg. G.M. ~LB.	Avg. Long. CC.-IN.	ROTOR RPM	Fly. Cond.	Theod. Comp.
▲	7610	7710	10000(BW)	380.0	CLIMB	0.000ST
□	7610	7910	14000(BW)	380.0	AUTOROTATION	0.004ST

NOTES: 1. SOLID SYMBOLS INDICATE TRIM POINTS
 2. E-3B CHIN TURRET INSTALLED (STOWED POSITION)
 3. TOTAL CONTROL DISPLACEMENT
 LONGITUDINAL = 10.93 INCHES FROM FULL FORWARD
 LATERAL = -9.40 INCHES FROM FULL LEFT
 DIRECTIONAL = 8.91 INCHES FROM FULL LEFT
 COLLECTIVE = 8.98 INCHES FROM FULL DOWN
 4. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED
 FROM ALL CONTROL FORCE DATA



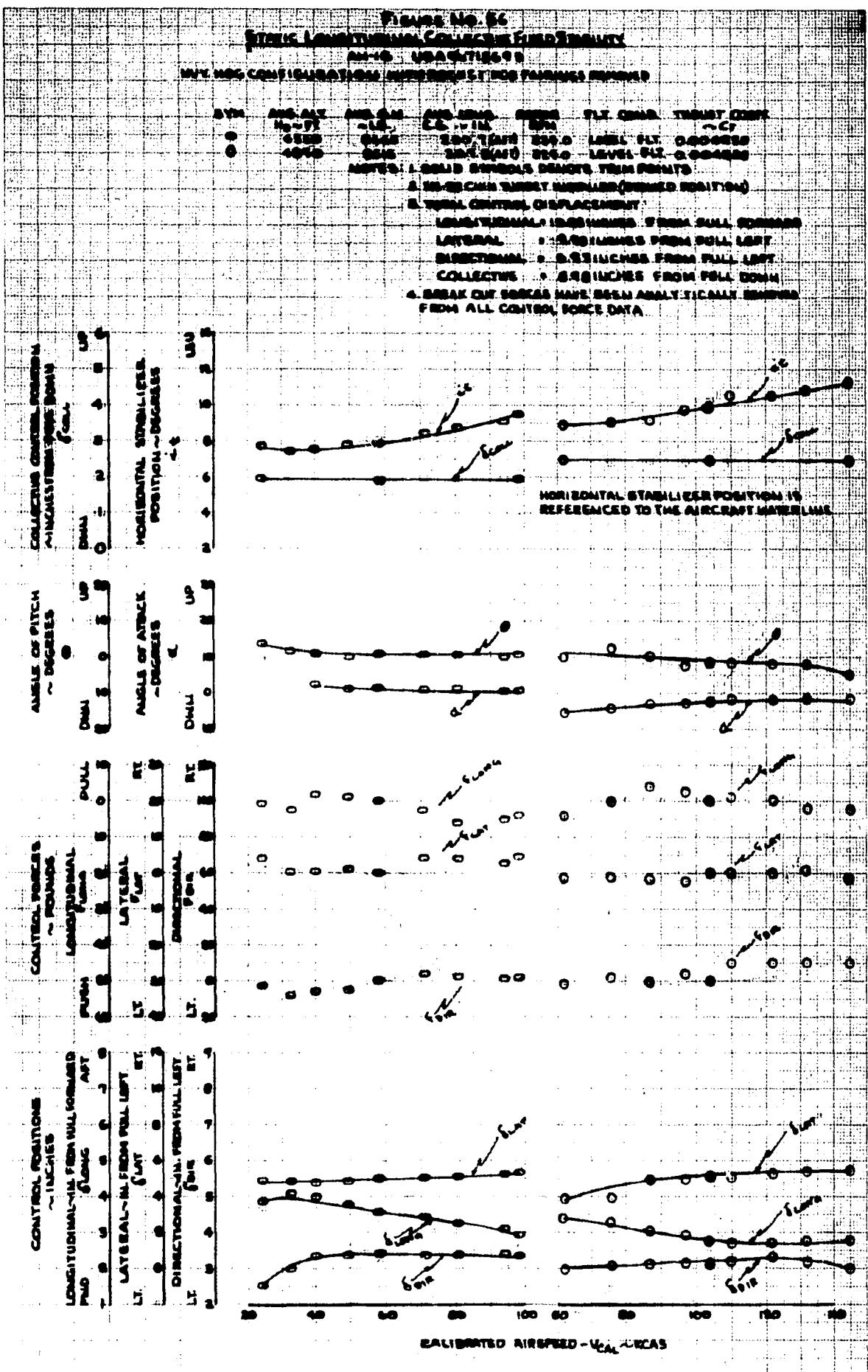


Figure No. 57
STATIC LONGITUDINAL COLLECTIVE FIN STABILITY
 AH-1S USAFT 19678
 HVY HOG CONFIGURATION WITH ROCKET POD PAIRINGS REMOVED

WT. AVG ALT. AVG GM. AVG LOAD. ROTOR RPM. FLT. COMD. THRUST COEF.
 $H_0 = 10^{\circ}$ - LB. C.G. ~11.5' ~2250 LEVEL FLT. 0.005415
 5000 8500 2800(FT) 2250 DIVS 0.020694
 9250 9750 3200(FT) 2850.0

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINTS

2. XM-28 CMU THRUST INSTALLED (STIMED POSITION)

3. TOTAL CONTROL DISPLACEMENT

LONGITUDINAL = 10 DEGREES FROM FULL FORWARD

LATERAL = 10 DEGREES FROM FULL LEFT

DIRECTIONAL = 20 DEGREES FROM FULL LEFT

COLLECTIVE = 5 DEGREES FROM FULL DOWN

4. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED
 FROM ALL CONTROL FORCE DATA

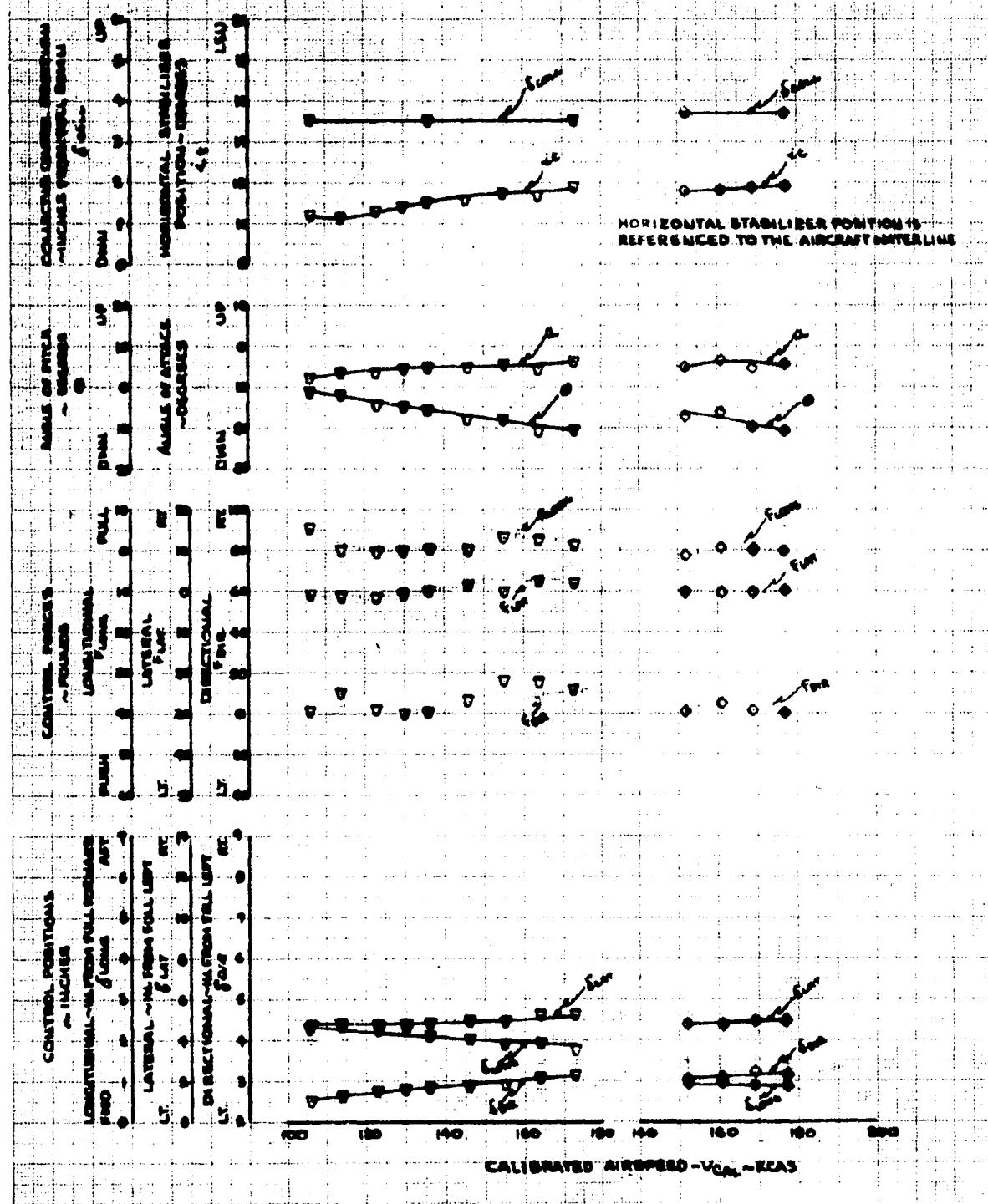


FIGURE NO. 58
STATIC LONGITUDINAL COLLECTIVE FIXED STABILITY
AH-1G URGENTIERS
HVV. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

BVM AVG ALT. AVG QM. AVG LONG. MOTOR FLT. COND. THRUST COEFF.
HOFT. 6000 0.015 0.015 3200.0 ~C_T
6000 0.015 0.015 3200.0 CLIMB 0.000003
6000 0.015 0.015 3200.0 AUTOROTATION 0.000003

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINTS

2 X-28 CHIN TURRET INSTALLED (STORED POSITION)

& TOTAL CONTROL DISPLACEMENT

LONGITUDINAL • 10.85 INCHES FROM FULL FORWARD

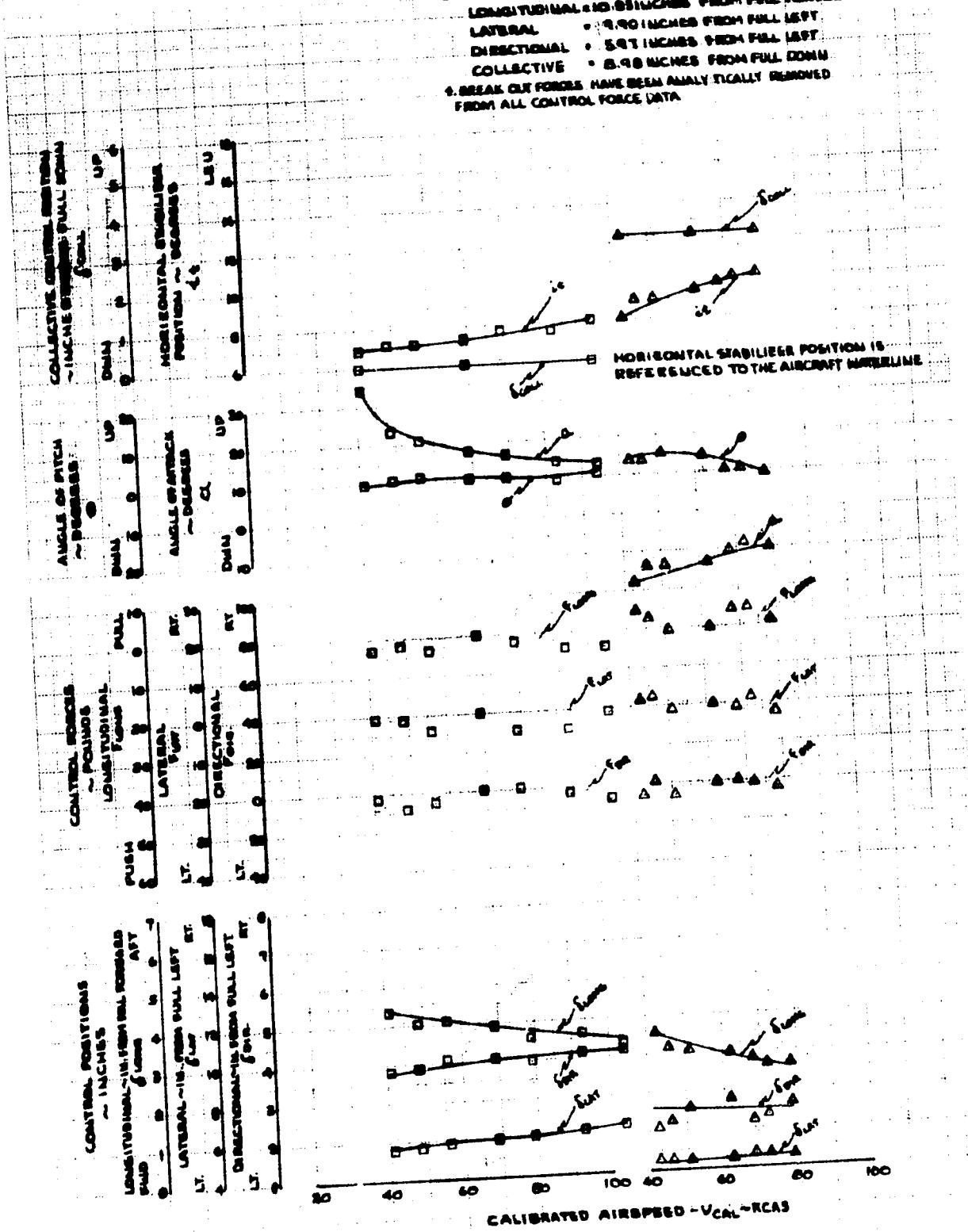
LATERAL • 9.90 INCHES FROM FULL LEFT

DIRECTIONAL • 5.91 INCHES FROM FULL LEFT

COLLECTIVE • 8.98 INCHES FROM FULL DOWN

3. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED

FROM ALL CONTROL FORCE DATA



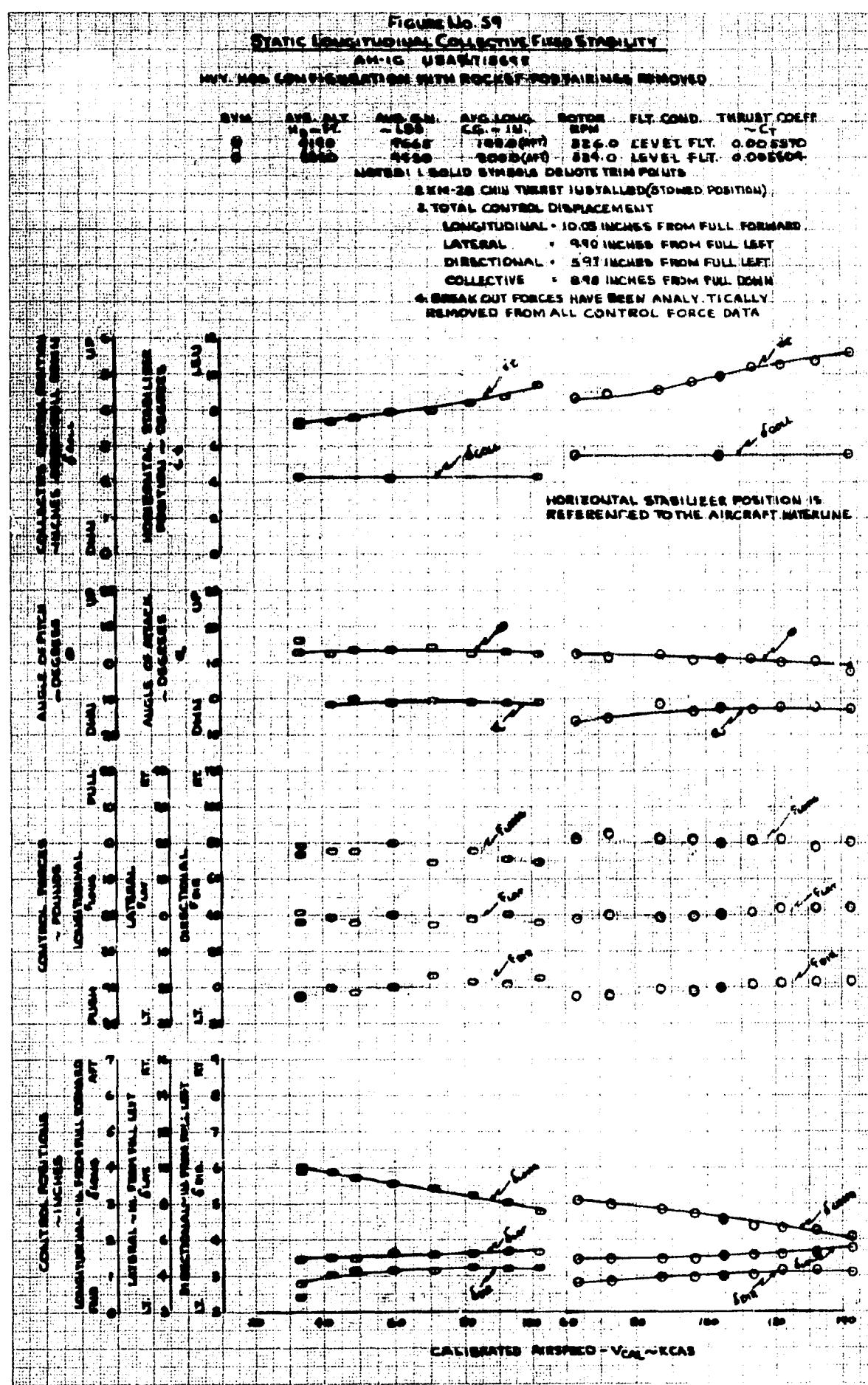


FIGURE NO. 60
 STATIC LONGITUDINAL COLLECTIVE CYCLE STABILITY
 AM-10 USAF 210002Z
 HUV, ADD CONFIGURATION WITH ROCKWELL PROPELLERS REMOVED

SYM. ALT. 4000 ft. AVG. L. 1000 RPM. Rotor 2000 LEVEL FLG. THRUST CRUSE.
 0310 1000 0000(0) 2000 ~C^o
 4000 1000 0000(0) 2000 0000 0000

NOTES: L=1000 RPM=1000 RPM. TBL PWR=0

2X6-10 CMM TURBINE MACHINES (THREE POSITION)

& TOTAL CENTRAL OIL PLACEMENT

MOMENTUM: 1. 1000 RPM FROM FULL DOWN

LATERAL: 1. 0.0000 FROM FULL LEFT

ROTATIONAL: 0.0000 FROM FULL LEFT

COLLECTIVE: 0.0000 FROM FULL DOWN

2. BREAK OUT FORCES HAVE BEEN ANALYTICALLY

REMOVED FROM ALL CONTROL FORCE DATA

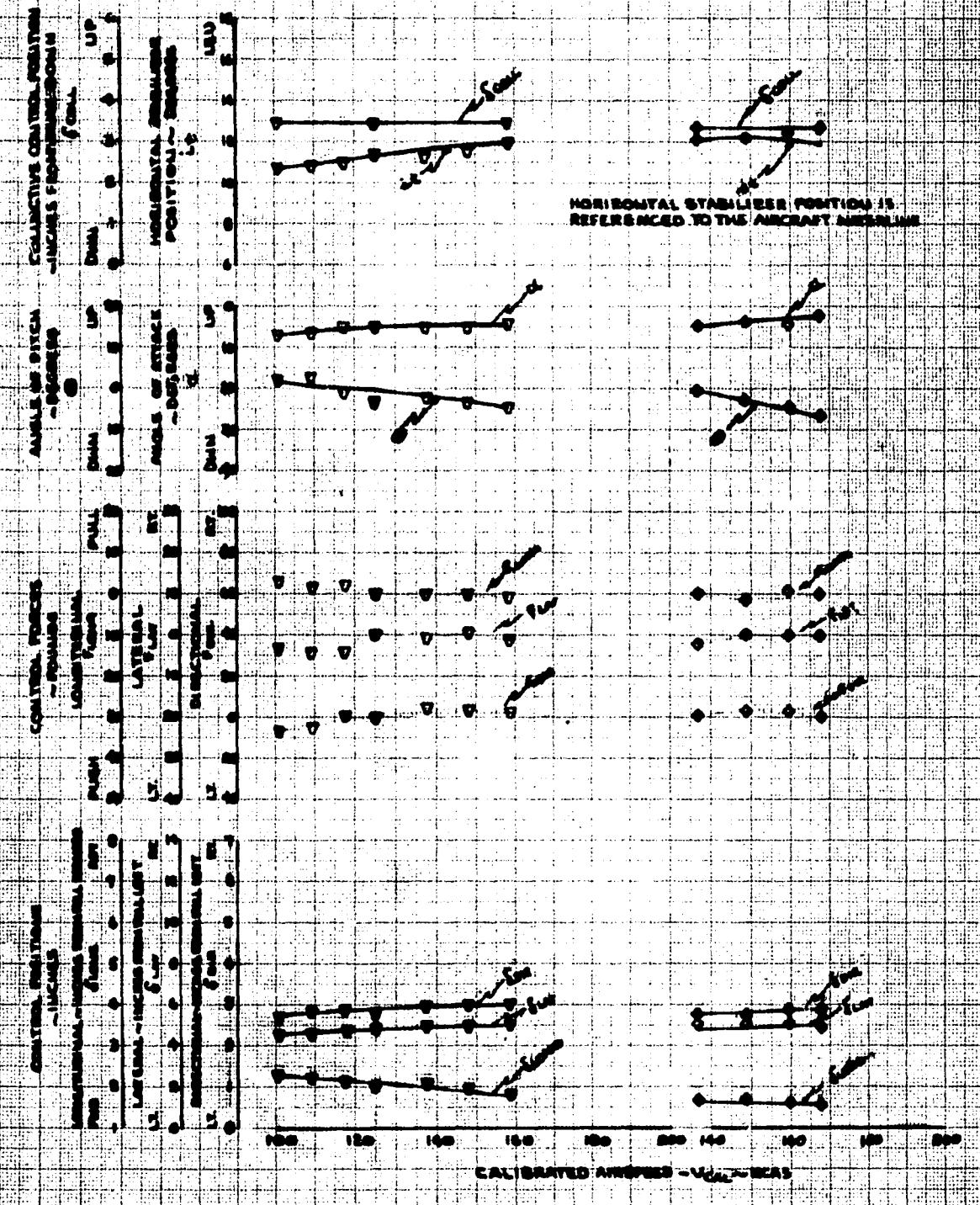
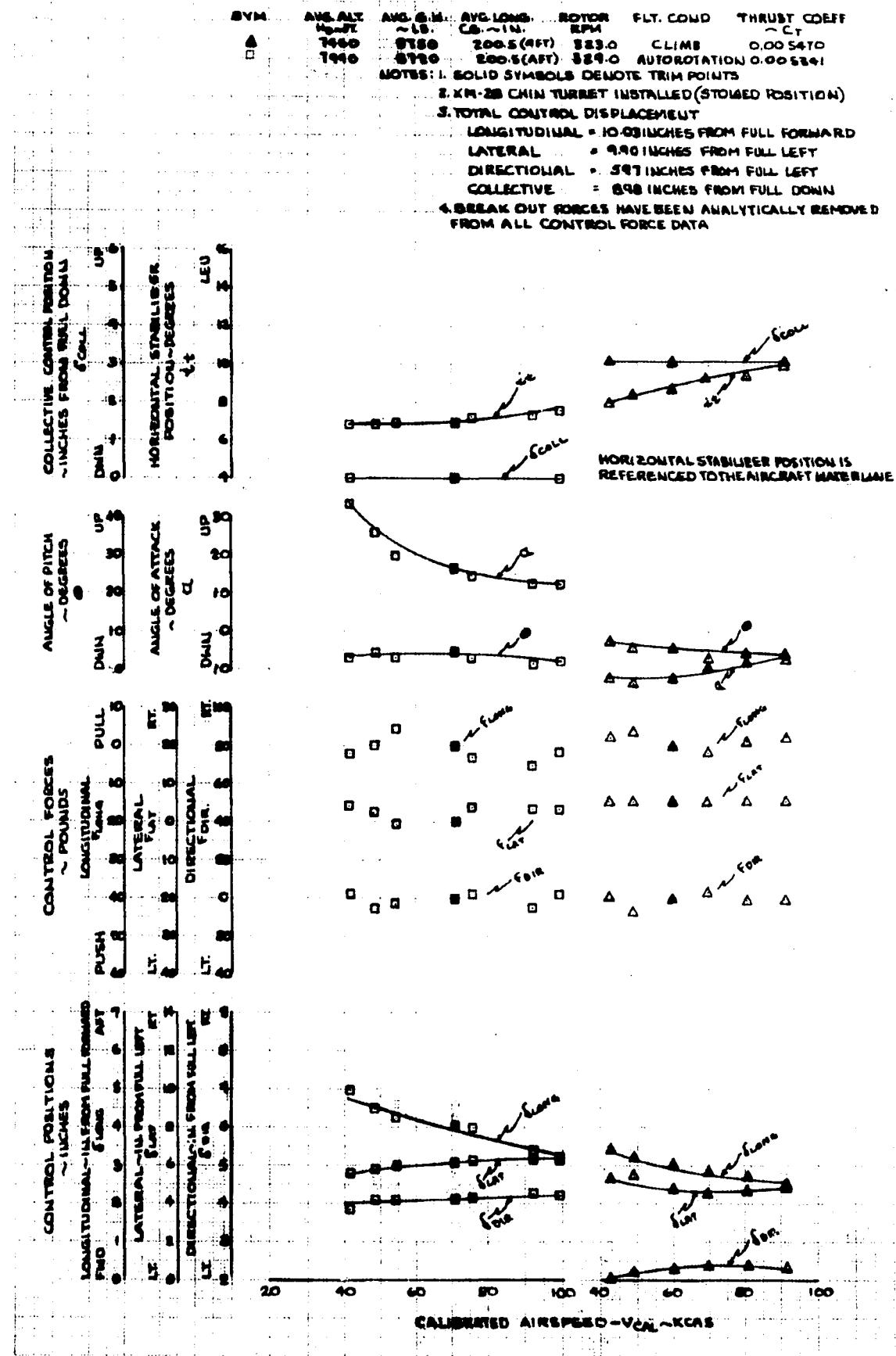


FIGURE NO. 61
STATIC LONGITUDINAL COLLECTIVE FIXED STABILITY
AH-1G USAF 71505
HVV. MOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED



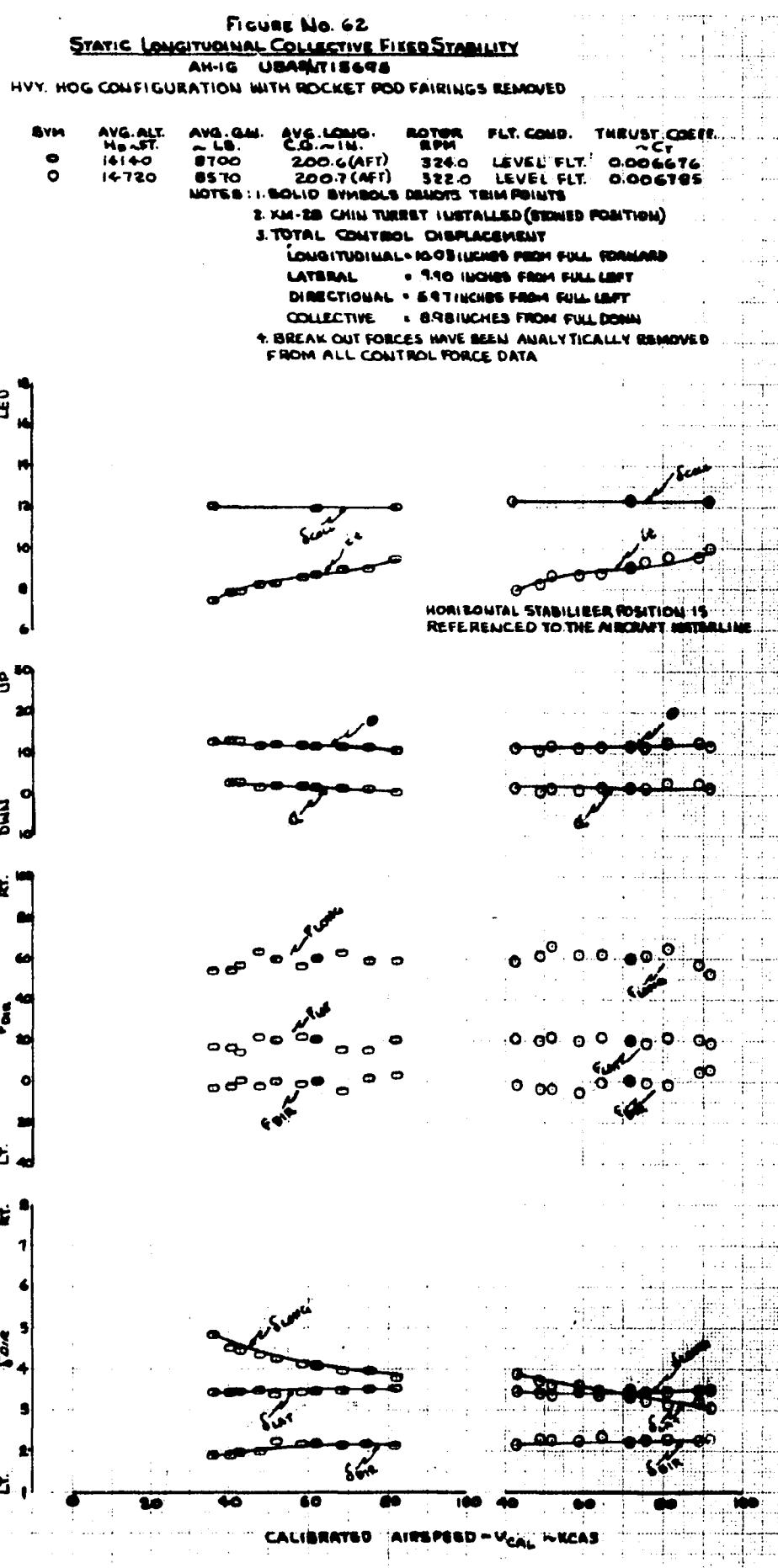
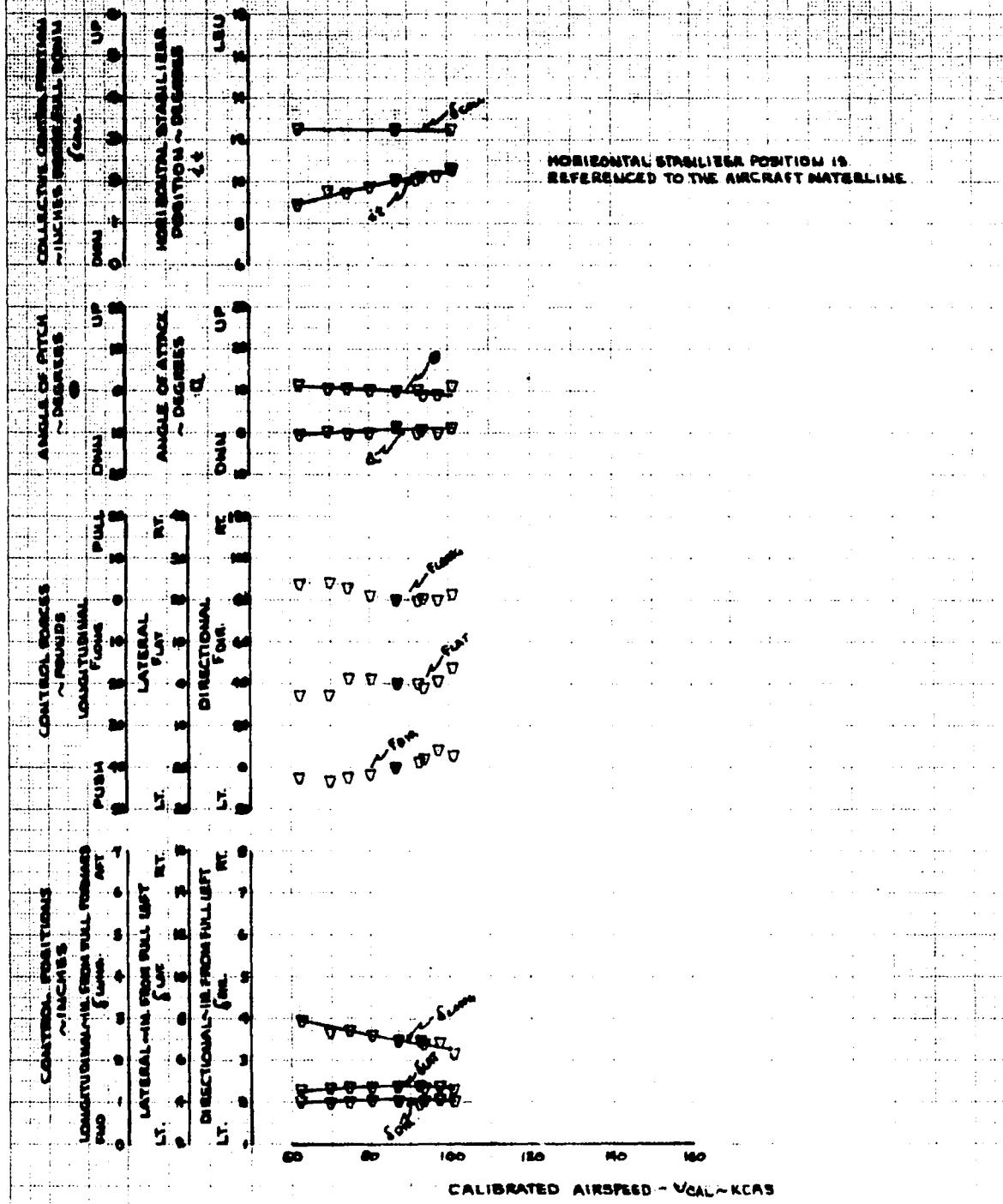


FIGURE NO. 63
STATIC LONGITUDINAL COLLECTIVE FIXED STABILITY
AH-1G UGARZ1669B

HUV-NOS CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED.

SYM. AVE ALT. AVE G.M. AVE. AHEAD. MOTOR ALT. COMP. THRUST COEF.
MOTOR - 10000 FT. 60 IN. 80% 0.0006713
10000 0.0006713 (RAFT) 0.0006713

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINTS.
2. KM-98 CHUTEREST INSTALLED (UPWARD POSITION).
3. TOTAL CONTROL DISPLACEMENT
LONGITUDINAL - 1000 INCHES FROM FULL FORWARD
LATENT - 800 INCHES FROM FULL LEFT
DIRECTIONAL - 800 INCHES FROM FULL LEFT
COLLECTIVE - 800 INCHES FROM FULL DOWN
4. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED
FROM ALL CONTROL FORCE DATA



HORIZONTAL STABILIZER POSITION IS REFERENCED TO THE AIRCRAFT MATERLINE.

FIGURE NO. 64
STATIC LONGITUDINAL COLLECTIVE FIXED STABILITY

AH-1G USAF 61-5901
 CLEAN CONFIGURATION WITH SKID TUBE FAIRINGS REMOVED

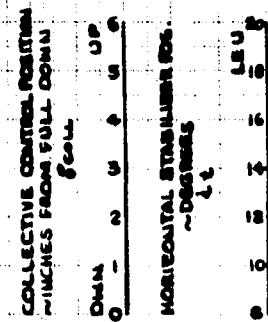
SYM. AVG. ALT. AVG. G.M. AVG. LONG. MOTOR THRUST COEFF. FLZ. CONST.
 $H_0 = 57$ ~14. C.G. = 18. RPM ~CT
 ✓ 5160 8640 149.1(FT) 522.0 0.004478 LEVEL FLT.
 ○ 4570 8370 149.1(FT) 522.0 0.004581 DIVE

- NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINTS
 2. TATROS CHIN TURRET INSTALLED (STOVED POSITION)

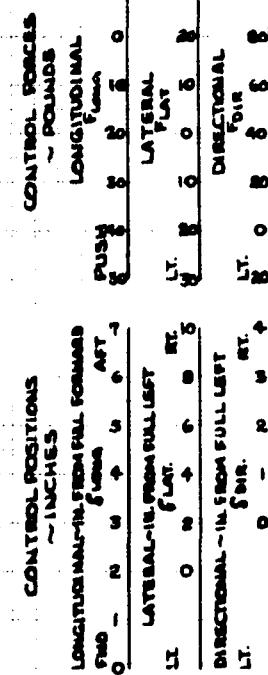
3. TOTAL CONTROL DISPLACEMENT
 LONGITUDINAL - 9.07 IN. FROM FULL FORWARD
 LATERAL - 10.00 IN. FROM FULL LEFT
 DIRECTIONAL - 7.07 IN. FROM FULL LEFT

COLLECTIVE - 7.9.80 IN FROM FULL DOWN
 4. BREAK OUT FORCES HAVE BEEN ANALYTICALLY
 REMOVED FROM ALL CONTROL FORCE DATA

HORIZONTAL STABILIZER POSITION IS
 REFERENCED TO THE AIRCRAFT WATERLINE



ANGLE OF ATTACK INOPERATIVE



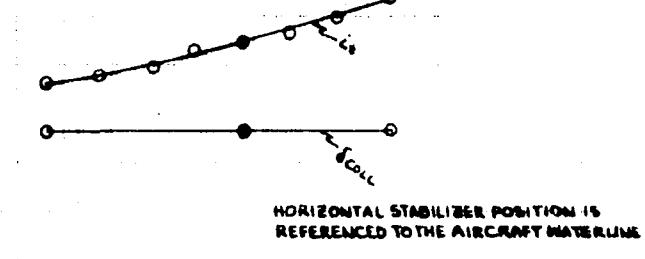
CALIBRATED AIRSPEED - V_{CAL} IN KCAS

FIGURE NO. 65
STATIC LONGITUDINAL COLLECTIVE FIXED STABILITY

AH-1G USA #615267
 CLEAN CONFIGURATION WITH SKID TUBE FAIRINGS REMOVED

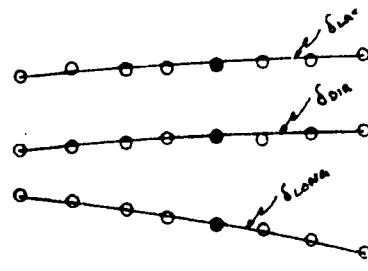
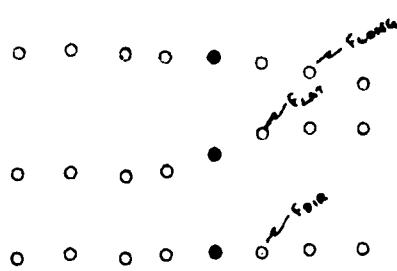
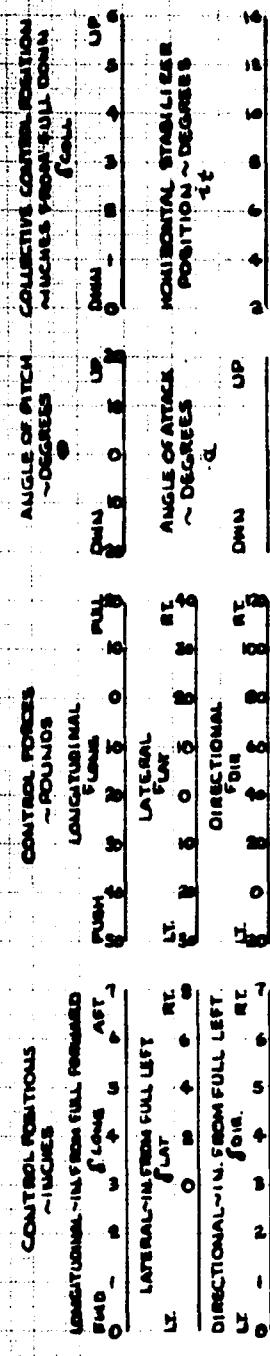
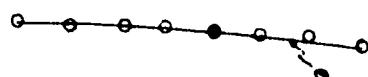
SVM AVG. ALT. AVG. GM. AVG. LONG. MOTOR THRUST CONST. FLT. COND.
 HGT ~91' ~LA C.G. ~IN. RPM ~CT
 0 6170 0385 199.0(FT) 322.0 0004415 LEVEL FLY.

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINTS
 2. STAT 103 CMN TURRET INSTALLED (STOWED POSITION)
 3. TOTAL CONTROL DISPLACEMENT
 LONGITUDINAL - 9.0 IN. FROM FULL FORWARD
 LATERAL - 10.0 IN. FROM FULL LEFT
 DIRECTIONAL - 10.0 IN. FROM FULL LEFT
 COLLECTIVE - 9.0 IN. FROM FULL DOWN
 4. BREAK-OUT FORCES HAVE BEEN ANALYTICALLY
 REMOVED FROM ALL CONTROL FORCE DATA



HORIZONTAL STABILIZER POSITION IS
 REFERENCED TO THE AIRCRAFT WATERLINE

ANGLE OF ATTACK INOPERATIVE



CALIBRATED AIRSPEED - V_{CAL} - KCAS

FIGURE NO. 66
SUMMARY OF LATERAL DIRECTIONAL STABILITY

AM-1G USAF 511668

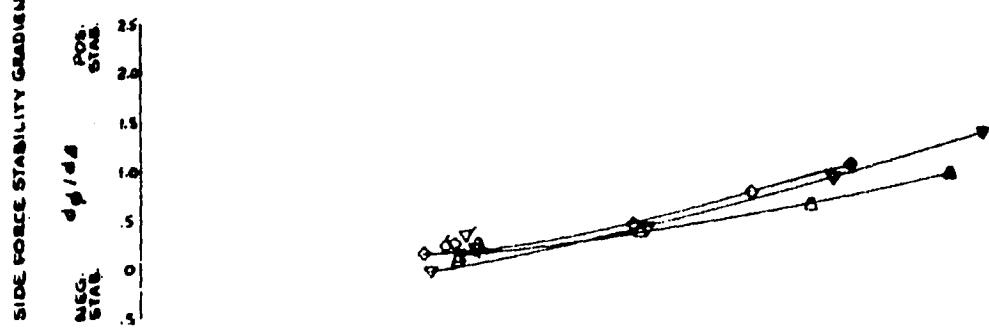
GROSS WEIGHT COMPARISON

SYM	AM ALT.	AM GENT.	AM LONG.	AMR 6000	THRUST CRSS.	CONFIGURATION
○	6000	6100	200.0(FT)	322.5	0.0004	MVY. HOG
△	8170	9466	200.0(FT)	322.0	0.000550	MVY. HOG
▽	4730	7765	201.3(FT)	322.0	0.000581	MVY. HOG

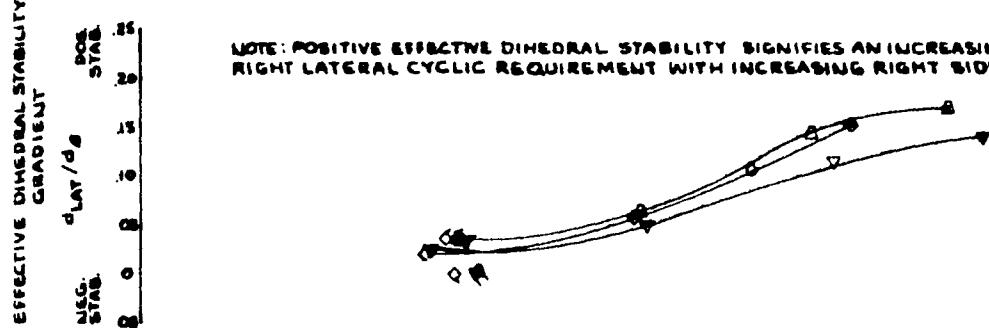
NOTES: 1. POINTS DERIVED FROM FIGURES 82 THROUGH 92.
 APPENDIX III

2. OPEN SYMBOLS DENOTE LEVEL FLIGHT
3. CROSSED SYMBOLS DENOTE DIVE
4. FLAGGED SYMBOLS DENOTE CLIMB
5. TAILED SYMBOLS DENOTE AUTOROTATION

NOTE: POSITIVE ROLL ATTITUDE STABILITY SIGNIFIES INCREASING RIGHT BANK ANGLE
 WITH INCREASING RIGHT SIDE-SLIP



NOTE: POSITIVE EFFECTIVE DIHEDRAL STABILITY SIGNIFIES AN INCREASING
 RIGHT LATERAL CYCLIC REQUIREMENT WITH INCREASING RIGHT SIDE-SLIP



NOTE: POSITIVE DIRECTIONAL STABILITY SIGNIFIES AN INCREASING LEFT
 DIRECTIONAL CONTROL REQUIREMENT WITH INCREASING RIGHT SIDE-SLIP

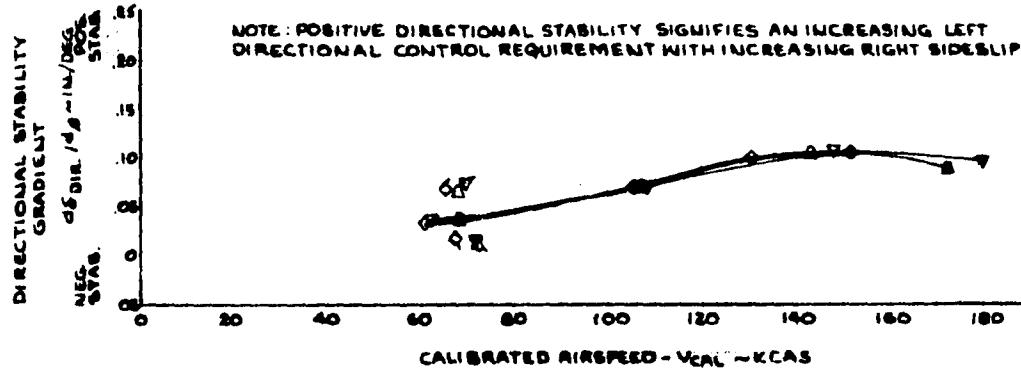
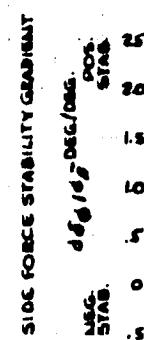


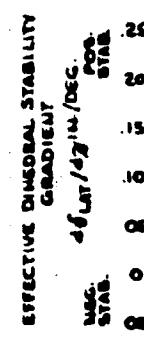
FIGURE NO. 67
SUMMARY OF LATERAL DIRECTIONAL STABILITY
AH-1G USAW156RS
C.G. & CONFIGURATION COMPARISON

SYM.	Avg. ALT. ft.	Avg. GRNT. in./sec.	Avg. LONG. in./sec.	ROTOR C. of. I. - IN. (APT)	THRUST CONST. lb.	CONFIGURATION
O	5000	8240	144.2(FWD)	323.0	0.004685	CLEAN
□	6070	8080	191.1(FWD)	326.5	0.004748	HUV. HOG
◊	6080	8310	200.9(APT)	323.5	0.004970	HUV. HOG
△	6010	8680	200.7(APT)	326.5	0.005085	OUT'D ALTERNATE
○	6750	8330	201.0(APT)	323.0	0.005085	HUV. SCOUT

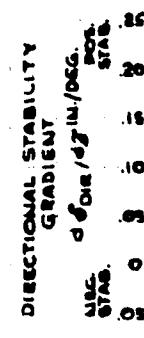
NOTES: 1. POINTS DERIVED FROM FIGURES 70 THROUGH 81
 AND 85 THROUGH 97, APPENDIX E
 2. OPEN SYMBOLS DENOTE LEVEL FLIGHT
 3. CROSSED SYMBOLS DENOTE DIVE
 4. FLAGGED SYMBOLS DENOTE CLIMB
 5. TAILED SYMBOLS DENOTE AUTOROTATION



NOTE: POSITIVE ROLL ATTITUDE STABILITY SIGNIFIES INCREASING RIGHT BANK ANGLE WITH INCREASING RIGHT SIDESLIP



NOTE: POSITIVE EFFECTIVE DIHEDRAL STABILITY SIGNIFIES AN INCREASING RIGHT LATERAL CYCLIC REQUIREMENT WITH INCREASING RIGHT SIDESLIP



NOTE: POSITIVE DIRECTIONAL STABILITY SIGNIFIES AN INCREASING LEFT DIRECTIONAL CONTROL REQUIREMENT WITH INCREASING RIGHT SIDESLIP

CALIBRATED AIRSPEED - V_{CAL} - KCAS

FIGURE NO. 68
SUMMARY OF LATERAL DIRECTIONAL STABILITY
AH-1G USA/TIGER
ALTITUDE COMPARISON

SYN.	Avg. ALT. ft.	Avg. GRWT. lb.	Avg. LONG. C.G. ~IN.	ROT. THRUST COEF.	CONFIGURATION
1.0	6000	8810	200.4(alt) 323.5	0.002470	HUV. HOG
2.0	14600	8810	200.8(alt) 324.0	0.006617	HUV. HOG

- NOTES: 1. POINTS DERIVED FROM FIGURES 85 THROUGH 92 AND 91 THROUGH 93, APPENDIX III
 2. OPEN SYMBOLS DENOTE LEVEL FLIGHT
 3. CROSSED SYMBOLS DENOTE DIVS
 4. FLAGGED SYMBOLS DENOTE CLIMB
 5. TAILED SYMBOLS DENOTE DESCENT

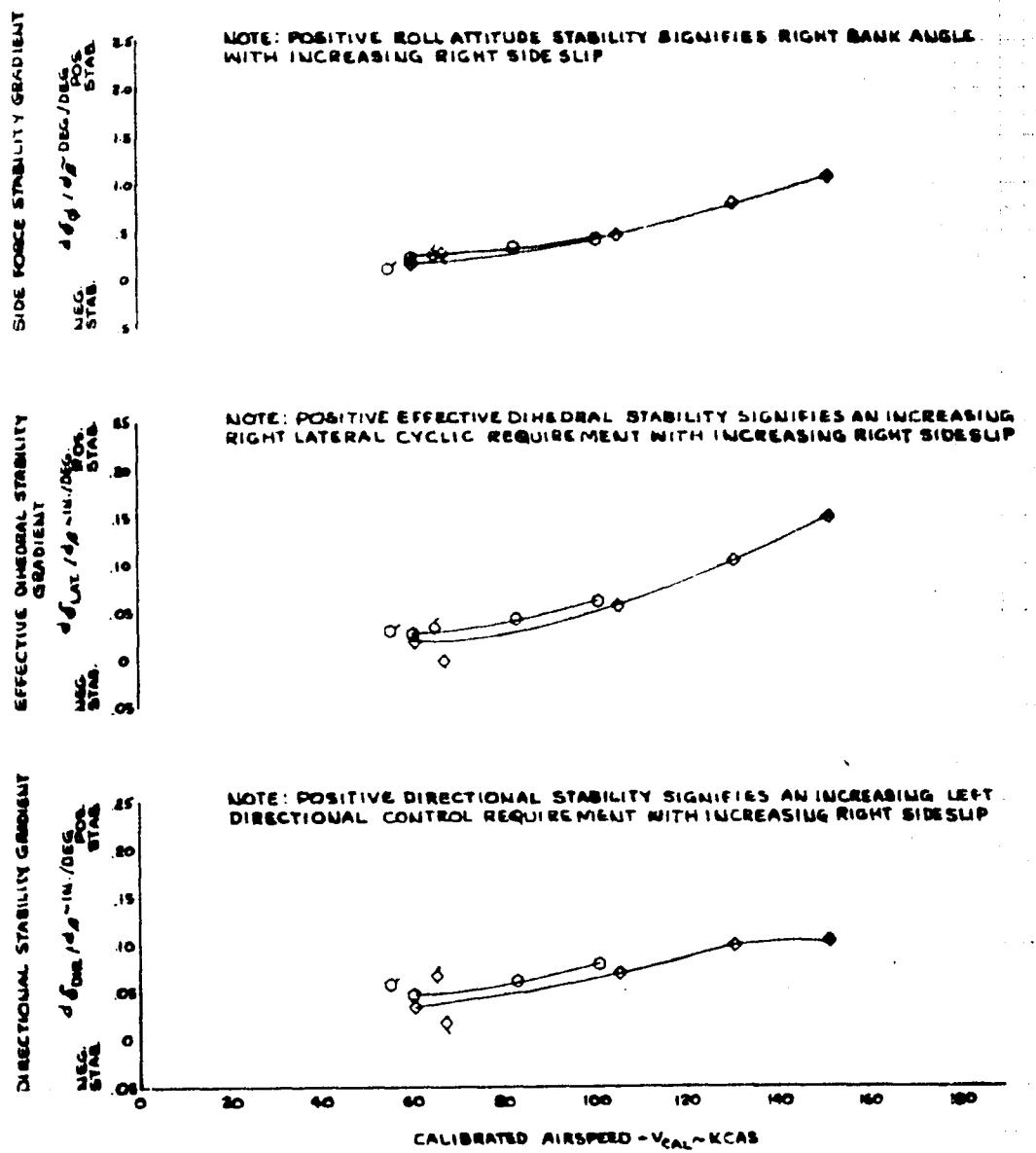


Figure No. 6A
SUMMARY OF LATERAL DIRECTIONAL STABILITY
AH-1G

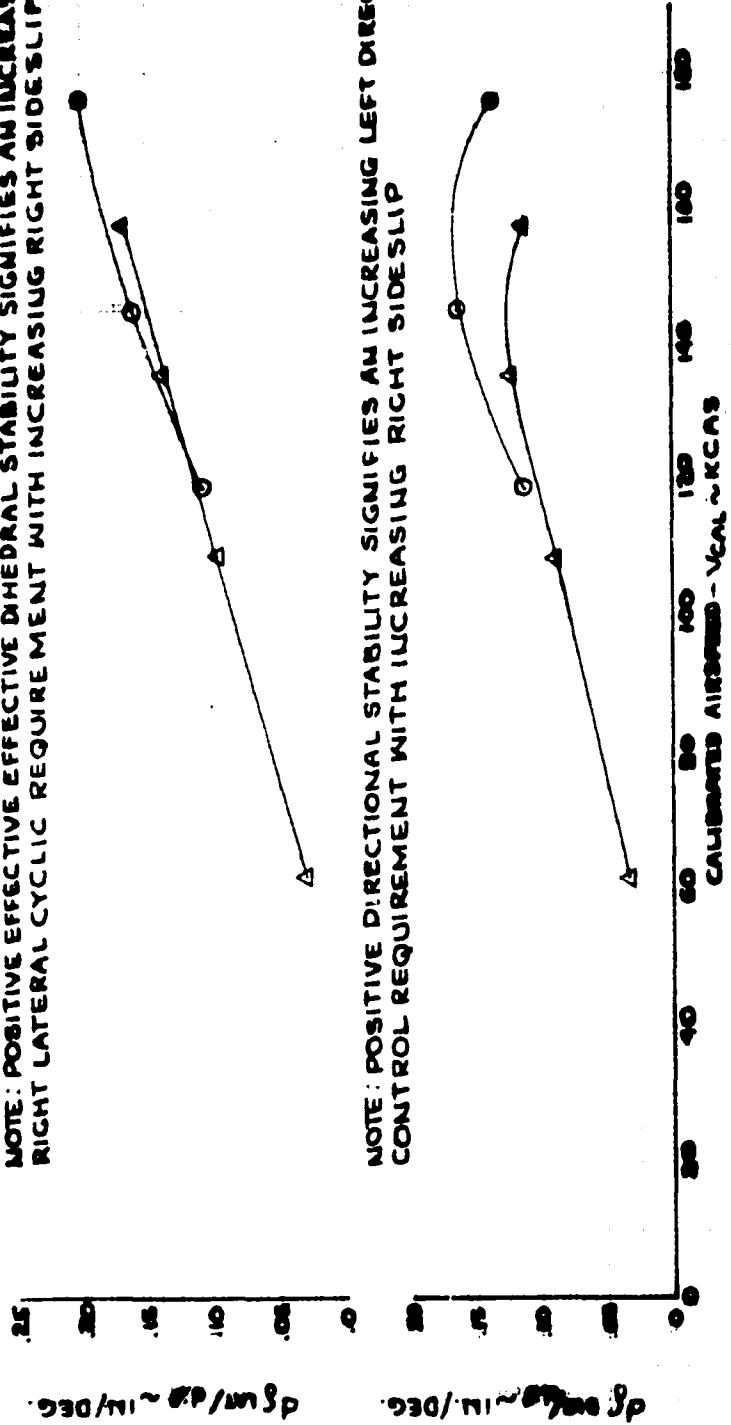
SYM	AVG. ALT. MS - FT	AVG. G.M. ~LS	ROTOR RPM	THrust Coeff. Configuration -C _T	AIRFOIL
O	5700	8770	200.5(ART)	323.0	CLEAN (LANDING GEAR CROSS TUBE FAIRINGS RETRACTED)
A	8400	8290	199.2(ART)	323.0	CLEAN

NOTE: POINTS DERIVED FROM FIGURES 70, 71, 94 & 95, APP III

2. OPEN SYMBOLS DENOTE LEVEL FLIGHT

3. CROSSED SYMBOLS DENOTE DIVE

NOTE: POSITIVE EFFECTIVE DIHEDRAL STABILITY SIGNIFIES AN INCREASING
RIGHT LATERAL CYCLIC REQUIREMENT WITH INCREASING RIGHT SIDESLIP



NOTE: POSITIVE DIRECTIONAL STABILITY SIGNIFIES AN INCREASING LEFT DIRECTIONAL
CONTROL REQUIREMENT WITH INCREASING RIGHT SIDESLIP

FIGURE NO. 70
STATIC LATERAL POSITIONAL STABILITY
AH-1S USAF 61486
CIRCUIT CONFIGURATION

GYRO	ARMED	ARM ALT.	ARMED ANGLE	POSITION	FLY CIRCUIT TESTS	
XGAS	NO	10° FT.	0°, -10°	UP	1000	
•	600	6000	100°(HT)	DOWN	LEVEL FL	6000
•	110.5	4000	0°(HT)	100°(HT)	100°(HT)	4000

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINT WITH AIRCRAFT'S BANK ATTITUDE, GYRO BALL CENTERED

2. COLLECTIVE POSITION HELD FIXED DURING TEST

3. COLLECTIVE STICK POSITION: 26.0 PERCENT FROM FULL DOWN

4. AH-1S CIRCUIT (ARMED)

5. TOTAL CONTROL DISPLACEMENT

LONGITUDINAL: 10.08 INCHES FROM FULL FORWARD

LATERAL: -4.90 INCHES FROM FULL LEFT

DIRECTIONAL: -5.97 INCHES FROM FULL LEFT

COLLECTIVE: +8.98 INCHES FROM FULL DOWN

6. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED FROM ALL CONTROL FORCE DATA

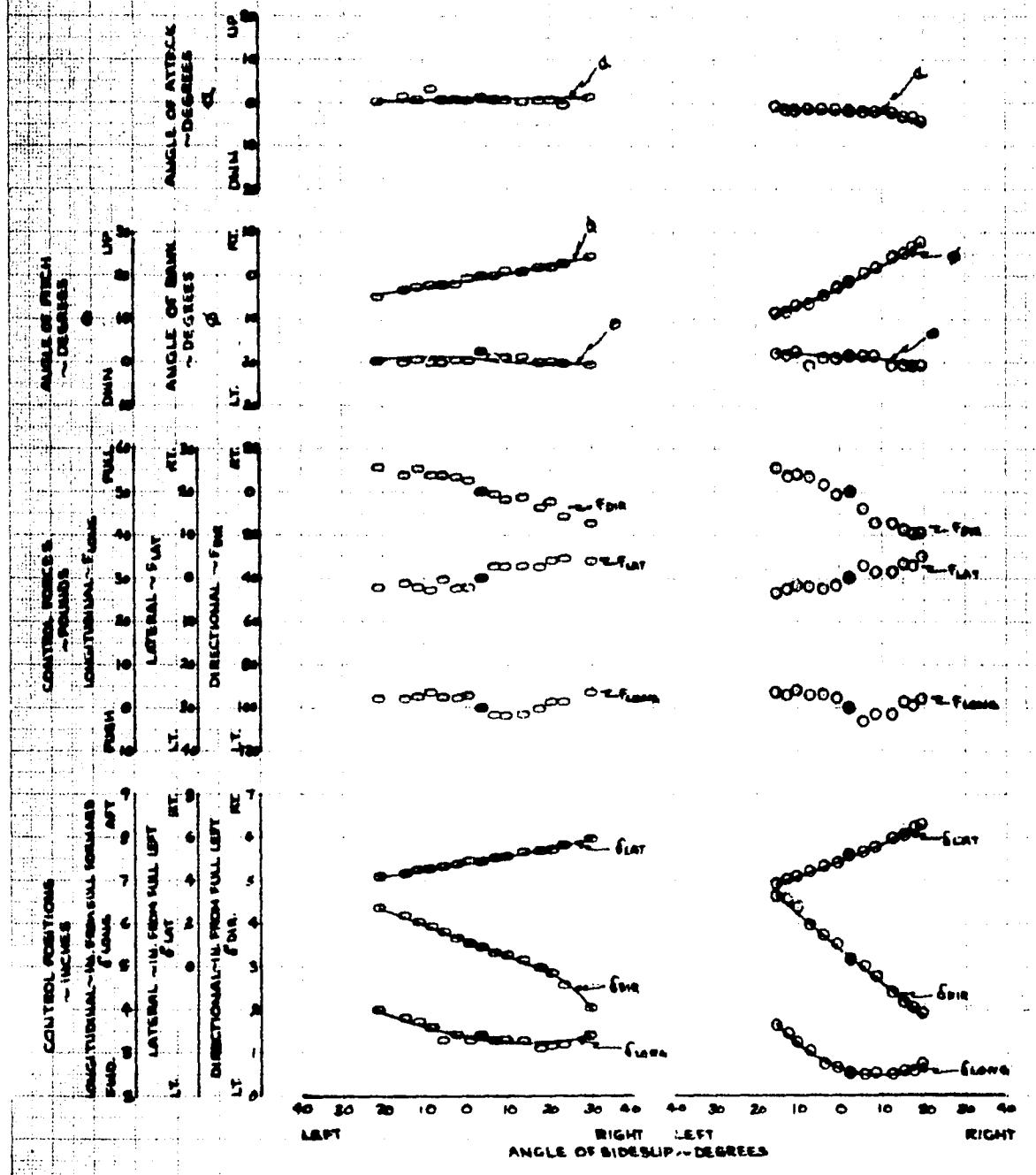


FIGURE NO. 1
STATIC LATERAL-DIRECTIONAL STABILITY
AM-10 USA 5715624
SEVEN CONFIGURATION

DATA ALIGNED AND ATT. ANGLES ARE IN DEGREES. CHIN TURBULENCE
 CHCAS H₂-FT ~1.0 C.G. AT 50% WINGSPAN
 1420 5510 0.95 100.0 (AFT) 0.016 100.0 (AFT) 0.00011
 1125 4400 0.95 100.0 (AFT) 0.016 100.0 (AFT) 0.00011

NOTES: 1. SOLID SYMBOLS INDICATE THAT POINT WITH AIRCRAFT'S BANK
 ATTITUDE WAS FULL CENTERED.

2. COLLECTIVE POSITION WAS FIXED DURING TEST.

3. COLLECTIVE STICK POSITION = 100.0 PERCENT FROM FULL DOWN.

4. AM-10 CHIN TURBULENCE (STUDIED).

5. TOTAL CONTROL DISPLACEMENT.

LONGITUDINAL = 10.0 INCHES FROM FULL FORWARD

LATERAL = 9.90 INCHES FROM FULL LEFT

DIRECTIONAL = 8.91 INCHES FROM FULL LEFT

COLLECTIVE = 8.98 INCHES FROM FULL DOWN.

6. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED
 FROM ALL CONTROL FORCE DATA.

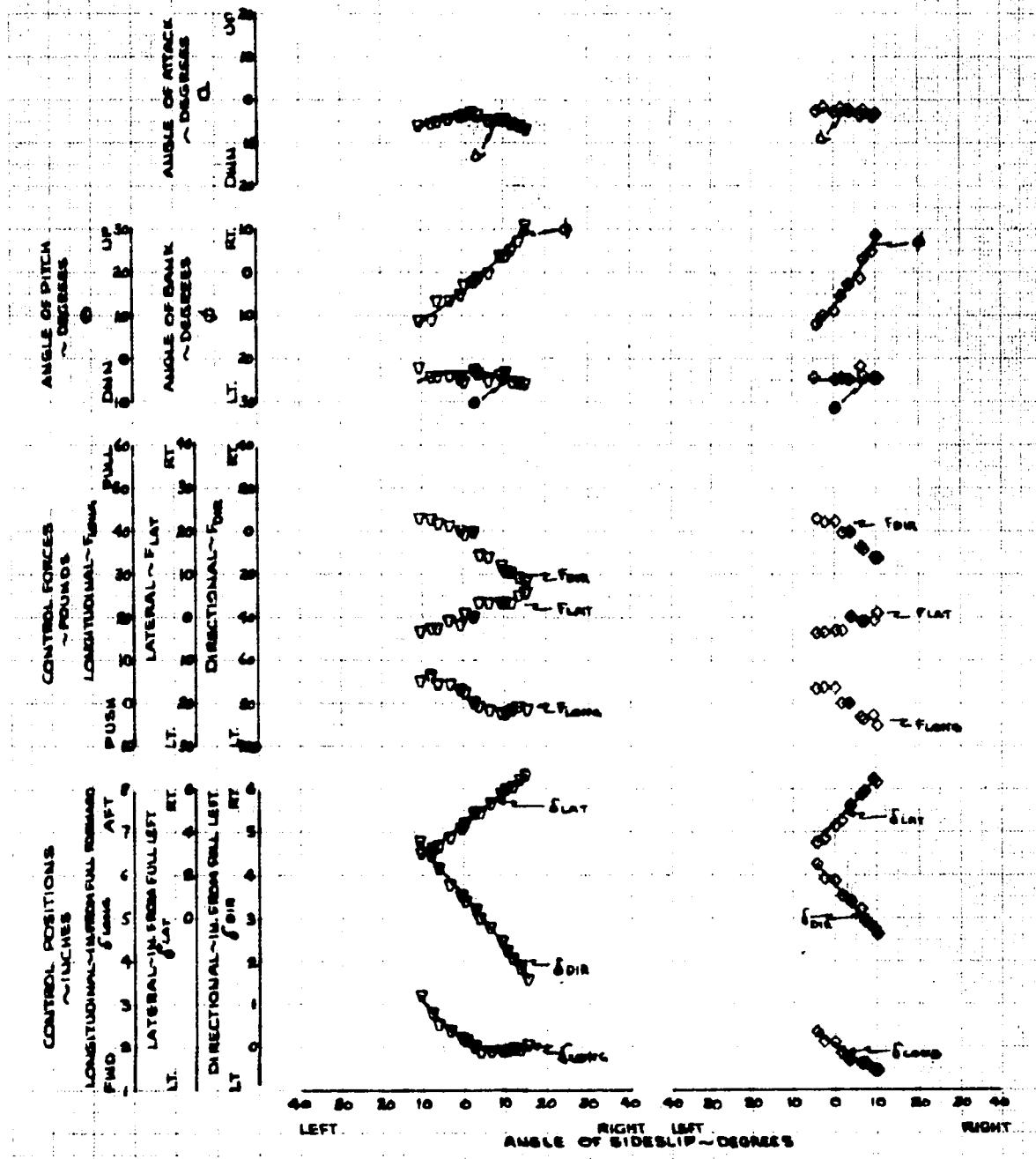


FIGURE NO. 72
STATIC LATERAL DIRECTIONAL STABILITY
AH-1G USAF T1676
CLEAN CONFIGURATION

GVM

AIR SPEED. AVG ALT. AVG. G.W. AVG. LONG. ROTOR. S.L.T. COGL. THRUST C.R.P.
 ~KCAS ~FT. ~LB. ~CU. IN. RPM °C
 50.5 5630 7908 144.1(AFT) 312.0 CLEAN 0.004725
 60.0 5650 7910 144.1(AFT) 319.0 TURB 0.005076

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINT WITH AIRCRAFT'S BANK
 ATTITUDE GYRO BALL CENTERED

2. COLLECTIVE POSITION HELD FIXED DURING TEST.

3. COLLECTIVE STICK POSITION = 56.0 PERCENT FROM FULL DOWN

4. 3M-20 CMU TURRET (STABILIZED)

5. TOTAL CONTROL DISPLACEMENT

LONGITUDINAL = 10.03 INCHES FROM FULL FORWARD

LATERAL = 9.90 INCHES FROM FULL LEFT

DIRECTIONAL = 5.93 INCHES FROM FULL LEFT

COLLECTIVE = 8.98 INCHES FROM FULL DOWN

6. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED FROM
 ALL CONTROL FORCE DATA

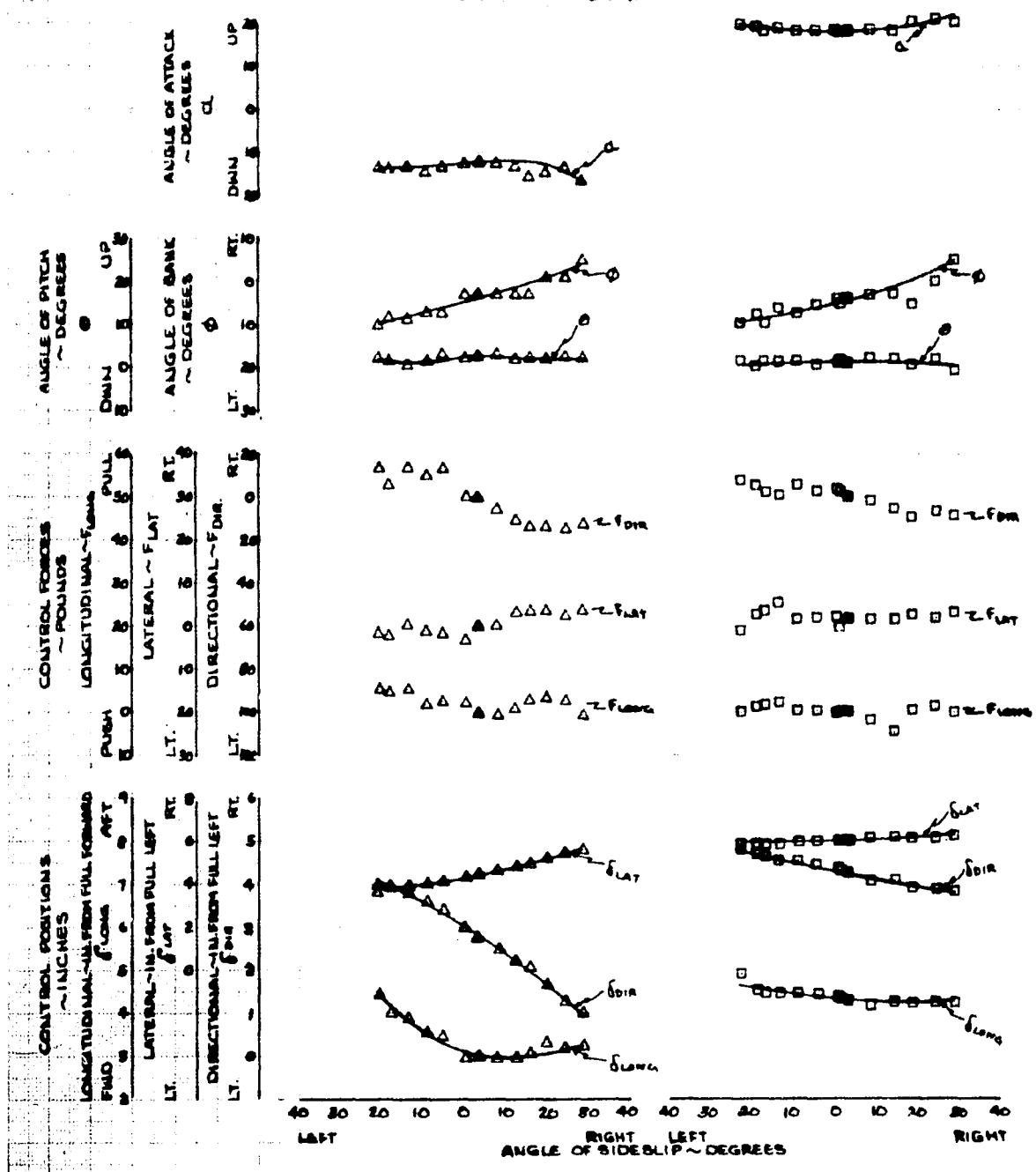


FIGURE NO. 73
STATIC LATERAL DIRECTIONAL STABILITY
AH-1G USAF 94-15648

OUTBOARD ALTERNATE CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM. AIRSPEED AVG. ALT. AVG. G.M. AVG. LONG. ROTOR FLT. COND. THRUST COEFF.
 -KCAS H₀~FT. C.G.~IN. RPM ~C_T
 0 62.0 4050 9475 200.4(FT) 325.0 LEVEL FLT. 0000414
 0 103.0 5780 8765 200.4(FT) 324.0 LEVEL FLT. 0003186

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINT WITH AIRCRAFT'S BANK ATTITUDE GYRO BALL CENTERED

2. COLLECTIVE POSITION HELD FIXED DURING TEST.

3. COLLECTIVE STICK POSITION +21.0 PERCENT FROM FULL DOWN

4. XM-2B CMU TURRET (STOWED)

5. TOTAL CONTROL DISPLACEMENT

LONGITUDINAL = 10.03 INCHES FROM FULL FORWARD

LATERAL = 9.90 INCHES FROM FULL LEFT

DIRECTIONAL = 5.97 INCHES FROM FULL LEFT

COLLECTIVE = 6.98 INCHES FROM FULL DOWN

6. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED FROM ALL CONTROL FORCE DATA

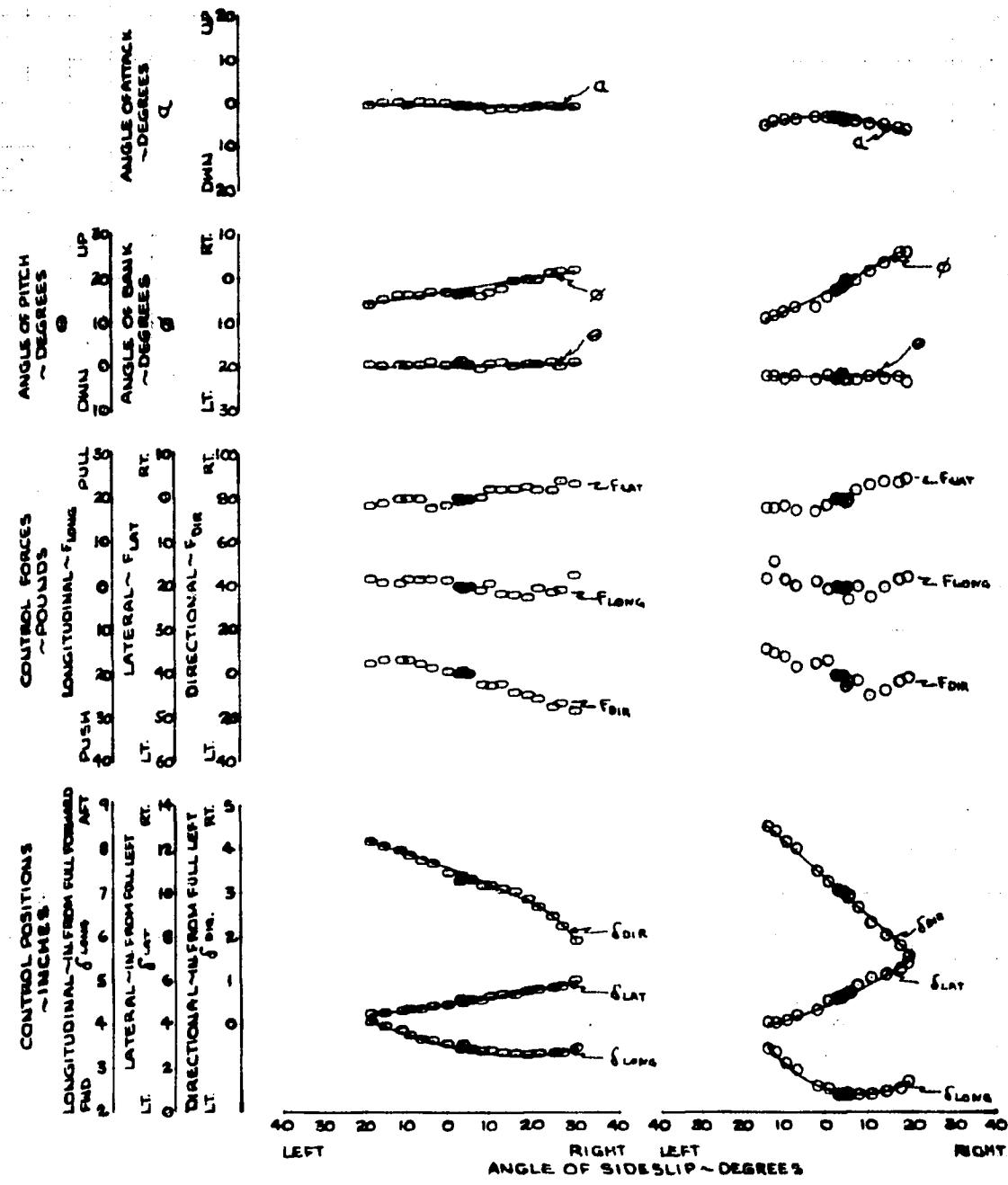


FIGURE NO. 74
STATIC LATERAL-DIRECTIONAL STABILITY

AH-1G USA 5215698

OUTBO ALTERNATE CONFIGURATION WITH DOWNGEAR FAIRINGS REMOVED

SYM	AIRSPD. ~KCAS	AVG. ALT. ft.	AVG. S. G. ~LB.	AVG. LONG. ~MIN.	MOTOR. RPM	FLY. COND. THRUST COEF.	CY
U	1585	3340	5007(AFT)	3240	LEVEL: FLZ 0.000012		
O	1575	3470	5097(AFT)	3360	DIVE: 0.000013		

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINTS WITH AIRCRAFT'S BANK ATTITUDE GYRO BALL CENTERED

2. COLLECTIVE POSITION HELD FIXED DURING TEST

3. COLLECTIVE STICK POSITION = 33.0 PERCENT FROM FULL DOWN

4. XM-12 CHIN TURRET (STOWED)

5. TOTAL CONTROL POSITIONS

LONGITUDINAL = 100.8 INCHES FROM FULL FORWARD

LATERAL = 9.90 INCHES FROM FULL LEFT

DIRECTIONAL = 5.97 INCHES FROM FULL LEFT

COLLECTIVE = 3.98 INCHES FROM FULL DOWN

6. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED FROM ALL CONTROL FORCE DATA

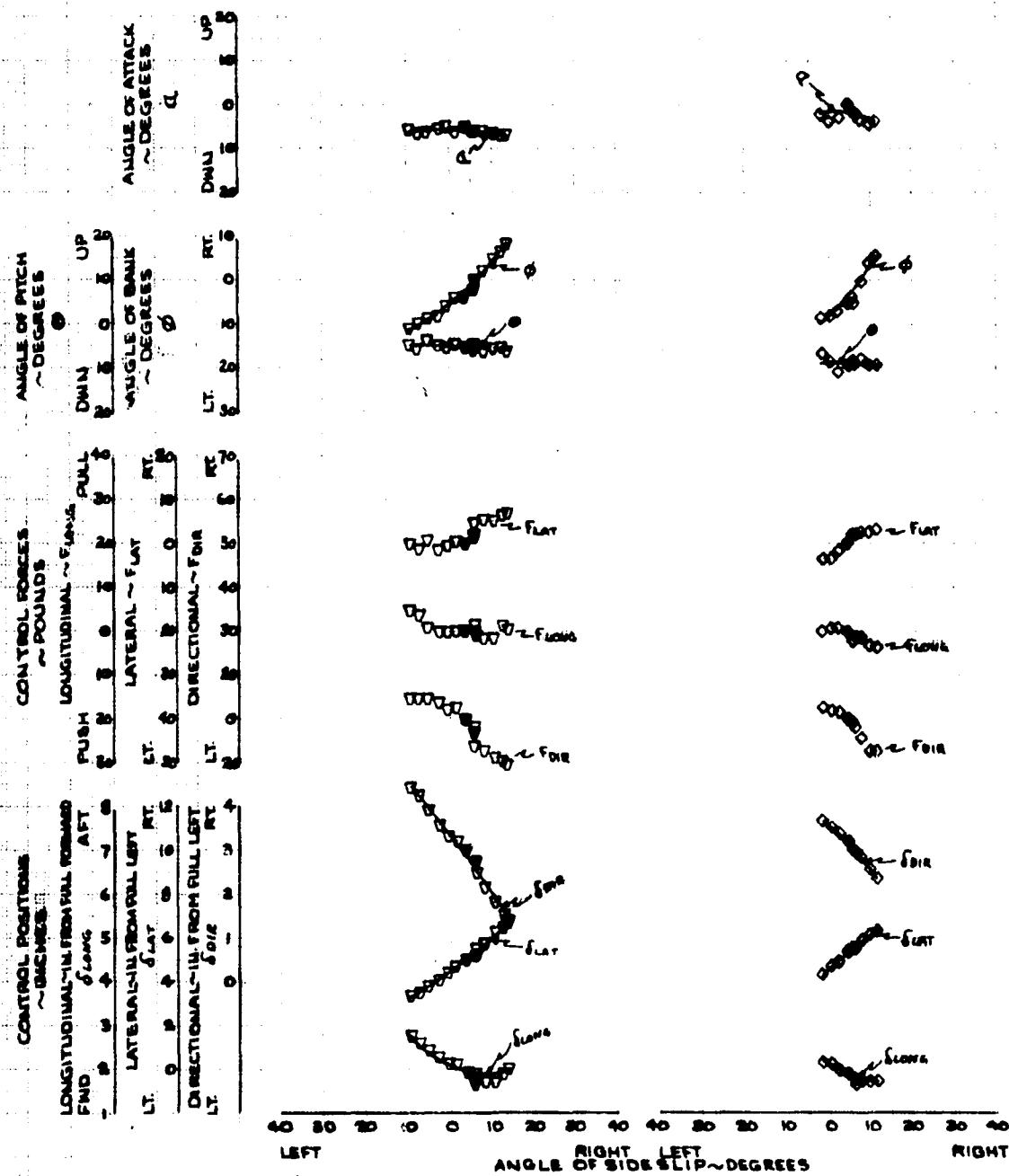


FIGURE NO. 75
STATIC LATERAL DIRECTIONAL STABILITY

AM-1G USA #718648
OUTBO ALTERNATE CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM	AIR SPEED ~KCAS	AVG. ALT. M ₂ ~FT.	AVG. G.W. C.D. ~LB.	AVG. LONG. RPM	ROTOR RPM	FLT. COND. THRUFT CORPS. ~CT	CLIMB AUTO.	DESCEND AUTO.
A	62.5	3530	6615	200.50(4)	200.6	Climb	Stabilized	
B	69.8	3560	6625	200.44(4)	2250	Auto.	Stabilized	

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINT WITH AIRCRAFT'S BANK ATTITUDE GYRO BALL CENTERED

2. COLLECTIVE POSITION HELD FIXED DURING TEST

3. COLLECTIVE STICK POSITION - 35.60 PERCENT FROM FULL DOWN

4. XM-28 CHIN TURBET (STONED)

5. TOTAL CONTROL DISPLACEMENT:

LONGITUDINAL - 10.88 IN. FROM FULL FORWARD

LATERAL - 9.90 IN. FROM FULL LEFT

DIRECTIONAL - 5.97 IN. FROM FULL LEFT

COLLECTIVE - 8.98 IN. FROM FULL DOWN

6. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED FROM ALL CONTROL FORCE DATA

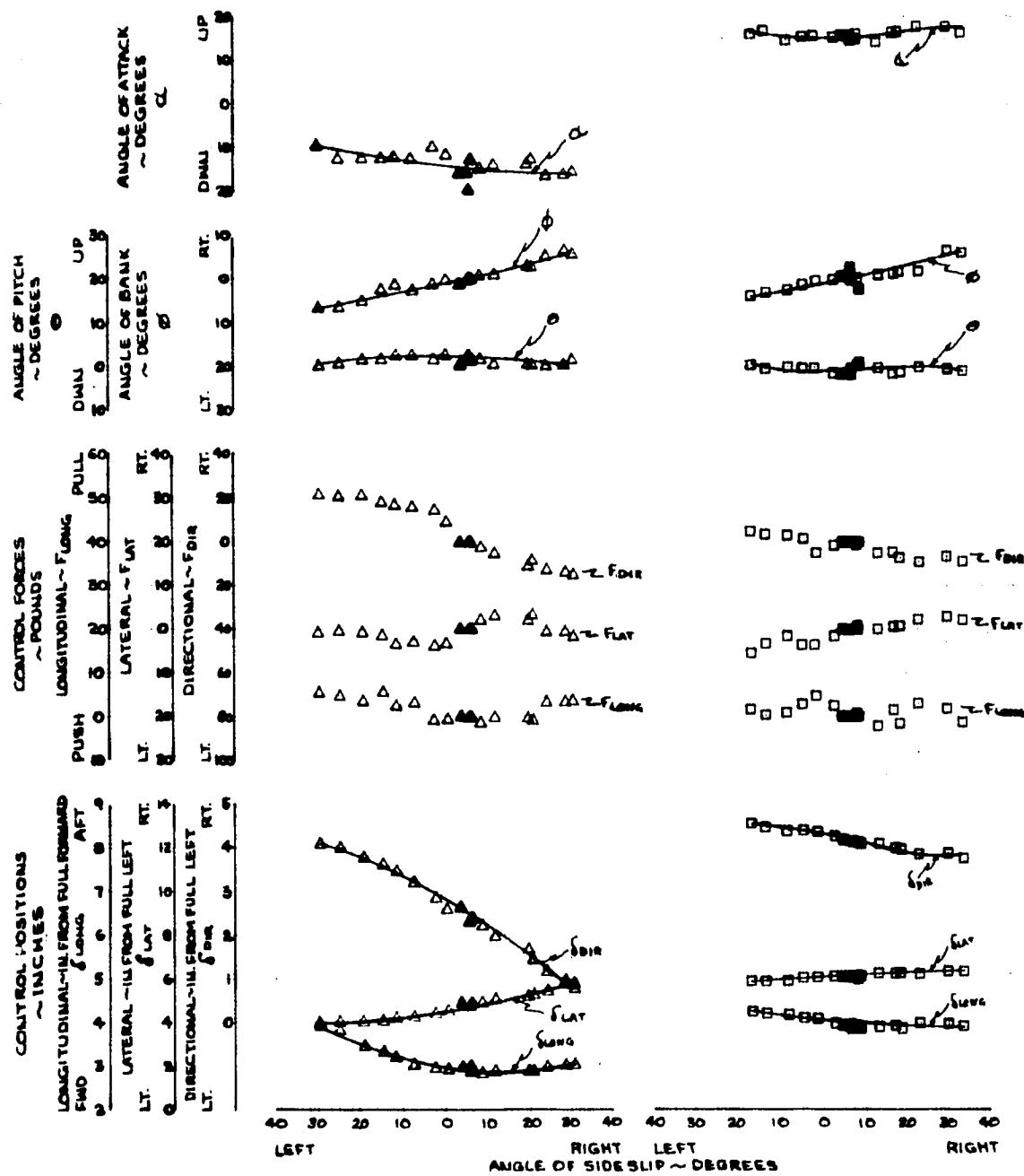


FIGURE NO. 76
STATIC LATERAL DIRECTIONAL STABILITY

AH-1G USAF 71-0049
MHV SCOUT CONFIGURATION WITH HULLY PODS AIRBAGS REMOVED

SYM	ARMED	ANG. ALT.	ANG. GLH	ANG. LONG.	ROTOR	FLT. COND.	THRUST COEFF.
O	~MCAB	~L	~L	~L	CQ ~IN.	UP	- CT
O	620	540	545	545	(ATT)	3250	LEVEL FLT
O	1025	220	220	220	(ATT)	3220	LEVEL FLT

NOTES: 1. SOLID SYMBOLS denote trim point with aircraft's bank.
 ATTITUDE GYRO BALL CENTERED

2. COLLECTIVE POSITION HELD FIXED DURING TEST

3. COLLECTIVE STICK POSITION = 30 PERCENT FROM FULL DOWN

4. XM-28 CMM TURRET (STEAMED)

5. TOTAL CONTROL DISPLACEMENT

LONGITUDINAL = 10.05 INCHES FROM FULL FORWARD

LATERAL = 9.90 INCHES FROM FULL LEFT

DIRECTIONAL = 5.77 INCHES FROM FULL LEFT

COLLECTIVE = 6.98 INCHES FROM FULL DOWN

6. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED
 FROM ALL CONTROL FORCE DATA

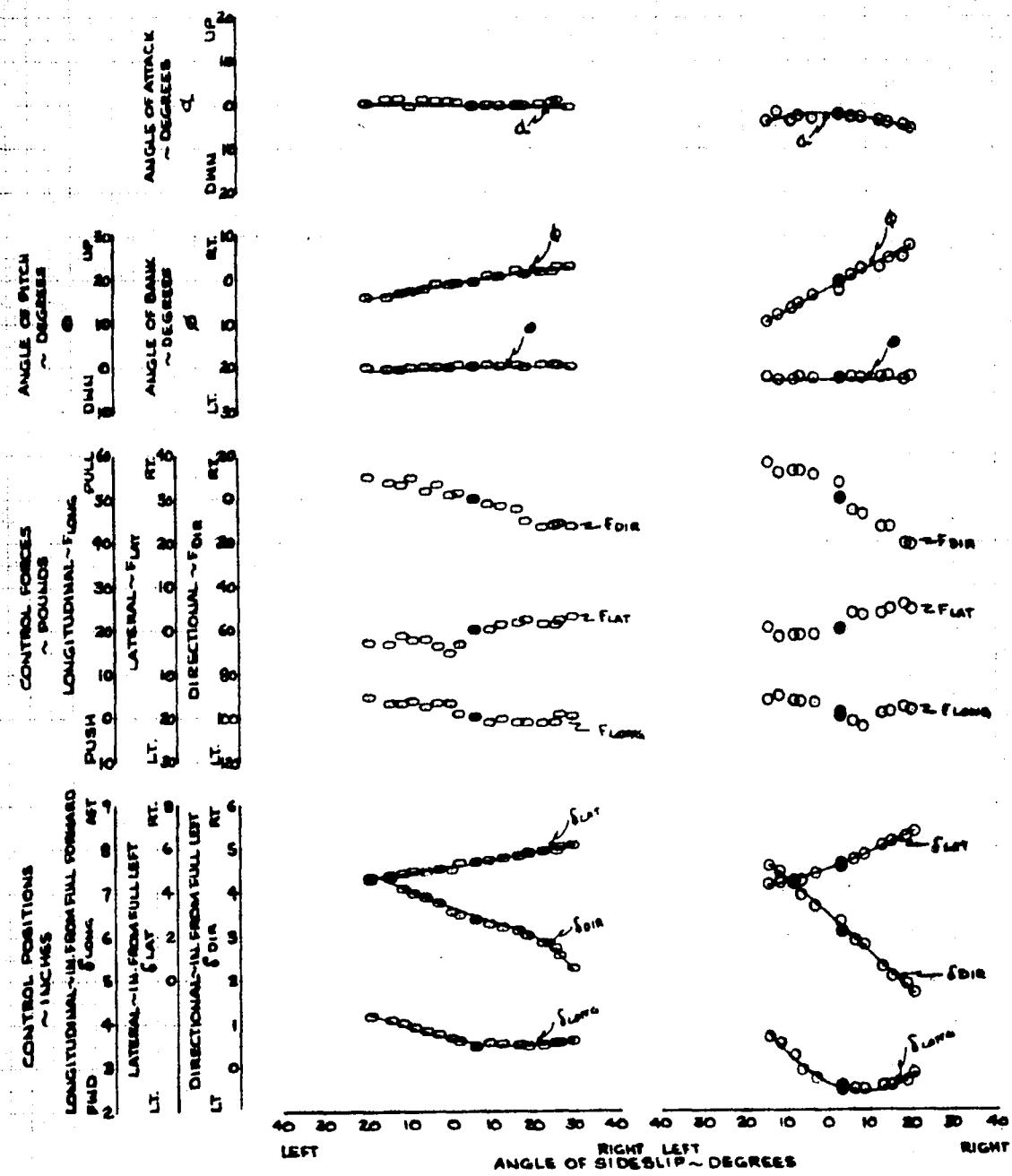


FIGURE NO. 77
STATIC LATERAL-DIRECTIONAL STABILITY
AM-10 USAF AIRCRAFT
HVK SCOUT CONFIGURATION WITH BRACKET POD FAIRINGS REMOVED

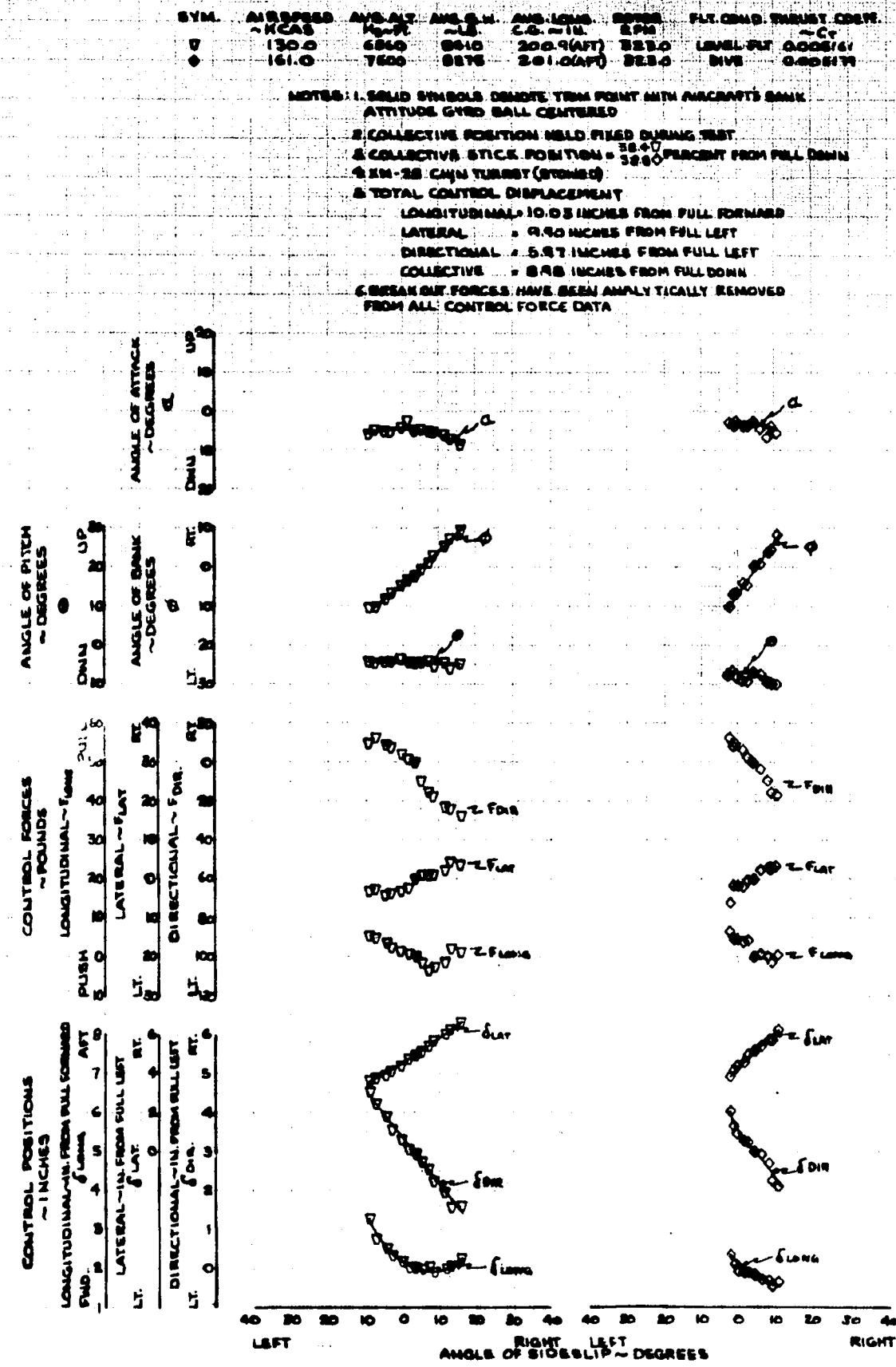


FIGURE NO. 78
STATIC LATERAL-DIRECTIONAL STABILITY
AN-106 USAF TIGER II

HV-2 SCOUT CONFIGURATION INSTRUMENTS AND FAIRINGS REMOVED

SYM. AIRFIELD AVG. ALT. AVG. S.H. AVG. LONG. ROLL FLY. COND. THRUST CORR.
 ~KCAS H-67 LD. C.G. -10.0
 4 630 6100 0000 SWING 3230 CLIMB 0.0000
 3 620 6000 0000 SWING 3230 AUTO 0.0000

NOTE: 1. SOLID SYMBOLS DENOTE ITEM RELEVANT WITH AIRCRAFT'S DRAWS.
 ATTITUDE GYRO BALL CENTERED

2. COLLECTIVE POSITION HELD SWING SWINGING ZERO.

3. COLLECTIVE STICK POSITION: 0.00 PULLDOWN FROM FULL DOWN

4. XM-28 CHIN TURRET (SWING)

5. TOTAL CONTROL DISPLACEMENT

LONGITUDINAL = 1000 INCHES FROM FULL FORWARD

LATERAL = 9.00 INCHES FROM FULL LEFT

DIRECTIONAL = 5.91 INCHES FROM FULL LEFT

COLLECTIVE = 0.78 INCHES FROM FULL DOWN

6. BREAKOUT FORCES HAVE BEEN ANALYTICALLY REMOVED
 FROM ALL CONTROL FORCE DATA.

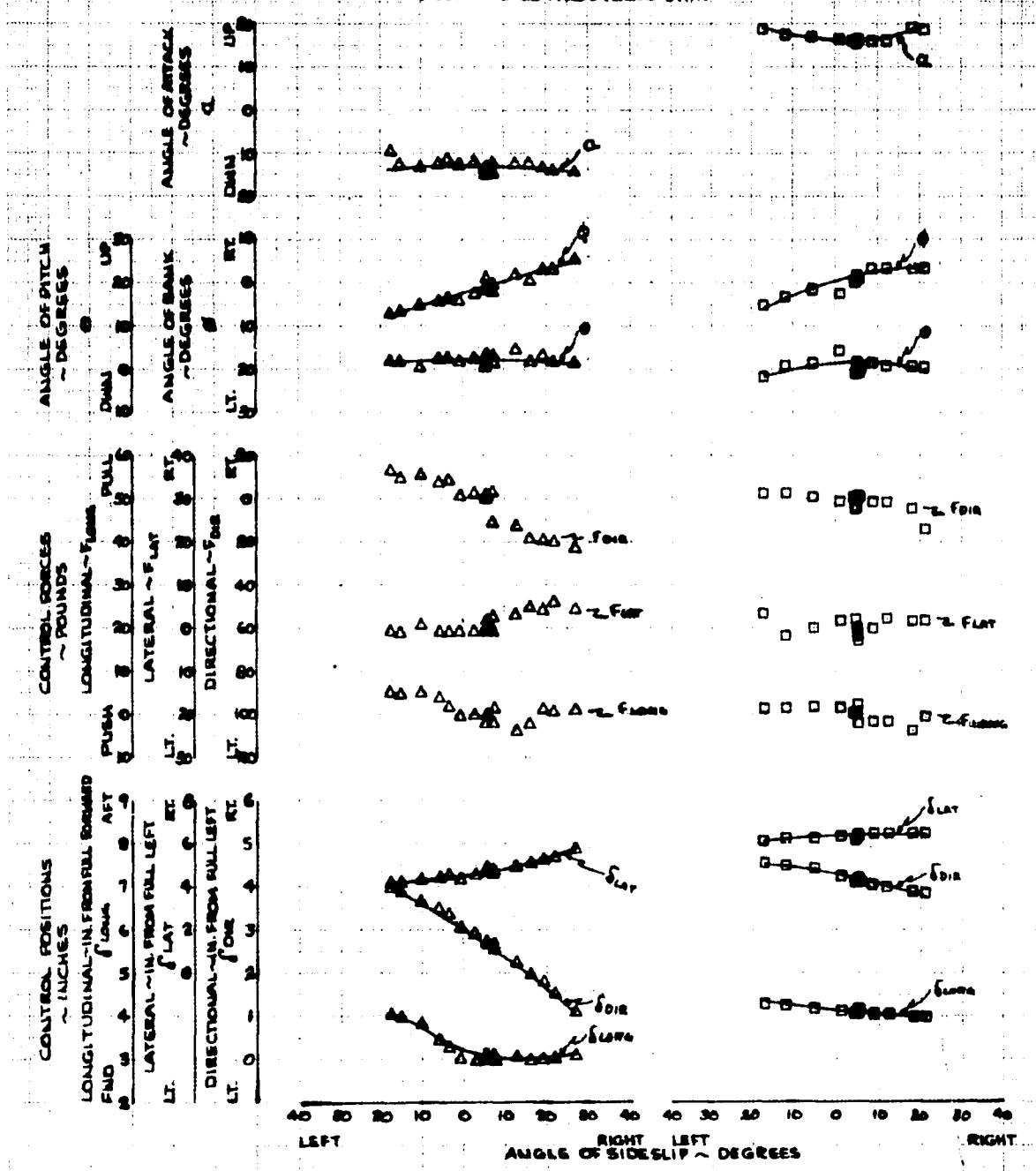


FIGURE NO. 79
STATIC LATERAL DIRECTIONAL STABILITY
AN-16 USAF/T16RS

HVV. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED.

SYM AIRSPEED AVG ALT. ANG. GIM ANGLONG. MOTOR FLT. COND. THRUST COEFF
 ~KCAS M-1ST ~LB. CG-1IN. RPM -CT
 O 525 0.220 0.875 191.8(FW) 324.0 LEVEL FLT. 0.00468K
 O 126.3 5200 0.870 191.8(RM) 324.0 LEVEL FLT. 0.00468K

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINT WITH AIRCRAFT'S BANK
 ATTITUDE GYRO BALL CENTERED

2. COLLECTIVE POSITION HELD FIXED DURING TEST

3. COLLECTIVE STICK POSITION - 70.8 PERCENT FROM FULL DOWN

4. XM-20 CHIN TURRET (SIDED)

5. TOTAL CONTROL DISPLACEMENT

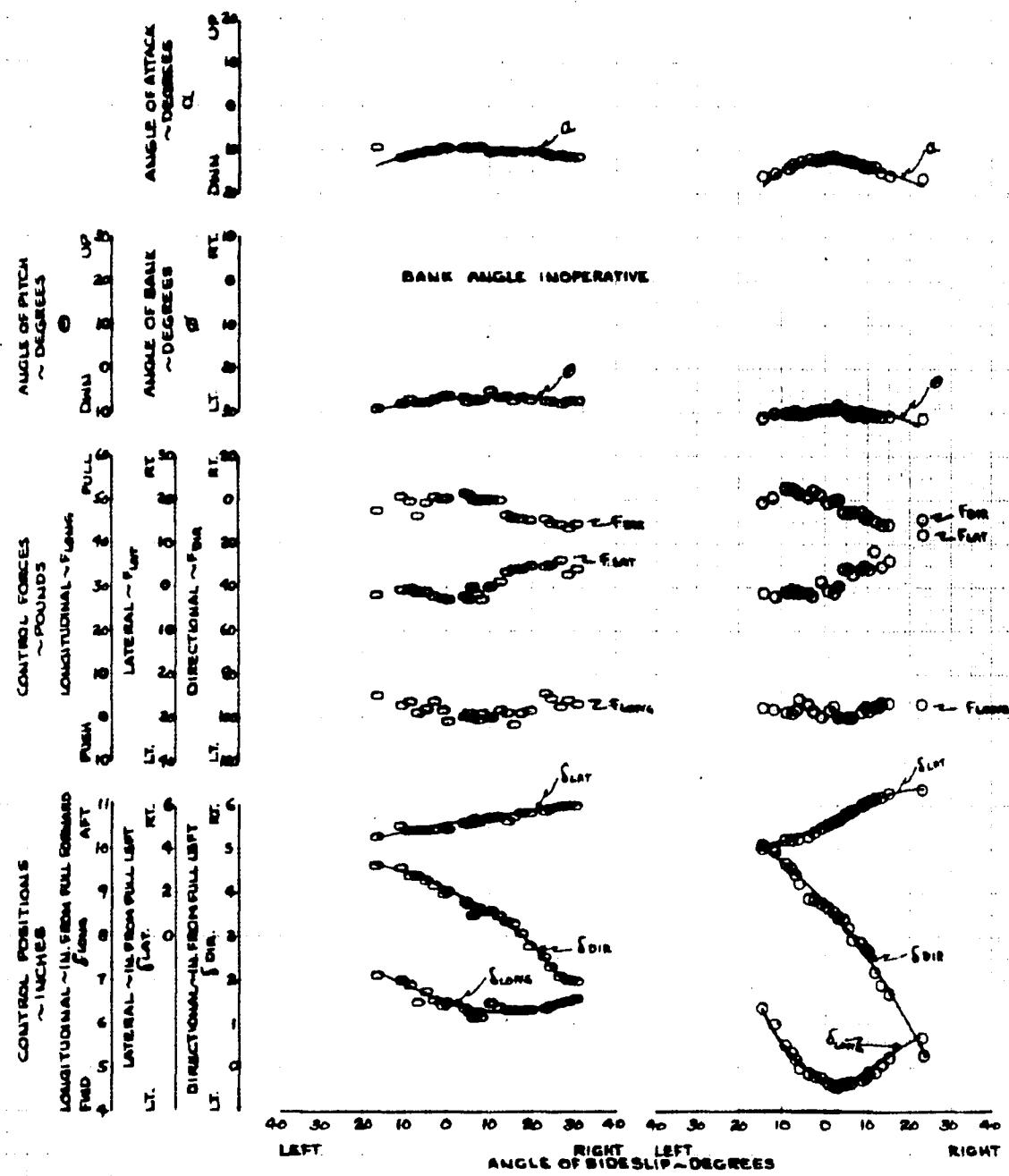
LONGITUDINAL - 10.28 INCHES FROM FULL FORWARD

LATERAL - 9.90 INCHES FROM FULL LEFT

DIRECTIONAL - 5.97 INCHES FROM FULL LEFT

COLLECTIVE - 8.98 INCHES FROM FULL DOWN

6. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED
 FROM ALL CONTROL FORCE DATA



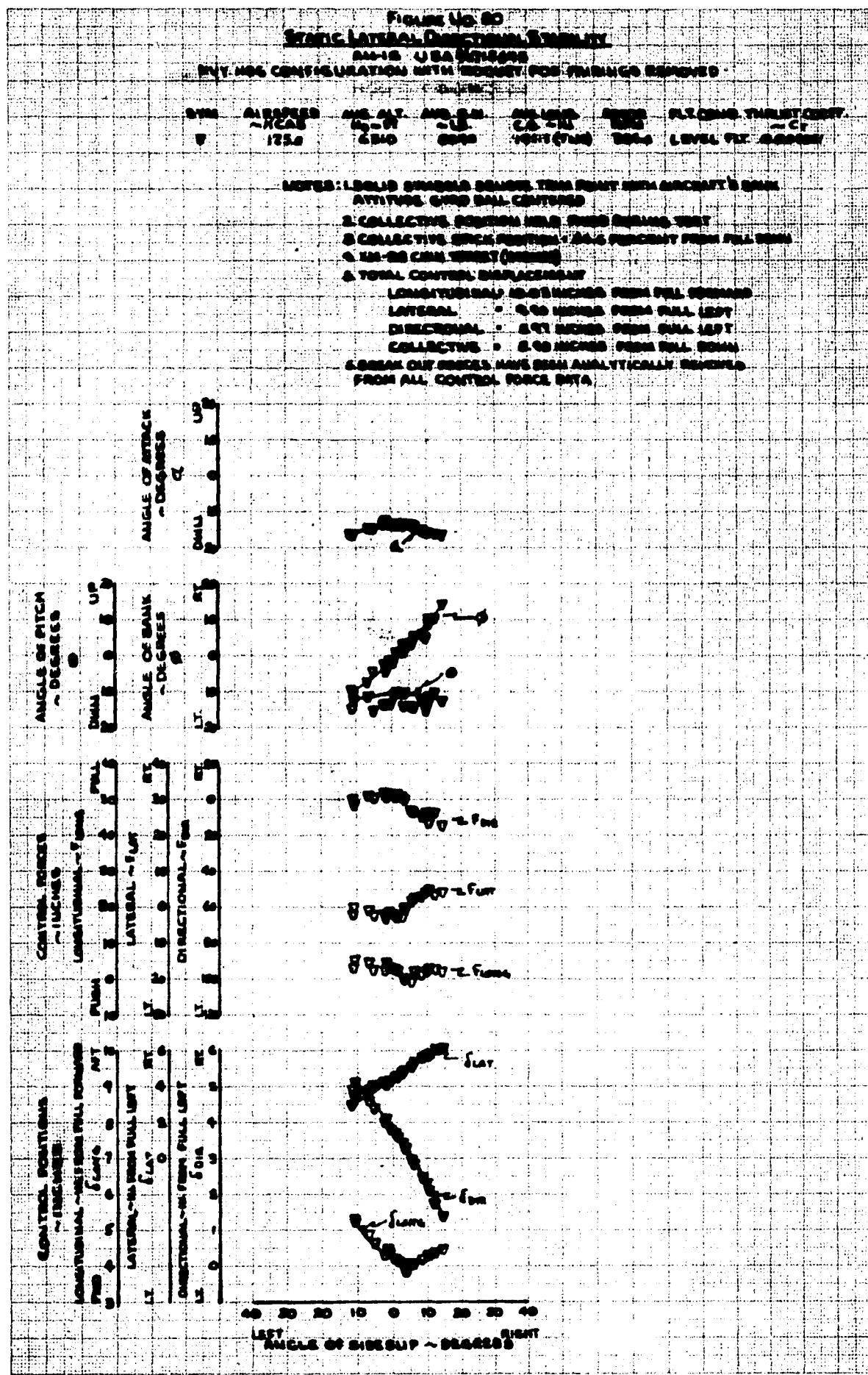


FIGURE No. 81

TESTING APPROXIMATE DIRECTIONAL STABILITY

DATA FOR U.S.A.F. F-4C
M.V. 1000 GROSS WEIGHT WITH ROCKET POD FAIRINGS REMOVED

DATA ALPHAS AND ALP. ANGLES AND LONG. RATES FLT. COMP. THROTTLE - C.
 AIRSPEED 1000 MPH CLIMB RATE 2500 FT/MIN. CLIMB RATE 3000 FT/MIN.
 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00

NOTE: 1. SOLID SYMBOLS DENOTE TESTS AT 90 DEGREE BANK
2. HORIZONTAL POSITION INDICATED DURING TEST

3. COLLECTIVE STICK POSITION FROM FULL DOWN
4. 100-25 GEAR DOWN (UPWARD)

5. TOTAL CONTROL DISPLACEMENT

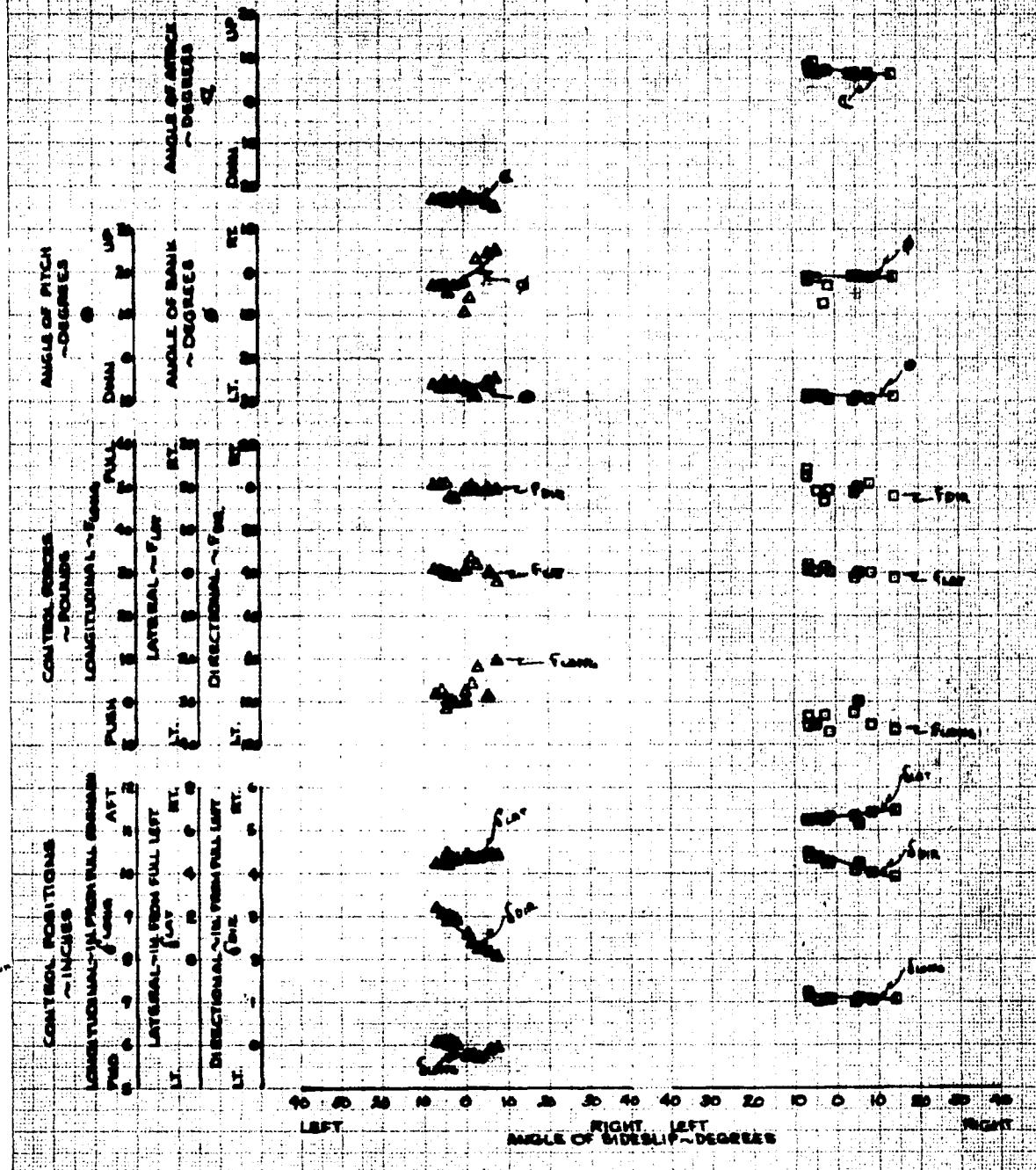
LATERAL THROTTLE POSITION FROM FULL POSITION

1. ROLL - 0.00 INCHES FROM FULL LEFT

2. DIRECTIONAL - 0.50 INCHES FROM FULL LEFT

3. COLLECTIVE - 0.50 INCHES FROM FULL DOWN

4. BREAK OUT FORCES AND SWELL ANALYTICALLY REMOVED
FROM ALL CONTROL FORCE DATA



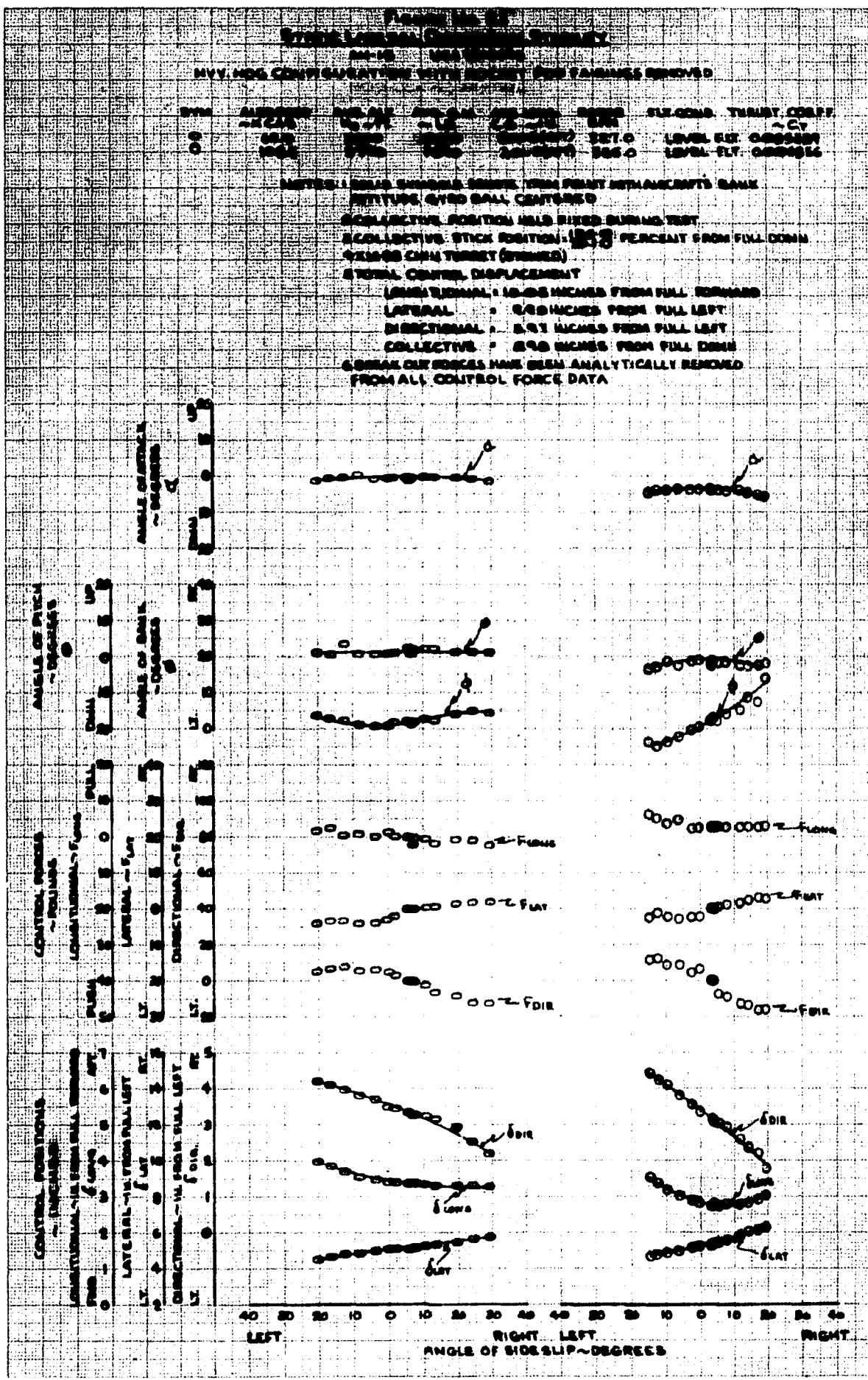


FIGURE No.83
STATIC LATERAL DIRECTIONAL STABILITY

AH-1G USAFT 18695

HUV. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

GYM	SPD SPEED	Avg. G.L.	Avg. G.W.	Avg. LONG.	MOTOR	FLT. COND.	THRUST COEFF.
U	MCAS	No. FT.	ALB.	C.G. ~IN.	RPM	~CV	
U	1450	3940	7760	201.3 (AFT)	323.0	LEVEL RLT. 0.004874	
O	1000	5730	7680	201.3 (AFT)	323.0	DIVE 0.004553	

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINT WITH AIRCRAFT'S BANK ATTITUDE GYRO BALL CENTERED

2. COLLECTIVE POSITION HELD FIXED DURING TEST

3. COLLECTIVE STICK POSITION = $\frac{300}{360}$ PERCENT FROM FULL DOWN

4. XM-28 CHIN TURRET (STOWED)

5. TOTAL CONTROL POSITIONS

LONGITUDINAL = 10.03 INCHES FROM FULL FORWARD

LATERAL = 9.90 INCHES FROM FULL LEFT

DIRECTIONAL = 5.97 INCHES FROM FULL LEFT

COLLECTIVE = 8.98 INCHES FROM FULL DOWN

6. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED FROM ALL CONTROL FORCE DATA

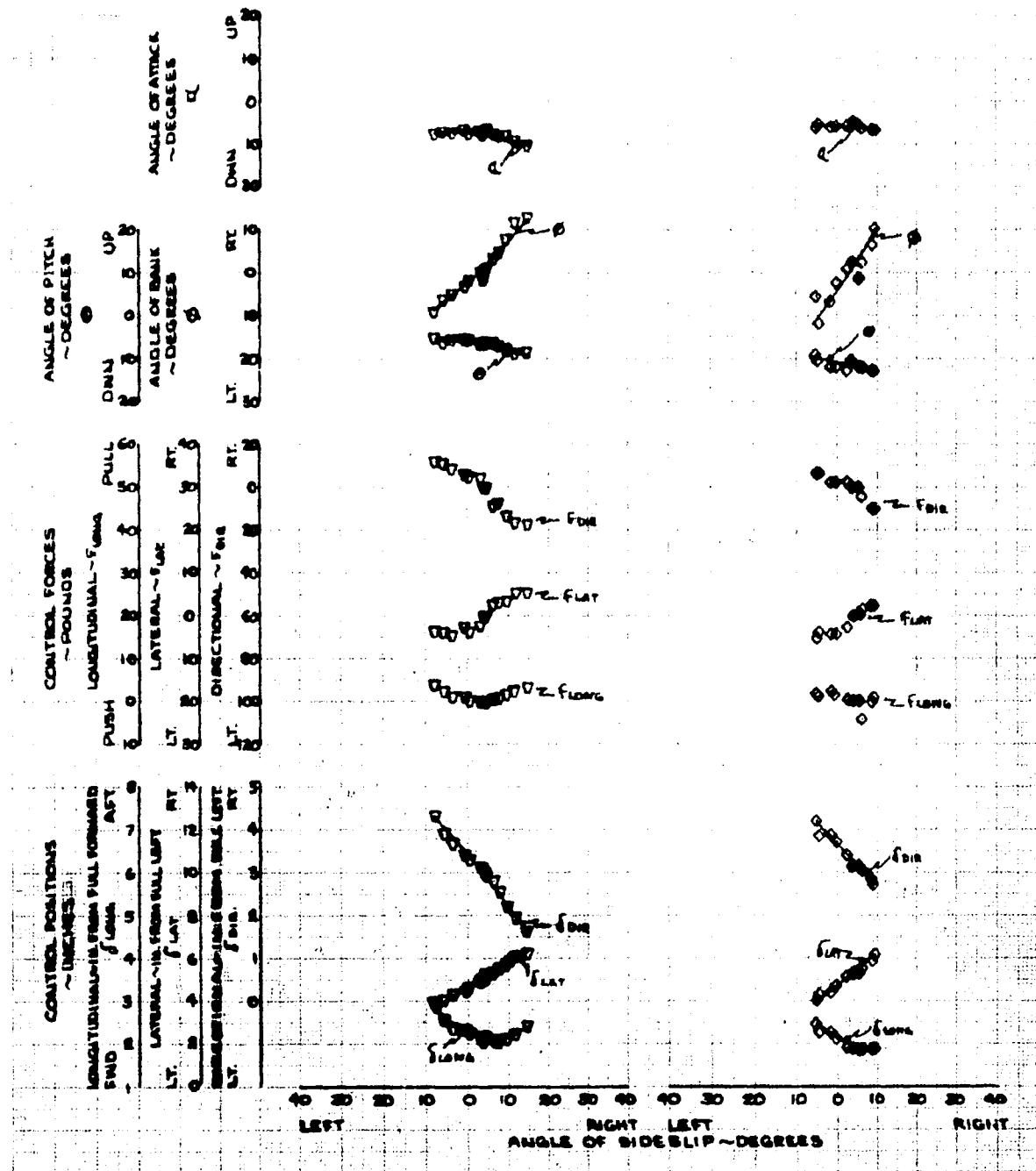


FIGURE NO. 64
STATIC LATERAL-DIRECTIONAL STABILITY
AM-16 U-BAR TIGER
HVV HOG CONFIGURATION WITH BRACKET POD FAIRINGS REMOVED

SYM. SURGED AVG. ALZ. ANG. OF LND. SENS. FLY. COEF. THRUST COEFF.
 -NCAS Hs=1.5 Cg=.1M. $\frac{C_L}{C_D}$ = .45
 0.5 2400 2200 2200 2200 CLIMB 2200
 1.5 2000 2000 2000 2000 DESCEND 2000 AUTOGRATION 2000

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINT WITH AIRCRAFT'S BANK ATTITUDE GYRO BALL CENTERED

2. COLLECTIVE POSITION HELD FIXED DURING TEST

3. COLLECTIVE STICK POSITION = 0.50 PERCENT FROM FULL DOWN

4. AM-16 CHIN TURRET (ARMED)

5. TOTAL CONTROL DISPLACEMENT

LONGITUDINAL = 10.03 IN. FROM FULL FORWARD

LATERAL = 9.90 IN. FROM FULL LEFT

DIRECTIONAL = 5.91 IN. FROM FULL LEFT

COLLECTIVE = 0.90 IN. FROM FULL DOWN

6. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED FROM ALL CONTROL FORCE DATA

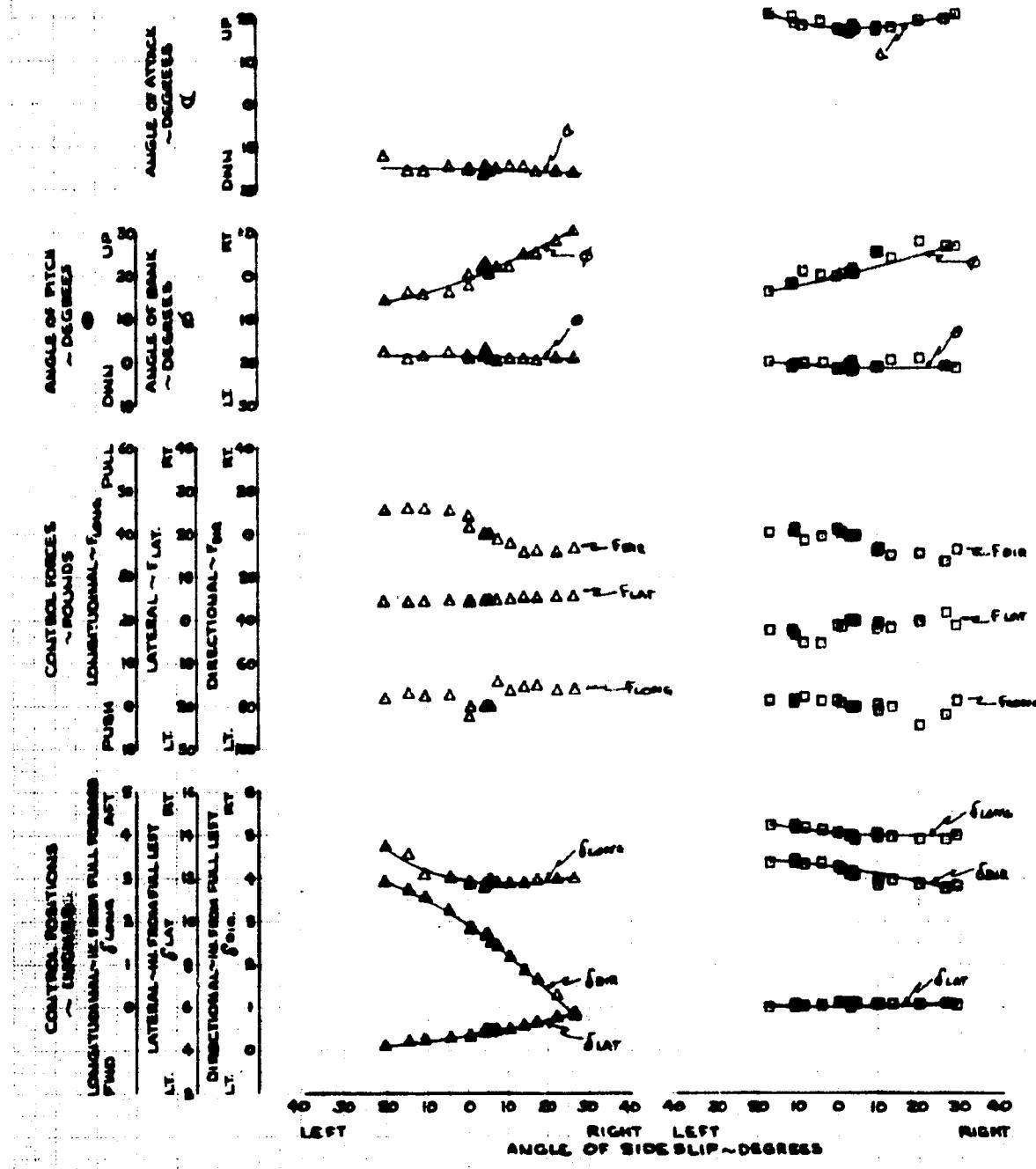


FIGURE NO. B5
STATIC LATERAL DIRECTIONAL STABILITY
AH-1G USAF 67-11268

HVV. HOG CONFIGURATION WITH ROCKET POD SWIMMING REMOVED

SYM	AIR SPEED	AVG. ALT.	AVG. G. M.	ANGLE OF PITCH	FLY. COND.	THRUST COEF.
O	~K CAS	~M FT.	~LBS	~DEG	~TAN	~CT
O	60.5	3160	8710	200.700	0.000	0.000
O	100.5	4160	8710	200.000	0.000	0.000

NOTE: 1. SOLID SYMBOLS DENOTE TRIM POINT WITH AIRCRAFT'S BANK ATTITUDE GYRO BALL CENTERED

2. COLLECTIVE POSITION HELD FIXED DURING TEST

3. COLLECTIVE STICK POSITION -28.5 PERCENT FROM FULL DOWN

4. XM-2B CHIN TURRET (STATION)

5. TOTAL CONTROL DISPLACEMENT

LONGITUDINAL 10.05 IN. FROM FULL FORWARD

LATERAL 9.90 IN. FROM FULL LEFT

DIRECTIONAL 5.87 IN. FROM FULL LEFT

COLLECTIVE 9.95 IN. FROM FULL DOWN

6. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED

FROM ALL CONTROL FORCE DATA

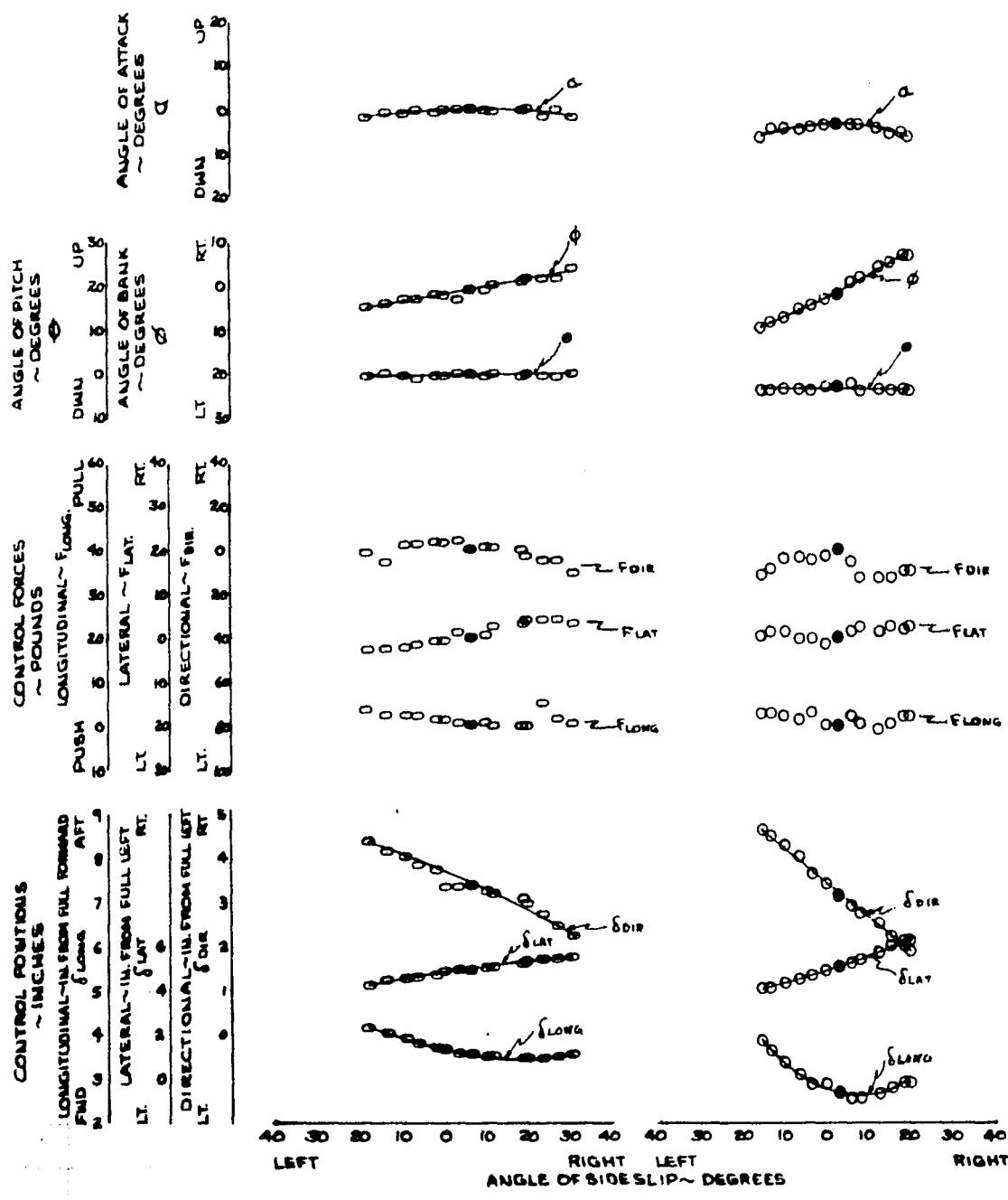


FIGURE NO. 86
STATIC LATERAL DIRECTIONAL STABILITY
AH-1G USA TESTS

HVV. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM	AIRSPED ~KCAB	AVG ALT. H _D -FT	AVG SGN. C.G.-IN.	AVG LONG. RPM	ROTOR	FLT. COND.	THRUST COEFF.
□	130.5	5440	8700	200.0(FT)	324.0	LEVEL FLG.	0.64905
◆	131.5	6340	8150	200.0(FT)	324.0	DIVE	0.68882

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINT WITH AIRCRAFT'S BANK ATTITUDE GYRO BALL CENTERED

2. COLLECTIVE POSITION HELD FIXED DURING TEST
3. COLLECTIVE STICK POSITION = 39.60 PERCENT FROM FULL DOWN
4. KM-28 CHIN TURRET (STONED)
5. TOTAL CONTROL DISPLACEMENT

LONGITUDINAL 10.03 INCHES FROM FULL FORWARD
 LATERAL + 9.90 INCHES FROM FULL LEFT

DIRECTIONAL + 8.97 INCHES FROM FULL LEFT
 COLLECTIVE + 8.98 INCHES FROM FULL DOWN

6. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED
 FROM ALL CONTROL FORCE DATA

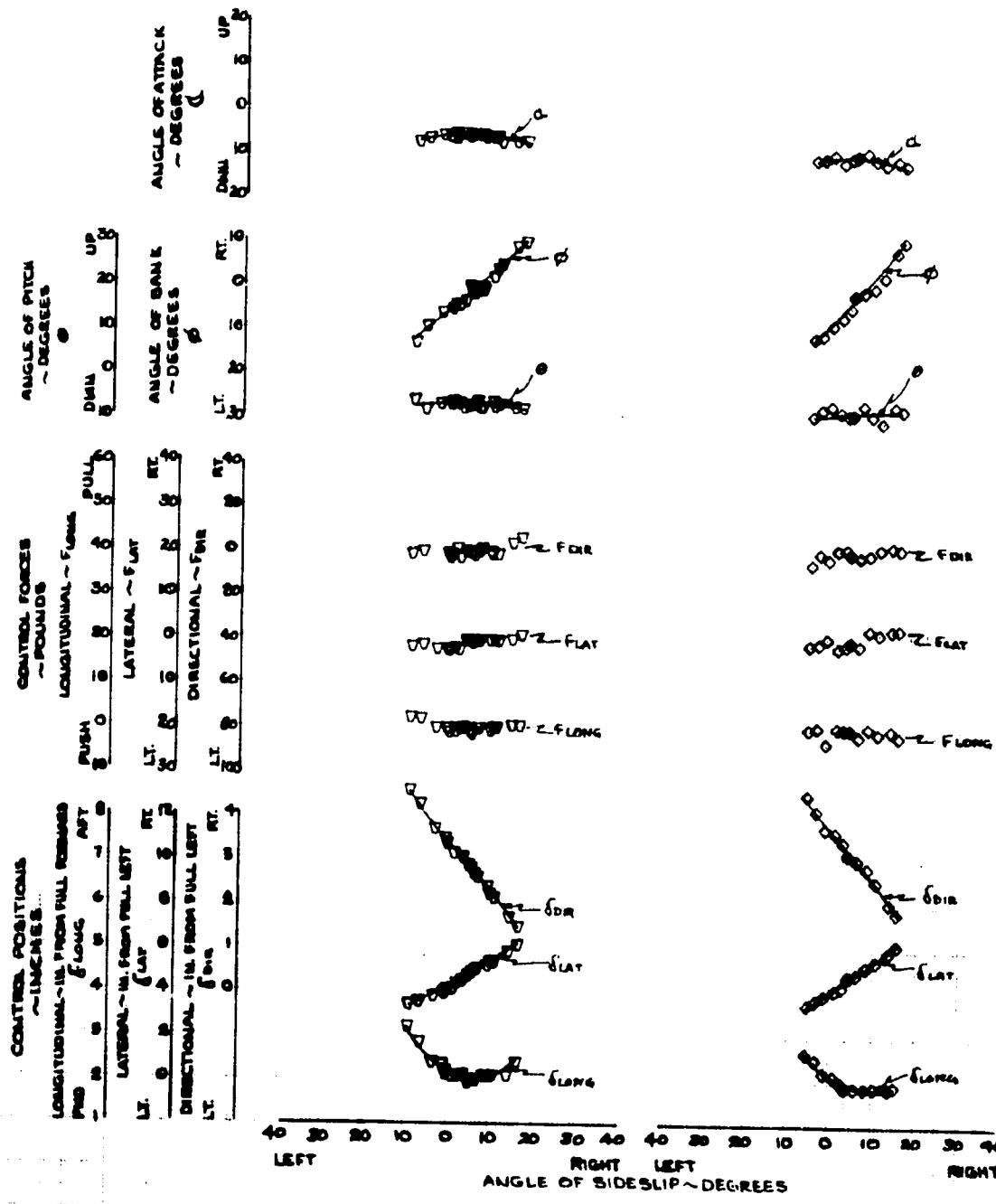


FIGURE NO. 87
STATIC LATERAL DIRECTIONAL STABILITY

AH-1G USA #715645
 HVY HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

DYN.	AIRSPD. ~KCAS	AVG ALT. HO FT.	AVG LONG. C.G. ~IN.	MOTOR RPM	FLT. COND.	THRUST COEF.
▲	68.0	7600	6000	200.0 (AFT)	THRO CLIMB	0.005151
○	67.0	8700	7800	200.0 (AFT)	220.0 AUTOROTATION	0.005000

NOTES: 1. SOLID SYMBOLS. DEMONSTRATE TRIM POINT WITH AIRCRAFT'S BANK ATTITUDE GYRO BALL CENTERED

2. COLLECTIVE POSITION HELD FIXED DURING TEST

3. COLLECTIVE STICK POSITION .25 INCHES PEACELUY FROM FULL DOWN

4. KM-2B CHIN TARGET (STABILIZED)

5. TOTAL CONTROL DISPLACEMENT

LONGITUDINAL: 10.08 INCHES FROM FULL FORWARD

LATERAL: -8.91 INCHES FROM FULL LEFT

DIRECTIONAL: -8.93 INCHES FROM FULL LEFT

COLLECTIVE: -0.98 INCHES FROM FULL DOWN

6. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED FROM ALL CONTROL FORCE DATA

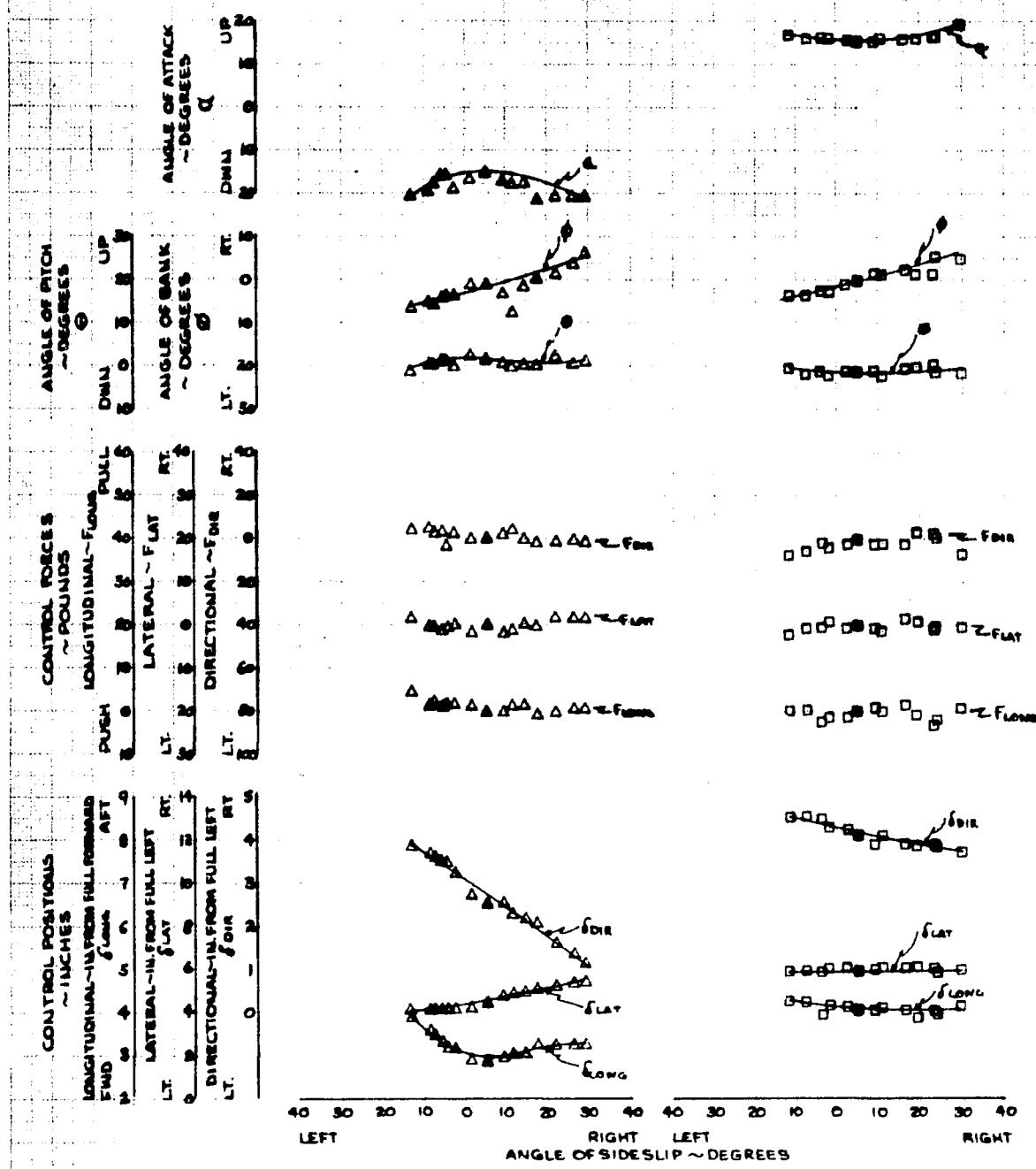


FIGURE NO. 88
STATIC LATERAL DIRECTIONAL STABILITY
AH-1G USAF 15628
MVY. HOG CONFIGURATION WITH HOCKEY POD FAIRINGS REMOVED

SYM.	MESSED	Avg. Alt. ft.	Avg. C.M. ft.	Avg. Low. ft.	Rudder deg.	Fly. Gnd. deg.	Thrust Creep ~ CT
W/CAB	4230	4740	4162 (AFT)	3285	14.0	14.0	0.0
O	4650	4620	4997 (AFT)	5555	14.0	14.0	0.0

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINT WITH AIRCRAFT'S BANK ATTITUDE GYRO BALL CENTERED

2. COLLECTIVE POSITION HELD FIXED DURING TEST

3. COLLECTIVE STICK POSITION - 100 PERCENT FROM FULL DOWN

4. AH-1G CHIN TURRET (STOWED)

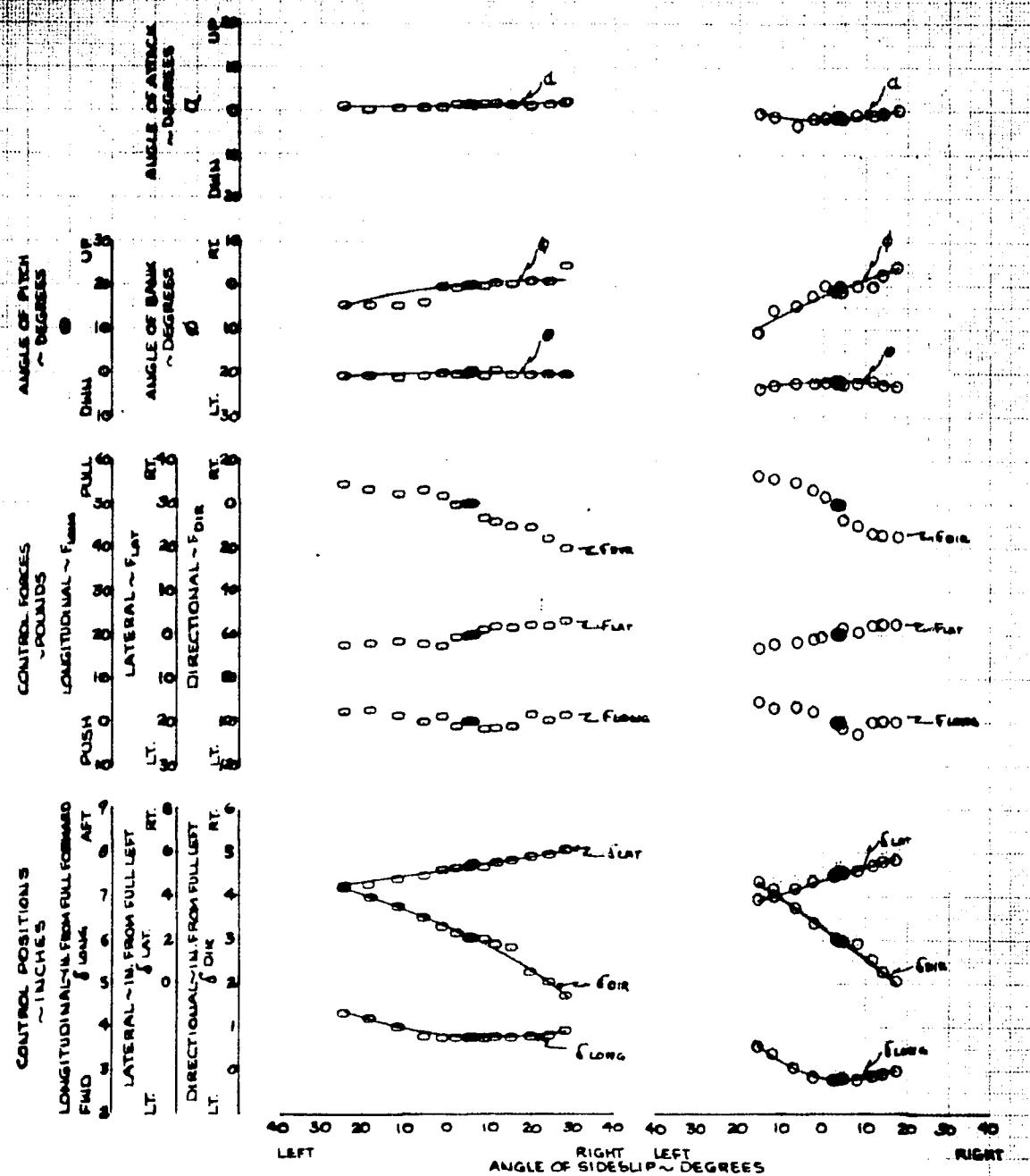
5. TOTAL CONTROL DISPLACEMENT

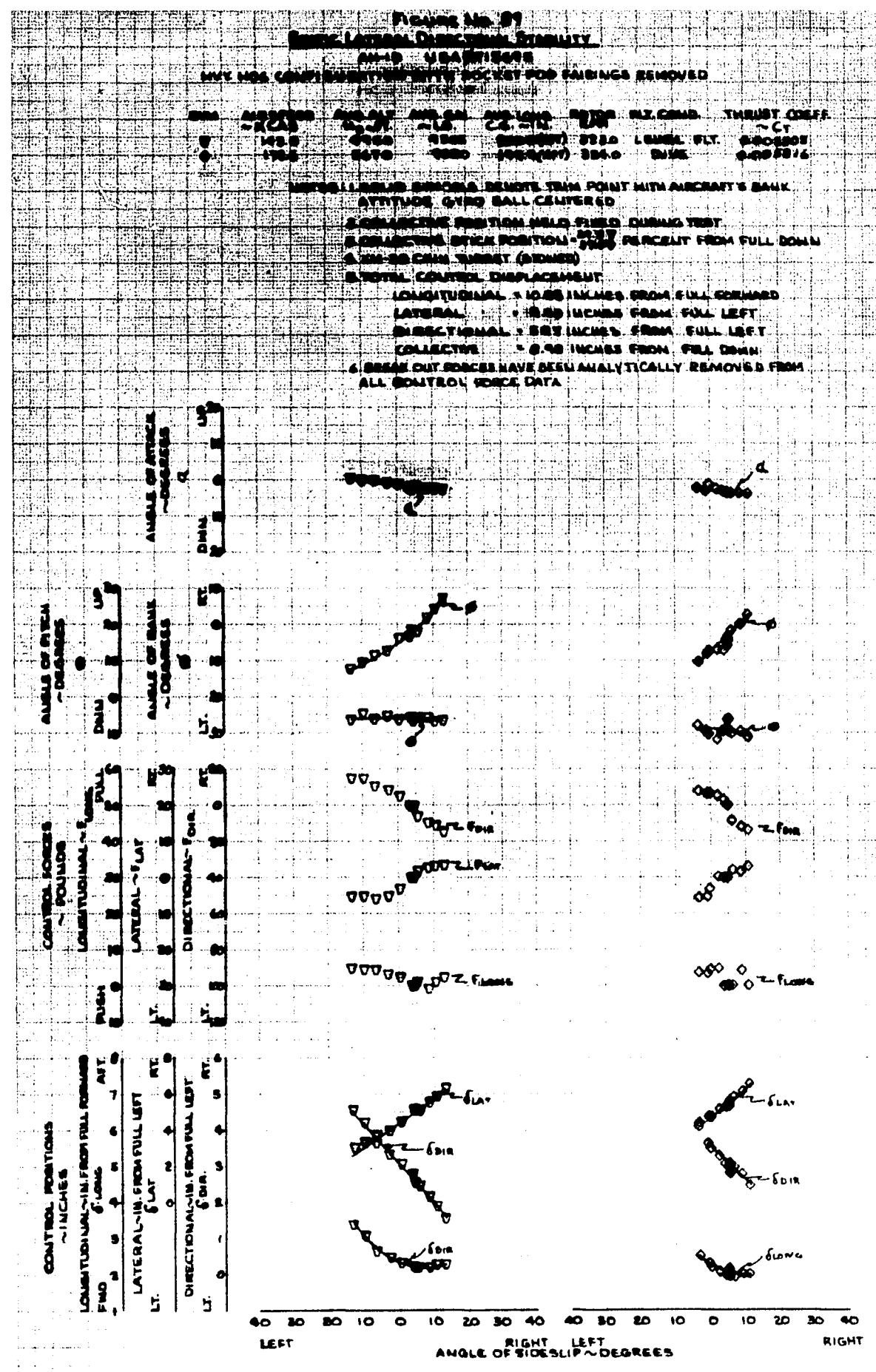
LONGITUDINAL - 10.8 INCHES FROM FULL FORWARD

LATERAL - 14.8 INCHES FROM FULL LEFT

DIRECTIONAL - 5.83 INCHES FROM FULL LEFT

COLLECTIVE - 8.98 INCHES FROM FULL DOWN





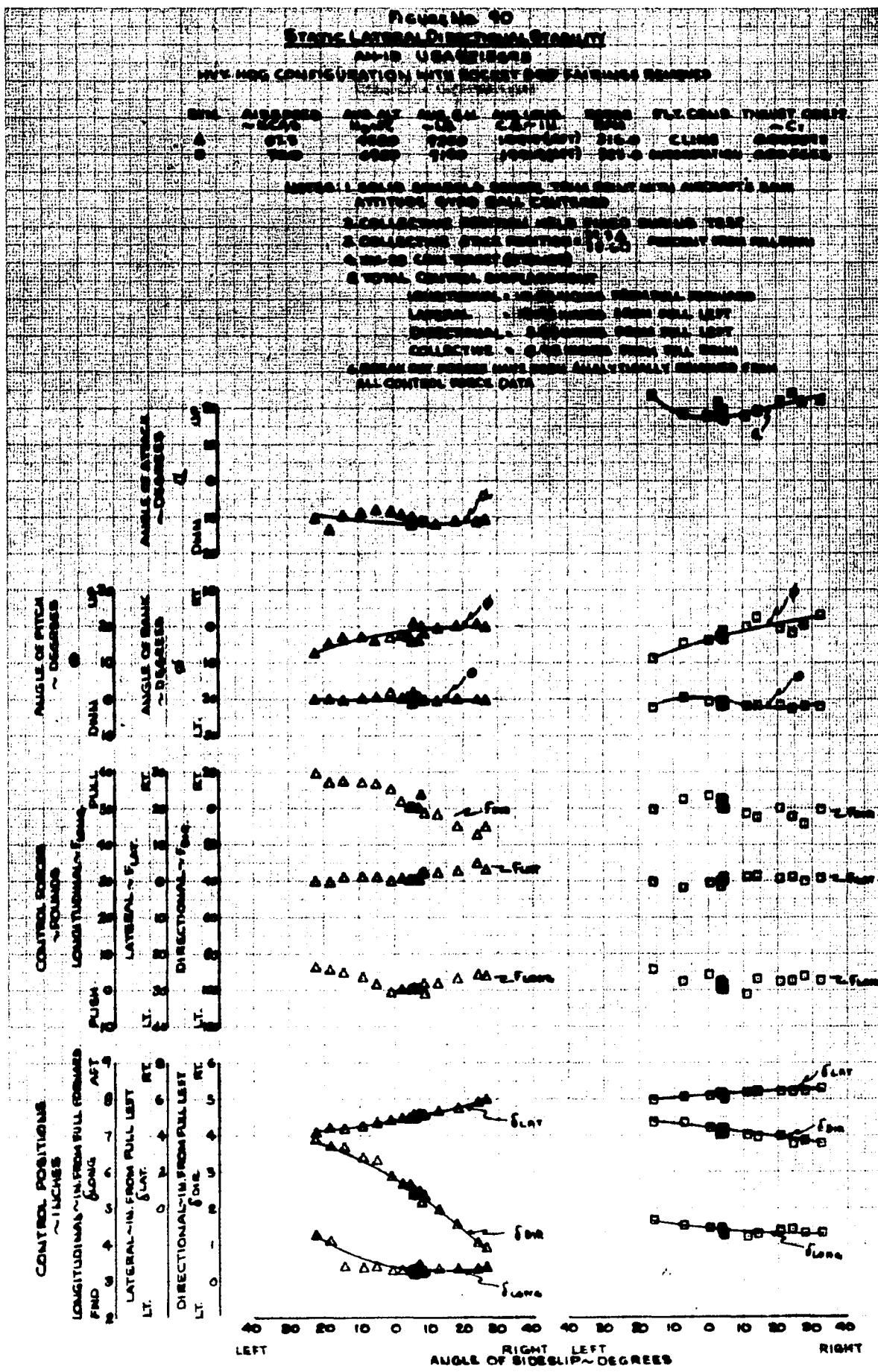


FIGURE NO. 91
STATIC LATENT DIRECTIONAL STABILITY
AH-1G USA #715695

MVY-HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM	AIR SPEED ~KCAS	Avg. Alt. Mo. - FT.	Avg. G.W. ~LB.	Avg. Long. Motor RPM	FLT. COND.	THRUST COEFF. ~CT
O	60.0	10560	8906	200.7 (AFT)	334.0	LEVEL FLT. 0.006569
O	63.0	14280	8395	200.6 (AFT)	326.0	LEVEL FLT. 0.006687

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINT WITH AIRCRAFT'S BANK ATTITUDE GYRO BALL CENTERED

2. COLLECTIVE POSITION HELD FIXED DURING TEST

3. COLLECTIVE STICK POSITION: $\pm 15\%$ PERCENT FROM FULL DOWN

4. KA-20 CHIN TURRET(STOWED)

5. TOTAL CONTROL DISPLACEMENT

LONGITUDINAL = 10.03 INCHES FROM FULL FORWARD

LATERAL = 9.90 INCHES FROM FULL LEFT

DIRECTIONAL = 8.97 INCHES FROM FULL LEFT

COLLECTIVE = 8.96 INCHES FROM FULL DOWN

6. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED
FROM ALL CONTROL FORCE DATA

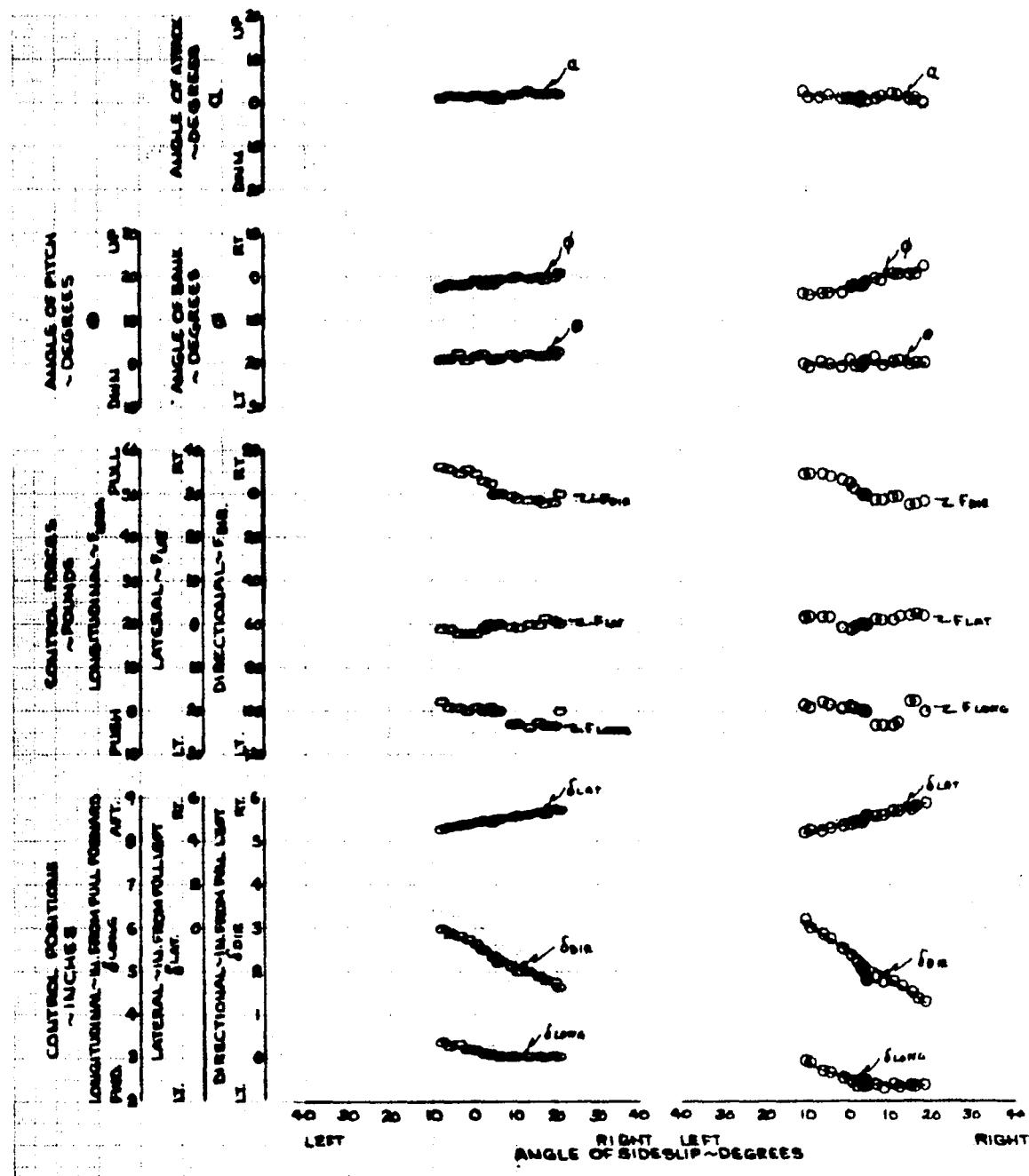


FIGURE NO. 92
STATIC LATERAL DIRECTIONAL STABILITY

AH-1Q USAF 61-0070
 HVY. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM AIRSPEED AVG. ALT. AVG. G.H. AVG. LONG. ROLLER FLT. C.G. THRUST COEF.
 ~KCAS ~FT. ~LS. ~IN. ~PSI ~CT
 □ 101.0 14070 0705 20050FT) 089.0 LEVEL R.P. 0205000

NOTES: 1. SOLID SYMBOLS INDICATE TRIM POINT WITH AIRCRAFT'S BANK
 ATTITUDE OF 60 DEGREE BALL CENTERED
 2. COLLECTIVE POSITION HOLD FIXED DURING TEST
 3. COLLECTIVE BACK POSITION = 31.7 PERCENT FROM FULL DOWN
 4. XM-28 CHIN TURRET (STANDBY)
 5. TOTAL CONTROL DISPLACEMENT
 LONGITUDINAL = 10.0 INCHES FROM FULL FORWARD
 LATERAL = 9.40 INCHES FROM FULL LEFT
 DIRECTIONAL = 8.47 INCHES FROM FULL LEFT
 COLLECTIVE = 8.75 INCHES FROM FULL DOWN
 6. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED FROM
 ALL CONTROL FORCE DATA

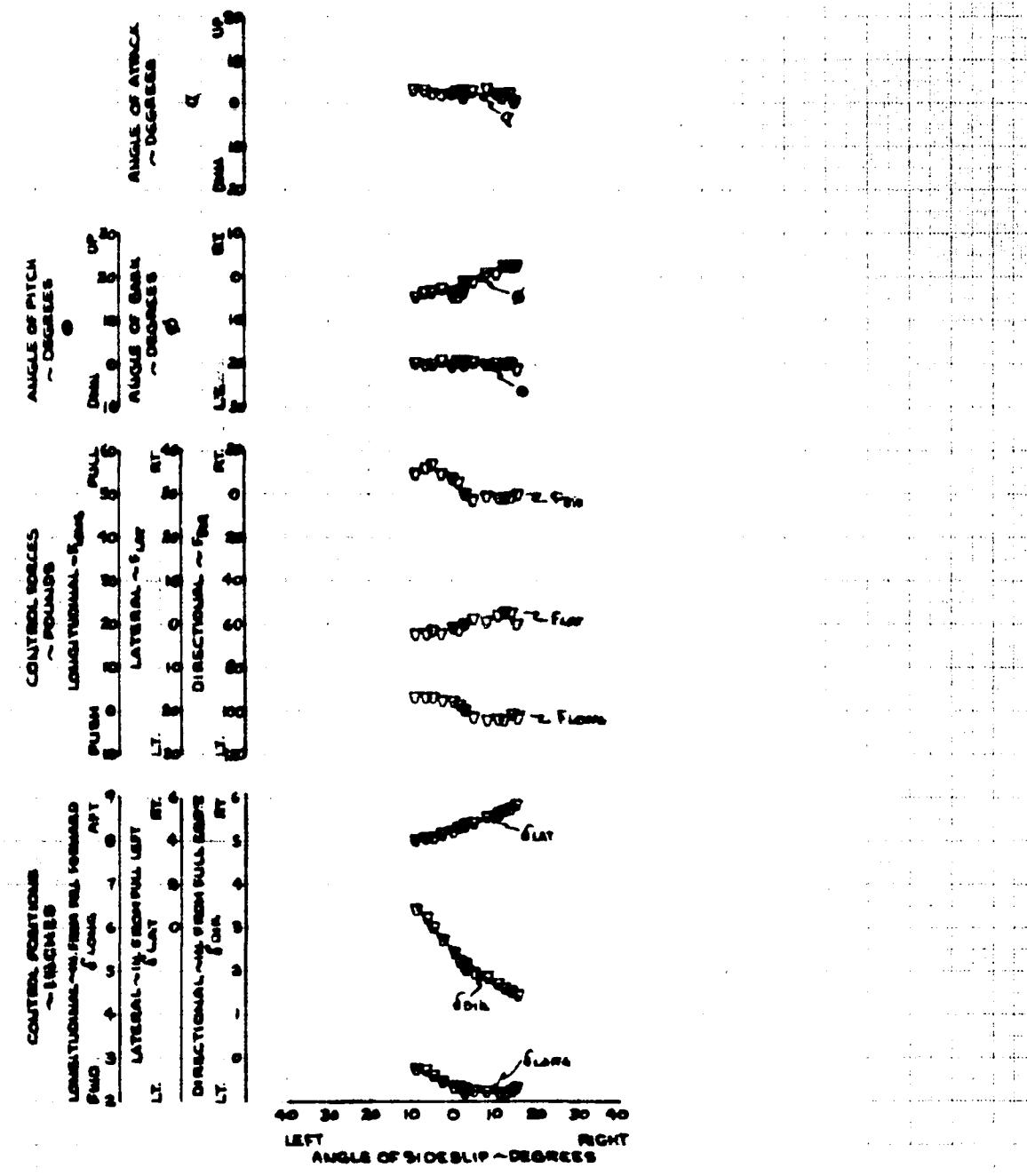


FIGURE NO. 93
STATIC LATERAL DIRECTIONAL STABILITY

AN-1G USAF 66347

MVY. HOG CONFIGURATION WITH REAR TAIL PINS REMOVED
 (REF. FIG. 1)

SYM. ALTITUDE. AVG. ALT. ANG. GLN. AVG. LONG. ROTOR FLT. COND. THRUST COEFF.
 ~KCAS HP-ST. ~LBS. C.G.~IM. RPM ~CT
 6 55.0 13650 6305 3207(AFT) 3340 CLMS 0.00008

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINT WITH AIRCRAFT'S BANK
 ATTITUDE GYRO BALL CENTERED

2. COLLECTIVE POSITION HELD FIXED DURING TEST
 3. COLLECTIVE STICK POSITION = 50% PERCENT FROM FULL DOWN
 4. XM-28 CANN TURRET (STIMED)

5. TOTAL CONTROL DISPLACEMENT

LONGITUDINAL = 10.03 INCHES FROM FULL FORWARD

LATERAL = 9.00 INCHES FROM FULL LEFT

DIRECTIONAL = 6.97 INCHES FROM FULL LEFT

COLLECTIVE = 0.98 INCHES FROM FULL DOWN

6. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED
 FROM ALL CONTROL FORCE DATA

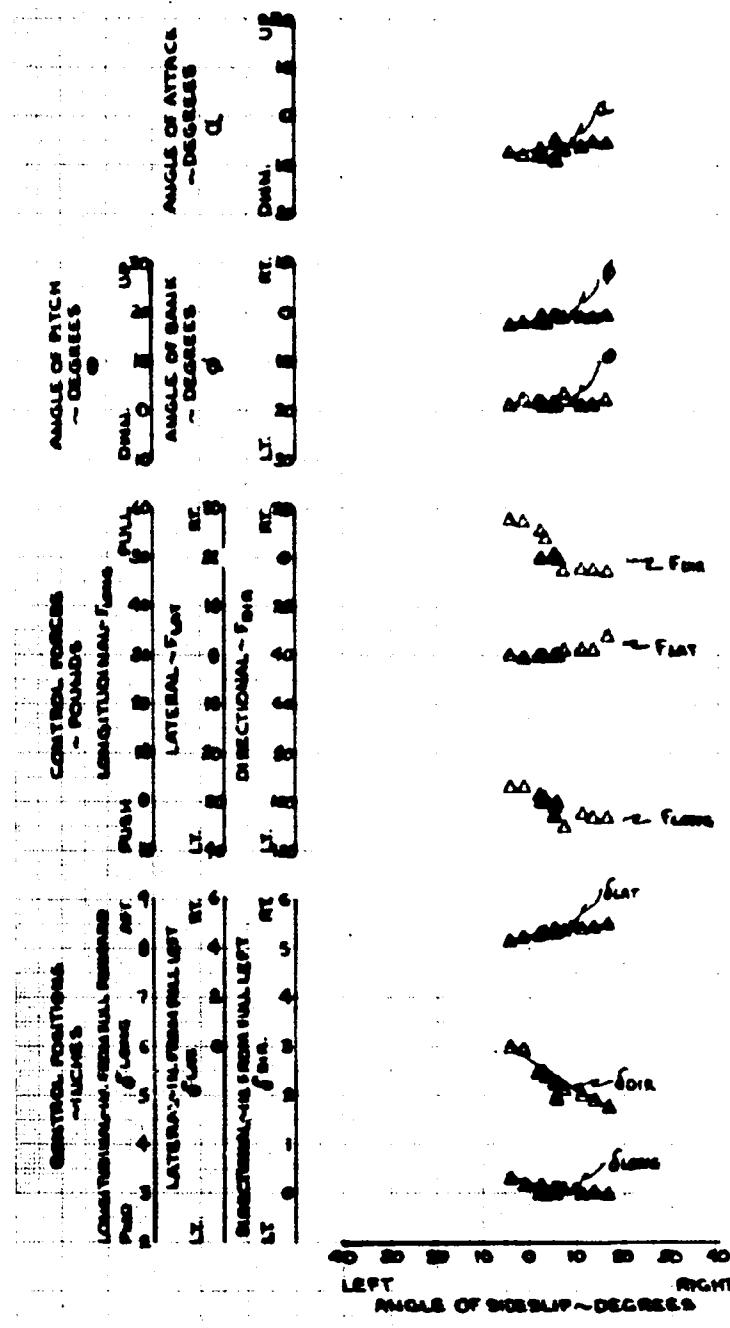


FIGURE No. 94
STATIC LATERAL-DIRECTIONAL STABILITY
 AH-1G USA #6718803

CLEAN CONFIGURATION WITH LANDING GEAR CROSS TUBE FAIRINGS REMOVED

SYM AIRFIELD ANG ALT ANG GM ANG LIFT SPRD FLYING THRUST COEFF
 ~KCAS 10-0° ~10° C.G. -10° 10° ~CT
 0 1100 2000 0720 200.0(FT) 025.0 LEVEL R.E. 0.000016

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINT WITH AIRCRAFT BANKED.

ATTITUDE GYRO BALL CENTERED

2. COLLECTIVE POSITION HELD FIXED DURING TEST

3. COLLECTIVE STICK POSITION = 30.5 PERCENT FROM FULL DOWN

4. EA-28 CHIN TURRET (STATION)

5. TOTAL CONTROL DISPLACEMENT:

LONGITUDINAL = 9.07 IN. FROM FULL FORWARDED

LATERAL = 10.0 IN. FROM FULL LEFT

DIRECTIONAL = 7.07 IN. FROM FULL LEFT

COLLECTIVE = 9.80 IN. FROM FULL DOWN

6. BREAK OUT FORCES HAVE BEEN ANALYTICALLY REMOVED
 FROM ALL CONTROL FORCE DATA

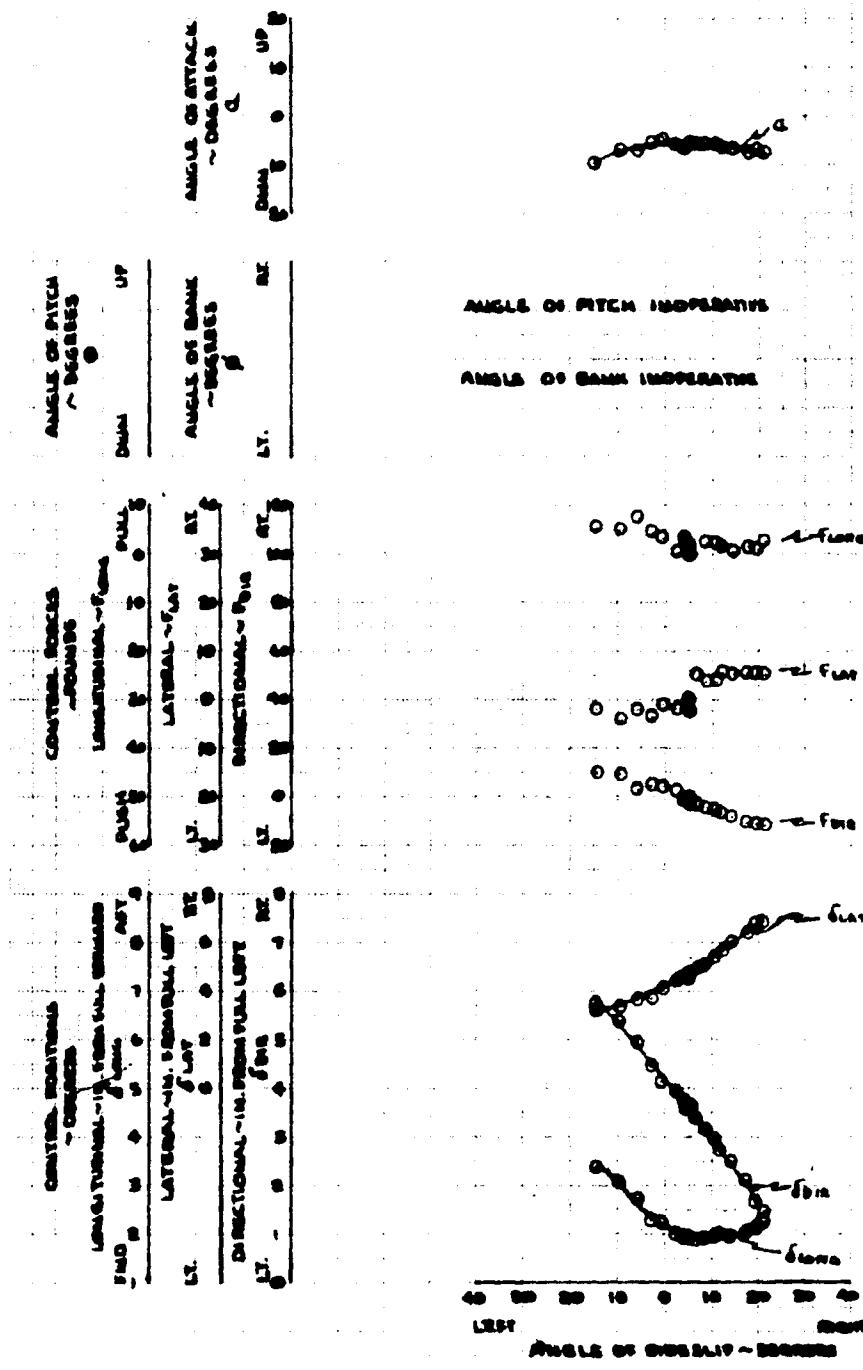


FIGURE NO. 95
STATIC LATERAL-DIRECTIONAL STABILITY

AM-1A USA 651534T
 C15AN CONFIGURATION WITH DANDIE GEAR CROSS TUBE FAIRINGS REMOVED

SYM AILERON ANGLE AND ALL ANGLE-OF-ATTITUDE SENSORS FLG. CONST. THRUST COEFF.
 $\Delta C_{L\alpha} = 148.0 \quad \Delta C_{M\alpha} = 0.000000 \quad C_{L\alpha} = 1.00$

0 148.0 0.000 0.000 (NAT) 0.000.0 LEVEL FLG 0.000000

0 148.0 0.000 0.000 0.000 (DRAFT) 0.000.0 DIVE 0.000000

NOTES: 1. SOLID SYMBOLS DENOTE TRIM POINT WITH AIRCRAFT BANK

ATTITUDE GYRO BALL CENTERED

2. COLLECTIVE POSITION HELD FIXED DURING TEST

3. COLLECTIVE STICK POSITION - 44.0 PERCENT FROM FULL DOWN

4. XM-20 CHIN TURRET (STOWED)

5. TOTAL CONTROL DISPLACEMENT:

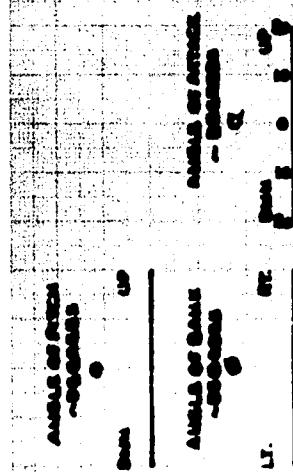
LONGITUDINAL - 9.07 IN. FROM FULL FORWARD

LATERAL - 10.00 IN. FROM FULL LEFT

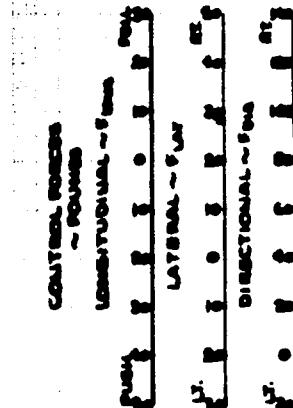
DIRECTIONAL - 7.07 IN. FROM FULL LEFT

COLLECTIVE - 9.30 IN. FROM FULL DOWN

6. BREAKOUT FORCES HAVE BEEN ANALYTICALLY REMOVED
 FROM ALL CONTROL FORCE DATA



ANGLE OF PITCH INOPERATIVE



ANGLE OF BANK INOPERATIVE

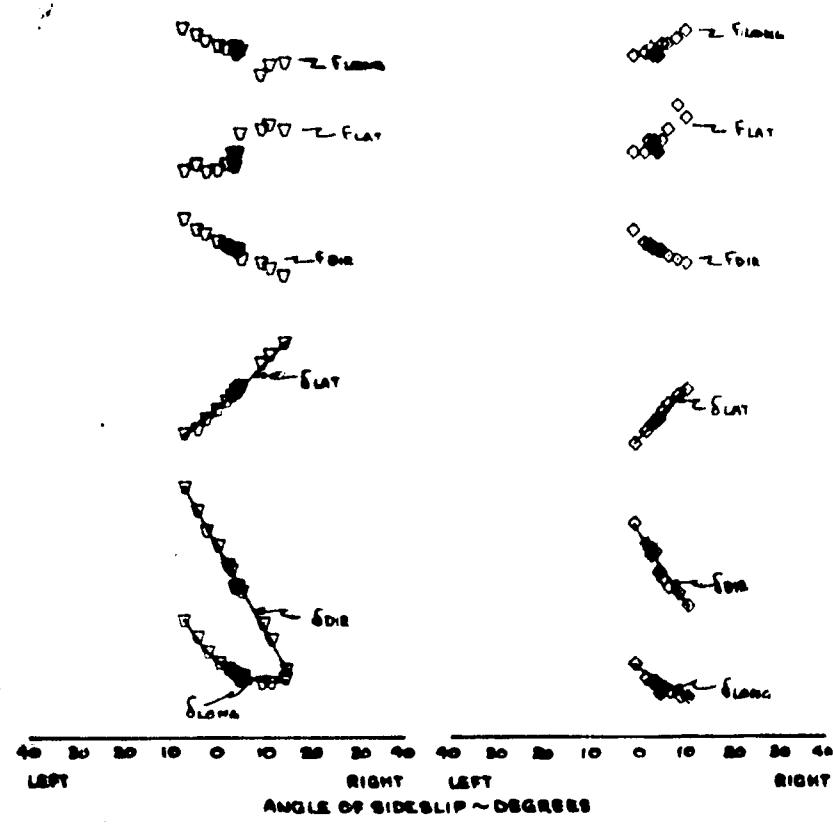
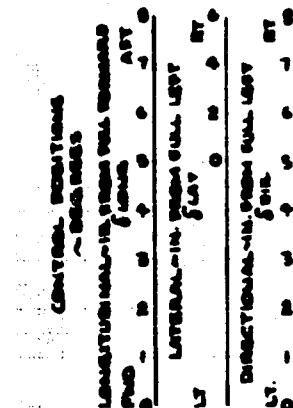


FIGURE NO. 96
IGE HOVERING IN WIND
FOR A TEN PERCENT DIRECTIONAL CONTROL MARGIN

AH-1G USA #NG15247

TSB-L-1B % LE14001

SKID HEIGHT = THREE FEET

- NOTES:
1. POINTS DERIVED FROM NO. 91 THROUGH 100 APP. VII
 2. WIND VELOCITY PRESENTED FOR CRITICAL WIND AZIMUTH
 3. SEVEN FOOT SKID HEIGHT REPRESENTS MOST CRITICAL CONDITION.
 4. FULL LEFT DIRECTIONAL CONTROL - 19° TAIL ROTOR BLADE ANGLE
 5. 10 PERCENT DIRECTIONAL CONTROL REMAINING FROM MEAN CONTROL POSITION REQUIRED DURING STABILIZED HOVER
 6. YAW SCAS OFF
 7. STANDARD DAY

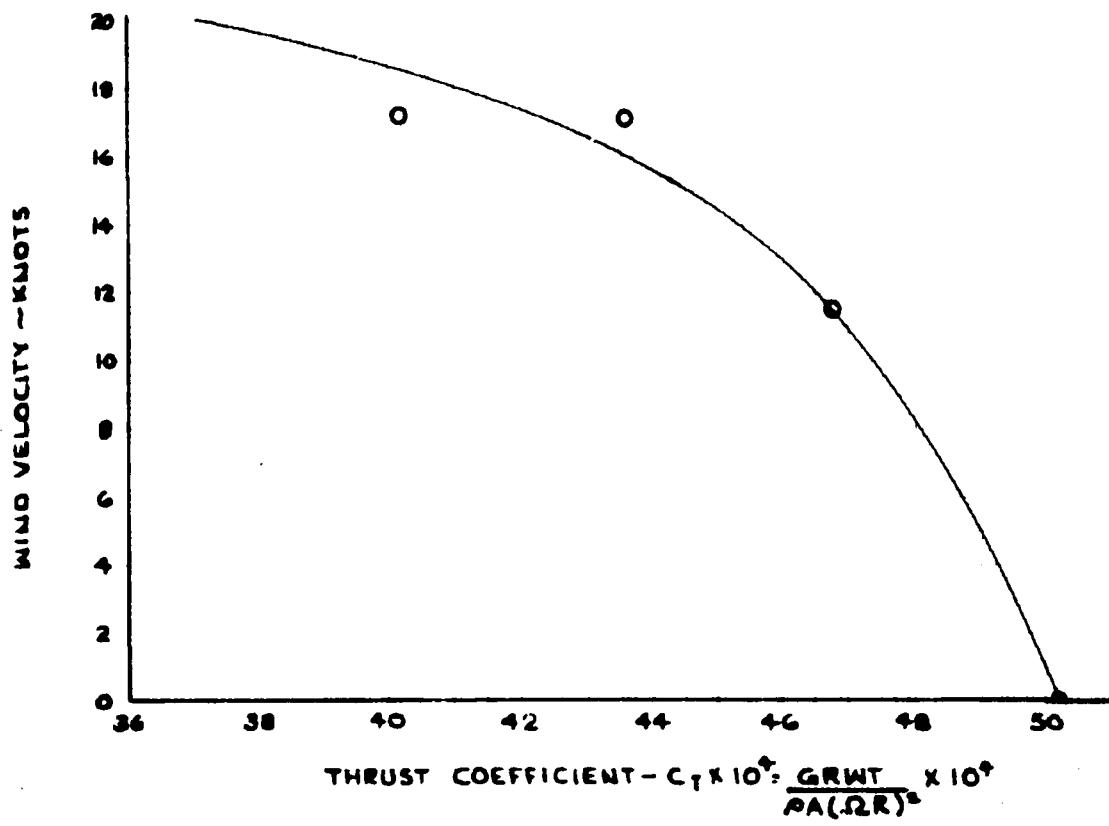


FIGURE NO. 97
DIRECTIONAL CONTROL SUMMARY
AH-1G USA S/N 615247

HVY SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED
ALTITUDE GROSS WEIGHT LONG. C.G. ROTOR SPEED THRUST COEFF.
 $H_0 \sim \text{FT}$ ~ LB ~ IN. ~ RPM ~ C_T
140 8060 200.4(AFT) 324 0.004018

NOTES:

1. 10% DIRECTIONAL CONTROL REMAINING FROM MEAN CONTROL POSITION REQUIRED DURING STABILIZED FLIGHT CONDITION

2. YAW SCAS OFF

3. TOTAL DIRECTIONAL CONTROL DISPLACEMENT = 707 IN FROM FULL LEFT

4. SHADED AREAS REPRESENT LESS THAN 10% DIRECTIONAL CONTROL MARGIN

5. POINTS DERIVED FROM FIGURES 101 THROUGH 107, APPENDIX

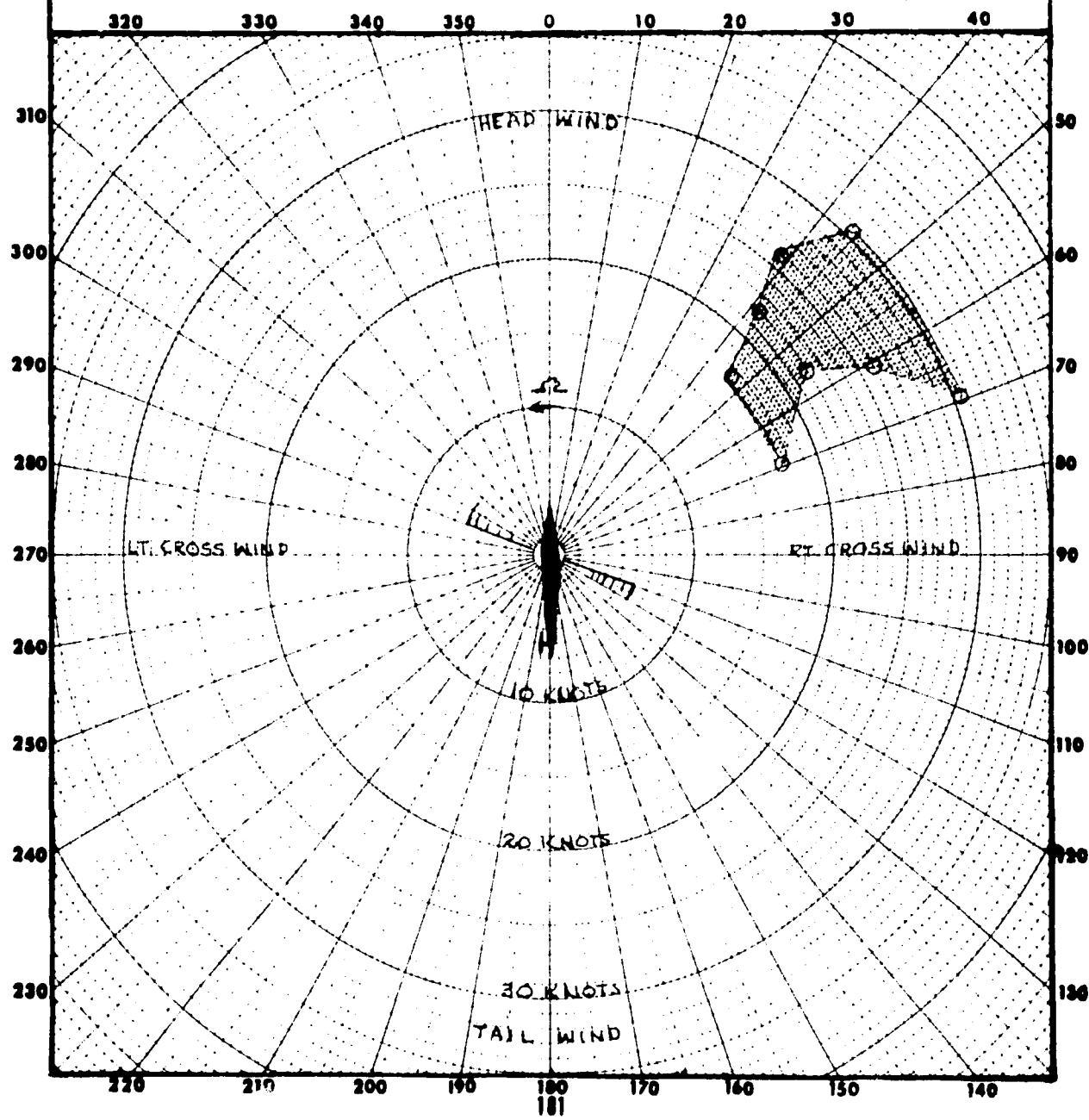


FIGURE NO. 98
DIRECTIONAL CONTROL SUMMARY

AH-1G USA SN 615247

HVV. SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED
 ALTITUDE GROSS WEIGHT LONG.C.G. ROTOR SPEED THRUST COEFF.
 H₀~FT. ~LB. ~IN. ~RPM ~C_T
 -40 8245 199.6(AFT) 314 0.004353

NOTES:

1. 10% DIRECTIONAL CONTROL REMAINING FROM MEAN CONTROL POSITION REQUIRED DURING STABILIZED FLIGHT CONDITION
2. YAW SCAS OFF
3. TOTAL DIRECTIONAL CONTROL DISPLACEMENT = 7.07 IN. FROM FULL LEFT
4. SHADED AREA REPRESENTS LESS THAN 10% DIRECTIONAL CONTROL MARGIN
5. POINTS DERIVED FROM FIGURES 108 THROUGH 114, APP. VII

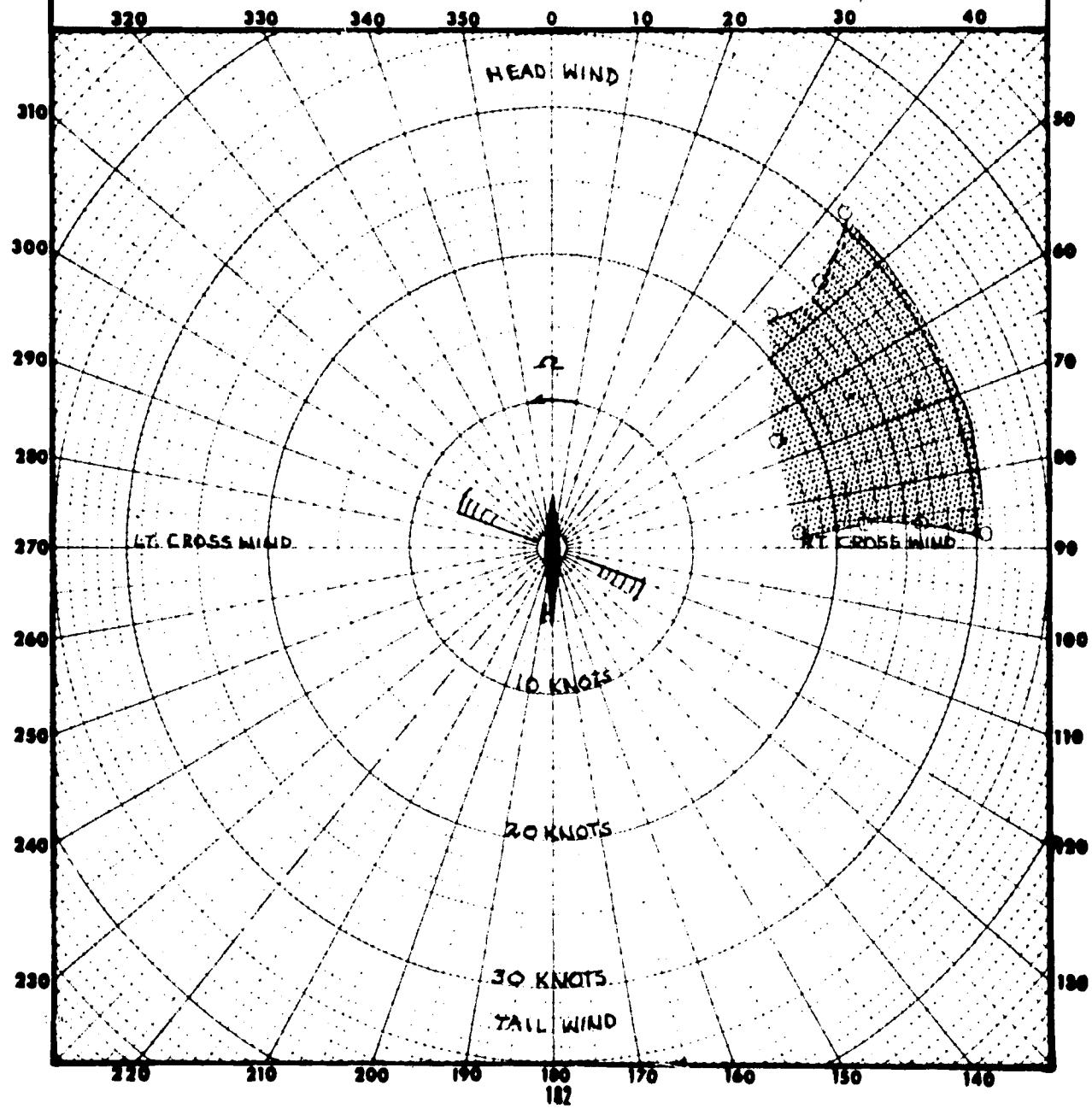


FIGURE No. 99
DIRECTIONAL CONTROL SUMMARY

AH-1G USA 4N615247

HVV SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

ALTITUDE HD~FT	GROSS WEIGHT ~LB.	LONG.C.G. ~IN.	ROTOR SPEED ~RPM	THRUST COEFF ~CT
5270	8050	200.7(AFT)	324	0.004678

NOTES:

1. 10% DIRECTIONAL CONTROL REMAINING FROM MEAN CONTROL POSITION REQUIRED DURING STABILIZED FLIGHT CONDITION
2. YAW SCAS OFF
3. TOTAL DIRECTIONAL CONTROL DISPLACEMENT = 7.07 IN. FROM FULL LEFT
4. SHADED AREA REPRESENTS LESS THAN 10% DIRECTIONAL CONTROL MARGIN
5. POINTS DERIVED FROM FIGURES 118 THROUGH 121 APP VII

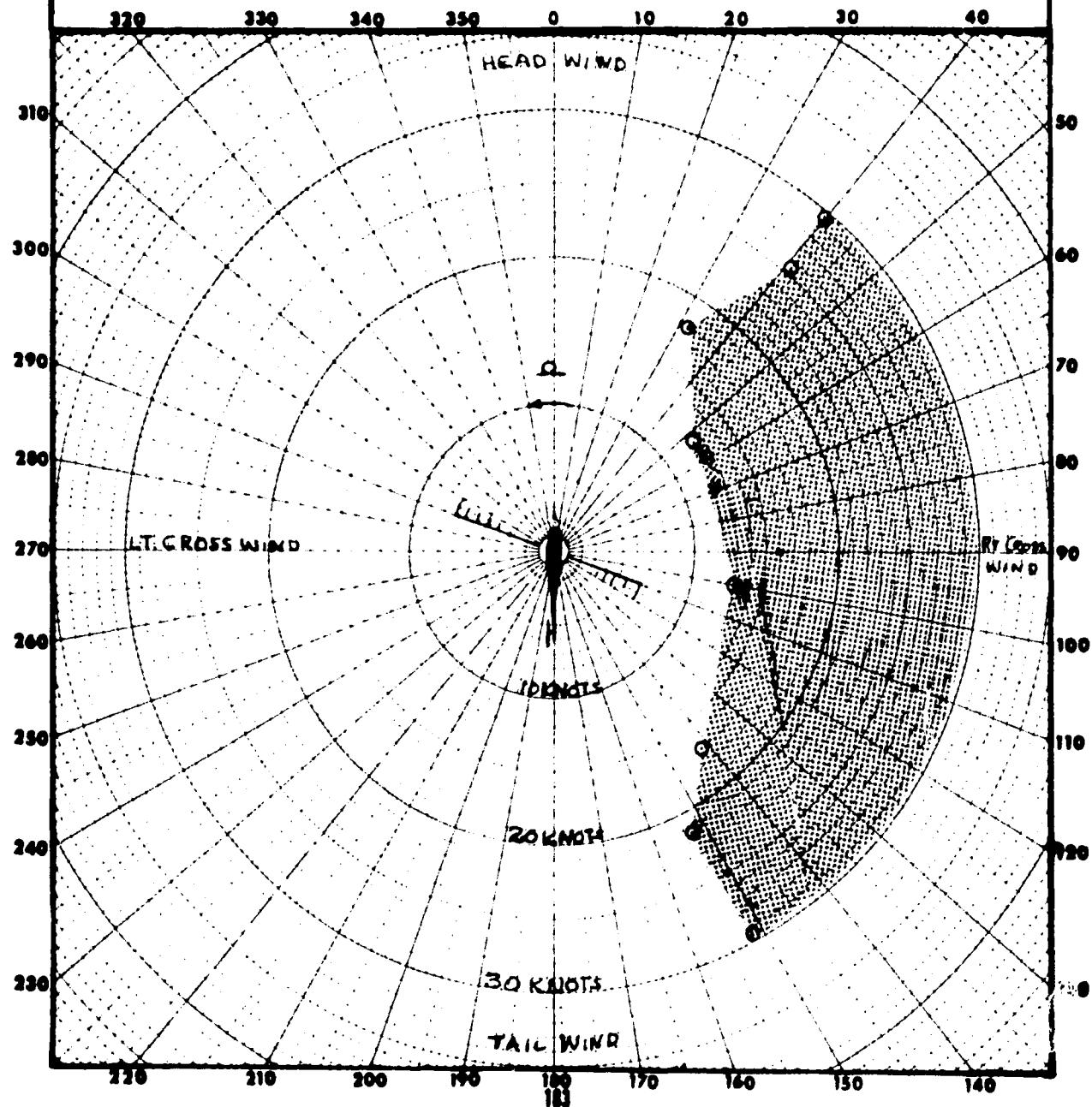


FIGURE NO 100
DIRECTIONAL CONTROL SUMMARY

AH-1G USAW 615247

HVY. SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

ALTITUDE HD~FT.	GROSS WEIGHT ~LB	LONG.CG. ~IN.	ROTOR SPEED ~RPM	THRUST COEFF. ~CT
11120	7210	195.4(MID)	324	0.005023

NOTES:

1. 10% DIRECTIONAL CONTROL REMAINING FROM MEAN CONTROL POSITION REQUIRED DURING STABILIZED FLIGHT CONDITION
2. YAW SCAS OFF
3. TOTAL DIRECTIONAL CONTROL DISPLACEMENT = 7.07 IN. FROM FULL LEFT
4. SHADED AREA REPRESENTS LESS THAN 10% DIRECTIONAL CONTROL MARGIN
5. POINTS DERIVED FROM FIGURES 122 THROUGH 124 APP VII

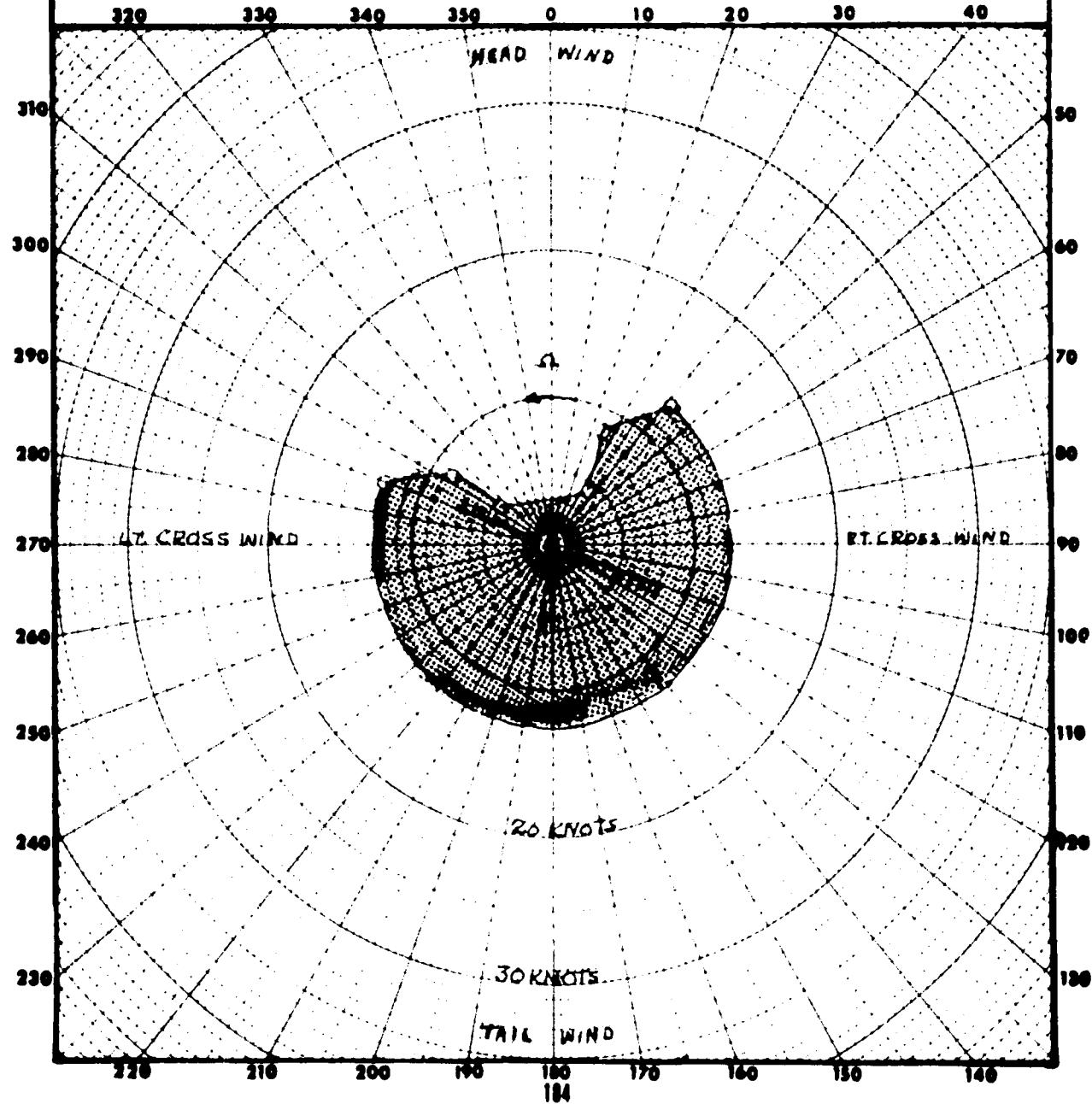


FIGURE NO. 1C
STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WIND AZIMUTH
AH-1G USA #615267
HVV SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

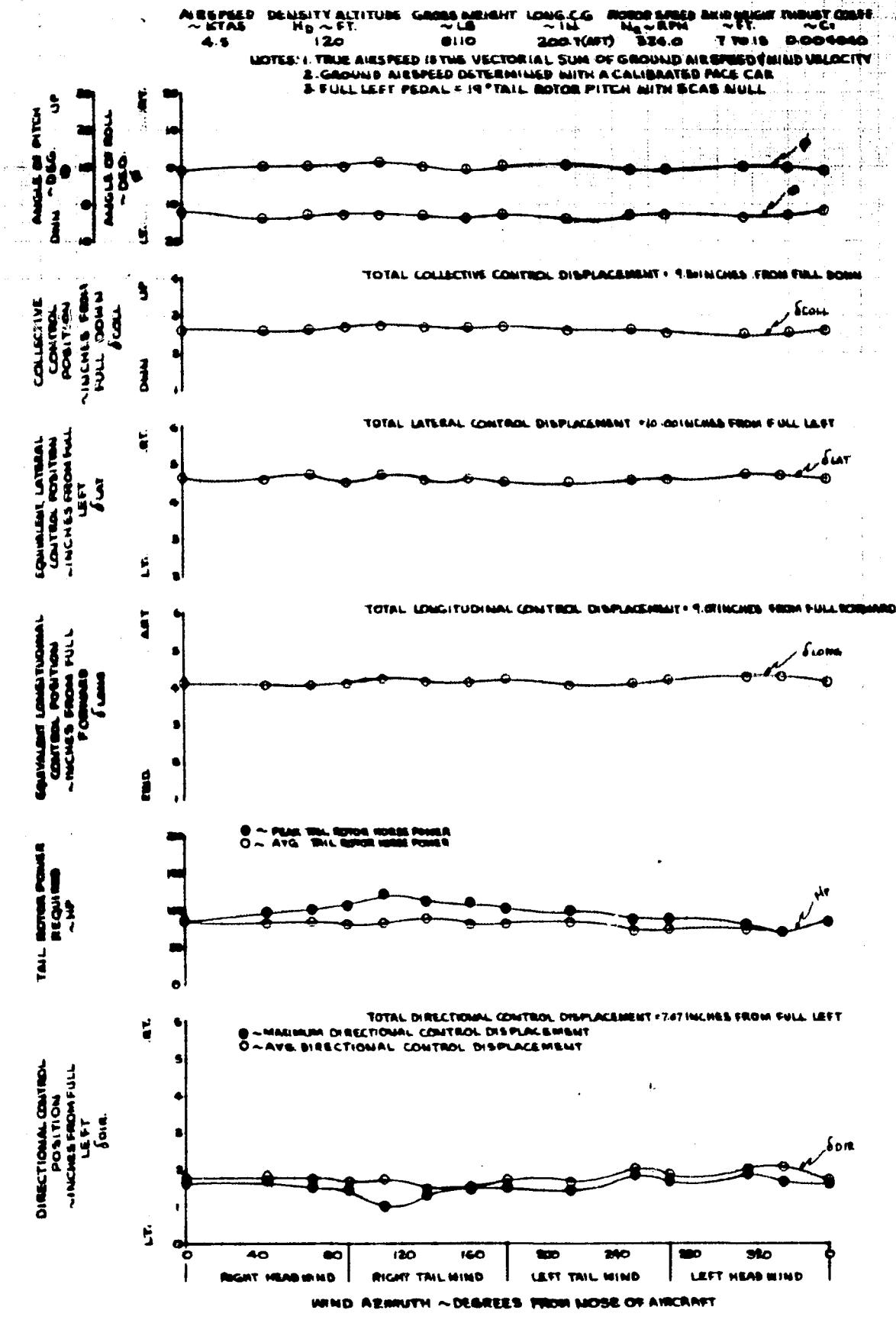


FIGURE NO. 102
STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WIND AZIMUTHS
AH-1G USAF 615267
MVY SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

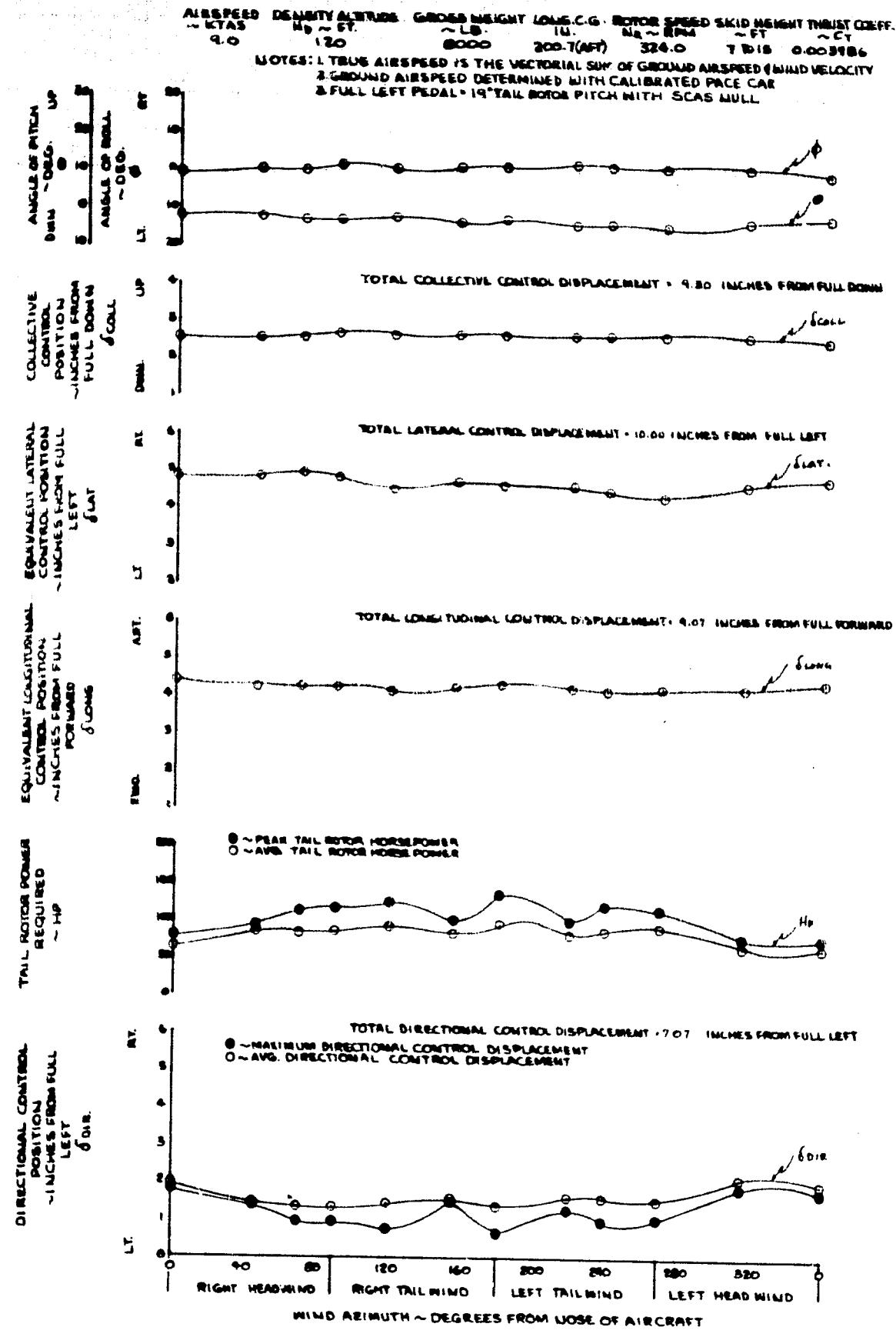


FIGURE NO 103
STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WIND AZIMUTH
AH-1G USA #615247
MVY SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

AIR SPEED DENSITY ALTITUDE GROSS WEIGHT LONG.C.G. ROTOR SPEED SKID HEIGHT THUST COEF.
~KTAS H_d ~FT ~LB ~IN. NR ~RPM ~FT ~CV
13.0 120 8000 200.5(AFT) 324.0 7 TO 15 0.0004026

NOTES: 1. TRUE AIRSPEED IS THE VECTORIAL SUM OF GROUND AIRSPEED & WIND VELOCITY

2. GROUND AIRSPEED DETERMINED WITH CALIBRATED PACE CAR

3. FULL LEFT PEDAL • 19° TAIL ROTOR PITCH WITH SCAS NULL

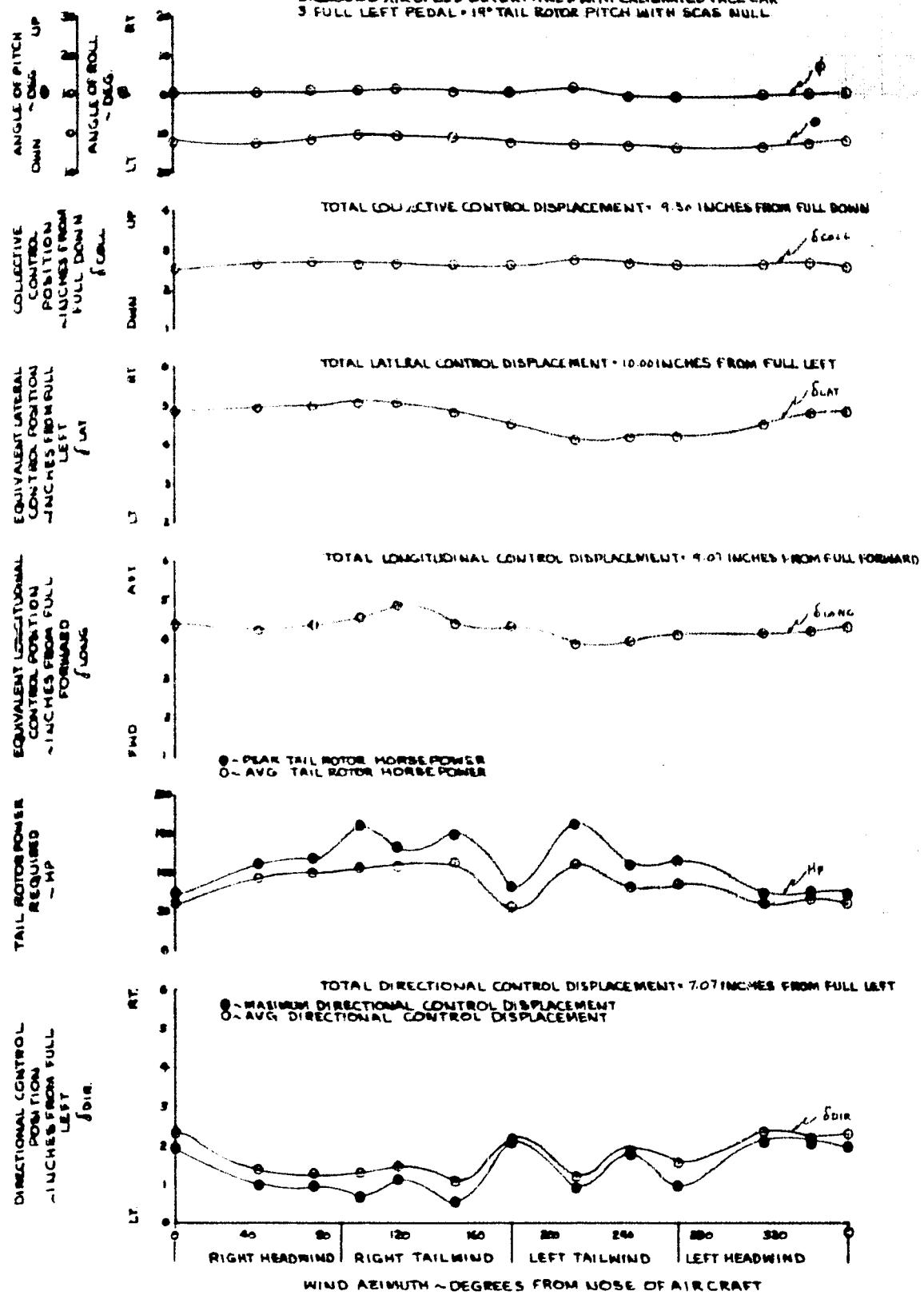


FIGURE NO. 106
 STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WIND AZIMUTH
 AH-1G USA 2615207
 NVY SCOUT CONFIGURATION WITH ROCKET POD ENGINES REMOVED

AIRSPED - ALTITUDE: CRUISE HEIGHT, LONG C.G. MOTOR SPINNED DOWN AIRPORT TURBULENT CLOUDS
 ~1700' MD ~67' ~10' ~10' NA ~10' ~5' ~5'
 17.5 120 0000 2000 (ADP) 324.0 77010 0000016

NOTES: 1. THIS AIRSPED IS THE VECTORIAL SUM OF GROUND AIR SPEED AND WIND VELOCITY
 2. GROUND AIR SPEED DETERMINED WITH CALIBRATED RACE CAR
 3. FULL LEFT PEDAL, 14° TAIL AILERON PITCH WITH SCAB MULL

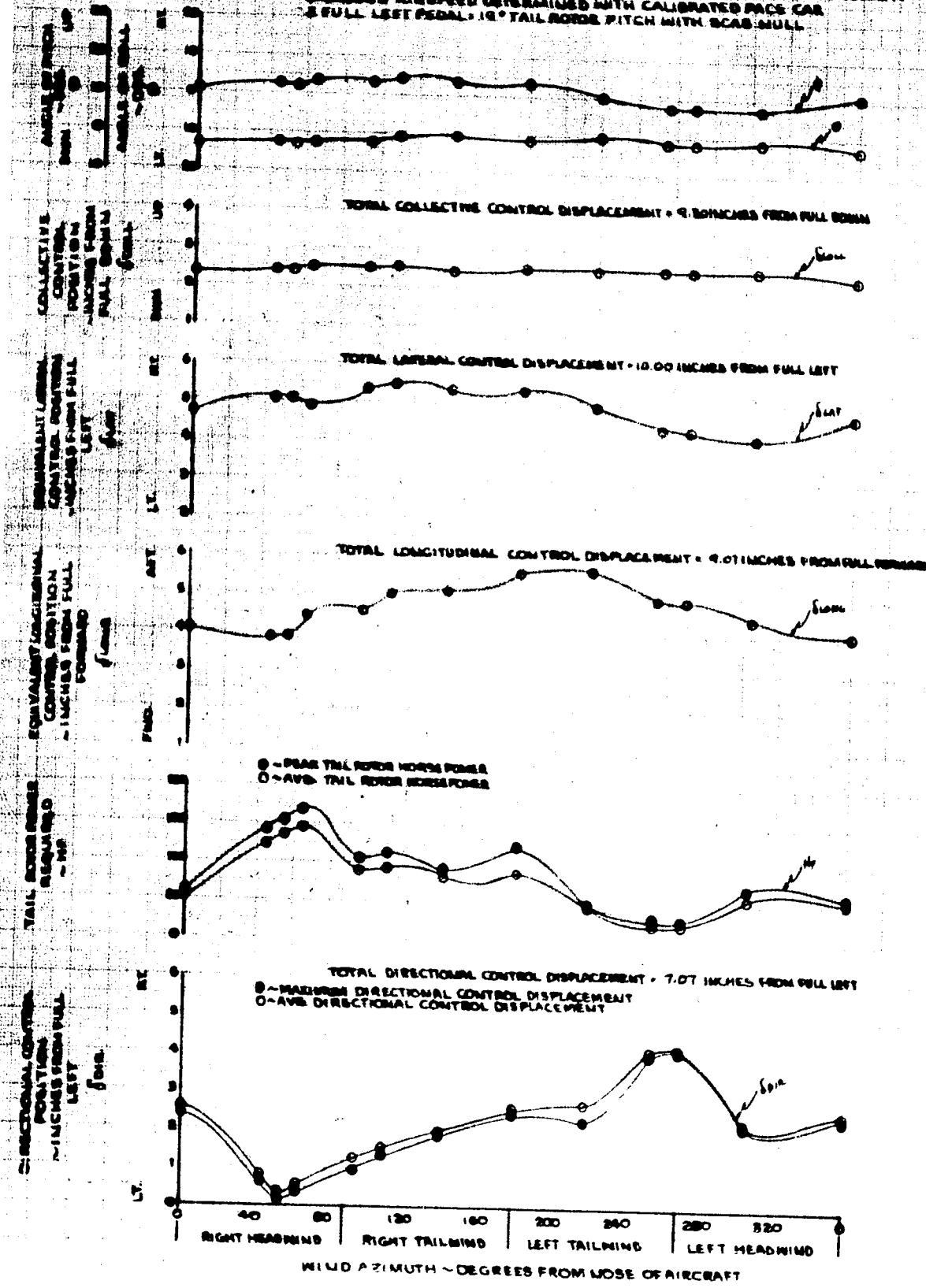


FIGURE NO. 105
STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WIND AZIMUTH
AN-1G USAF 615267
KVV. SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

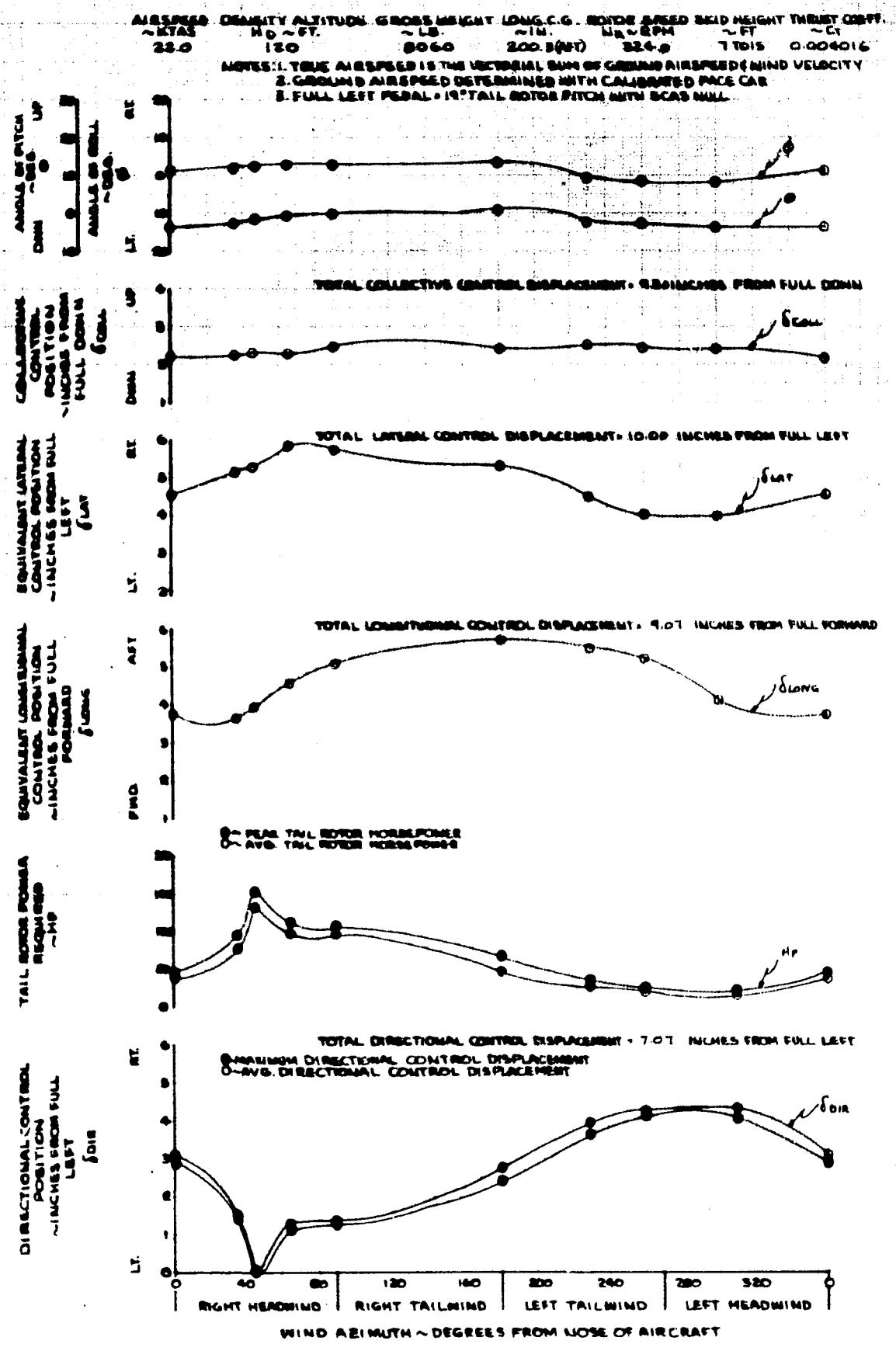


FIGURE NO. 106
STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WIND AZIMUTH
AH-1G USA FG152AT
HVV SCOUT CONFIGURATION WITH BOOM POD FAIRINGS REMOVED

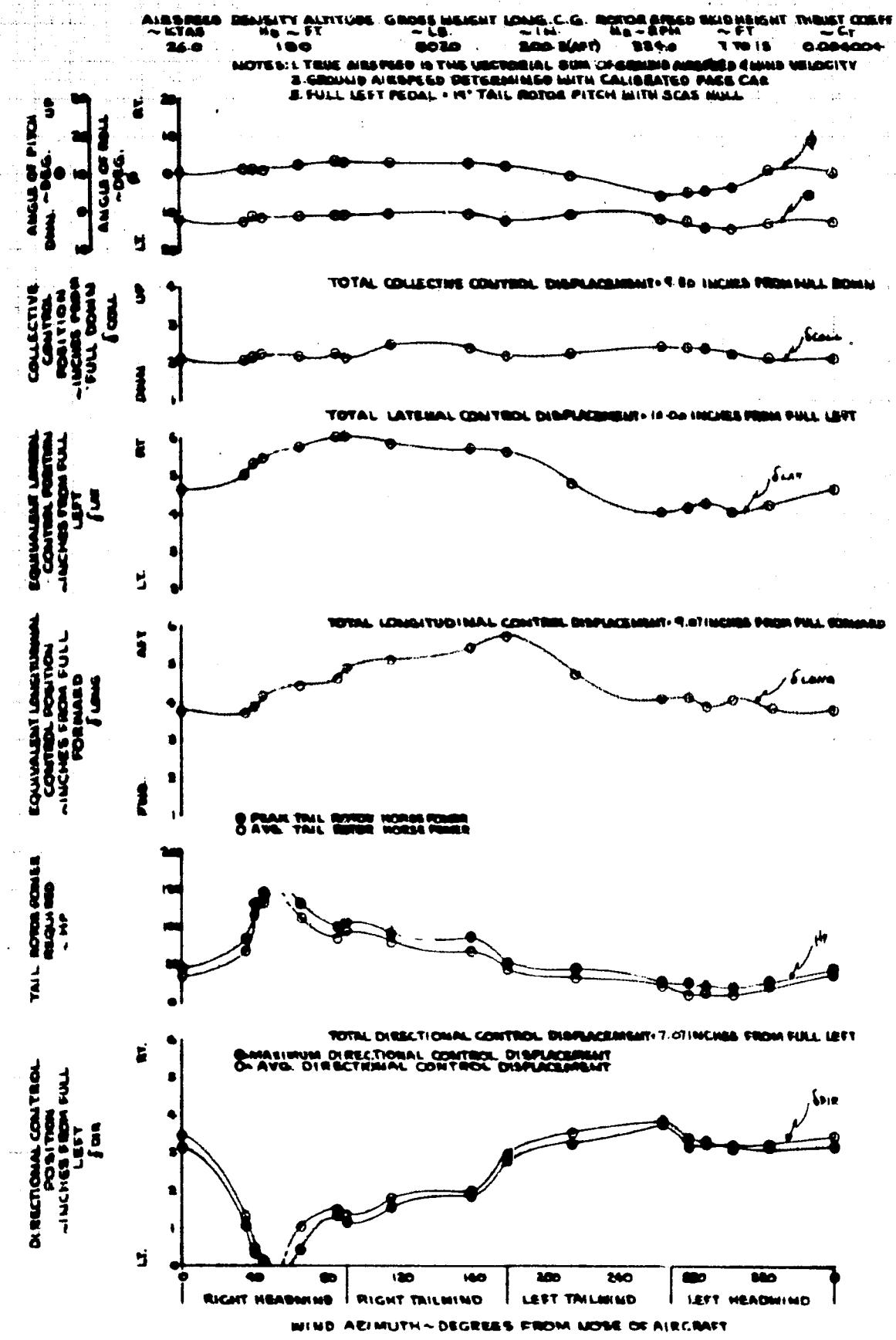


FIGURE NO. 107
STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WIND AZIMUTHS
AM-IC USA #618267
HUV SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

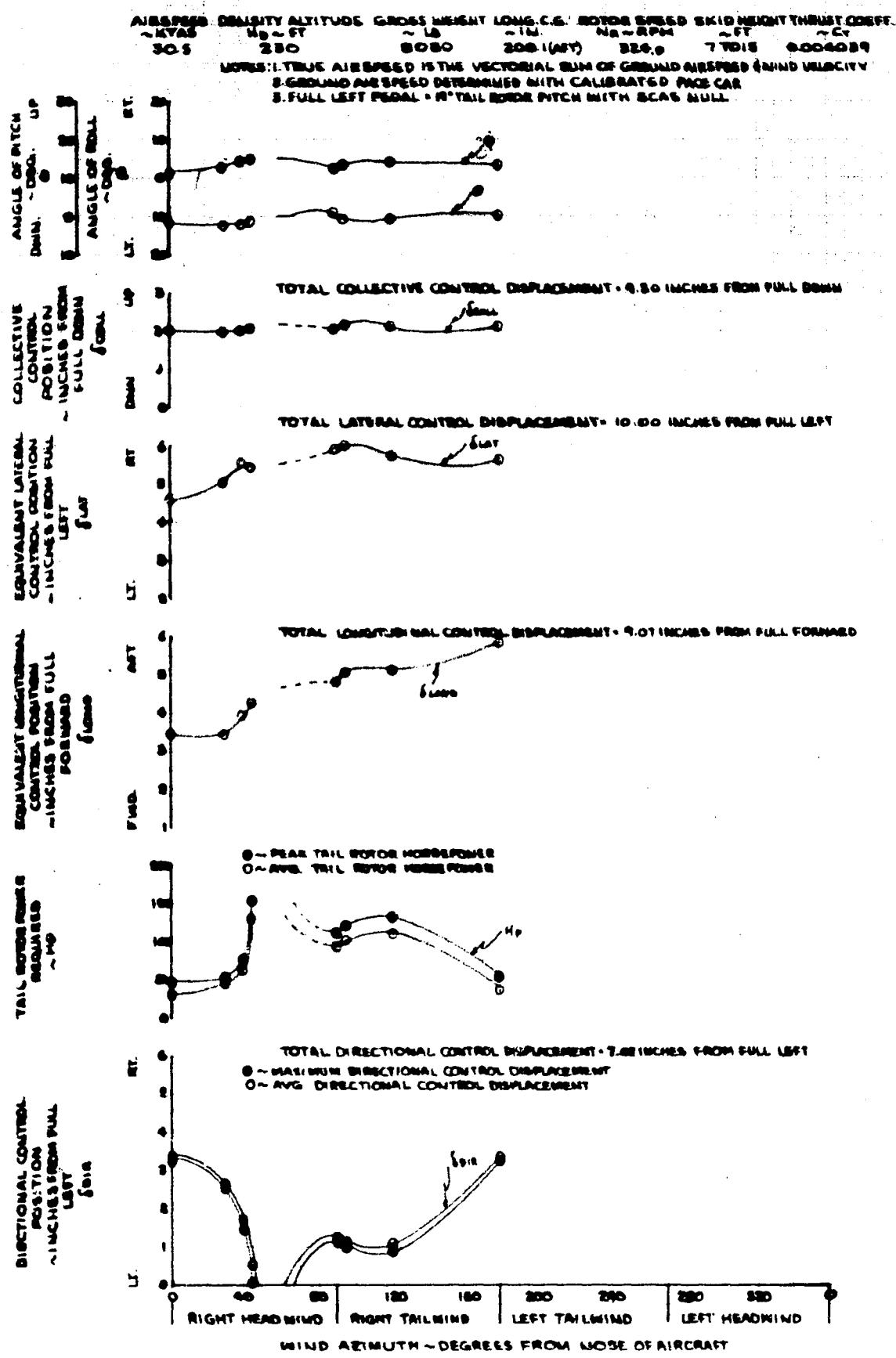


FIGURE NO. 108
STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WIND AZIMUTH
AH-1G USA #612367

MVT. SCOUT CONFIGURATION WITH ROCKET PODS/SHELVES REMOVED

AIRFOIL DENSITY ALTITUDE GROSS WEIGHT LOAD C.G. MOTOR SPEEDS SHD WEIGHT THRUST COEFF.
~STAB ~10 ~5T ~15 ~1000 ~1000 ~1000 ~C₁
0.6 500 5000 5000 5000 5000 5000 5000

NOTES: 1. TIME AVERAGE IS THE VERTICAL SUM OF GROUND AIRSPEED & WIND VELOCITY
2. GROUND AIRSPEED DETERMINED WITH CALIBRATED RACE CAR
3. FULL LEFT PEDAL & 10° TAIL MOTOR PITCH WITH SCAT MULL

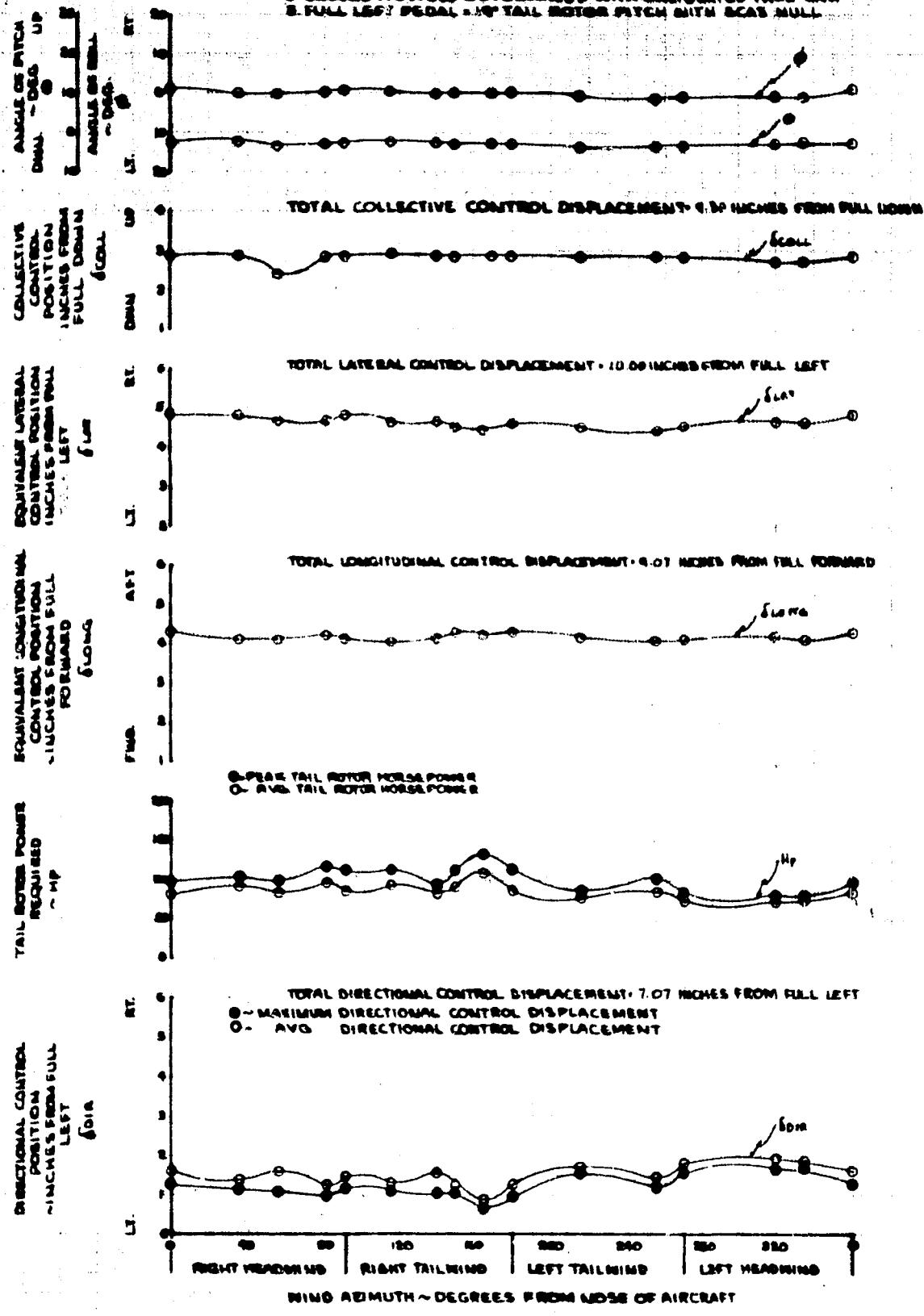


FIGURE NO. 109
STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WIND AZIMUTH
 AM-1G USA #615261
 NVV SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

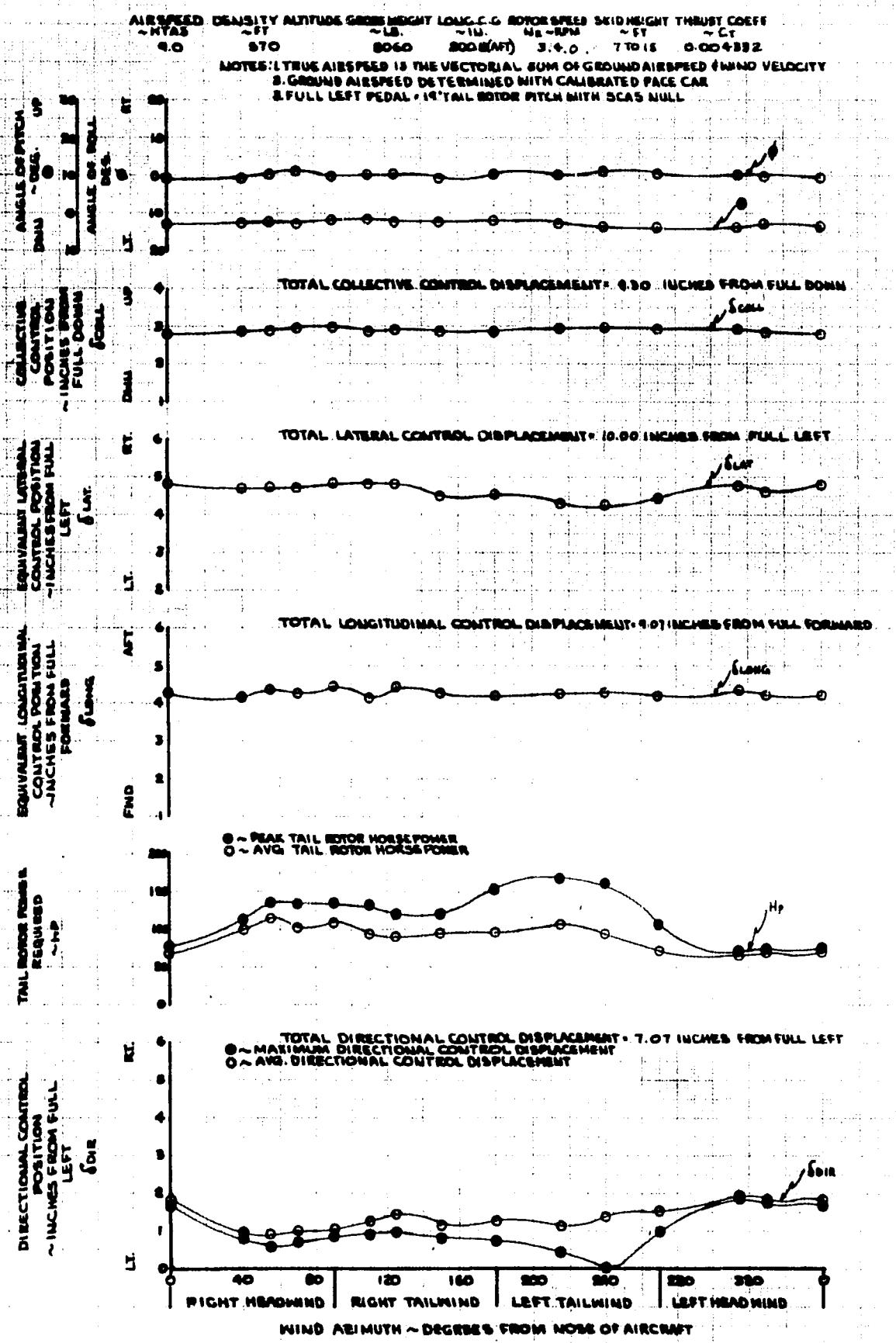


FIGURE NO. 110
STATIC TRIM STABILITY IN GROUND EFFECT WITH VARIOUS WIND AZIMUTH

AH-1G USA 5C15267
HVE SCOUT CONFIGURATION WITH BOOMET POD FINS/BNS REMOVED

AIR SPEED, DENSITY ALTITUDE, GROSS WEIGHT, MAX C.G. ROTOR SPEED, SOIL HEIGHT, THRUST COEFF.
~75AS ~FT. ~LB. ~IN. ~RPM. ~FT. ~C
130. 8TO 6000 2000(HP) 314.0 177015 0.000521

NOTES: 1. THIS AIR SPEED IS THE VECTORIAL SUM OF GROUND AIR SPEED AND VELOCITY
2. GROUND AIR SPEED DETERMINED WITH CALIBRATED PACE CAR
3. FULL LEFT PEDAL + 10° TAIL ROTOR PITCH WITH SCAB NULL

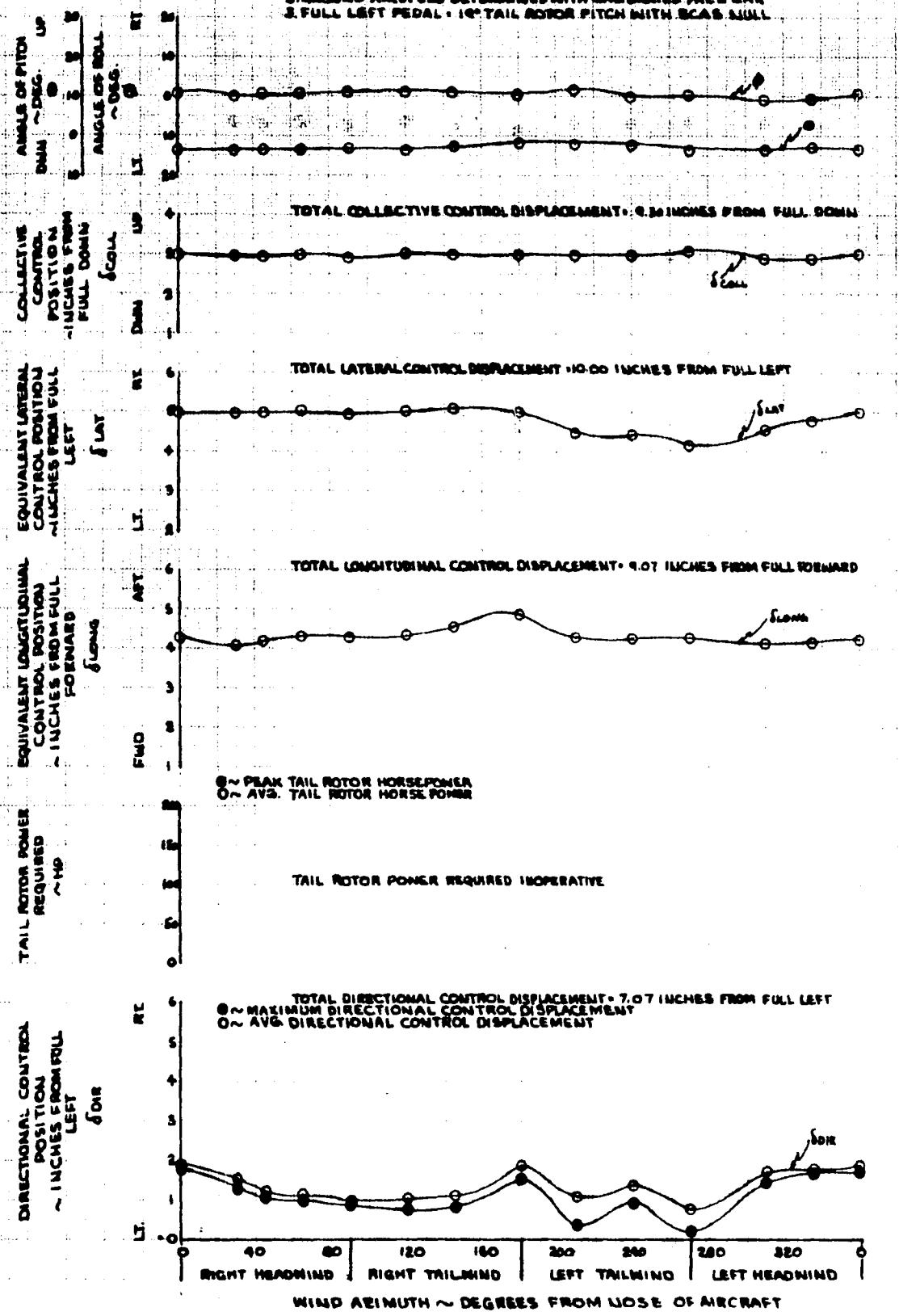


FIGURE No. III
STATIC TRIM STABILITY IN GROUND EFFECT WITH VARIOUS WIND AZIMUTH
 AH-1G USA #615267
 HVY. SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

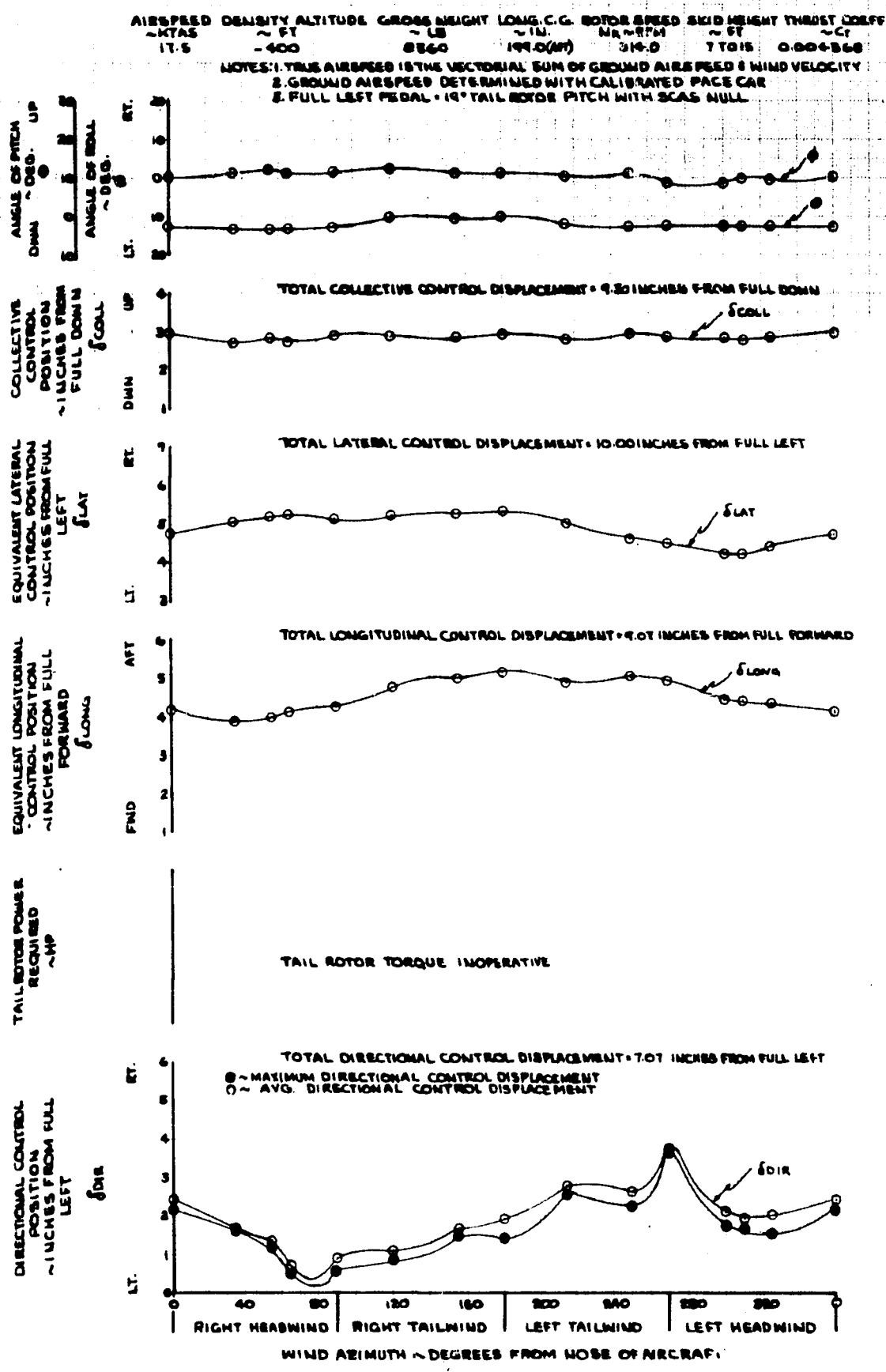


FIGURE NO. 112
 STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WIND ANGLE
 AH-1G USAF 615207

AH-1G SCOUT CLASSIFICATION WITH TAIL ROTOR FAIRING REMOVED

AIRFIELD: DENSITY ALTITUDE, 5100 FT. GROSS WEIGHT, 10,000 LB. GROSS THRUST, 20,000 LB.
 - 5100 FT. - 10,000 LB. - 20,000 LB.

NOTES: 1. THIS AIRCRAFT IS IN THE VECTATIONAL FORM OF GROUND EFFECT FLIGHT VELOCITY
 2. GROUND AIR SPEED DETERMINED WITH CALIBRATED DICE CAR
 3. FULL LEFT PEDAL = 10° TAIL ROTOR PITCH WITH SCAS NULL

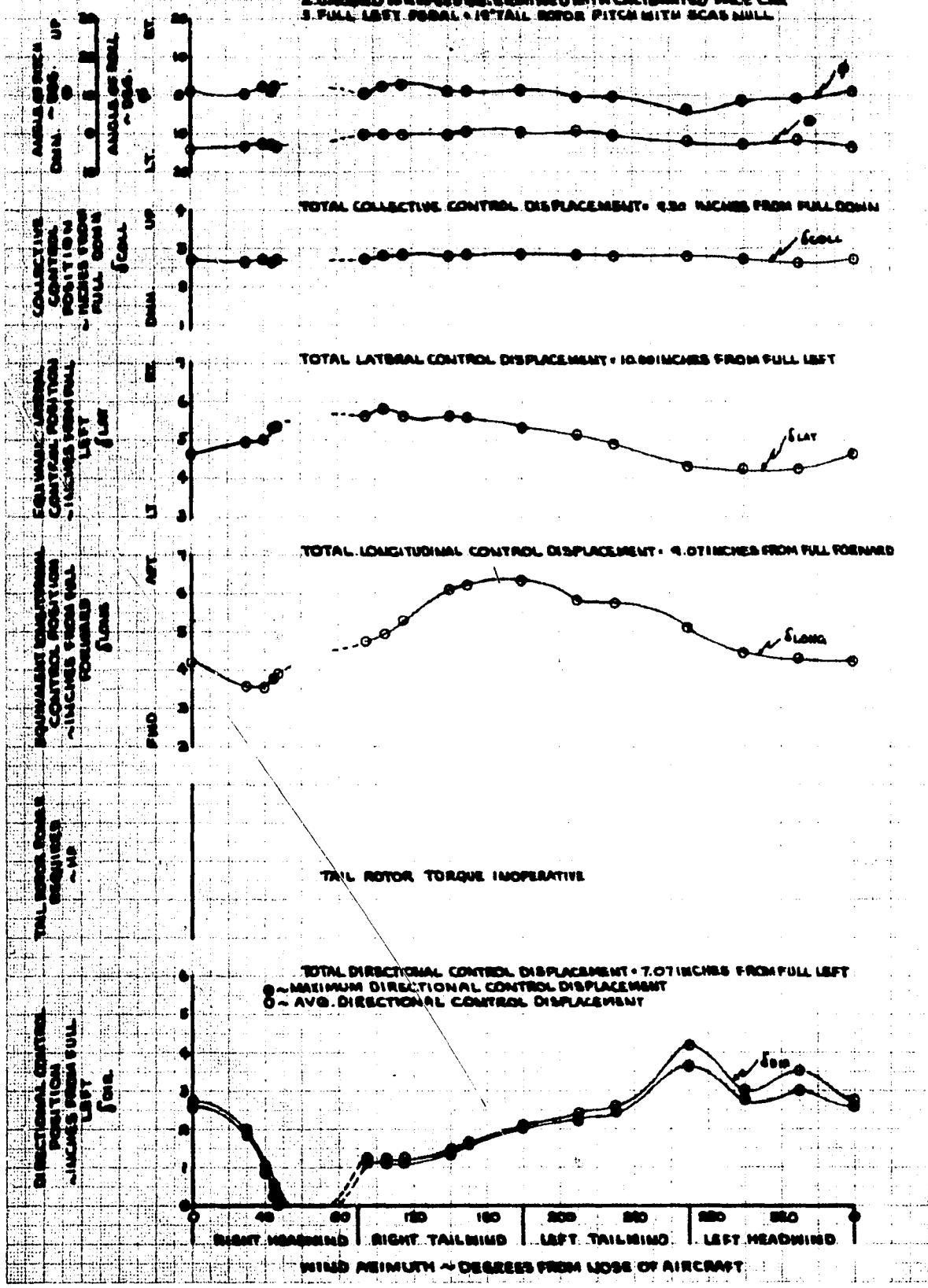


FIGURE NO. 113
STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WIND AZIMUTH

AH-1G USA #615247

HVV. SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

AIR SPEED DENSITY ALTITUDE GROSS WEIGHT LOW WING C.G. AIR SPEED, GROSS WEIGHT, THRUST C.G.S.

~FT. ~LB. ~IN. ~RPM. ~FY. ~C.G.
26.0 -400 8340 198.7(AFP) 314.0 11 TO 15 0004338

NOTES: 1. TRUE AIRSPEED IS THE VECTORIAL SUM OF GROUND AIRSPEED & WIND VELOCITY
2. GROUND AIRSPEED DETERMINED WITH CALIBRATED PACE CAR
3. FULL LEFT PEDAL + 19° TAIL MOTOR PITCH WITH SCAS NULL

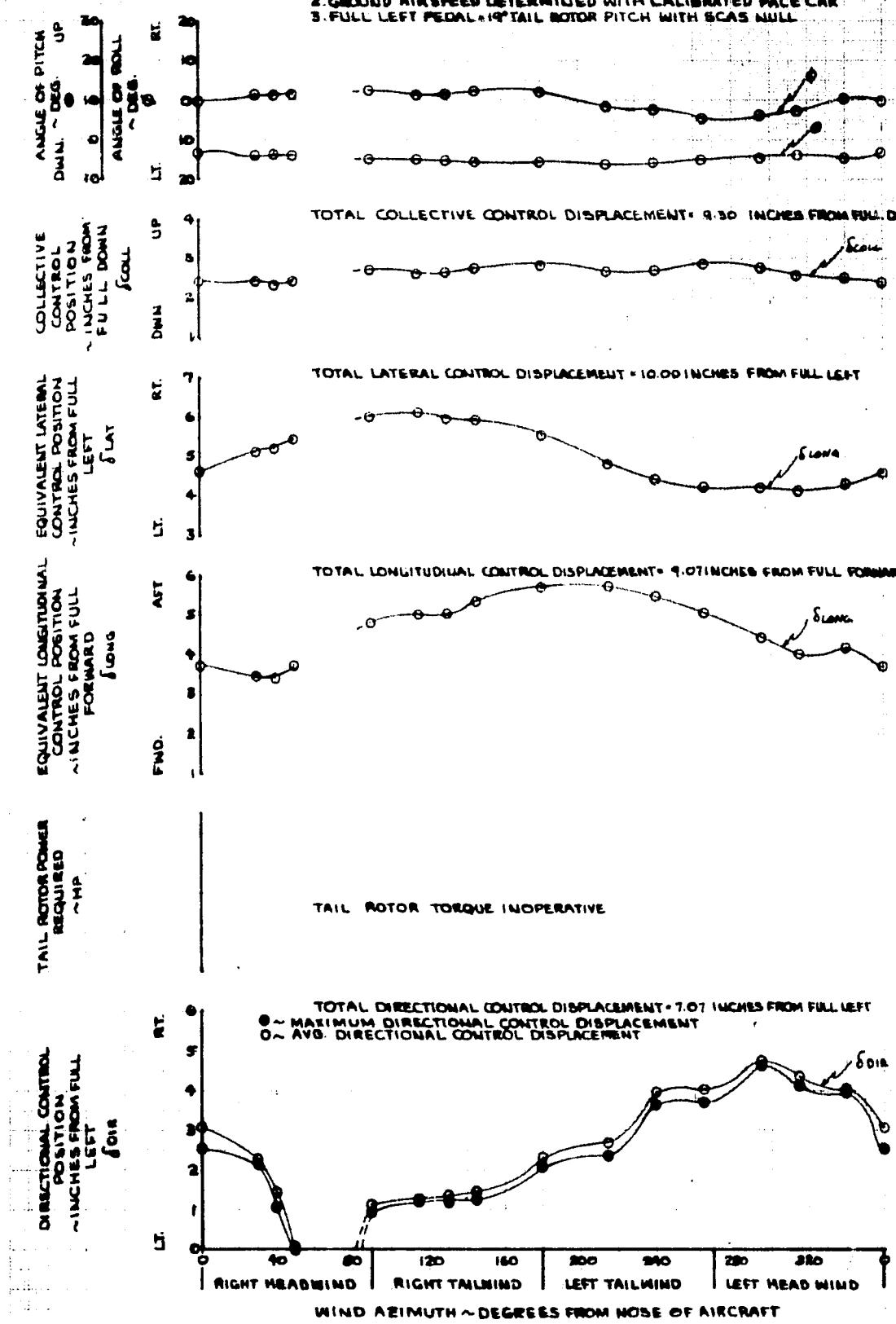


FIGURE NO 114
STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WIND AZIMUTH

AH-1G USA XG15267

MVY. SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

AIRSPD. DENSITY ALTITUDE GROSS WEIGHT LONG. E.G. ROCK SPEED SKIDMIGHT THRUST COEFF.
~KIAS ~FT ~LB. ~IN. ~RPM ~FT ~CT
20.5 - 400 8290 198.7(Avg) 314.0 7 TO 15 0.004831

NOTES: 1. TRUE AIRSPD IS THE VECTORIAL SUM OF GROUND AIRSPD + WIND VELOCITY
2. GROUND AIRSPD DETERMINED WITH CALIBRATED PACE CAR
3. FULL LEFT PEDAL = 19° TAIL ROTOR PITCH WITH ECAB NULL

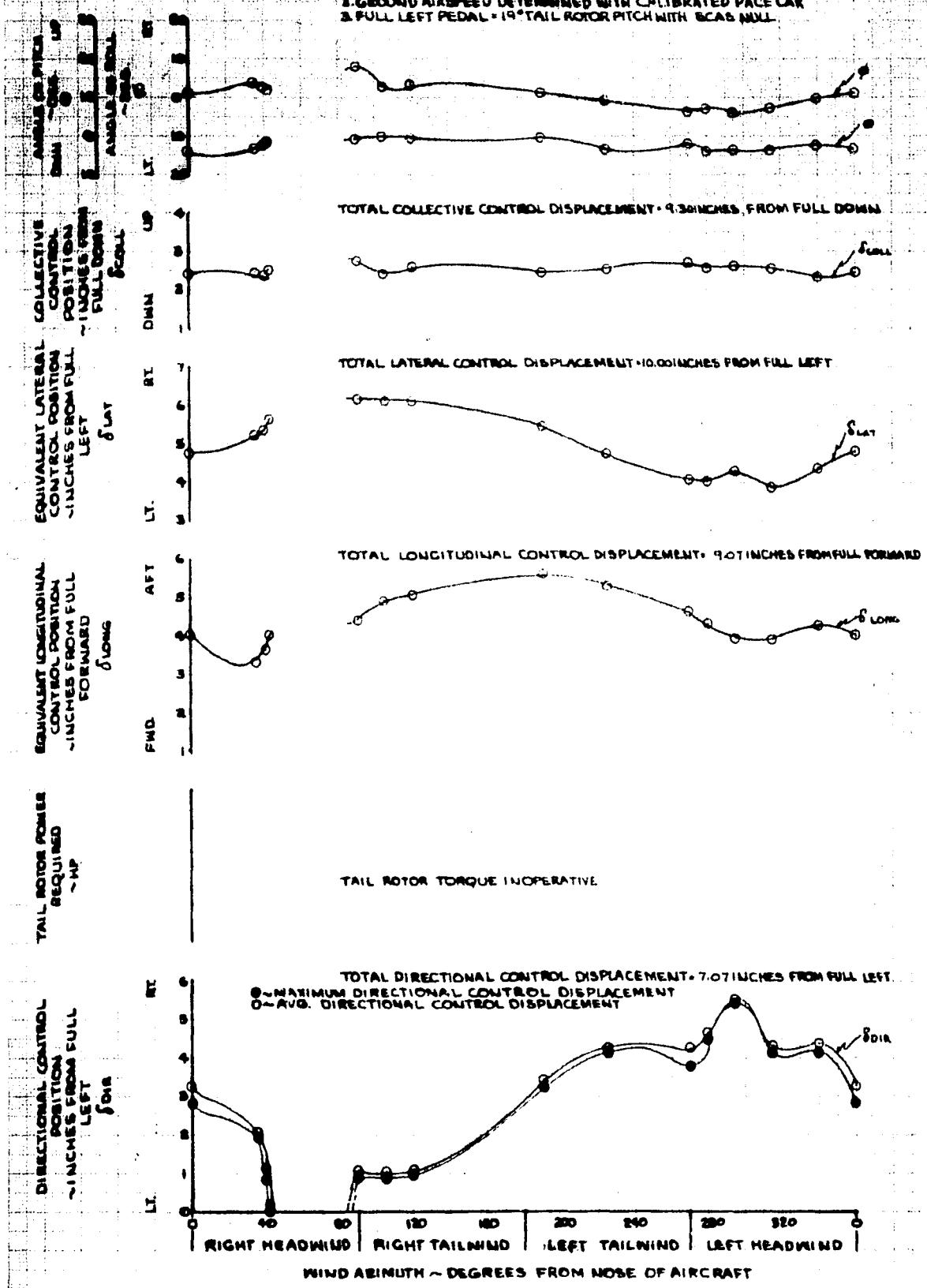
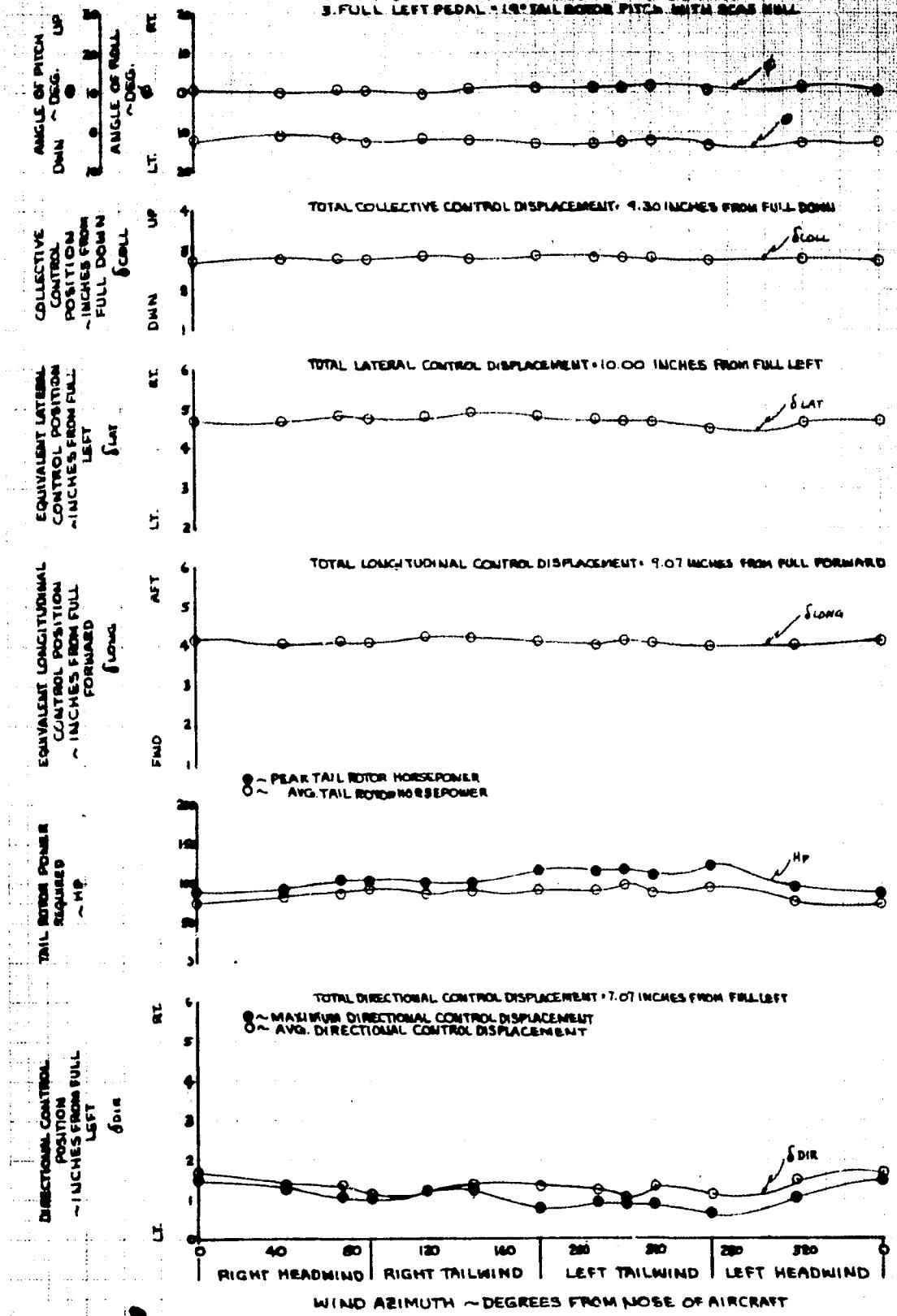


FIGURE NO 115
STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WINDAZIMUTHS
AH-1G USA REGIS 267
HVY. SCOUT CONFIGURATION WITH ROCKET POD PARACHUTE DEPLOYED

AIRSPEED: DENSITY ALTITUDE: GROSS WEIGHT: LOAD C.G.: ROLLING RATE: SHIR: RPM
 ~1023 ~ FT ~ LB ~ IN. ~ deg/min 4.5 5130 5000 200.0(M) 336.0 7 TO 15 0.0000
 NOTES: 1. TRUE AIRSPEED IS THE VECTORIAL SUM OF GROUND AIRSPEED AND WIND SPEED
 2. GROUND AIRSPEED DETERMINED WITH CALIBRATED PACE CAR
 3. FULL LEFT PEDAL = 100% TAIL MOTOR POWER WITH 2000 RPM



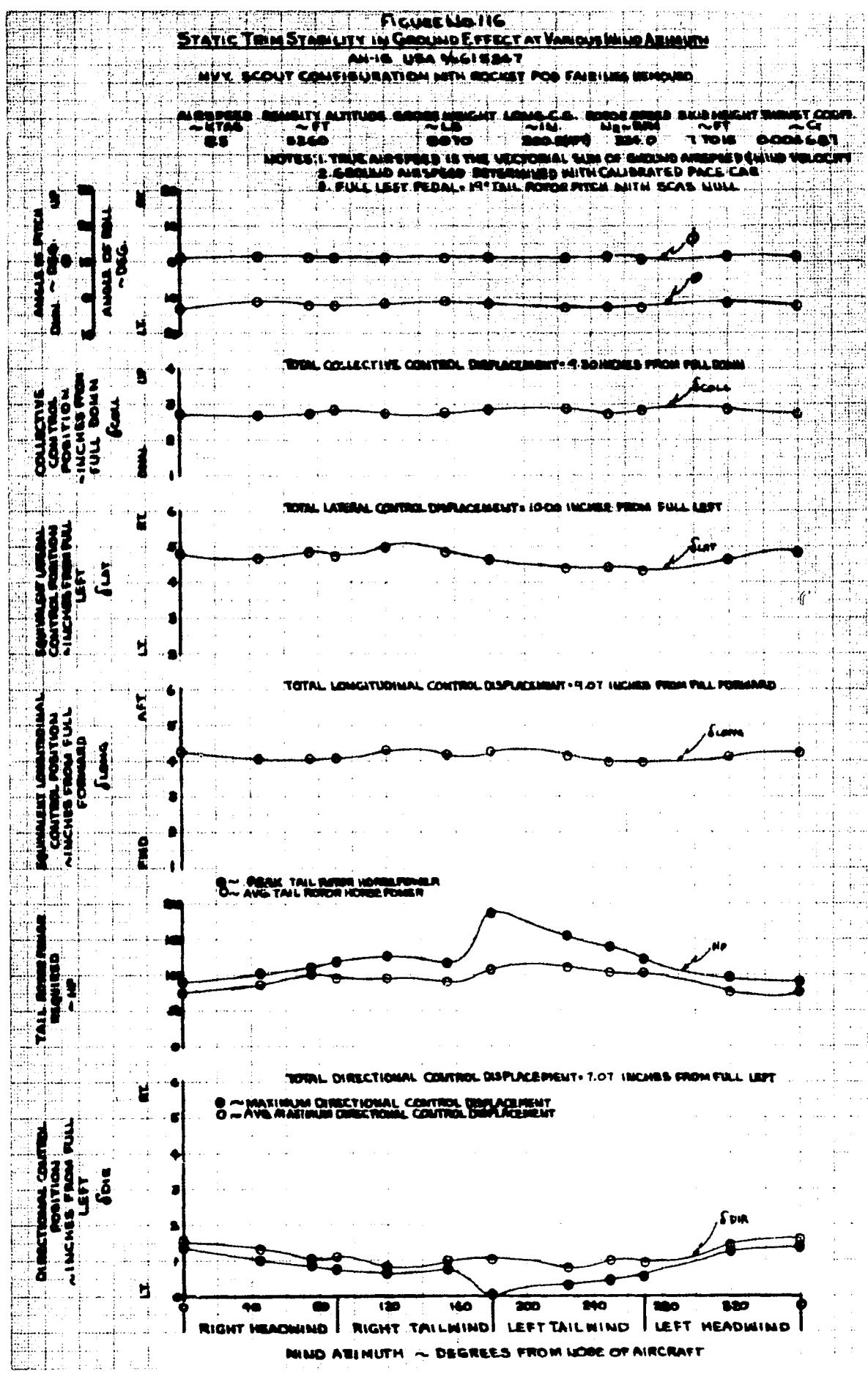


FIGURE NO 117
 STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WIND AZIMUTH
 AH-1G USA #615247
 HVY. SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

AIR SPEED DENSITY ALTITUDE GROSS WEIGHT LOWS C.G. ROTOR SPEED SKID HEIGHT TAIL RPM
 ~ KIAS ~ FT ~ LB ~ RPM ~ FT ~ °
 12.5 5240 8090 200.6(FT) 324.0 7 TO 15 0.045 RT

NOTES: 1. TRUE AIR SPEED IS THE VECTORIAL SUM OF GROUND AIR SPEED AND WIND VELOCITY
 2. GROUND AIR SPEED DETERMINED WITH CALIBRATED PACE CAR.
 3. FULL LEFT PEDAL + 10° TAIL ROTOR PITCH WITH SEAS MULL.

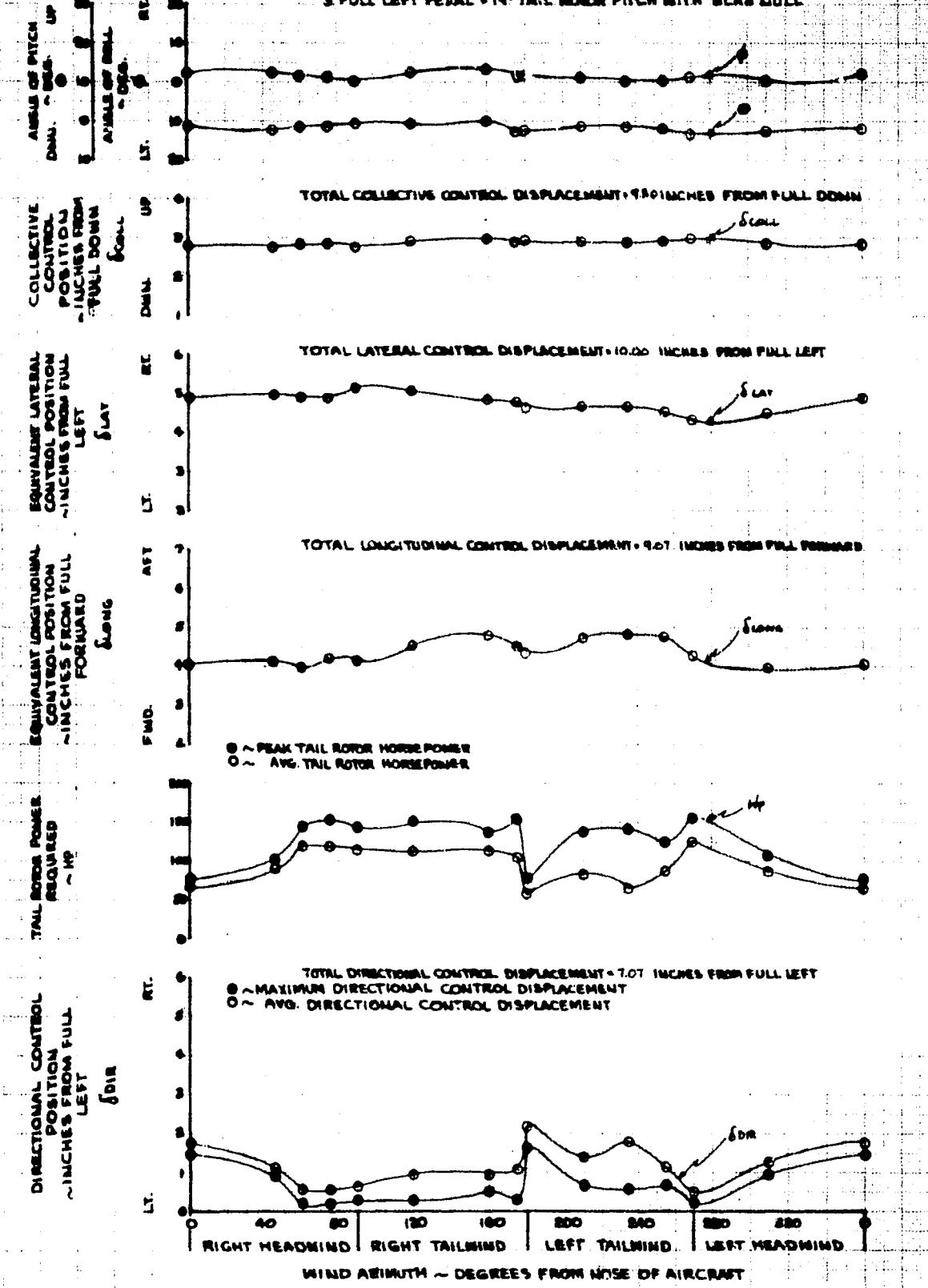


FIGURE NO 110
STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WIND AZIMUTH
AM-H USA 461524T
MV. SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

ALBEDO .65 DENSITY ALTITUDE 6000 FEET GROSS WEIGHT 10,000 LBS C.G. POSITION 50% OF FWD. LENGTH 35' 0" TAIL NUMBER 5210 RPM 1400 RPM ALTITUDE 1000 FT TTO 15 SEC 0.665

NOTES: 1. TRUE AIRSPEED IS THE VECTORIAL SUM OF GROUND AIRSPEED/WIND VELOCITY
 2. GROUND AIRSPEED DETERMINED WITH CALIBRATED PACE CAR
 3. FULL LEFT PEDAL + 10° TAIL ROTOR PITCH WITH SCAB NULL.

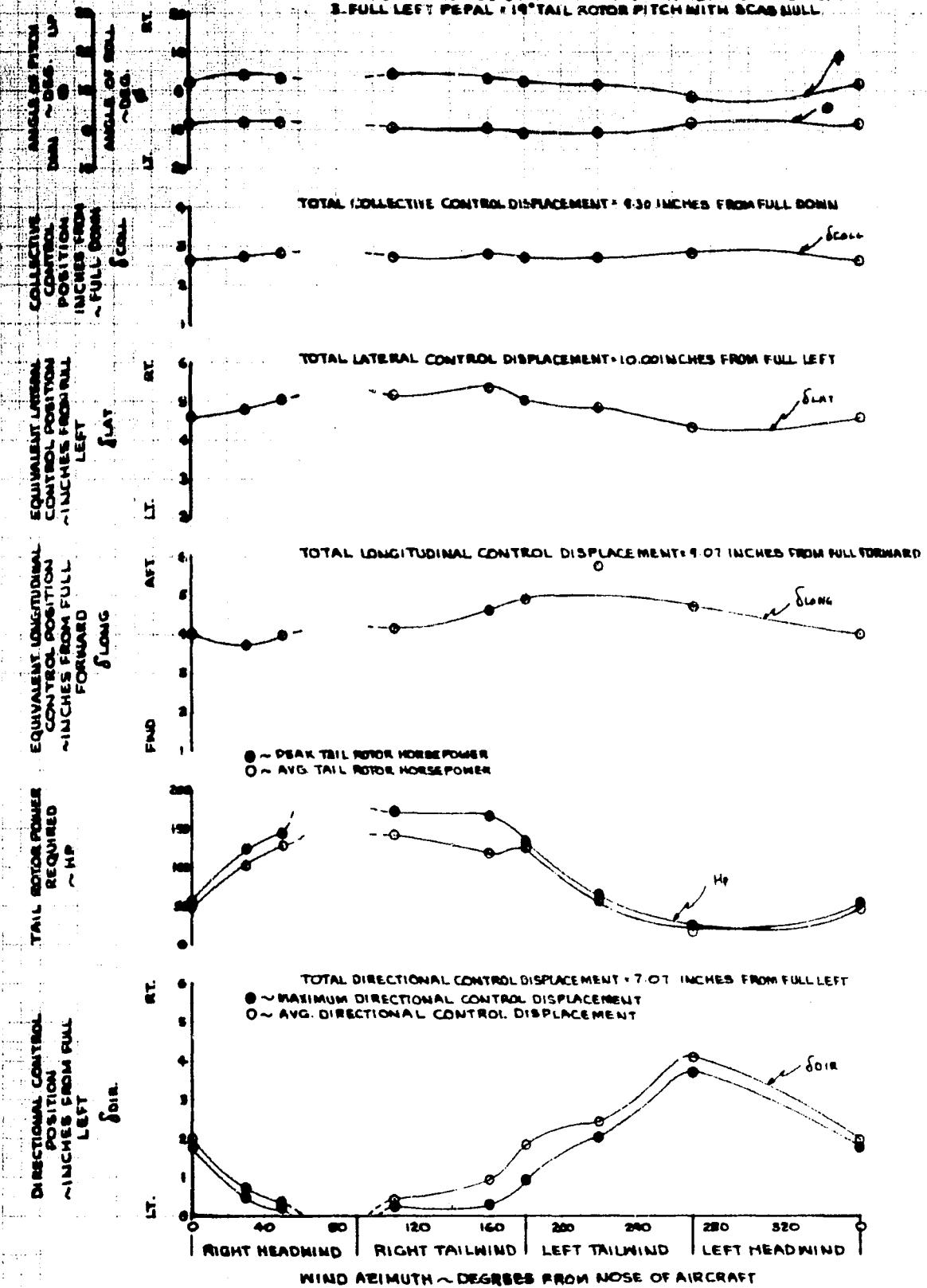
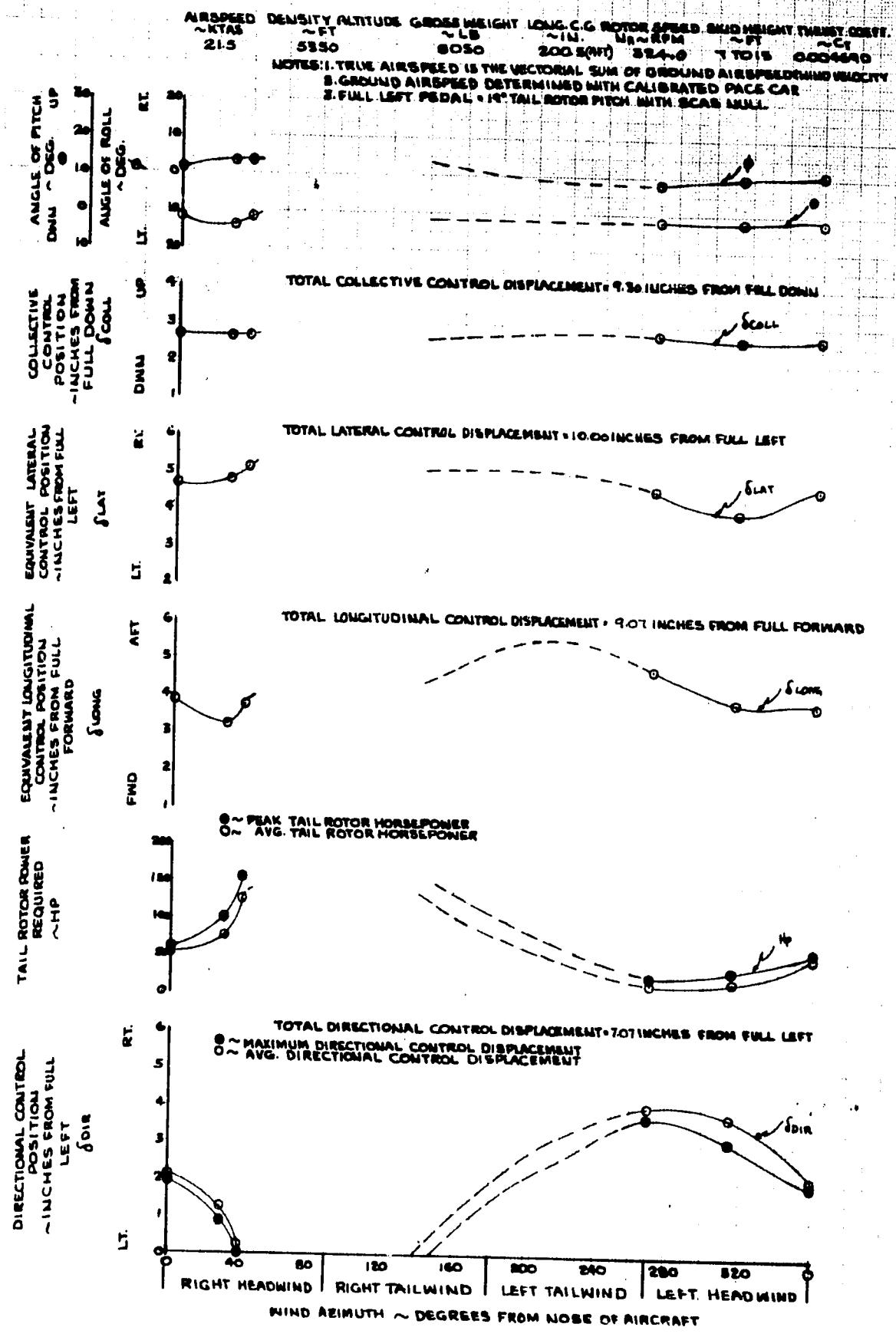


FIGURE NO. 119
 STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WIND AZIMUTH
 AH-1G USA #615247
 HVY. SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED



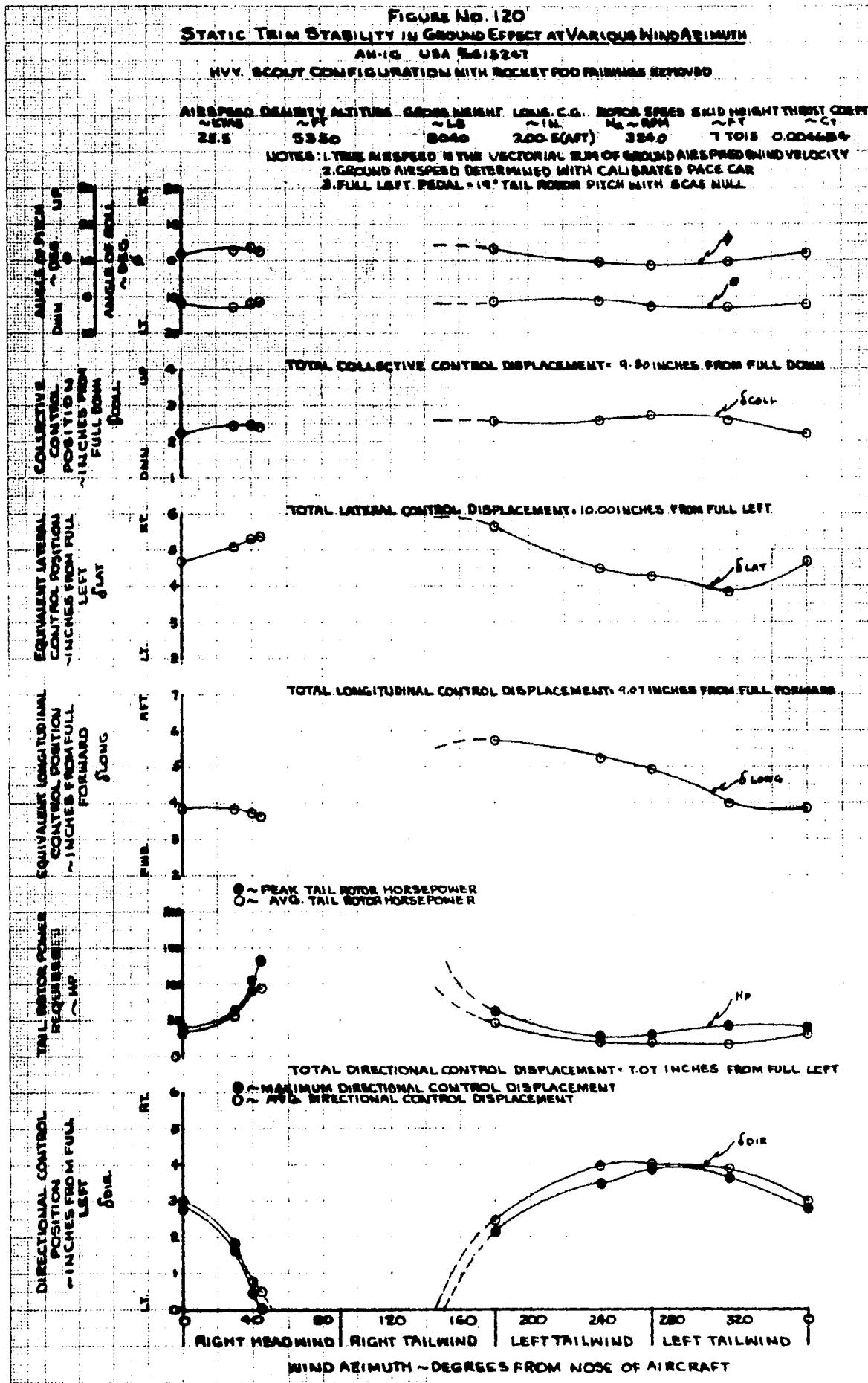


FIGURE NO 121
STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WIND AZIMUTH

AM-15 USA 4615207

MVY SCOUT CONFIGURATION WITH ROCKET PODS TAKEN REMOVED

AIRPROPS DENSITY ALTITUDE GROSS WEIGHT LONG C.G. ROTOR SPEED TAIL HEIGHT TAIL ROTOR RPM.
~LXTAS ~FT ~LB ~RPM ~FT ~C
24.5 6820 1000 200 (MAX) 324.0 7 TO 15 ROLLING

NOTES: 1. TOTAL WIND IS THE VECTOR SUM OF THE GROUND WIND AND THE WIND VELOCITY.

2. GROUND WIND WAS DETERMINED WITH CALIBRATED PROBE CAR.

3. FULL LEFT PEDAL 110° TAIL ROTOR PITCH WITH SCAB NULL.

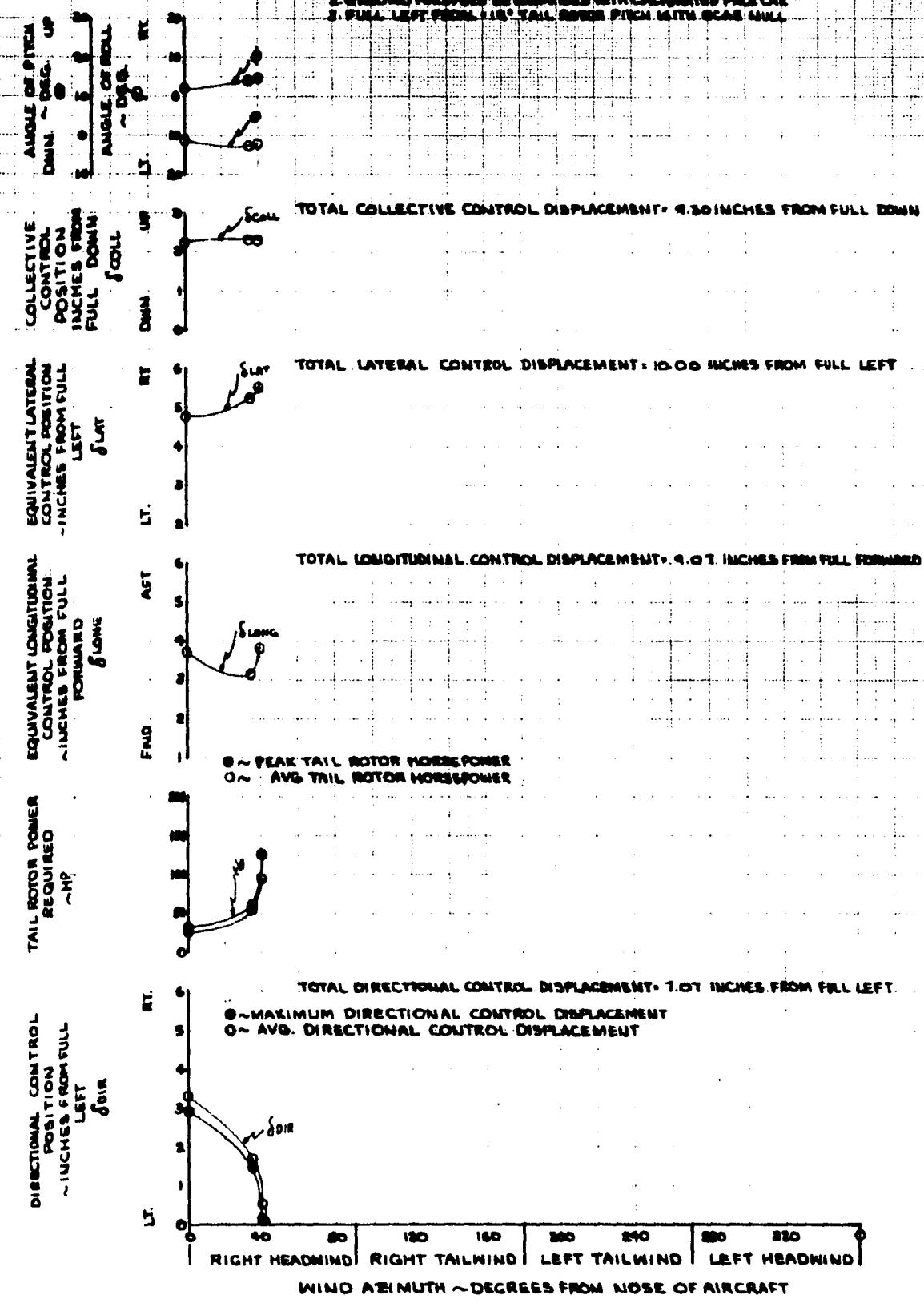


FIGURE NO. 122
STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WIND AZIMUTH
AMIC USA KC13247
HUV SCOUT CONFIGURATION WITH HOCKEY POOL FAIRINGS REMOVED

AIR SPEED DENSITY ALTITUDE GROSS WEIGHT LONG C.G. MOTOR SPEED SKID WEIGHT THRUST COEFF.
~KTAS ~FT ~LB ~IN. ~HP ~LBS ~FT. ~CT
4.5 10950 7550 149.6 (HPD) 324.0 TTO 15 0.005094

NOTES: 1. TRUE AIRSPEED IS THE VECTORIAL SUM OF GROUND AIRSPEED/WIND VELOCITY
2. GROUND AIRSPEED DETERMINED WITH CALIBRATED PACE CAR
3. FULL LEFT PEDAL + 19° TAIL ROTOR PITCH WITH SCAB NULL

PITCH & ROLL ATTITUDE INOPERATIVE

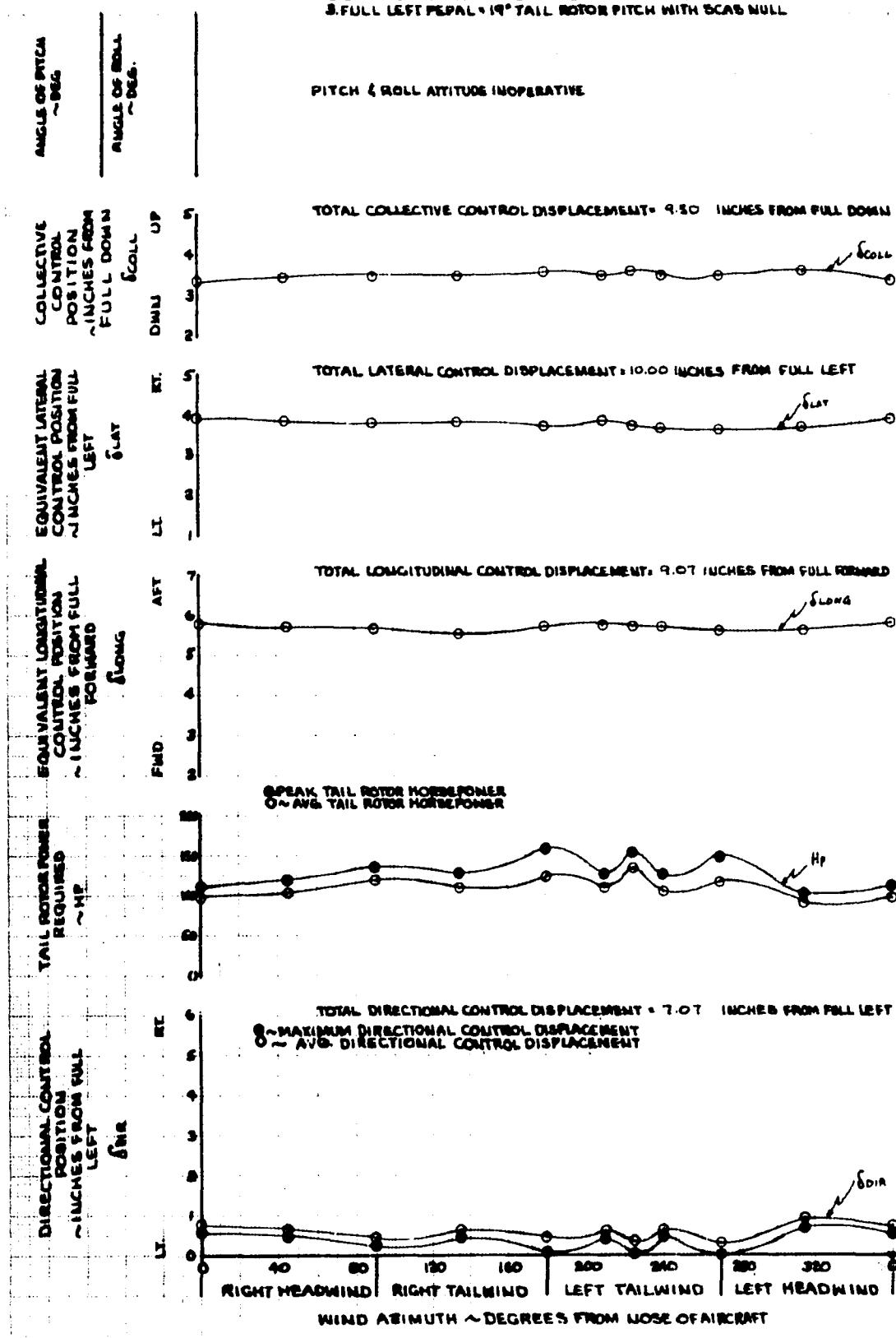


FIGURE NO. 123
 STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WIND AZIMUTH
 AH-1G USA #615247
 HVY SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

AIRSPEED DENSITY ALTITUDE GROSS WEIGHT LONG C.C. ROTOR SPEED SKID HEIGHT THRUST COEFF.
 ~ KTAS ~ FT. ~ LB ~ IN. ~ RPM ~ FT ~ C_T
 0.5 11090 7210 145.4(alt) 324.0 7.015 0.005018

NOTES: 1. TRUE AIRSPEED IS THE VECTORIAL SUM OF GROUND AIRSPEED & WIND VELOCITY
 2. GROUND AIRSPEED DETERMINED WITH CALIBRATED PACE CAR
 3. FULL LEFT PEDAL - 19° TAIL ROTOR PITCH WITH SEAT NULL

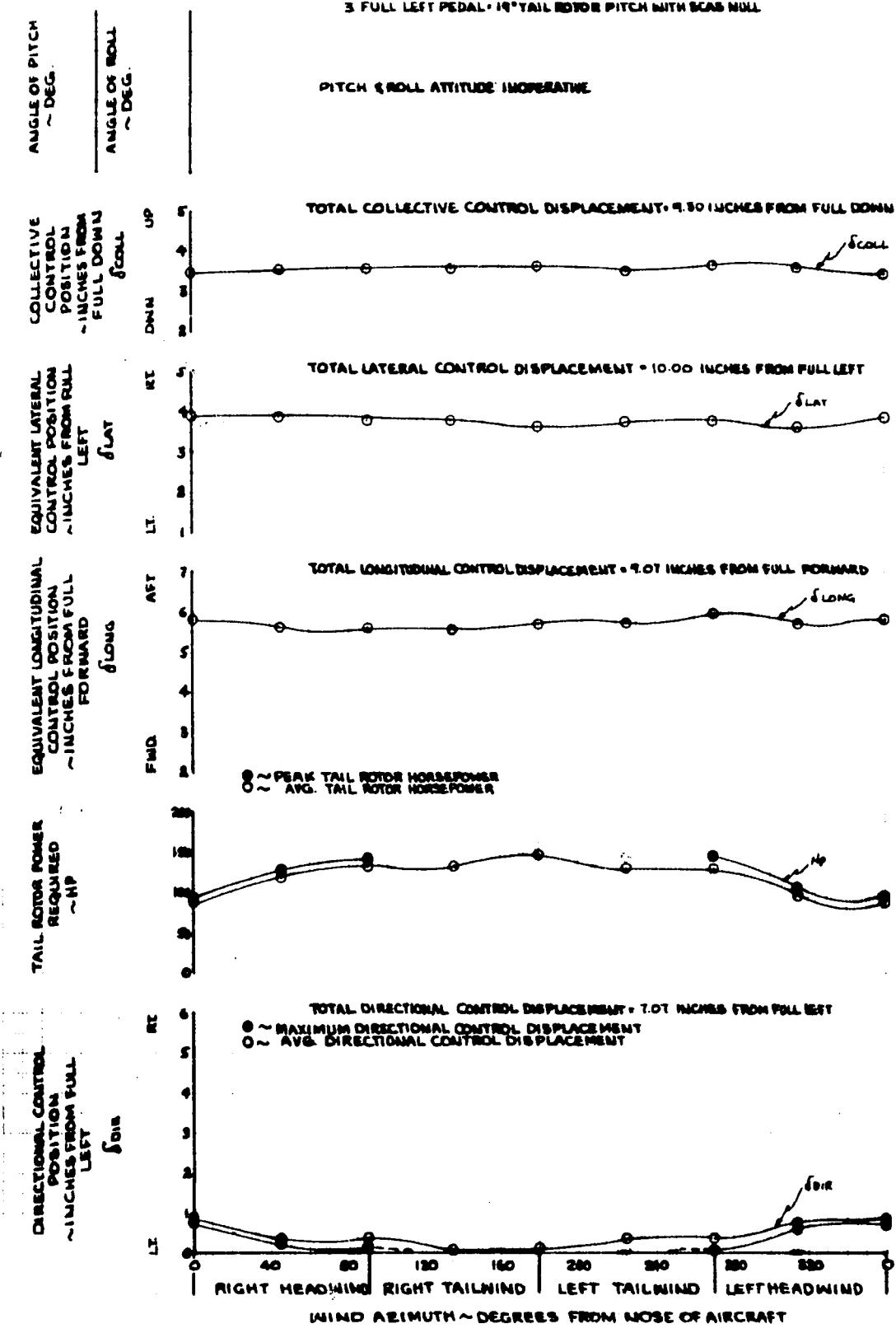


FIGURE No. 124
STATIC TRIM STABILITY IN GROUND EFFECT AT VARIOUS WIND AZIMUTH
 AH-1C USA #615247
 HVY. SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

AIR SPEED DENSITY ALTITUDE GROSS WEIGHT LONG. C.G. ROTOR SPEED SKID HEIGHT THRUST COEF.
 ~ KIAS ~ FT. ~ LB ~ IN. N~ RPM ~ FT. ~ CT
 12.5 11320 TOTO 1953(MID) 324.0 7 TO 15 0.006965

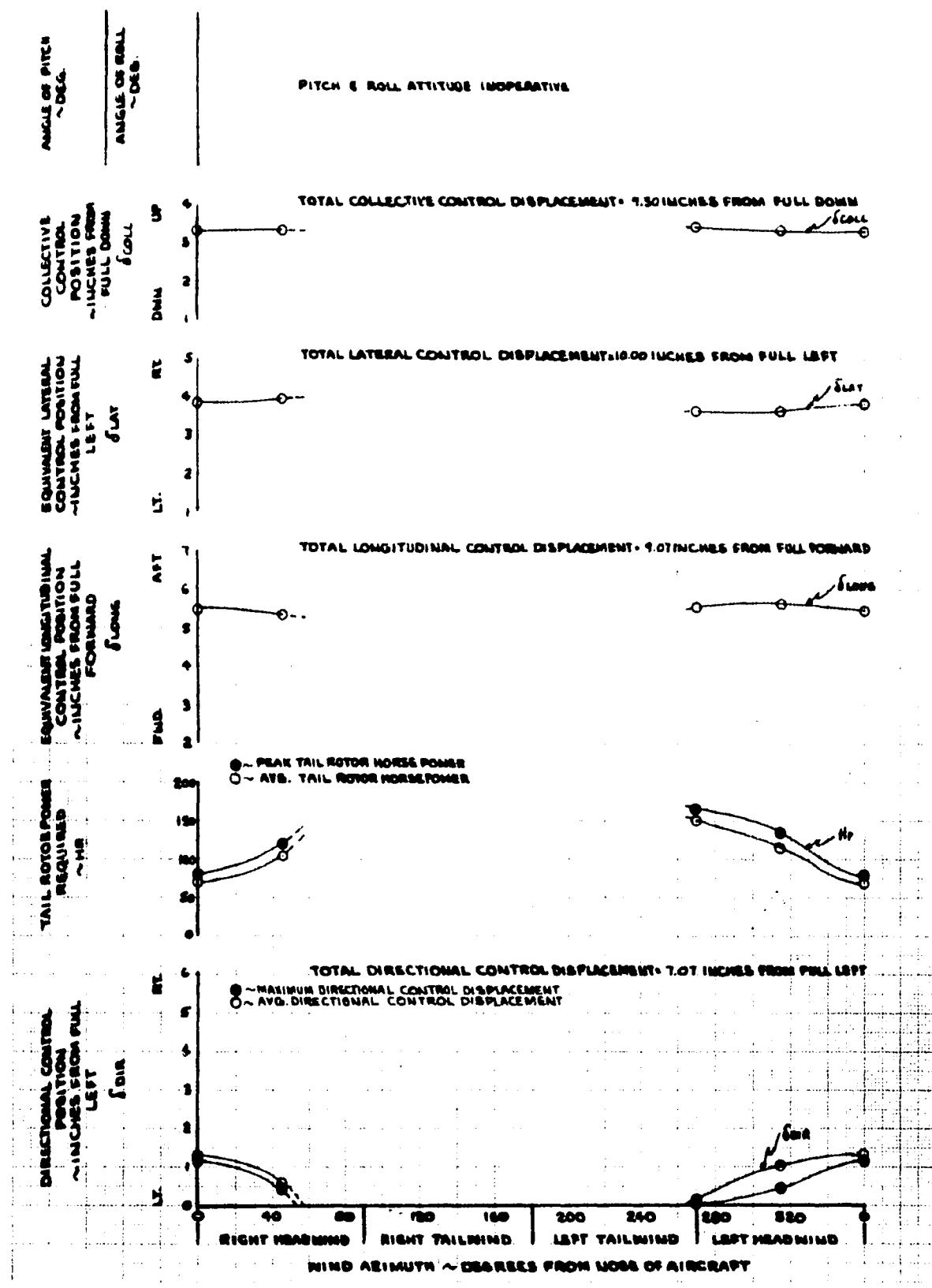


FIGURE NO 125
SIDEWARD & REARWARD FLIGHT

AH-1G USA MAG 15 ZET

MVY. SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED
LANDING GEAR CROSS TUBE FAIRINGS REMOVED

DENSITY ALTITUDE GROSS WEIGHT LONG C.G. ROTOR SPEED SKID HEIGHT TORQUE GRIPS
H₀ ~ FEET ~ LBS ~ IN. NR ~ RPM ~ FT. ~ CT
8030 8000 201.1(AFT) 829.0 77015 .004568

NOTES: 1. TRUE AIRSPEED IS THE VECTORIAL SUM OF GROUND AIRSPEED & WIND VELOCITY
2. GROUND AIRSPEED DETERMINED WITH CALIBRATED PACE CAR
3. FULL LEFT PEDAL = 19° TAIL ROTOR, PITCH SCAB NULL

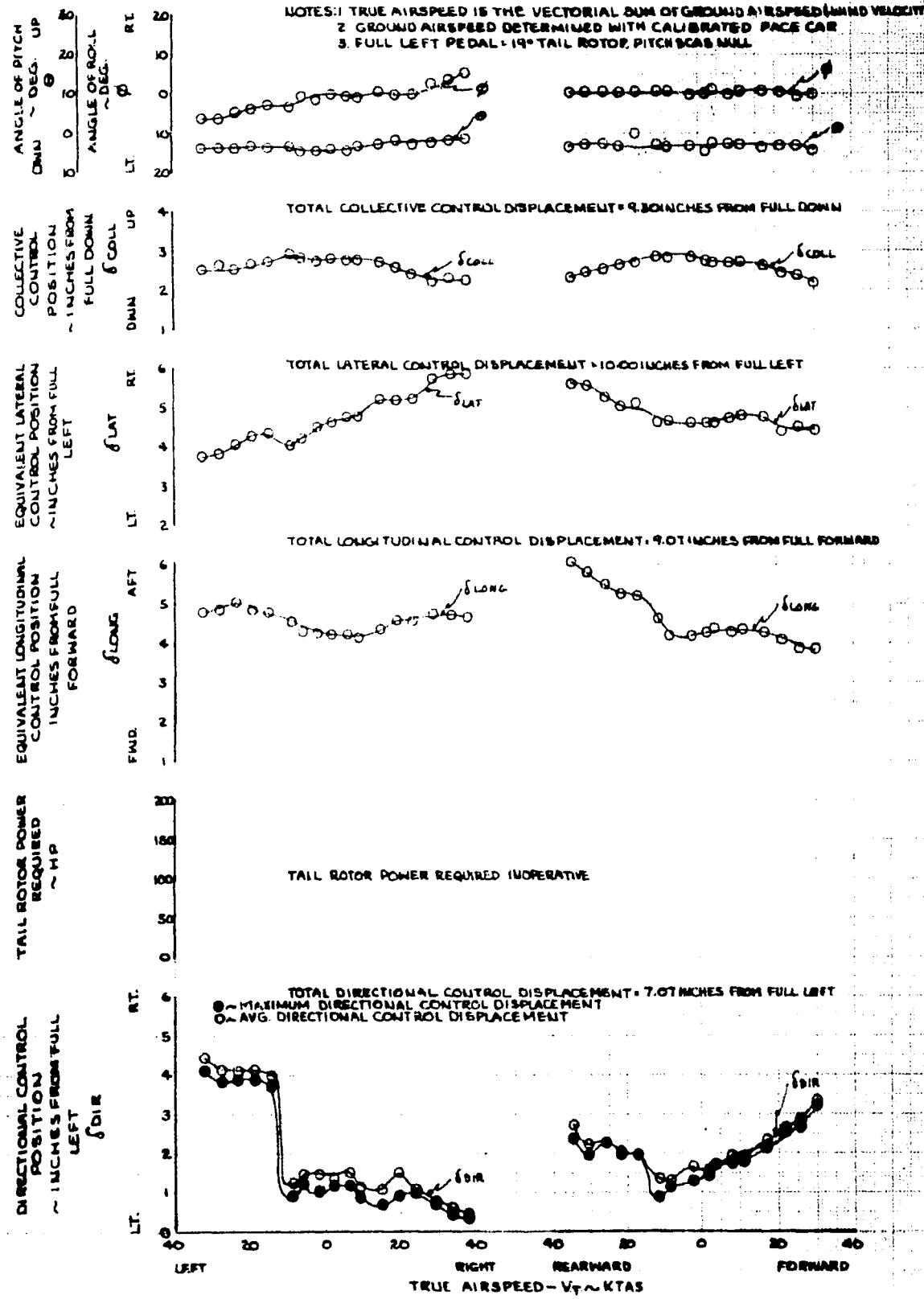


FIGURE NO. 126
 LONGITUDINAL DYNAMIC STABILITY SUMMARY
 AH-1G USA S/N 715695

CONFIG	AVG G.W. ~LB	AVG ALT H.D~FT	AVG LONG C.G. ~IN	SCAS	V _{MIN POWER} (LEVEL FLT)			.8 V _H (LEVEL FLT)			V _H (LEVEL FLT)			
					w c	DESCRIP	AIRSPD ~ CAS	w c	DESCRIP	AIRSPD ~ CAS	w c	DESCRIP	AIRSPD ~ CAS	
CLEAN	7660	5000	190.5 (FWD)	ON	NA	NA	DEAD BEAT	63	NA	DEAD BEAT	106	NA	DEAD BEAT	137
					OFF	NA	DEAD BEAT		NA	DEAD BEAT		NA	DEAD BEAT	
CLEAN	7540	4000	201 (AFT)	ON	.26 1.7	HEAVILY DAMPED	65	NA	DEAD BEAT	108	NA	DEAD BEAT	142	
					OFF	.05 .9	HEAVILY DAMPED	.09 .3	LIGHTLY DAMPED	.16 .4	HEAVILY DAMPLD			
HEAVY HOG	7740	4300	201 (AFT)	ON	NA	NA	DEAD BEAT	62	NA	DEAD BEAT	105	.28 1.45	HEAVILY DAMPED	150
					OFF	.08 .1	UNDAMPED		.02 .3	UNDAMPED		.08 .9	HEAVILY DAMPED	
HEAVY HOG	9340	4400	200 (AFT)	ON	NA	NA	DEAD BEAT	65	NA	DEAD BEAT	104	NA	DEAD BEAT	132
					OFF	NF	NF		NF	NF		.06 .4	LIGHTLY DAMPLD	
HEAVY HOG	7730	15000	201 (AFT)	ON	.06 1.2	HEAVILY DAMPED	56	NA	DEAD BEAT	86	NA	DEAD BEAT	105	
					OFF	NF	NF	NF	NF	NA	UNDAMPED			
HEAVY SCOUT	9310	4500	200 (AFT)	ON	NF	NF	NF	NA	DEAD BEAT	104	NA	DEAD BEAT	140	

CONFIG	AVG G.W. ~LB	AVG ALT H.D~FT	AVG LONG C.G. ~IN	SCAS	V _{LIMIT} (DIVE)			V _{MAX} (R/L)			V _{MIN} (R/D)			
					w c	DESCRIP	AIRSPD ~ CAS	w c	DESCRIP	AIRSPD ~ CAS	w c	DESCRIP	AIRSPD ~ CAS	
CLEAN	7660	5000	190 (FWD)	ON	NA	NA	DEAD BEAT	150	NA	DEAD BEAT	60	NA	DEAD BEAT	72
					OFF	NA	DEAD BEAT		NA	DEAD BEAT		NA	DEAD BEAT	
CLEAN	7540	4000	201 (AFT)	ON	.49 1.8	HEAVILY DAMPED	180	NA	DEAD BEAT	65	NA	DEAD BEAT	70	
					OFF	.10 .6	HEAVILY DAMPED	.09 .5	LIGHTLY DAMPED	.10 .6	HEAVILY DAMPLD			
HEAVY HOG	7740	4300	201 (AFT)	ON	NA	NA	DEAD BEAT	170	NA	DEAD BEAT	68	NA	DEAD BEAT	69
					OFF	.15 .1	LIGHTLY DAMPED		.09 .5	LIGHTLY DAMPED		NA	DEAD BEAT	
HEAVY HOG	9340	4400	200 (AFT)	ON	NF	NF	NF	NF	NA	DEAD BEAT	62	NF	NF	NI
					OFF	NF	NF		.15 .5	LIGHTLY DAMPED		NF	NF	
HEAVY SCOUT	9310	4500	200 (AFT)	ON	NA	NA	DEAD BEAT	170	NA	DEAD BEAT	60	NF	NF	NF

NOTE: ALL APPLICABLE NOTES ARE PRESENTED ON FIGURE 150.

FIGURE NO. 127
AFT LONGITUDINAL PULSE SCAS ON

AH-1G USA #6715695
CLEAN CONFIGURATION

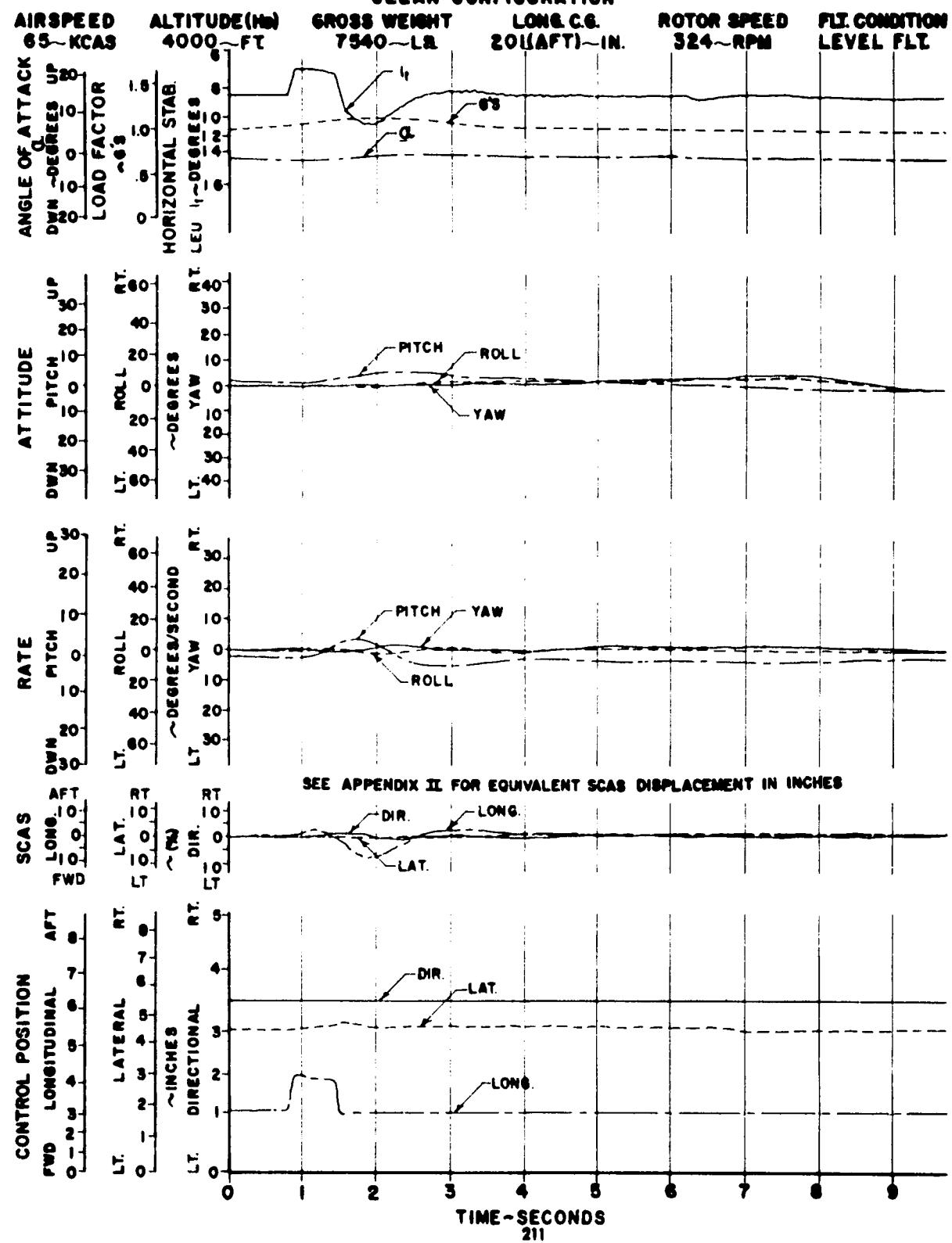


FIGURE NO. 128
AFT LONGITUDINAL PULSE SCAS ON

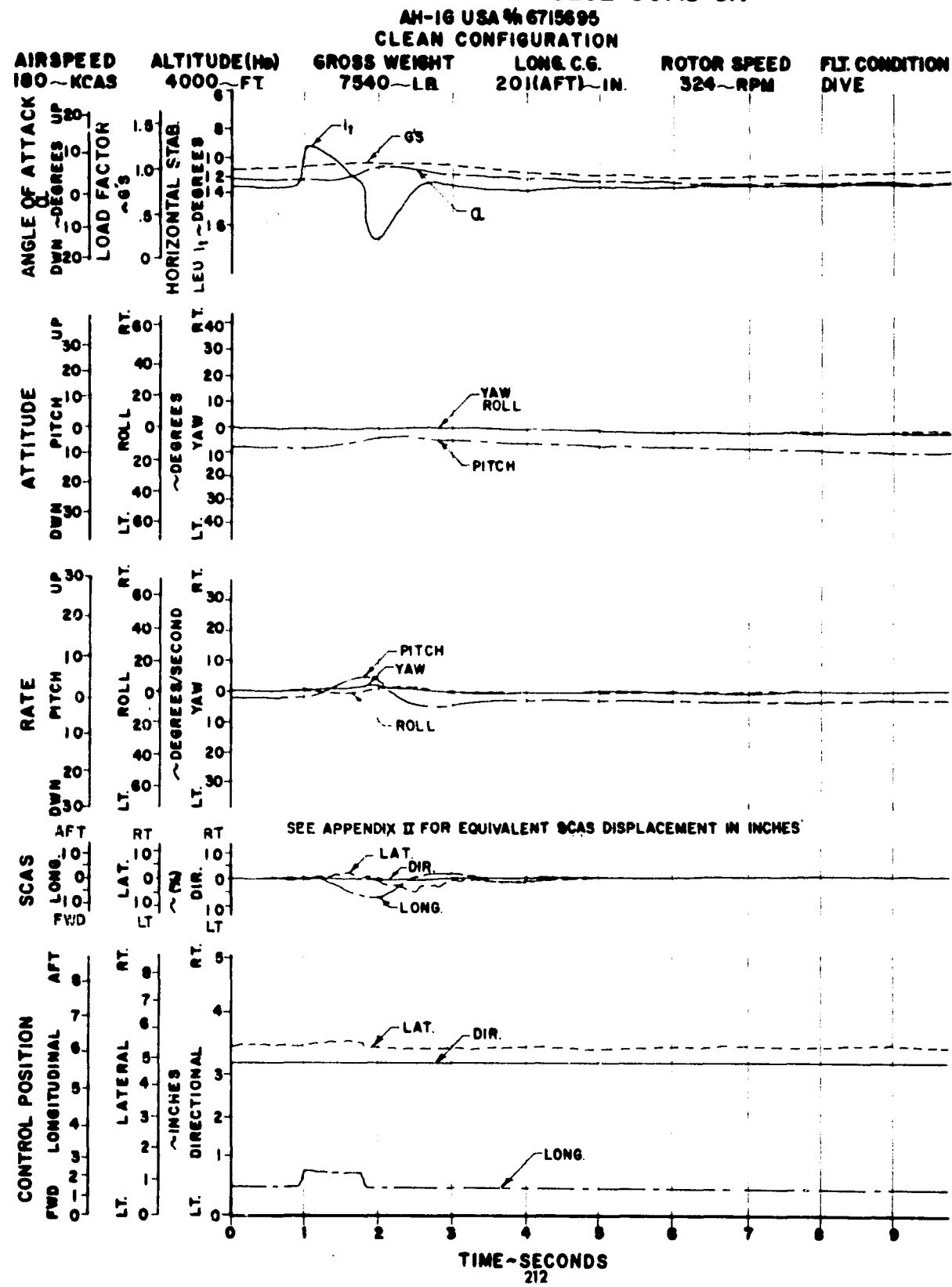


FIGURE NO. 129
AFT LONGITUDINAL PULSE SCAS ON

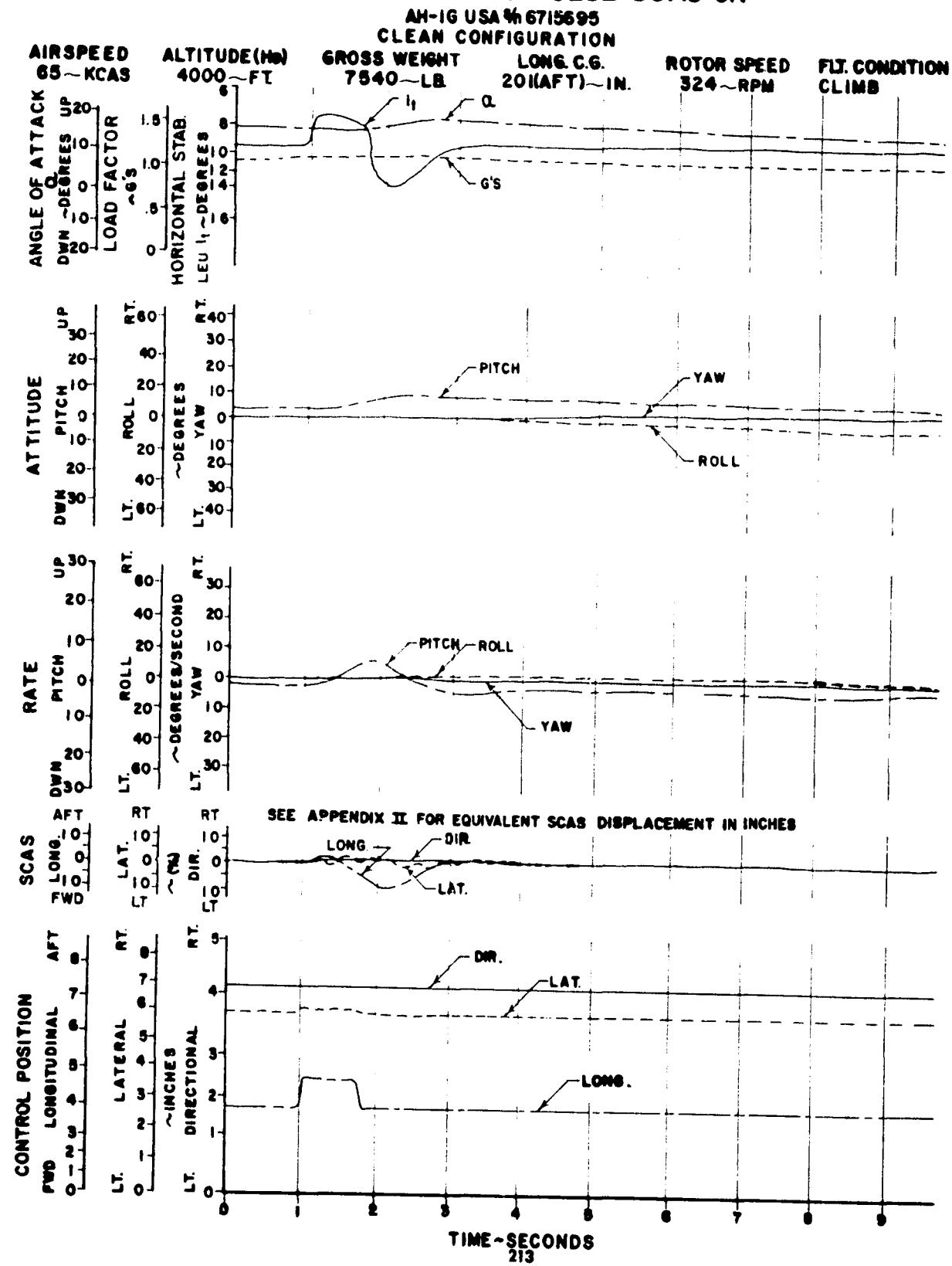


FIGURE NO. 130
AFT LONGITUDINAL PULSE SCAS ON

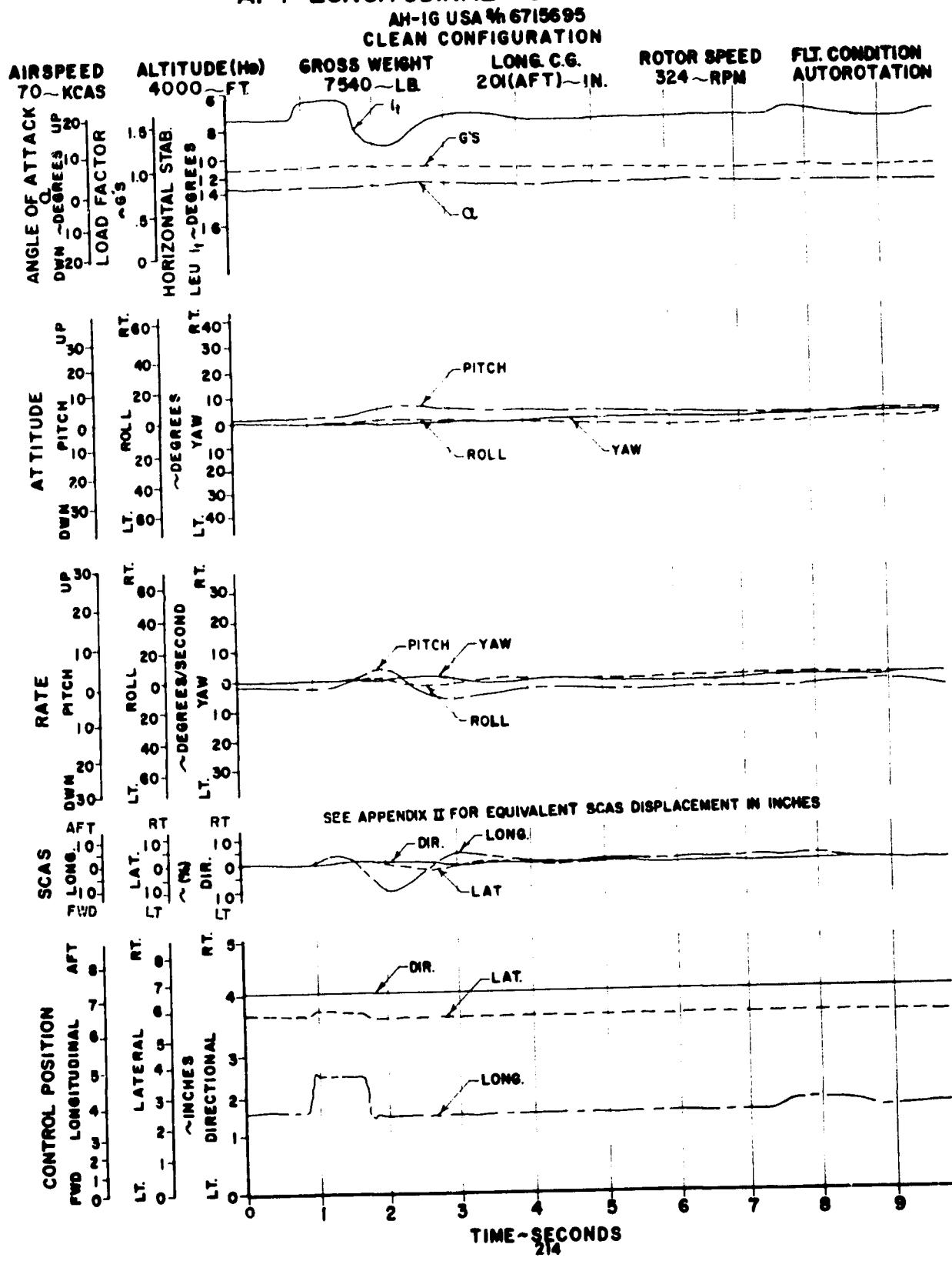


FIGURE NO.131
AFT LONGITUDINAL PULSE SCAS ON

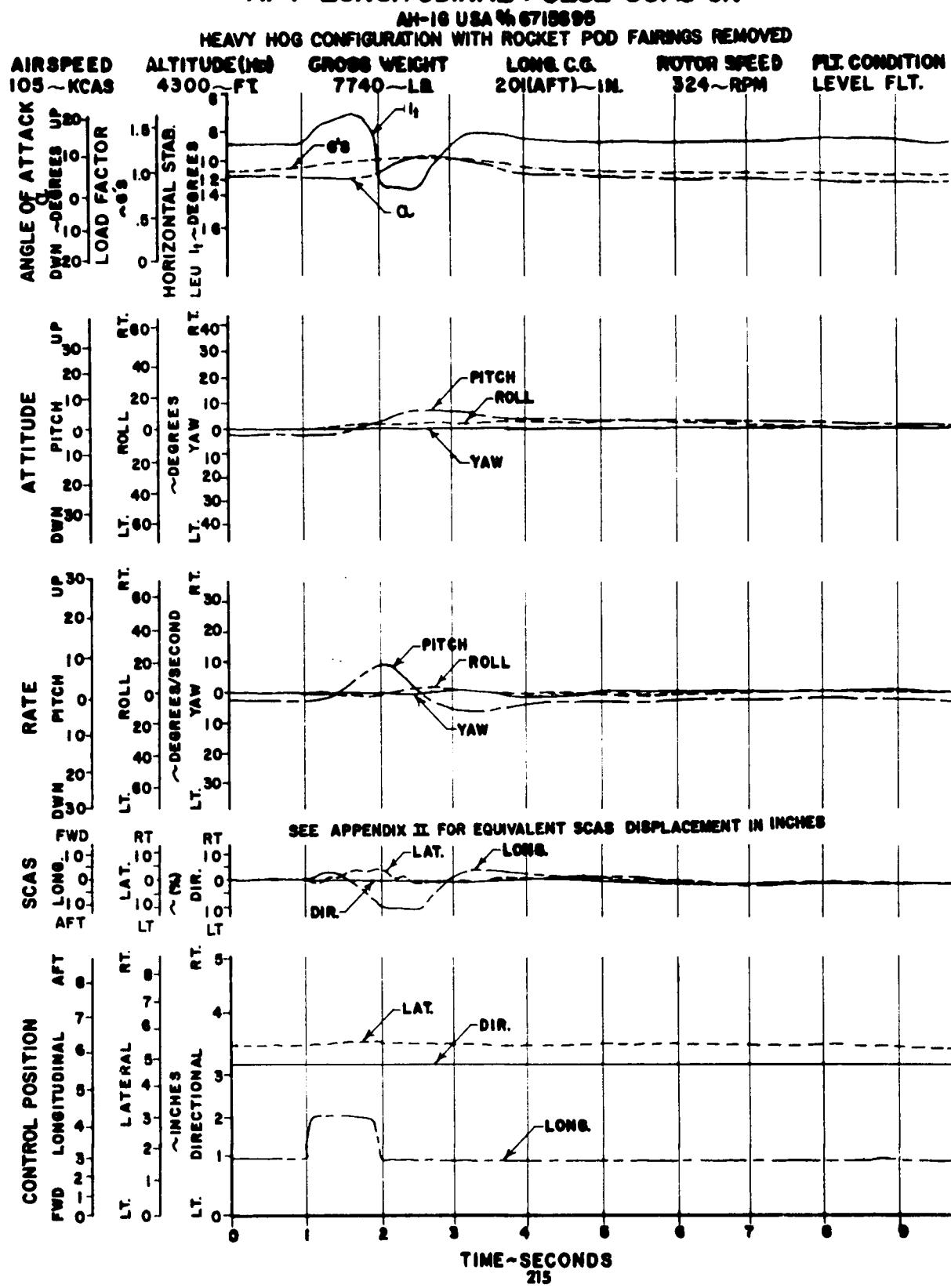


FIGURE NO. 132
AFT LONGITUDINAL PULSE SCAS ON

AH-1S USA # 6715898

HEAVY HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

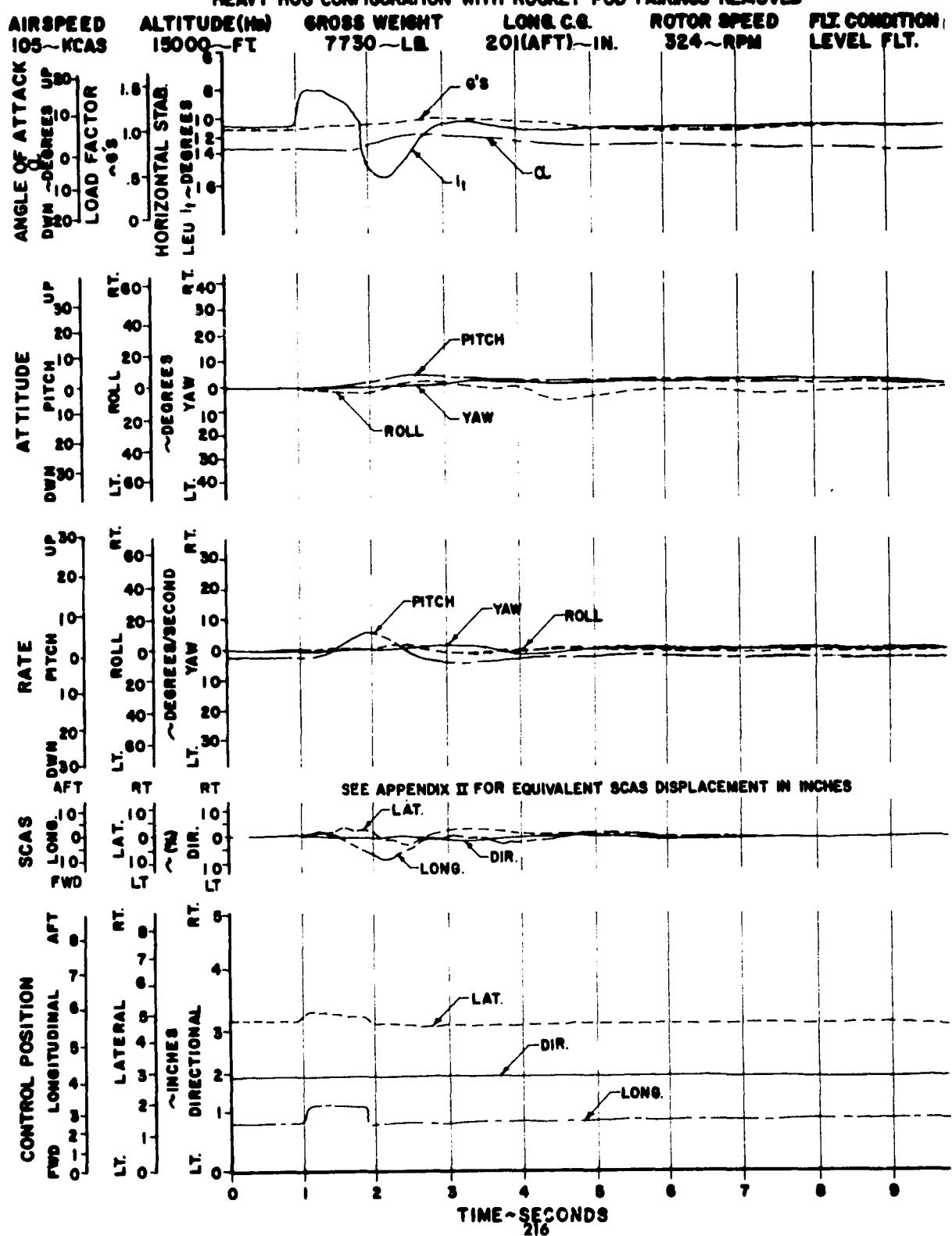
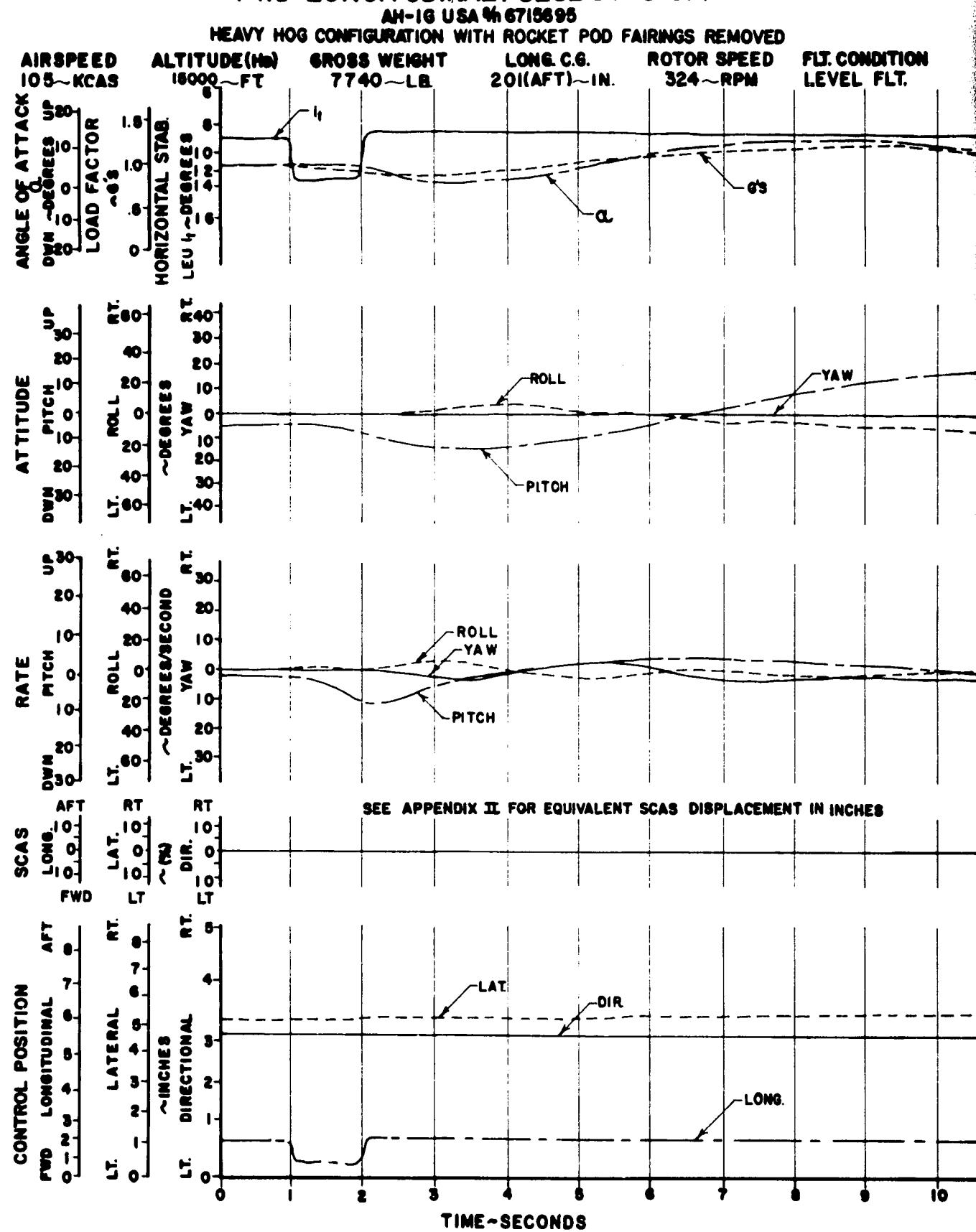


FIGURE NO. 133
FWD LONGITUDINAL PULSE SCAS OFF



0.133

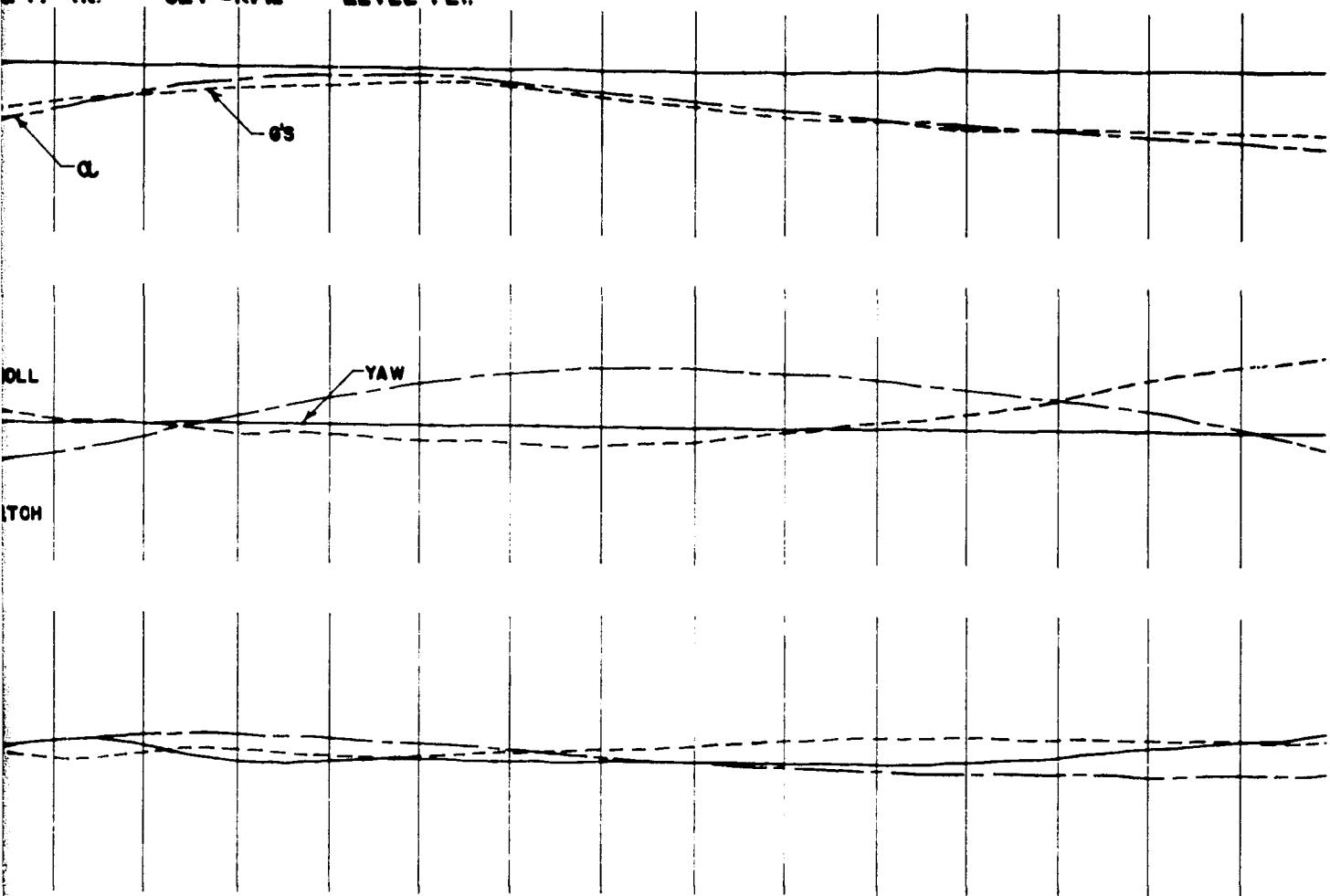
ELSE SCAS OFF

1895

KET POD FAIRINGS REMOVED
G.C.G.
(FT) - IN.

ROTOR SPEED
324 ~ RPM

FLT. CONDITION
LEVEL FLT.



EQUIVALENT SCAS DISPLACEMENT IN INCHES

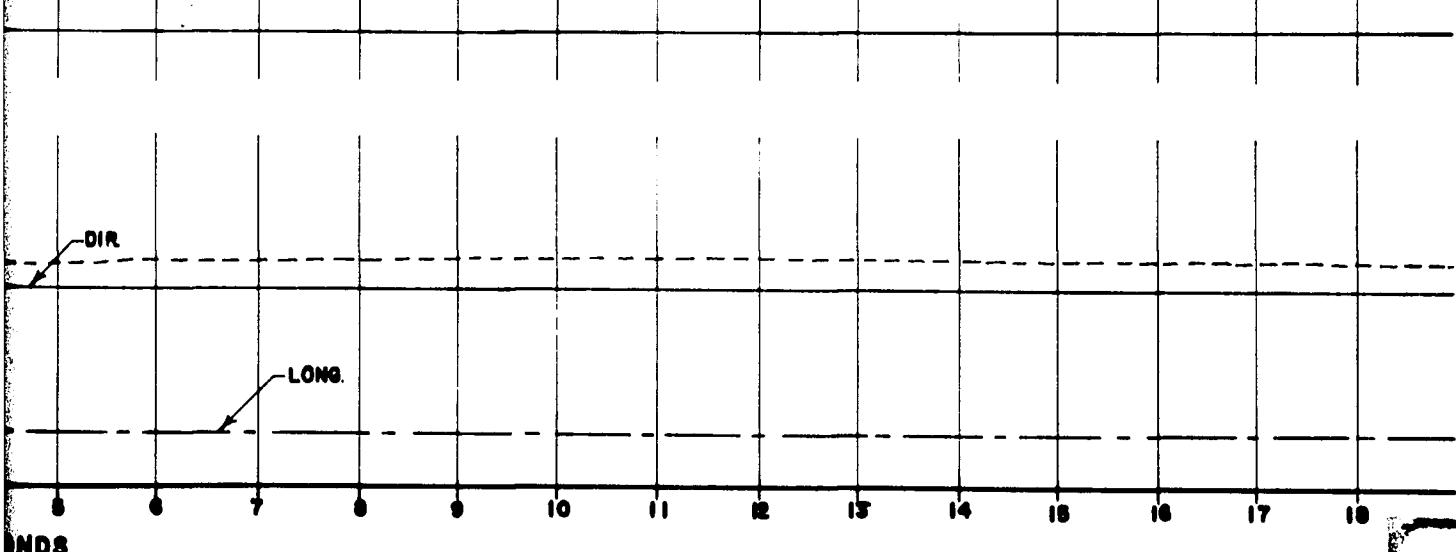


FIGURE NO. 154
LATERAL DYNAMIC STABILITY SUMMARY
AH-1G USA S/N 715693
LEFT AND RIGHT CONTROL PULSES

CONFIG	AVG GW LB	AVG ALT H _D - FT	AVG LONG C.G. - IN	SCAS	V _{MIN POWER} (LEVEL FLT)			.8V _H (LEVEL FLT)			V _H (LEVEL FLT)		
					$\frac{d}{dt}$	DESCRIP	AIRSPED - CAS	$\frac{d}{dt}$	DESCRIP	AIRSPED - CAS	$\frac{d}{dt}$	DESCRIP	AIRSPED - CAS
CLEAN	7300	4100	201 (AFT)	ON	.15 1.3	HEAVILY DAMPED	65	.57 1.8	HEAVILY DAMPED	106	NA NA	DEAD BEAT	14.
					.14 .8	HEAVILY DAMPED		.19 .6	HEAVILY DAMPED		.25 .1	LIGHTLY DAMPED	
HEAVY HOG ◇	7620	3700	201 (AFT)	ON	NA NA	DEAD BEAT	60	.05 1.1	HEAVILY DAMPED	106	NA NA	DEAD BEAT	150
					.29 .6	HEAVILY DAMPED		.27 .1	LIGHTLY DAMPED		.21 .1	LIGHTLY DAMPED	
HEAVY HOG ◇	8360	4500	195 (MID)	ON	.03 .9	HEAVILY DAMPED	60	.06 1.3	HEAVILY DAMPED	104	NA NA	DEAD BEAT	138
					.17 .1	LIGHTLY DAMPED		.24 .1	LIGHTLY DAMPED		.27 .1	LIGHTLY DAMPED	
HEAVY HOG ◇ ◇	8680	3600	195 (MID)	ON	.17 1.3	HEAVILY DAMPED	62	.36 1.6	HEAVILY DAMPED	103	NA NA	DEAD BEAT	138
					.23 .3	LIGHTLY DAMPED		.24 .1	LIGHTLY DAMPED		.27 .1	LIGHTLY DAMPED	
HEAVY HOG ◇ ◇	9270	4300	200 (AFT)	ON	NF NF	NF	NF	.20 1.2	HEAVILY DAMPED	104	NA NA	DEAD BEAT	132
					OFF	NF		NF	NF		.21 .1	LIGHTLY DAMPED	
HEAVY HOG ◇	7690	15060	201 (AFT)	ON	.07 .9	HEAVILY DAMPED	55	NA NA	DEAD BEAT	68	NA NA	DEAD BEAT	102
					OFF	NF		NF	NF		.27 .1	LIGHTLY DAMPED	
◇ ◇ HEAVY SCOUT	9000	5000	200 (AFT)	ON	NF	NF	NF	NA NA	DEAD BEAT	103	.30 1.5	HEAVILY DAMPED	140

CONFIG	AVG GW LB	AVG ALT H _D - FT	AVG LONG C.G. - IN	SCAS	V _{LIMIT} (DIVE)			V _{MAX} (R/C)			V _{MIN} (R/D)		
					$\frac{d}{dt}$	DESCRIP	AIRSPED - CAS	$\frac{d}{dt}$	DESCRIP	AIRSPED - CAS	$\frac{d}{dt}$	DESCRIP	AIRSPED - CAS
CLEAN	7300	4100	201 (AFT)	ON	.44 1.5	HEAVILY DAMPED	180	.20 1.3	HEAVILY DAMPED	65	NF NF	NF	NF
					.29 .1	LIGHTLY DAMPED		.26 .1	LIGHTLY DAMPED		NF NF	NF	
HEAVY HOG ◇	7620	3700	201 (AFT)	ON	NA NA	DEAD BEAT	170	NF	NF	NF	NA NA	NF	NF
					OFF	.27 0		NF	NF		NF NF	NF	
HEAVY HOG ◇	8360	4500	195 (MID)	ON	NA NA	DEAD BEAT	170	.27 1.4	HEAVILY DAMPED	60	NA NA	DEAD BEAT	68
					OFF	.16 .2		.25 .1	LIGHTLY DAMPED		.12 .8	HEAVILY DAMPED	
HEAVY HOG ◇ ◇	8680	3600	195 (MID)	ON	.14 1.2	HEAVILY DAMPED	180	.27 1.4	HEAVILY DAMPED	64	.07 1.1	HEAVILY DAMPED	74
					OFF	.22 .1		.24 0	NEUTRAL DAMPED		NF NF	NF	
◇ ◇ HEAVY HOG	9270	4300	200 (AFT)	ON	.16 1.2	HEAVILY DAMPED	170	NF	NF	NF	NF	NF	NF

NOTE: ALL APPLICABLE NOTES ARE PRESENTED ON FIGURE 150.

FIGURE NO. 135
RIGHT LATERAL PULSE SCAS ON

AH-1G USA #6715695

CLEAN CONFIGURATION

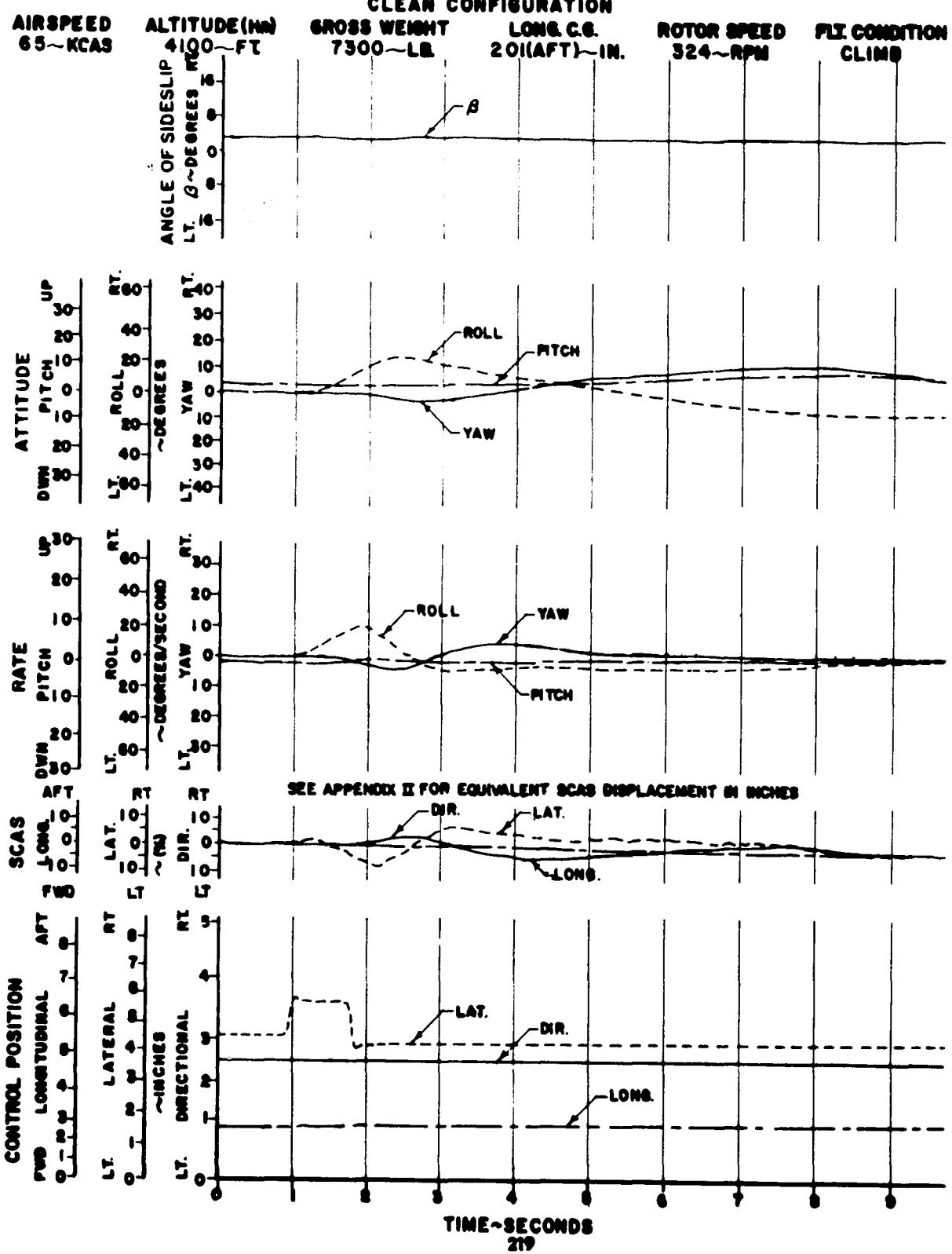


FIGURE NO. 136
RIGHT LATERAL PULSE SCAS ON

AH-1G USA #6715695

HEAVY HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

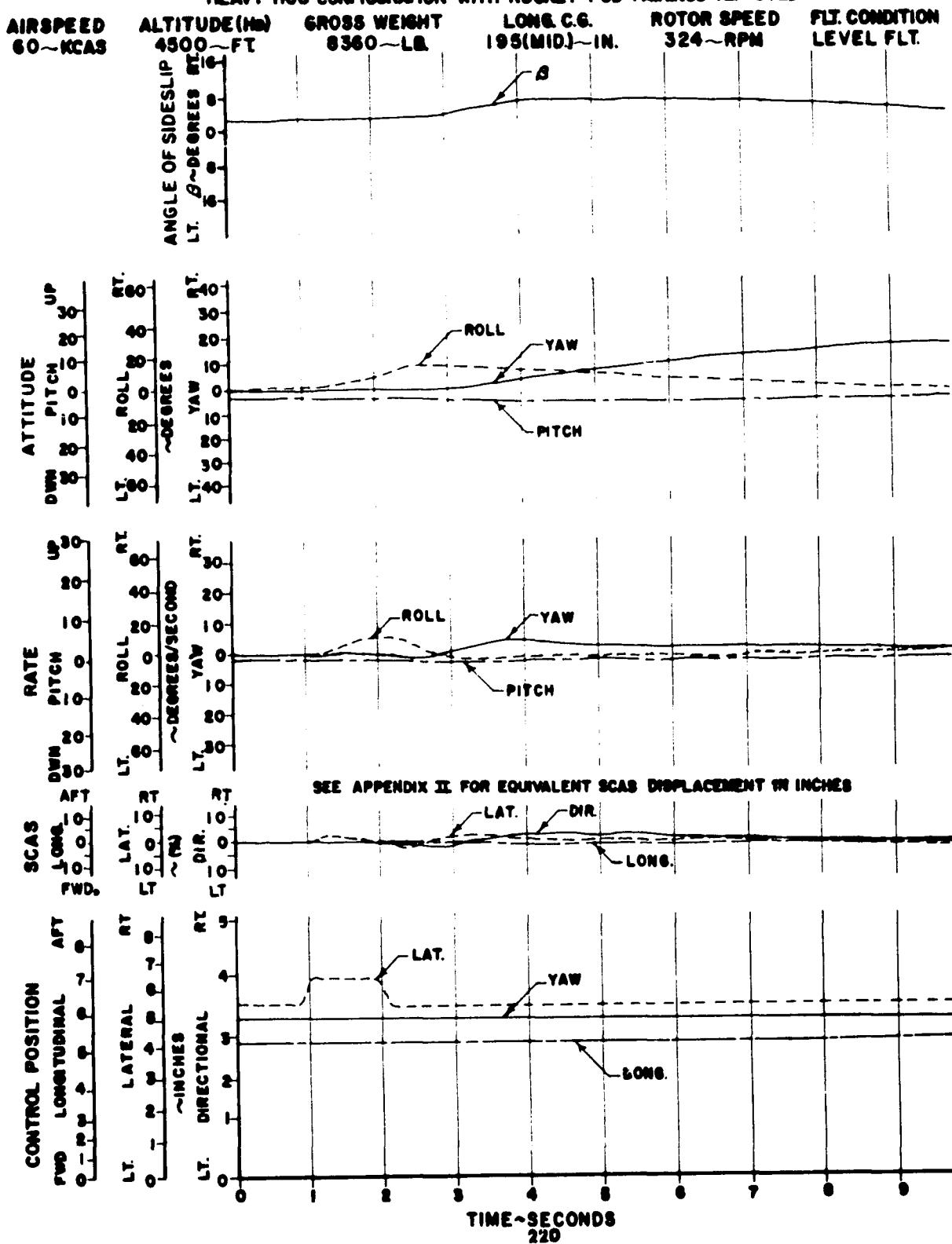


FIGURE NO. 137
RIGHT LATERAL PULSE SCAS ON

AH-1G USA 546715695

HEAVY HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

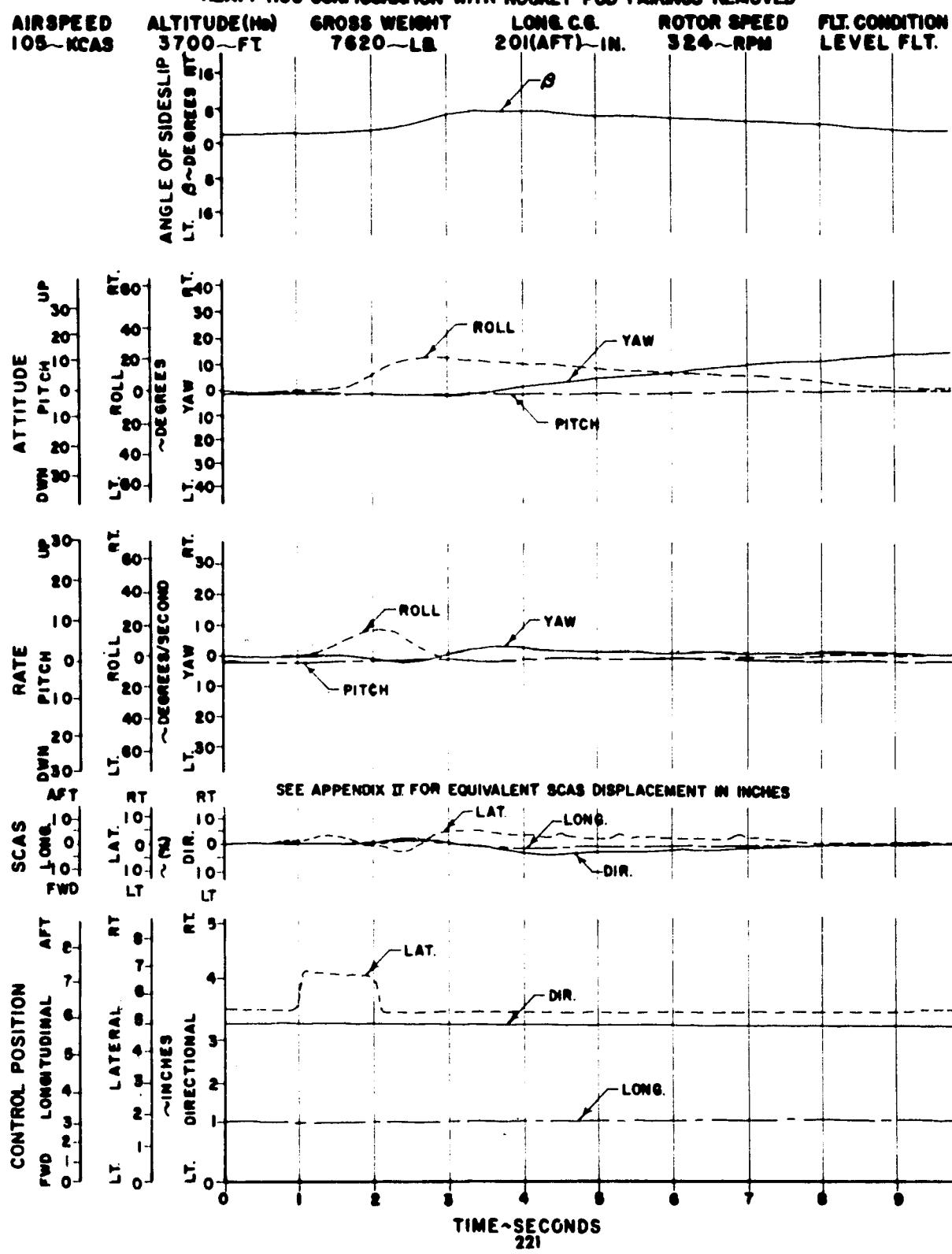


FIGURE NO. 138
RIGHT LATERAL PULSE SCAS ON

AH-1G USA #6715695

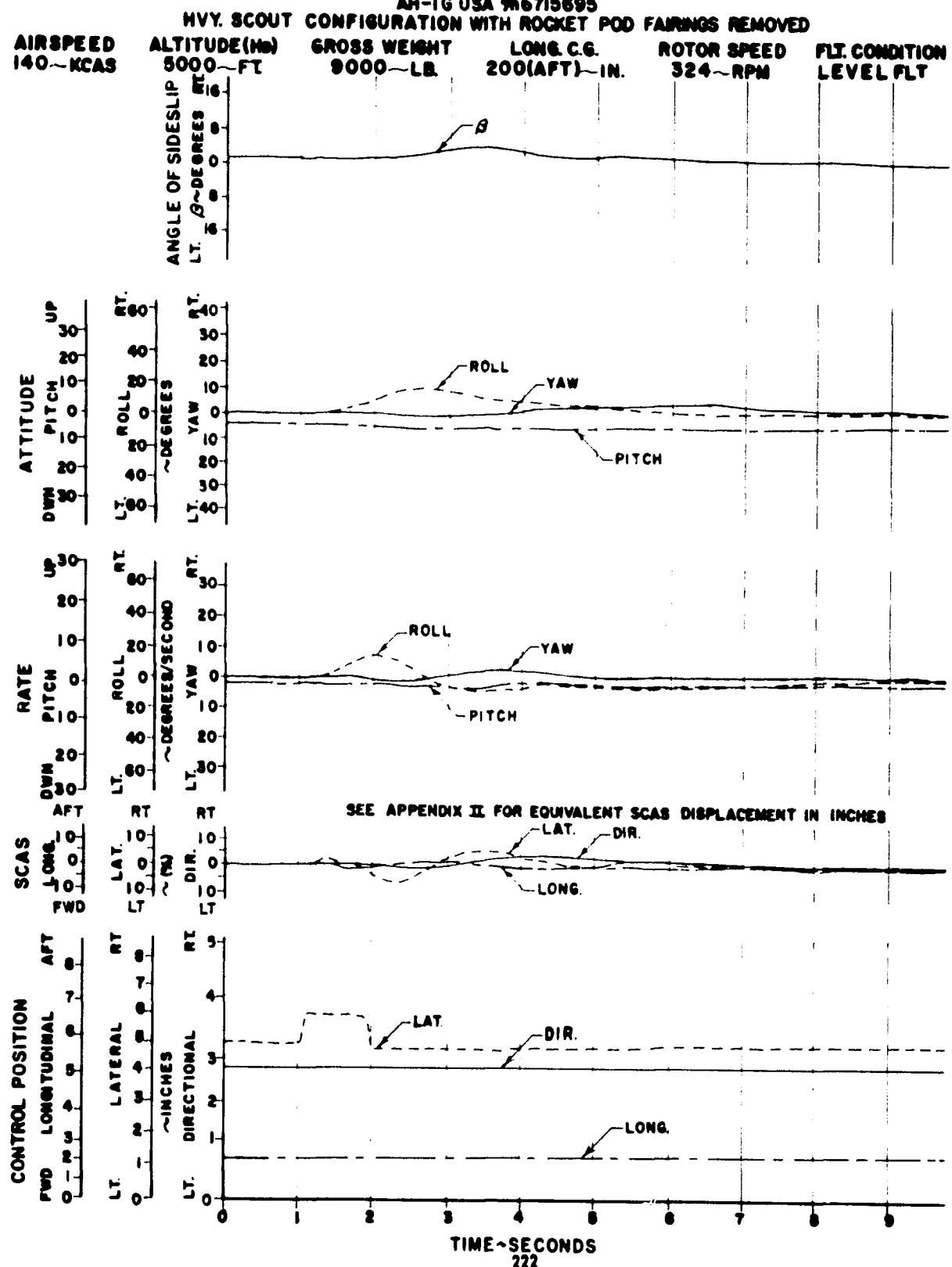


FIGURE NO. 139
RIGHT LATERAL PULSE SCAS ON

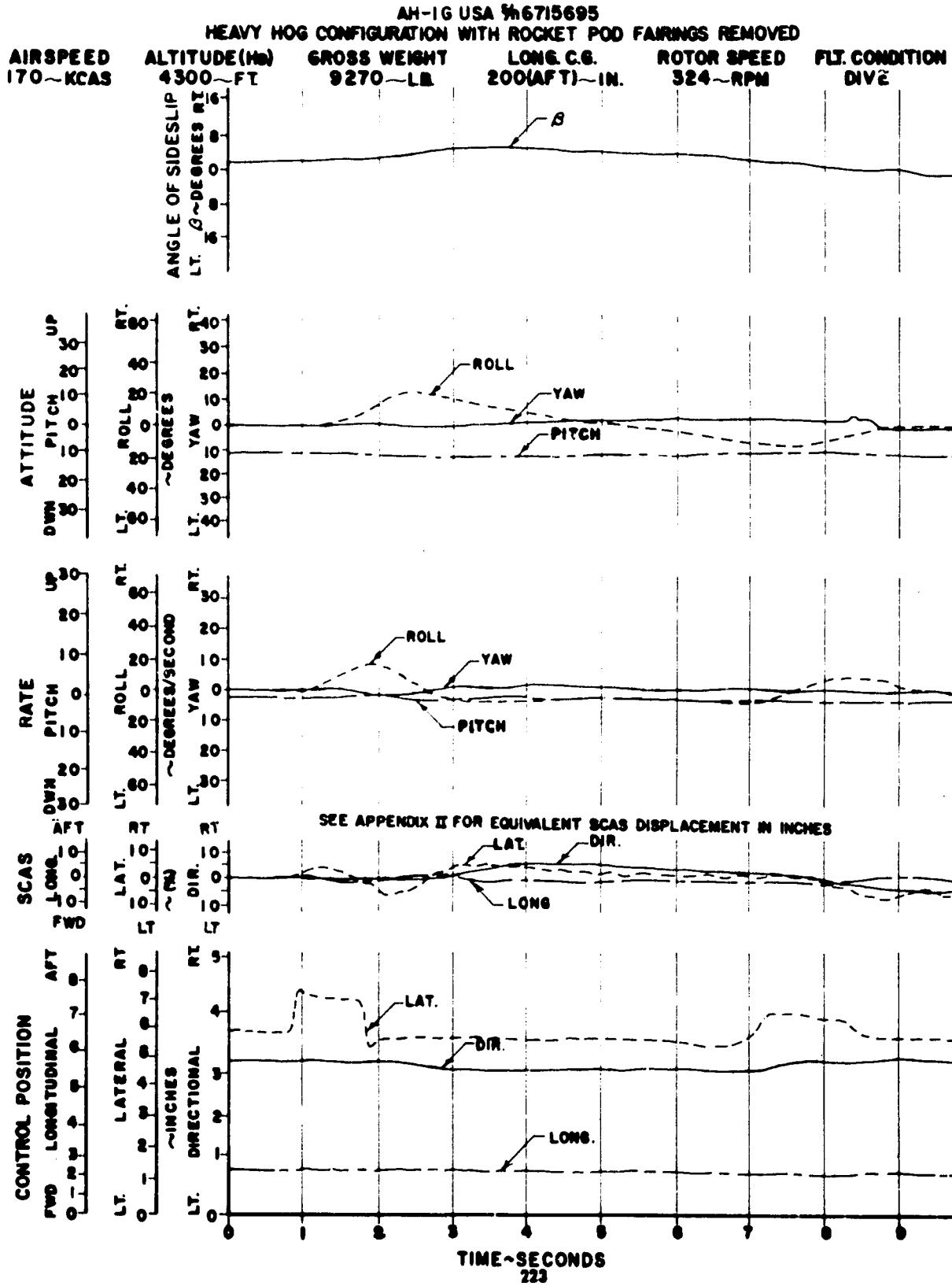
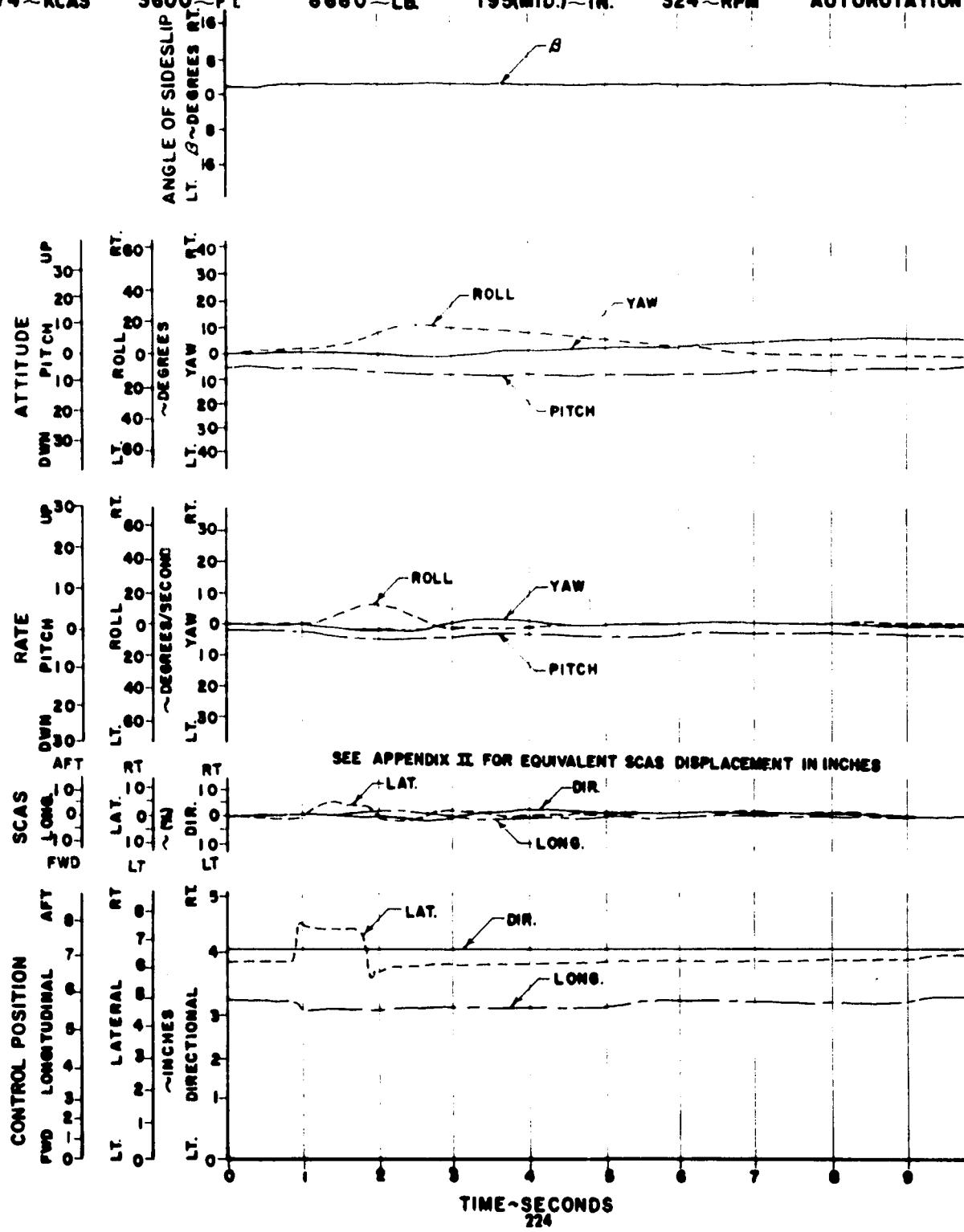


FIGURE NO.140
RIGHT LATERAL PULSE SCAS ON

AH-1G USA #6715695

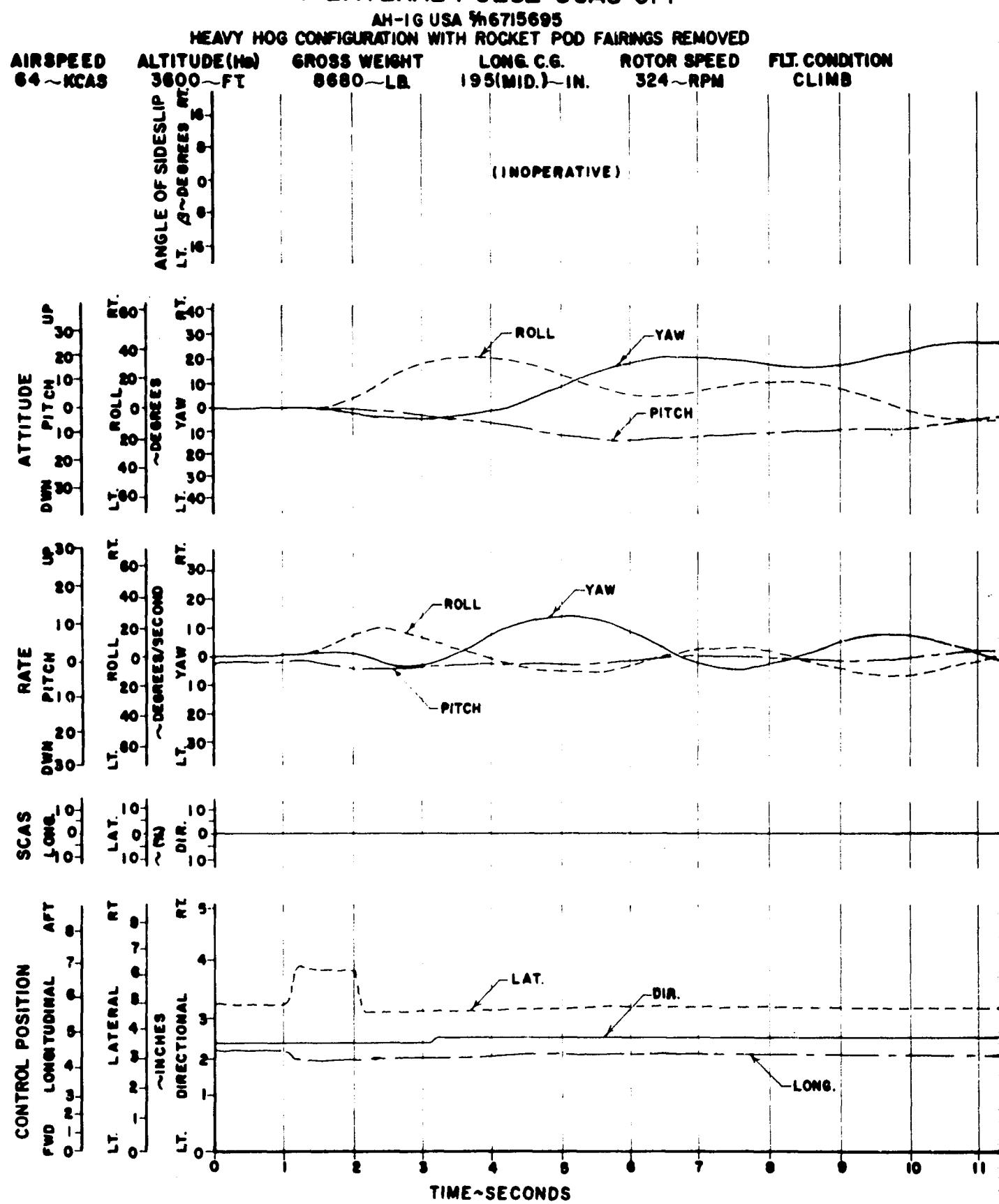
HEAVY HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

AIRSPEED 74~KCAS	ALTITUDE(Ms) 3600~FT	GROSS WEIGHT 8680~LB.	LONG. C.G. 195(MID.)~IN.	ROTOR SPEED 324~RPM	FLT. CONDITION AUTOROTATION
---------------------	-------------------------	--------------------------	-----------------------------	------------------------	--------------------------------



TIME~SECONDS
224

FIGURE NO. 141
RIGHT LATERAL PULSE SCAS OFF



D. 141
SE SCAS OFF

5695
SET POD FAIRINGS REMOVED
C.G. ROTOR SPEED
10.1 IN. 324~RPM

FLT. CONDITION
CLIMB

(OPERATIVE)

ROLL

YAW

PITCH

YAW

LAT.

DIR.

LONG.

COND'S

225

2

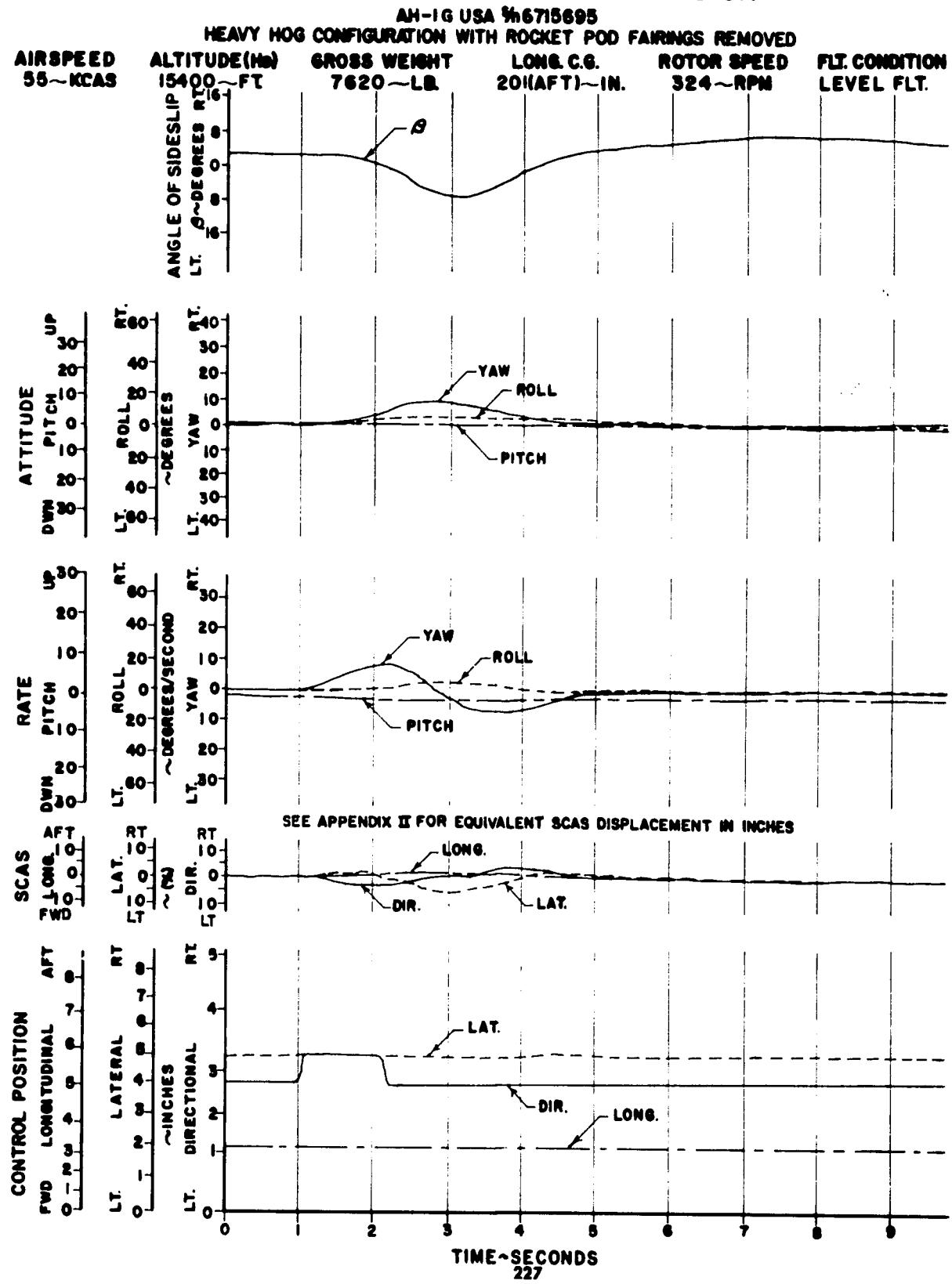
FIGURE NO. 142
DIRECTIONAL DYNAMIC STABILITY SUMMARY
AH-1G USA S/N 715695
LEFT & RIGHT CONTROL PULSES

CONFIG	AVG GW LB	AVG ALT H _D FT	AVG LONG CG IN	SCAS	V _{MIN} POWER (LEVEL FLT)			.8 V _H (LEVEL FLT)			V _H (LEVEL FLT)		
					$\frac{w}{c}$	DESCRIP	AIRSPED CAS	$\frac{w}{c}$	DESCRIP	AIRSPED CAS	$\frac{w}{c}$	DESCRIP	AIRSPED CAS
CLEAN	7210	4200	201 (AFT)	ON	.13 1.0	HEAVILY DAMPED	65	NA NA	DEAD BEAT	107	.29 .6	HEAVILY DAMPED	138
				OFF	.22 .5	HEAVILY DAMPED		.27 .2	LIGHTLY DAMPED		.27 0	NEUTRAL DAMPED	
HEAVY HOG ◆	7490	5000	201 (AFT)	ON	.15 .6	HEAVILY DAMPED	60	.10 .9	HEAVILY DAMPED	105	NF NF	NF	NF
				OFF	.19 .2	LIGHTLY DAMPED		.24 .1	LIGHTLY DAMPED		NF NF	NF	
HEAVY HOG ◇ ◇	9180	4600	200 (AFT)	ON	NA NA	DEAD BEAT	60	.23 .7	HEAVILY DAMPED	104	.26 .5	HEAVILY DAMPED	136
				OFF	NF NF	NF		.22 .6	NF		.25 .1	LIGHTLY DAMPED	
HEAVY HOG ◇	7620	15400	201 (AFT)	ON	.11 .9	HEAVILY DAMPED	55	.12 1.1	HEAVILY DAMPED	88	.36 1.3	HEAVILY DAMPED	103
				OFF	NF NF	NF		NF NF	NF		.25 .1	LIGHTLY DAMPED	

CONFIG	AVG GW LB	AVG ALT H _D FT	AVG LONG CG-IN	SCAS	V _{LIMIT} (DIVE)			V _{MAX} (R/C)			V _{MIN} (R/D)		
					$\frac{w}{c}$	DESCRIP	AIRSPED CAS	$\frac{w}{c}$	DESCRIP	AIRSPED CAS	$\frac{w}{c}$	DESCRIP	AIRSPED CAS
CLEAN	7210	4200	201 (AFT)	ON	.21 .9	HEAVILY DAMPED	180	.31 .6	HEAVILY DAMPED	64	NA NA	DEAD BEAD	75
				OFF	.27 0	NEUTRAL DAMPED		.21 .3	UNDAMPED		.09 1.1	HEAVILY DAMPED	
HEAVY HOG ◆	7490	5000	201 (AFT)	ON	NA NA	DEAD BEAT	170	NA NA	DEAD BEAT	60	.18 .6	HEAVILY DAMPED	68
				OFF	.27 0	NEUTRAL DAMPED		.24 .1	LIGHTLY DAMPED		.12 .5	LIGHTLY DAMPED	
HEAVY HOG ◇ ◇	9180	4600	200 (AFT)	ON	.28 .5	HEAVILY DAMPED	170	NF NF	NF	NF	NF NF	NF	NF
				OFF	.21 0	NEUTRAL DAMPED		NF NF	NF		NF NF	NF	

NOTE: ALL APPLICABLE NOTES ARE PRESENTED ON FIGURE 150.

FIGURE NO. 143
RIGHT DIRECTIONAL PULSE SCAS ON



TIME-SECONDS
227

FIGURE NO. 144
RIGHT DIRECTIONAL PULSE SCAS ON

AH-1G USA #6715695

HEAVY HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

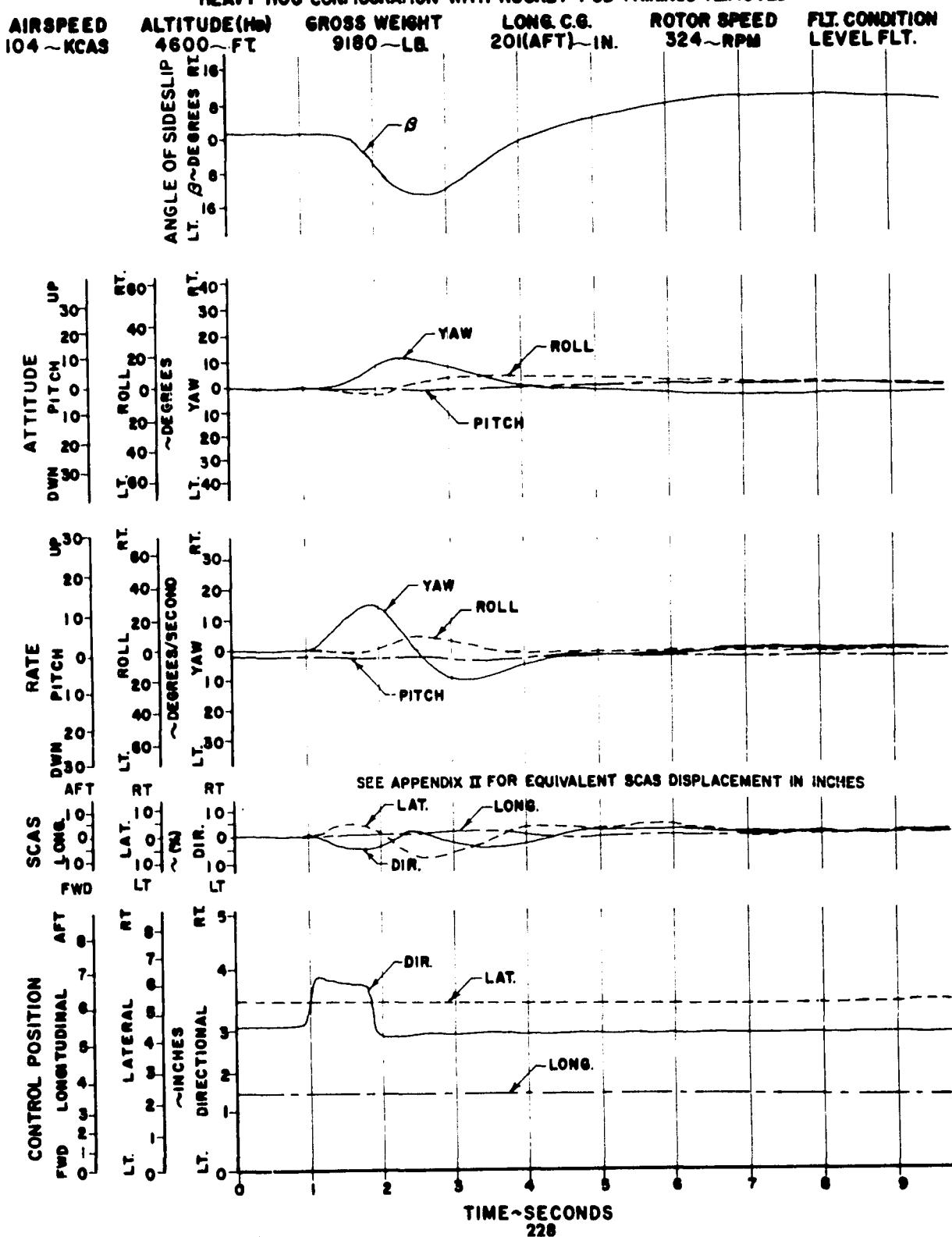


FIGURE NO. 145
LEFT DIRECTIONAL PULSE SCAS ON

AH-1G USA #6715695

HEAVY HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

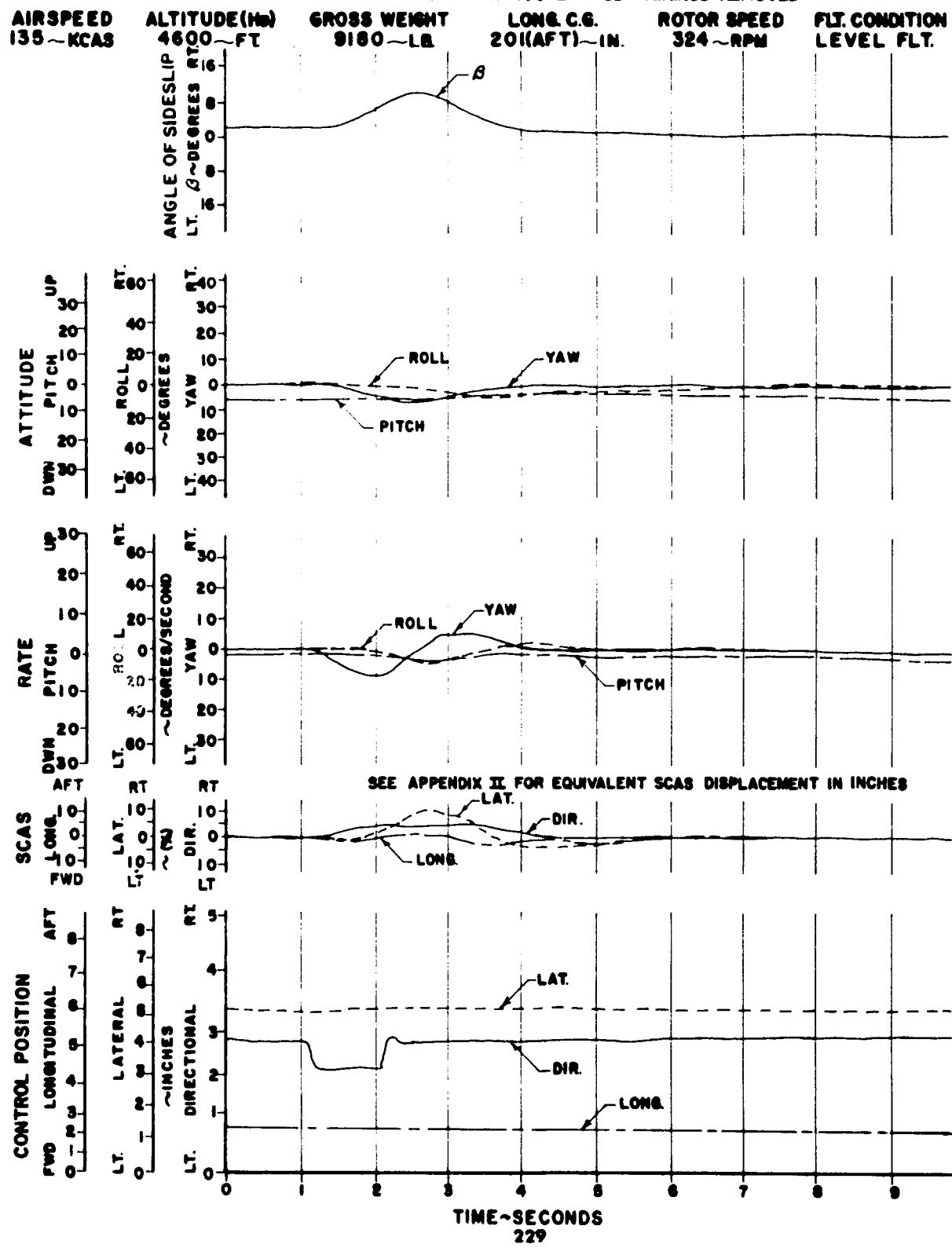


FIGURE NO. 146
LEFT DIRECTIONAL PULSE SCAS ON

AH-1G USA #6715695

HEAVY HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

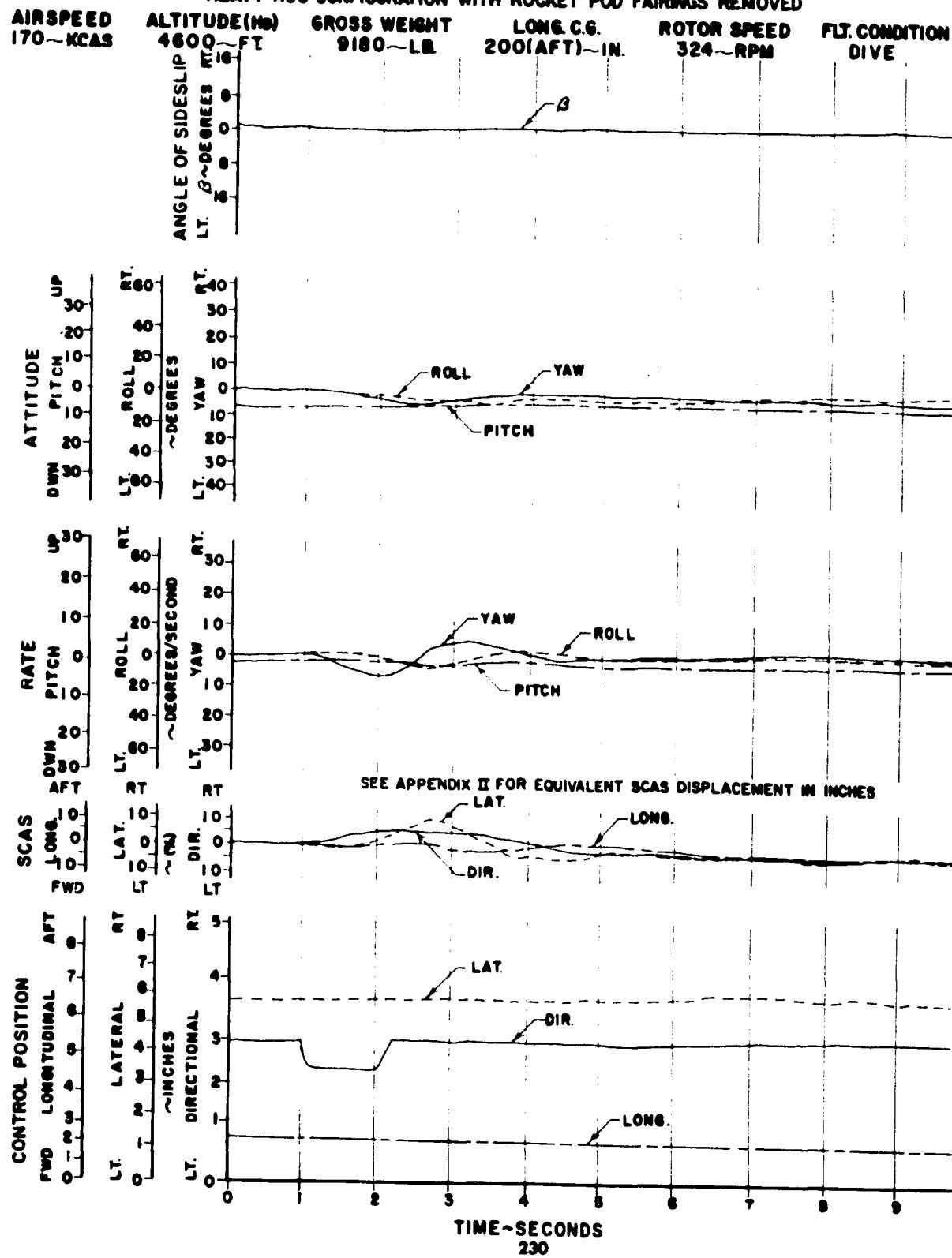


FIGURE NO. 147
LEFT DIRECTIONAL PULSE SCAS ON

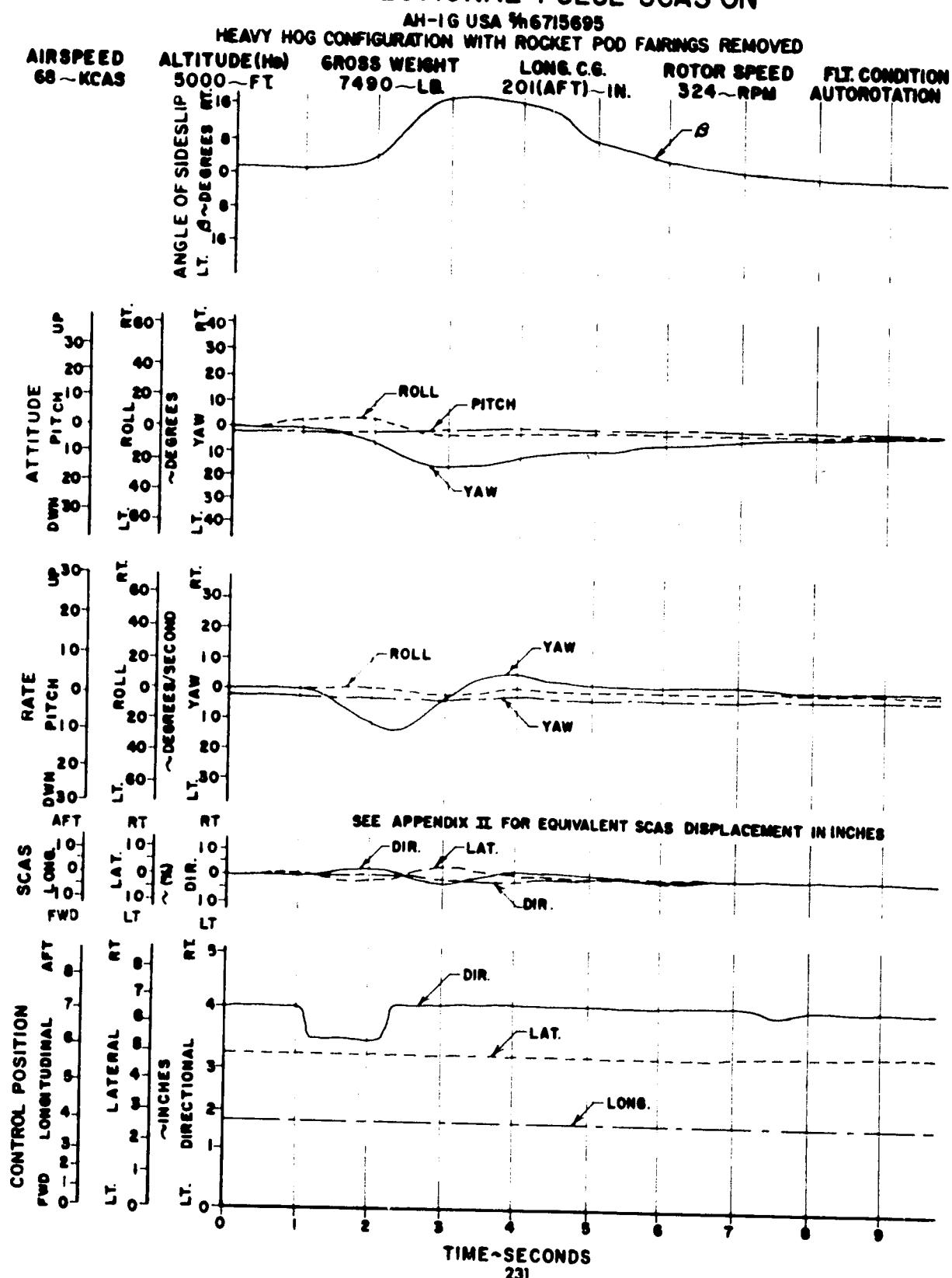
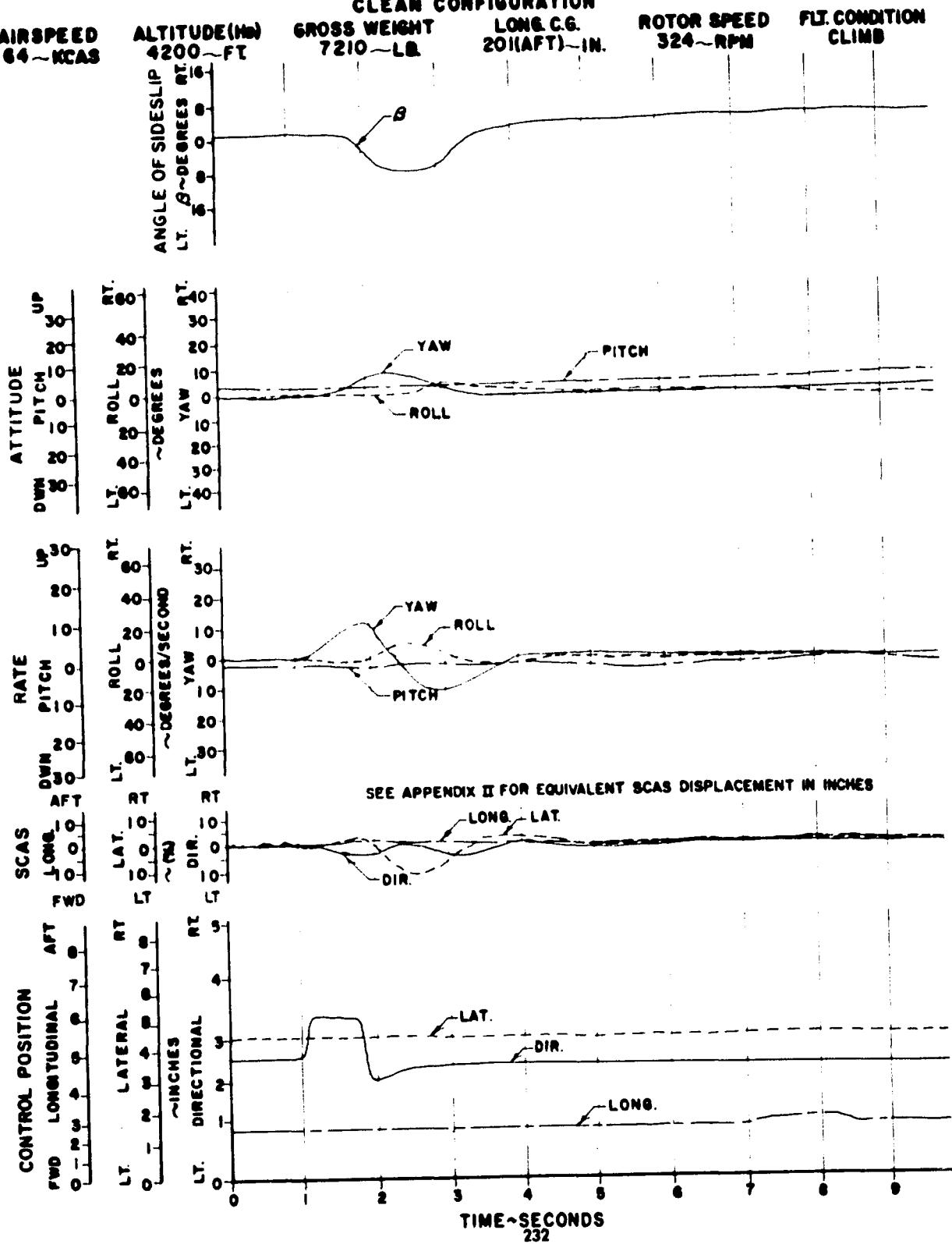


FIGURE NO. 148
RIGHT DIRECTIONAL PULSE SCAS ON

AH-1G USA 56715695
CLEAN CONFIGURATION

AIR SPEED 64-KIAS ALTITUDE(MIN) 4200-FT GROSS WEIGHT 7210-LB LONG. C.G. 20(AFT)-IN. ROTOR SPEED 324-RPM FLT. CONDITION CLIMB



232

FIGURE NO. 149
RIGHT DIRECTIONAL PULSE SCAS OFF

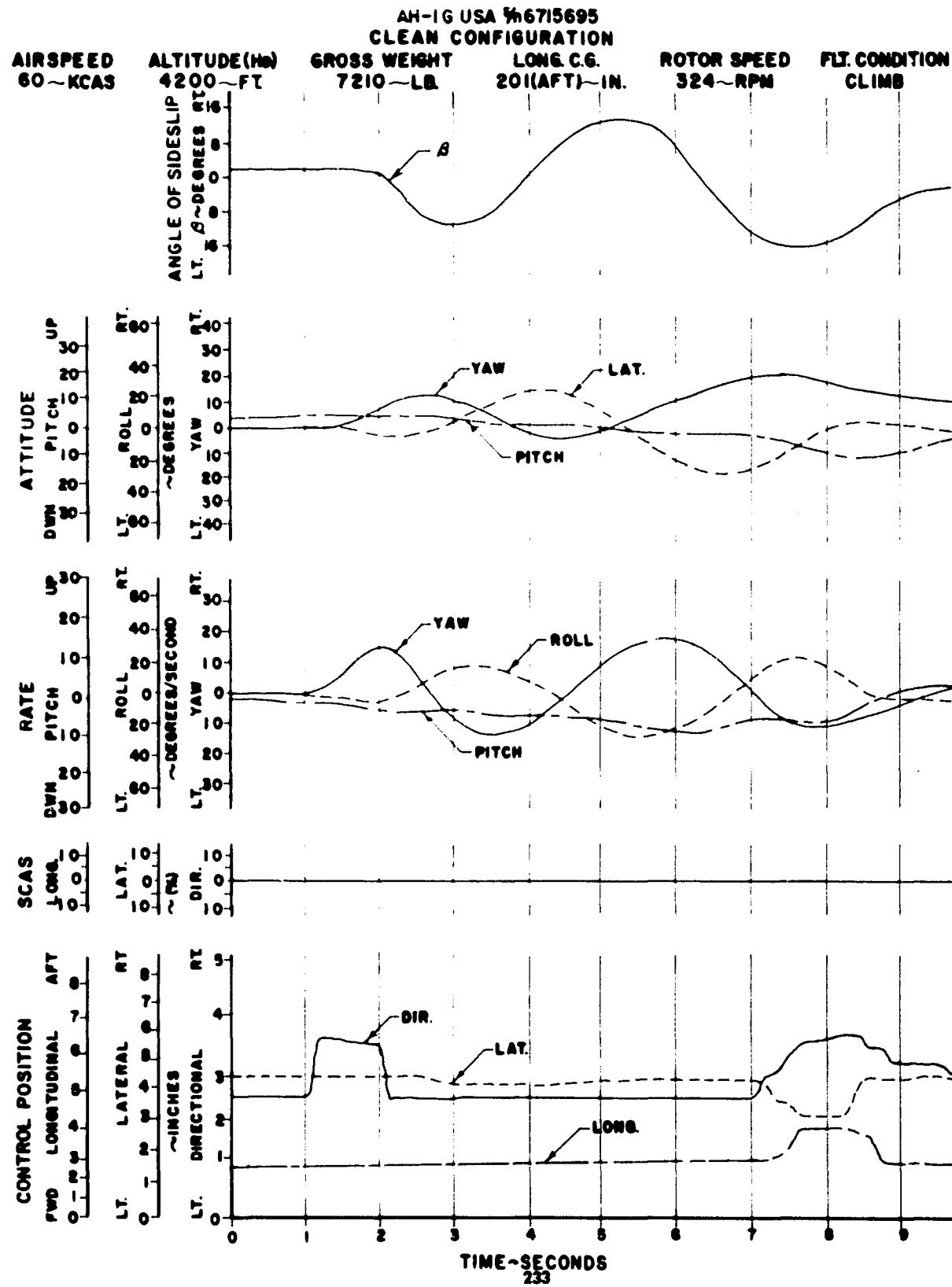


FIGURE NO. 150
LATERAL DIRECTIONAL DYNAMIC STABILITY
SKID TUBE FAIRING COMPARISON
LEFT AND RIGHT CONTROL PULSES

LATERAL

CONFIG	AVG GW LB	AVG ALT FT	AVG LONG CG-IN	SCAS	ω_n^2 (LEVEL FLT)			ω_n^2 (LEVEL FLT)			ω_n^2 (DIVE)			AH-1G USA S/N	
					ζ	DESCRIP	AIRSPD - CAS	ζ	DESCRIP	AIRSPD - CAS	ζ	DESCRIP	AIRSPD - CAS		
CLEAN SKID FAIR- INGS OFF	8630	3700	199.5 (APT)		ON	.20 1.4	HEAVILY DAMPED	110	.51 1.0	HEAVILY DAMPED	143	NA NA	DEAD BEAT	165	615247
					OFF	NF NF	NF		.29 .1	UNDAMPED		.29 .1	UNDAMPED		
CLEAN	7500	4100	201 (AFT)		ON	.57 1.3	HEAVILY DAMPED	100	NA NA	DEAD BEAT	142	.44 1.5	HEAVILY DAMPED	180	715695
					OFF	.19 .6	HEAVILY DAMPED		.29 .1	LIGHTLY DAMPED		.29 .1	LIGHTLY DAMPED		

DIRECTIONAL

CONFIG	AVG GW LB	AVG ALT FT	AVG LONG CG IN	SCAS	ω_n^2 (LEVEL FLT)			ω_n^2 (LEVEL FLT)			ω_n^2 (DIVE)			AH-1G USA S/N	
					ζ	DESCRIP	AIRSPD - CAS	ζ	DESCRIP	AIRSPD - CAS	ζ	DESCRIP	AIRSPD - CAS		
CLEAN SKID TUBE FAIR- INGS OFF	8630	3700	199.5 (AFT)		ON	NA NA	HEAVILY DAMPED	115	.29 .5	HEAVILY DAMPED	143	.41 .5	HEAVILY DAMPED	165	615247
					OFF	.25 .1	UNDAMPED		.25 .2	UNDAMPED		NF NF	NF		
CLEAN	7210	4200	201 (AFT)		ON	NA NA	DEAD BEAT	107	.29 .6	HEAVILY DAMPED	138	.21 .9	HEAVILY DAMPED	180	715695
					OFF	.27 .2	LIGHTLY DAMPED		.27 .3	NEUTRAL DAMPED		.27 .0	NEUTRAL DAMPED		

- NOTES:
1. \odot DENOTES WITHOUT ROCKETS.
 2. \odot \odot DENOTES WITH ROCKETS.
 3. ω_n IS THE DAMPED NATURAL FREQUENCY IN CYCLES PER SECOND.
 4. ζ DAMPING RATIO.
 5. DESCRIPTION DENOTES DEGREE OF DAMPING BASED ON THE FOLLOWING DEFINITIONS.
 - a. DEAD BEAT ($\zeta = 1.8$)
 - b. HEAVILY DAMPED ($\zeta = .5$ to 1.8)
 - c. LIGHTLY DAMPED ($\zeta = .1$ to $.4$)
 - d. NEUTRALLY DAMPED ($\zeta = 0$)
 - e. UNDAMPED ($\zeta < 0$)
 6. "NA" DENOTES THAT ω_n and ζ ARE NOT AVAILABLE.
 7. "NF" DENOTES THAT THE CONDITION WAS NOT FLOWN.
 8. ALL ABOVE NOTES ARE APPLICABLE FOR FIGURE 126, 134, AND 142.

FIGURE No. 151
SUMMARY LATERAL-DIRECTIONAL DYNAMIC STABILITY
AH-1G UBA 4715695
SCAS ON

NOTES: 1. ALL CONDITIONS TESTED ON S/N 715695
 FALL WITHIN SOLID LINE

2. O DENOTES CONDITIONS TESTED ON
 S/N 615247 WITH SKID TUBE FAIRINGS
 REMOVED

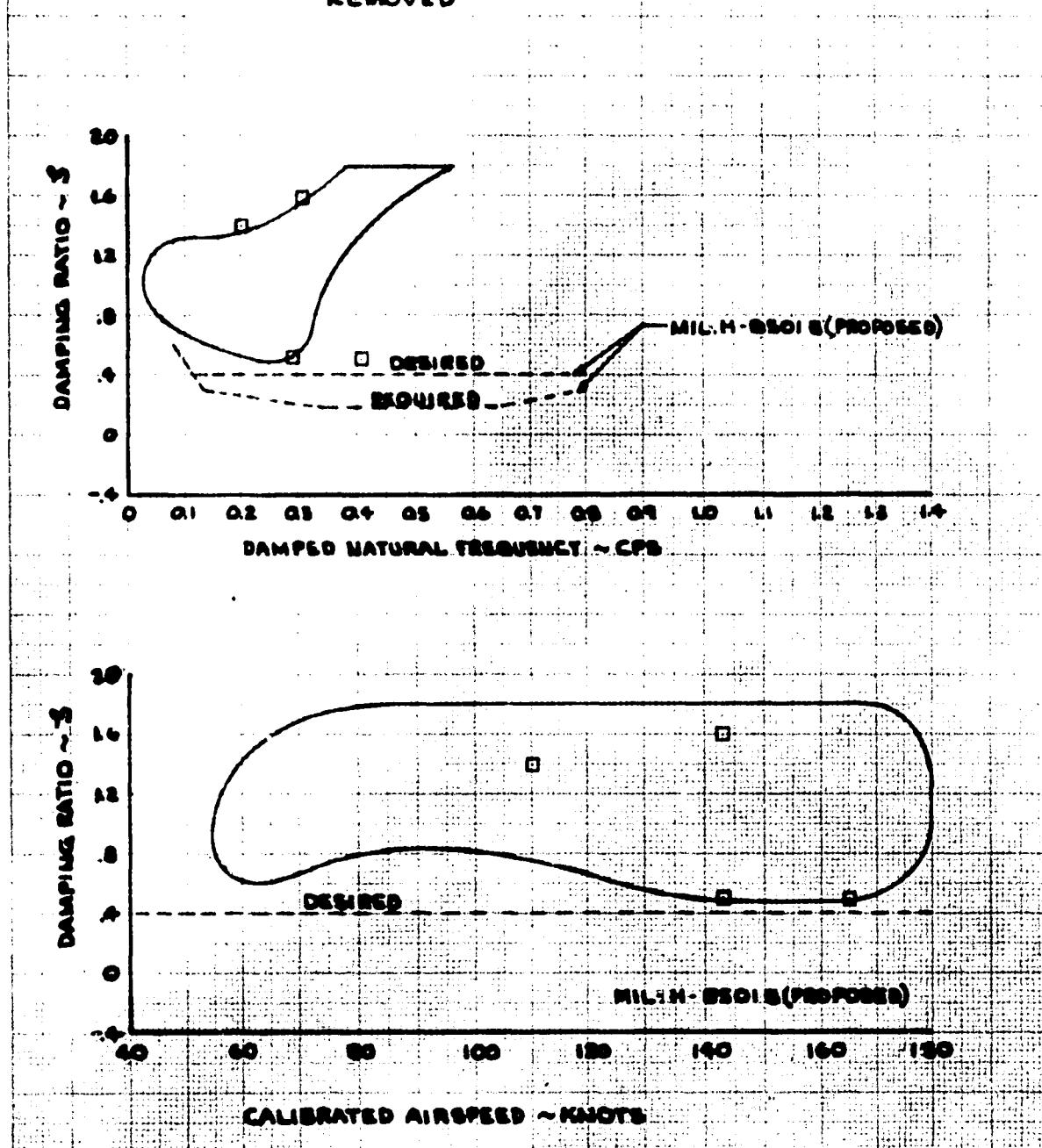


FIGURE NO. 152
SUMMARY LATERAL-DIRECTIONAL DYNAMIC STABILITY
AH-1G USA #715695
SKID OFF

NOTES: 1. ALL CONDITIONS TESTED ON S/N 715695.
 FALL WITHIN SOLID LINE.

2. O DENOTES CONDITIONS TESTED ON
 S/N 615247 WITH SKID TUBE FAIRINGS
 REMOVED

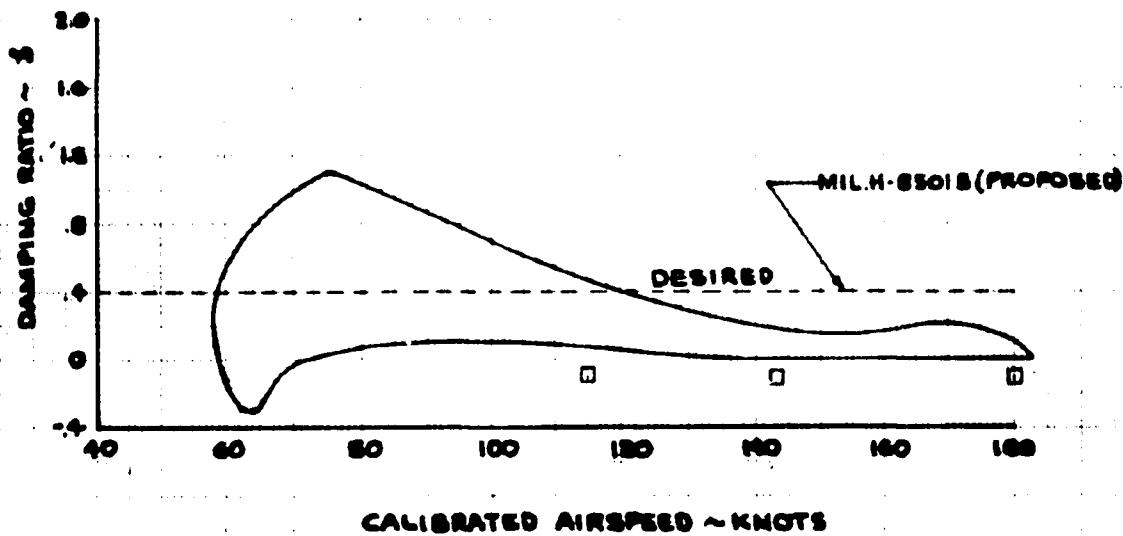
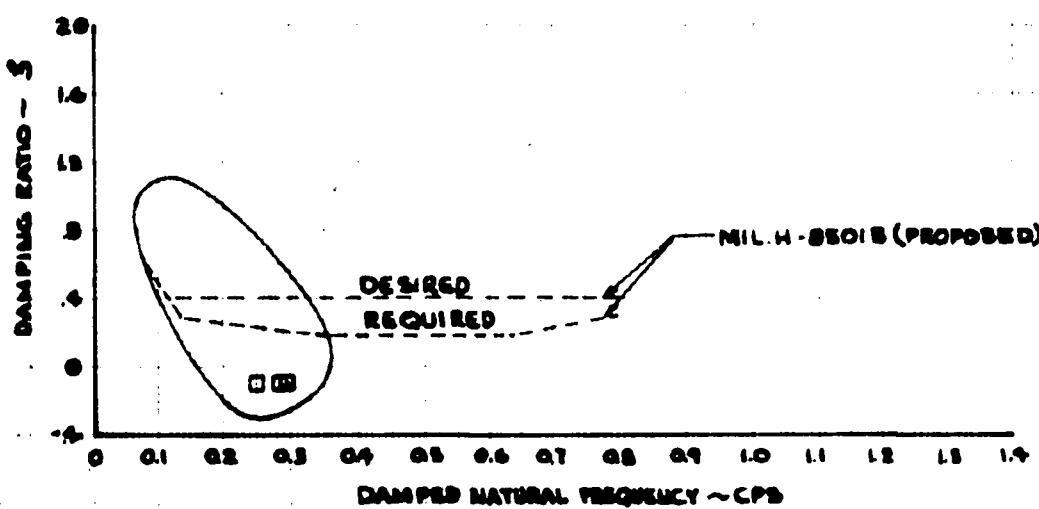
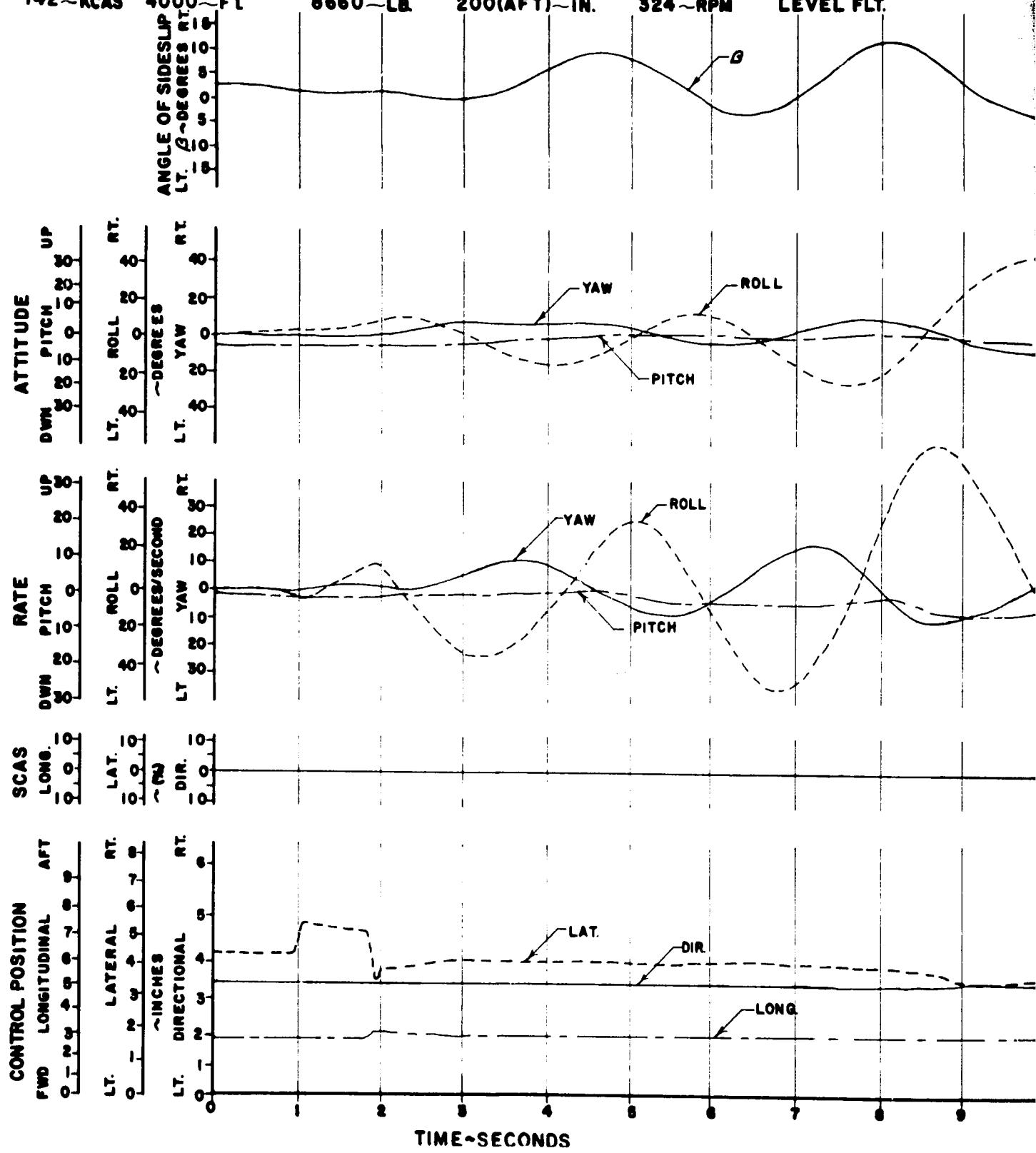


FIGURE NO. 153
RIGHT LATERAL PULSE SCAS OFF

AH-1G USA 96615247

CLEAN CONFIGURATION WITH LANDING GEAR CROSS TUBE FAIRINGS REMOVED

AIRSPEED ALTITUDE(HA) 4000~FT GROSS WEIGHT 8660~LB. LONG. C.G. 200(AFT)~IN. ROTOR SPEED 324~RPM FLT. CONDITION LEVEL FLT.



O. 153

LSE SCAS OFF

15247

AR CROSS TUBE FAIRINGS REMOVED

B.C.G.
FT)~IN. ROTOR SPEED FLT. CONDITION
 324~RPM LEVEL FLT.

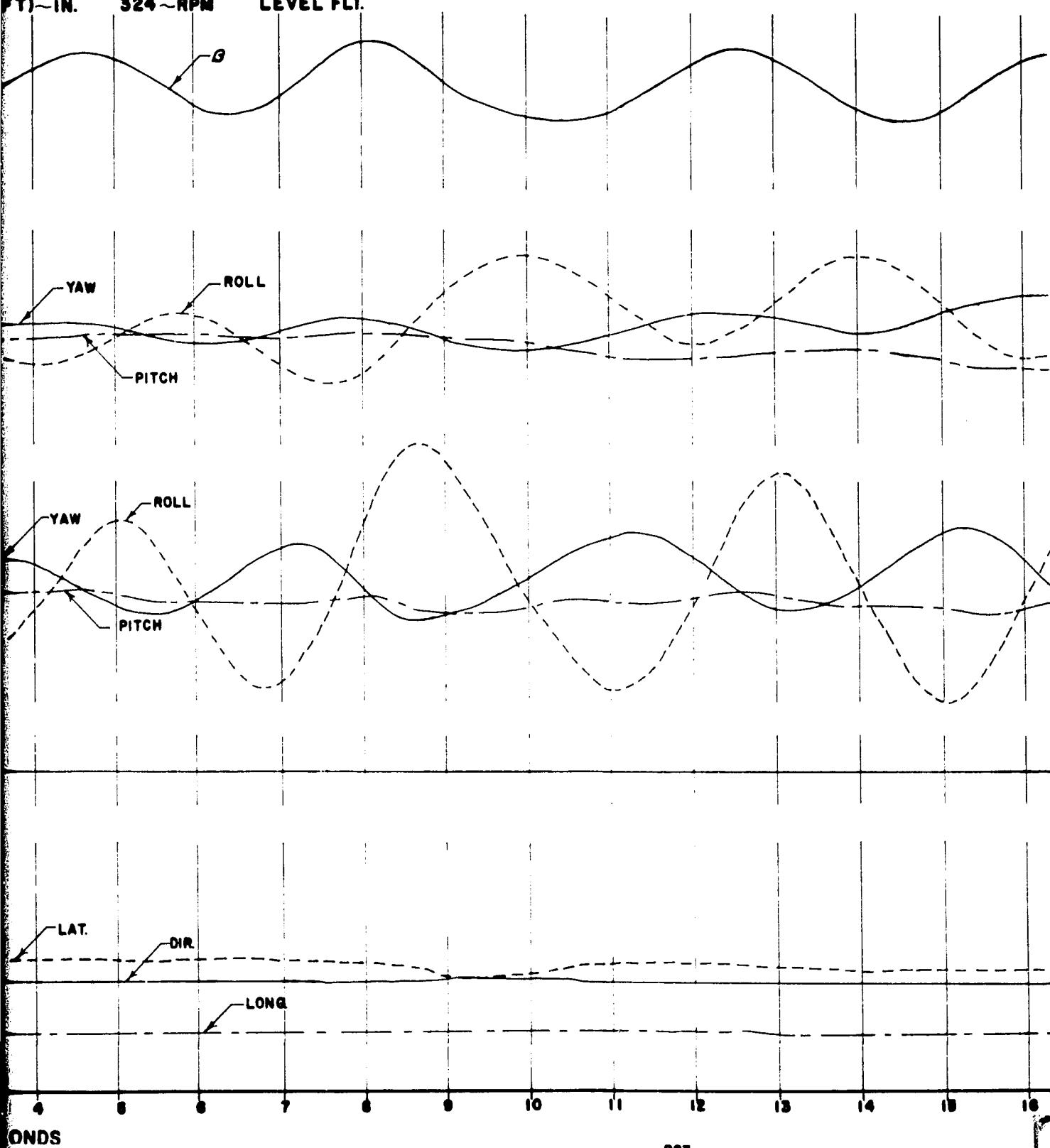
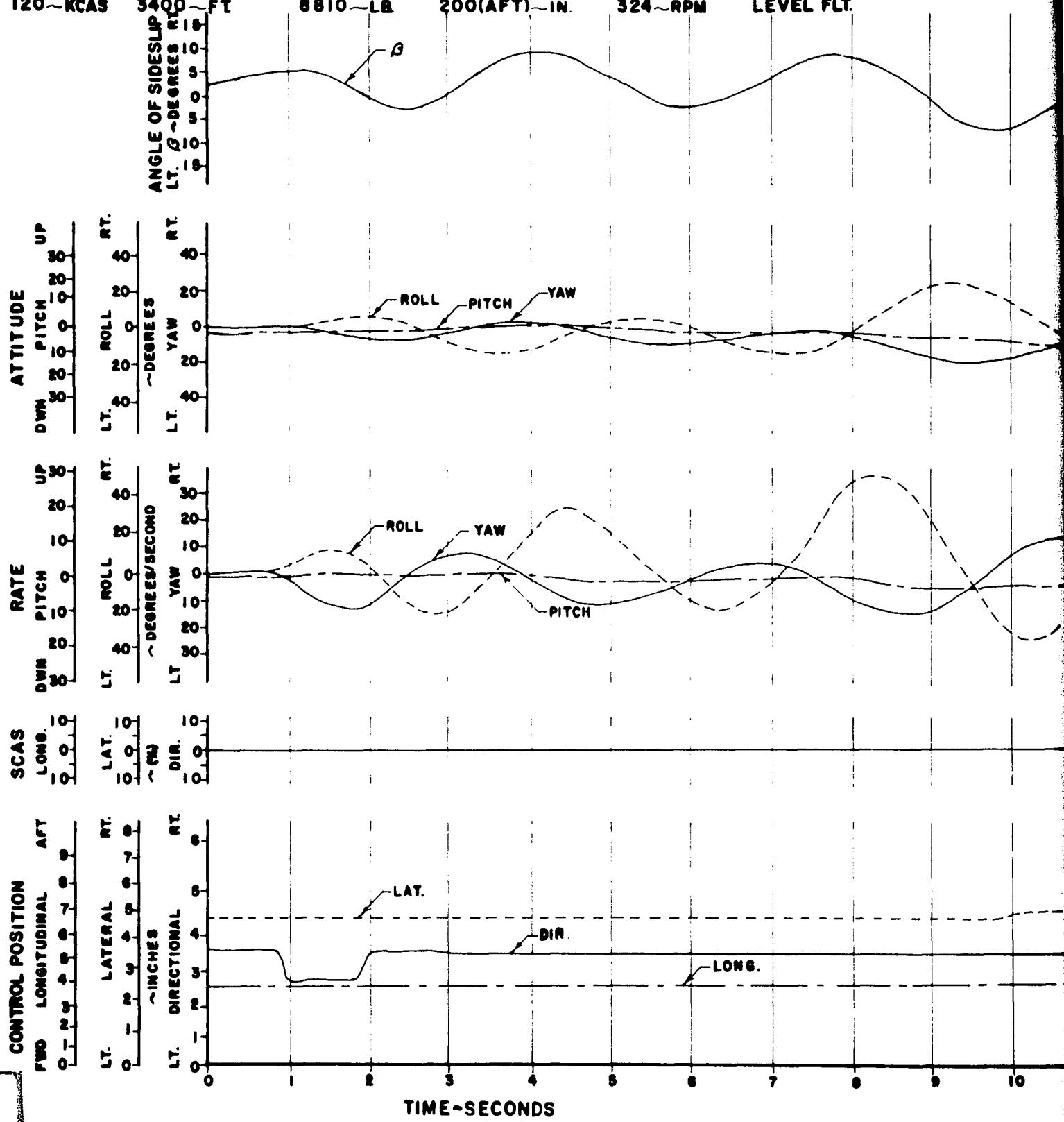


FIGURE NO. 154
LEFT DIRECTIONAL PULSE SCAS OFF

AH-1G USA 96615247

CLEAN CONFIGURATION WITH LANDING GEAR CROSS TUBE FAIRINGS REMOVED

AIR SPEED 120-KCAS ALTITUDE (HO) 3400 FT GROSS WEIGHT 8810 LB. LONG. C.G. 200(AFT)-IN. ROTOR SPEED 324-RPM FLT. CONDITION LEVEL FLT.



SCAS OFF

TUBE FAIRINGS REMOVED

ROTOR SPEED 324~RPM FLT. CONDITION LEVEL FLT.

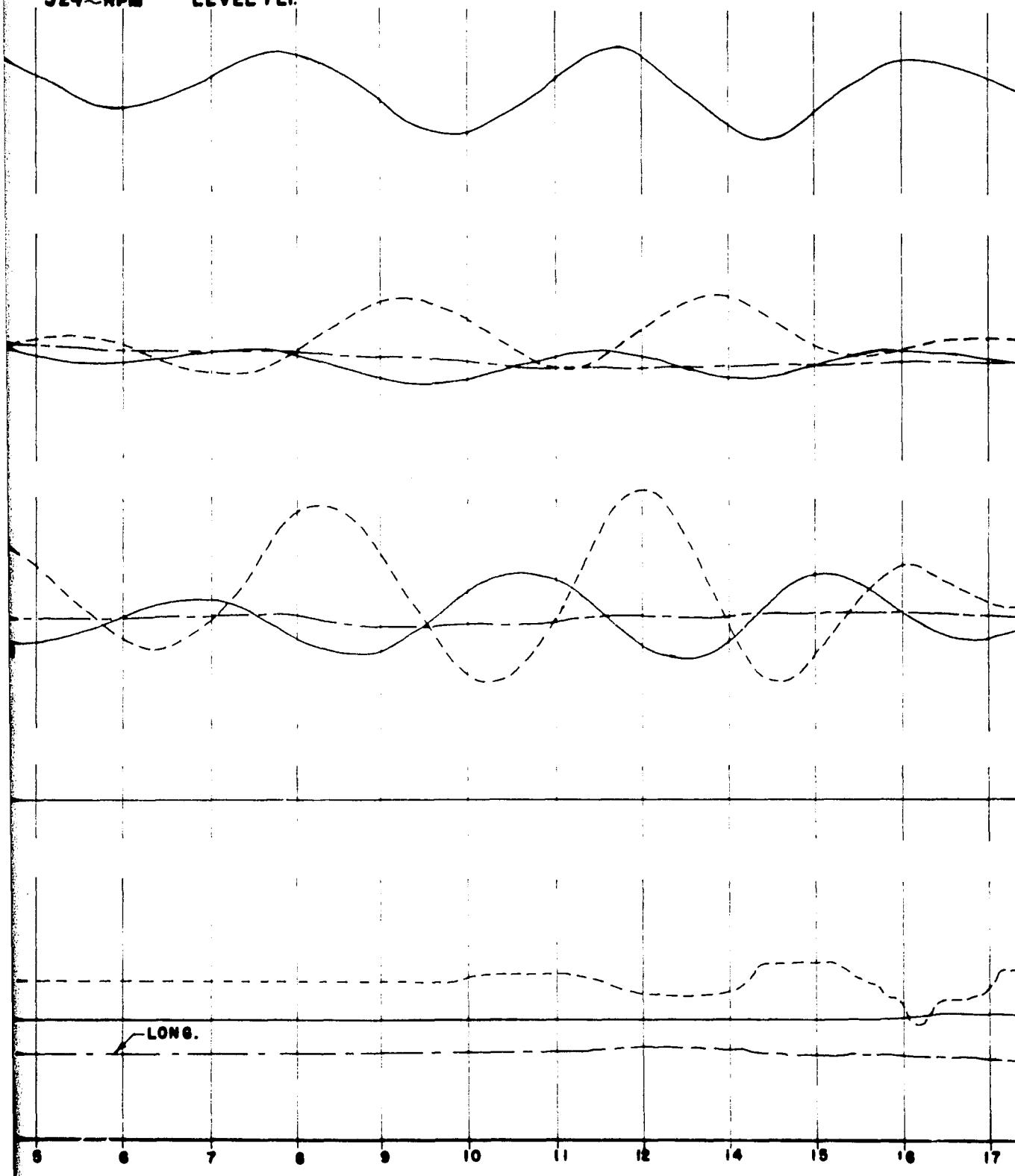


FIGURE NO. 155

LONGITUDINAL RESPONSE CHARACTERISTICS

AH-1G USA T-15695

TRIM AIRSPEED ~CAS	AVG. ALT. ~FT	AVG. GEAR ~IN.	AVG. LONG. ROTOR RPM	FLY. COMP. COMING THROTTLE CONST. ~%
111	3500	7800	201.0(FLT)	324.0 LEV. FLY.
116	4600	7760	201.0(FLT)	324.0 LEV. FLY.
119	5000	7400	200.8(FLT)	324.0 LEV. FLY.
152	4000	7800	200.4(FLT)	324.0 LEV. FLY.
172	3500	8040	200.4(FLT)	324.0 DIVE
108	4000	9350	200.1(FLT)	324.0 LEV. FLY.
133	5060	9180	200.2(FLT)	324.0 LEV. FLY.
108	4000	7670	191.8(FWD)	324.0 LEV. FLY.
139	3500	7470	191.0(GND)	324.0 LEV. FLY.
172	4000	7480	191.0(FWD)	324.0 DIVE

NOTE: OPEN SYMBOLS DENOTE SCAS ON
SOLID SYMBOLS DENOTE SCAS OFF

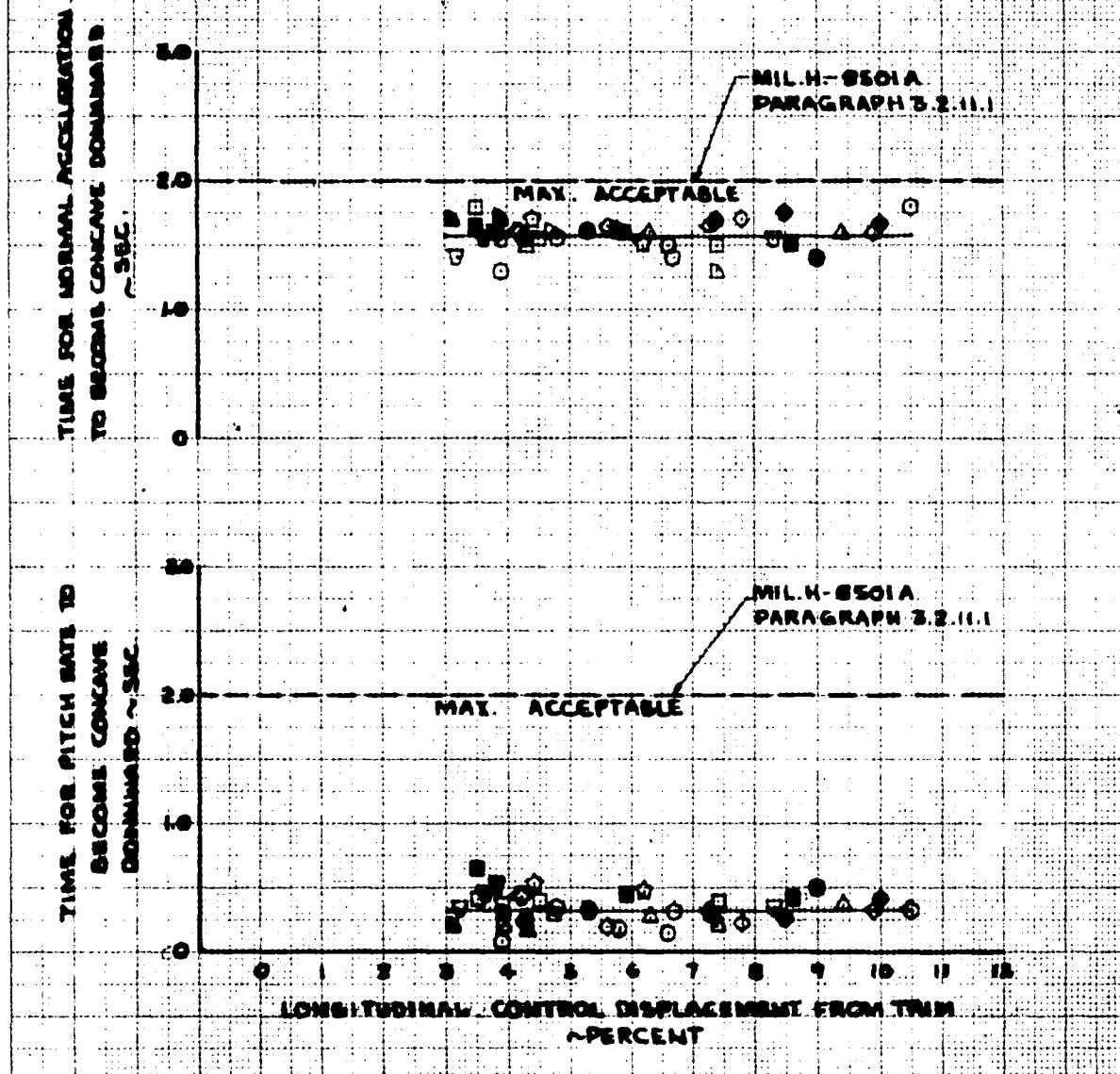
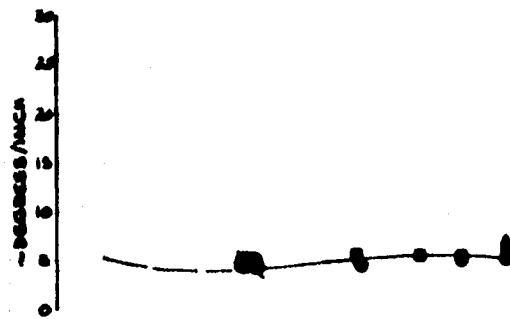


FIGURE No. 156
LONGITUDINAL CONTROLLABILITY SUMMARY
AH-1G USA #715695
GROSS WEIGHT COMPARISON

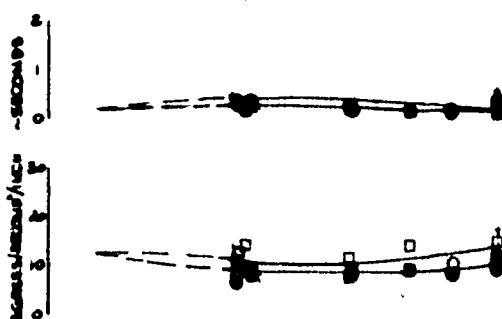
SYM AVG ALTITUDE AVG GROSS WEIGHT AVG LOAD. BEFORE COMING. THRUST GRPH. PODS LOADING
 $H_0 \sim 6T.$ ~ LB. C.G. ~1M. ~ RPM. ~ CT
 O 5060 7910 199.6 (AFT) 3260 HVY. HOG 0.004666 PODS EMPTY
 □ 3470 9490 200.0 (AFT) 3260 HVY. HOG 0.008560 PODS LOADED
 (1654 LB. TOTAL)

- NOTES: 1. OPEN SYMBOLS DENOTE FORWARD INPUT
 2. SOLID SYMBOLS DENOTE AFT INPUT
 3. PLAIN SYMBOLS DENOTE LEVEL FLIGHT
 4. FLAGGED SYMBOLS DENOTE CLIMB
 5. TAILED SYMBOLS DENOTE AUTOROTATION
 6. SYMBOLS WITH CROSSES DENOTE DIVE
 7. AUTO ROTATIONAL ROTOR SPEED RANGE ~300 → 330 RPM
 8. POINTS DERIVED FROM FIGURES 180 THROUGH 187, APPENDIX III

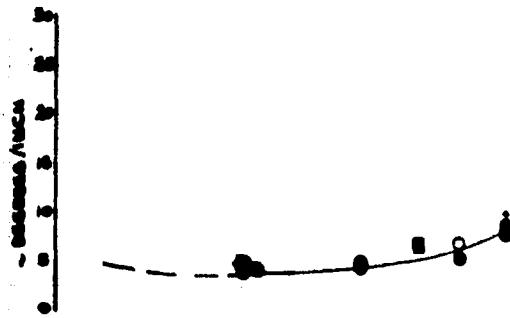
DISPLACEMENT AT ONE SECOND
 SCAS ON



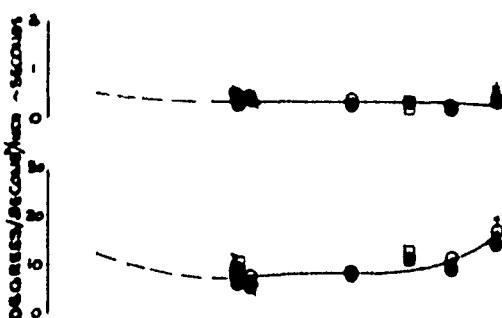
SENSITIVITY
 SCAS ON



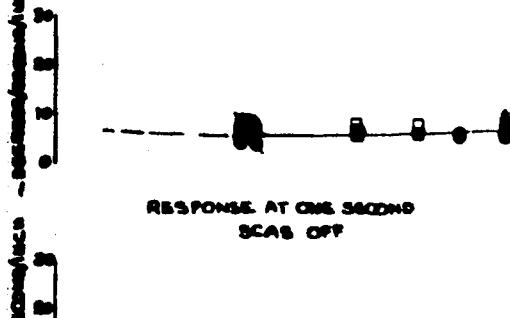
DISPLACEMENT AT ONE SECOND
 SCAS OFF



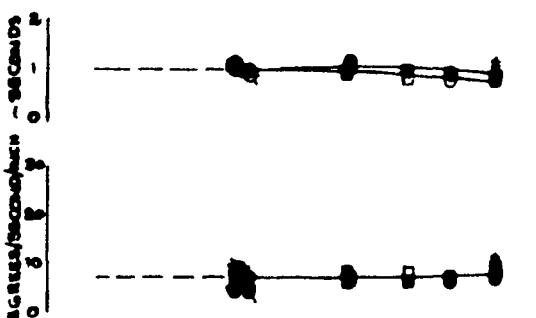
SENSITIVITY
 SCAS OFF



RESPONSE AT ONE SECOND
 SCAS ON



MAXIMUM RESPONSE
 SCAS ON



RESPONSE AT ONE SECOND
 SCAS OFF

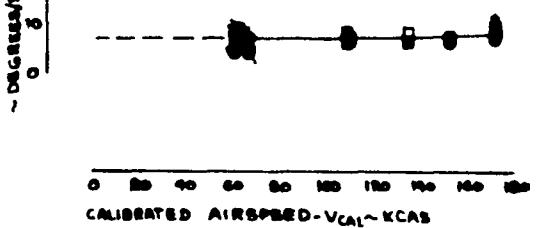
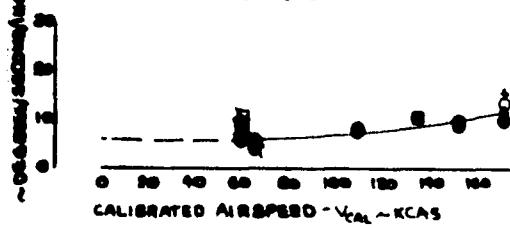


FIGURE NO 157
LONGITUDINAL CONTROLLABILITY SUMMARY
AH-1G USA #71565
CONFIGURATION COMPARISON

SYM AVG ALTITUDE AVG GROSS WEIGHT AVG LONG. ROTOR C.G. CONING. THRUST COEFF. PODS LOADING
 $H_0 \sim \text{FT}$ ~LBS C.G.~IN RPM ~C_T
 0 5060 7910 199.6(AFT) 8240 HVY. HOG 0.004566 PODS EMPTY
 0 5440 7780 201.2(AFT) 8260 CLEAN 0.004498 NO PODS

NOTES: 1. OPEN SYMBOLS DENOTE FORWARD INPUT
 2. SOLID SYMBOLS DENOTE AFT INPUT
 3. PLAIN SYMBOLS DENOTE LEVEL FLIGHT
 4. FLAGGED SYMBOLS DENOTE CLIMB
 5. TAILED SYMBOLS DENOTE AUTOROTATION
 6. SYMBOLS WITH CROSS DENOTE DIVE
 7. AUTOROTATIONAL ROTOR SPEED RANGE ~300-330 RPM
 8. POINTS DERIVED FROM FIGURES 172 THROUGH 176, AND 180
 THROUGH 185, APPENDIX VII

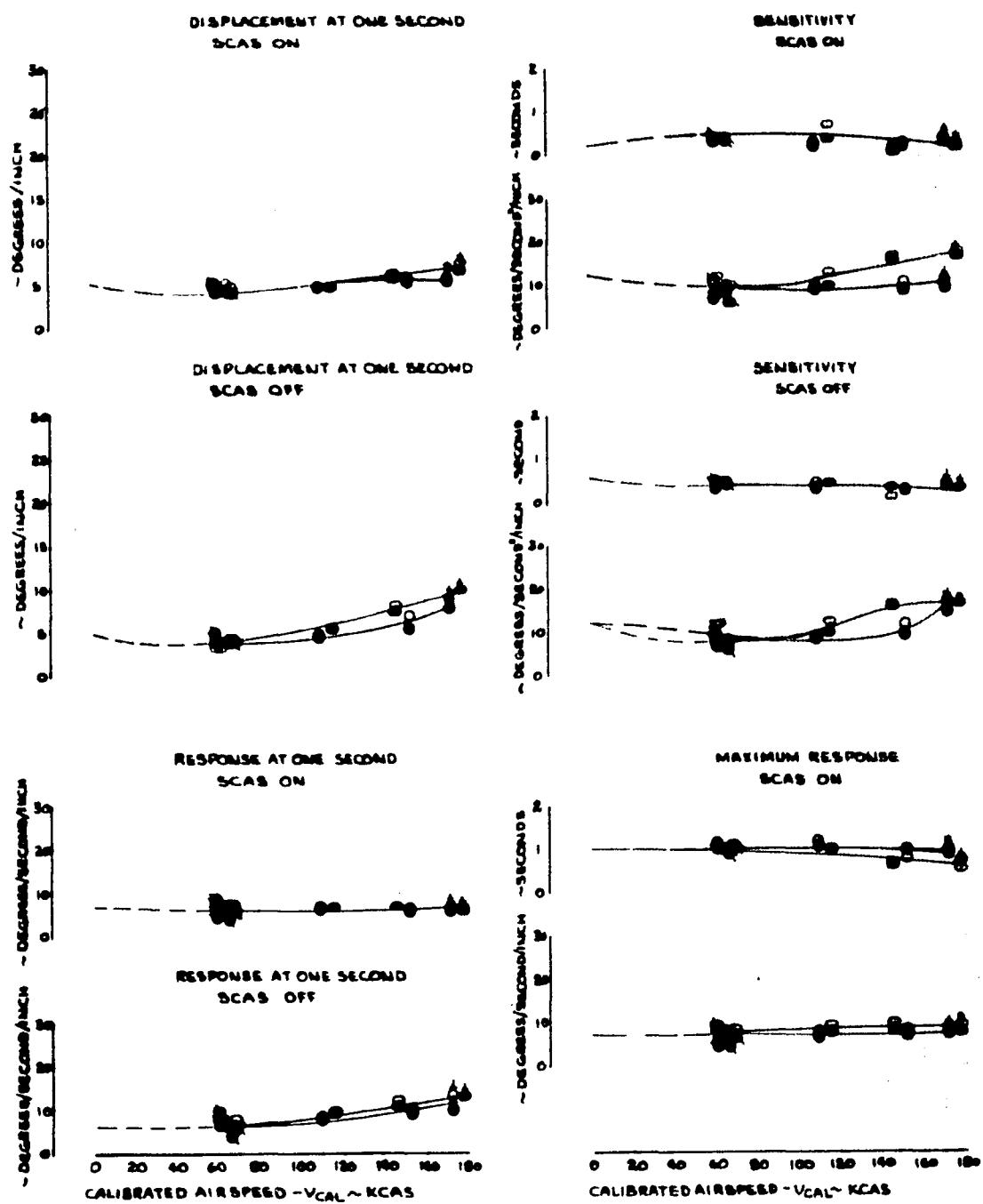


FIGURE No. 158
LONGITUDINAL CONTROLLABILITY SUMMARY
 AH-1G USA #715645
 CENTER OF GRAVITY COMPARISON

SYM	ANGLE ALTITUDE HGT - FT.	Avg. GROSS WEIGHT	Avg. LONG. MTR CONFIG.	THRUST COEFF.	PODS LOADING
O	6200	7610	190.8(FWD)	324.0 CLEAN	0.004548 NO PODS
●	6440	7780	201.2(AFT)	324.0 CLEAN	0.004543 NO PODS

NOTES: 1. OPEN SYMBOLS DENOTE FORWARD INPUT
 2. SOLID SYMBOLS DENOTE AFT INPUT
 3. PLAIN SYMBOLS DENOTE LEVEL FLIGHT
 4. FLAGGED SYMBOLS DENOTE CLIMB
 5. TAILED SYMBOLS DENOTE AUTOROTATION
 6. SYMBOLS WITH CROSS DENOTE DIVE
 7. AUTOROTATIONAL ROTOR SPEED RANGE ~300~330 RPM
 8. POINTS DERIVED FROM FIGURES 169 THROUGH 175, APPENDIX VII

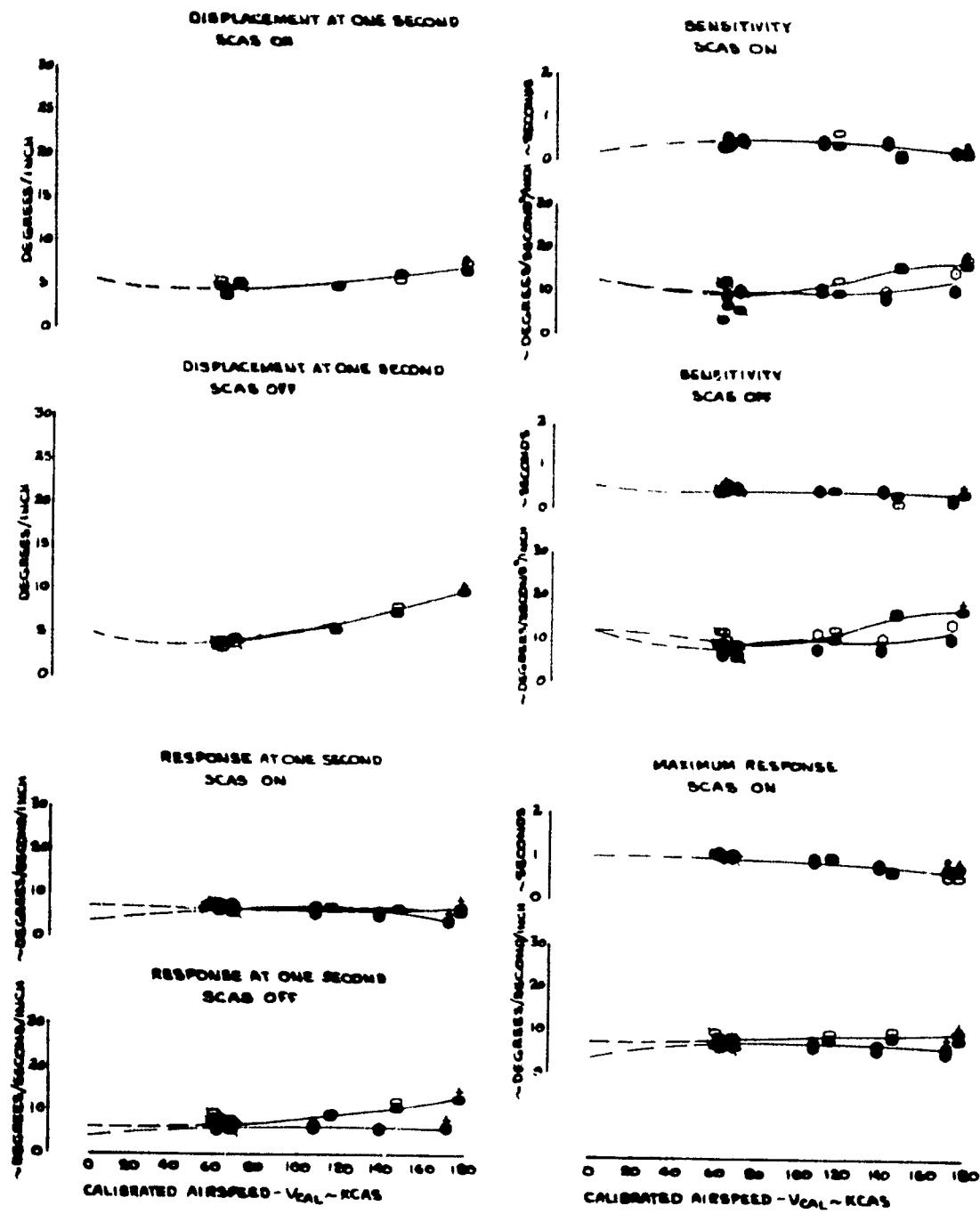


FIGURE NO. 159
LONGITUDINAL CONTROLLABILITY SUMMARY
 AH-1G USA #6718698
 ALTITUDE COMPARISON

SYM	Avg. Altitude Hg~FT	Avg. Gross Weight LBS	Avg. Long.C.G. IN	Rotor Config.	Thrust Coeff.	Ross Loading
O	5060	7910	199.6(AFT)	3240 HVY HOG	0.004556	PODS EMPTY
▲	15520	7840	200.9(AFT)	3240 HVY HOG	0.006896	PODS EMPTY

NOTES: 1. OPEN SYMBOLS DENOTE FORWARD INPUT
 2. SOLID SYMBOLS DENOTE AFT INPUT
 3. PLAIN SYMBOLS DENOTE LEVEL FLIGHT
 4. FLAGGED SYMBOLS DENOTE CLIMB
 5. TAILED SYMBOLS DENOTE AUTOROTATION
 6. SYMBOLS WITH CIRCLES DENOTE DIVE
 7. AUTOROTATIONAL ROTOR SPEED RANGE ~ 300 → 330 RPM
 8. POINTS DERIVED FROM FIGURES 180 THROUGH 185, AND 188
 THROUGH 191, APPENDIX VII

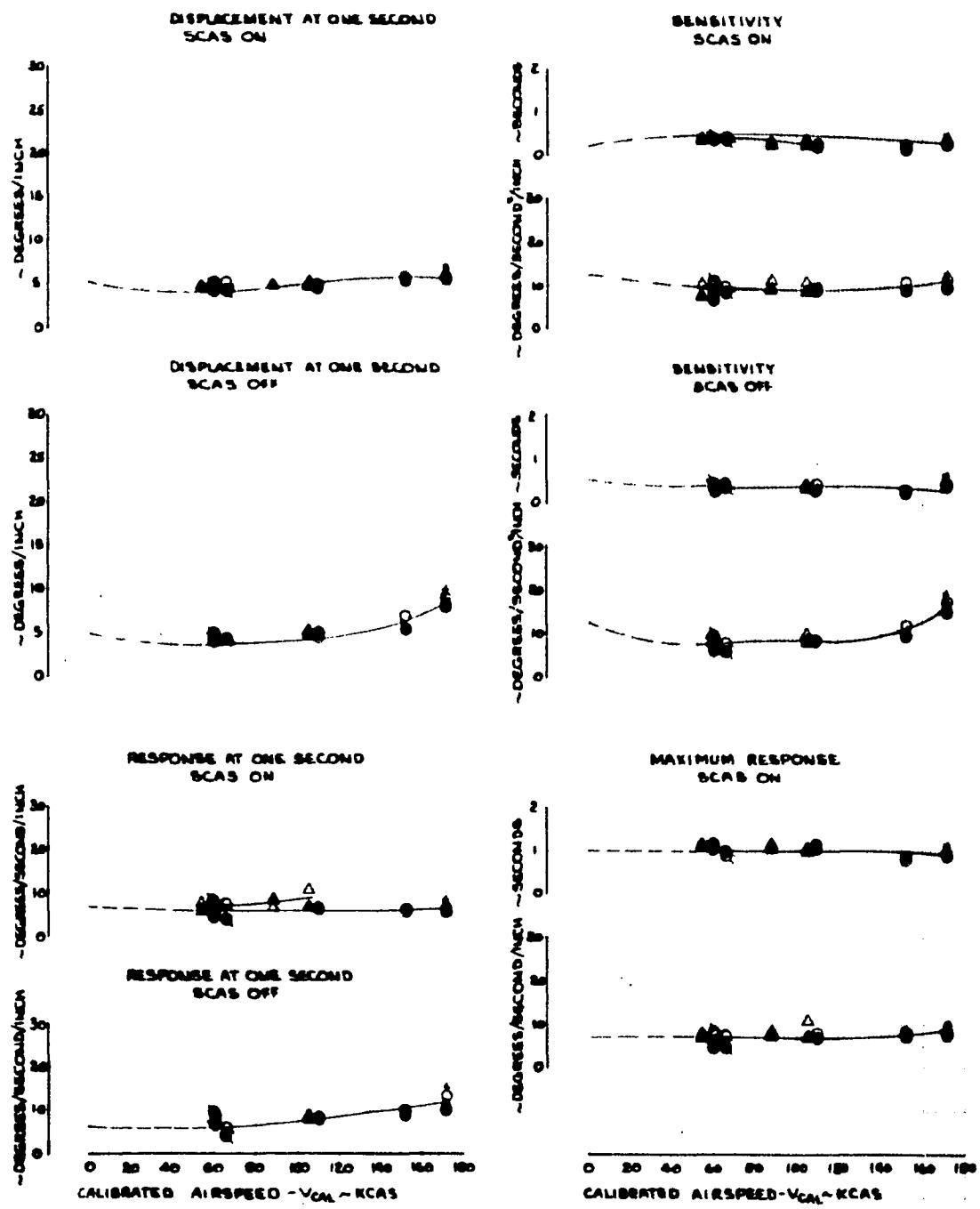


FIGURE NO. 160
LATERAL CONTROLLABILITY SUMMARY
 AH-1G USA #715698
 GROSS WEIGHT COMPARISON

SYM.	Avg. ALTITUDE H ₀ ~ FT.	Avg. GROSS WEIGHT ~ LBS.	Avg. LONG. C.G. ~ IN.	ROTOR CONFIG.	THRUST COEFF.	POD LOADS
O	5290	7800	200.2(FT)	324.0	HVV HOG	0.004534 PODS EMPTY
□	5270	9390	200.2(FT)	324.0	HVV HOG	0.005953 PODS LOADED

NOTES: 1. OPEN SYMBOLS DENOTE LEFT INPUT
 2. SOLID SYMBOLS DENOTE RIGHT INPUT
 3. PLAIN SYMBOLS DENOTE LEVEL FLIGHT
 4. FLAGGED SYMBOLS DENOTE CLIMB
 5. TAILED SYMBOLS DENOTE AUTOROTATION
 6. SYMBOLS WITH CROSS DENOTE DIVE
 7. AUTOROTATIONAL ROTOR SPEED RANGE ~ 300-360 RPM
 8. POINTS DERIVED FROM FIGURES 212 THROUGH 218, APPENDIX III

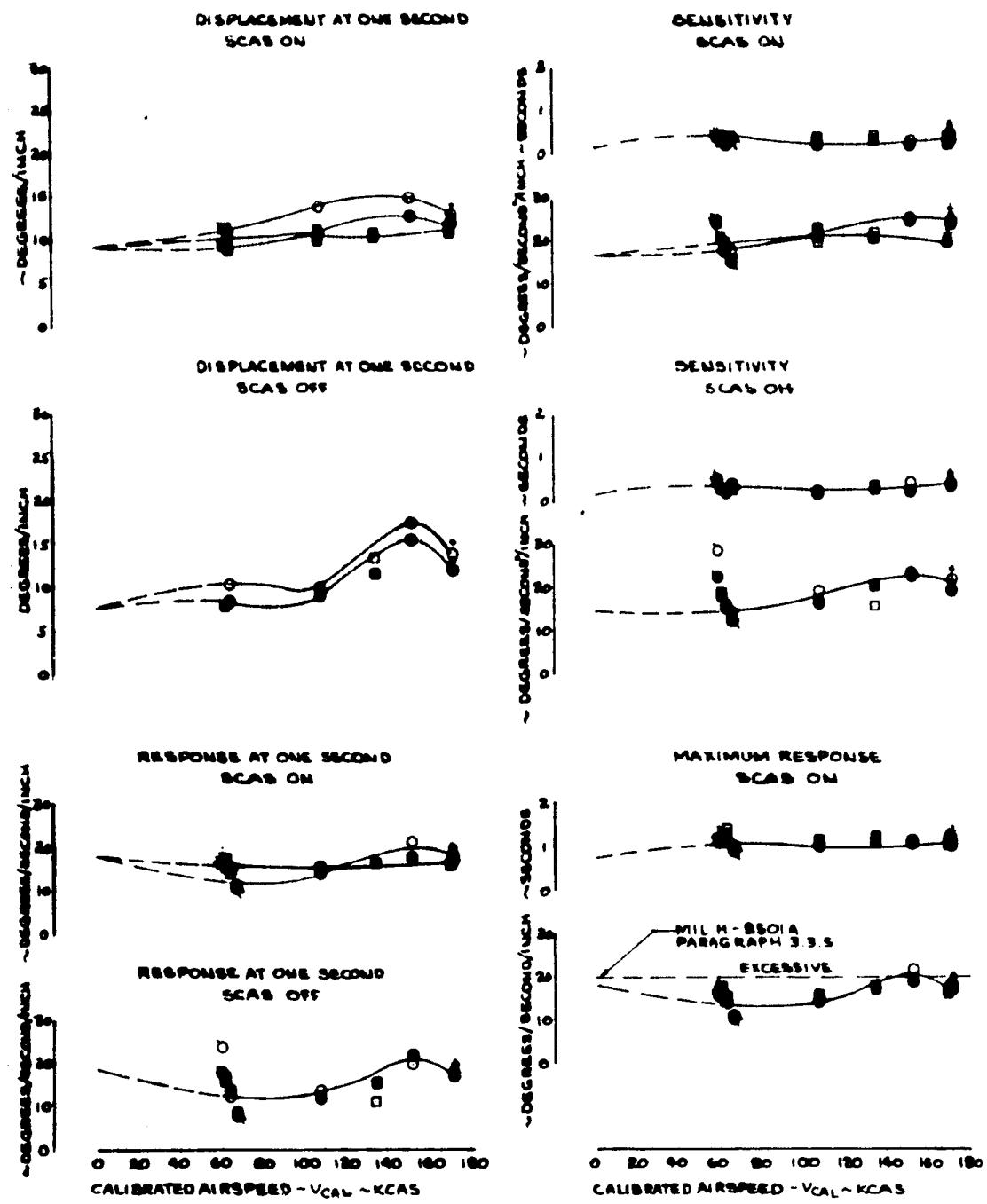


FIGURE NO. 161
LATERAL CONTROLLABILITY SUMMARY
AH-1G USAF 67-10645
POD LOADING COMPARISON

STAB ANG. ALTITUDE AVG. GROSS WEIGHT AND LOADS. ROTOR CONFIG. THRUST COEFF. POD LOADING
 $H_0 \sim 52$ ~15.0 C.G. ~14.5 RPM ~C_T
 □ 6030 6630 195.0 (MID) 324.0 HGT. HOG 0.0064461 POD LOADING
 ◆ 6150 6630 195.1 (MID) 325.0 HGT. HOG 0.0064461 PODS EMPTY

NOTES:
 1. OPEN SYMBOLS DENOTE LEFT INPUT
 2. SOLID SYMBOLS DENOTE RIGHT INPUT
 3. PLAIN SYMBOLS DENOTE LEVEL FLIGHT
 4. FLAGGED SYMBOLS DENOTE CLIMB
 5. TAILED SYMBOLS DENOTE AUTOROTATION
 6. SYMBOLS WITH CROSS DENOTE DIVE
 7. AUTOROTATIONAL ROTOR SPEED RANGE ~4000~8800 RPM
 8. POINTS DERIVED FROM FIGURES 209 THROUGH 211, APPENDIX III

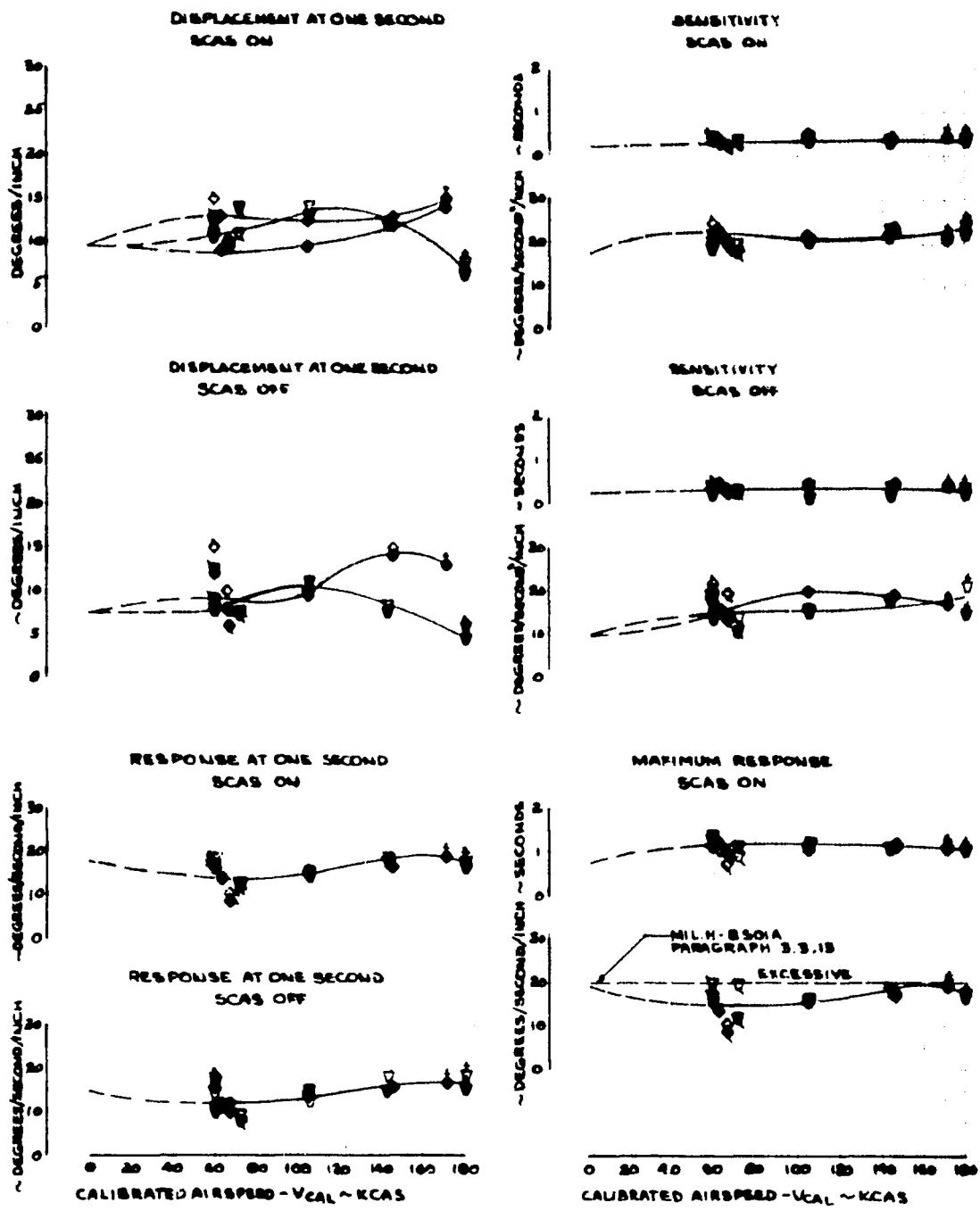
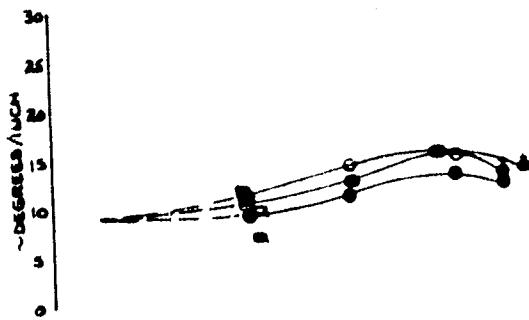


FIGURE NO 162
LATERAL CONTROLLABILITY SUMMARY
 AH-1G USAF TIGERS
 CONFIGURATION COMPARISON

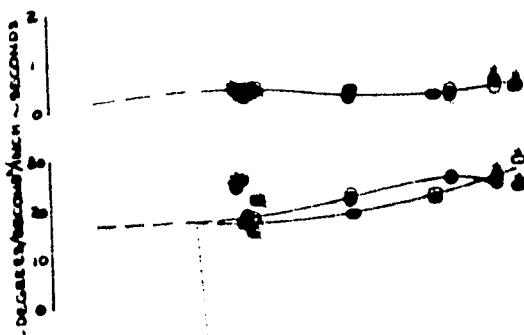
SYM. AVG. ALTITUDE AVG. GROSS WEIGHT AVG. LWT. MOTOR CONFIG THRUST COEFF. PODS LOADING
 H_g ~ FT. ~ LB. CG. ~ IN. RPM C_T Hvy Nog 0.004554 Pods Empty
 0 5290 7800 200.2(AFT) 3240 Hvy Nog 0.004554 Pods Empty
 0 4270 7590 201.2(AFT) 3290 Clean 0.004281 No Pods

NOTES: 1. OPEN SYMBOLS DENOTE LEFT INPUT
 2. SOLID SYMBOLS DENOTE RIGHT INPUT
 3. PLAIN SYMBOLS DENOTE LEVEL FLIGHT
 4. FLAGGED SYMBOLS DENOTE CLIMB
 5. TAILED SYMBOLS DENOTE AUTOROTATION
 6. SYMBOLS WITH CROSS DENOTE DIVE
 7. AUTOROTATIONAL ROTOR SPEED RANGE ~ 300 - 380 RPM
 8. POINTS DERIVED FROM FIGURES 192 THROUGH 193 AND
 216 THROUGH 218, APPENDIX III

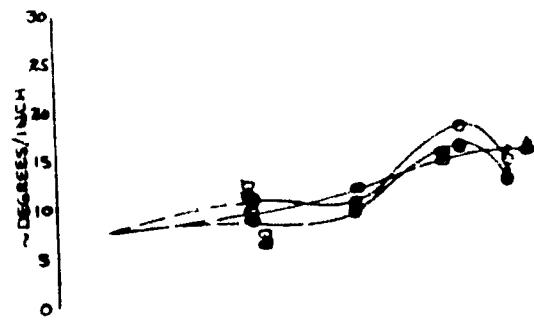
DISPLACEMENT AT ONE SECOND
 SCAS ON



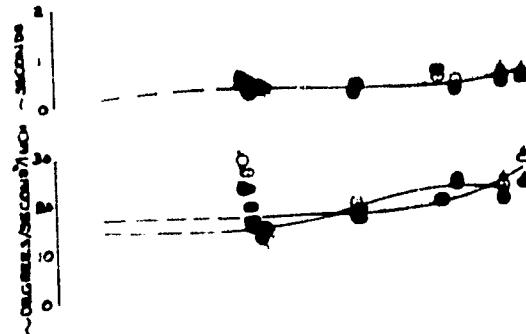
SENSITIVITY
 SCAS ON



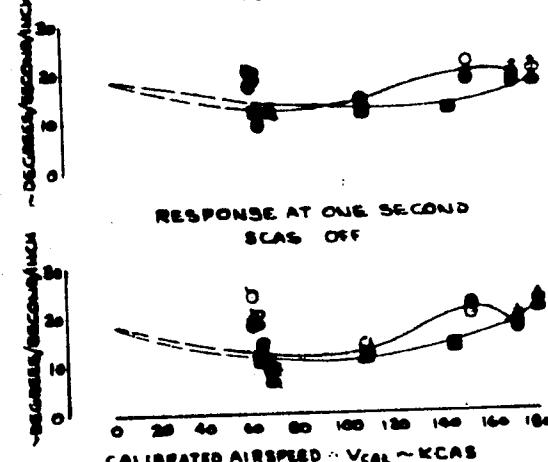
DISPLACEMENT AT ONE SECOND
 SCAS OFF



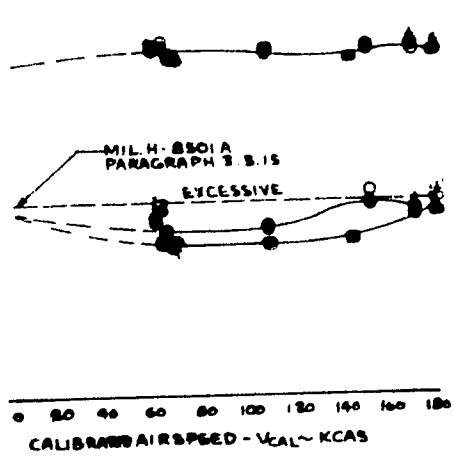
SENSITIVITY
 SCAS OFF



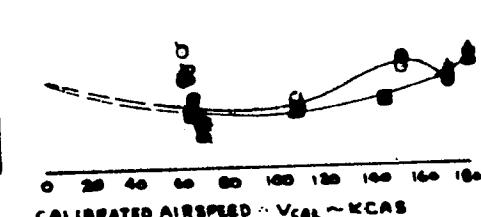
RESPONSE AT ONE SECOND
 SCAS ON



MAXIMUM RESPONSE
 SCAS ON



RESPONSE AT ONE SECOND
 SCAS OFF



0 20 40 60 80 100 120 140 160 180
 CALIBRATED AIRSPEED - VCAL - KCAS

FIGURE NO. 163
LATERAL CONTROLLABILITY SUMMARY
AH-1G USA #715695
ALTITUDE COMPARISON

SYM	Avg. ALTITUDE H _d ~ FT.	Avg. GROSS WEIGHT ~ LB.	Avg. LONG. C.G. ~ IN.	MOTOR CONFIG.	THRUST COEFF. PODS	LOADING
O	5290	7800	200.2	3240 HVY. HOG	0.004534	PODS EMPTY
△	16150	7780	200.9	3240 HVY. HOG	0.006836	PODS EMPTY

- NOTES: 1. OPEN SYMBOLS DENOTE LEFT INPUT
 2. SOLID SYMBOLS DENOTE RIGHT INPUT
 3. PLAIN SYMBOLS DENOTE LEVEL FLIGHT
 4. FLAGGED SYMBOLS DENOTE CLIMB
 5. TAILED SYMBOLS DENOTE AUTOROTATION
 6. SYMBOLS WITH CROSS DENOTE DIVE
 7. AUTOROTATION ROTOR SPEED RANGE ~ 300 - 330 RPM
 8. POINTS DERIVED FROM FIGURES 216 THROUGH 222, APPENDIX III

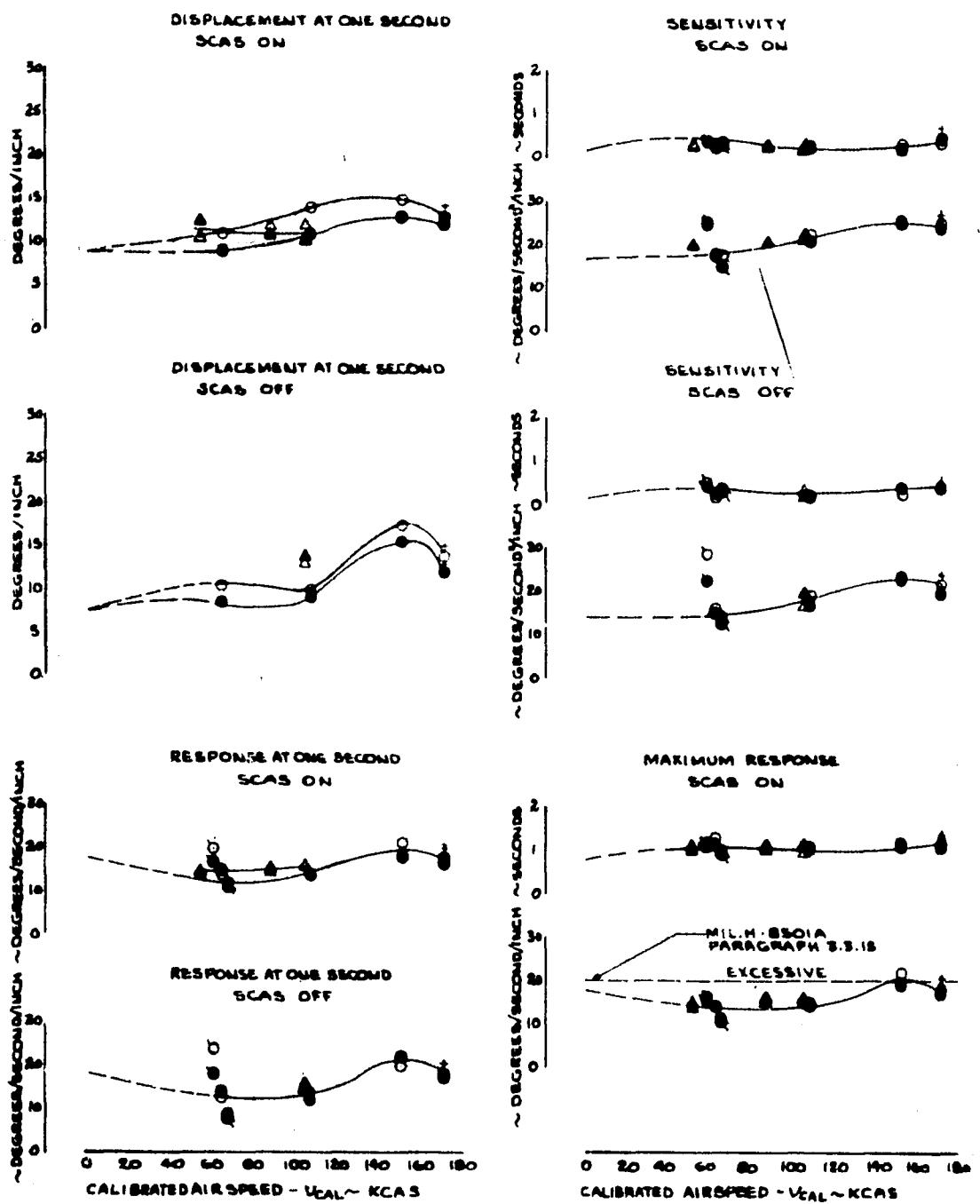


FIGURE NO 164
LATERAL CONTROLLABILITY SUMMARY
 AH-1G

SYN. AVG. ALT. AVG.G.W. AVG.LONG. ROTOR THRUST COEFF CONFIGURATION S/N
 H₀-FT. ~LB. C.G. -IN. BHP ~C_T
 0 4270 7590 201.2(FT) 324.0 0.004278 CLEAN 715695
 0 4070 7840 199.5(FT) 323.0 0.004188 CLEAN(LANDING GEAR DOWN)
 CROSS TUBE FAIRINGS REMOVED

NOTES: OPEN SYMBOLS DENOTE LEFT INPUT
 2 SOLID SYMBOLS DENOTE RIGHT INPUT
 3 PLAIN SYMBOLS DENOTE LEVEL FLIGHT
 4 FLAGGED SYMBOLS DENOTE CLIMB
 5 TAILED SYMBOLS DENOTE AUTOROTATION
 6 SYMBOLS WITH CROSS DENOTE DIVE
 7 AUTOROTATIONAL ROTOR SPEED RANGE ~ 300-330RPM
 8 POINTS DERIVED FROM FIGURES 192 THROUGH 199, APPENDIX III

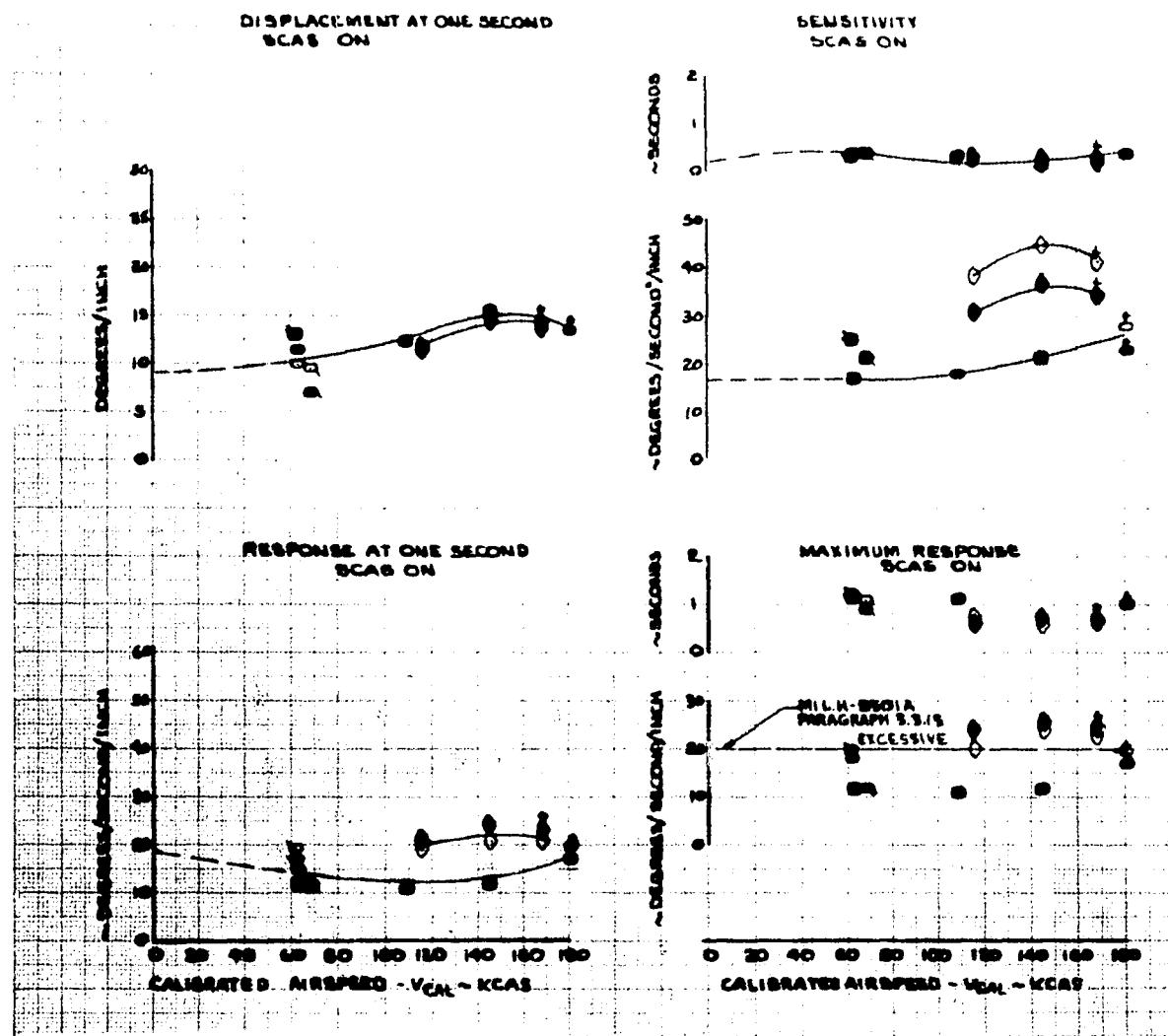


FIGURE NO. 165
DIRECTIONAL CONTROLLABILITY SUMMARY
AH-1G USA #71563
GROSS WEIGHT COMPARISON

SFM AVG ALTITUDE AVG GROSS WEIGHT AVG LONG. ROTOR CONFIG. THRUST COEF. PODS
 Hg ~FE C.G. ~IL RPM ~CT LOADING
 0 4650 7640 300.5(AFT) 3240(HVY. HOG 0.004556 PODS EMPTY
 0 6060 9280 300.5(AFT) 3240(HVY. HOG 0.005522 PODS LOADED
 (1634-LB TOTAL)

- NOTES: 1. OPEN SYMBOLS DENOTE LEFT INPUT
 2. SOLID SYMBOLS DENOTE RIGHT INPUT
 3. PLAIN SYMBOLS DENOTE LEVEL FLIGHT
 4. FLAGGED SYMBOLS DENOTE CLIMB
 5. TAILED SYMBOLS DENOTE AUTOROTATION
 6. SYMBOLS WITH CROSS DENOTE DIVE
 7. AUTOROTATIONAL ROTOR SPEED RANGE ~ 300 - 330 RPM
 8. POINTS DERIVED FROM FIGURES 281 THROUGH 288, APPENDIX III

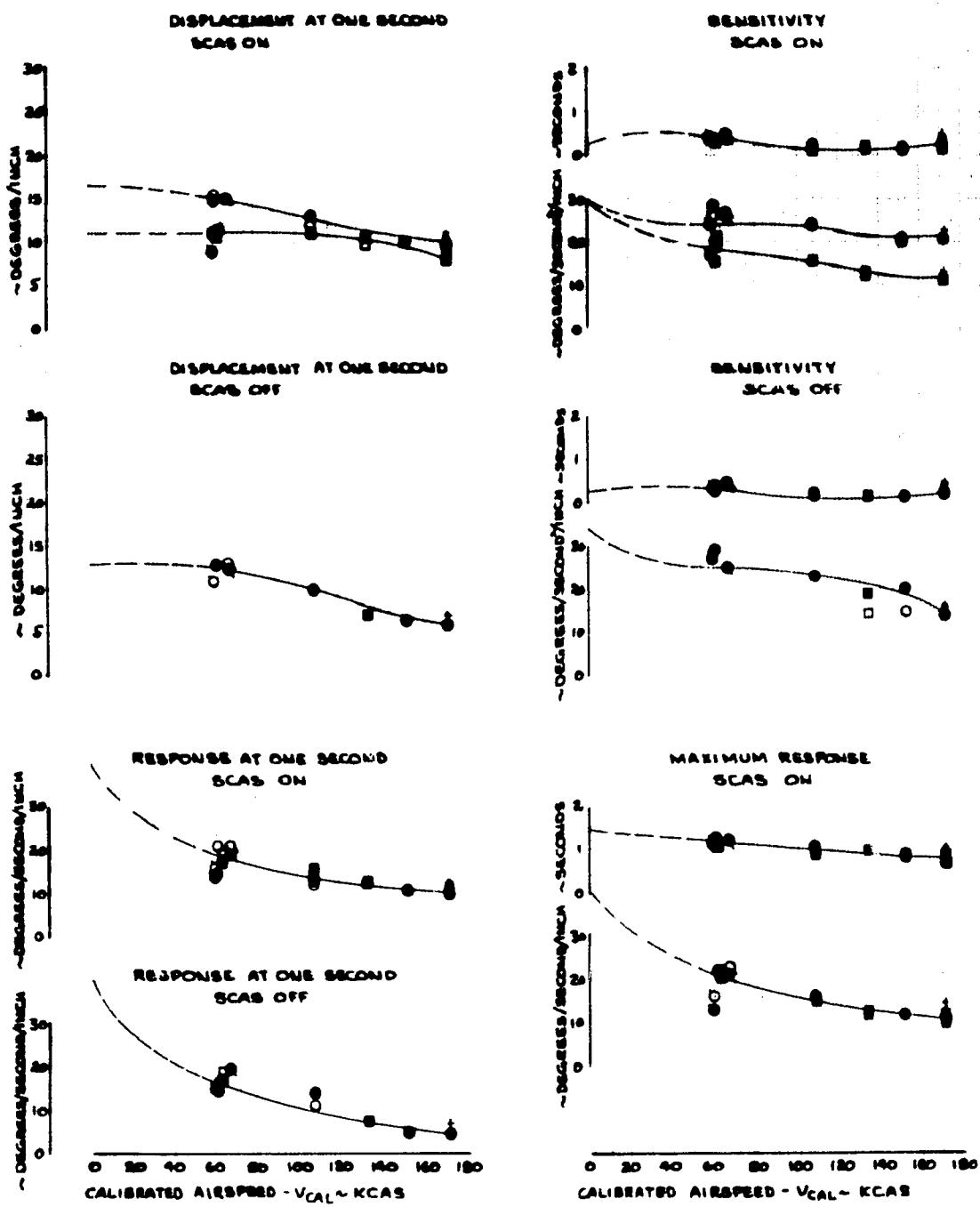
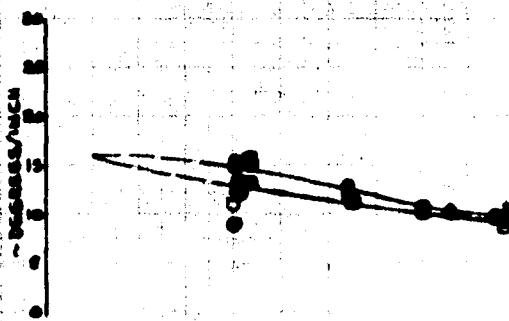


FIGURE NO. 166
DIRECTIONAL CONTROLLABILITY SUMMARY
AH-1S USA 46715005
CONFIGURATION GENERATION

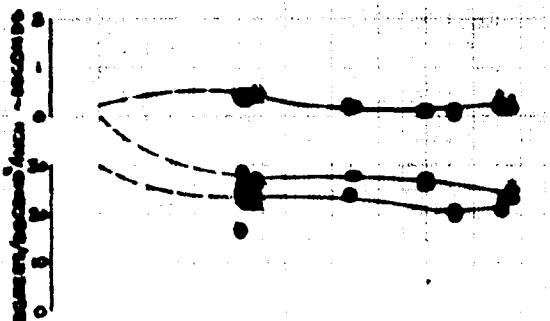
GVM AND ALTITUDE AND GROSS WEIGHT AND LOAD SCHEDULE COMING THRU THE CHT. POSE LOADING
 NO. ~FT. ~LB. C.G. -IN. GVM
 O 0650 7650 200.5(FT) 3300 MTW 0004529 POSE EMPTY
 O 0900 1450 201.5(FT) 3300 CLEAN 0004530 TWO POSE

- 1. OPEN SYMBOLS DENOTE LEFT INPUT
- 2. SOLID SYMBOLS DENOTE RIGHT INPUT
- 3. PLAIN SYMBOLS DENOTE LEVEL FLIGHT
- 4. FLAGGED SYMBOLS DENOTE CLIMB
- 5. TAILED SYMBOLS DENOTE DESCENT
- 6. SYMBOLS WITH CROSSES DENOTE DIVE
- 7. ANGULAR VELOCITY RANGE ~300°/SEC/SEC
- 8. POINTS DERIVED FROM FIGURES 222 THROUGH 225, AND
 233 THROUGH 235, APPENDIX XII

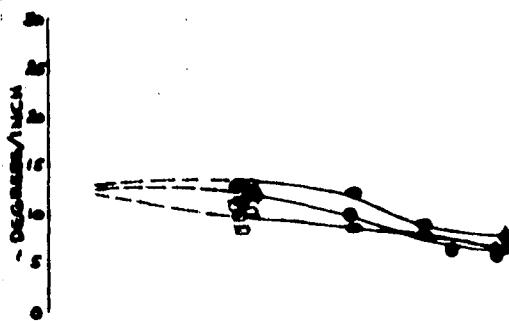
DISPLACEMENT AT ONE SECOND
SCAS ON



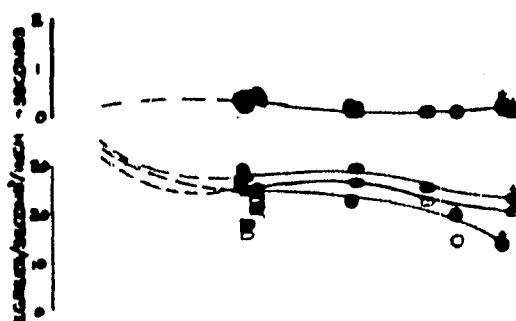
Sensitivity
SCAS ON



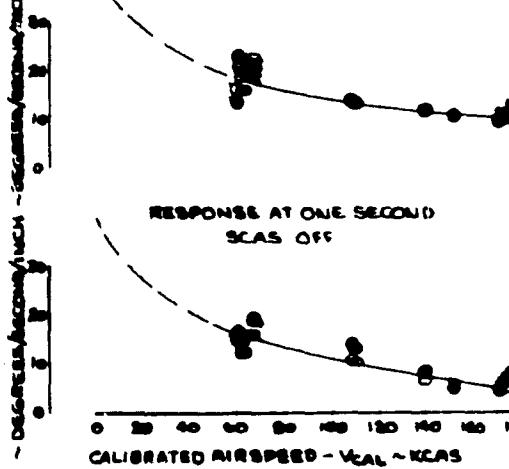
DISPLACEMENT AT ONE SECOND
SCAS OFF



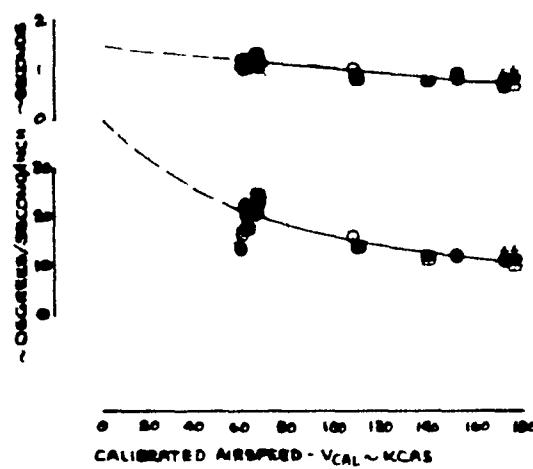
Sensitivity
SCAS OFF



RESPONSE AT ONE SECOND
SCAS ON



MAXIMUM RESPONSE
SCAS ON



RESPONSE AT ONE SECOND

SCAS OFF



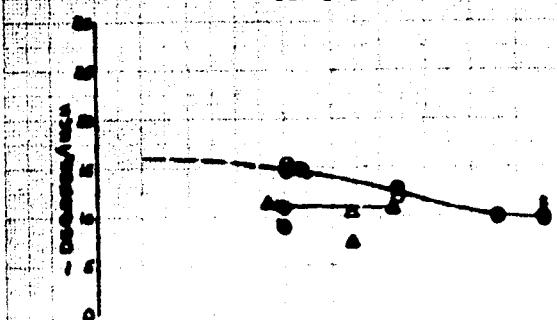
CALIBRATED AIRSPEED - VCAL ~ KCAS

Figure No. 167
Directional Coupling Summary
 AM-1A USAF 61-8674
 ALTITUDE COMPARISON

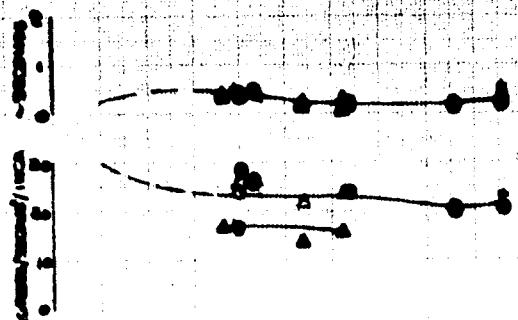
SUM AND ALTITUDE AND CROSS WIND AND LOADS CENTER TRAILER CARGO - 1000
 LD - 50
 O - 6650 7640 8000 8300 8600 9000 9300 9600 10000 10300 10600 11000 11300 11600 12000
 △ - 10650 10400 10000 9600 9200 8800 8400 8000 7600 7200 6800 6400 6000 5600 5200

NOTES: 1. OPEN SYMBOLS DENOTE LEFT INPUT
 2. SOLID SYMBOLS DENOTE RIGHT INPUT
 3. PLAIN SYMBOLS DENOTE LEVEL FLIGHT
 4. FLAMED SYMBOLS DENOTE CLIMB
 5. TAILED SYMBOLS DENOTE DESCENT
 6. SYMBOLS WITH CROSS DENOTE DIVE
 7. INTERSTATIONAL SYMBOL DENOTE CROSSWIND
 8. POINTS DERIVED FROM FIGURES 201 THROUGH 209, AND
 213 THROUGH 220, APPENDIX I

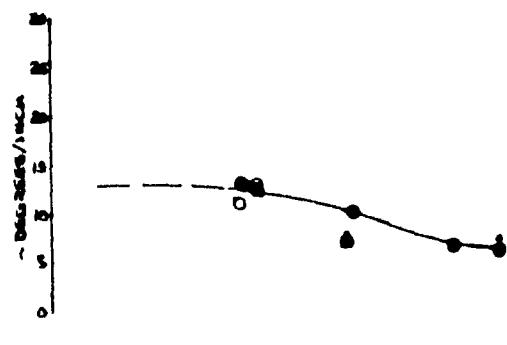
DISPLACEMENT AT ONE SECOND
 SCAS ON



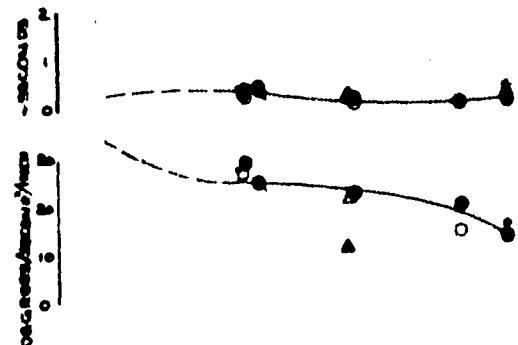
Sensitivity
 SCAS ON



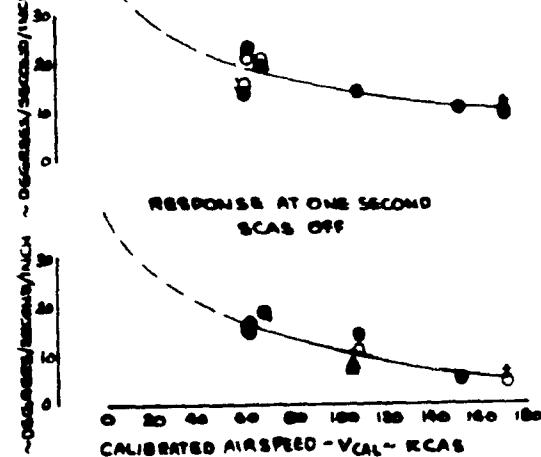
DISPLACEMENT AT ONE SECOND
 SCAS OFF



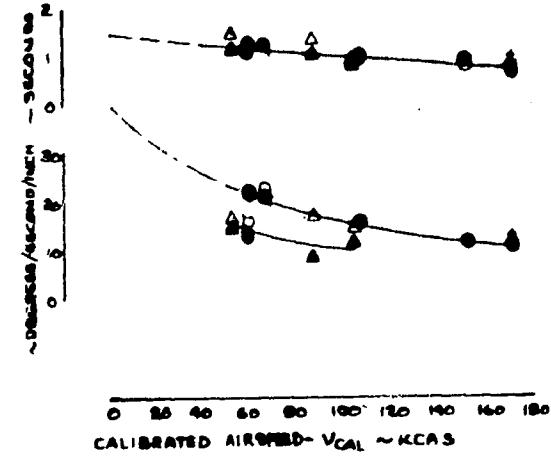
Sensitivity
 SCAS OFF



RESPONSE AT ONE SECOND
 SCAS ON



MAXIMUM RESPONSE
 SCAS ON



0 20 40 60 80 100 120 140 160 180
 CALIBRATED AIRSPEED - V_{CAL} - KCAS

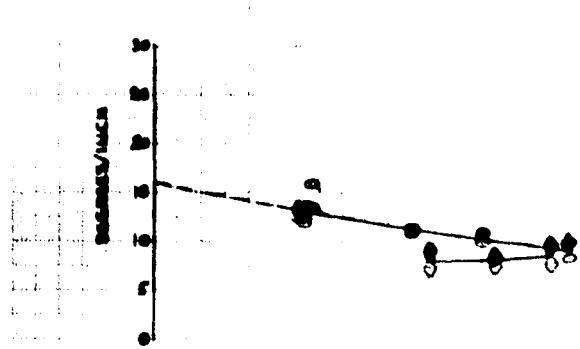
0 20 40 60 80 100 120 140 160 180
 CALIBRATED AIRSPEED - V_{CAL} - KCAS

FIGURE No. 168
DIRECTIONAL CONTROLLABILITY SUMMARY
AN-10 FUSA STAB

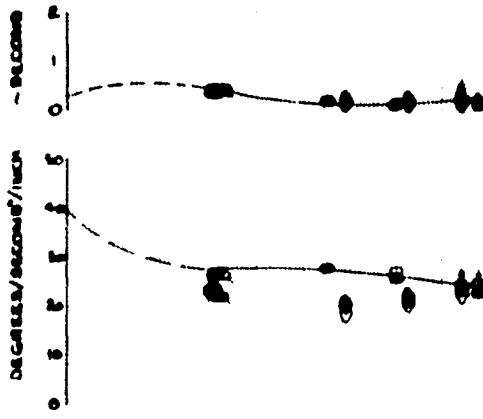
SYM AVE ALT ANG. & AVG. L. & R. MOTORS. THUST COEF. CONFIGURATION SW
 HGT - FE. ~10 CG - IN. 8000 ~CT
 0 5000 10000 20000(0) 30000 40000 50000 60000 70000 80000 90000 100000 110000 120000 130000 140000 150000
 0 4000 8000 12000 16000 20000 24000 28000 32000 36000 40000 44000 48000 52000 56000 60000 64000
 CLEAN, 10° THICK
 CLEAN (WING SAW 61504)
 CANTERBERY MIRRORS
 REMOVED)

NOTE: OPEN SYMBOL DENOTES LEFT INPUT
 SOLID SYMBOL DENOTES RIGHT INPUT
 PLAIN SYMBOLS DENOTE LEVEL FLIGHT
 FLAGGED SYMBOLS DENOTE CLIMB
 TAILED SYMBOLS DENOTE AUTOROTATION
 SYMBOLS WITH CROSS DENOTE DIVE
 1. AUTOROTATIONAL TORQUE SPEED RANGE ~ 20000-30000 RPM
 2. OUTLTS DERIVED FROM FIGURES 222 THROUGH 229, APPENDIX III

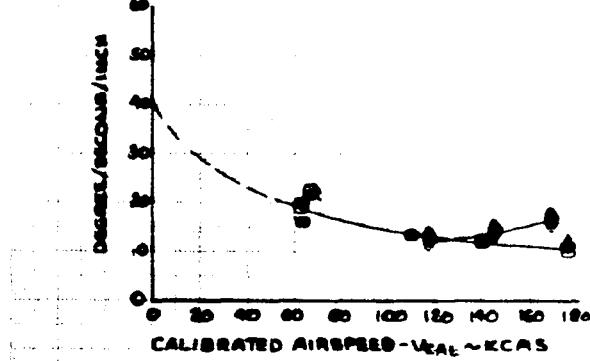
DISPLACEMENT AT ONE SECOND
 SCAS ON



SENSITIVITY
 SCAS ON



RESPONSE AT ONE SECOND
 SCAS ON



MAXIMUM RESPONSE
 SCAS ON

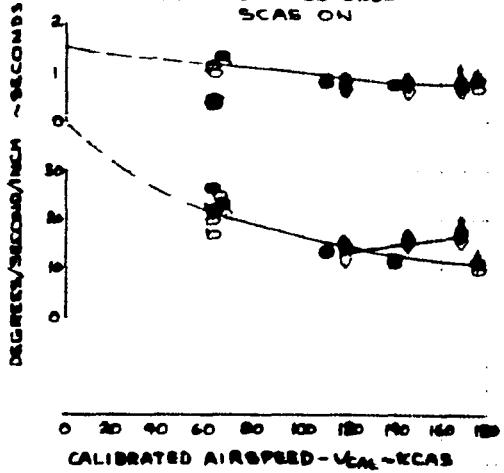
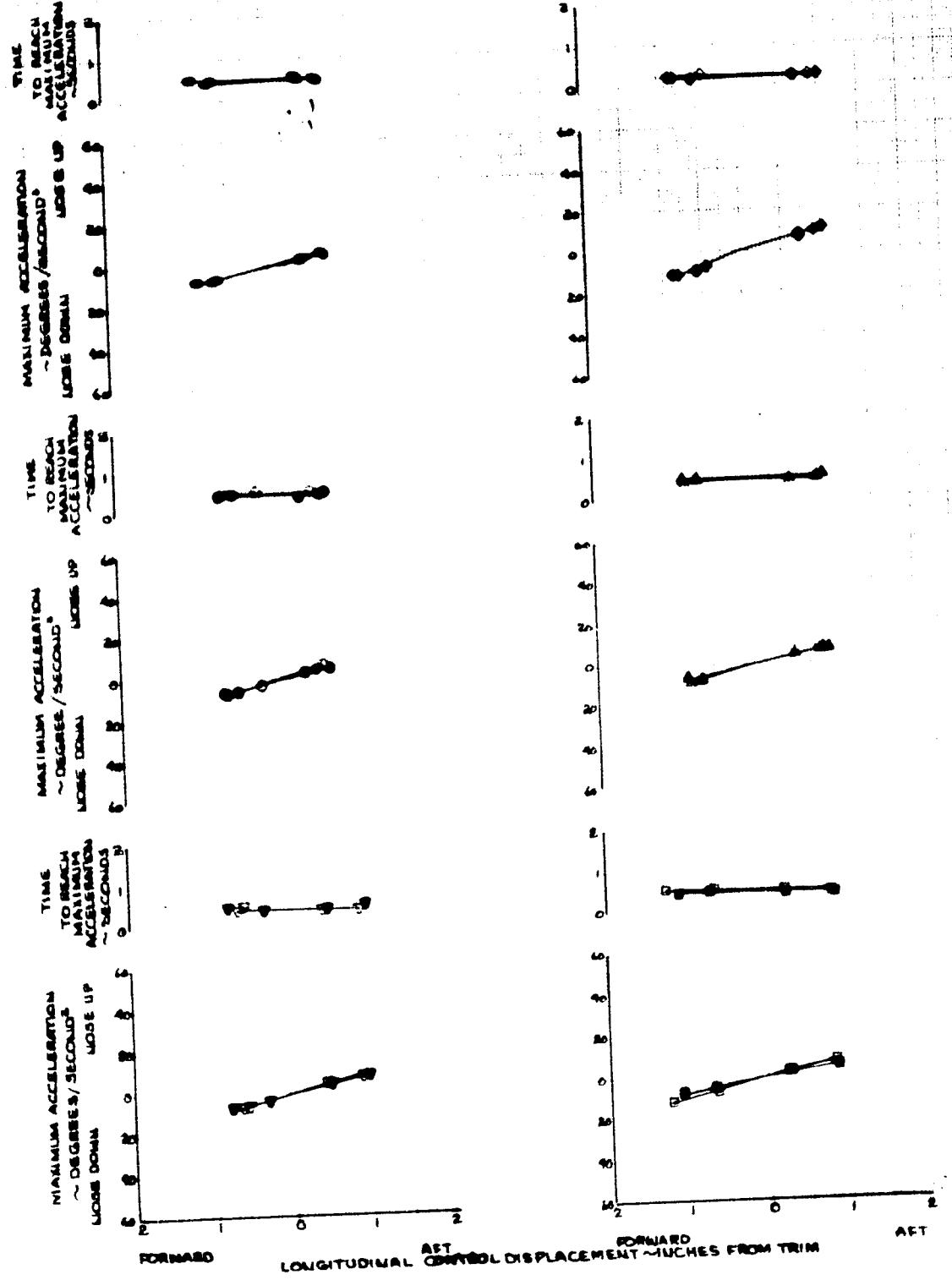


FIGURE NO. 169
LONGITUDINAL CONTROL SENSITIVITY
 AN-10 USAF/TIS/SES
 CLEAN CONFIGURATION

SYN	AIRSPD CAS	Avg. Alt. ft.	Avg. Gmt	Avg. Long. C.G. ~1M	RIDGE FLIGHT CONDITION THRUST COEF. ~ FT
X100	62.0	3800	1960	196.0 (PER)	325.0
	108.0	6660	7120	198.8 (PER)	326.0
	132.0	7120	7430	198.8 (PER)	327.0
	172.0	6600	6930	198.8 (PER)	327.0
	62.5	5920	7200	198.0 (PER)	DIVE 0.004827
	62.5	7210	7200	198.0 (PER)	CLIMB 0.004725
					AUTOROTATION 0.004771

NOTE: OPEN SYMBOLS DENOTE SCAS ON
 SOLID SYMBOLS DENOTE SCAS OFF



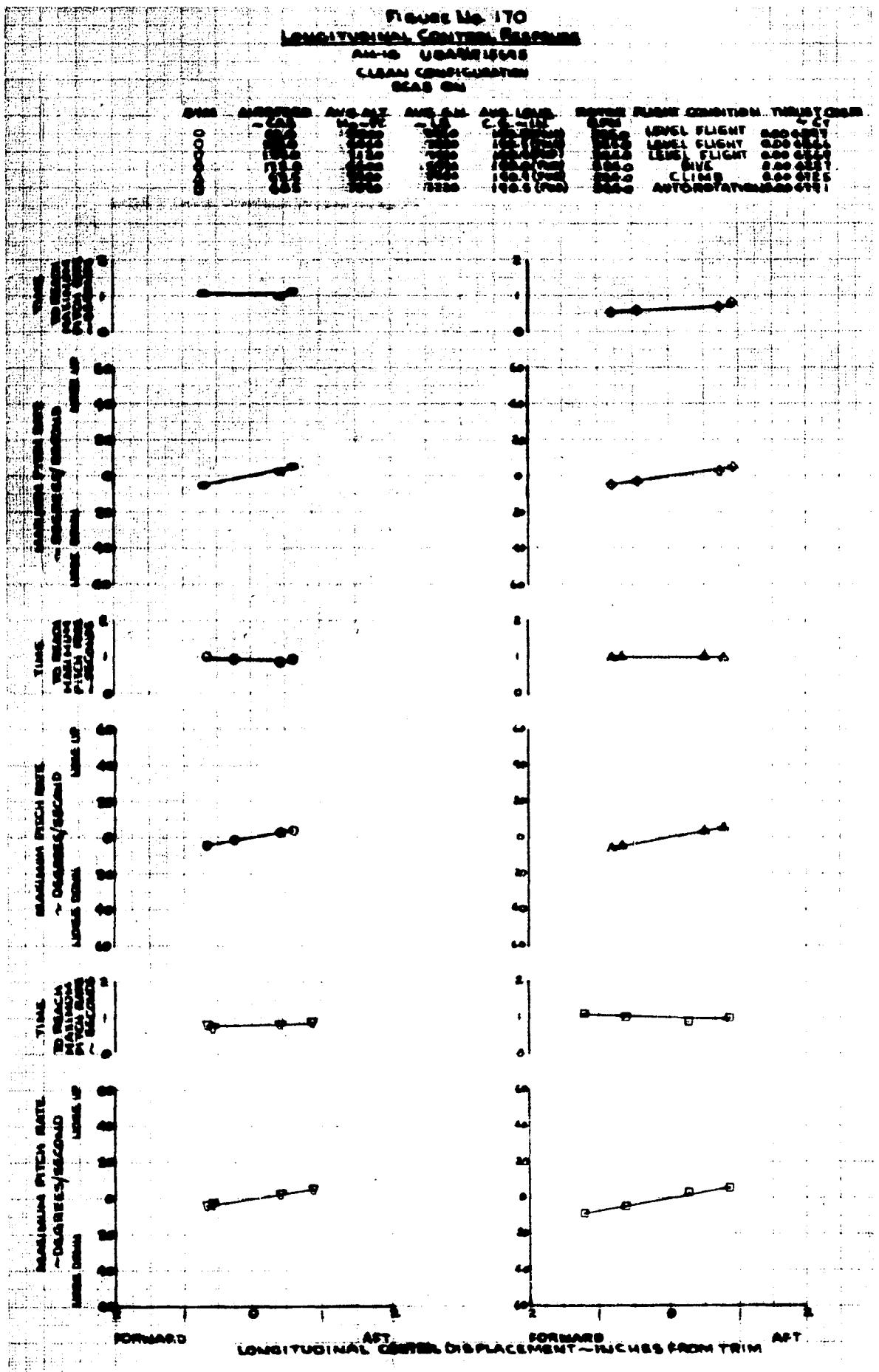


FIGURE NO. 171
LONGITUDINAL RESPONSE AT ONE SECOND
AH-1G USA #715693
CLEAN CONFIGURATION

SYM	AIR SPEED ~CAS	Avg. Alt. MS ~FT	Avg. Gmt. ~LB.	Avg. Long. CG ~IN.	MOTOR SPEEDS RPM	FLYING COND.
O	62.0	7800	7360	100.0 (FWD)	5200	LEVEL FLIGHT
O	102.0	2600	3380	100.0 (AFT)	5100	LEVEL FLIGHT
O	151.0	7120	1430	100.0 (AFT)	5200	LEVEL FLIGHT
O	172.0	6600	6400	100.0 (AFT)	5300	DIVE
O	62.5	5930	1900	100.0 (AFT)	5200	CLIMB
O	68.5	7290	7730	100.0 (AFT)	5200	AUTOROTATION

NOTE: OPEN SYMBOLS DENOTE SCAS ON
SOLID SYMBOLS DENOTE SCAS OFF

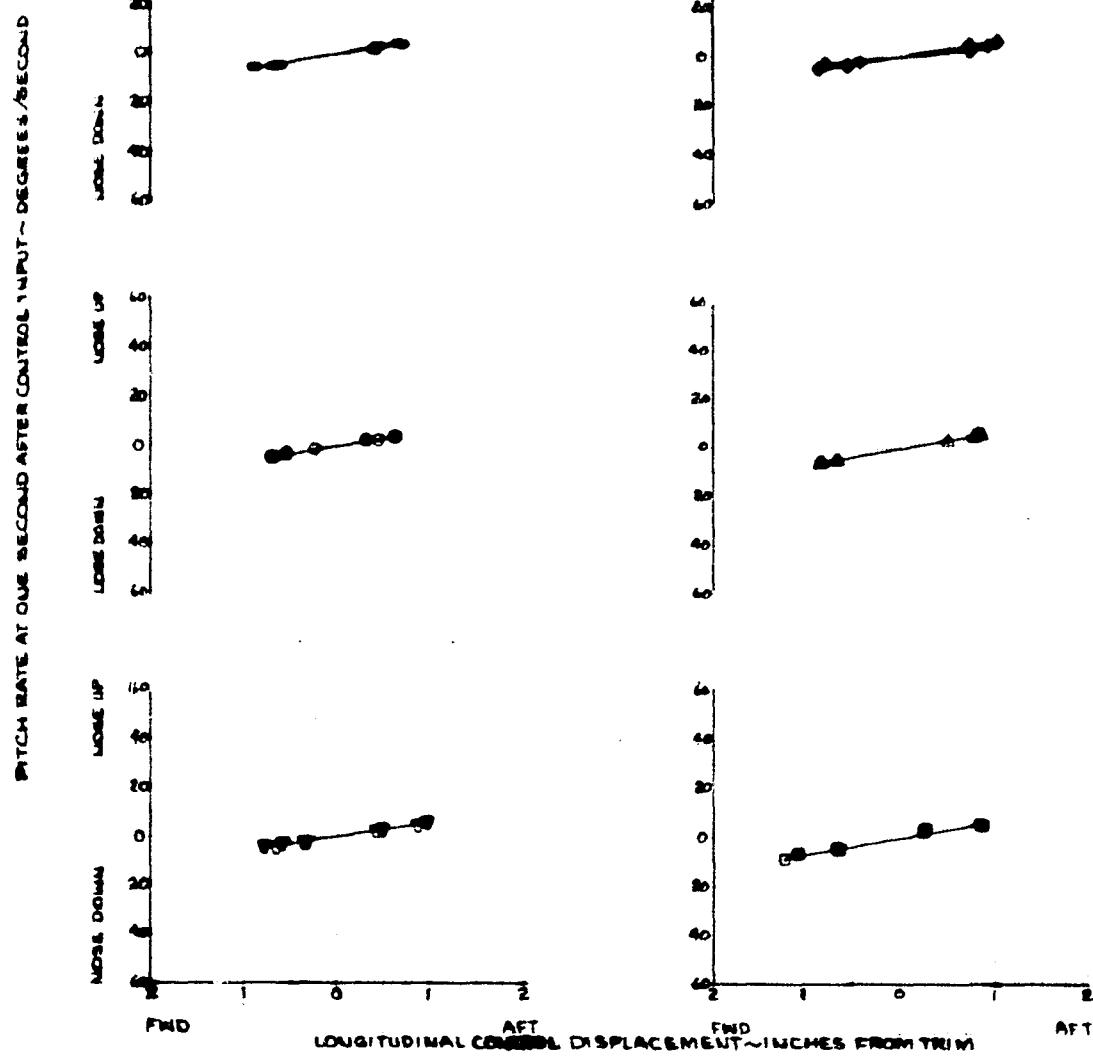


FIGURE NO. 172
LONGITUDINAL CONTROL SENSITIVITY
AH-1G USAF#15695
CLEAN CONFIGURATION

SYM.	AVERAGE ~CAB HO-FF	AVG. ALT. ~LB HO-FF	Avg. GANT ANG. LONG. HO-FF	ROTOS	FLIGHT CONDITIONS	THRUST DEGR. ~C+
O	62.0	7760	7712	201.8(AFT)	2000	LEVEL FLIGHT 0.000001
O	112.5	6450	7712	201.1(AFT)	2000	LEVEL FLIGHT 0.000001
O	162.5	6550	7760	201.2(AFT)	2000	LEVEL FLIGHT 0.000001
O	171.3	4870	1800	201.2(AFT)	2000	DIVE 0.000006
O	44.0	4840	1810	200.8(AFT)	2000	CLIMB 0.000006
O	44.0	8510	7420	201.2(AFT)	2000	AUTO ROTATION 0.000006

NOTE - OPEN SYMBOLS DENOTE SCAD ON
SOLID SYMBOLS DENOTE SCAD OFF

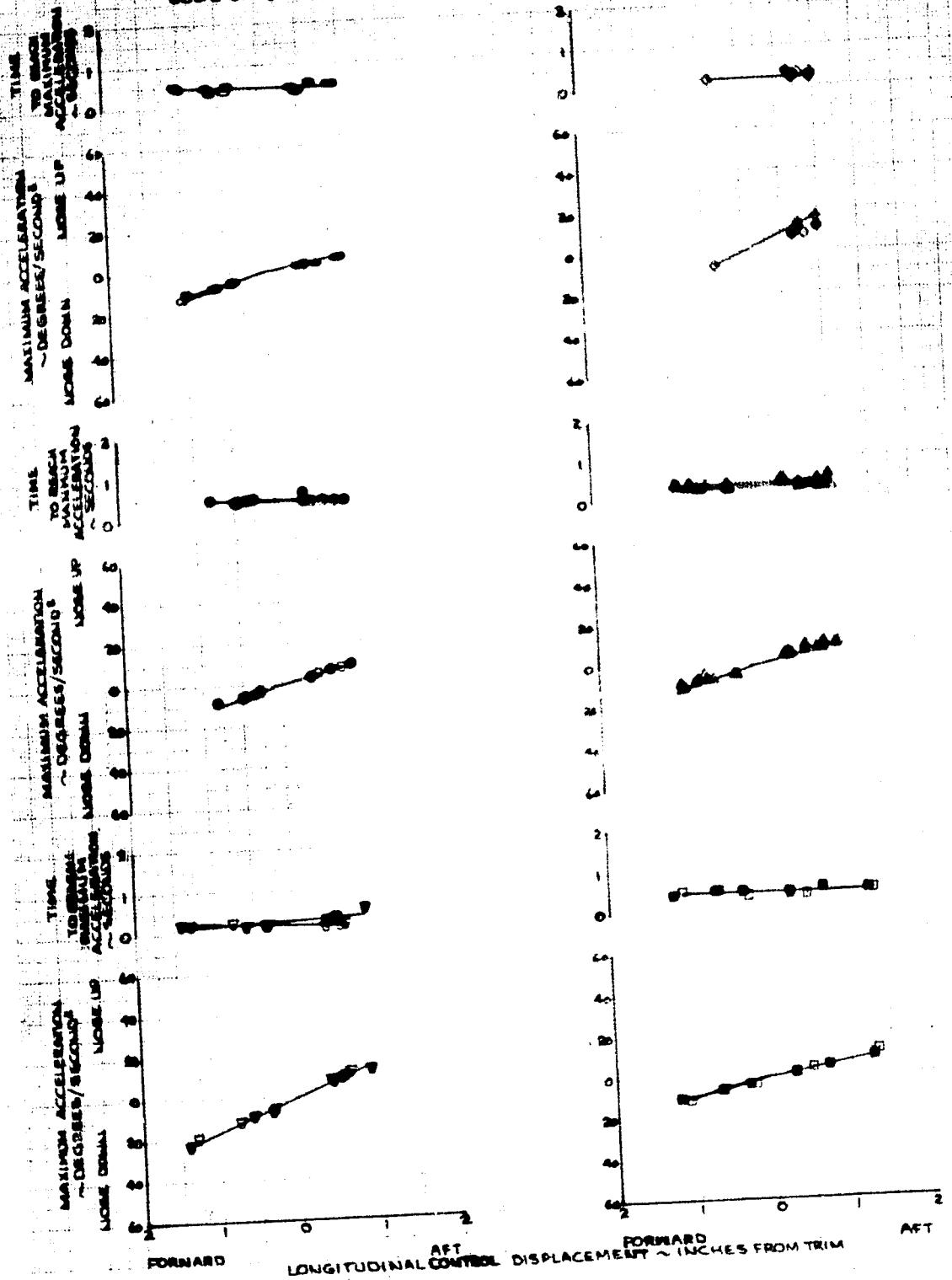


FIGURE NO. 173
LONGITUDINAL CONTROL RESPONSE
AMIG USAF 718695
CLEAN CONFIGURATION
SCAS ON

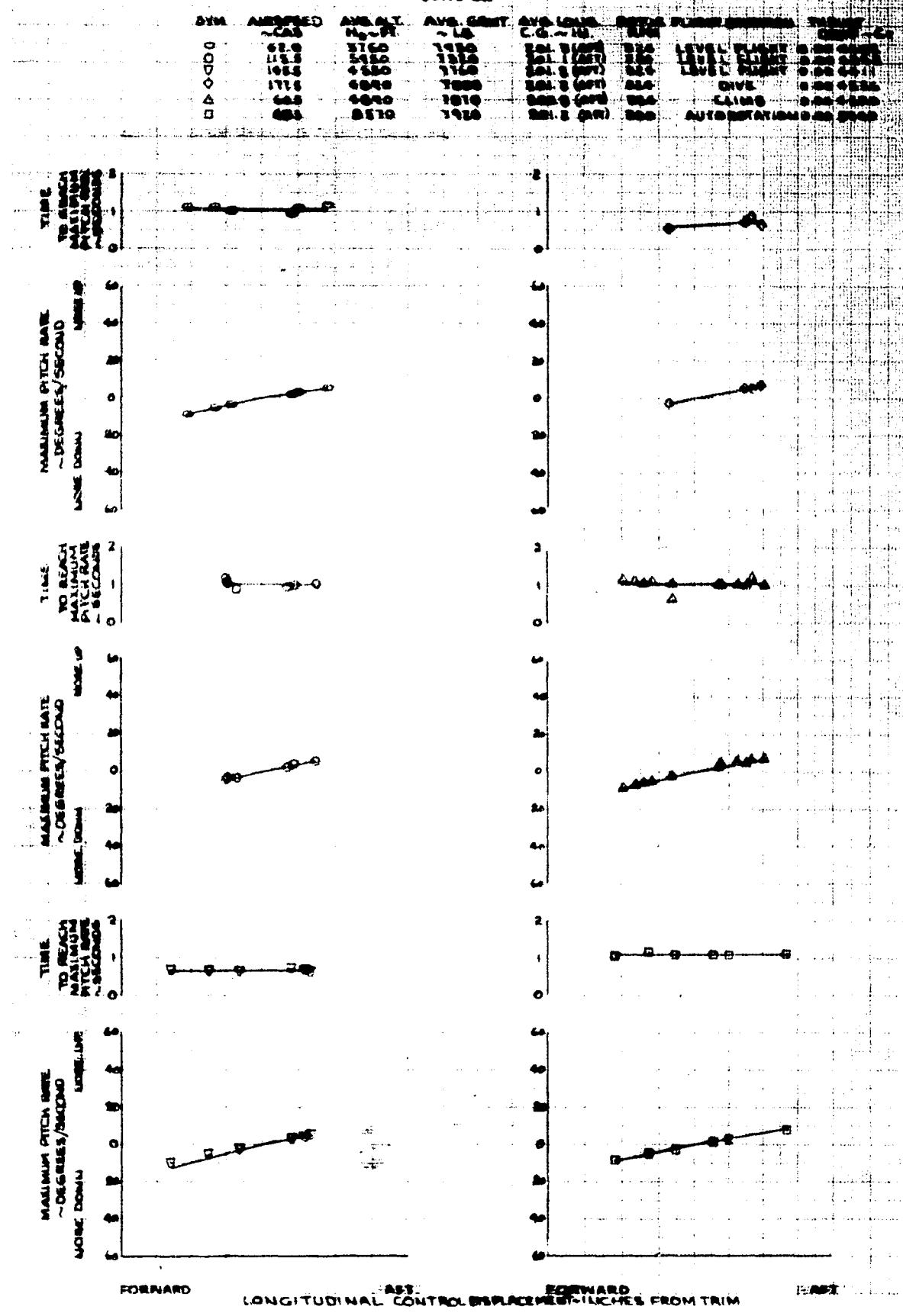


FIGURE NO. 174
LONGITUDINAL RESPONSE AT ONE SECOND
AH-6 USAF 671569
CLEAN CONFIGURATION

CG	AIR SPEED CAS	AVG ALT. ft.	AVG. GENT AVG. LONG. C.G. ~IN.	MOTOR FLIGHT COMBINATION	THROTTLE - CT
0	111.8	3150	1100	ROLL (AFT)	0.000002
0	145.5	4150	1100	ROLL (AFT)	0.000002
0	177.5	4600	1000	ROLL (AFT)	0.000011
0	60.5	4910	1070	DIVE	0.000026
0	60.5	5570	5070	CLIMB	0.000026
				AUTO ROTATION	0.000010

NOTE: OPEN SYMBOLS DENOTE SCAS ON
SOLID SYMBOLS DENOTE SCAS OFF

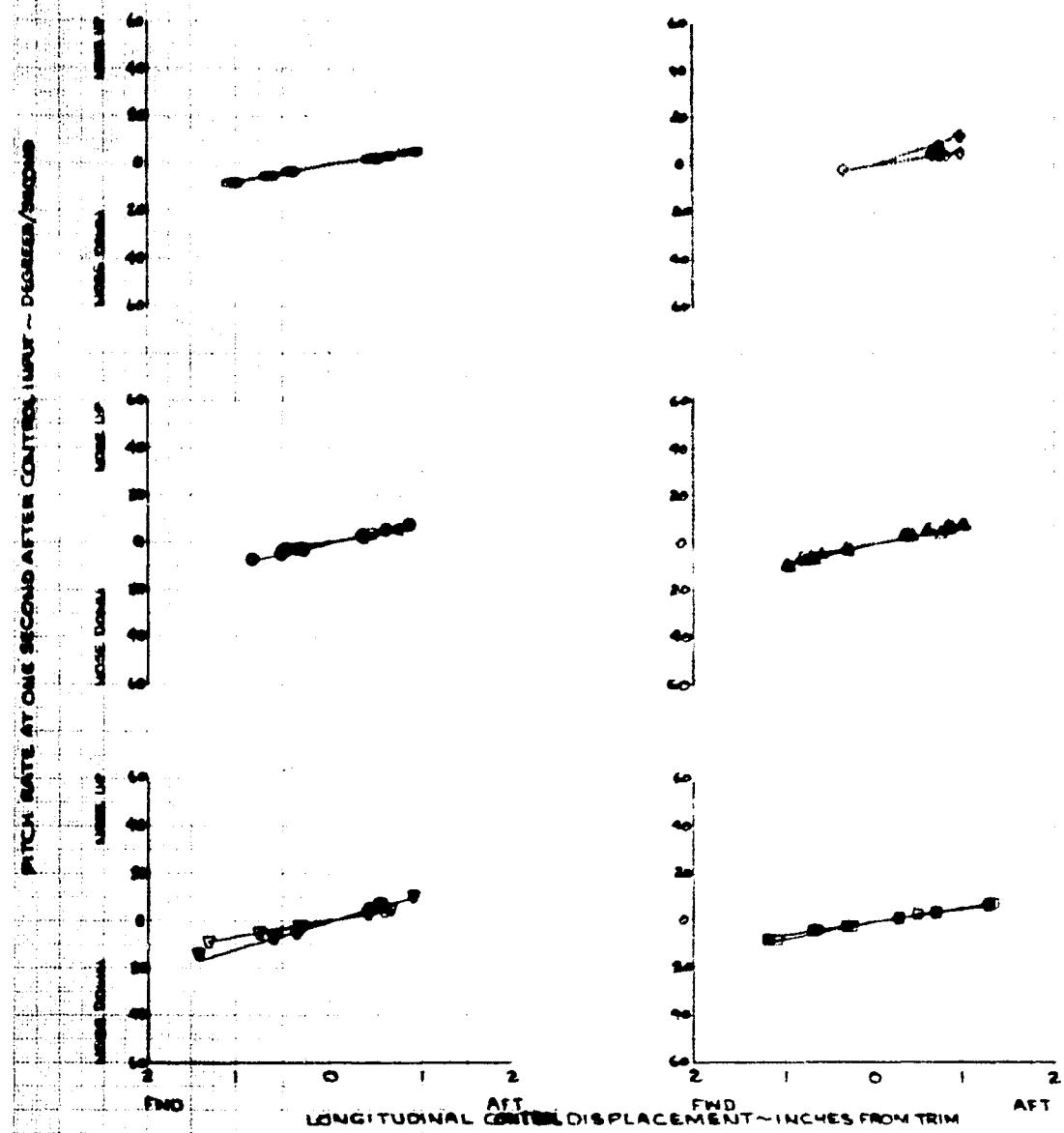


FIGURE NO. 175
ANGULAR PITCH DISPLACEMENT
AH-1G USAF T-16C
CLEAN CONFIGURATION

SYM.	AIRSPD. ~CAS	AVG. ALT. H ₀ ~FT	AVG. SPWY. LNG. ~IN.	DATA POINTS	COMBINATION	TURBT. CORR.	-CT
				C.G. ~IN.	TIME		
○	62.0	3700	1430	201.0(0)	3240 LEVEL FLIGHT	0.000403	
○	116.5	3700	7820	201.1(0)	2640 LEVEL FLIGHT	0.000366	
○	145.5	4550	7760	201.2(0)	3360 LEVEL FLIGHT	0.000411	
○	177.5	4870	7820	201.3(0)	3240 DIVE	0.000326	
△	60.5	7890	1870	201.8(0)	3240 CLIMB	0.000320	
○	62.5	8570	1920	201.9(0)	3240 AUTOROTATION	0.000440	

NOTE: OPEN SYMBOLS DENOTE SCAS ON
SOLID SYMBOLS DENOTE SCAS OFF

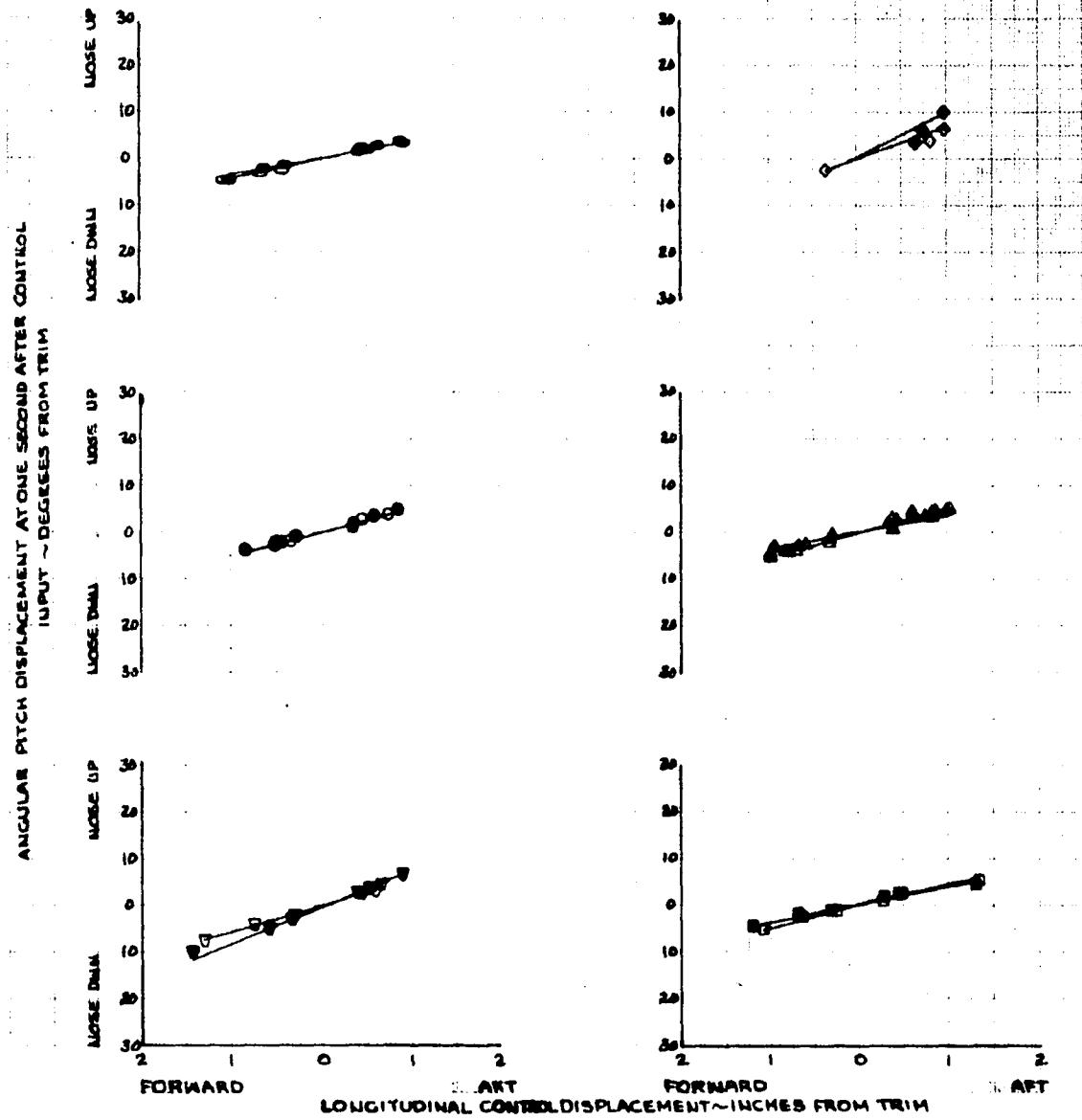


FIGURE NO. 176
LONGITUDINAL CONTROL SENSITIVITY

AH-1G USAF 715695
 HVY SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED
 SCAB ON

SVM.	AIRSPEED	AUG. ALT. ~FT	AUG. GRD. ~LB.	AUG. LONG. MOTOR FLIGHT CONDITION	THRUST COEFF. ~CT	FLIGHT CONDITION	
						C.G. ~IN.	RPM
O	106.0	5550	9160	200.3(AFT)	3240	LEVEL FLIGHT	0.005867
O	106.0	5140	9830	200.1(AFT)	3240	LEVEL FLIGHT	0.005899
O	112.0	7570	9590	200.0(AFT)	3240	DIVE	0.005978
A	98.0	2730	9630	200.0(AFT)	3240	CLIMB	0.005183

NOTE: 817 LB. IN OUTSD. ROCKET POD'S

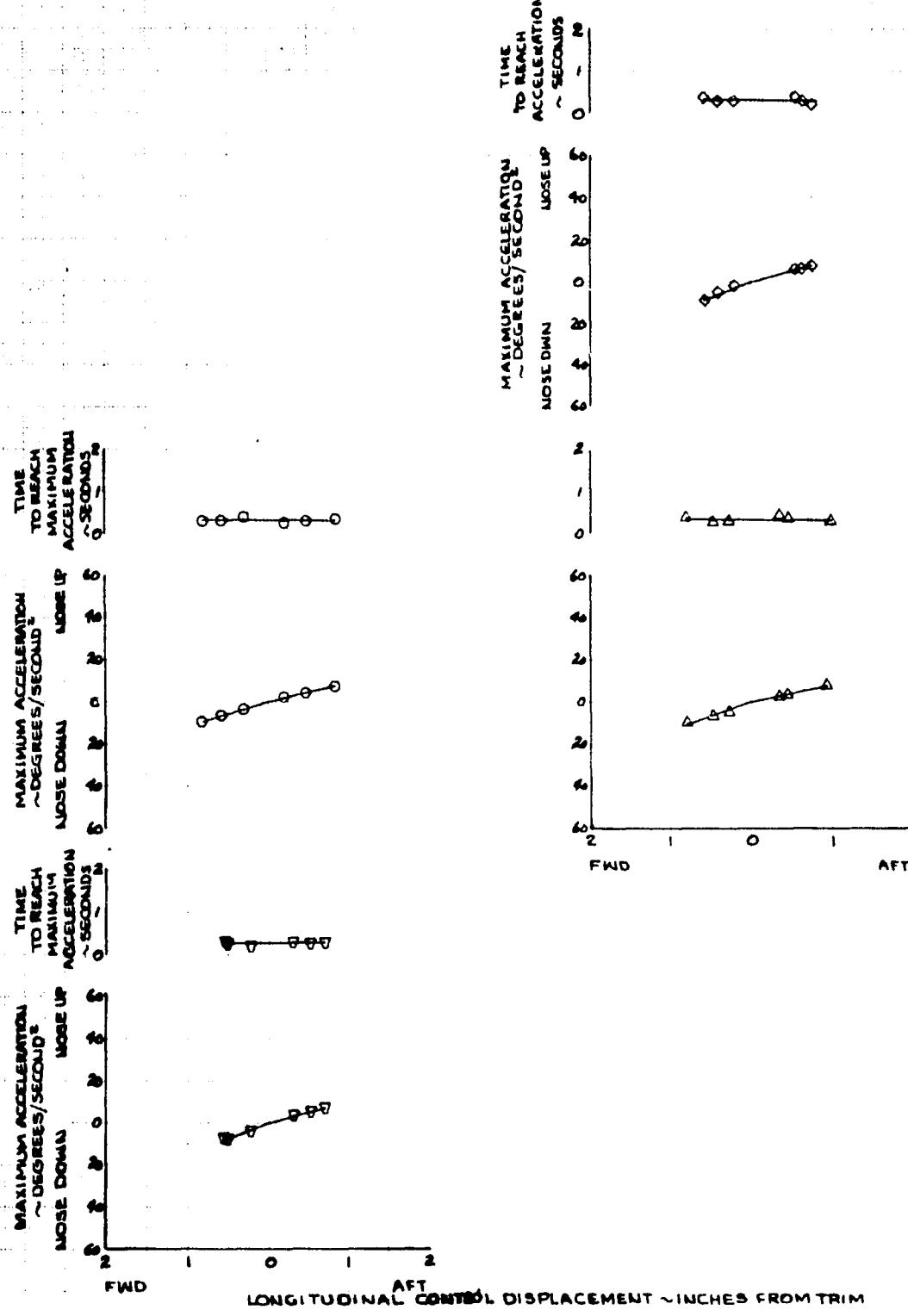
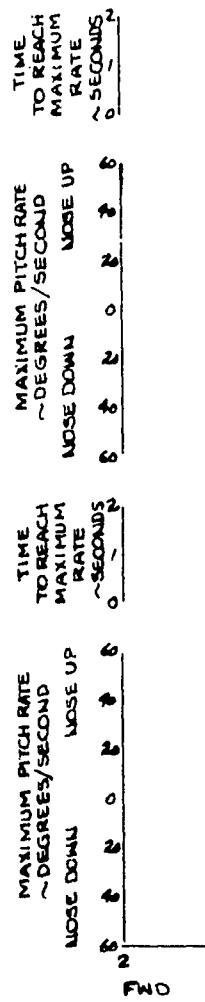


FIGURE NO. 177
LONGITUDINAL CONTROL RESPONSE

AH-1G USA X#118698
 HVY SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED
 SCAS ON

SYM	AIR SPEED ~CAS	AVG. ALT. M ₀ -FT.	Avg. GRAD. ~LB	Avg. LONG. C.G. -IN.	ROTOR FLIGHT CONDITION	THRUST COEF.
O	106.0	5660	9160	200.3 (AFT)	3240 LEVEL FLIGHT	0.005867
O	146.0	5140	9330	200.1 (AFT)	3240 LEVEL FLIGHT	0.005874
O	172.0	7570	9590	200.0 (AFT)	3240 DIVE	0.005878
△	58.0	2720	9630	200.0 (AFT)	3240 CLIMB	0.005103

NOTE: 81 LB. IN OUTBOARD ROCKET POD



0

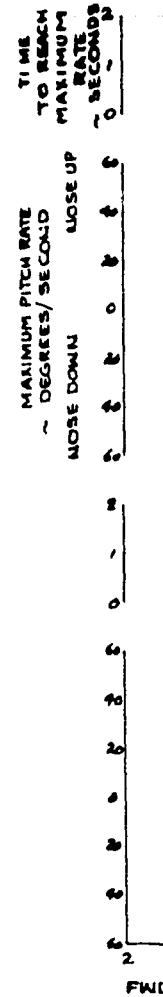
0

0

0

FWD AFT

LONGITUDINAL CONTROL DISPLACEMENT ~ INCHES FROM TRIM



0

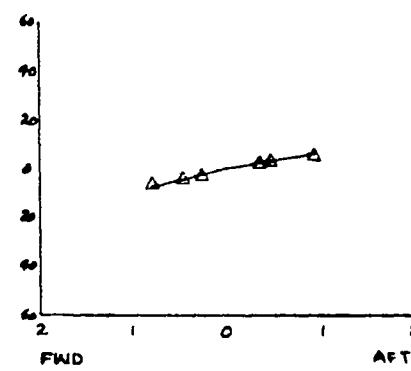
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0

0

FWD

AFT



0

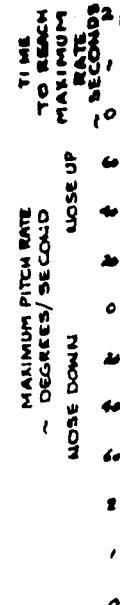
0

0

0

FWD

AFT



0

0

0

0

0

0

0

0

FWD

AFT

FIGURE NO. 17B
 LONGITUDINAL RESPONSE AT ONE SECOND

AH-1G USAFT 19695
 HVY. SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED
 BCAS ON

SYM	AIRSPD ~CAS	Avg. ALT. ft.	Avg. CRHTNG. deg.	LONG. MOTOR FLIGHT CONDITION	THRUST COEFF. ~CT
O	106.0	5860	9160	200.0(AFT)	0.005367
D	146.0	5140	9380	200.1(AFT)	0.005399
D	172.0	7570	9690	200.0(AFT)	0.005978
A	58.0	2730	9630	200.0(AFT)	0.005183

NOTE: 817 LB. IN. OUTWD. ROCKET PODS

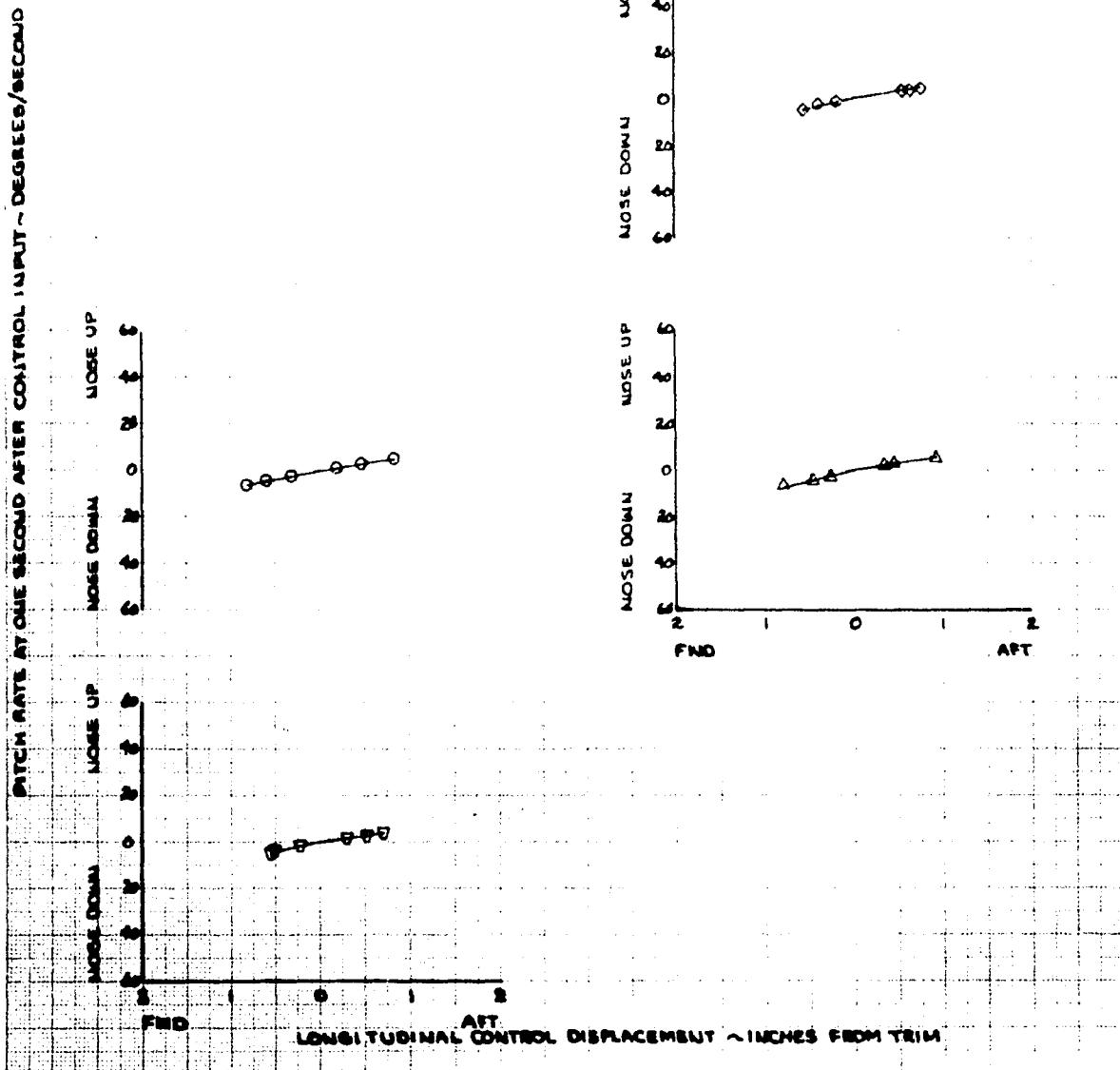
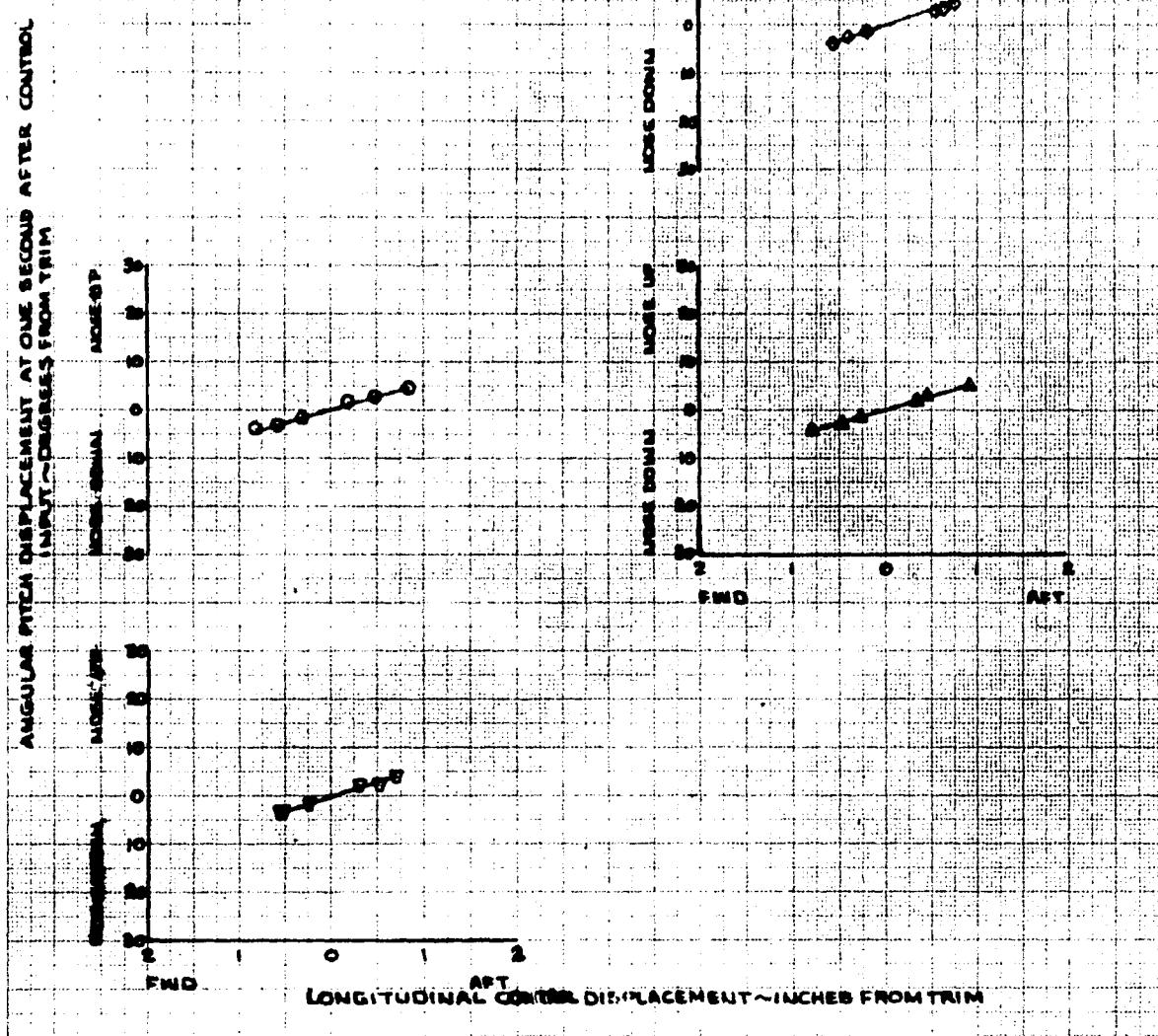
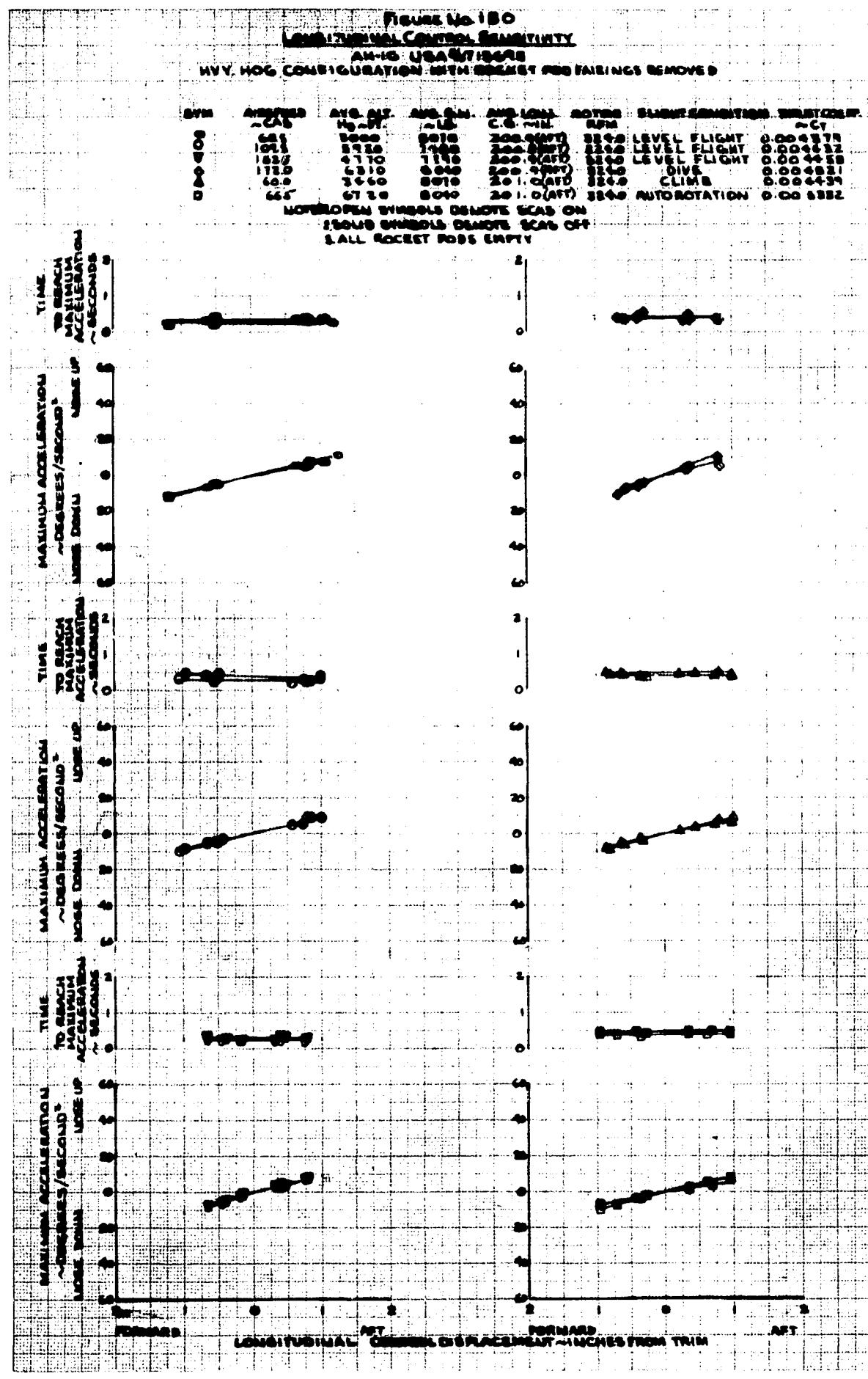


FIGURE NO. 179
 ANGULAR PITCH DISPLACEMENT
 AM-1G USAF 1968
 HY. SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM	AIRSPED	AVG ALT.	ANG. PNT. AVGLONG.	ROTOR ELEMENT POSITION	THRUST COEFF.
-CAS	M ₀ - FT.	-10	C.G. - IN.	1000	-CT
1060	1150	8100	1000 (M)	0.00 5867	
1160	1250	8200	1000 (M)	0.00 5399	
1220	1350	8300	1000 (M)	0.00 5978	
1320	1500	8400	1000 (M)	0.00 5183	

NOTE: DATA IS MEASURED IN HORIZONTAL POSITION



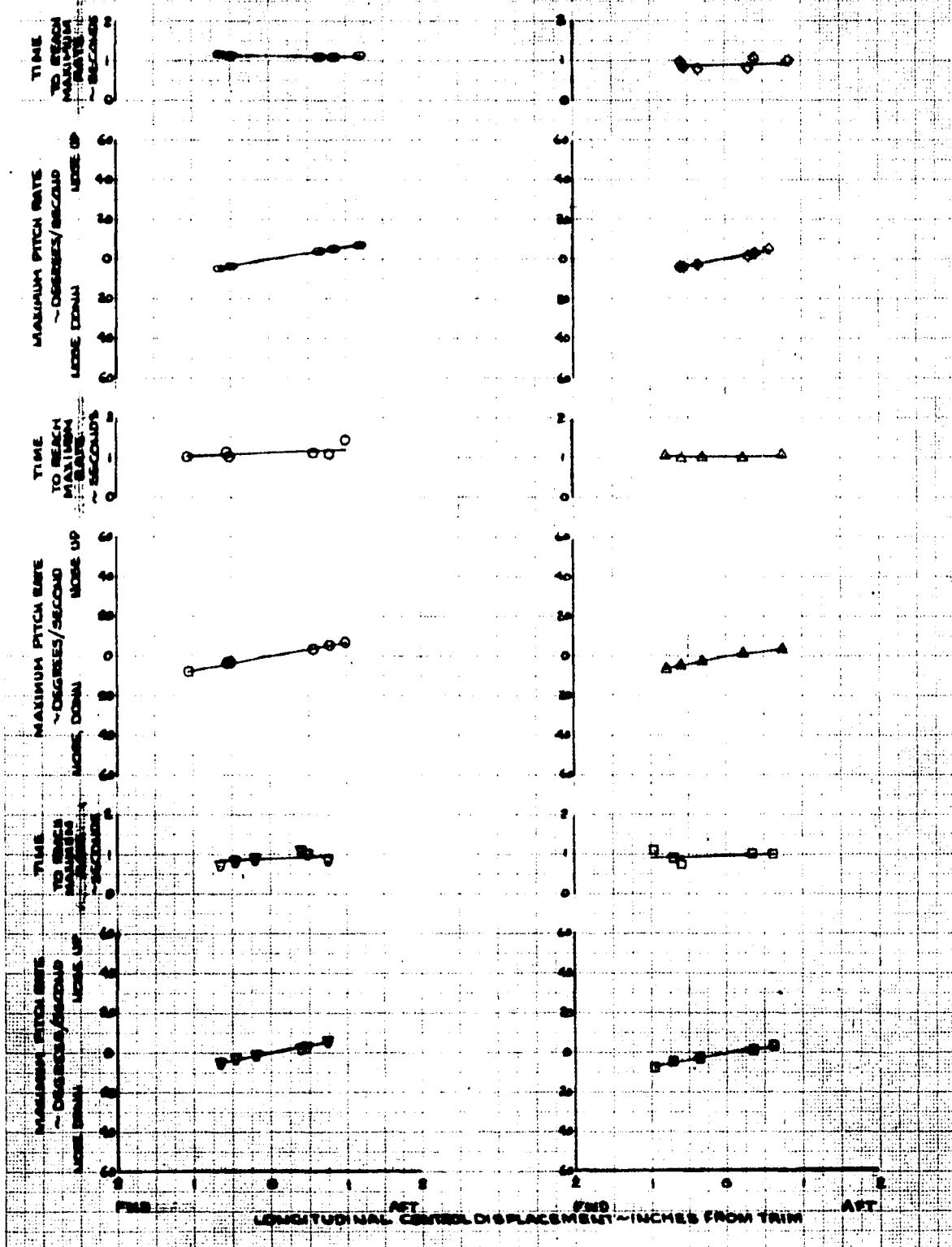


2
FIGURE NO 101
LONGITUDINAL CONTROL RESPONSE

AH-1G USAF 61-15645
HVV, HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED
SCAB ON

SYM	AIRSPD	ANG ALT	ANG G.L.	ANG VERT	ROTAT	FLIGHT DURATION	TIME
•	CAS	10°	-10°	0°	0°	0.004374	0.000000
○	60.5	2000	0000	0000 (APT)	32.40	LEVEL FLIGHT 0.004462	0.000000
○	109.2	2720	1100	2000 (APT)	31.00	LEVEL FLIGHT 0.004458	0.000000
○	143.5	4770	1170	2000 (APT)	32.40	LEVEL FLIGHT 0.004458	0.000000
○	178.0	6710	0000	2000 (APT)	31.00	DIVE	0.004458
▲	240	3660	0000	2010 (APT)	31.00	CLIMB	0.004457
○	65.9	6720	0000	2010 (APT)	30.00	AUTOROTATION 0.005732	0.000000

NOTE: ALL ROCKET PODS EMPTY



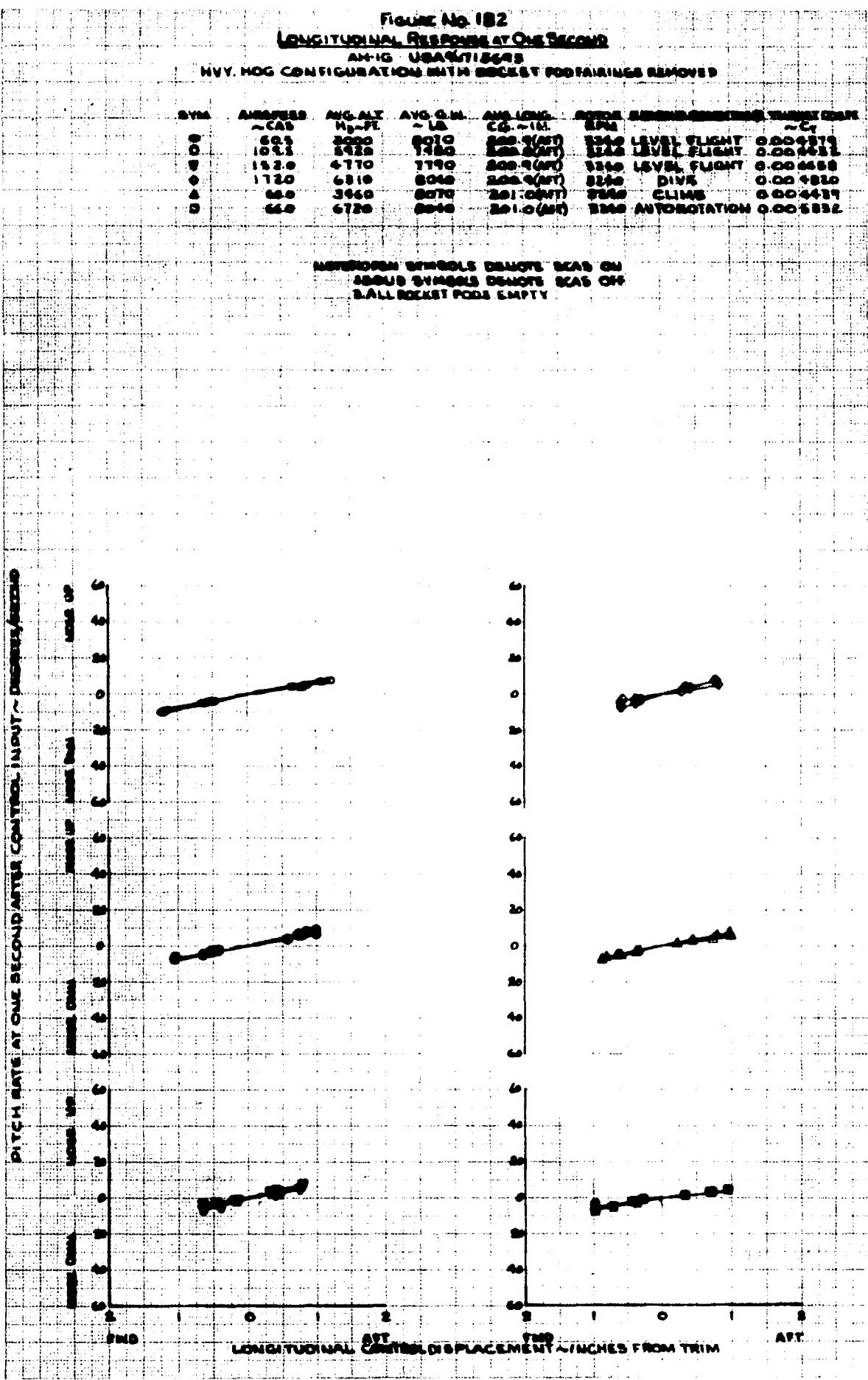


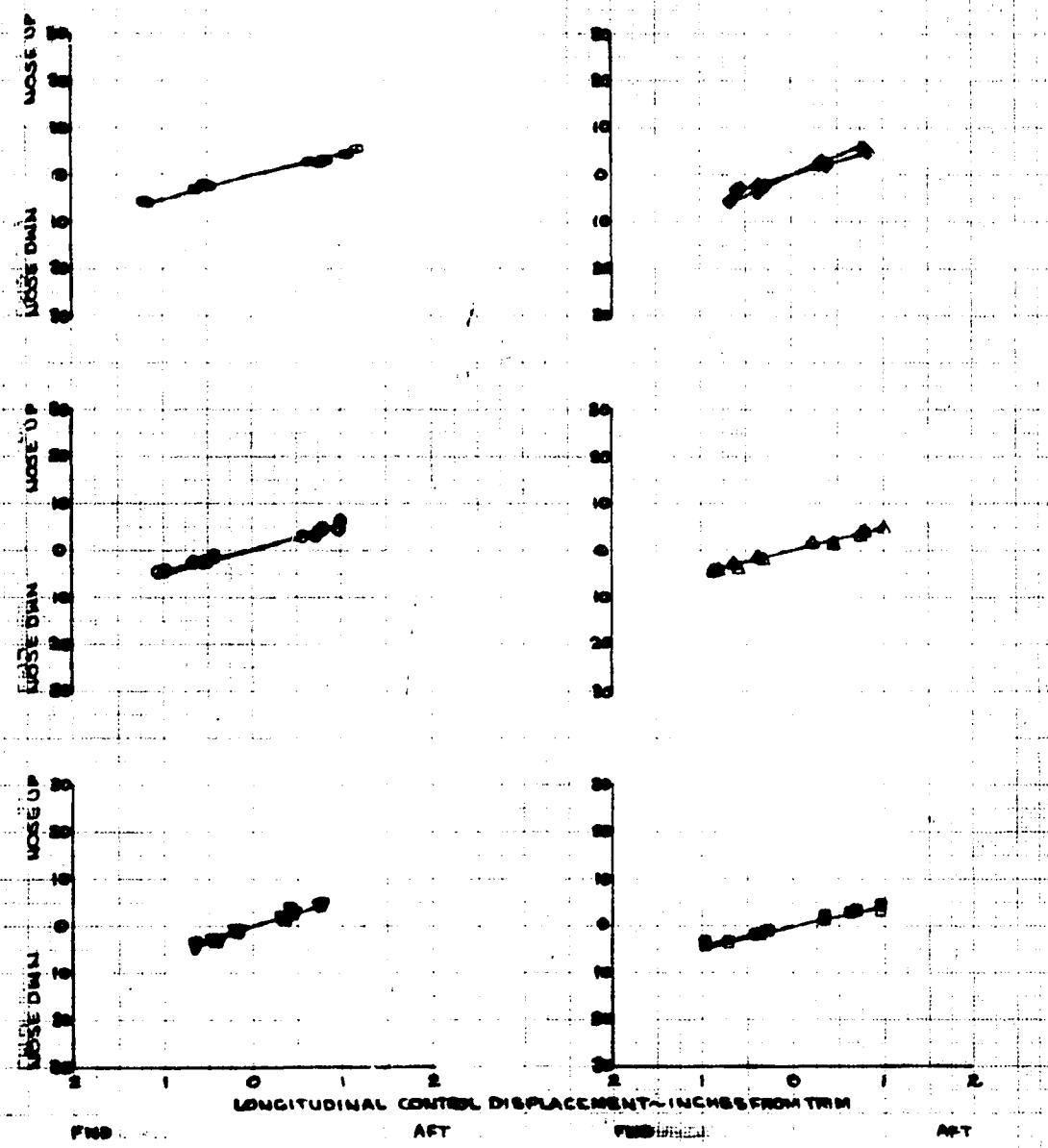
Figure No. 183
ANGULAR PITCH DISPLACEMENT

AH-1S USAF 67-6066
HVY. HCG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM.	AIR SPEED	Avg. ALT.	Avg. GM	Avg. LOAD	NOTES
○	60.0	3000	5010	200.0(AFT)	3240 LEVEL FLIGHT 0.0005176
○	102.0	3220	7620	200.0(AFT)	3240 LEVEL FLIGHT 0.0004488
○	152.0	4770	1770	200.0(AFT)	3240 LEVEL FLIGHT 0.0004550
○	172.0	6810	6010	200.0(AFT)	3240 DIVE 0.0004620
△	60.0	3460	8010	201.0(AFT)	3240 CLIMB 0.0004497
○	66.0	6720	6000	201.0(AFT)	3240 AUTOROTATION 0.0004192

NOTES: OPEN SYMBOLS DENOTE SCAS ON
SOLID SYMBOLS DENOTE SCAS OFF
3. ALL ROCKET PODS EMPTY

ANGULAR PITCH DISPLACEMENT AT ONE SECOND AFTER CONTROL INPUT - DEGREES FROM TRIM



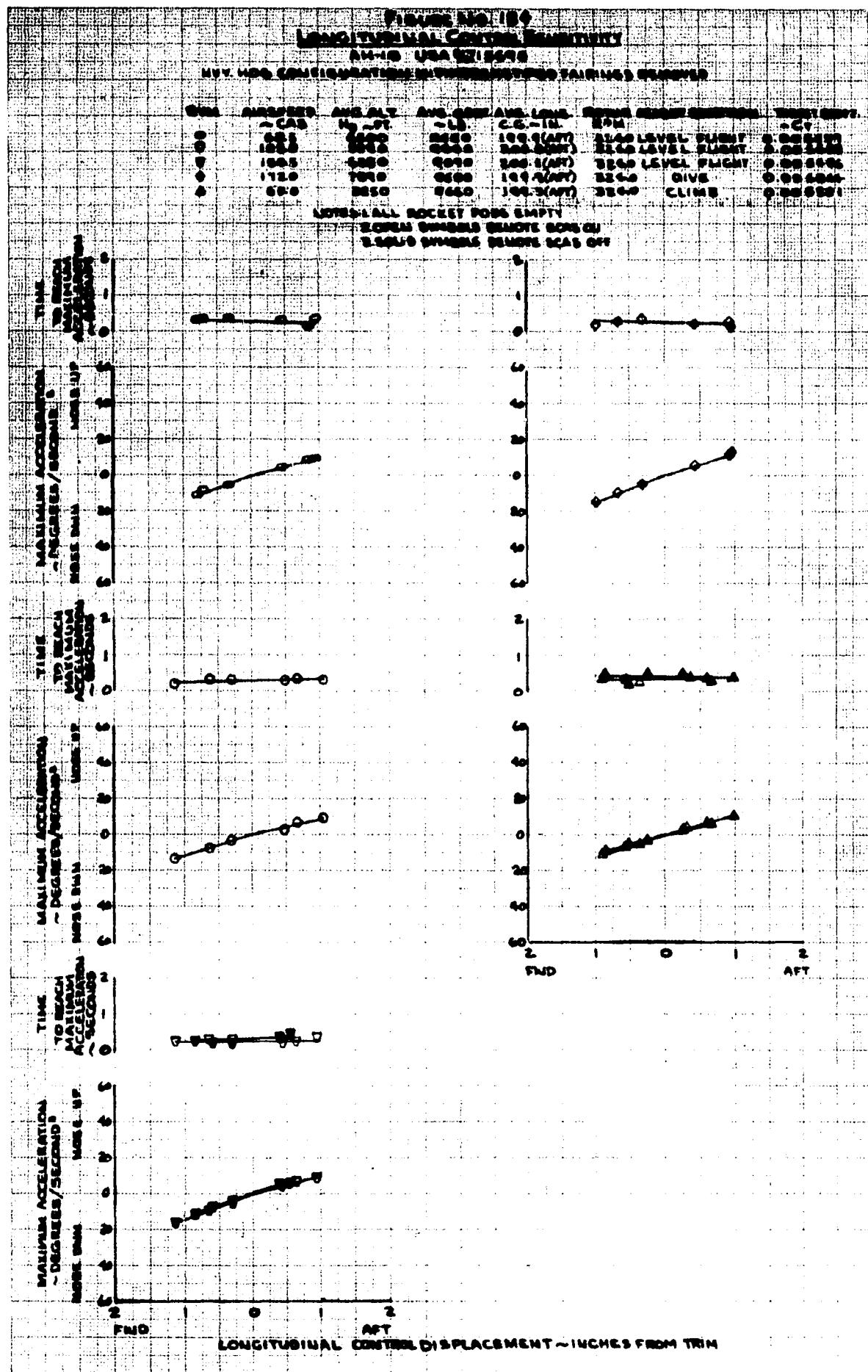


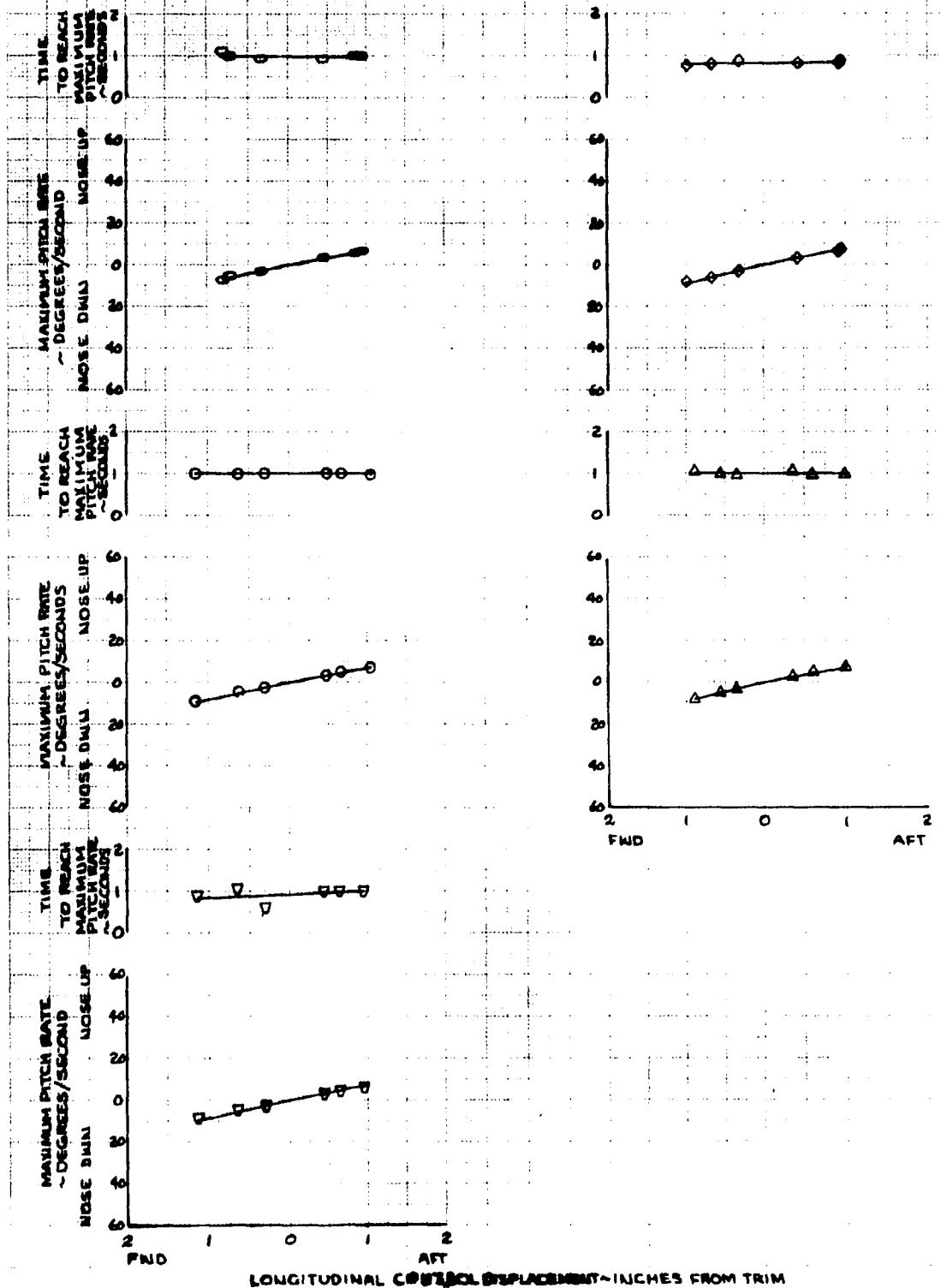
FIGURE NO. 185
LONGITUDINAL CONTROL RESPONSE

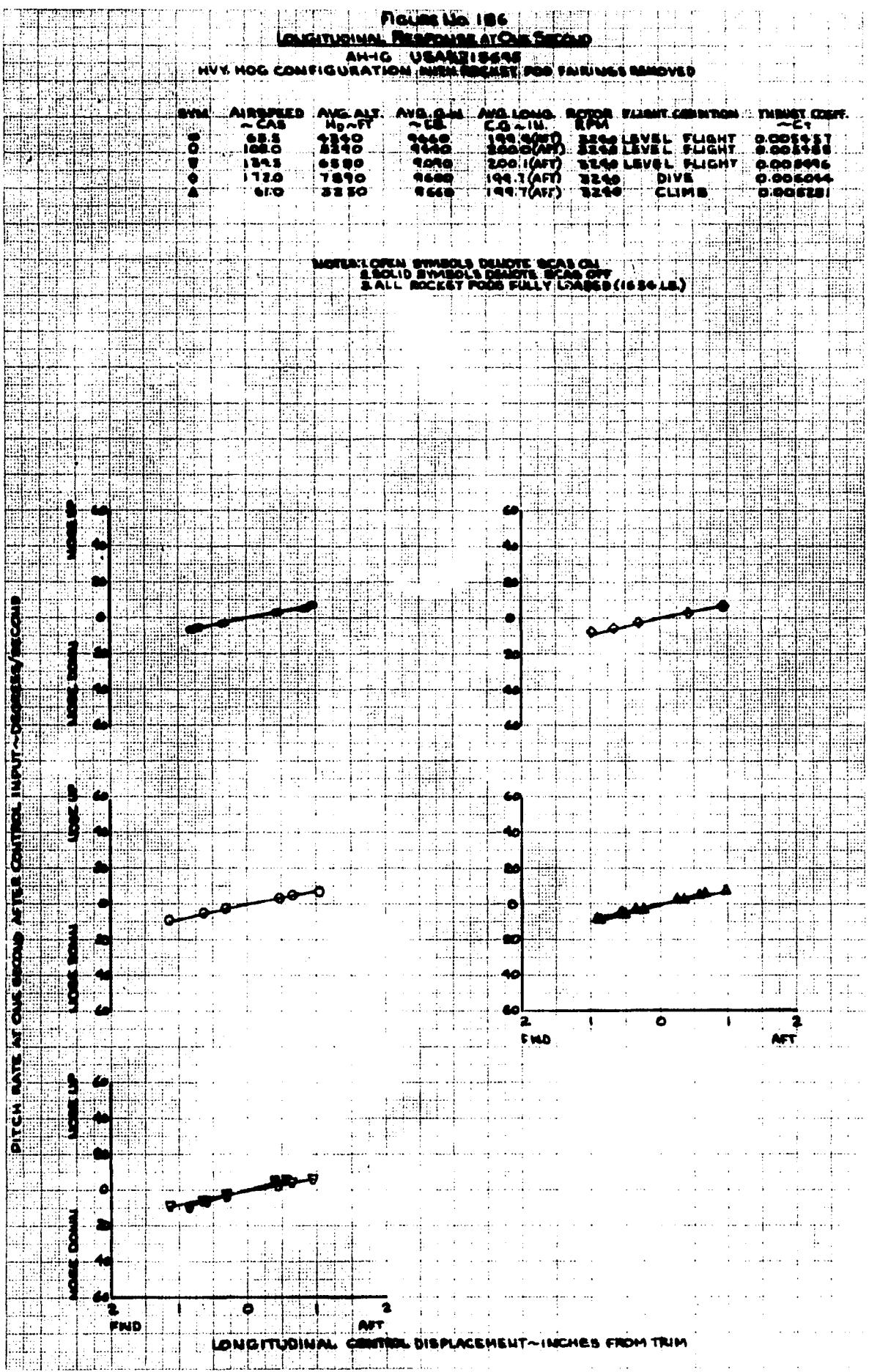
AH-1G USA4718695
H.V.Y. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

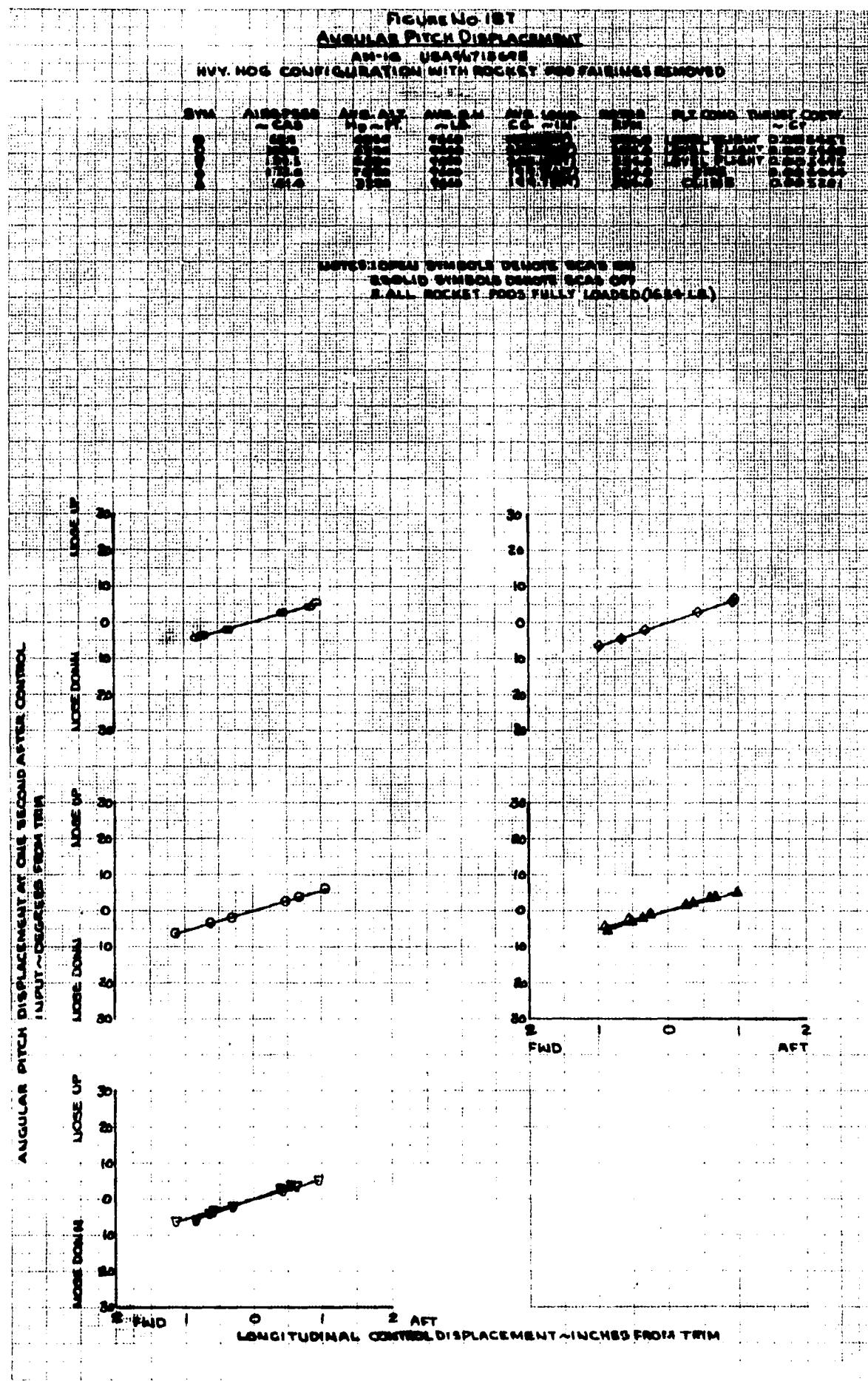
SCAB ON

SYM.	AIRSPEED ~CAS	Avg. ALT. Hd - FT.	Avg. G.W. ~FT.	Avg. LONG. C.G. ~IN.	ROTOR FLIGHT CONDITION	THRUST COEF. ~Cr
○	62.8	4240	9660	199.9(AFT)	324.0 LEVEL FLIGHT	0.00 5457
○	1020	2240	9440	200.0(AFT)	324.0 LEVEL FLIGHT	0.00 5458
○	134.3	6280	9040	200.1(AFT)	324.0 LEVEL FLIGHT	0.00 5446
○	1720	1870	7600	199.7(AFT)	324.0 DIVE	0.00 5014
△	61.0	3260	9660	199.7(AFT)	324.0 CLIMB	0.00 5281

NOTE : ALL ROCKET PODS LOADED (1634 LB.)







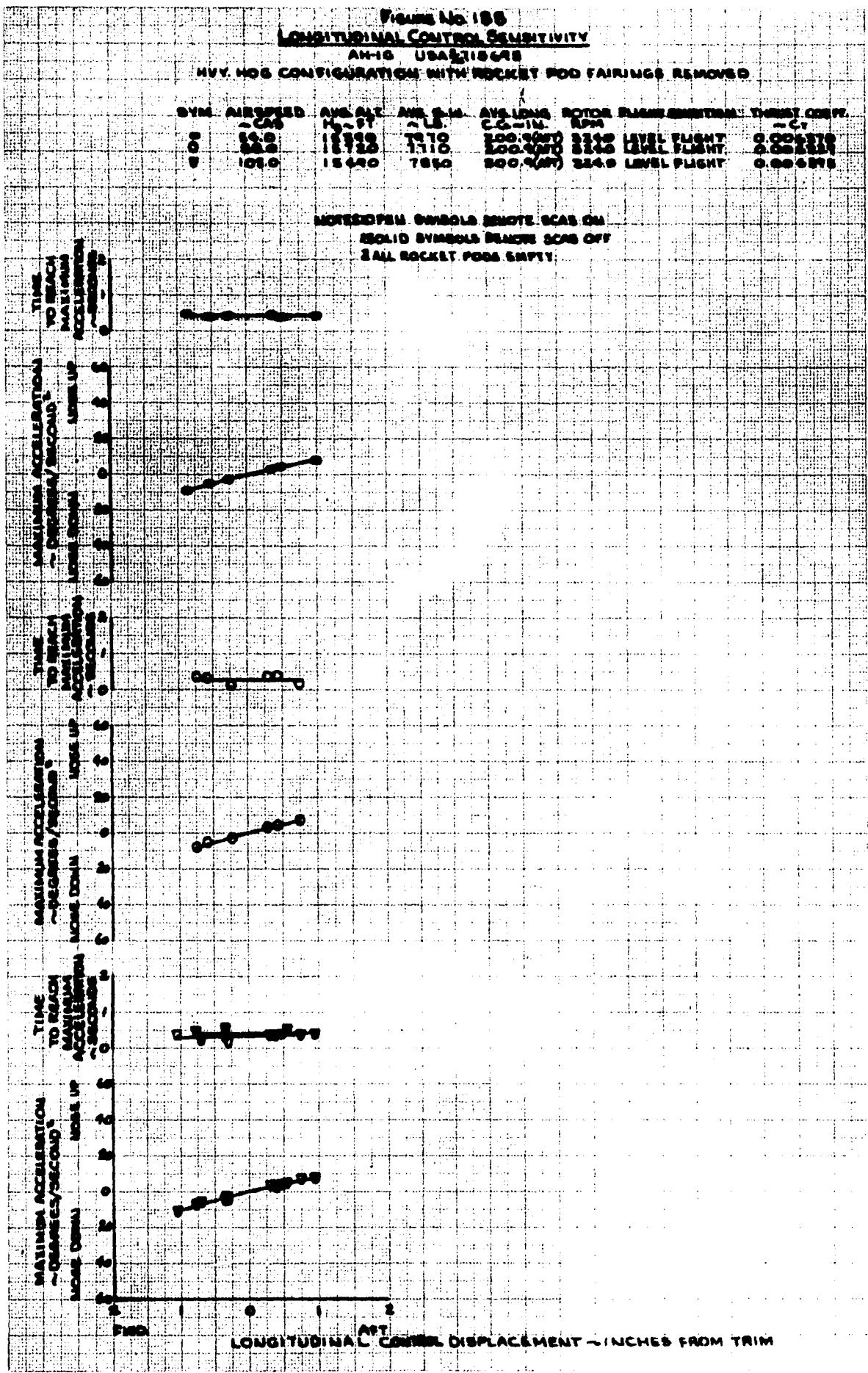
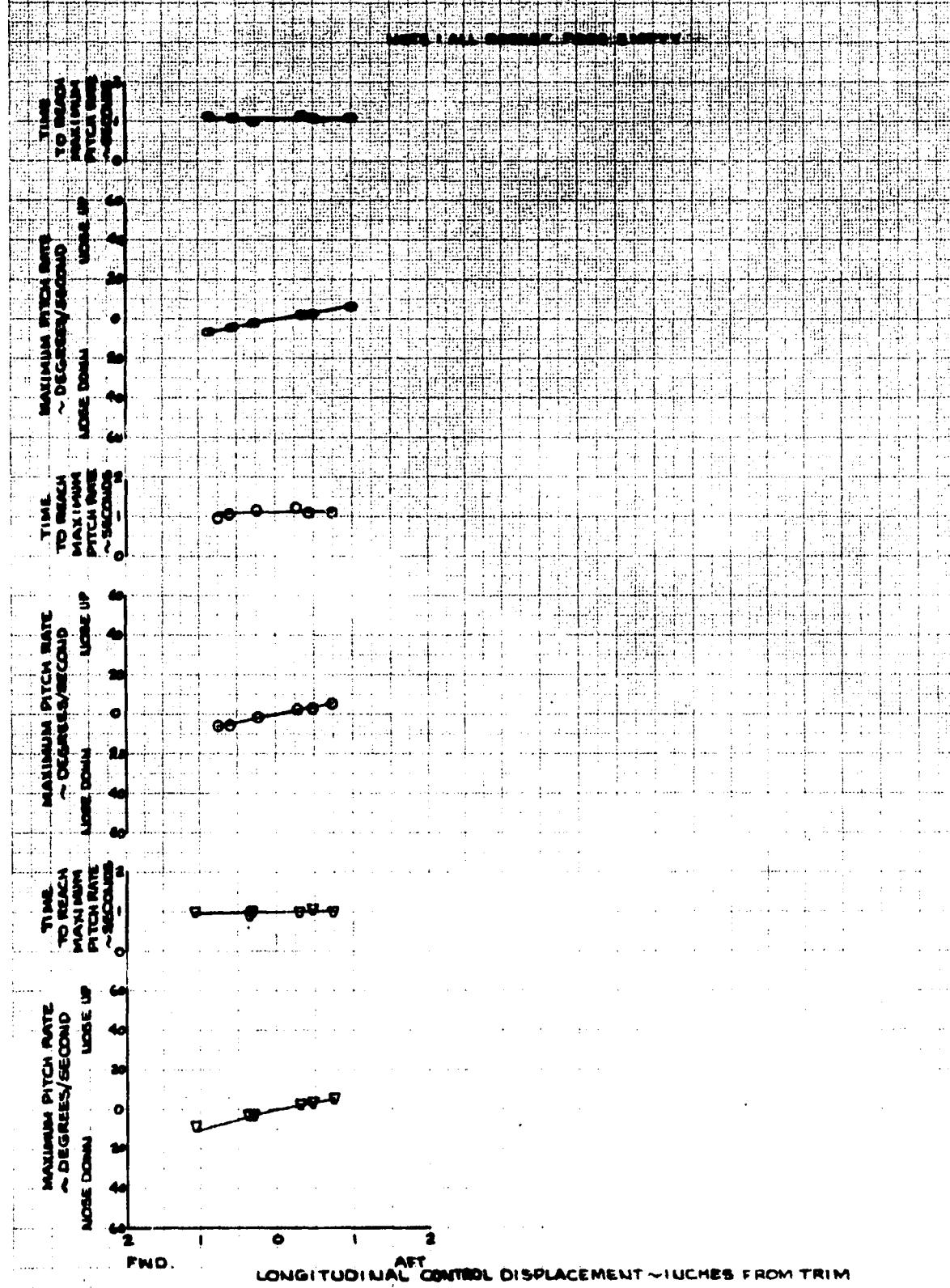


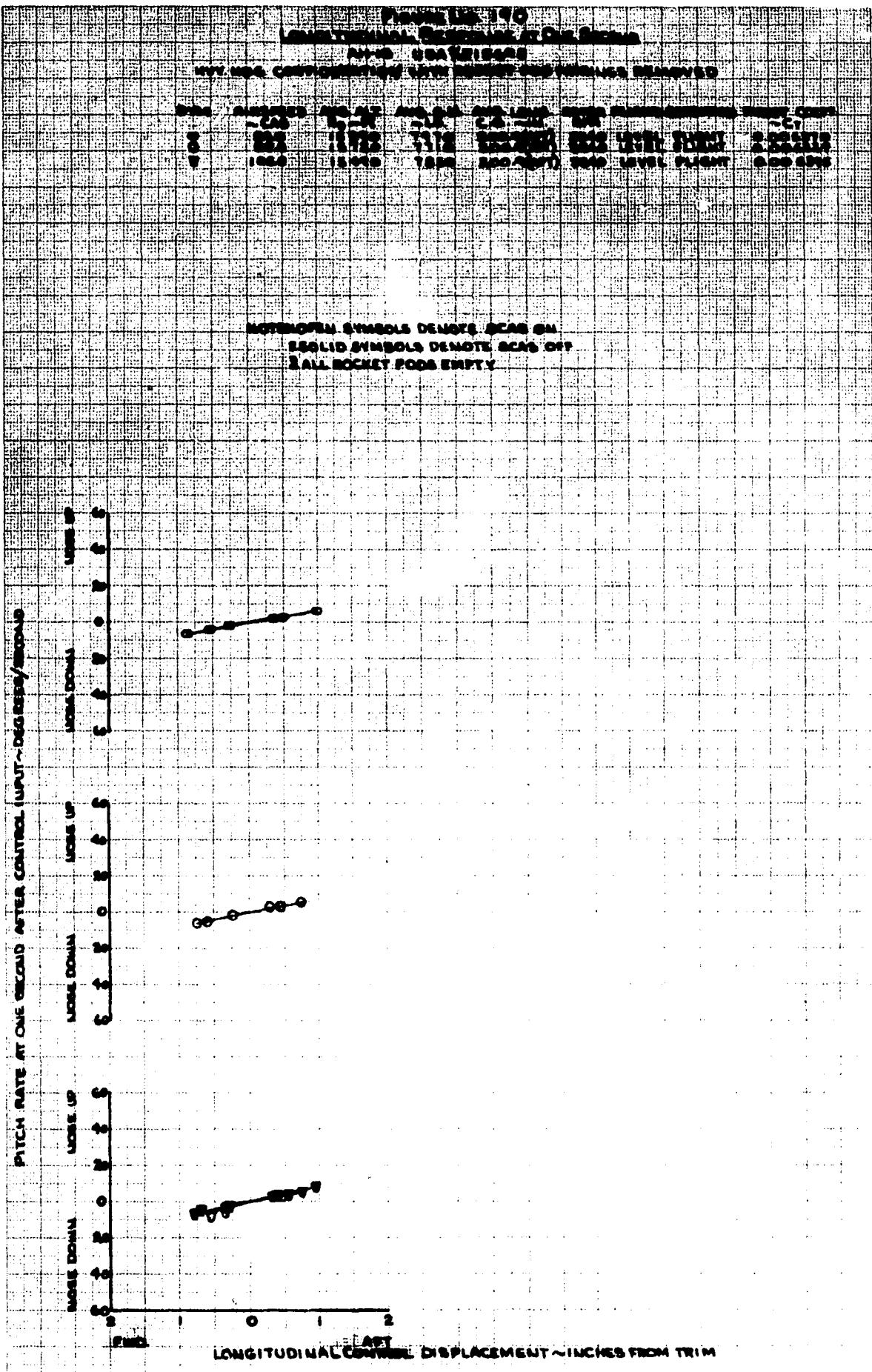
Figure No. 189
LONGITUDINAL CONTROL RESPONSE

AMERICAN USAFTICERS

WY-2 HIGH CONFIGURATION WITH LOWER TAIL FAIRINGS REMOVED

...SACRED





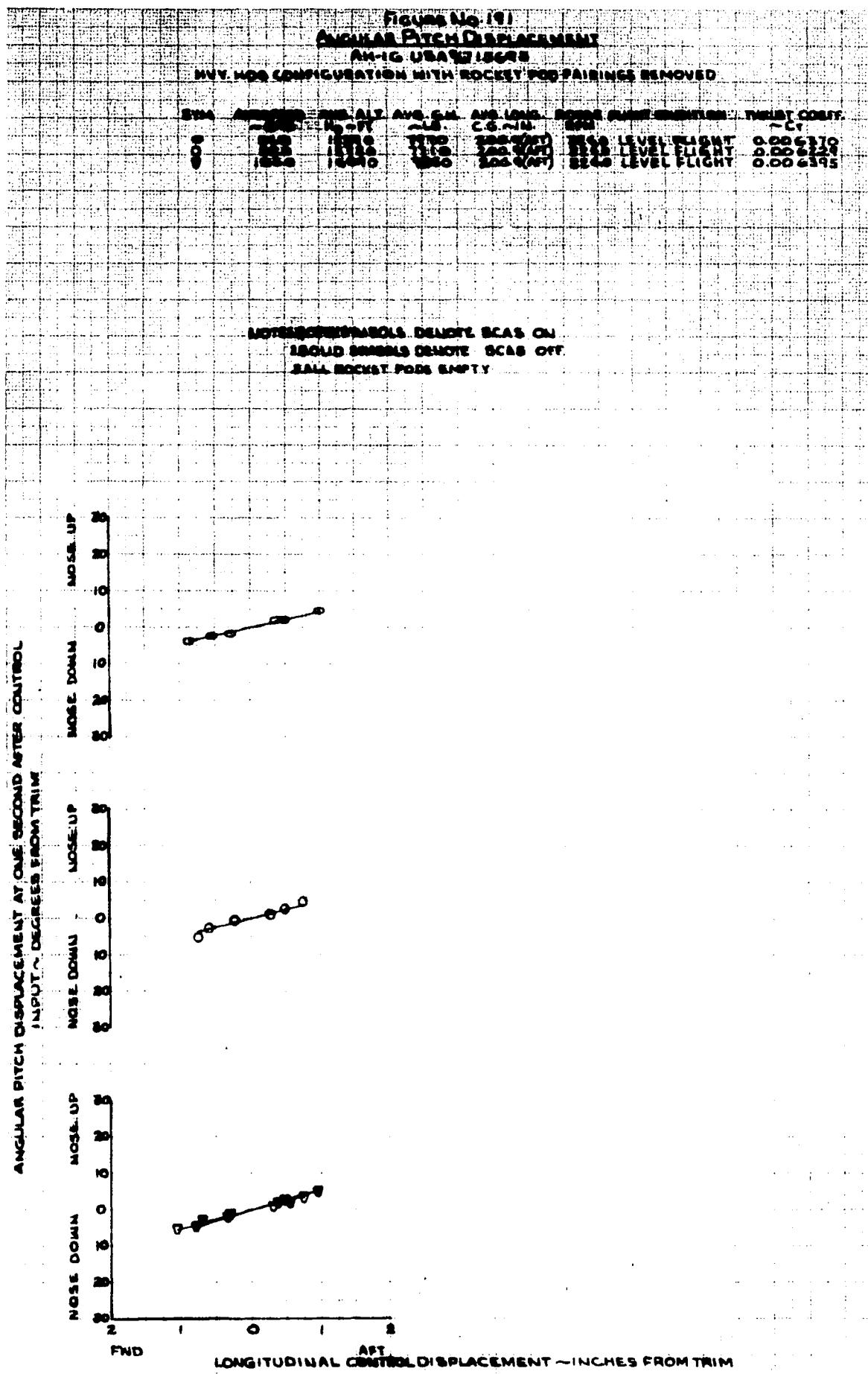


FIGURE NO. 1A2
LATERAL CONTROL SENSITIVITY
 AH-1G USAF/TIS/GR
 CLEAN CONFIGURATION

SYM	AIRSPD ~CAS	AVG ALI No. 52	AVG G.H. ~LS	AVG LONG. C.G.-IN	MOTOR FLIGHT CONDITION THRUST COEF.
○	65.0	4970	7710	201.2 (AFT)	3240 LEVEL FLIGHT 0.004439
○	101.0	6740	7300	201.1 (AFT)	3240 LEVEL FLIGHT 0.004443
△	145.0	4960	7460	201.2 (AFT)	3240 LEVEL FLIGHT 0.004420
◇	181.0	3140	7700	201.2 (AFT)	3240 DIVE 0.004183
△	62.0	2490	7620	201.2 (AFT)	3240 CLIMB 0.004066
□	68.0	7290	7730	201.2 (AFT)	3240 AUTOROTATION 0.004435

NOTE : OPEN SYMBOLS DENOTE SCALON
 SOLID SYMBOLS DENOTE SCALOFF

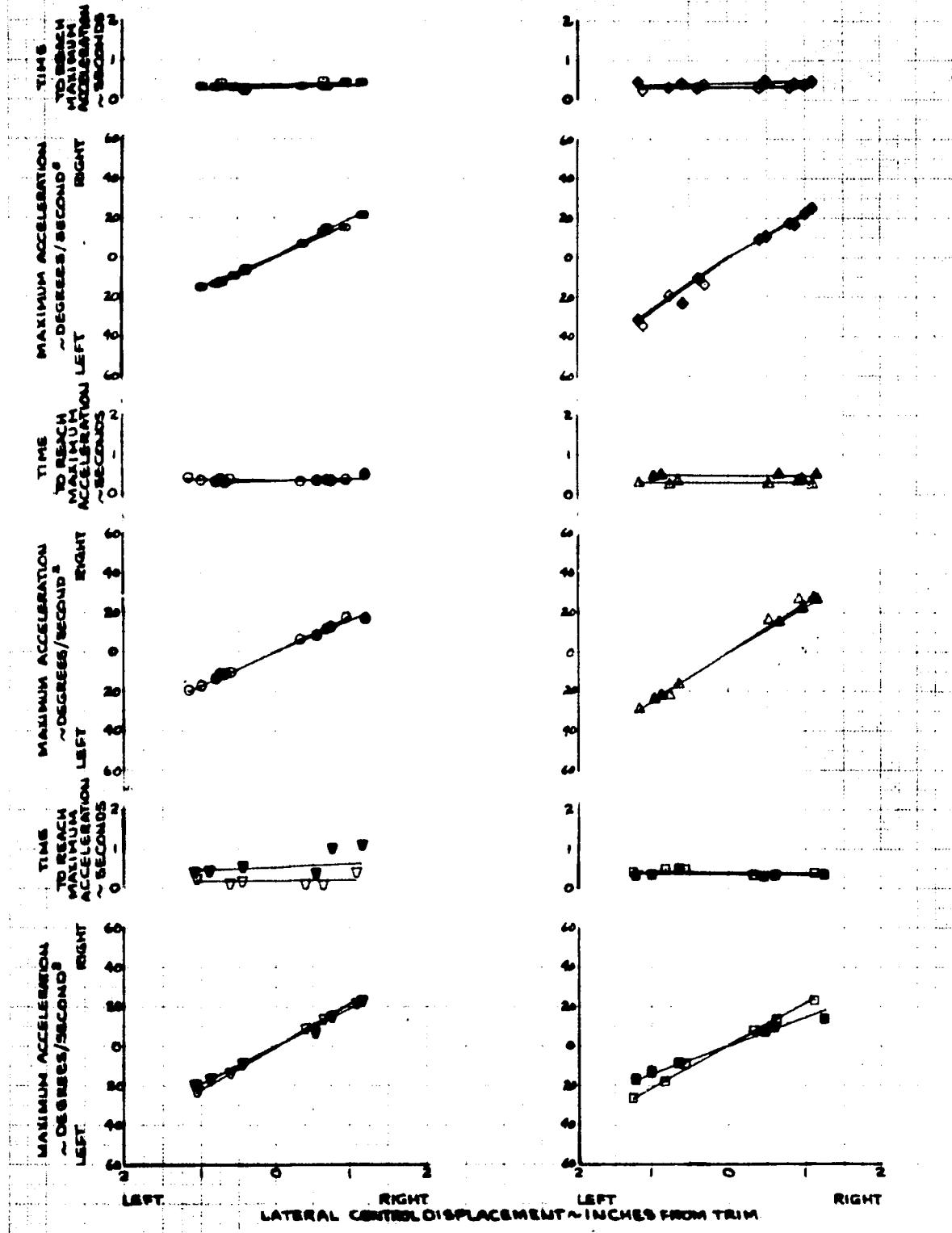


FIGURE NO. 193
LATERAL CONTROL RESPONSE
 AM-1G USA #6715698
 CLEAN CONFIGURATION
 SCAB ON

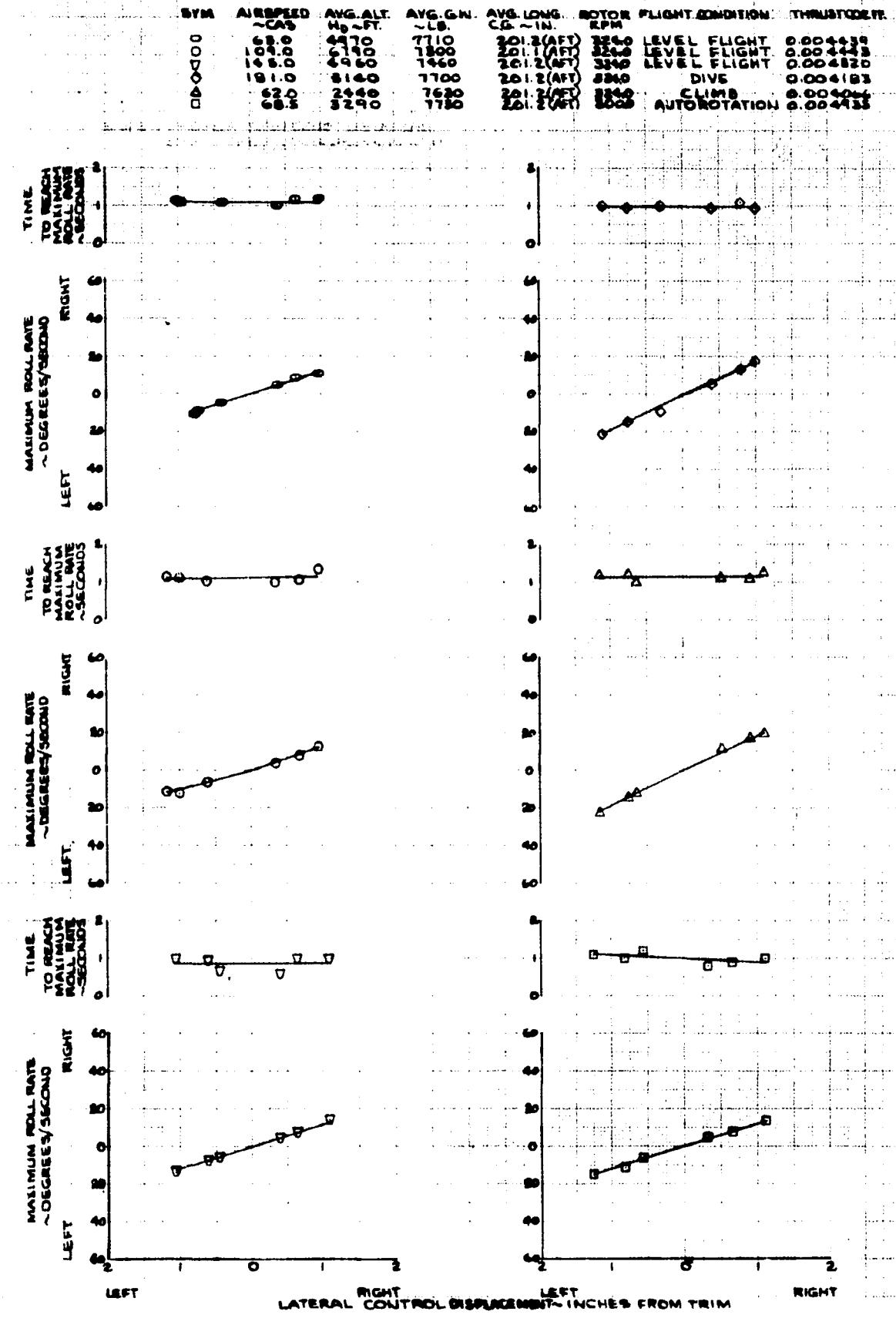


FIGURE NO. 194
LATERAL RESPONSE AT ONE SECOND
 -AH-1G USAF/TIGRE
 CLEAN CONFIGURATION

SYNTH.	AIR SPEED ~CAS	Avg. ALT. H ₀ ~ FT	Avg. G-W. ~LB	Avg. LOAD. C.G. ~IN.	MOTOR SELENT CONDITION	ROLL RATE ~CT
O	63.0	4970	7710	201.2(AFT)	SCAS LEVEL FLIGHT	0.004037
O	104.0	6790	7500	201.1(AFT)	SCAS LEVEL FLIGHT	0.004483
O	145.0	4950	1960	201.2(AFD)	SCAS LEVEL FLIGHT	0.004326
O	186.0	3140	7100	201.2(AFT)	SCAS DIVE	0.004183
O	227.0	2440	7650	201.2(AFT)	SCAS CLIMB	0.004016
O	68.0	8290	7730	201.2(AFT)	SCAS AUTOROTATION	0.004136

NOTE: OPEN SYMBOLS DENOTE SCAS ON
 SOLID SYMBOLS DENOTE SCAS OFF

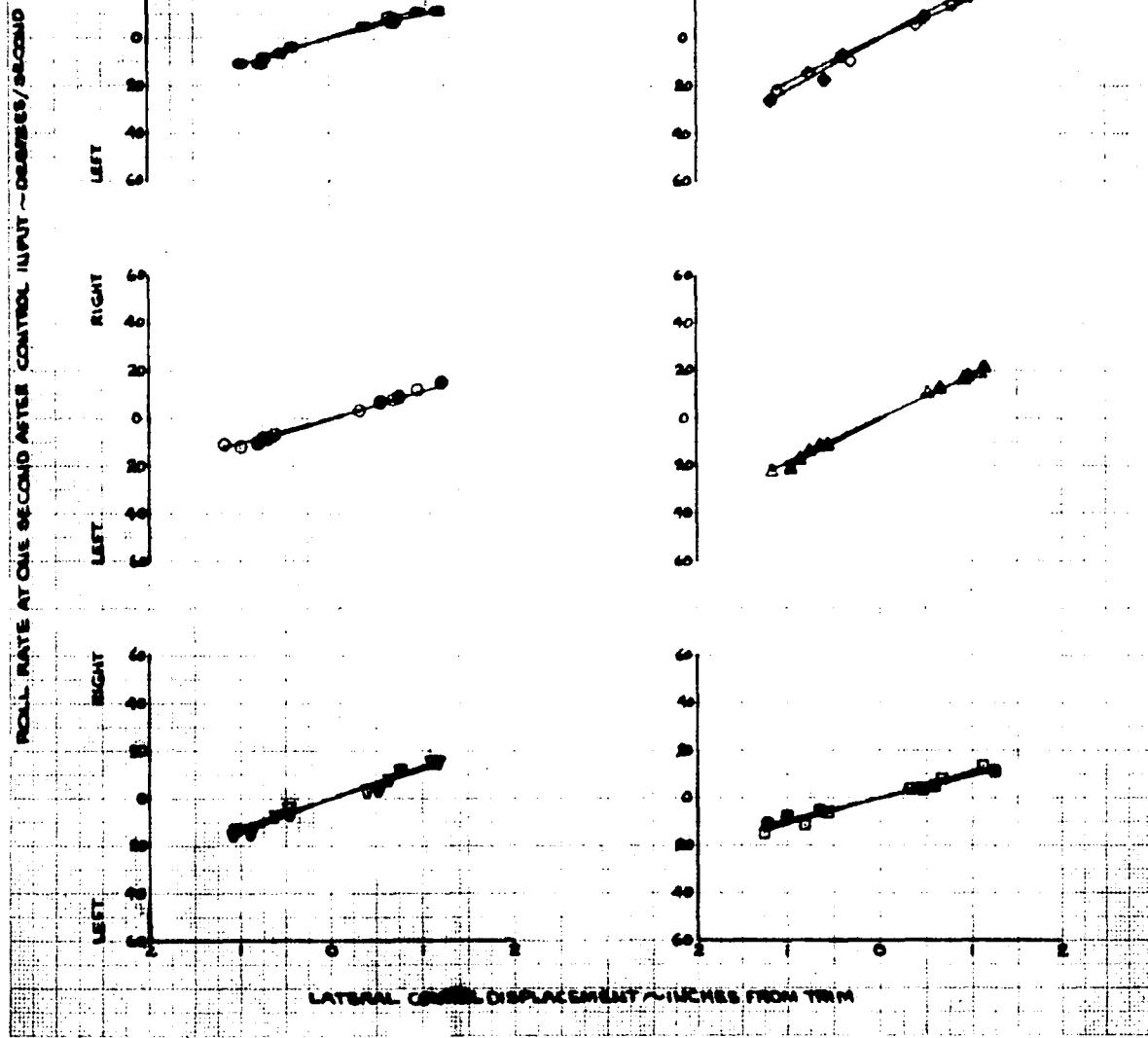


FIGURE NO. 195
ANGULAR ROLL DISPLACEMENT
AM-10 USAF 6715678
CLEAN CONFIGURATION

SYM. AIRSPEED AVG. ALT. AVG. L.G. AVG. LONG. MOTOR FLIGHT CONDITION THRUST COEF.
 ~CAS H_g-FT. ~LB. C.G. ~IN. RPM ~C_T
 □ 68.0 4910 7710 201.2(AFT) 3240 LEVEL FLIGHT 0.004481
 □ 107.0 6790 7700 201.2(AFT) 3240 LEVEL FLIGHT 0.004443
 □ 143.0 4960 7760 201.2(AFT) 3240 LEVEL FLIGHT 0.004480
 □ 161.0 3140 7700 201.2(AFT) 3240 DIVE 0.004183
 ▲ 62.0 2440 7620 201.2(AFT) 3240 CLIMB 0.004066
 □ 68.0 3290 7780 201.2(AFT) 3240 AUTOROTATION 0.004485

NOTE: OPEN SYMBOLS DENOTE SCAS ON
 SOLID SYMBOLS DENOTE SCAS OFF

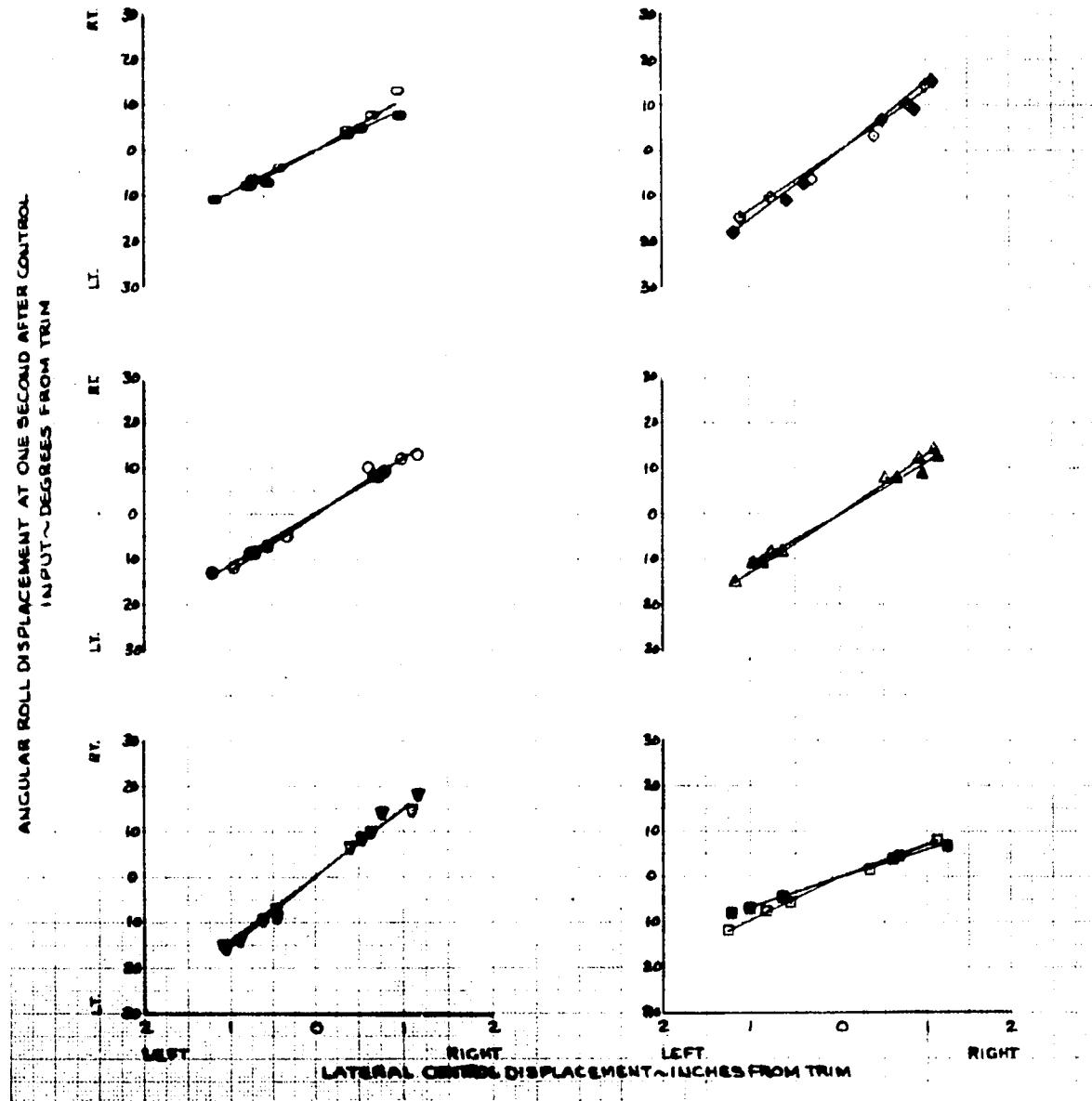
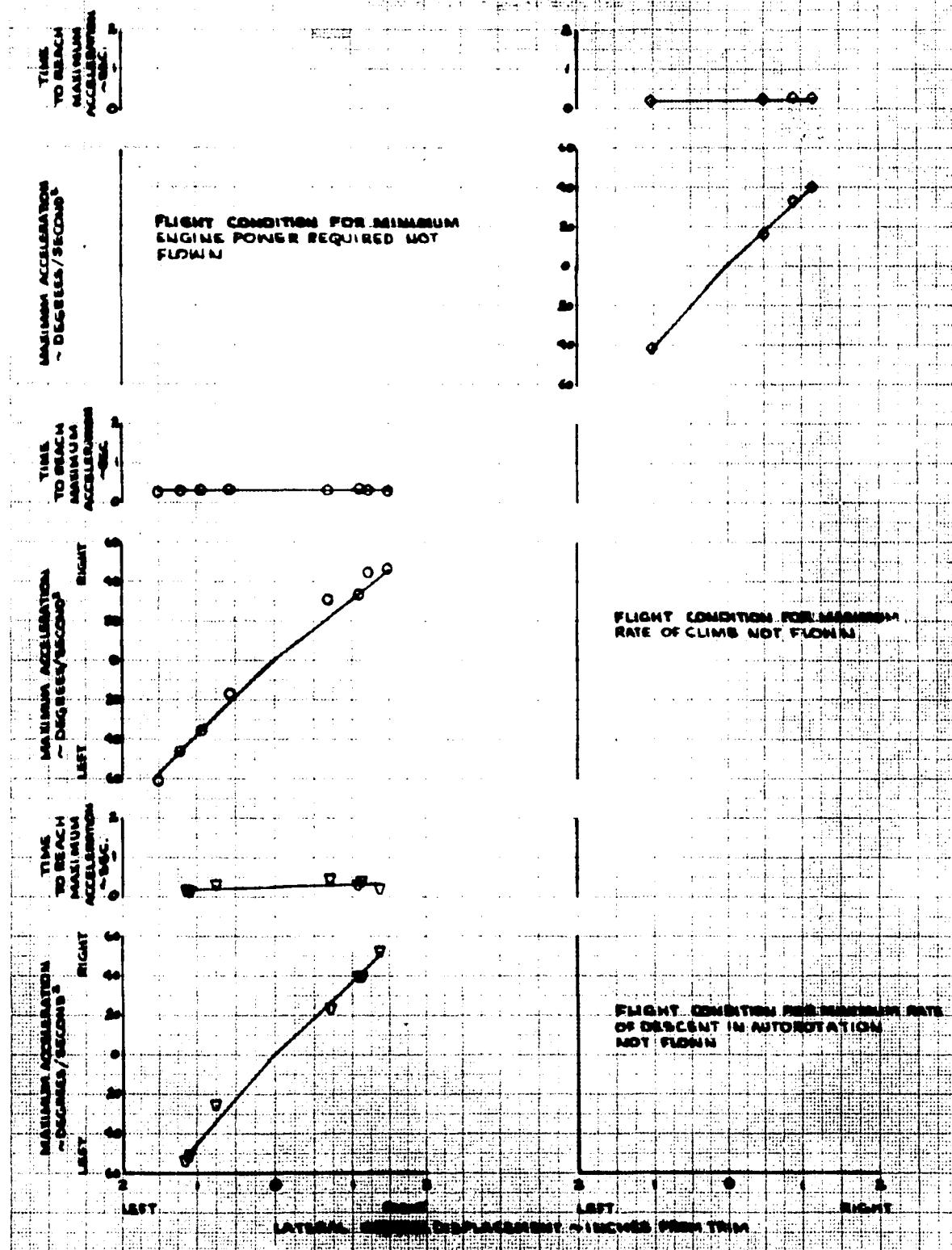


FIGURE NO. 196
LATERAL CONTROL SENSITIVITY
 AH-1G USA N4994T
 CLEAN CONFIGURATION WITH LANDING GEAR DOWN TIRE SWINGING REMOVED
 SEAS ON

WING AIRSPEED	Avg. ALT.	Avg. GMA	Avg. LOAD	ROTOR FLIGHT COEF. THRUST COEF.	
~ CAS	M _{0.77}	~ 10	C.G. ~ M _{0.5}	~ CT	
0	116.0	3760	8800	88.6(GST)	88.6 LEVEL FLIGHT 0.004674
0	145.5	3760	6100	142.6(GST)	6100 LEVEL FLIGHT 0.004661
0	169.0	8090	8870	192.4(GST)	8870 DIVE 0.004661



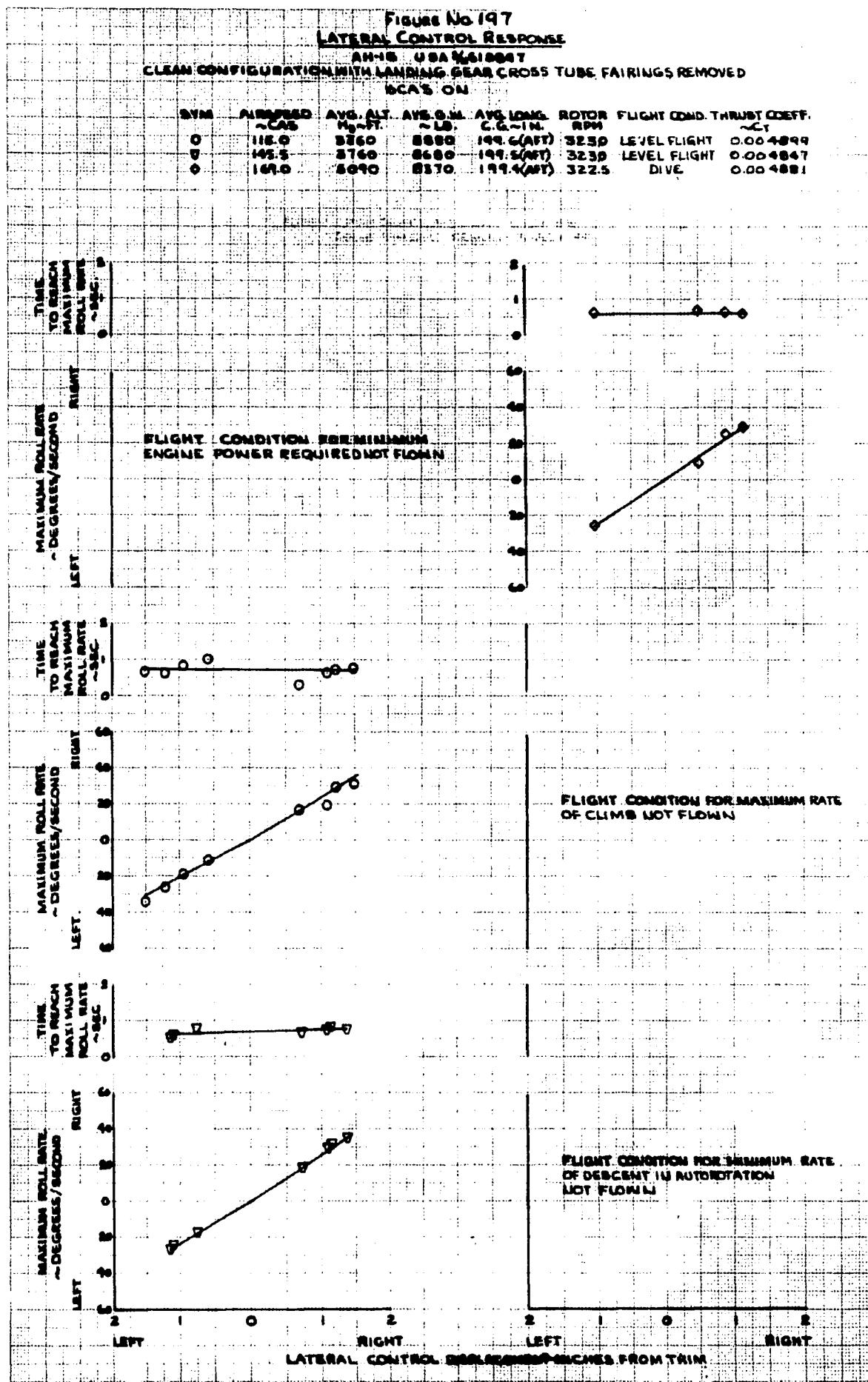


FIGURE NO. 198
LATERAL RESPONSE AT ONE SECOND

**AM-1G USA 261525Z
 CLEAN CONFIGURATION WITH LANDING GEAR CROSS TUBE FAIRINGS REMOVED
 SCAS ON**

SYM.	AIR SPEED ~CAS	Avg. ALT. Hg ~FT.	Avg. G.M. ~LB.	Avg. LONG. C.G. ~IN.	ROT. RPM	FLIGHT COND.	THRUST COEFF.	CY
O	116.0	3860	6880	199.6(AFT)	3230	LEVEL FLIGHT	0.004899	
O	145.5	3760	6680	199.6(AFT)	3230	LEVEL FLIGHT	0.004841	
O	169.0	5090	6370	199.4(AFT)	3225	DIVE	0.004881	

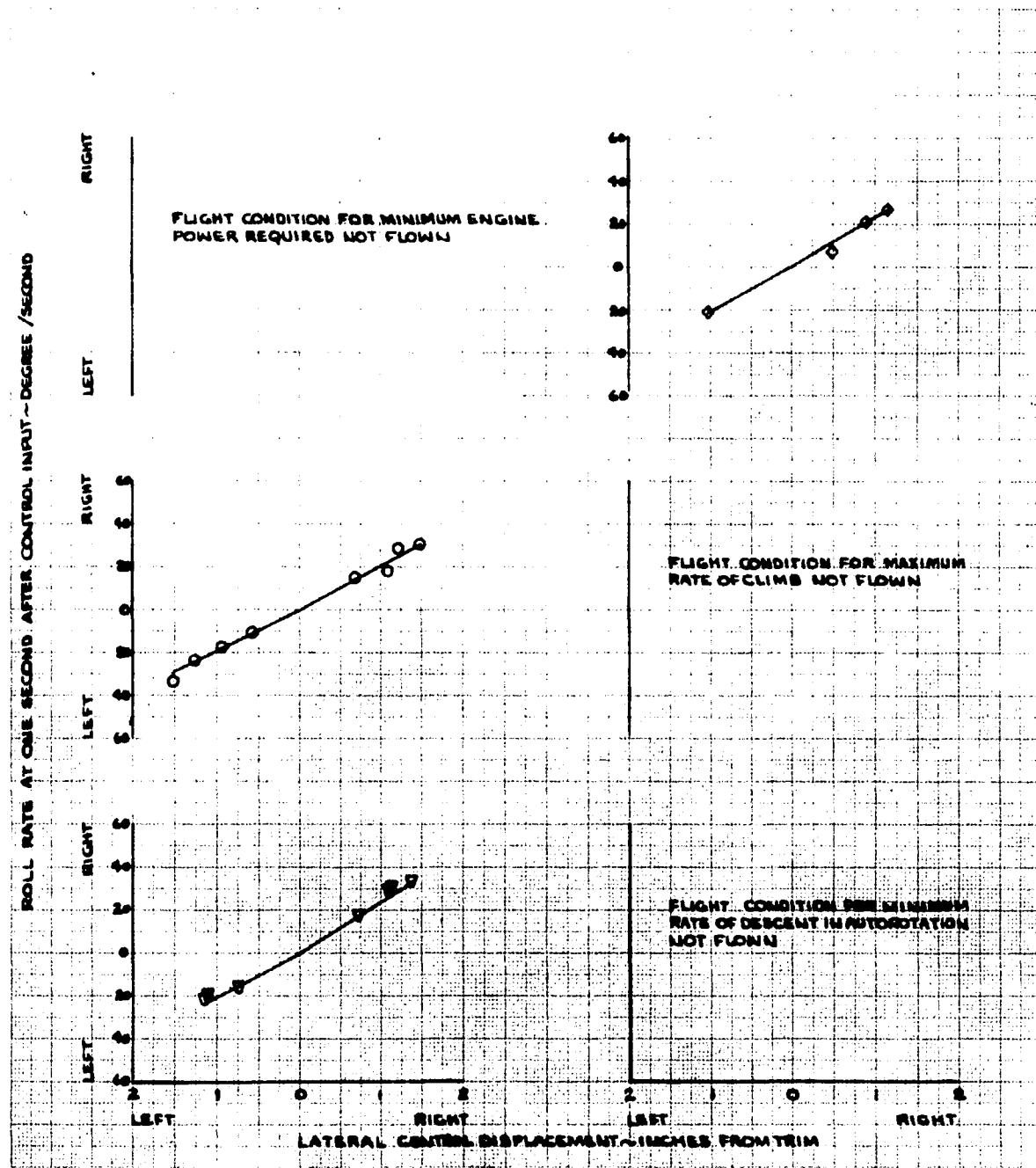


FIGURE NO. 199
ANGULAR ROLL DISPLACEMENT

AH-1G USA #618207
 CLEAN CONFIGURATION WITH LANDING GEAR CROSS TUBE FAIRINGS REMOVED
 SCAS ON

SVM	AIR SPEED ~CAS	Avg. ALT. Hr ~FT	Avg. G.W. ~LB.	Avg. LONG. MOM. IN.	ROT. RPM	FLIGHT COND.	THRUST COEFF. ~CT
0	116.0	3360	8880	199.6(FT)	3230	LEVEL FLIGHT	0.004899
0.50	146.5	8760	8880	199.6(FT)	3230	LEVEL FLIGHT	0.004847
0	169.0	5000	8870	199.4(FT)	322.5	DIVE	0.004881

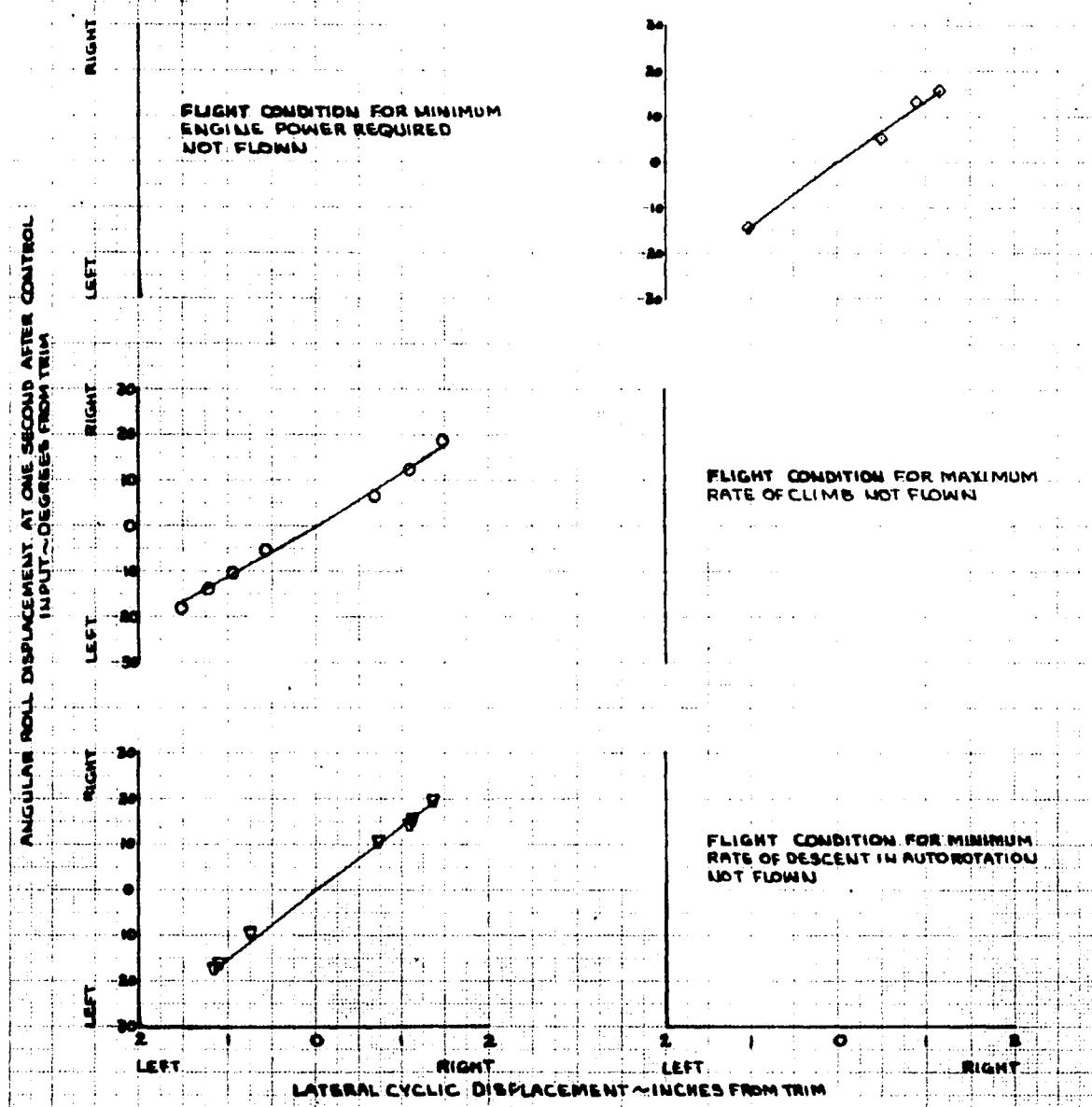


FIGURE NO. 200
LATERAL CONTROL SENSITIVITY

AL-1G USA KT 18695
MVY. SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED
SCAST ON

SVM	AIR SPEED	AVG. ALT.	AVG. SW.	AVG. LONG.	MOTOR	FLIGHT CONDITION	THRUST COEF.
~CAS	HD.-FT	~LB.	C.G.-IN.	RPM			~CT.
0	105.0	5770	9070	200.3(AFT)	3240	LEVEL FLIGHT	0.005350
0	143.0	5490	9240	200.2(AFT)	3240	LEVEL FLIGHT	0.005404
0	172.0	6310	9440	200.0(AFT)	3240	DIVE	0.005661
4	58.0	2870	9480	300.0(AFT)	3240	CLIMB	0.006124

NOTE: 0.01 LB. IN. OUT OF ROCKET PODS

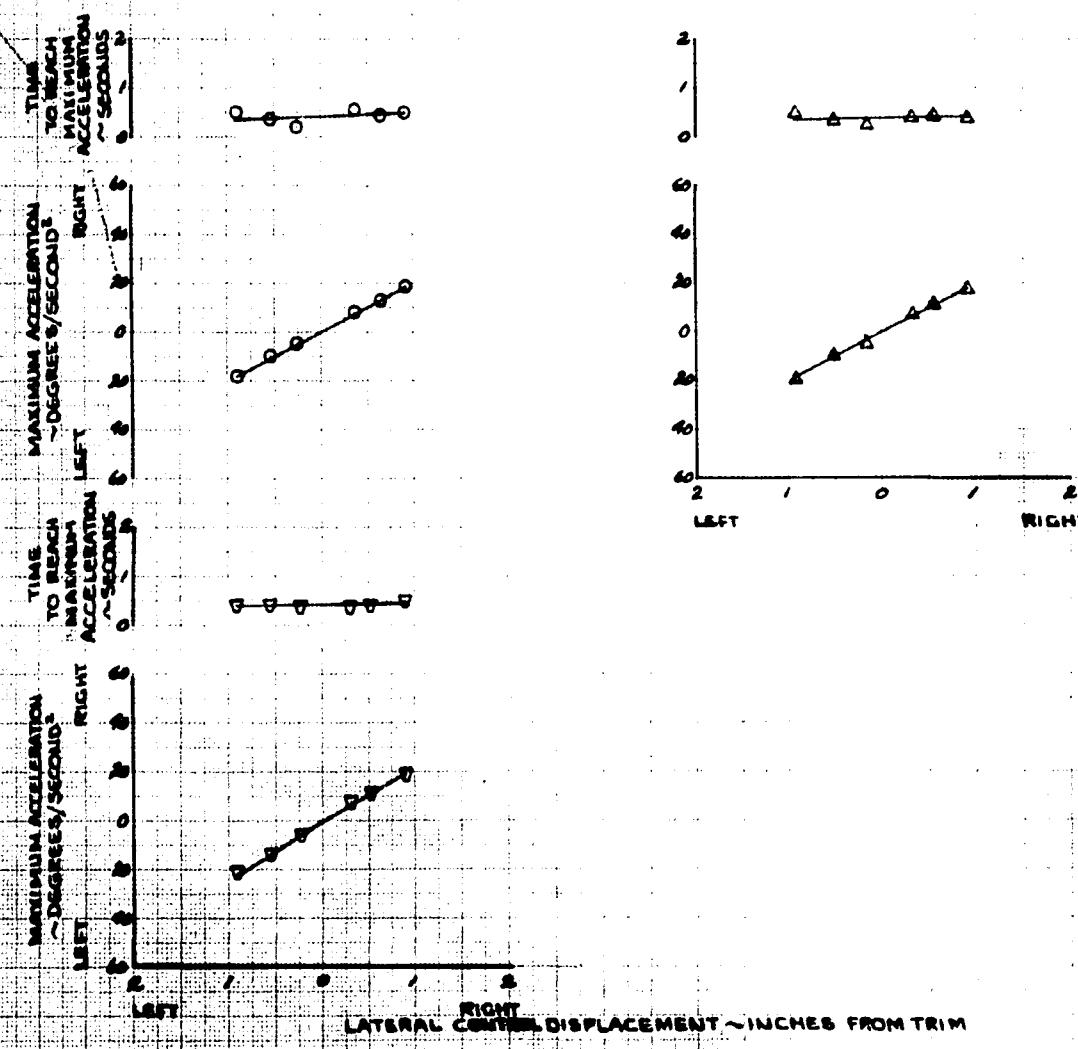


FIGURE NO. 201
LATERAL CONTROL RESPONSE

AM-10 USA971565
MV. SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED
SCAB ON

SYM.	AIRSPD.	Avg. ALT. ~CAS	Avg. G.W. lb	Avg. LONG. MOTOR	WING SPAN	THRUST COEFF. ~CT
O	105.0	6770	9070	200.2(AFT)	32.60	LEVEL FLIGHT 0.005350
O	143.0	5490	9240	200.2(AFT)	32.60	LEVEL FLIGHT 0.005404
O	172.0	6310	9440	200.2(AFT)	32.60	DIVE 0.005661
A	88.0	2070	9160	200.0(AFT)	32.60	CLIMB 0.005124

NOTE: 811 LB IN OUTTED ROCKET POD

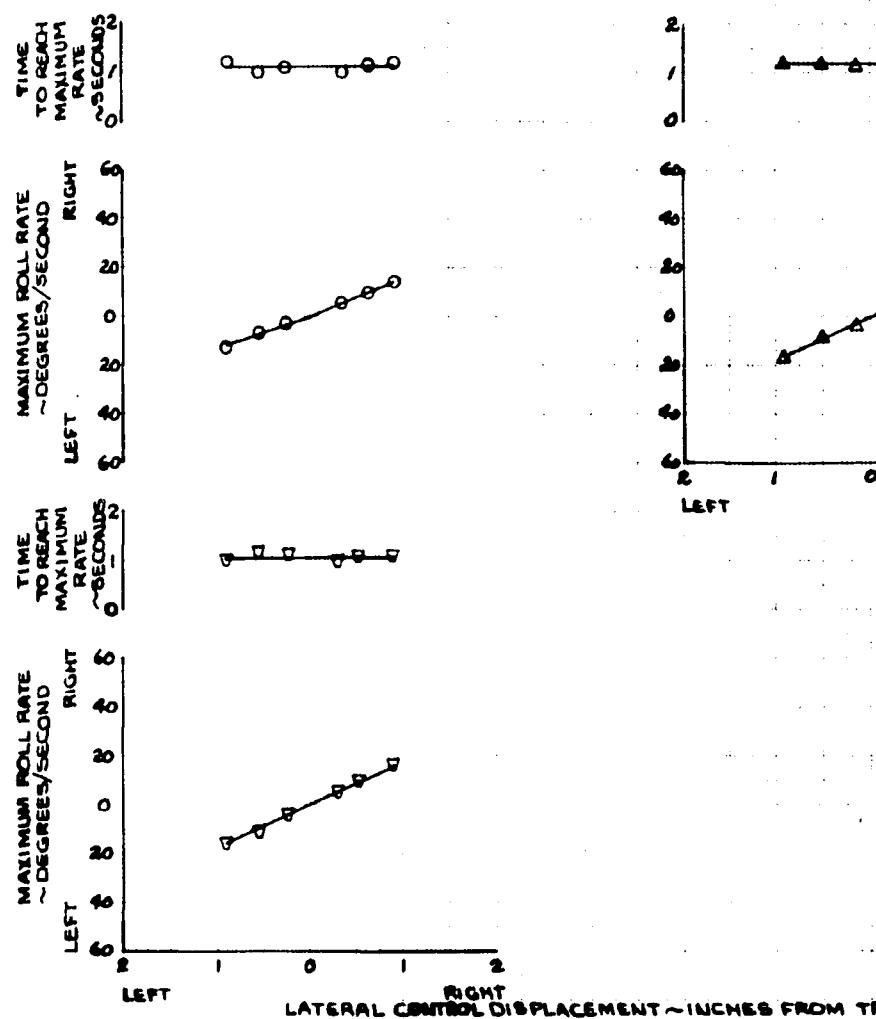
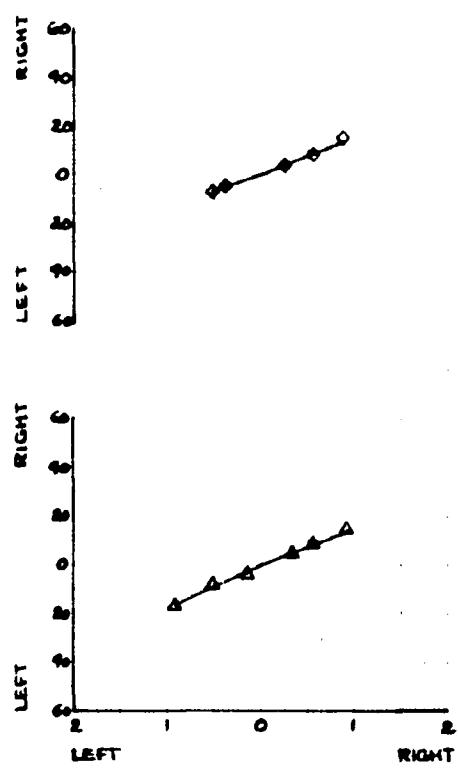
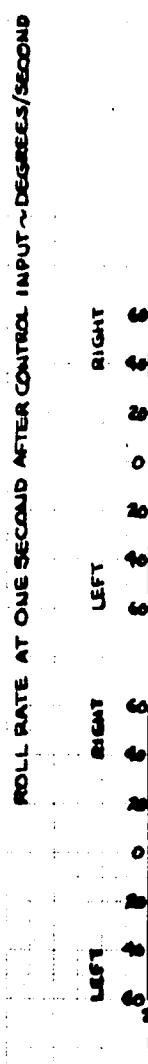


FIGURE NO. 202
LATERAL RESPONSE AT ONE SECOND

AH-1G USAF/T18695
 HVY. SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED
 SCAS ON

SYM	AIRSPEED ~CAS	Avg. ALT. MDAFT	Avg. G.W. ~LB	Avg. LONG. MOTOR	FLIGHT COMBINATION	THRUST COEF.	~CT
0	1060	5770	9070	200.0(AFT)	3240	LEVEL FLIGHT	0.005880
5	1430	5490	9240	200.2(AFT)	3240	LEVEL FLIGHT	0.005404
9	1720	6210	9460	200.0(AFT)	3240	DIVE	0.003661
A	880	2670	9480	200.0(AFT)	3240	CLIMB	0.005124

NOTE : 817 LB. IM OUTBD. ROCKET PODS



LATERAL CONTROL DISPLACEMENT ~ INCHES FROM TRIM

FIGURE NO. 205

ANGULAR ROLL DISPLACEMENT

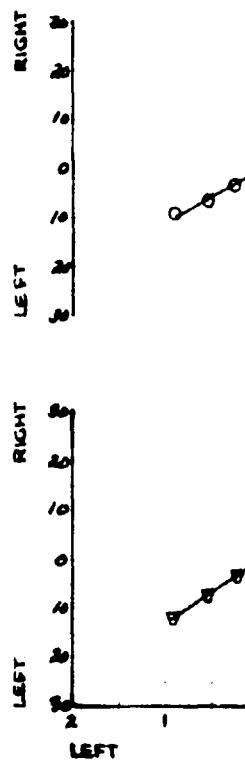
AH-1G USAF 971869B

HVV. SCOUT CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED
SCAB ON

SYM	AIR SPEED	AVG ALT.	AVG G.M.	AVG LONG. ROTOR RPM	FLIGHT CONDITION	THRUST COEFF
	~CAS	H ₀ -FT	~LB.	C.G. ~IN	RPM	~C _T
0	1050	5770	9070	200.3(FT)	324.0 LEVEL FLIGHT	0.008850
5	1480	5440	9240	200.2(FT)	384.0 LEVEL FLIGHT	0.005404
9	1720	6310	9440	200.0(FT)	324.0 DIVE	0.005661
8	580	2870	9480	200.0(FT)	324.0 CLIMB	0.005124

NOTE: 817 LB IN OUTBOARD ROCKET PODS

ANGULAR ROLL DISPLACEMENT AT ONE SECOND AFTER CONTROL INPUT - DEGREES FROM TRIM



LATERAL CONTROL DISPLACEMENT ~ INCHES FROM TRIM

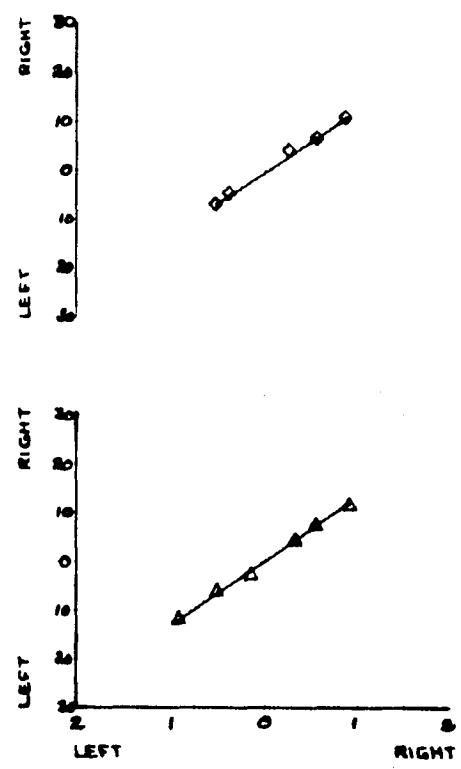


FIGURE NO. 204
LATERAL CONTROL SENSITIVITY
 AH-1G USAF 6715675
 HVY. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM	AIR SPEED ~CAS	Avg. Alt. Hg ~FT.	Avg. G.M. ~LB.	Avg. Long. C.G. ~IN.	MOTOR FLIGHT CONDITION	THRUST COEF.
					RPM	-CY
O	63.0	3970	8790	195.1(MID)	3250	LEVEL FLIGHT 0.004679
O	106.0	5160	8580	195.1(MID)	3220	LEVEL FLIGHT 0.004704
D	146.5	5740	8550	195.0(MID)	324.5	LEVEL FLIGHT 0.005024
O	172.0	8180	8680	195.2(MID)	8260	DIVE 0.005515
A	60.0	1550	8450	195.0(MID)	8260	CLIMB 0.004749
O	67.0	6480	8460	195.0(MID)	3100	AUTOROTATION 0.003873

NOTES: 1. OPEN SYMBOLS DENOTE SCAB ON
 2. SOLID SYMBOLS DENOTE SCAB OFF
 3. ALL ROCKET PODS EMPTY

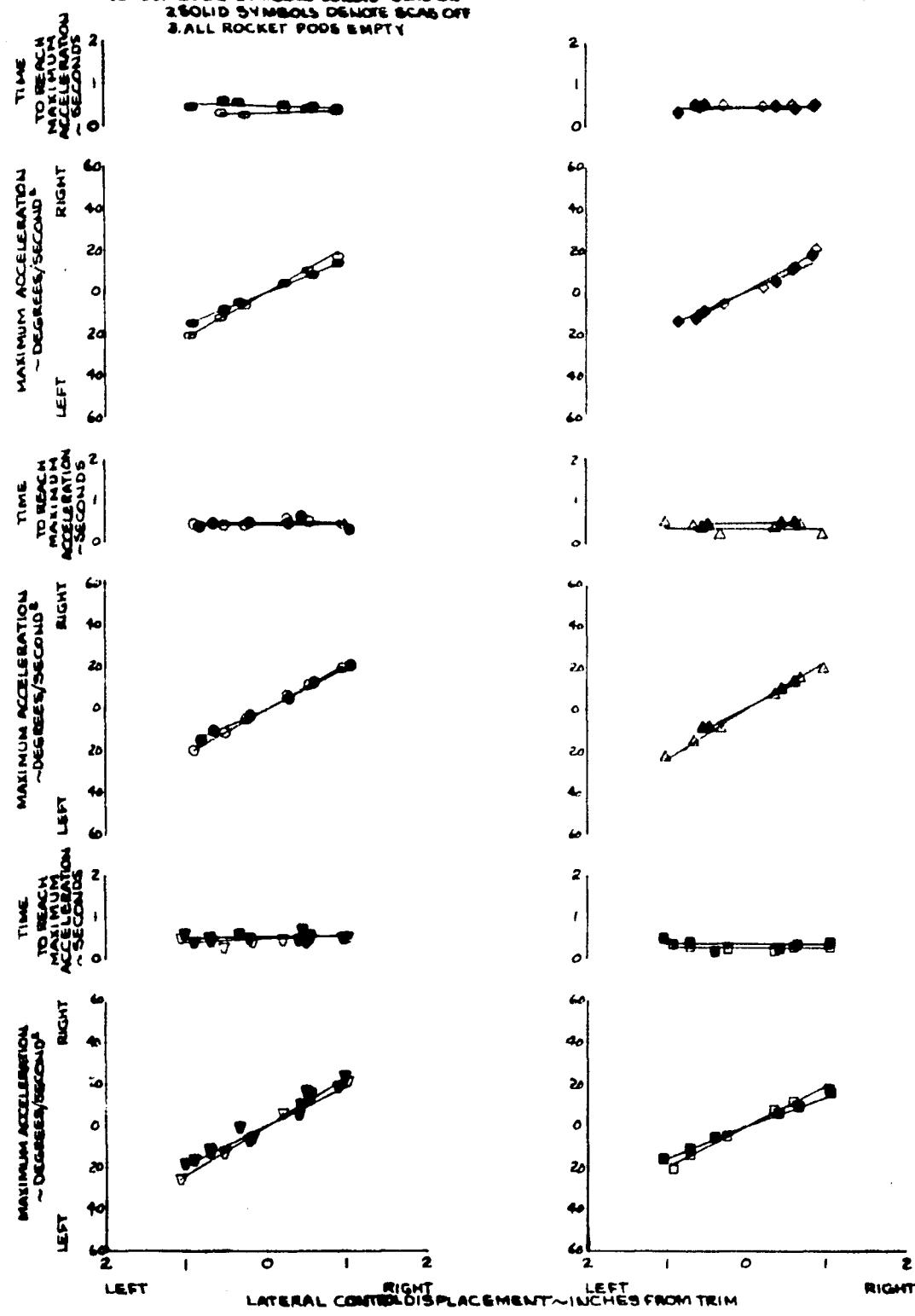


FIGURE NO. 205
LATERAL CONTROL RESPONSE

AH-1G USAF/N16698
 HVT. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED
 SCAS ON

STM	AIRSPD ~CAS	Avg. ALT. M.-FT.	Avg. G.W. LB.	Avg. LONG. C.G. ~IN.	ROUTE FLIGHT COMBINATION THRU CHTS	TIME ~SEC.
00	68.0	3970	8790	195.1(MID)	3258 LEVEL FLIGHT 0.00 48719	
00	108.0	5160	8580	195.0(MID)	3248 LEVEL FLIGHT 0.00 48024	
00	146.8	5740	8550	195.0(MID)	3245 LEVEL FLIGHT 0.00 50224	
00	172.0	6180	8680	195.2(MID)	3246 DIVE 0.00 5615	
00	60.0	1580	8450	195.0(MID)	3246 CLIMB 0.00 4392	
00	67.0	6480	8460	195.0(MID)	3108 AUTOROTATION 0.00 6872	

NOTE : ALL PODS EMPTY

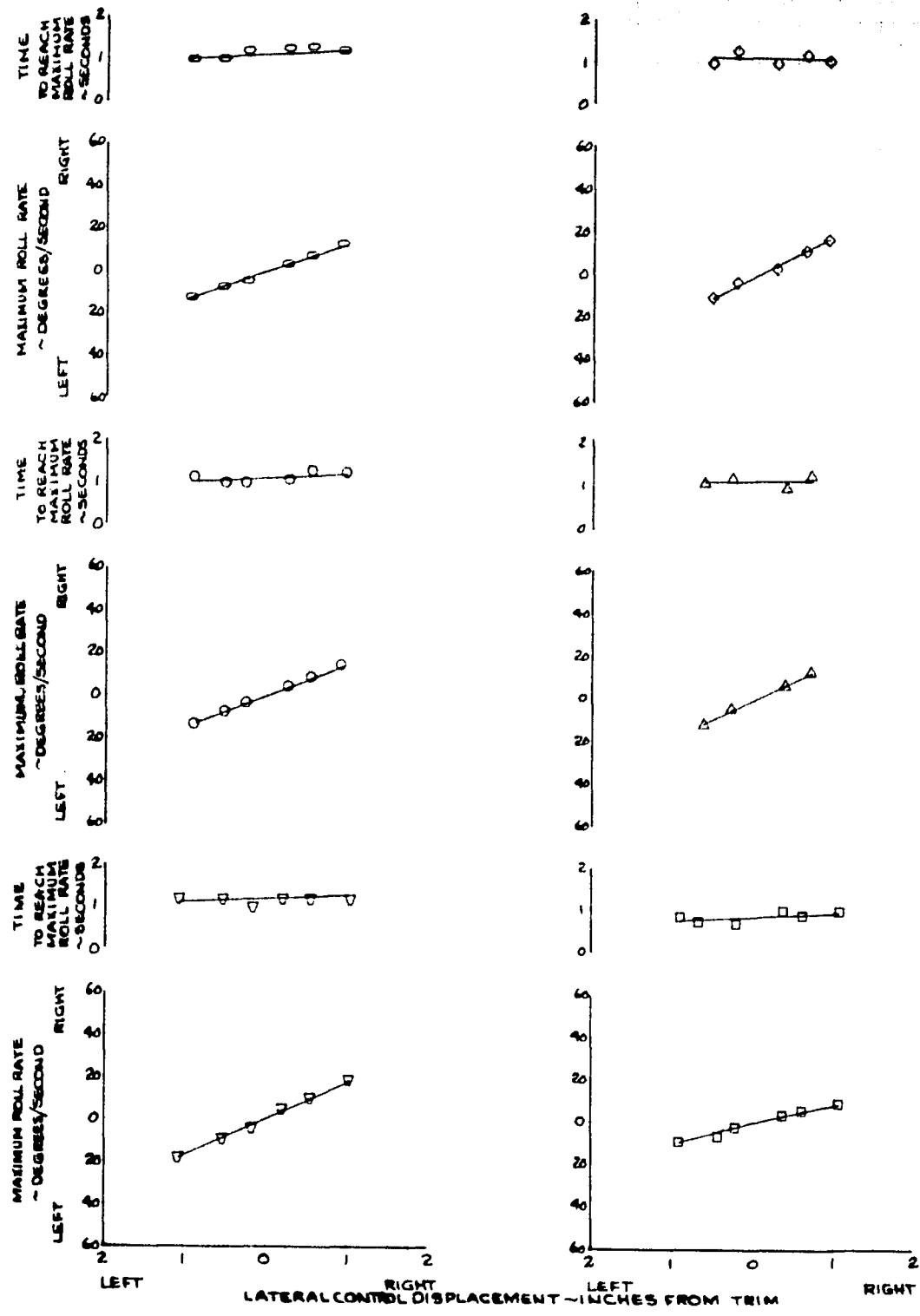


FIGURE NO. 206
LATERAL RESPONSE AT ONE SECOND
AH-1G USAF 6716698

HVV. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM	AIR SPEED KIAS	ANG. ALT. H-FT.	AVG. G-W	AVG. LONG. C.G.-IN.	MOTOR FLIGHT DURATION SEC/MIN CYCLE
O	62.0	5110	0.740	195.1(MIN)	324.0
O	103.0	3160	0.630	145.1(MIN)	322.8 LEVEL FLIGHT 0.00 507.9
O	146.8	5140	0.630	145.0(MIN)	322.8 LEVEL FLIGHT 0.00 502.6
O	172.0	5180	0.630	145.2(MIN)	DIVE 0.00 501.8
O	208.0	1550	0.450	195.0(MIN)	324.0 CLIMB 0.00 500.0
O	270	5480	0.460	195.0(MIN)	310.0 AUTOROTATION 0.00 37.7

NOTES: (1) OPEN SYMBOLS DENOTE SCAS ON
(2) SOLID SYMBOLS DENOTE SCAS OFF
(3) ALL ROCKET PODS EMPTY

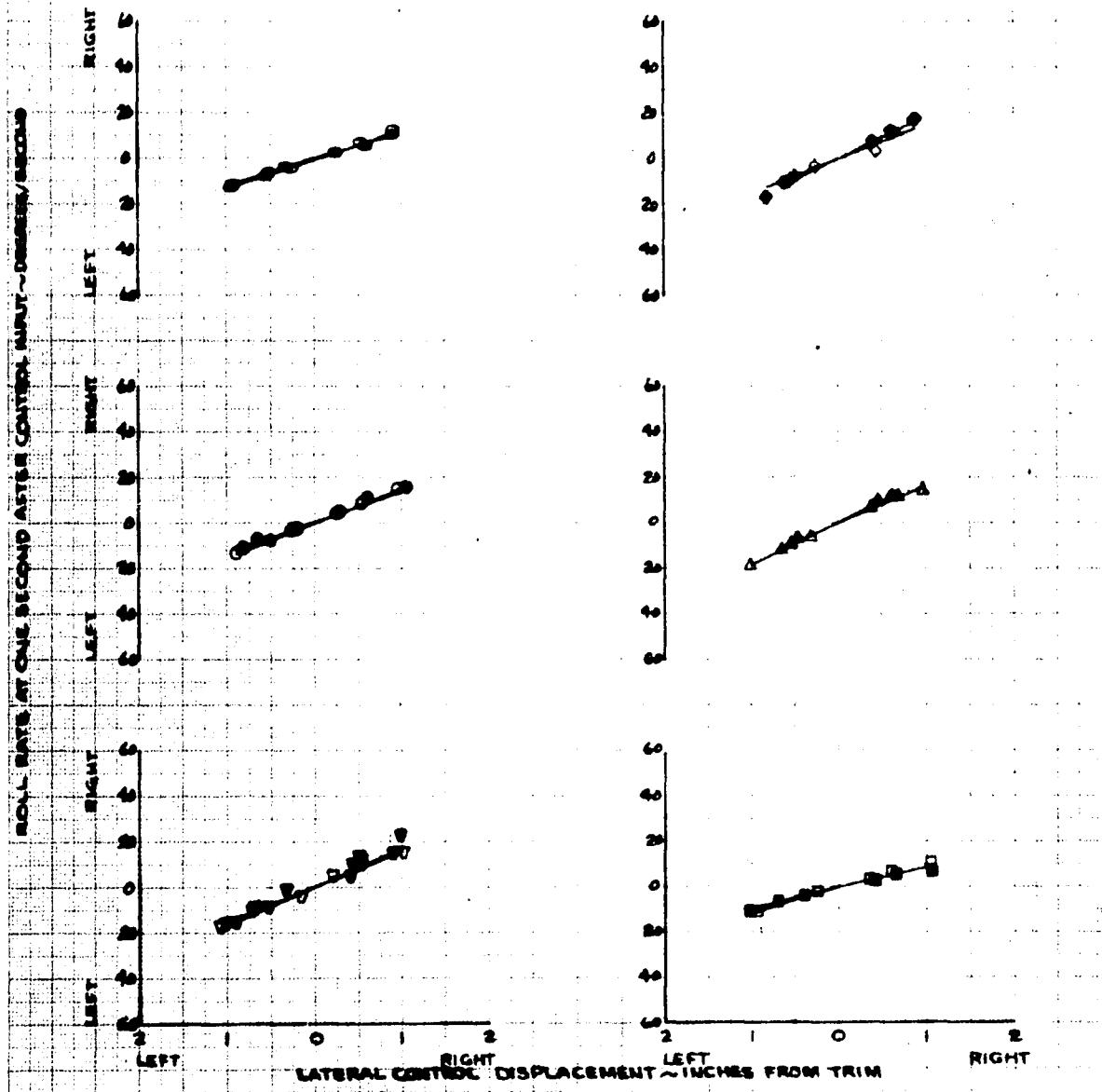


FIGURE NO. 207
ANGULAR ROLL DISPLACEMENT

AH-1G USA #115645
 HVT. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM.	AIRCRAFT	Avg. ALT. ~FT.	Avg. G-W.	Avg. LONG. ~IN.	MOTOR RPM	ANGLE OF DISPLACEMENT DEGREES
—○—	—○—	2970	0.120	195.0(MIN)	3250	LEVEL FLIGHT 0.004875
—○—	—○—	2160	0.120	195.0(MID)	3250	LEVEL FLIGHT 0.004804
—○—	—○—	1440	0.120	195.0(HIGH)	324.5	LEVEL FLIGHT 0.005024
—○—	—○—	1770	0.120	195.0(MIN)	324.0	DIVE 0.005515
—○—	—○—	880	0.120	195.0(MID)	324.0	CLIMB 0.006190
—○—	—○—	670	0.120	195.0(HIGH)	3100	AUTOROTATION 0.005573

NOTES: OPEN CIRCLE SYMBOLS DENOTE SCAS ON
 SOLID SYMBOLS DENOTE SCAS OFF
 ALL ROCKET PODS EMPTY

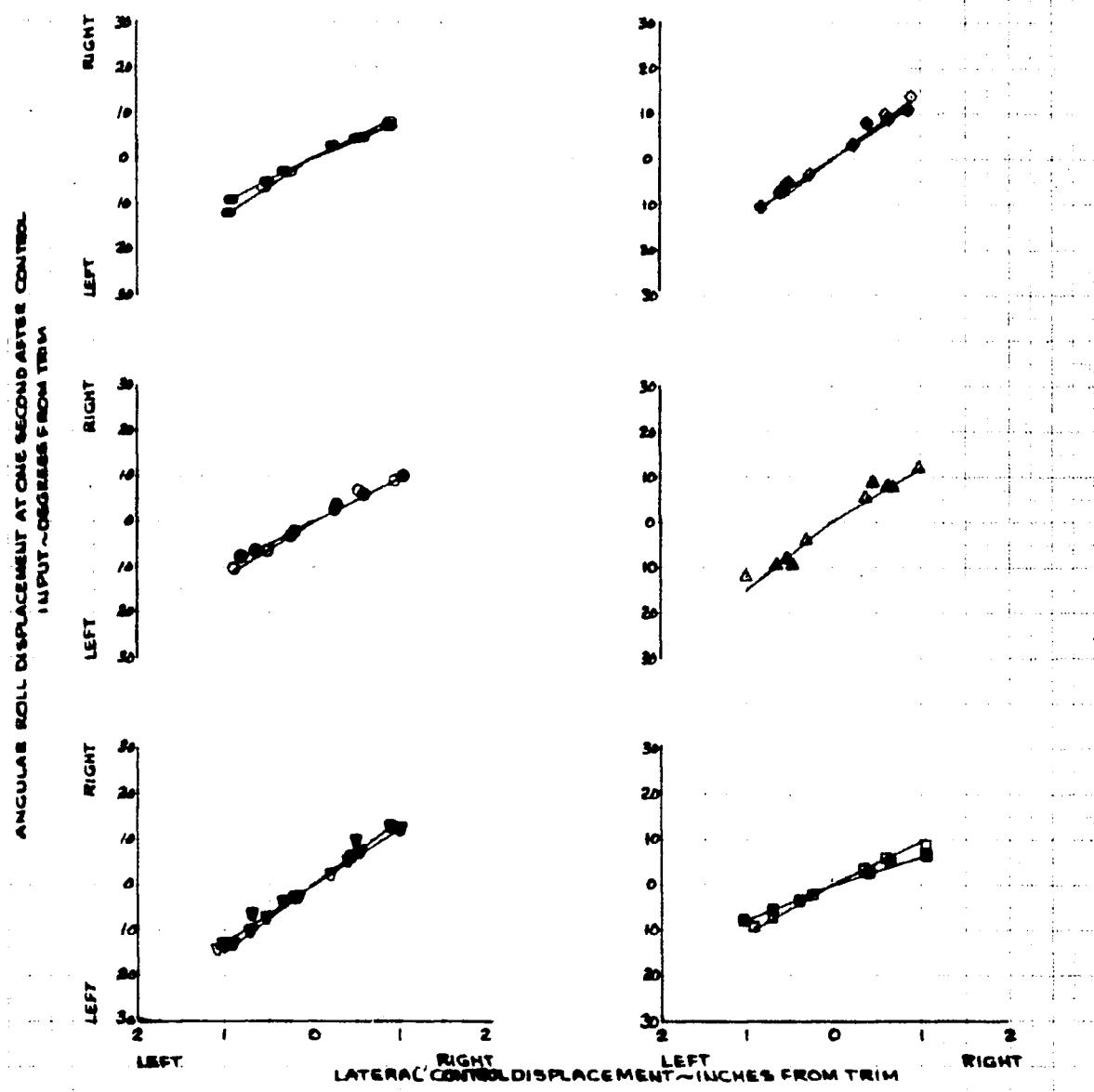
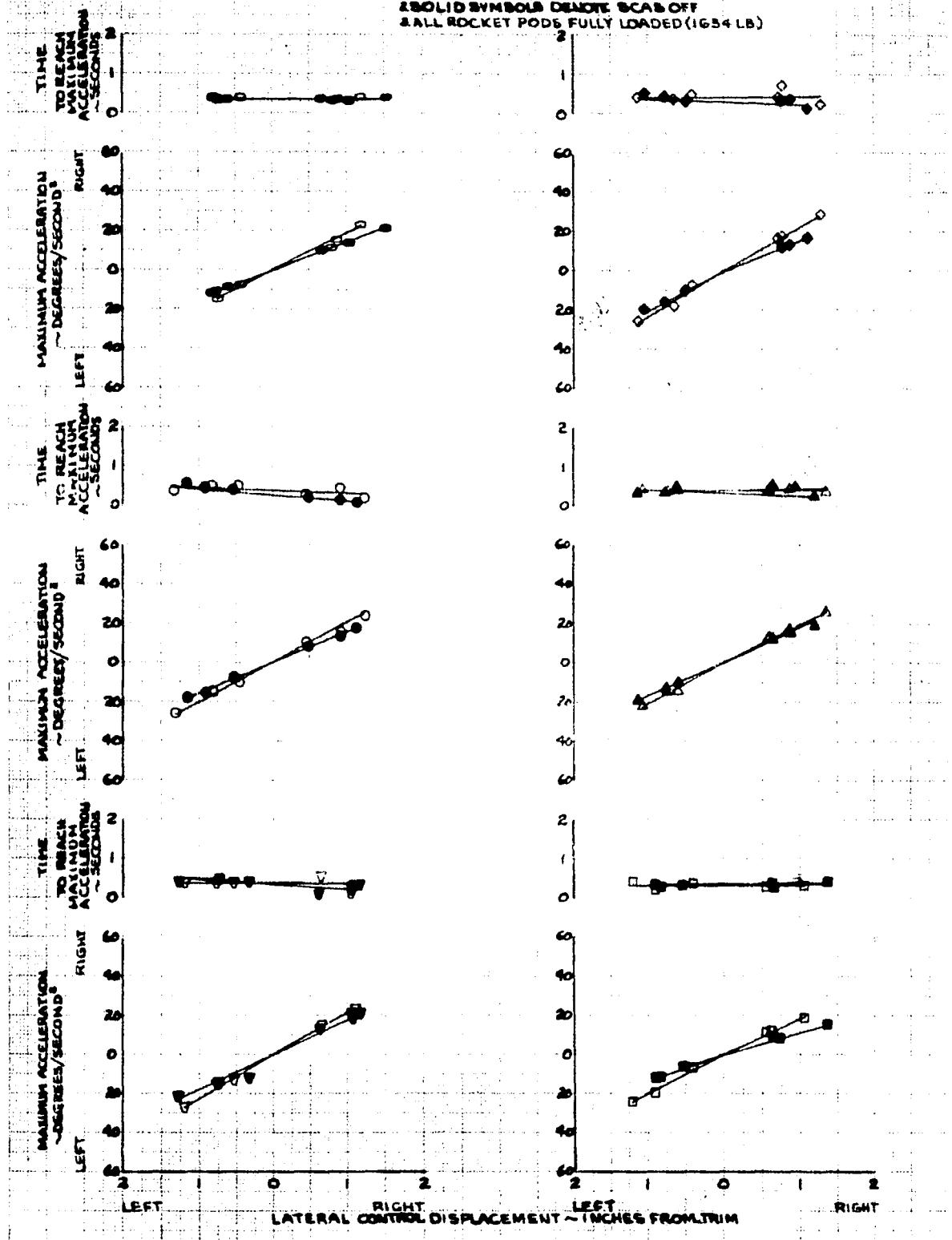


FIGURE NO. 208
LATERAL CONTROL SENSITIVITY
AM-10 USAFT13698

BVM	AIR SPEED ~CAS	AVG ALT. HGS - FT	AVG LONG. C.G. - IN.	MOTOR SPEED ~RPM	FLIGHT POSITION	THRUST COEFF - C _T
000	600	3150	1951	3240	LEVEL FLIGHT 0.00 4817	
000	1060	3630	1920	3240	LEVEL FLIGHT 0.00 4821	
000	1440	4100	1981	3240	LEVEL FLIGHT 0.00 4940	
000	1810	6680	1998	3240	DIVE 0.00 5192	
000	600	980	1975	3240	CLIMB 0.00 4625	
000	120	5580	1978	310.0	AUTO ROTATION 0.00 5766	

NOTE: OPEN SYMBOLS DENOTE SCAB ON
 & SOLID SYMBOLS DENOTE SCAB OFF
 & ALL ROCKET PODS FULLY LOADED (1634 LB)



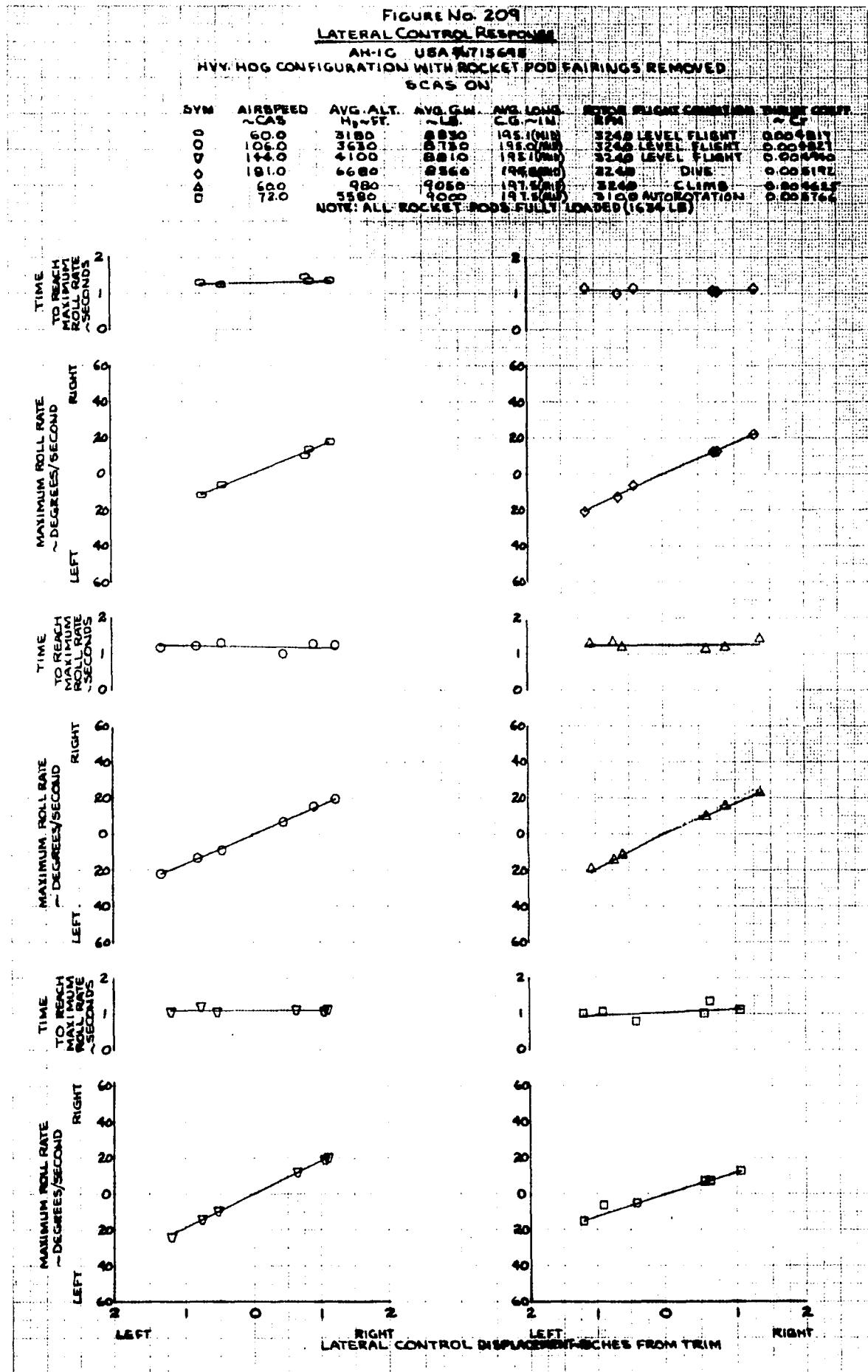


FIGURE NO. 210
LATERAL RESPONSE AT ONE SECOND

AM-1G USA 941864

HVV HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM	AIR SPEED ~CAS M _a ~FT.	AVG. ALT. ~LB.	AVG. GEAR C.G. ~IN.	ROT. FLGHT. SENSITIV.	THRUST CTRF. ~CP.
○	60.0	3150	9810	195.1(MID)	324.0
○	106.0	2680	8120	195.0(MID)	324.0
○	144.0	4100	8810	195.1(MID)	324.0
○	181.0	6680	8560	194.8(MID)	324.0
△	60.0	900	9050	197.5(MID)	324.0
□	72.0	5680	9000	197.4(MID)	310.0

NOTES: OPEN SYMBOLS DENOTE SCAS ON
2 SOLID SYMBOLS DENOTE SCAS OFF
3. ALL ROCKET PODS FULLY LOADED (163+LB)

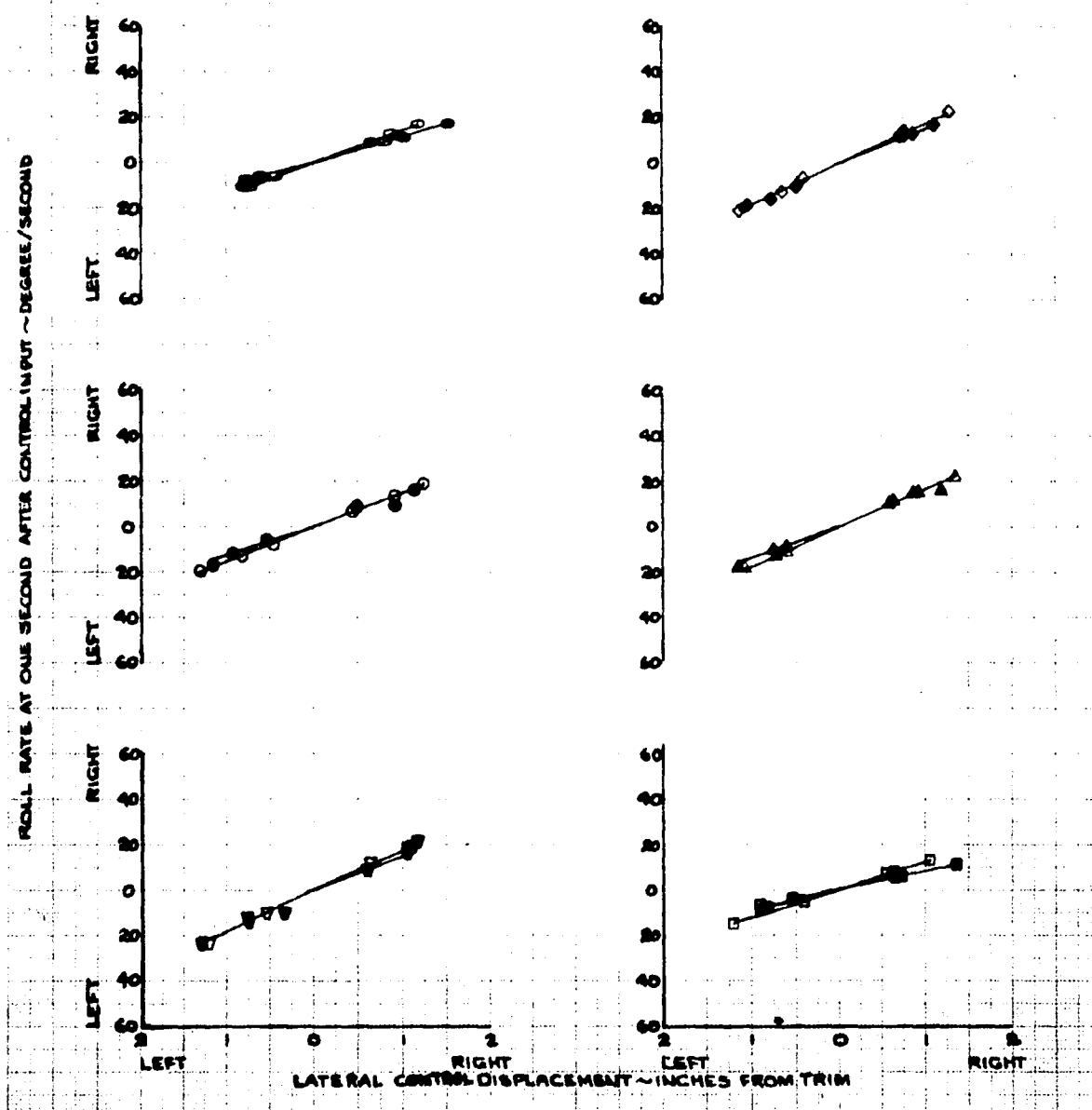
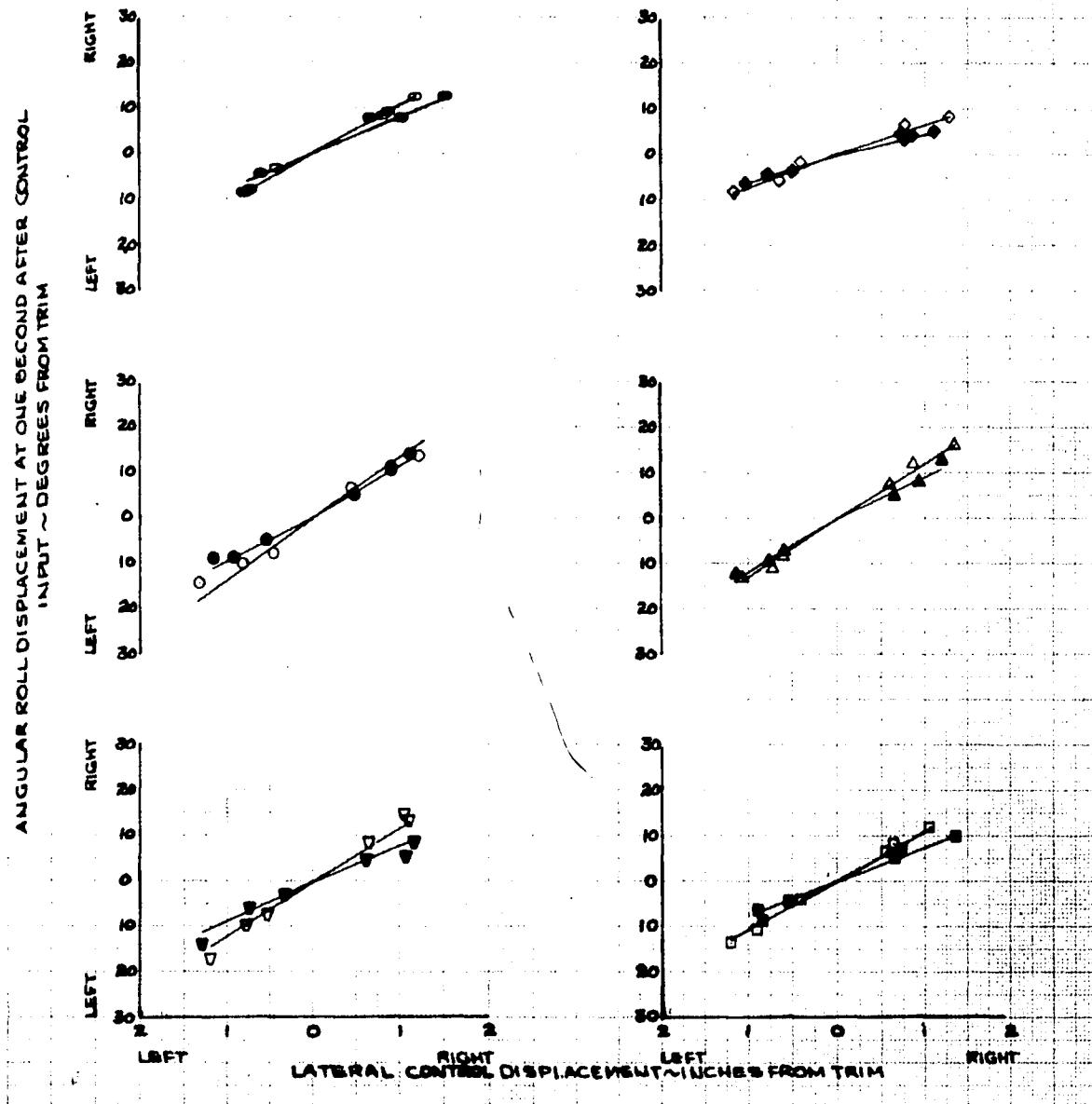


FIGURE NO. 211
ANGULAR ROLL DISPLACEMENT
AM-1G USAF TIGERS
HVV. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM	AIR SPEED ~CAS	AVG. ALT. HO-FT.	AVG. G.W. ~LB.	AVG. LONG. CG. ~IN.	MOTOR RPM	FLIGHT CONDITION	THRUST COEFF-C _T
○	600	2100	9000	192.1(MID)	3240	LEVEL FLIGHT	0.004817
○	1000	3600	9100	192.0(MID)	3240	LEVEL FLIGHT	0.004827
○	1400	4100	9010	192.1(MID)	3240	LEVEL FLIGHT	0.004840
○	1800	6000	8760	194.8(MID)	3240	DIVE	0.005192
○	600	900	9060	197.5(MID)	3240	CLIMB	0.004625
○	720	3500	9000	197.5(MID)	3100	AUTOROTATION	0.005766

NOTES: 1. OPEN SYMBOLS DENOTE SCAS ON
 2. SOLID SYMBOLS DENOTE SCAS OFF
 3. ALL ROCKET PODS FULLY LOADED (634 LB.)



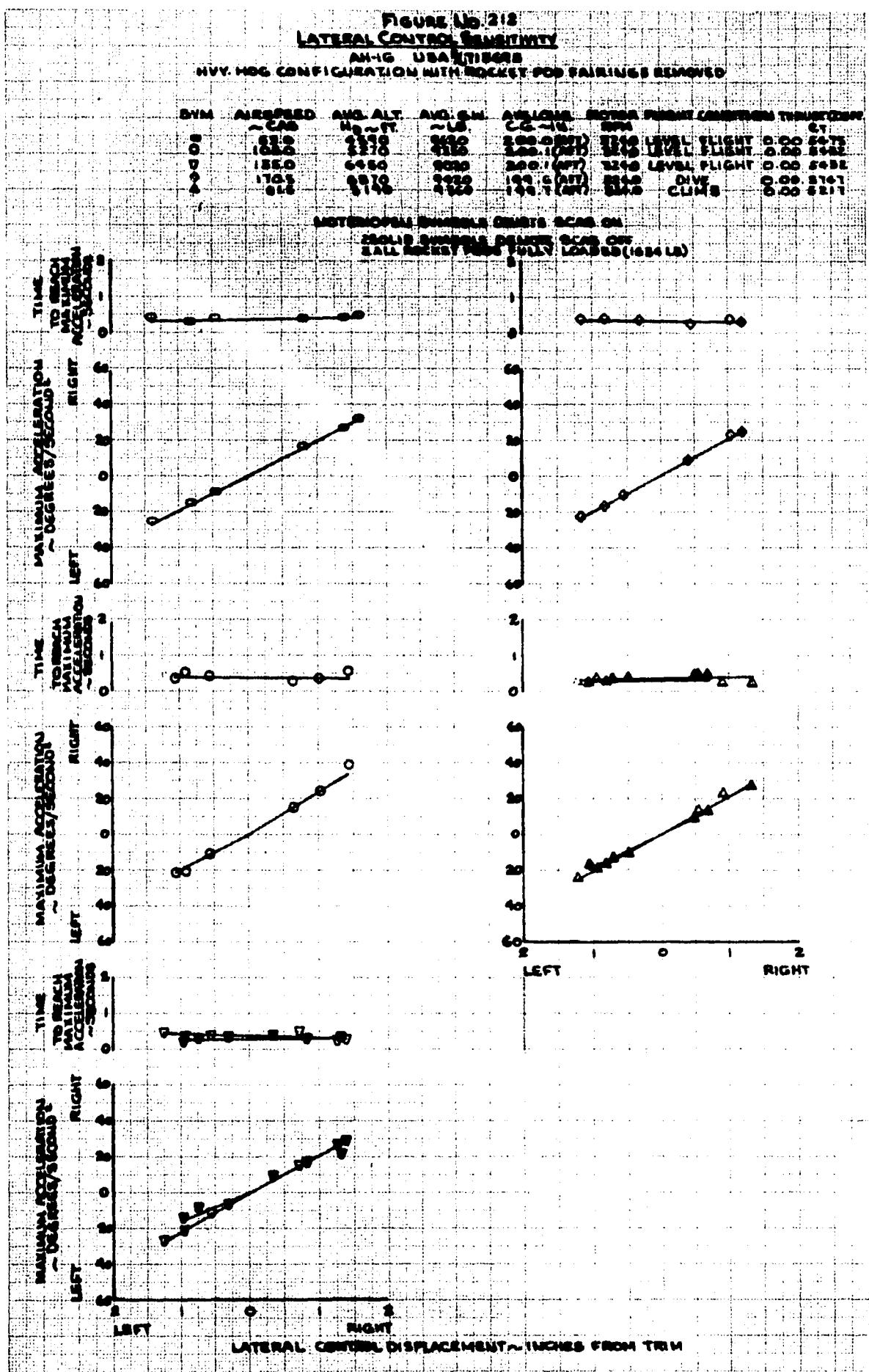
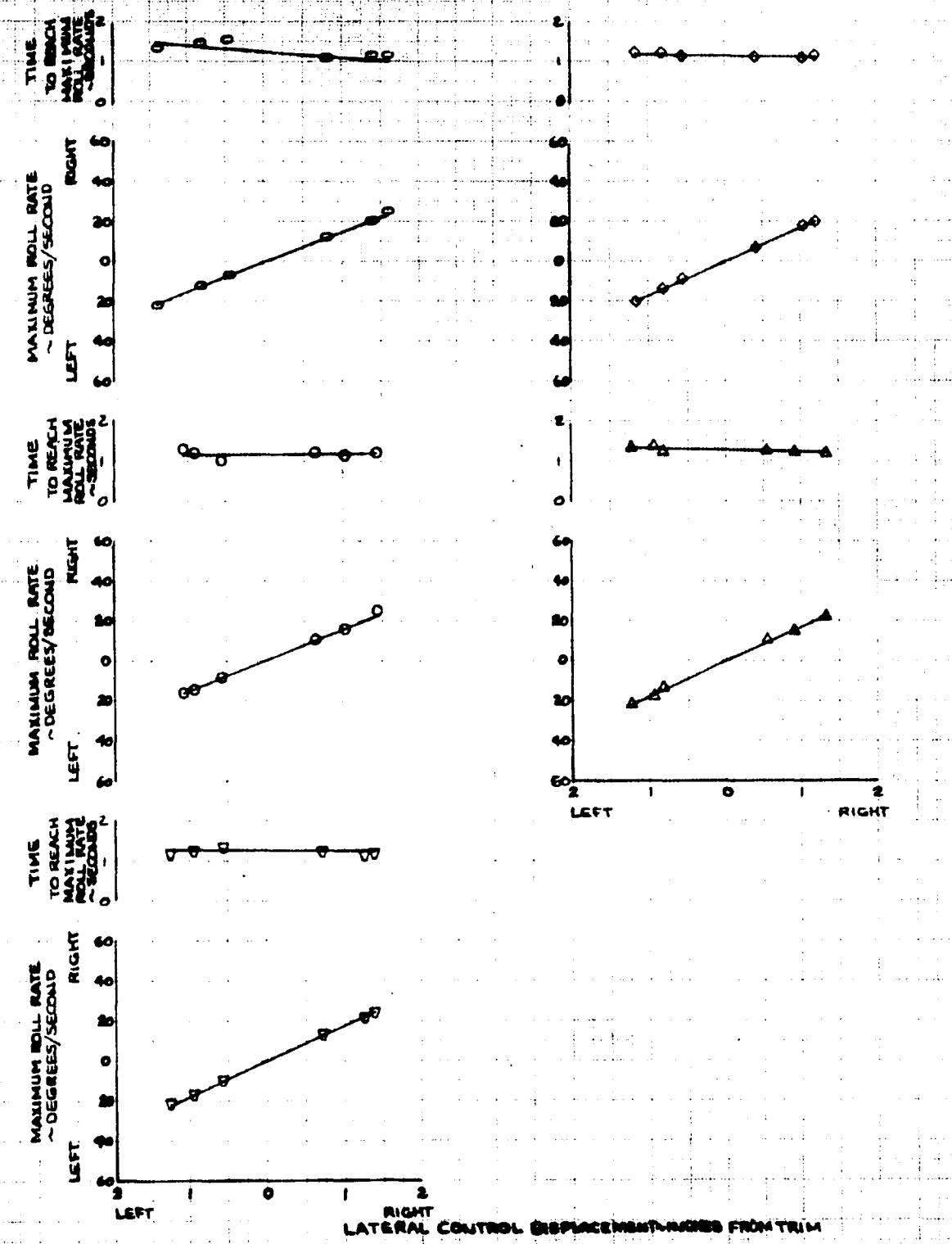


FIGURE No. 213

LATERAL CONTROL RESPONSE

AH-1G USA TITAN
MVY. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED
SCAB ON

BIN AIRSPEED ANG. ALT. ANG. G.M. ANG. LONG. MOTION FLIGHT CONDITION THRUST COEF.
 -CAB H₀ ~5° ~15° C.G. ~IM. RPM ~CT
 0 67.5 4590 6610 300.0(FT) 3200.0(FT) 3200.1(FT) 3200.1(FT) 0.00 5475
 0 108.0 5270 4820 300.1(FT) 3200.1(FT) 3200.1(FT) 3200.1(FT) 0.00 5432
 0 136.0 6450 4020 200.0(FT) 3200.0(FT) 3200.1(FT) 3200.1(FT) 0.00 5482
 0 170.5 6870 4420 199.6(FT) 3240 DIVE 0.00 5747
 A 01.5 3190 4560 189.7(FT) 3240 CLIMB 0.00 5217
 NOTE: ALL ROCKET PODS FULLY UNLOADED (1634 LB)



LATERAL CONTROL DISPLACEMENT MEASURED FROM TRIM

FIGURE NO. 214
LATERAL RESPONSE AT ONE SECOND

AH-1G USAF 118695
HVV. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM	AIRSPD	ANG. ALT.	ANG. S.H.	ANG. LONG.	MOTOR FLIGHT DURATION	THRST COEF.	CT
	-CAS	H ₀ - FT.	L ₀	C ₀ - IN.	SPM		
8	625	4570	9120	200.0(AFT)	3240	LEVEL FLIGHT	0.005471
0	1080	5170	9120	200.0(AFT)	3240	LEVEL FLIGHT	0.005482
0	1330	6450	9020	200.1(AFT)	3240	LEVEL FLIGHT	0.005482
0	1705	6970	9420	199.6(AFT)	3240	DIVE	0.005747
▲	615	3190	9560	199.7(AFT)	3240	CLIMB	0.005817

NOTES: 1 OPEN SYMBOLS DENOTE SCAB ON
2 SOLID SYMBOLS DENOTE SCAB OFF
3 ALL ROCKET PODS FULLY LOADED (1634 LB.)

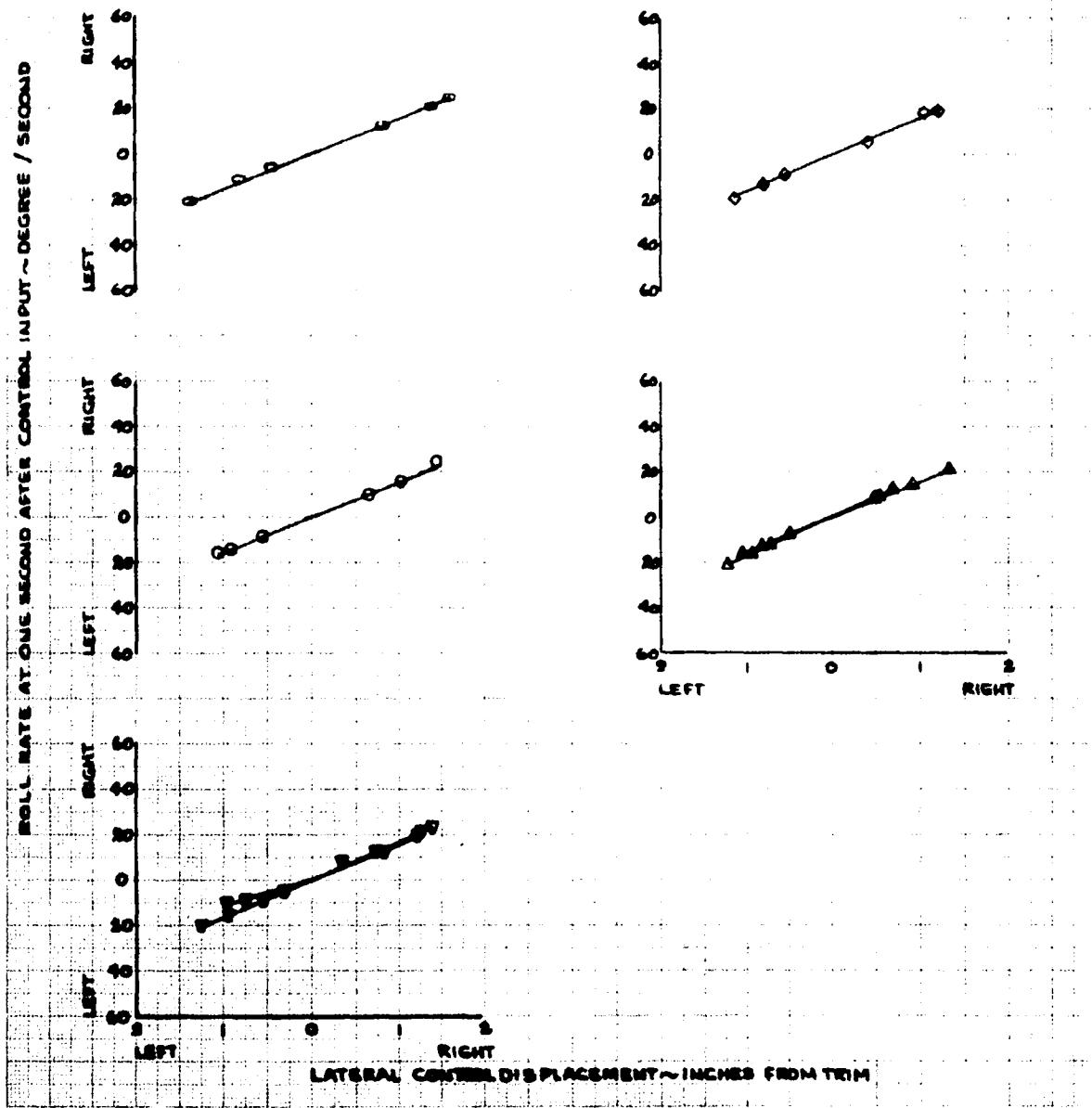


FIGURE NO. 215
ANGULAR ROLL DISPLACEMENT
AM-1G USAK715698
HVV. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM	AIRSPD	ANG. ALZ	ANG. AGL	AVG. LONG.	MOTOR BURN TIME	THROTTLE POSITION
~CAB	~65.5	~55.5	~55.5	~920	200.0(AFT)	2240 LEVEL FLIGHT 0.00 54.75
○	165.0	82.0	82.0	1830	202.1(AFT)	2260 LEVEL FLIGHT 0.00 54.32
○	135.0	64.5	64.5	920	200.1(AFT)	2240 LEVEL FLIGHT 0.00 54.32
○	170.5	68.0	68.0	920	199.6(AFT)	2240 DIVE 0.00 57.47
△	61.5	71.0	71.0	9360	198.7(AFT)	3240 CLIMB 0.00 52.17

NOTES: 1. OPEN SYMBOLS DENOTE SCAS ON
 2. SOLID SYMBOLS DENOTE SCAS OFF
 3. ALL ROCKET PODS FULLY LOADED(1634 LB)

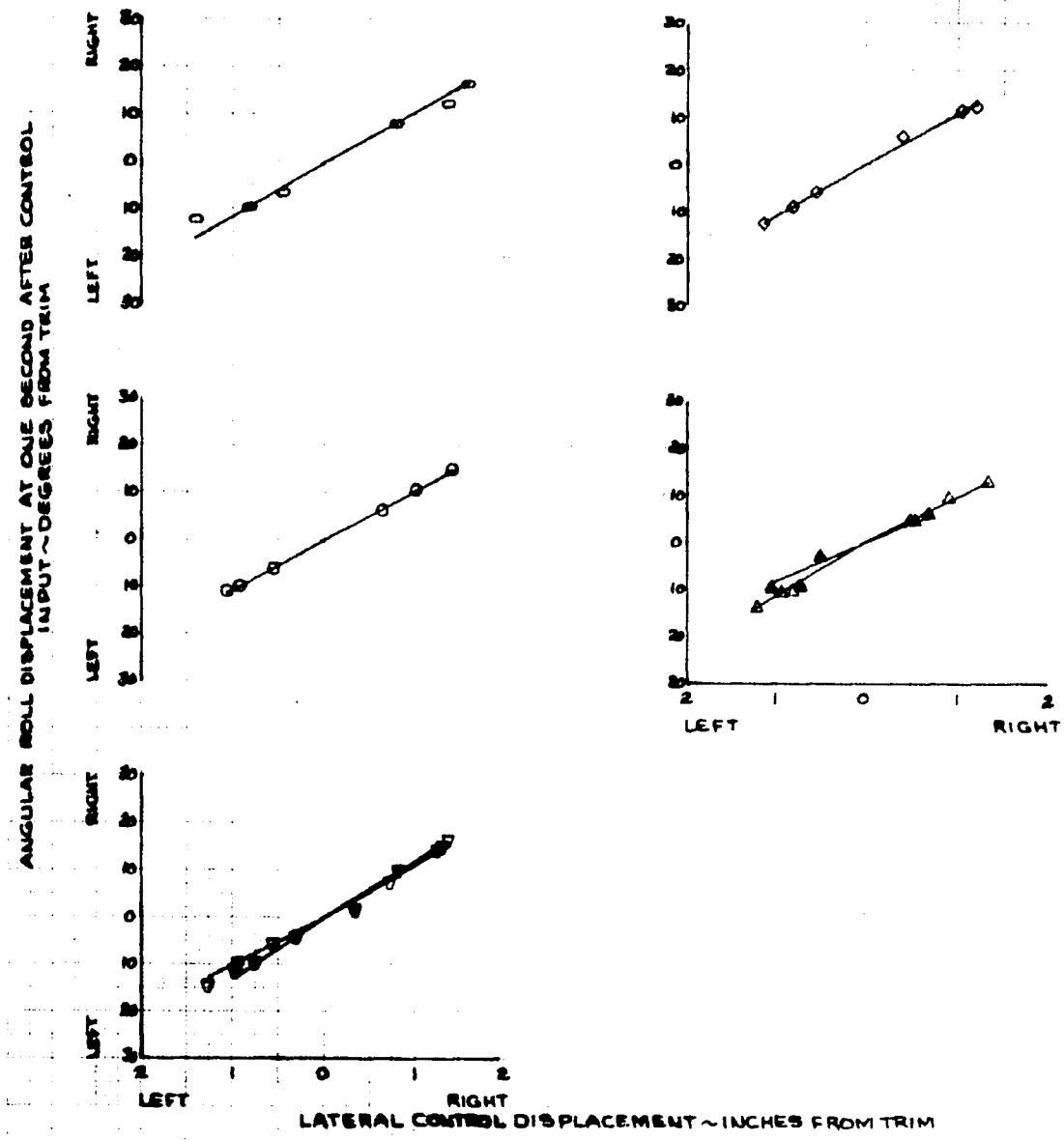


FIGURE NO. 216
LATERAL CONTROL SENSITIVITY

AM-10 USAF 61-151645
HVV. MOG CONFIGURATION WITH ROCKET PODS/BINNS REMOVED

SYM.	AVERAGE -CAS MACH	Avg. ALT. ft	Avg. GM	Avg. LGM	TIME	FLIGHT CONDITION	THrust CODE
0	0.68	3400	1110	200.9(MT)	324.0	LEVEL FLIGHT	0006301
0	1.00	3640	8200	200.9(MT)	324.0	LEVEL FLIGHT	0006301
0	1.81	5840	1580	200.9(MT)	324.0	LEVEL FLIGHT	0006301
0	1.72	7640	1800	200.9(MT)	325.0	DAVE	0006304
0	0.60	3370	1140	200.9(MT)	324.0	CLIMB	0006305
0	0.70	7200	1800	200.9(MT)	324.0	AUTOROTATION	0006301

METACRUISE SWINGLES DENOTE SCAS ON
SOLID SYMBOLS DENOTE KADS ON
& ALL ROCKET PODS EMPTY

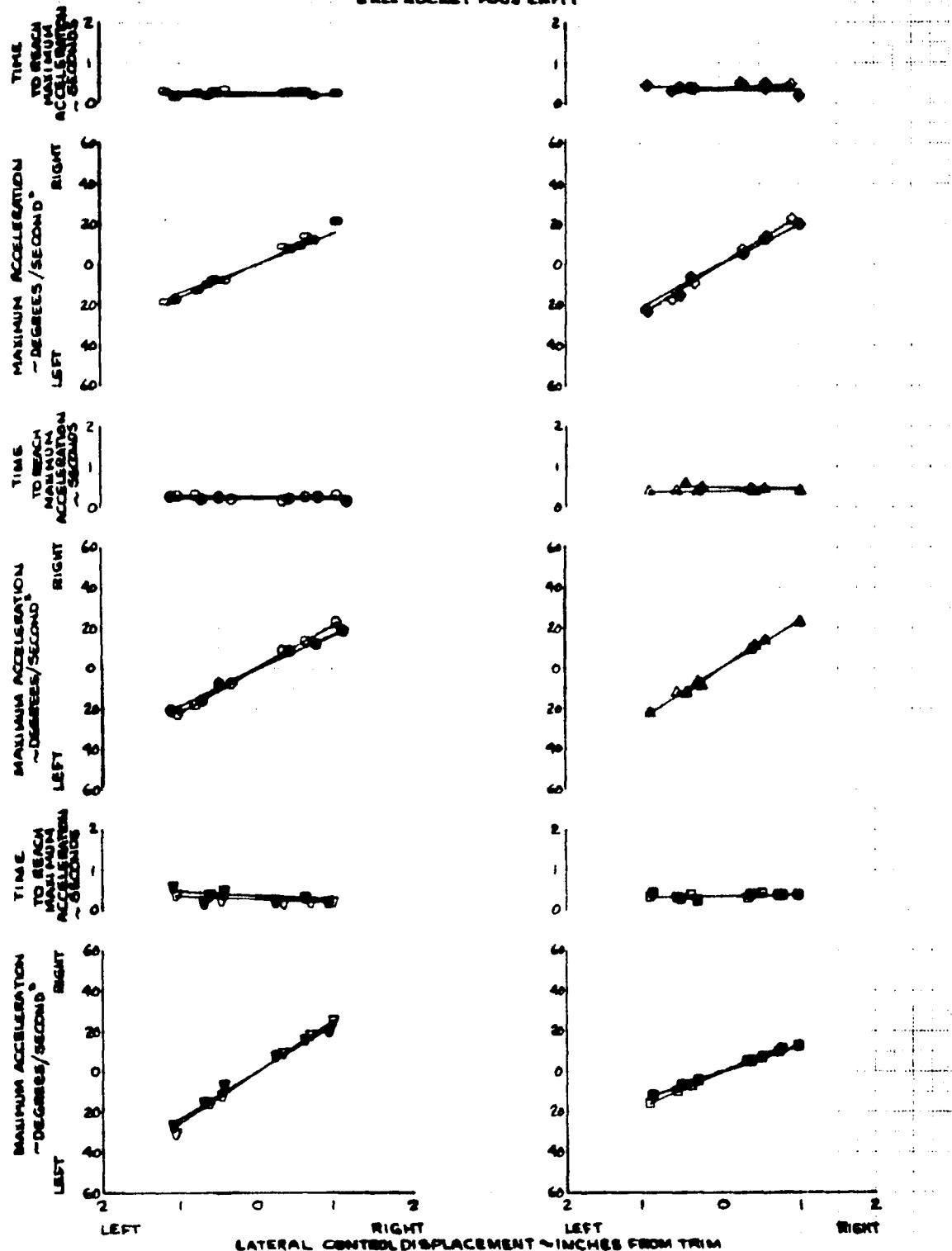


FIGURE NO 217
LATERAL CONTROL RESPONSE

AN-12 LIGAR 1000
HUE MOG CONFIGURATION WITH GROWST POD FAIRINGS REMOVED
SCAS ON

TIME	MAXIMUM SIDE THRUST -DEGREES/SECOND	MAXIMUM ROLL RATE -DEGREES/SECOND	MAXIMUM DIVE RATE -DEGREES/SECOND	MAXIMUM CLIMB RATE -DEGREES/SECOND	ROLL STABILITY	ROLL DAMPING	LEVEL FLIGHT	DIVE	CLIMB	THROTTLE AUTOMATION
-2.5	0	0	0	0	0.00	0.00	0.00	0.00	0.00	0.00
-1.5	0.12	0.20	0.30	0.40	0.00	0.00	0.00	0.00	0.00	0.00
-1.0	0.18	0.30	0.40	0.50	0.00	0.00	0.00	0.00	0.00	0.00
0.0	0.20	0.40	0.50	0.60	0.00	0.00	0.00	0.00	0.00	0.00
1.0	0.22	0.42	0.52	0.62	0.00	0.00	0.00	0.00	0.00	0.00
1.5	0.25	0.45	0.55	0.65	0.00	0.00	0.00	0.00	0.00	0.00
2.0	0.28	0.50	0.60	0.70	0.00	0.00	0.00	0.00	0.00	0.00

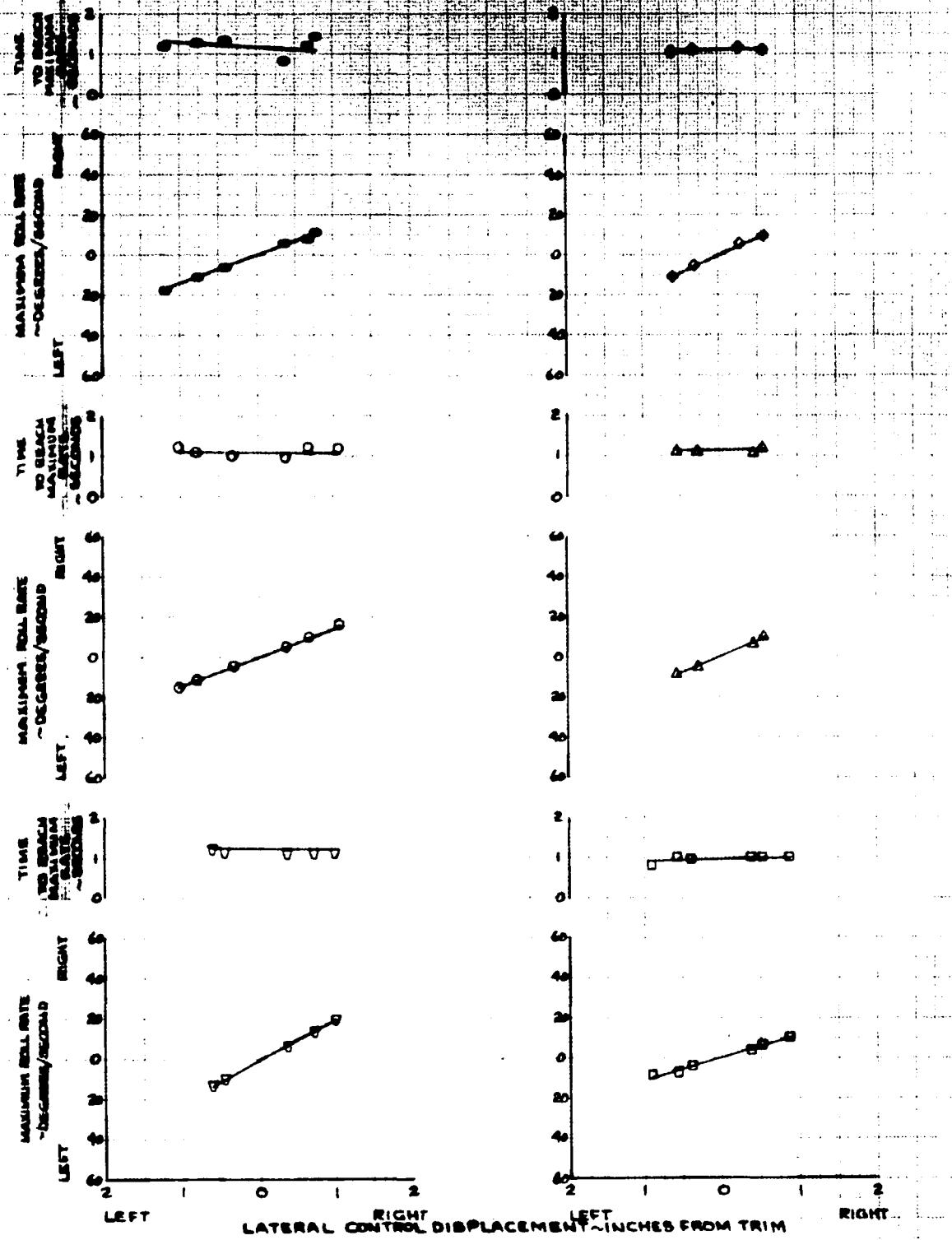


FIGURE NO. 218
LATERAL RESPONSE AT ONE SECOND

AM-10 USAF 716078
HVY HOG CONFIGURATIONS WITH ROCKET POD FAIRINGS REMOVED

SYM	AIRCRAFT	ANG. ALT.	ANG. C.G.	ANG. LOAD	MOTOR NUMBER		ANGLE OF PITCH
					CAB	H ₀ -P ₁	
○	160	3100	770	300.0(FT)	1	1.0	0.000100
○	160	3100	5000	300.0(FT)	1	1.0	0.000100
○	162.5	3840	7800	320.0(FT)	1	1.0	0.000100
○	172.0	7640	7800	320.0(FT)	1	1.0	0.000100
△	620	7570	7700	320.0(FT)	1	1.0	0.000100
○	67.0	7120	7800	320.0(FT)	1	1.0	0.000100

NOTES: 1 OPEN SYMBOLS DENOTE SCAS ON
 2 SOLID SYMBOLS DENOTE SCAS OFF
 3 ALL ROCKET PODS EMPTY

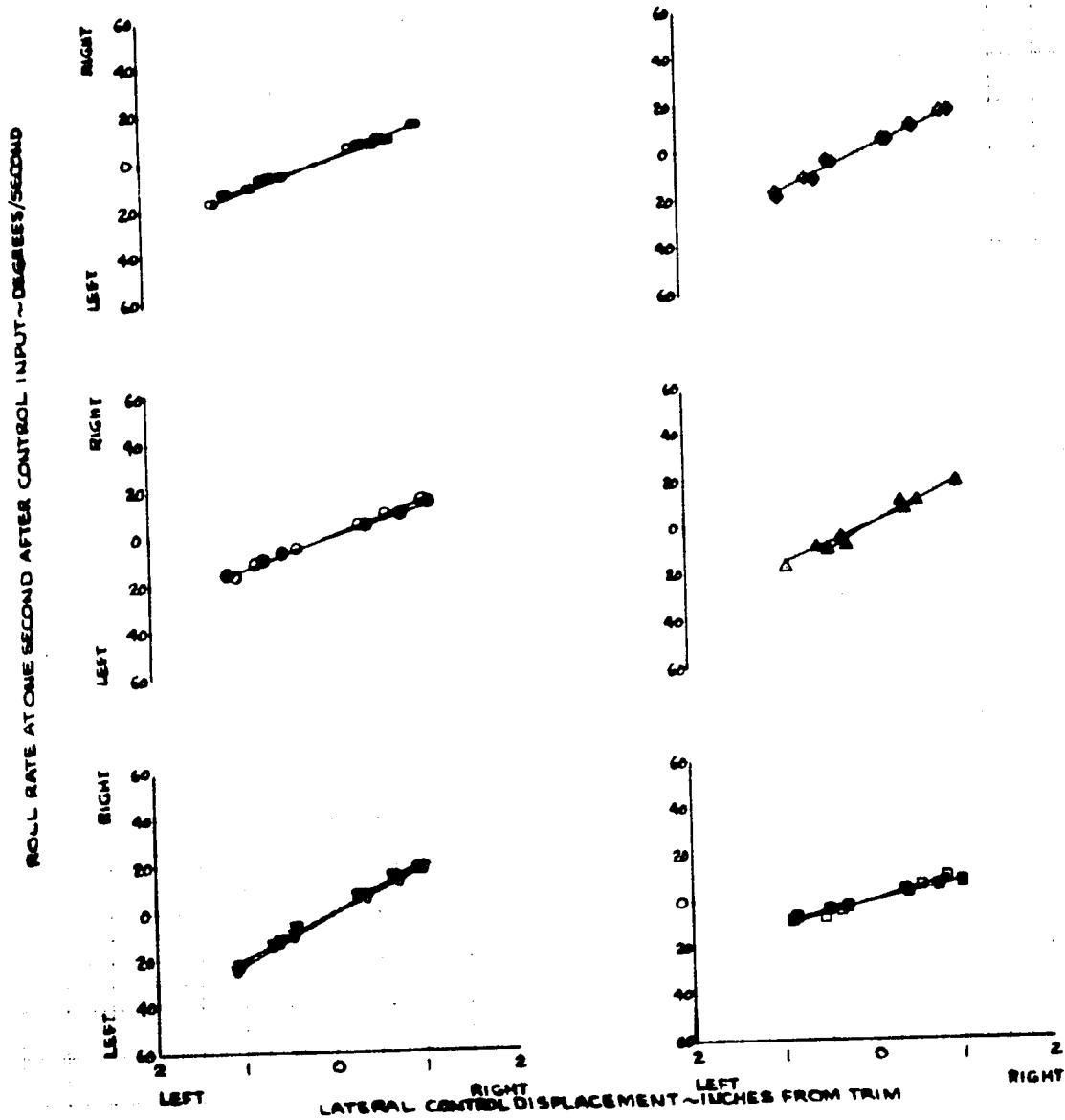


FIGURE NO. 219
ANGULAR ROLL DISPLACEMENT

AH-1G USAF 15628
 HVY. HOG CONFIGURATION WITH BRAKE PEDALS REMOVED

GYM	AIRFIELD	Avg. Alt. ft.	Avg. GM in.	Avg. Ldg. wt. lb.	Wing load lb./sq. ft.	Fwd. load lb./sq. ft.	Flight load lb./sq. ft.	Flight load lb./sq. ft.
8	CAB	5200	1770	200000	100.00	100.00	100.00	100.00
8	1000	5200	1800	200000	100.00	100.00	100.00	100.00
8	1525	5200	1800	200000	100.00	100.00	100.00	100.00
8	1720	5200	1800	200000	100.00	100.00	100.00	100.00
8	800	5200	1770	200000	100.00	100.00	100.00	100.00
8	610	5200	1700	200000	100.00	100.00	100.00	100.00

NOTE: 1 OPEN SYMBOLS DENOTE SCAS ON
 2 SOLID SYMBOLS DENOTE SCAS OFF
 3 ALL BRAKES PEDALS EMPTY

ANGULAR ROLL DISPLACEMENT AT ONE SECOND AFTER CONTROL
 INPUT ~ DEGREES FROM TRIM

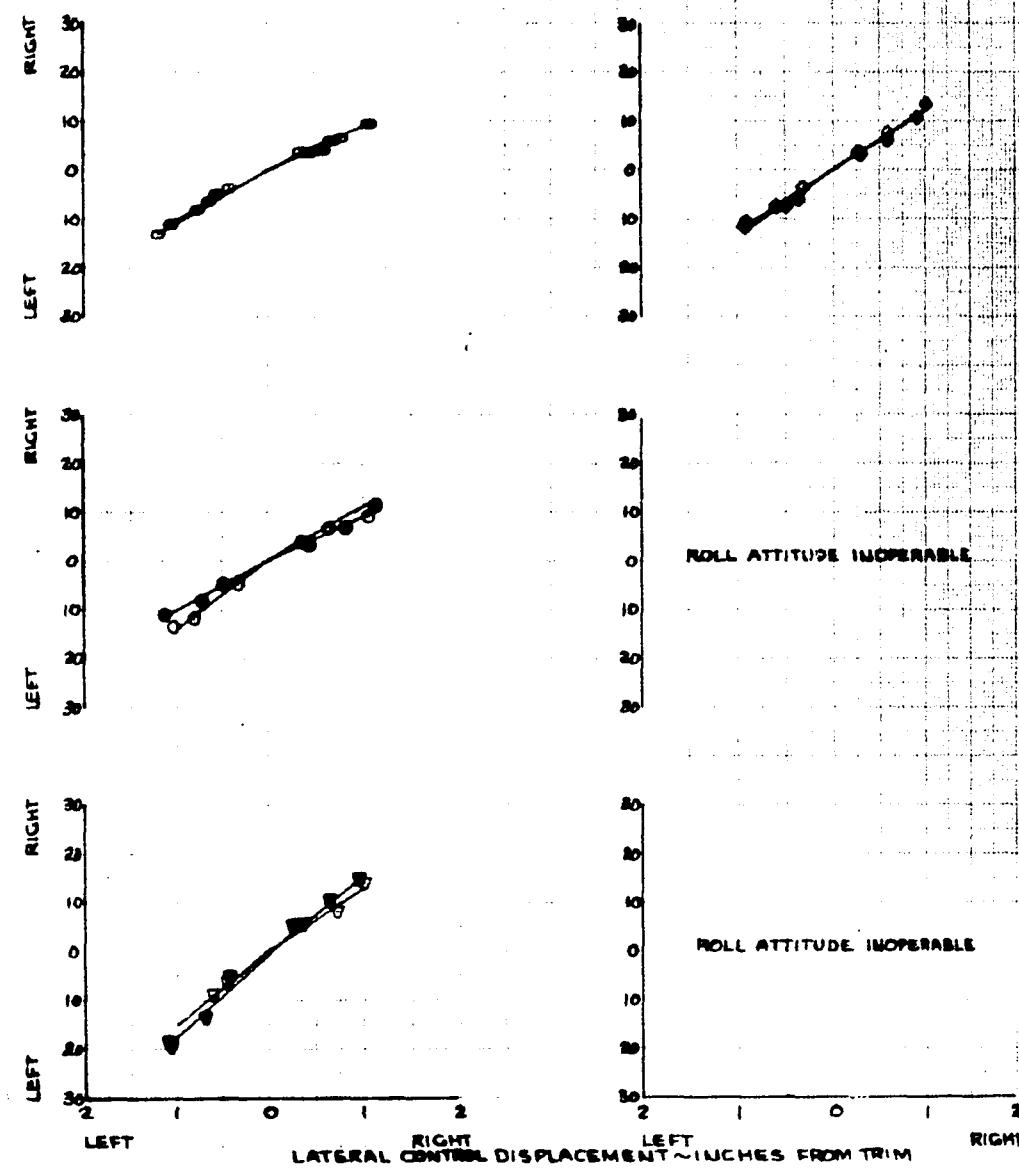


FIGURE NO. 220
LATERAL CONTROL SENSITIVITY
 AH-1G USAF T1098
 HVY. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYN. AIRSPEED AVG ALT. AVG G.M. AVG. LOAD RATIO DUE TO G. M. THRUST COEFF.
 ~CAS H₀ - ST. ~18. C.G. -14. R₀ ~C_T
 0 53.0 16160 11190 200.0 (APT) 1.240 LEVEL FLIGHT 0.006885
 0 68.0 17010 1300 200.0 (APT) 1.240 LEVEL FLIGHT 0.006882
 0 105.0 16160 7680 200.0 (APT) 1.240 LEVEL FLIGHT 0.006887

NOTES: OPEN SYMBOLS DENOTE SCAS ON
 2 SOLID SYMBOLS DENOTE SCAS OFF
 3 ALL ROCKET PODS EMPTY

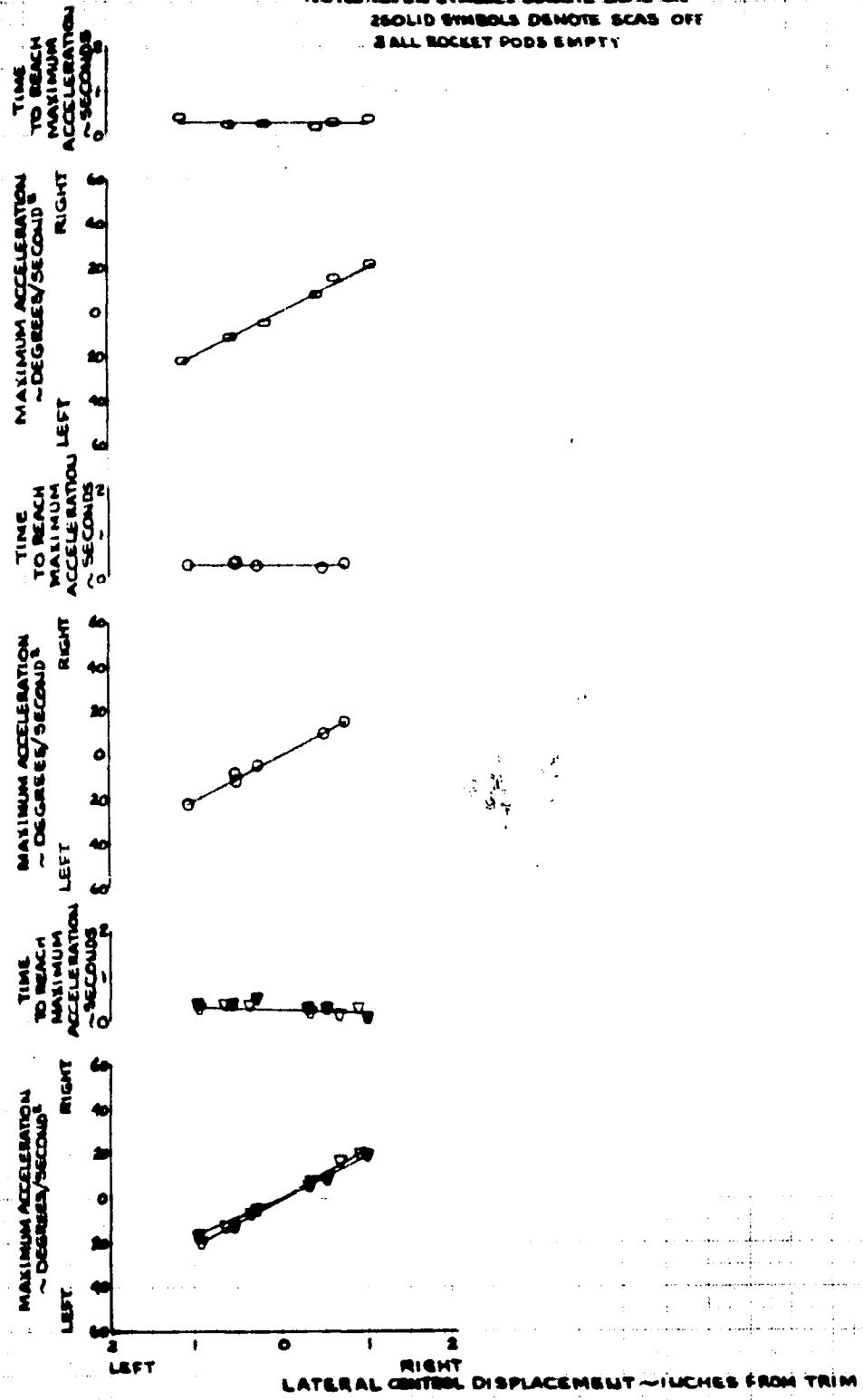


FIGURE NO. 221
LATERAL CONTROL RESPONSES

AH-1G USA 371864B
 HVY. HOG CONFIGURATION WITH ROCKETS POSSIBLY REMOVED
 SCAB ON

DVM	AIRFIELD	ANG. ALT.	Avg. G.H.	Avg. LOAD	ROTOR RPM	THROTTLE POS.
0	CAB	HR ~ FT	~ LBS	G.G. ~ LBS	~ RPM	~ %
500	520	16160	7740	300.0(?)	3200 LEVEL FLIGHT	0.00
800	820	17010	7800	320.0(?)	3200 LEVEL FLIGHT	0.002152
1000	1050	16160	7630	300.0(?)	3200 LEVEL FLIGHT	0.0006264

NOTE: ALL ROCKETS POSSIBLY REMOVED

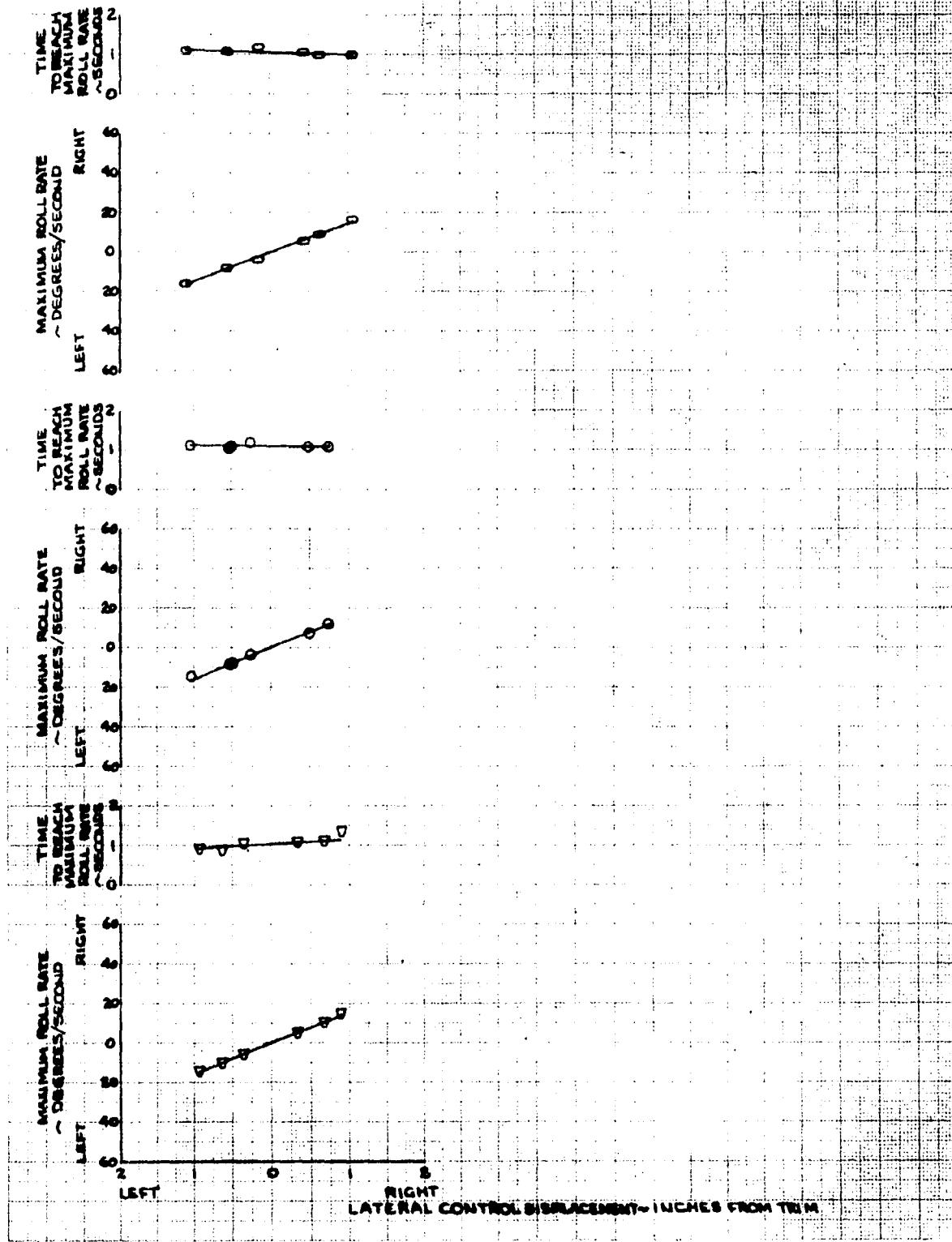


FIGURE NO. 222
LATERAL RESPONSE AT ONE SECOND

AN-1G USAF 571569B
 HVY. HOG CONFIGURATION, INTERMEDIATE PODS FAIRINGS REMOVED

DYN	AIR SPEED	AIR. ALT.	AIR. GDN	AIR. LONG.	ROT. RATE	ROT. POSITION
-	- CAS	HGT - FT	~LG	C.G. - IN.	DEG/SEC	DEG
O	230	19190	7190	220.9 (APT)	3120	LEVEL FLIGHT
O	1050	16160	7680	200.8 (APT)	3200	LEVEL FLIGHT

NOTE: OPEN SYMBOLS DENOTE SCAB ON
 & SOLID SYMBOLS DENOTE SCAB OFF
 ALL ROCKET PODS EMPTY

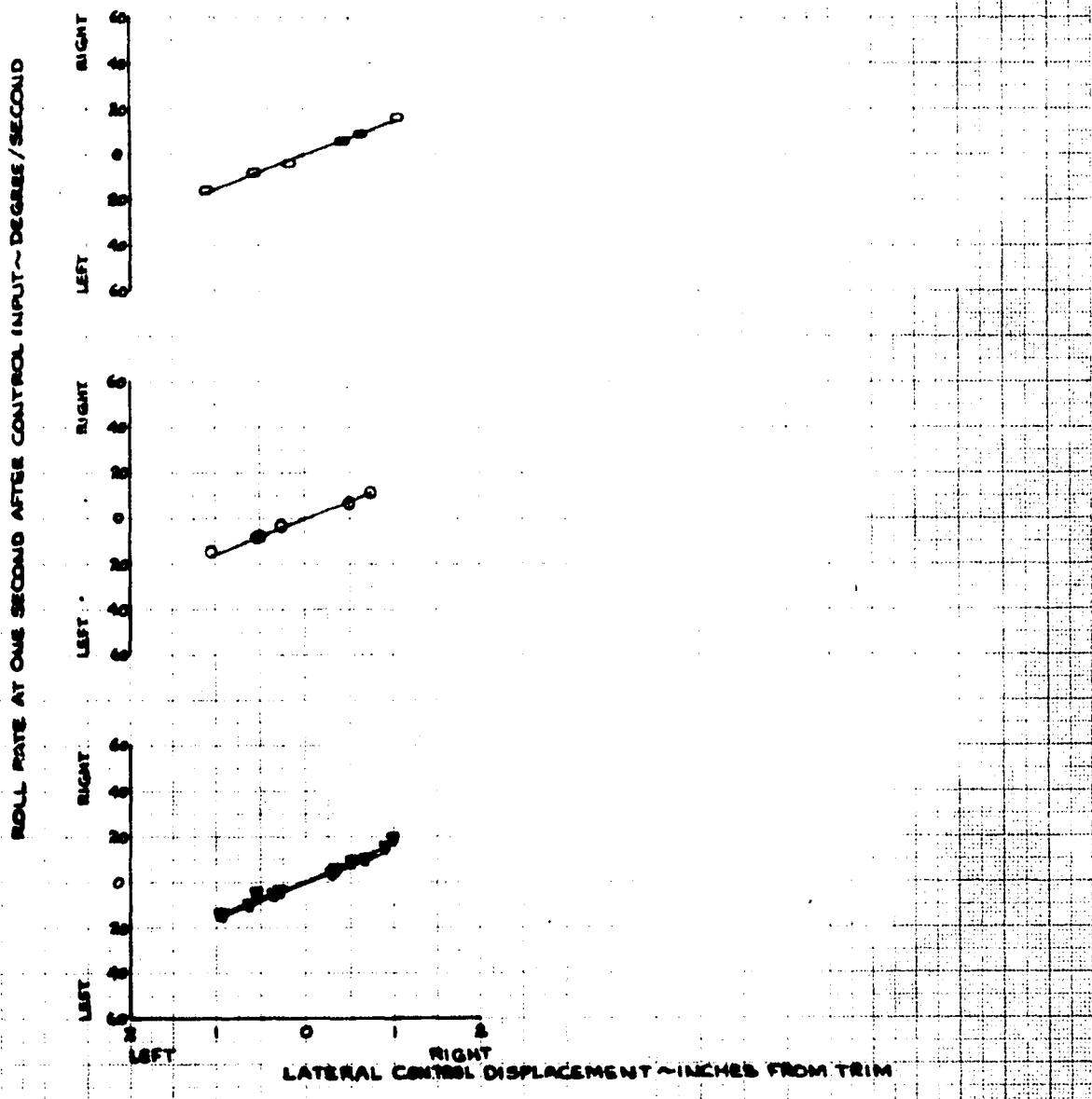


FIGURE NO. 223
 ANGULAR ROLL DISPLACEMENT
 AH-1G USAF 118698
 HVY. HOG CONFIGURATION WITH ROCKET POD CARRIERS REMOVED

SYM	AIR SPEED	ANG. ALT.	ANG. G.W.	ANG. LIFT	WEIGHT	ROLL	DISPLACEMENT
ACAS	400	45°-55°	-10°	200°(EST)	3340	LEVEL	0.005763
	330	15°00'	10°00'	3340	LEVEL	0.002623	
	1000	15°00'	11°00'	3340(EST)	3340	LEVEL	0.001674

NOTES: 1. OPEN SYMBOLS DENOTE SCAB ON
 2. SOLID SYMBOLS DENOTE SCAB OFF
 3. ALL ROCKET PODS EMPTY

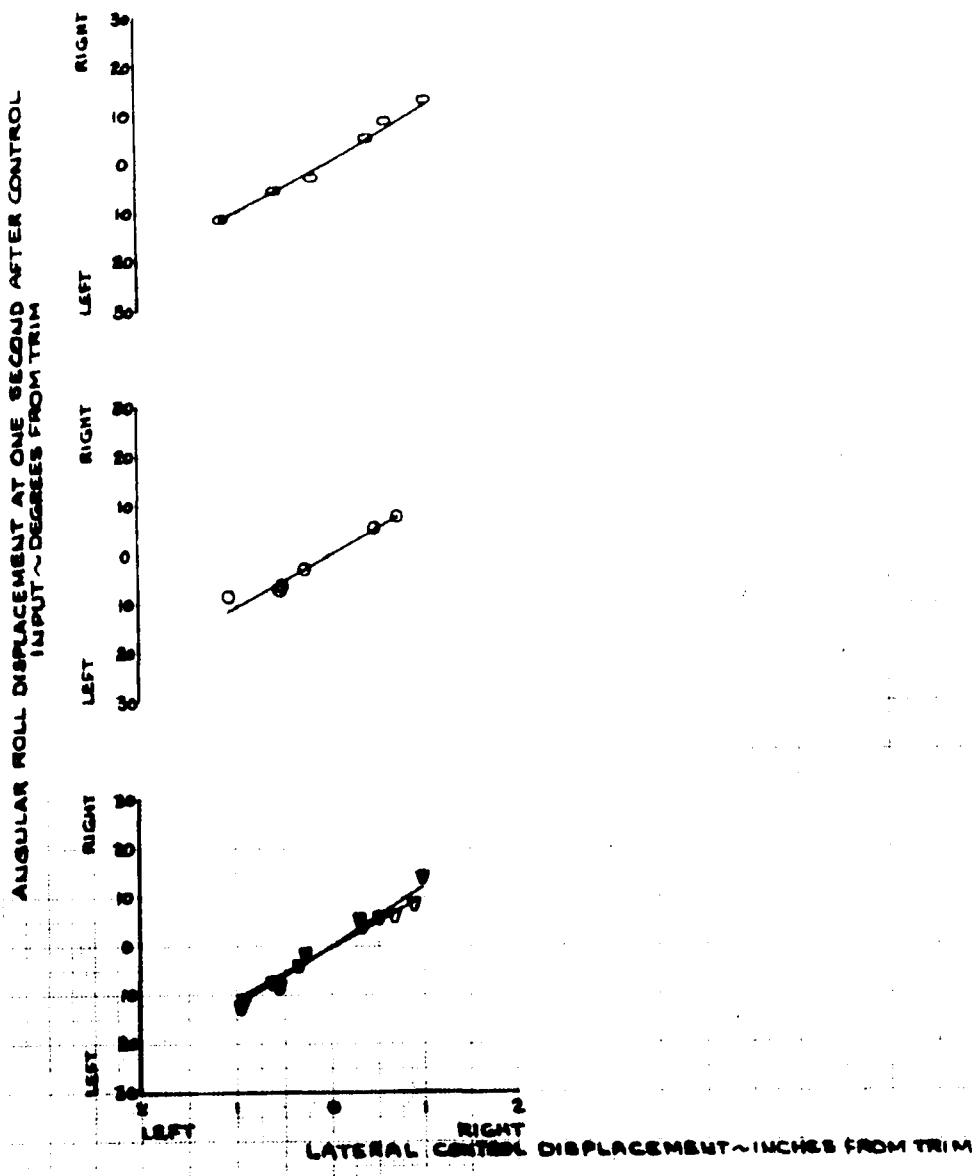


FIGURE NO. 224
DIRECTIONAL CONTROL SENSITIVITY
AH-1W USAF 215GRS
CLEAN CONFIGURATION

SYM	AIRSPED ~CAS	Avg. Alt. Hg ~ft.	Avg. G.M. ~IN.	Avg. Load C.G. ~IN.	MOTOR RPM	FLIGHT CONDITION	THRUST COEF.
○	6.80	4970	7710	201.3 (AFT)	3240	LEVEL FLIGHT	0.004439
○	10.90	6790	7300	201.1 (AFT)	3240	LEVEL FLIGHT	0.004443
○	14.50	4960	7460	201.2 (AFT)	3240	LEVEL FLIGHT	0.004430
○	161.0	8140	7700	201.2 (AFT)	3240	DIVE	0.004183
○	62.9	2440	7620	201.2 (AFT)	3240	CLIMB	0.004066
○	68.9	5270	7730	201.2 (AFT)	3000	AUTOROTATION	0.004988

NOTE: OPEN SYMBOLS DENOTE SCAS ON
SOLID SYMBOLS DENOTE SCAS OFF

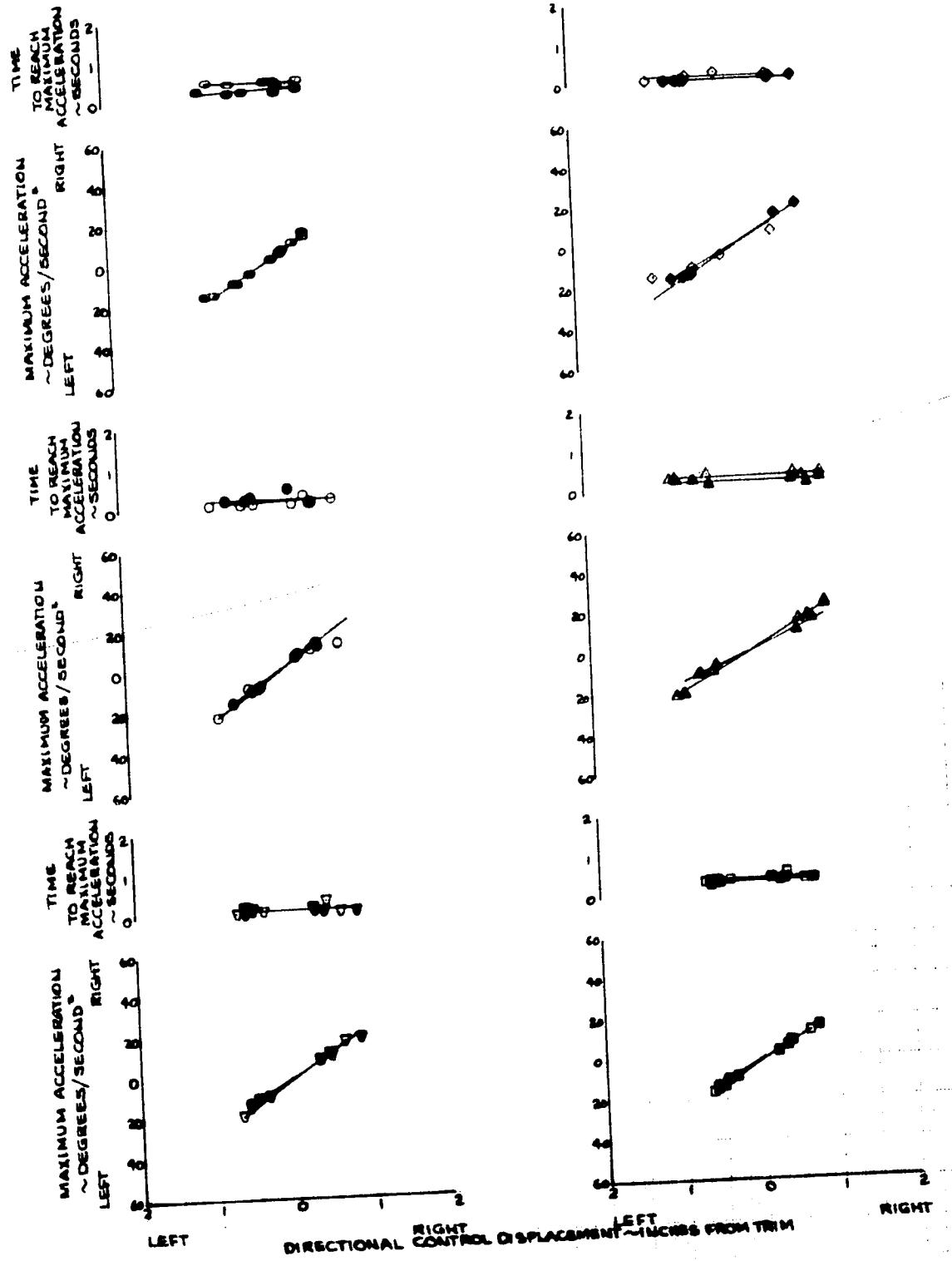


FIGURE NO. 225
DIRECTIONAL CONTROL RESPONSE
 AH-1G USAF/NISERS
 CLEAN CONFIGURATION
 BCAS ON

SYM	AIR SPEED ~CAS	AVG. ALT. HO ~FT.	AVG.G.H. ~LB	AVG. LONG. C.G. ~IN.	ROTORS FLIGHT. CONDITION	THROTTLE CTRD. ~%
○	63.0	4970	7710	201.2(AFT)	3240 LEVEL FLIGHT	0.004934
△	105.0	6790	7800	201.1(AFT)	3240 LEVEL FLIGHT	0.004923
○	145.0	4900	7460	201.2(AFT)	3240 LEVEL FLIGHT	0.004920
○	181.0	3140	7700	201.2(AFT)	3240 DIVE	0.004918
□	62.0	2940	7620	201.2(AFT)	3240 CLIMB	0.004916
○	68.3	3290	7780	201.2(AFT)	3240 AUTO ROTATION	0.004916

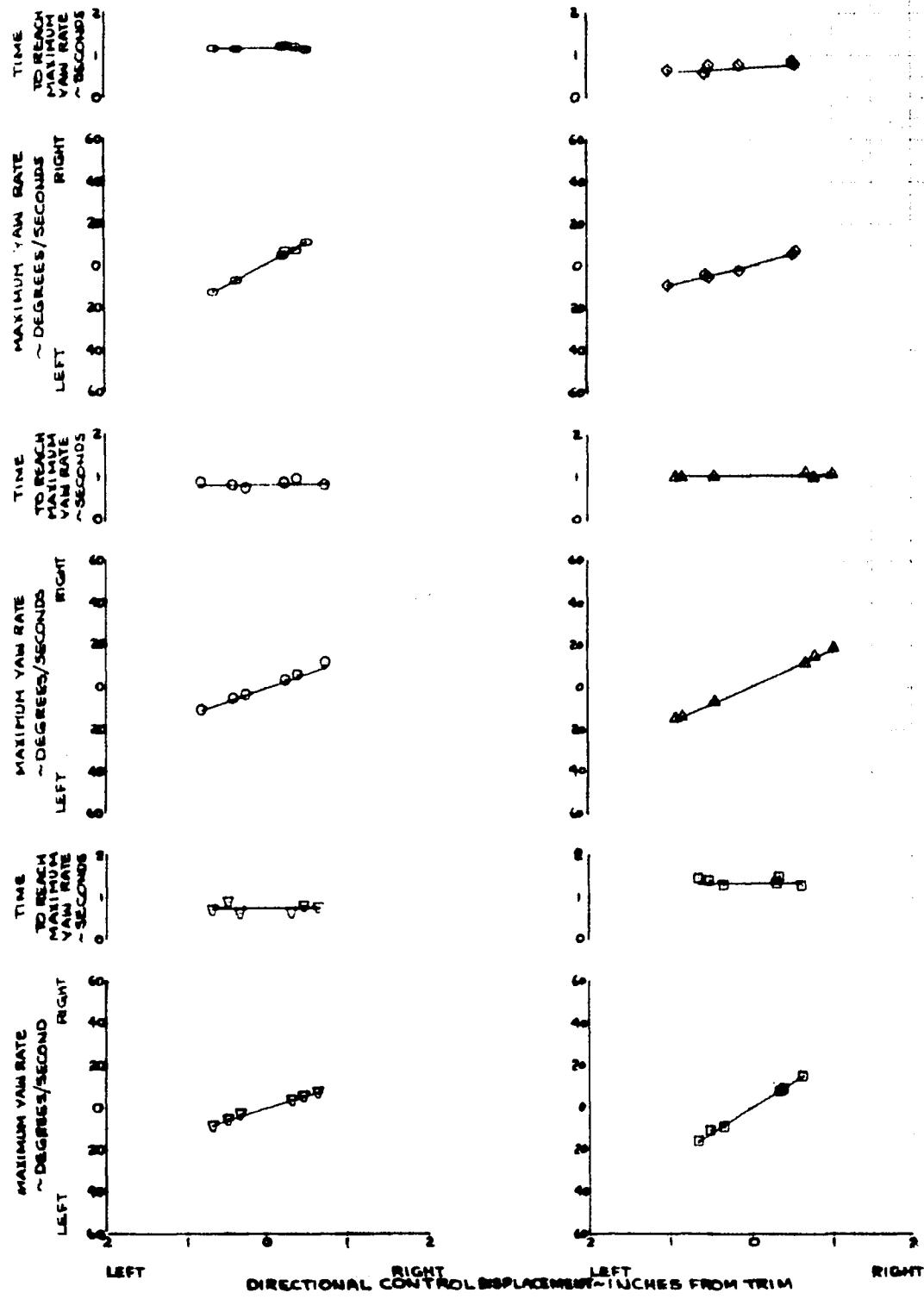


FIGURE NO. 226
DIRECTIONAL RESPONSE AT ONE SECOND
AH-1G USAF 1968
CLEAN CONFIGURATION

SYM	Avg Speed ~CAS	Avg Alt. ft	Avg G-L	Avg Long. dist.	GROSS FLAMES CONDITION	THRUST COEFF. ~C _T
○	53.0	4470	7710	201.2(FT)	3240 LEVEL FLIGHT	0.004474
○	104.0	6190	12000	201.1(FT)	3240 LEVEL FLIGHT	0.004473
○	145.0	6460	1460	201.2(FT)	3220 LEVEL FLIGHT	0.004326
○	181.0	3140	7700	201.2(FT)	3220 DIVE	0.004183
△	620	2460	7620	201.2(FT)	3240 CLIMB	0.004066
□	68.5	3290	7780	201.2(FT)	3200 AUTO ROTATION	0.004485

NOTE: OPEN SYMBOLS DENOTE SCAS ON
SOLID SYMBOLS DENOTE SCAS OFF

VAN RATE AT ONE SECOND AFTER CONTROL INPUT ~ DEGREES/SECOND

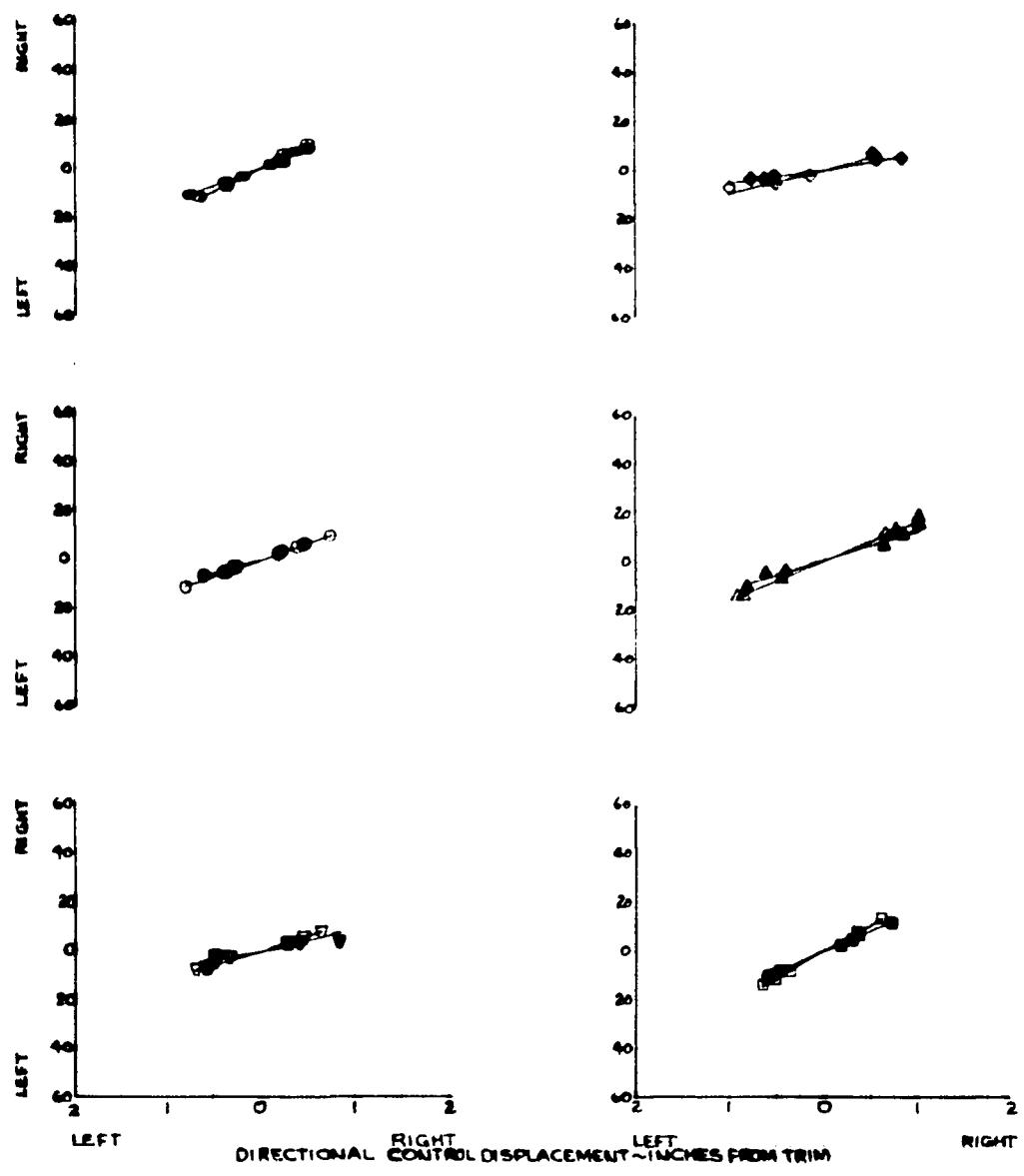


FIGURE NO. 227
ANGULAR YAW DISPLACEMENT
 AH-1G USAF/TIS678
 CLEAN CONFIGURATION

SYM	AIR SPEED ~CAS	Avg. Alt. H ₀ ~FT.	Avg. GM ~LB.	Avg. Long. C.G. ~IN.	MOTOR FLIGHT COMBINATION	THRUST COEFF. ~C _T
●	52.0	4410	7710	201.3(MT)	3240 LEVEL FLIGHT	0.004479
○	102.0	6140	7300	201.1(MP)	3240 LEVEL FLIGHT	0.004443
□	143.0	4760	7960	201.2(MD)	3240 LEVEL FLIGHT	0.004520
△	181.0	8140	1100	201.2(MP)	3240 DIVE	0.004181
▲	62.0	2440	7620	201.2(MT)	3240 CLIMB	0.004866
□	62.5	8240	1180	201.2(MP)	3000 AUTOROTATION	0.004436

NOTE: OPEN SYMBOLS DENOTE SCAS ON
 SOLID SYMBOLS DENOTE SCAS OFF

ANGULAR YAW DISPLACEMENT AT ONE SECOND AFTER CONTROL INPUT ~ DEGREES FROM TRIM

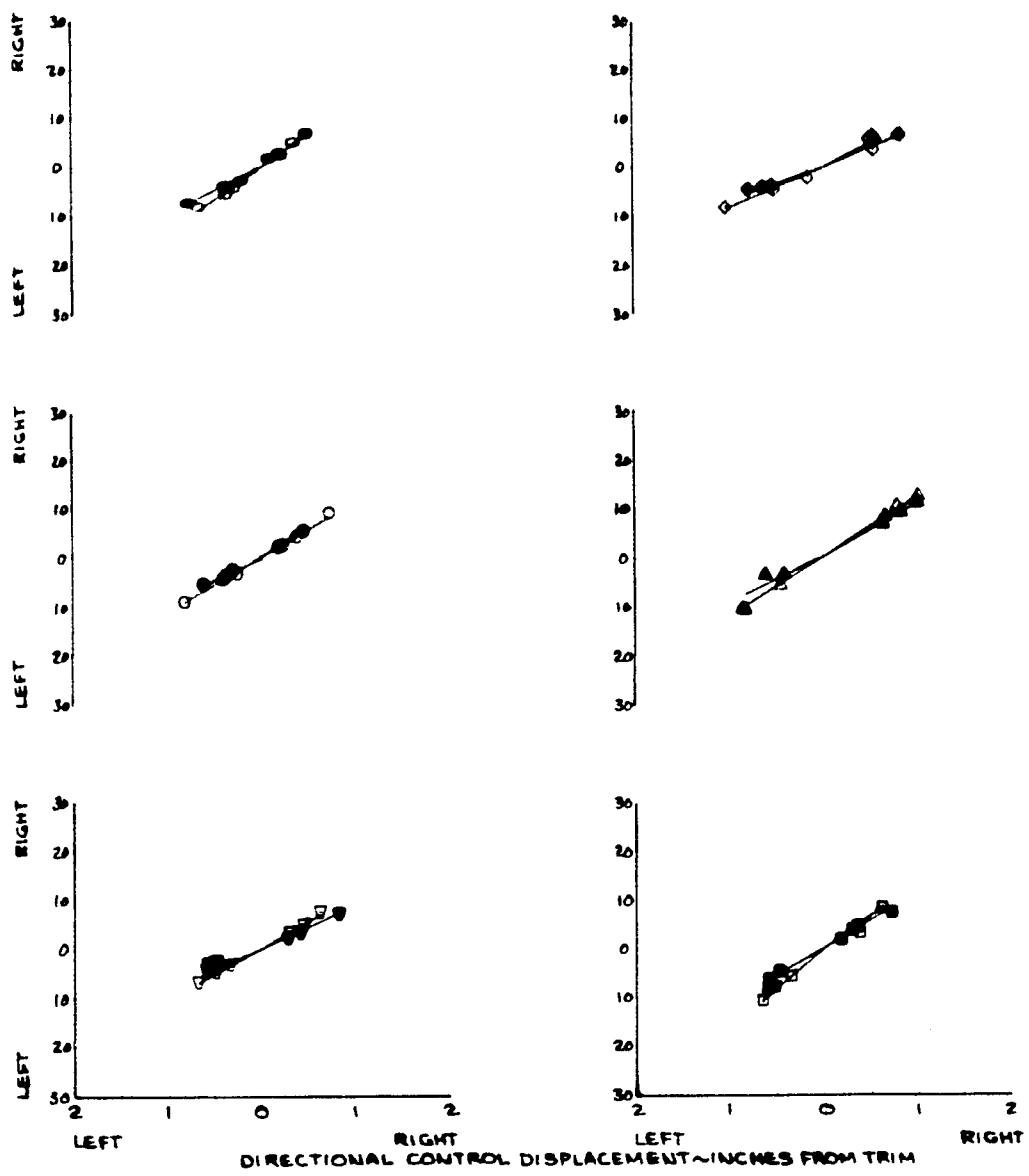


FIGURE NO. 228
DIRECTIONAL CONTROL SENSITIVITY
 AH-1G USA N4884T
 CLEAN CONFIGURATION WITH LANDING GEAR CROSS TUBE FAIRINGS REMOVED

SYM	MEASURED	Avg Alt.	Avg C.G. ~C.G. ft	Avg Long. ~LG. ft	Motor Flight Cen.	Thrust Cen.	~C.G.
O	1160	8180	6620	199.6(FT)	3220	LEVEL FLIGHT	0.004887
O	145.5	4010	6640	199.5(FT)	3220	LEVEL FLIGHT	0.004929
O	1690	5780	6540	199.5(FT)	3220	DIVE	0.005103

NOTE: OPEN SYMBOLS DENOTE SCAB ON
 SOLID SYMBOLS DENOTE SCAB OFF

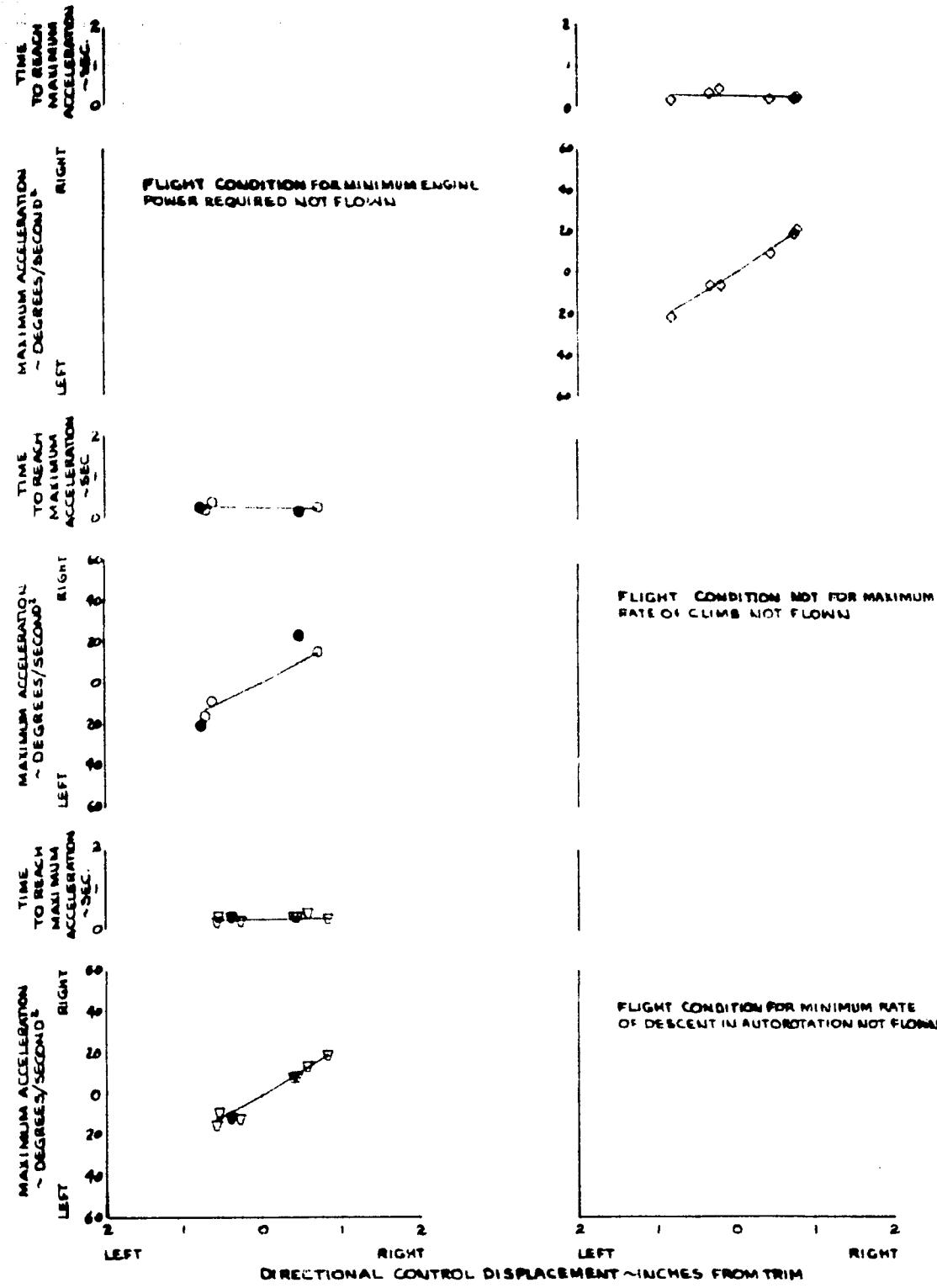


FIGURE No. 229
DIRECTIONAL CONTROL RESPONSE
 AMIG USA 46016297
 CLEAN CONFIGURATION WITH LANDING GEAR CROSS TUBE FAIRINGS REMOVED

SYM.	AIRSPEED ~CAS	HGT. ~FT.	AVG.G.W. ~LB	AVG.LONG. C.G. ~IN.	ROTOR RPM	FLIGHT COMB. THRUST ~CWT.	~CT
O	118.0	3150	6820	194.6(FT)	3220	LEVEL FLIGHT 0.004837	
□	145.5	4070	6890	194.5(FT)	3220	LEVEL FLIGHT 0.004929	
◊	169.0	5780	6840	197.5(FT)	3220	DIVE 0.005103	

NOTE: OPEN SYMBOLS DENOTE SCAS ON
 SOLID SYMBOLS DENOTE SCAS OFF

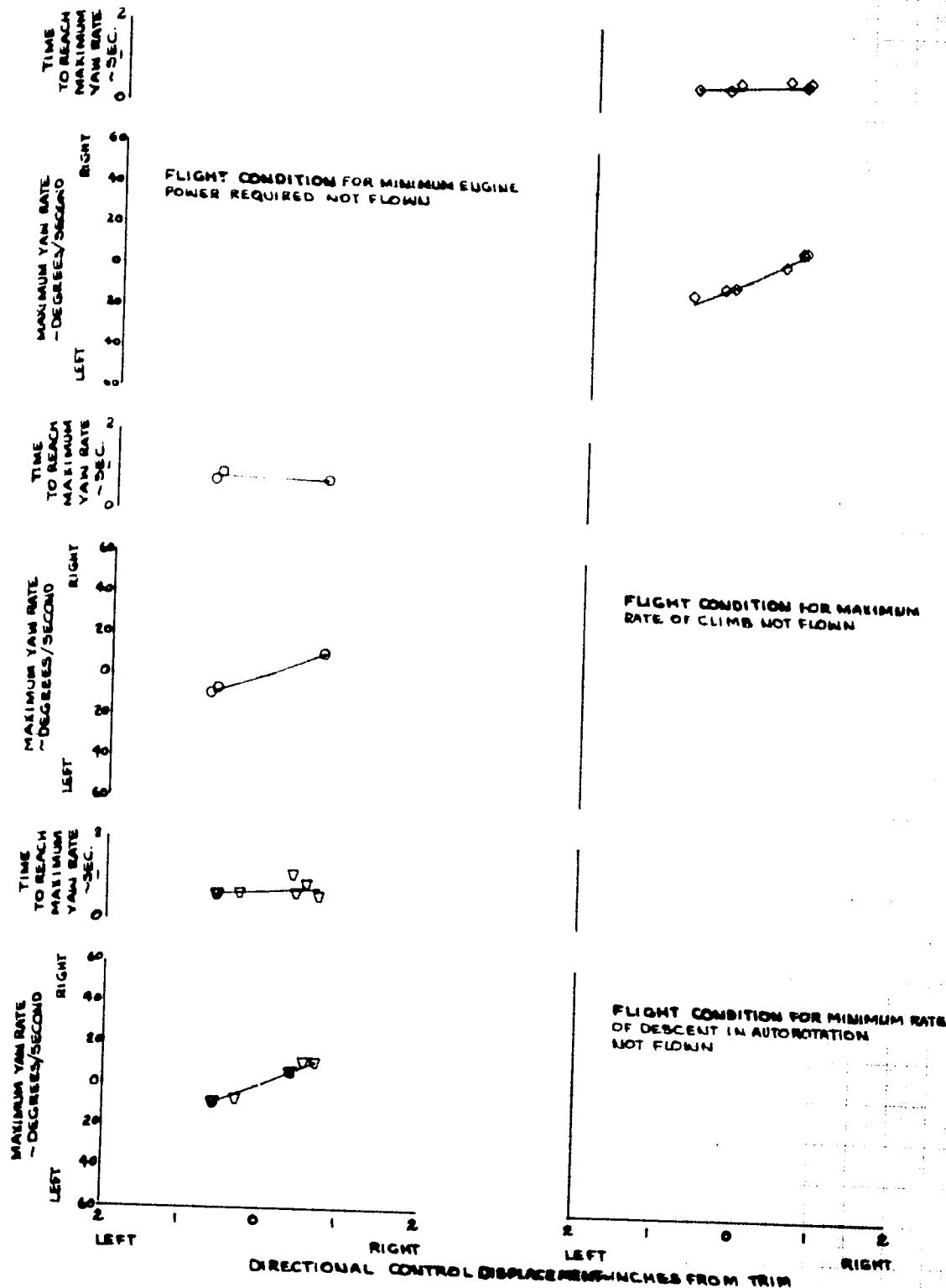


FIGURE NO. 230
DIRECTIONAL RESPONSE AT ONE SECOND

AH-1G USA VERSION
CLEAN CONFIGURATION WITH LANDING GEAR CROSS TUBE FAIRINGS REMOVED

SYM.	WHEELS UP	WHEELS DOWN	ROLL ANG. (DEG.)	ROLL RATE (IN/SEC)	THROTTLE POS.	FLIGHT COND.
○	110.0	310.0	882.0	109.600	322.0	LEVEL FLIGHT 0.00 4837
○	145.5	407.0	864.0	109.500	322.0	LEVEL FLIGHT 0.00 4129
●	161.0	518.0	854.0	109.500	322.0	DIVE 0.00 5108

NOTE: OPEN SYMBOLS DENOTE SCAS ON
 SOLID SYMBOLS DENOTE SCAS OFF

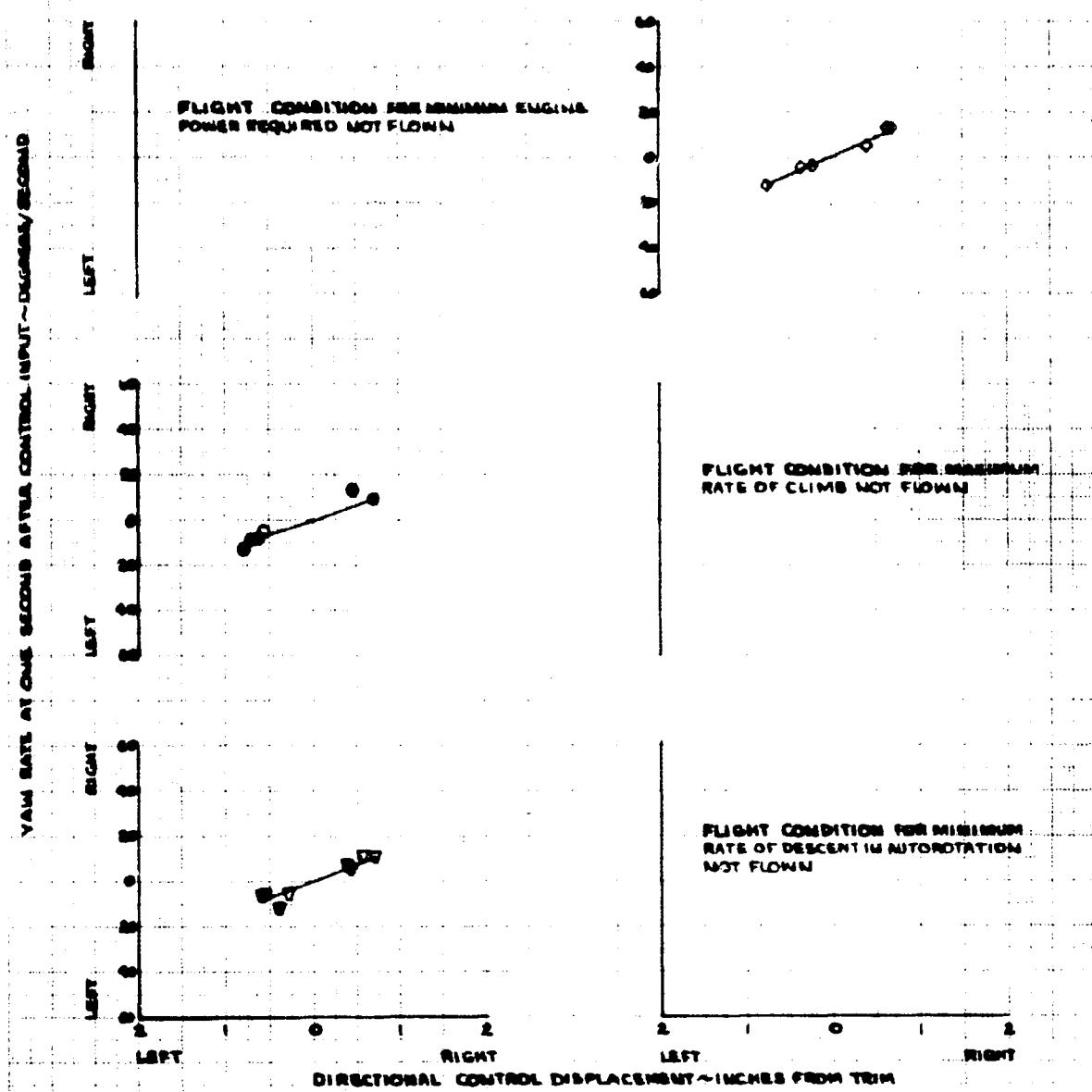


FIGURE NO. 251
ANGULAR YAW DISPLACEMENT
 AH-1G USA NUMBER
 CLEAN CONFIGURATION WITH LANDING GEAR CROSSTUBE FAIRINGS REMOVED

SYM	AIRSPD	Avg Alt	Avg G.M.	Avg L.W.	Boots	Flight Cond.	Traint. Config.
-CAB	No -ft.	-lb.	C.G. -in.	MM			-C
0	1160	3150	6620	199.6(FT)	3120	LEVEL FLIGHT	0.00-4927
0	108.8	4070	6670	199.5(FT)	3120	LEVEL FLIGHT	0.00-4929
0	107.0	5700	6640	144.3(FT)	3120	DIVE	0.00-5103

NOTE: OPEN SYMBOLS DENOTE SCARborough
 SOLID SYMBOLS DENOTE SCAD CITY

ANGULAR YAW DISPLACEMENT AT ONE SECOND AFTER CONTROL INPUT - DEGREES FROM TRIM

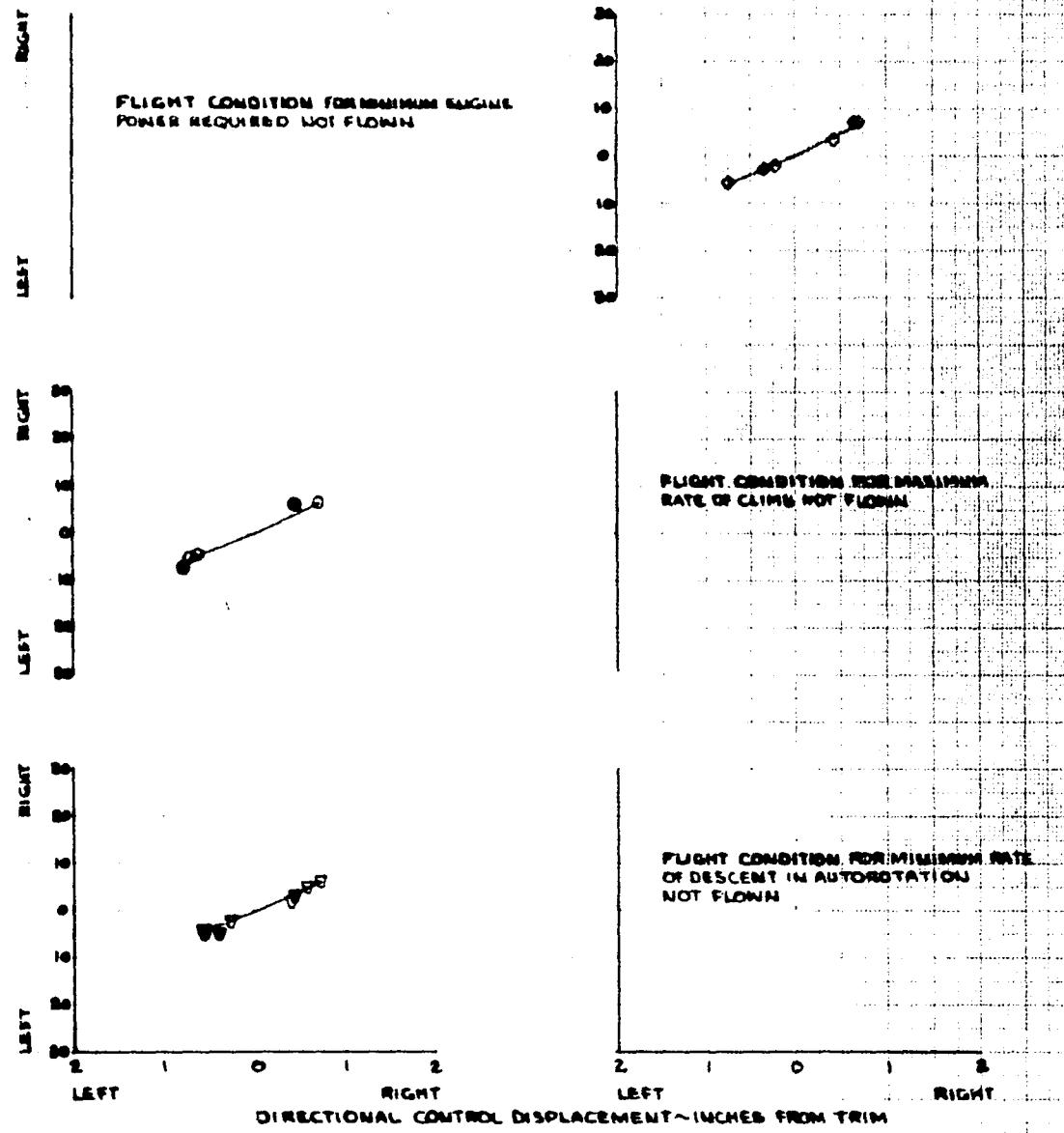


FIGURE No. 232
 DIRECTIONAL CONTROL SENSITIVITY
 AH-1G USA #718695
 HVY HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM	AIRSPD ~CAS	Avg Alt M0-ST	Avg G-n ~LB	Avg Long. C.G ~IN.	ROTOR RPM	FLIGHT CONDITION	THRUST COEFF. ~C _T
0	630	4800	9640	300.0(AFT)	324.0	LEVEL FLIGHT	0.00 5464
0	1080	5800	9280	200.2(AFT)	324.0	LEVEL FLIGHT	0.00 5396
0	1340	6940	9120	800.0(AFT)	324.0	LEVEL FLIGHT	0.00 5454
0	1720	6870	9250	199.6(AFT)	324.0	DIVE	0.00 5643
0	620	6380	9420	199.6(AFT)	324.0	CLIMB	0.00 5661

NOTE: OPEN SYMBOLS DENOTE SCAS ON
 SOLID SYMBOLS DENOTE SCAS OFF

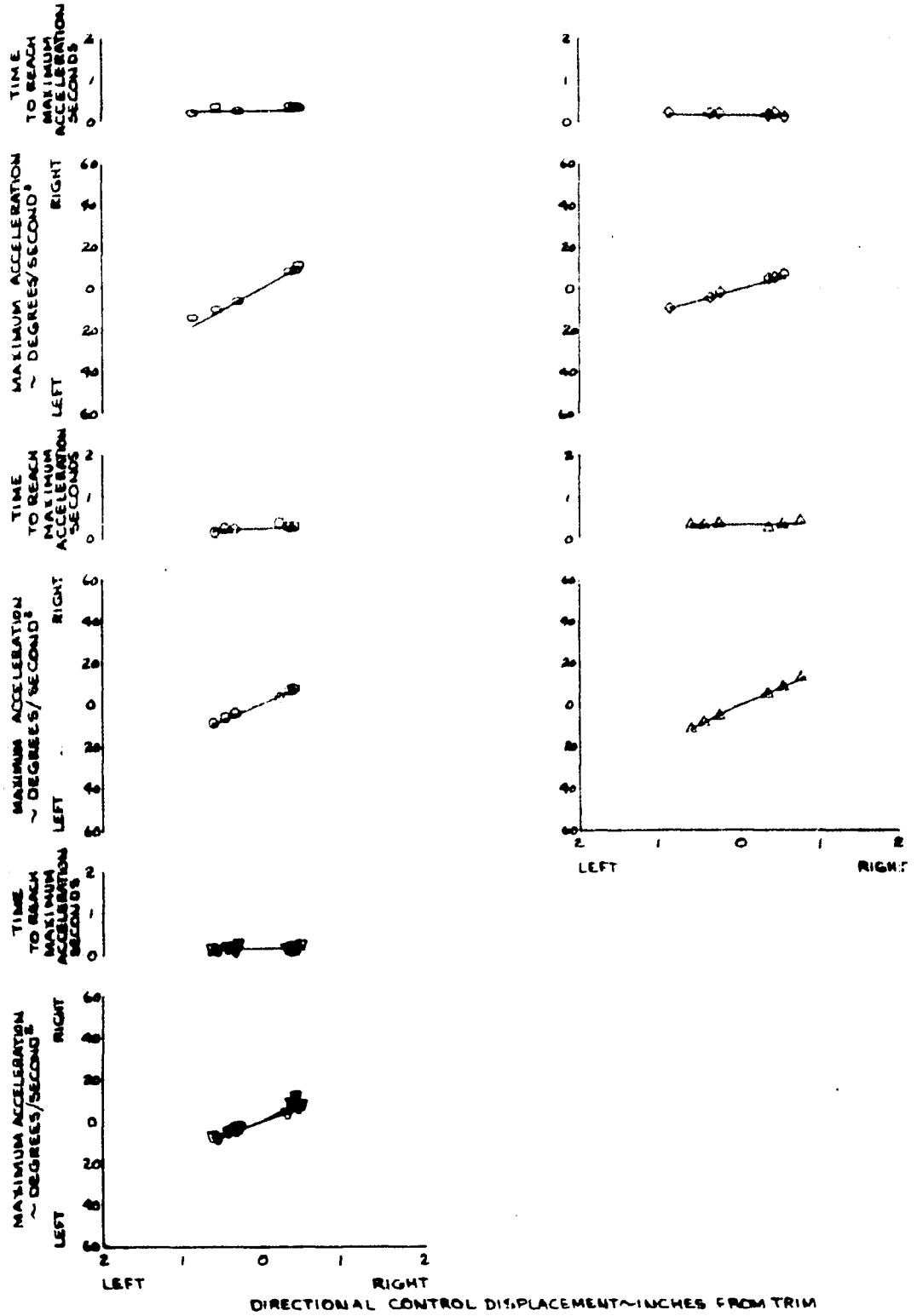


FIGURE NO. 2.53

DIRECTIONAL CONTROL RESPONSE

AN-46 USA #715695
HVV HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED
SCAS ON

SVM AIRSPEED AND ALT. AND G-M. AVG. 15.000 METER FLIGHT DURATION THROTTLE CUTOFF.
~CAS Hg - ST. ~Lb. C.G. - IN. RPM ~C¹
 0 63.0 4800 9540 200.0(AFT) 3240 LEVEL FLIGHT 0.00 5466
 0 108.0 5300 9280 200.1(AFT) 3260 LEVEL FLIGHT 0.00 5376
 0 134.0 6140 6420 200.6(AFT) 3240 LEVEL FLIGHT 0.00 5454
 0 172.0 6870 4250 199.6(AFT) 3240 DIVE 0.00 5643
 0 62.0 6350 4450 3240 CLIMB 0.00 5661
 NOTE: ALL ROCKET PODS FULLY LOADED (1634 LB)

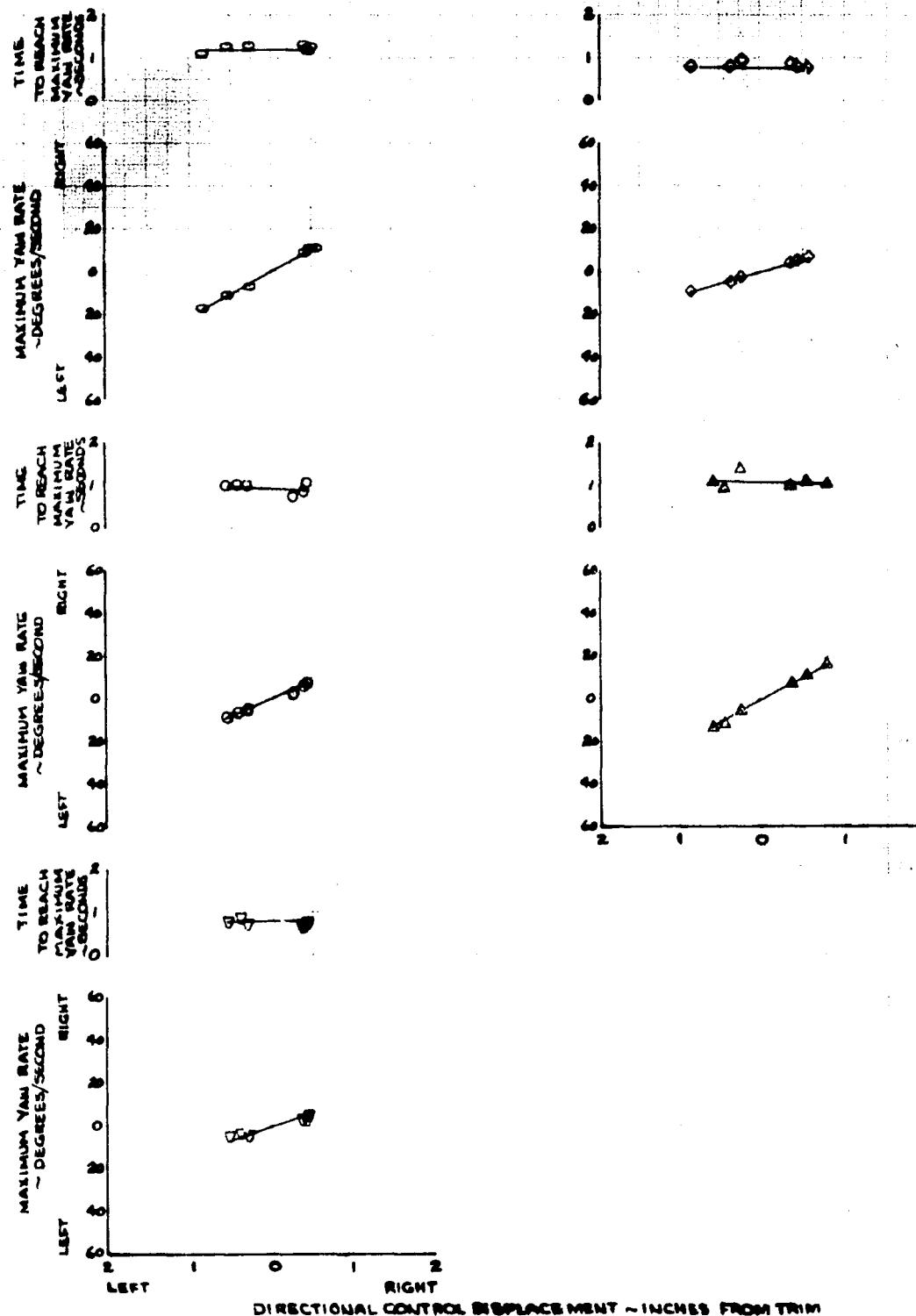


FIGURE No. 234
DIRECTIONAL RESPONSE AT ONE SECOND

AH-1G USA#4715693
 HVY. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM	AIR SPEED ~CAS	Avg. ALT. HO ~FT.	Avg. S.H. ~LS	Avg. LONG. C.G. ~IN.	MOTOR FLIGHT CONDITION	THRUST COEFF CT
O	68.0	4800	9400	200.0(FT)	3240 LEVEL FLIGHT	0.005444
O	108.0	3800	9200	200.0(FT)	3240 LEVEL FLIGHT	0.006897
D	124.0	6940	9420	200.0(FT)	3240 LEVEL FLIGHT	0.005450
D	172.0	6870	9250	199.6(FT)	3240 DIVE	0.005663
A	62.0	6380	9420	199.6(FT)	3240 CLIMB	0.005661

NOTE: OPEN SYMBOLS DENOTE SCAS ON
 1. SOLID SYMBOLS DENOTE SCAS OFF
 3. ALL ROCKET PODS FULLY LOADED (1634 LB.)

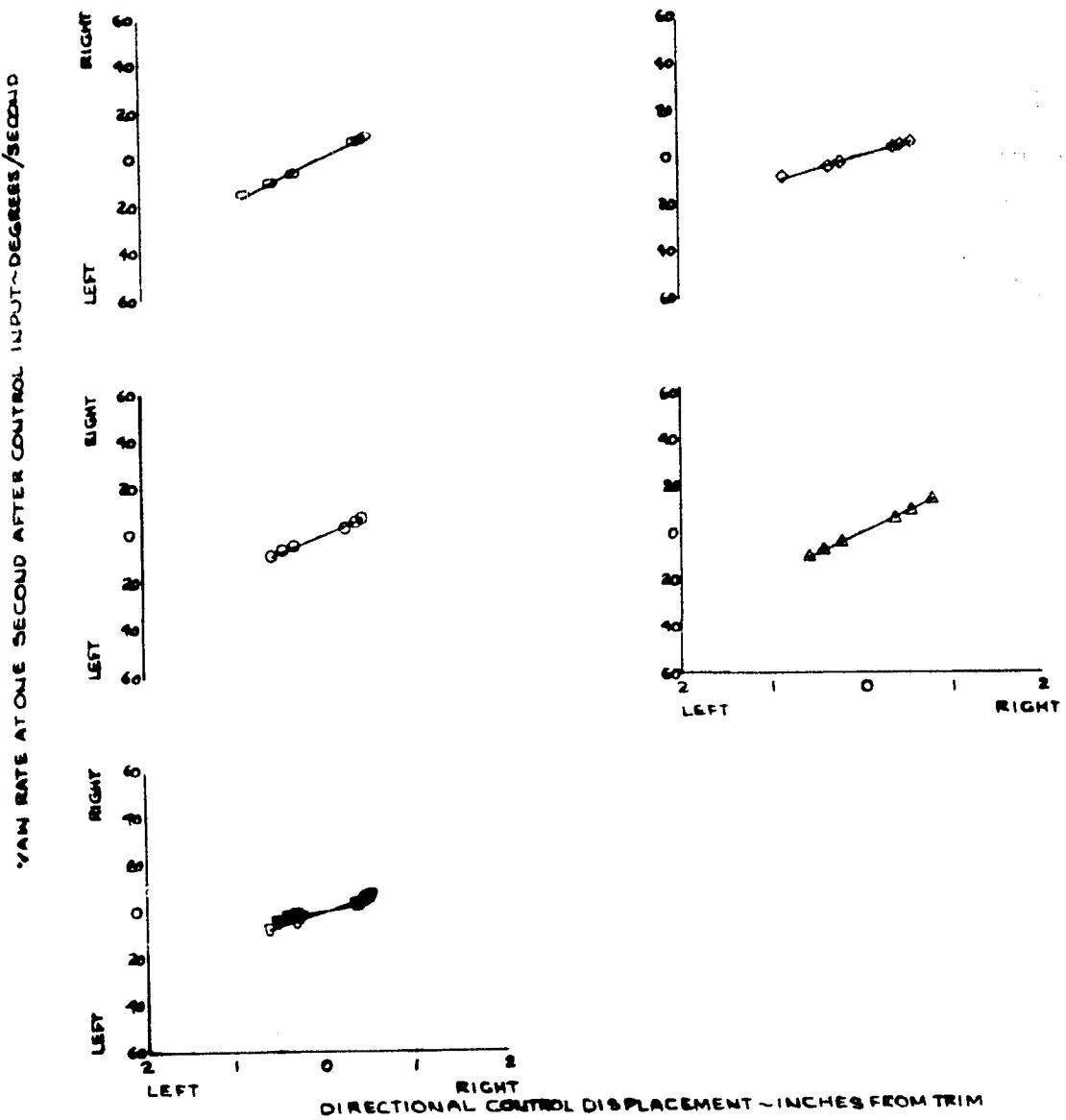


FIGURE No. 235
ANGULAR YAW DISPLACEMENT
AH-1G USAF TIGERS
HVV. HOG CONFIGURATION WITH EXKEE POD FAIRINGS REMOVED

SYM	AIRSPD	Avg. ALT.	Avg. G-LL	Avg. LONG.	MOTOR	FLIGHT	THRUST COEF.
	CAS	ft.	lb.	lb.	RPM		
o	65.0	4600	5200	200.0(AFT)	214.0	LEVEL FLIGHT	0.002644
o	100.0	5200	5200	200.0(AFT)	214.0	LEVEL FLIGHT	0.002644
o	135.0	6140	5720	200.0(AFT)	214.0	LEVEL FLIGHT	0.002644
o	172.0	6872	6260	199.6(AFT)	224.0	DIVE	0.002643
▲	62.0	6380	6380	199.6(AFT)	224.0	CLIMB	0.002661

NOTE: 1) OPEN SYMBOLS DENOTE SCAS ON
 2) SOLID SYMBOLS DENOTE SCAS OFF
 3) ALL ROCKET PODS FULLY LOADED

ANGULAR YAW DISPLACEMENT AT ONE SECOND AFTER CONTROL INPUT - DEGREES FROM TRIM

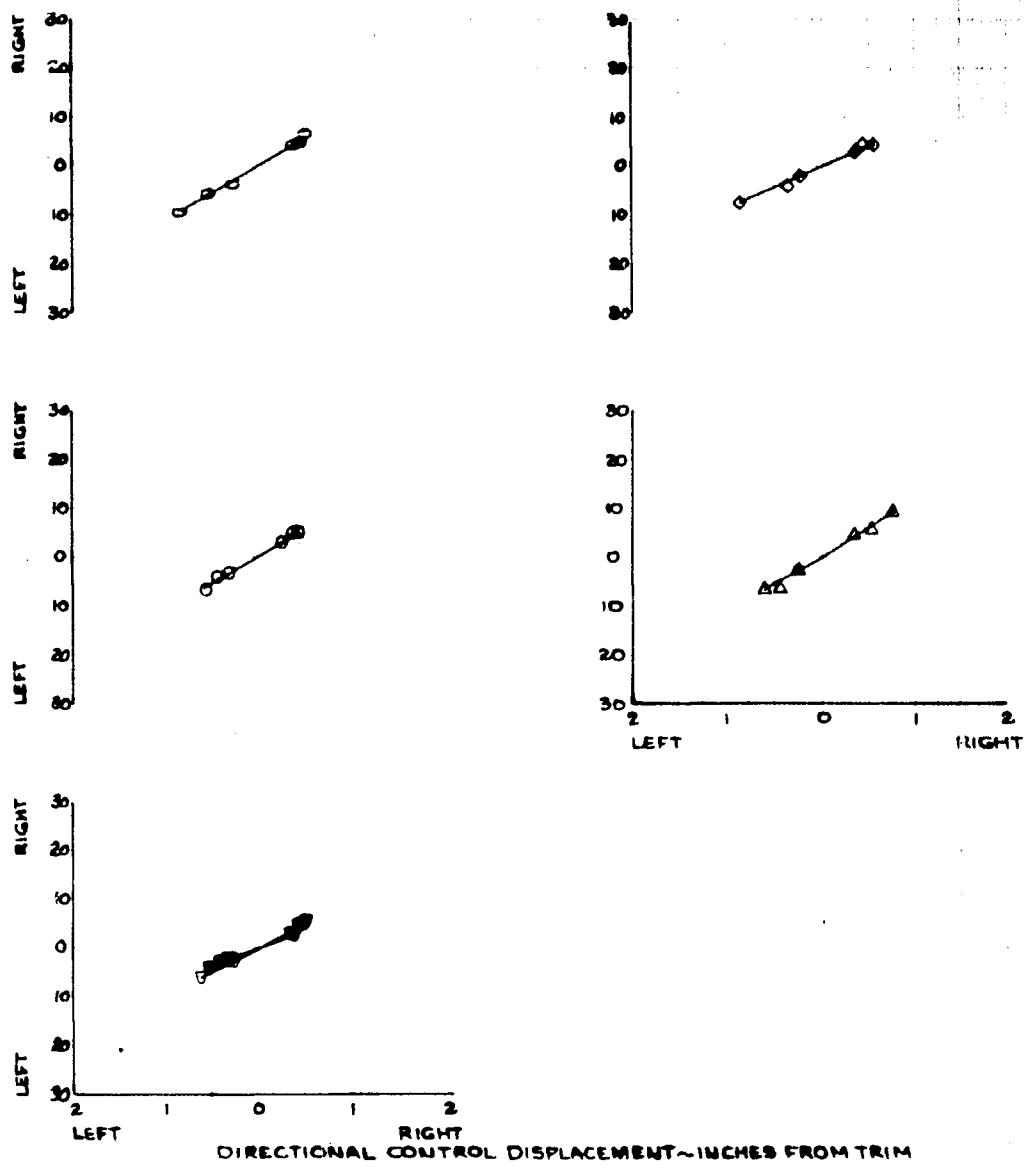


FIGURE NO. 236
DIRECTIONAL CONTROL INERTIALITY

AH-6 USAF 64-0002
HVV MOG CONFIGURATION WITH REAR SEAT SHIP DRAINED REMOVED

SYM	ARMED	AVG. ALT. IN FT.	MAX. ALT. IN FT.	AVG. LDM. IN FT.	MAX. LDM. IN FT.	DISPLACEMENT IN INCHES	MOMENTUM IN OZS
~	CAB	~10	~10	~10	~10	~10	~10
0	SLO	3100	7000	200 3000	1100 2000	LEVEL FLIGHT	0.00 2211
0	1000	3100	7000	200 3000	1100 2000	LEVEL FLIGHT	0.00 2211
0	1520	5100	7000	200 3000	1100 2000	LEVEL FLIGHT	0.00 2211
0	1720	5000	7000	200 3000	1100 2000	DIVE	0.00 2214
0	400	4000	7000	200 3000	1100 2000	CLIMB	0.00 2213
0	670	3100	7000	200 3000	1100 2000	AUTOMOTIVE	0.00 2213

NOTE: LOCH SWING SYMBOLS SCALe ON
2 SWING SYMBOLS SCALe OFF
& ALL ROCKET PODS EMPTY

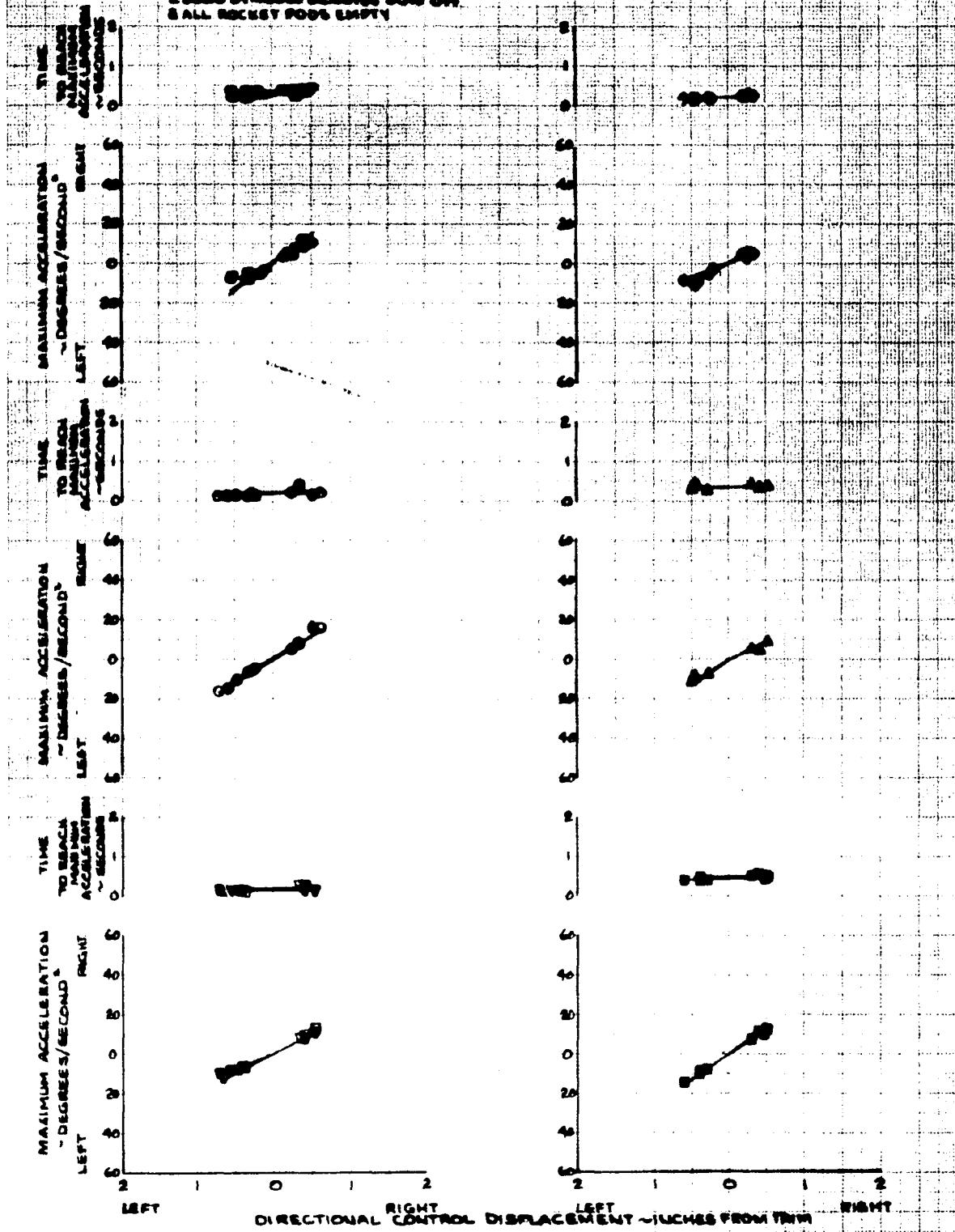


FIGURE NO. 237
DIRECTIONAL CONTROL RESPONSES
 AN-10 USAF/TIGERS
 MPP, HOG CONFIGURATION WITH REARSEAT POD FAIRINGS REMOVED
 SCAB ON

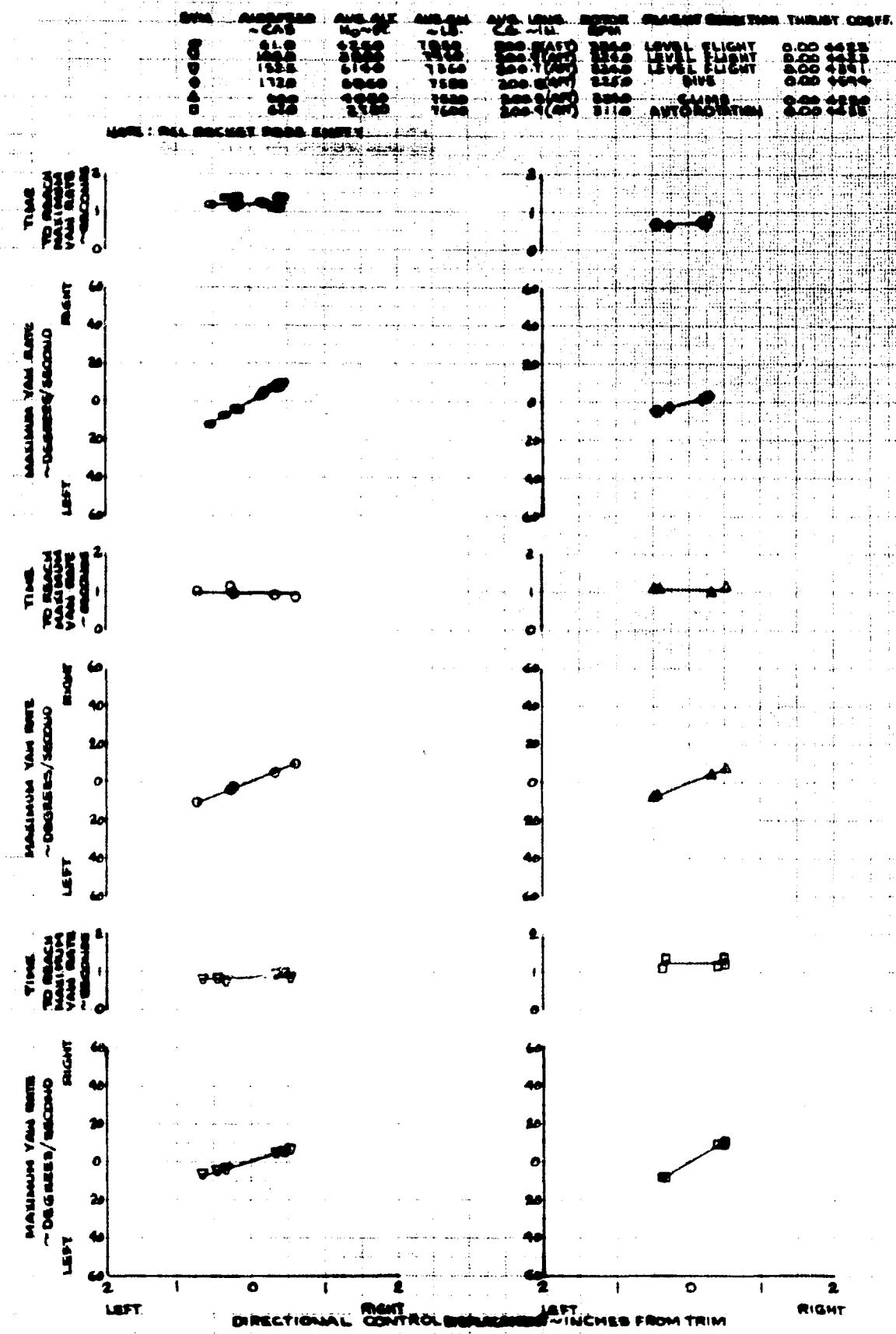


FIGURE NO. 230
DIRECTIONAL RESPONSE AT ONE SECOND
 AH-1G USAF 15685
 HVY-HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SIM	AIR SPEED	Avg. ALT. ft.	Avg. G-L	Avg. LOAD C.G. ~ IN.	ROTOR RPM	MOTOR RPM	THRUST CODE FF.
~	CAS		~ 1.0				
○	GLO	7230	1.850	200.0 (AFT)	3240	LEVEL FLIGHT	0.00 4422
○	1000	7120	1.940	200.0 (AFT)	3240	LEVEL FLIGHT	0.00 4423
○	153.5	6190	1.860	200.7 (AFT)	3240	LEVEL FLIGHT	0.00 4424
○	172.0	6860	1.880	200.8 (AFT)	3250	DIVE	0.00 4424
△	60.0	4080	1.830	200.8 (AFT)	3240	CLIMB	0.00 4420
□	61.0	2100	1.800	200.9 (AFT)	3110	AUTOROTATION	0.00 4435

NOTE: OPEN SYMBOLS DENOTE SCAB ON
 SOLID SYMBOLS DENOTE SCAB OFF
 ALL ROCKET PODS EMPTY

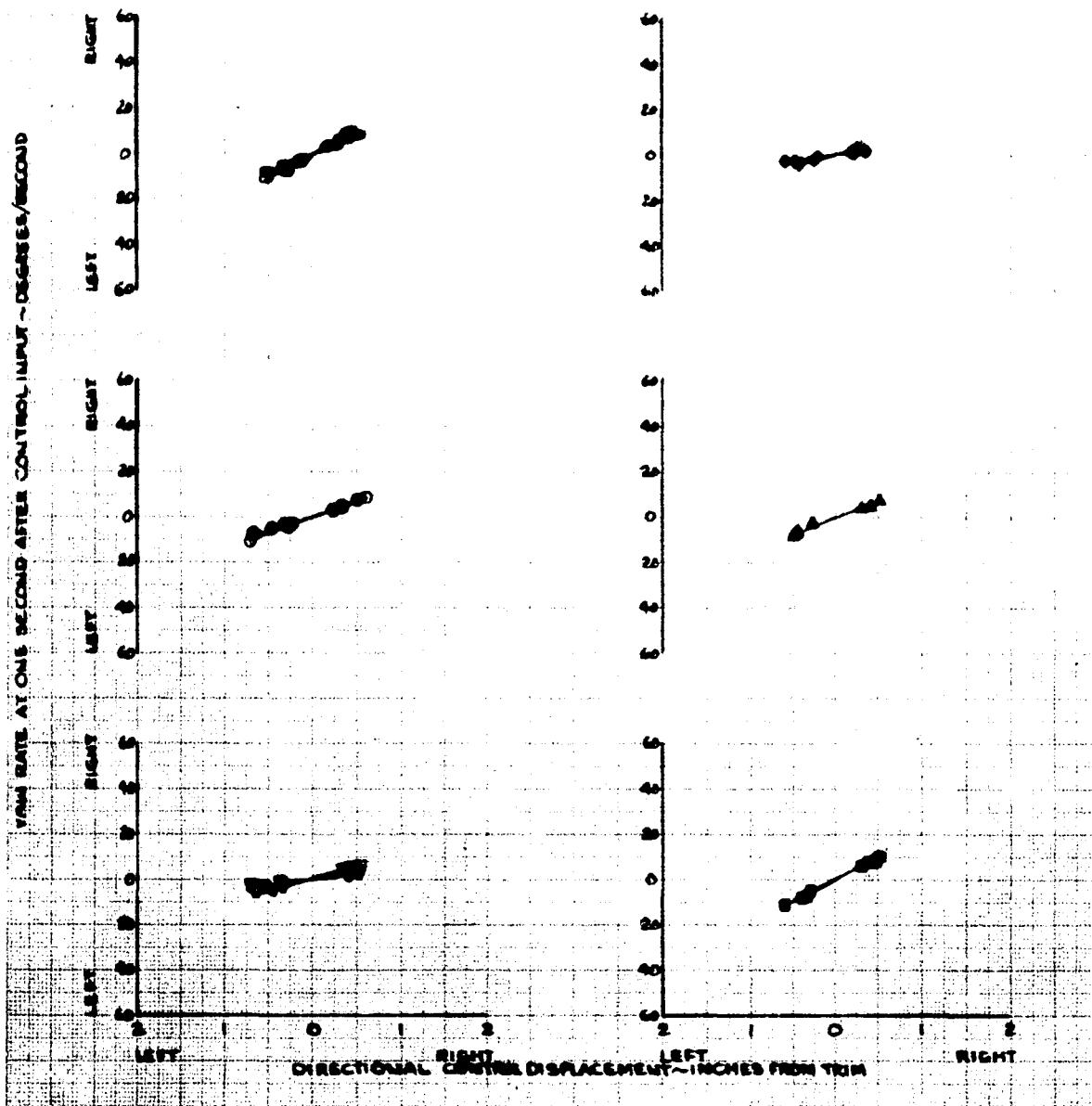


FIGURE No. 239
 ANGULAR VAN DISPLACEMENT
 AH-1G UCAV/TIGERS
 MVY. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

TIME	ANGLE RAD	ANGLE DEG								
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.025	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.050	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.075	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.100	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.125	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.150	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.175	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.200	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.225	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.250	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.275	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.300	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.325	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.350	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.375	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.400	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.425	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.450	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.475	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.500	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.525	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.550	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.575	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.600	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.625	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.650	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.675	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.700	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.725	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.750	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.775	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.800	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.825	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.850	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.875	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.900	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.925	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.950	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.975	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
1.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

NOTE: OPEN SYMBOLS DENOTE OCAS ON
 2 SOLID SYMBOLS DENOTE OCAS OFF
 3 ALL ROCKET PODS EMPTY

ANGULAR VAN DISPLACEMENT AT ONE SECOND AFTER CONTROL
 INPUT - DEGREES FROM TRIM

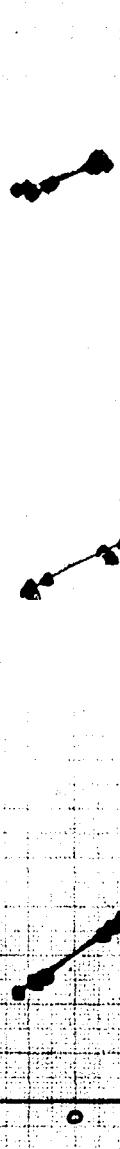
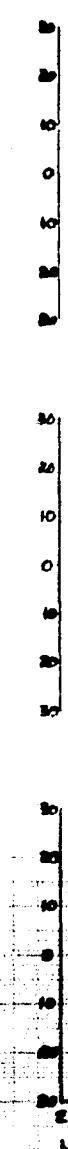
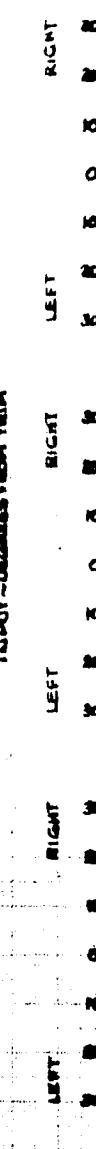


FIGURE NO 240
DIRECTIONAL CONTROL SENSITIVITY
AH-1G USA 671568
HVT. HOG CONFIGURATION WITH BOOMET POD FAIRINGS REMOVED

STM AIRSPEED AVG ALT AVG G.M. AVG LONG. ROTOR BLADES C.G. THRUST COEFF.
 ~CAS ~ft ~deg ~in. ~ft ~N ~C
 000 88.0 15780 7860 200.9(FT) 3228 LEVEL FLIGHT 0.002222
 000 88.0 15810 7600 200.3(FT) 3228 LEVEL FLIGHT 0.002222
 000 105.0 15840 7780 200.4(FT) 3250 LEVEL FLIGHT 0.006214

NOTES: 1. OPEN CIRCUIT BRAKES SET ON
 2. SOLID BRAKES BRAKE 100% OFF
 3. ALL ROCKET PODS EMPTY

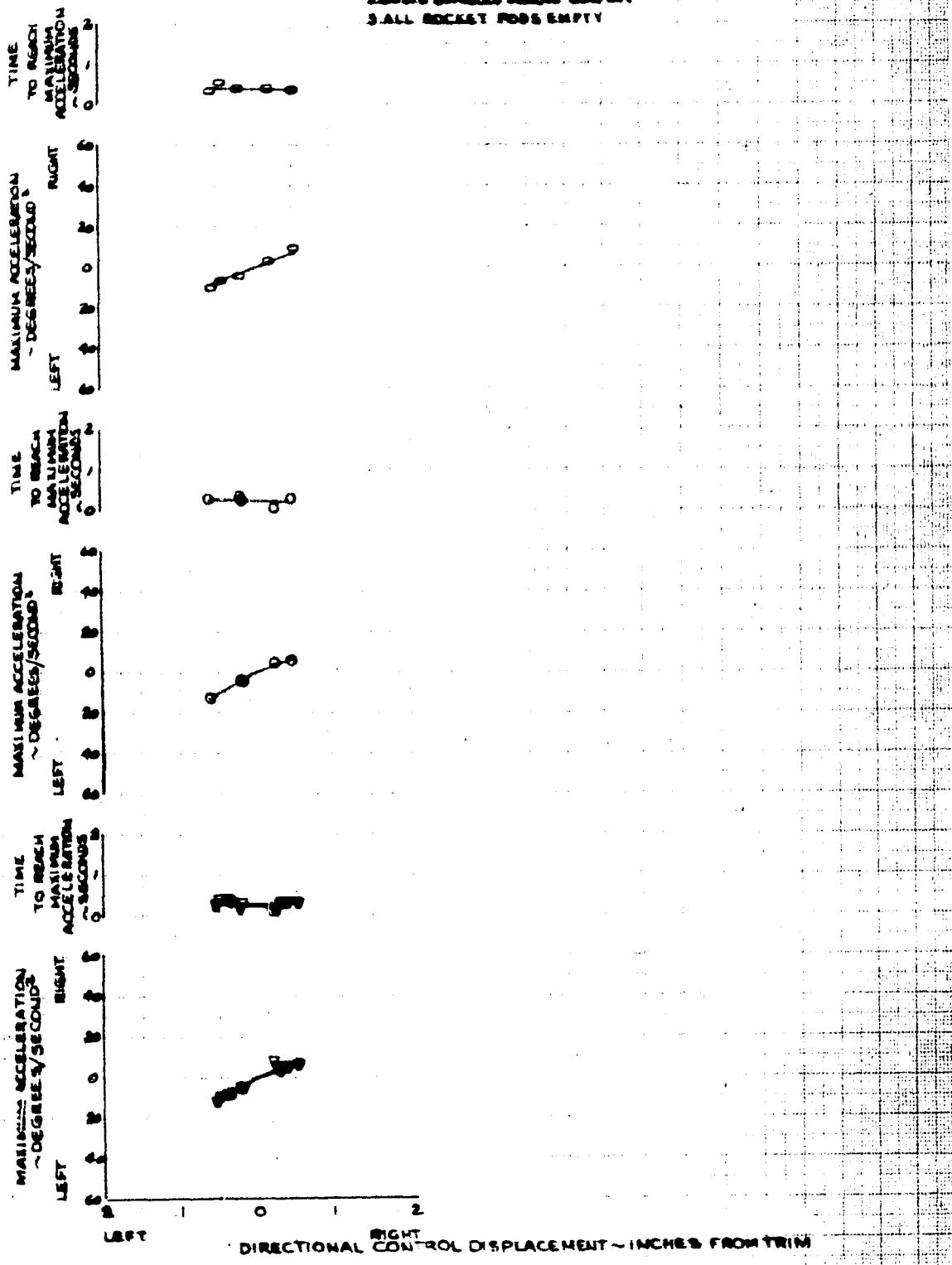


FIGURE NO. 241
DIRECTIONAL CONTROL RESPONSES

CH-16 USA 571668
 HVY HOG CONFIGURATION WITH SIDE POD FRAMING'S REMOVED
 SEAS ON

SYM. AIRFIELD - AVG ALT AND G.A. AND LOAD FRACTION DETERMINED FROM TAILBL STS.
 - CAS NO. 11.25 C2 11.25
 510 15100 1700 200.00% DOUBLE LEVEL FLIGHT 000 2323
 625 15210 1700 200.00% DOUBLE LEVEL FLIGHT 000 2323
 1040 15300 1700 200.00% DOUBLE LEVEL FLIGHT 000 2323

NOTE: ALL TESTS AT 100% POWER

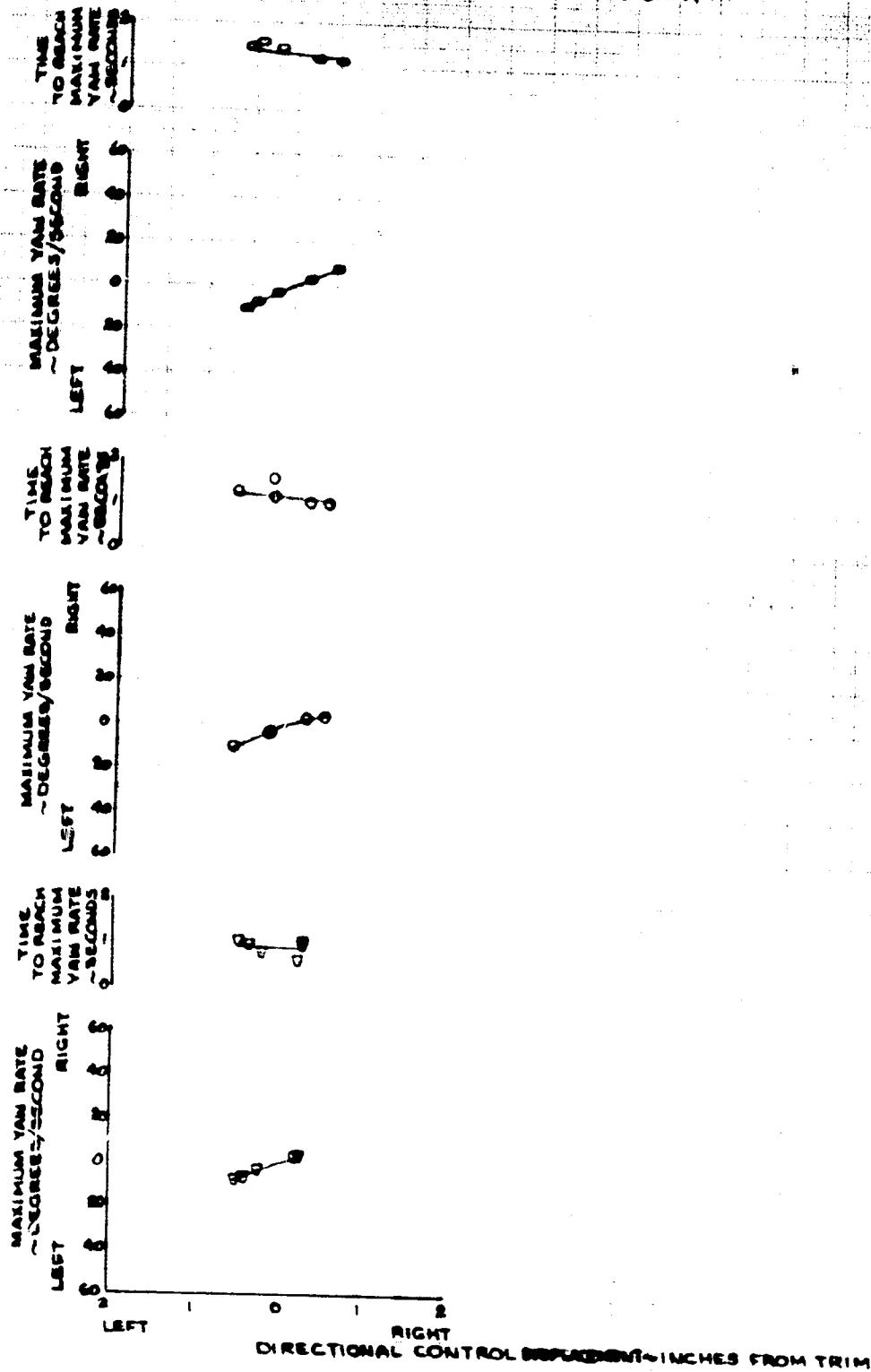


FIGURE NO. 242
DIRECTIONAL RESPONSE AT ONE SECOND

AH-1G USAF 715693
 HVY. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM	AIR SPEED	ANG. ALT.	ANG. W.	AVG. LONG. ROLL	FLIGHT SEQUENCE	TWIST COEF.
~CAS	400-500	~10°	CG ~14°	8PM	-C1	
○	510	15780	7460	200.9(FT) 3240	LEVEL FLIGHT	0.006363
○	520	16810	7600	208.8(FT) 3240	LEVEL FLIGHT	0.006368
○	1050	16860	7780	200.9(FT) 3240	LEVEL FLIGHT	0.006374

NOTES: 1. OPEN SYMBOLS DENOTE SCADS ON
 2. SOLID SYMBOLS DENOTE SCADS OFF
 3. ALL ROCKET PODS EMPTY

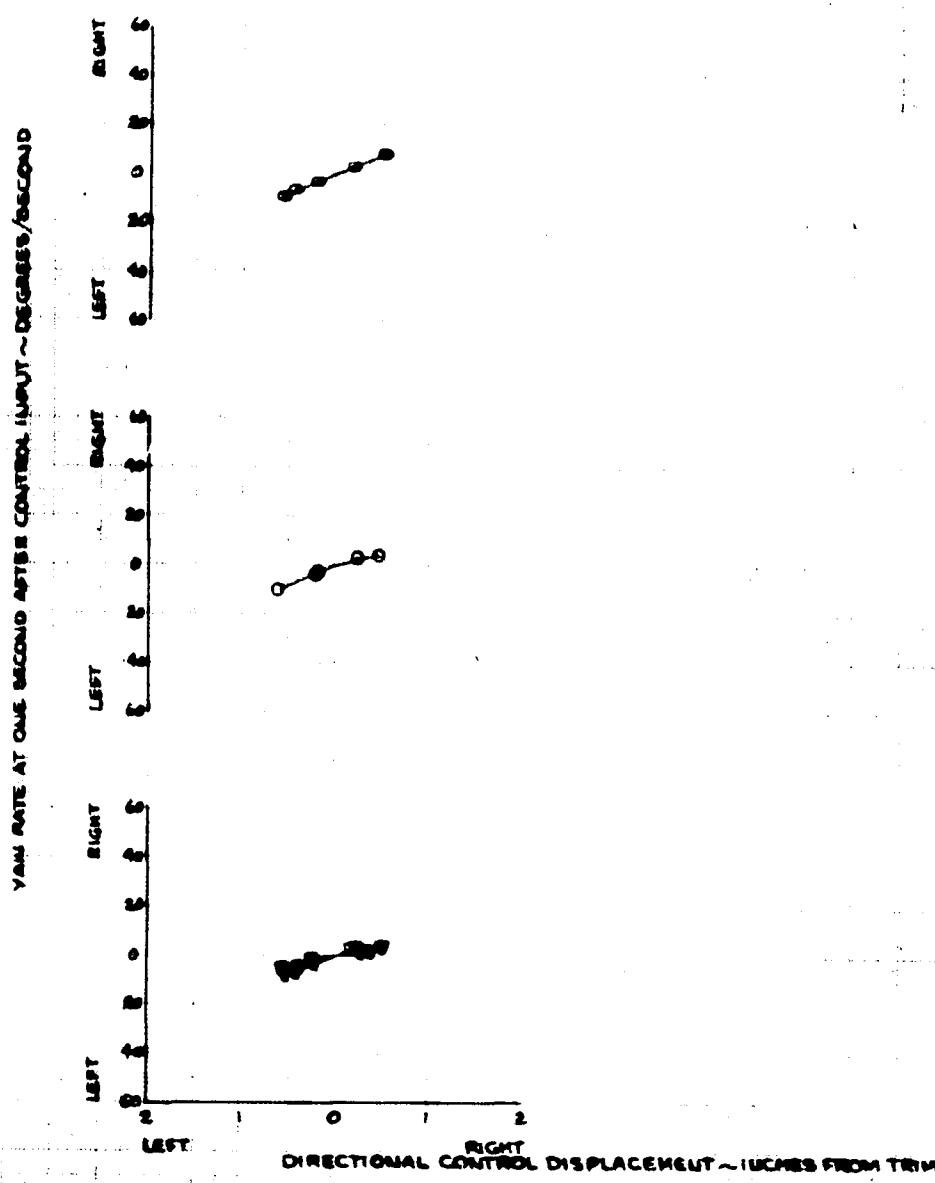


FIGURE NO. 243
ANGULAR VAN DISPLACEMENT

AM-1G USA #18648
 HVY. HOG CONFIGURATION WITH BOOM POD FAIRINGS REMOVED

SYM AIRSPEED AVG. ALT. AVG. G.M. AND LONG. ROTOR FLIGHT CONDITION. THRUST COEFF. ~C₁
 ~CAS Hg - FT. ~LB. C.G. - IN. RPM
 0 510 16160 7700 200.0 (RFT) 3100 LEVEL FLIGHT 0.006285
 0 620 12810 7500 200.0 (RFT) 3100 LEVEL FLIGHT 0.006232
 0 1020 16160 7600 200.0 (RFT) 3240 LEVEL FLIGHT 0.006254

NOTE: OPEN SYMBOLS DENOTE SCAS ON
 SOLID SYMBOLS DENOTE SCAS OFF
 ALL BOOM PODS EMPTY

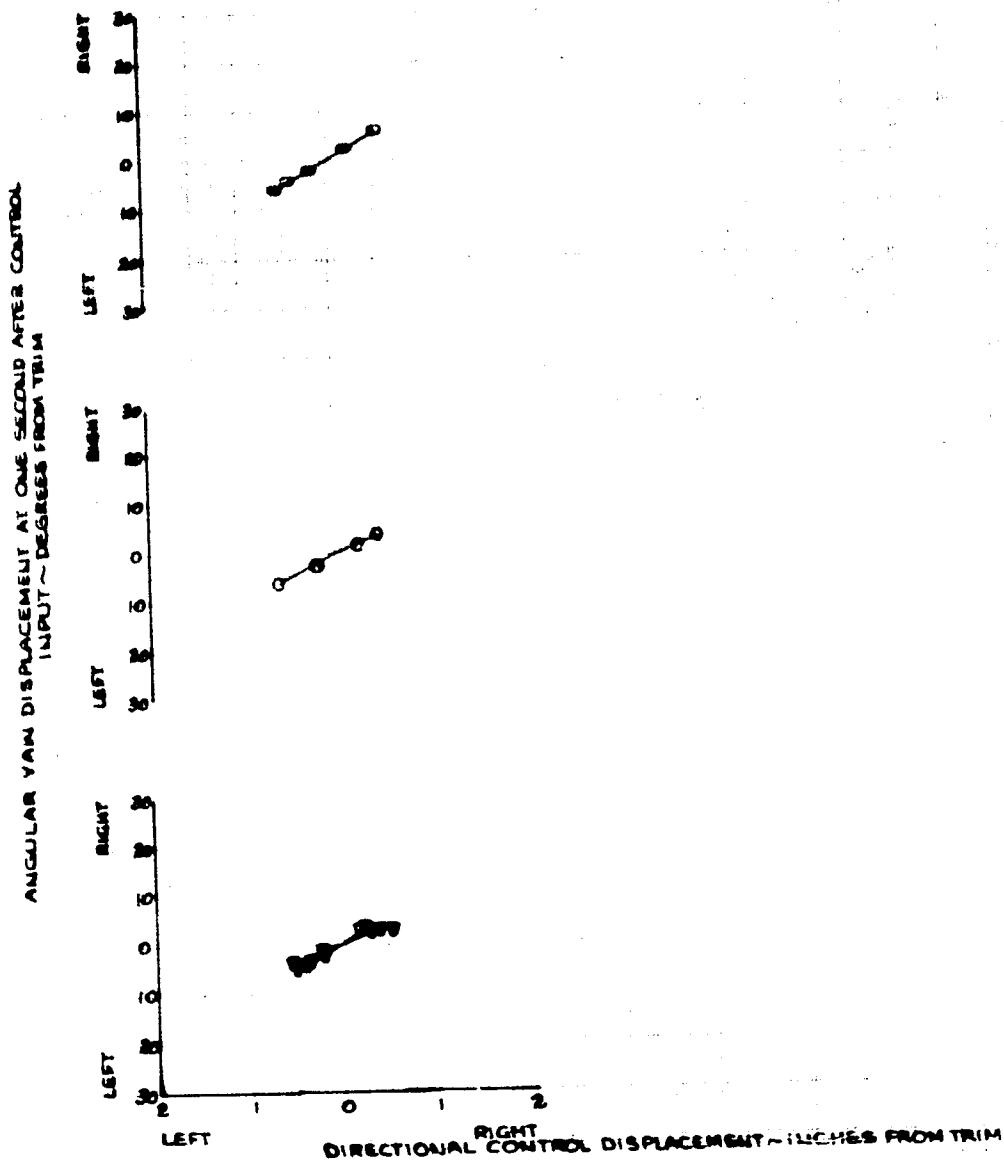


FIGURE NO. 244
LONGITUDINAL CONTROLLABILITY SUMMARY DURING HOVER

AH-1G

SYM. COINING S/N POD LOADING
 O CLEAN 610301 NO PODS
 ♦ MVT NO SIGNAT. NOTED
 ♦ MVT NO SIGNAT. PODS EMPTY
 □ MVT. MNG TURNS NOTED

NOTES: 1. OPEN SYMBOLS DENOTE FORWARDED INPUT
 2. SOLID SYMBOLS DENOTE AST INPUT
 3. PLAIN SYMBOLS DENOTE SCAS ON
 4. SOLIDED SYMBOLS DENOTE SCAS OFF
 5. (V) ALL ROCKET PODS EMPTY
 6. (D) 611 LB. IN USED ROCKET PODS, 501 LB. IN USED
 ROCKET PODS. 1876 LB. TOTAL
 7. POINTS DERIVED FROM FIGURES 245 THROUGH
249, APPENDIX 2D

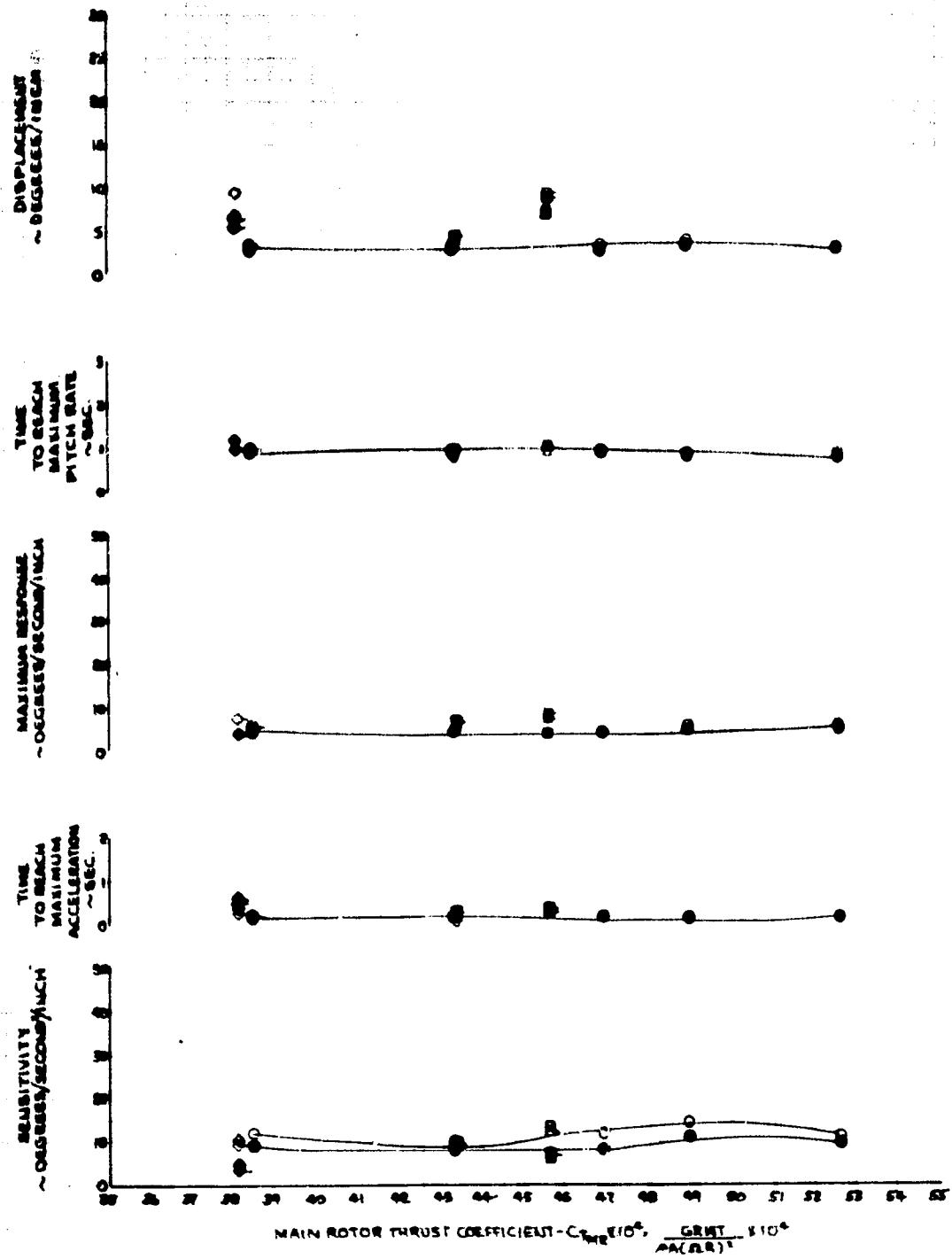


FIGURE NO. 245
LATERAL CONTROLLABILITY SUMMARY DURING HOVER
AH-1G

SYM CONFIG S/N POD LOADING

- O CLEAN G15207 NO PODS
 - ▲ HVY. HOG G15207 ALL PODS EMPTY
 - HVY. HOG G15207 NOTED
 - HVY. HOG G15207 ALL PODS LOADED
 - HVY. HOG TIGER NOTED
 - ◊ HVY. HOG TIGER ALL PODS EMPTY
- NOTES: 1. OPEN SYMBOLS DENOTE LEFT INPUT. 2. SCAS ON - 387 LB. IN OUTBD ROCKET PODS
 3. SOLID SYMBOLS DENOTE RIGHT INPUT SCAS OFF - 554 LB. IN OUTBD ROCKET PODS
 4. PLAIN SYMBOLS DENOTE SCAS ON 5. ALL ROCKET PODS FULLY LOADED (1634 LB.)
 6. FLAGGED SYMBOLS DENOTE SCAS OFF 7. POINTS DERIVED FROM FIGURES 257 THROUGH 266
 APPENDIX XII.

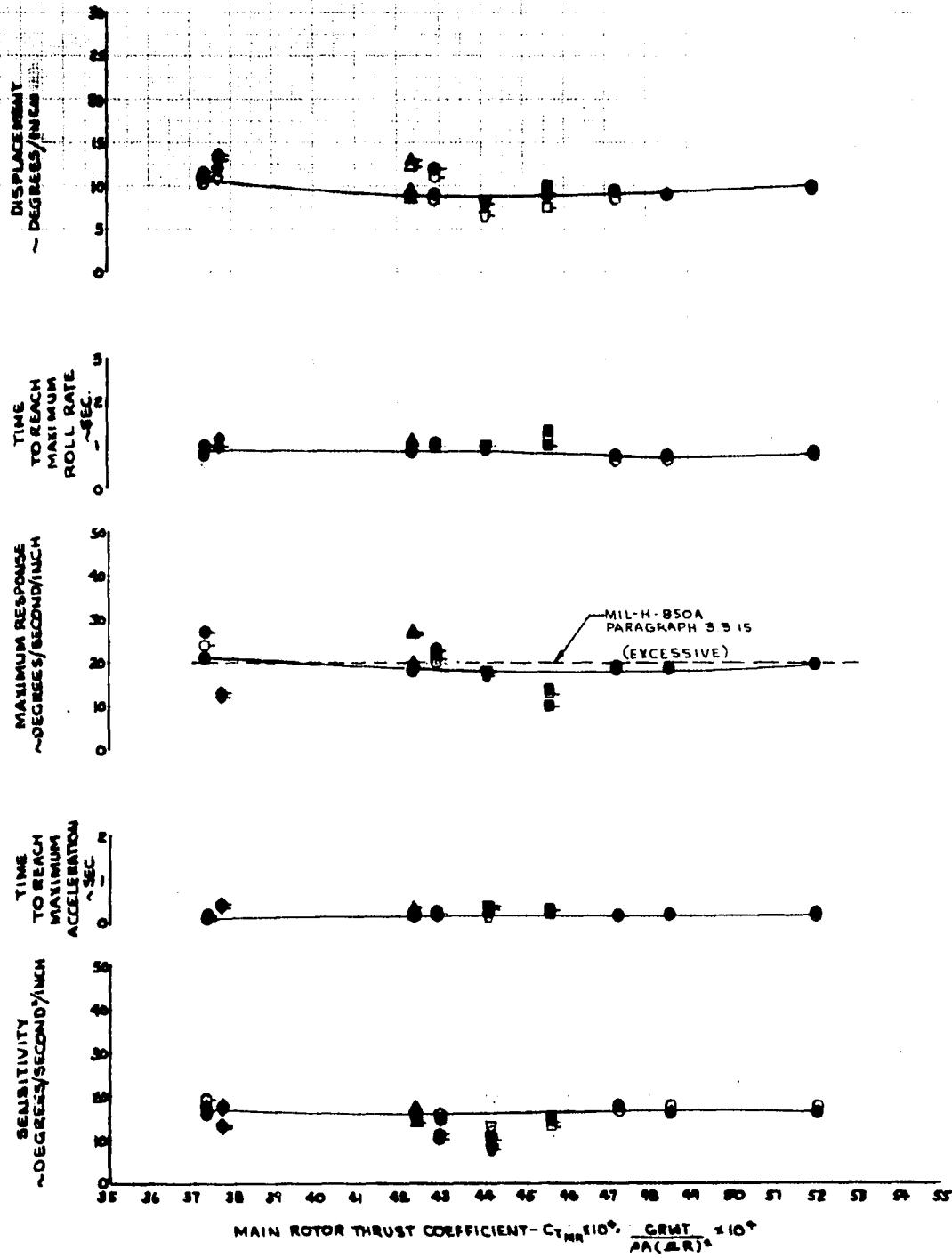


FIGURE NO 246
DIRECTIONAL CONTROLLABILITY SUMMARY-DURING FLIGHT
AH-1G

SYM CONFIG S/N POD LOADING

○	CLEAN	615207	NO PODS
△	HVV. HOG	615207	PODS EMPTY
□	HVV. HOG	615207	NOTED
○	HVV. HOG	715615	PODS EMPTY
□	HVV. HOG	715615	NOTED

NOTES: 1. OPEN SYMBOLS DENOTE LEFT INPUT
 2. SOLID SYMBOLS DENOTE RIGHT INPUT

6. 615 LB. IN OUT PODS, 301 LB. IN OUTED PODS, 1116 LB. TOTAL.

3. PLAIN SYMBOLS DENOTE SCAS ON
 4. FLAGGED SYMBOLS DENOTE SCAS OFF

7. DATA POINTS ADJUSTED TO COINCIDE WITH MAXIMUM
 AVAILABLE PEDAL ALMOST CRITICAL SKID HEIGHT

5. (7) $C_T = 0.004651 \sim$ ALL ROCKET PODS EMPTY
 $C_T = 0.004304 \sim 359$ LB. IN OUTED PODS

8. POINTS DERIVED FROM FIGURES 267 THROUGH 279,
 APPENDIX XII

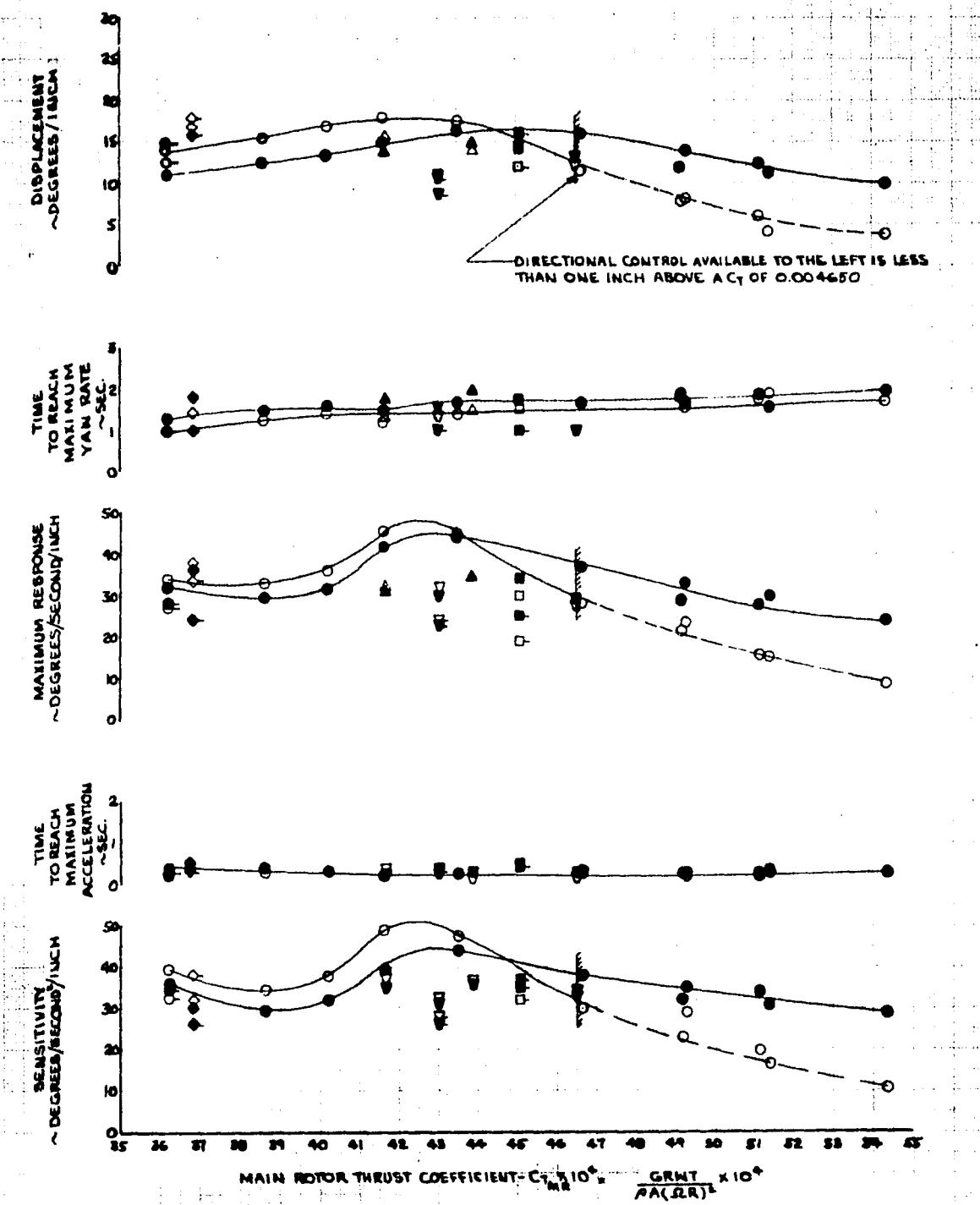
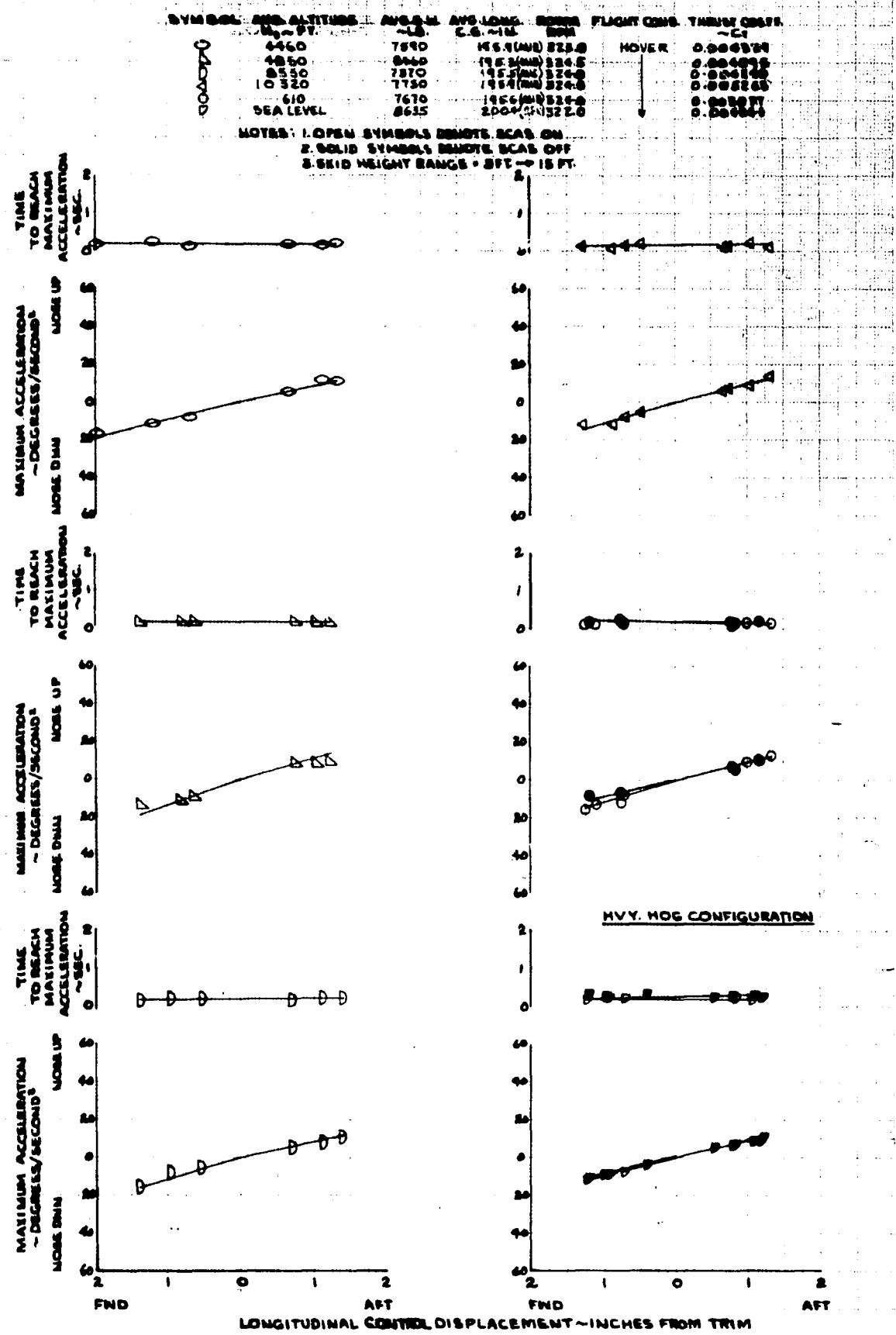


FIGURE NO. 247
LONGITUDINAL CONTROL SENSITIVITY
AH-1G USAF/HB/SDT
CLEAN CONFIGURATION



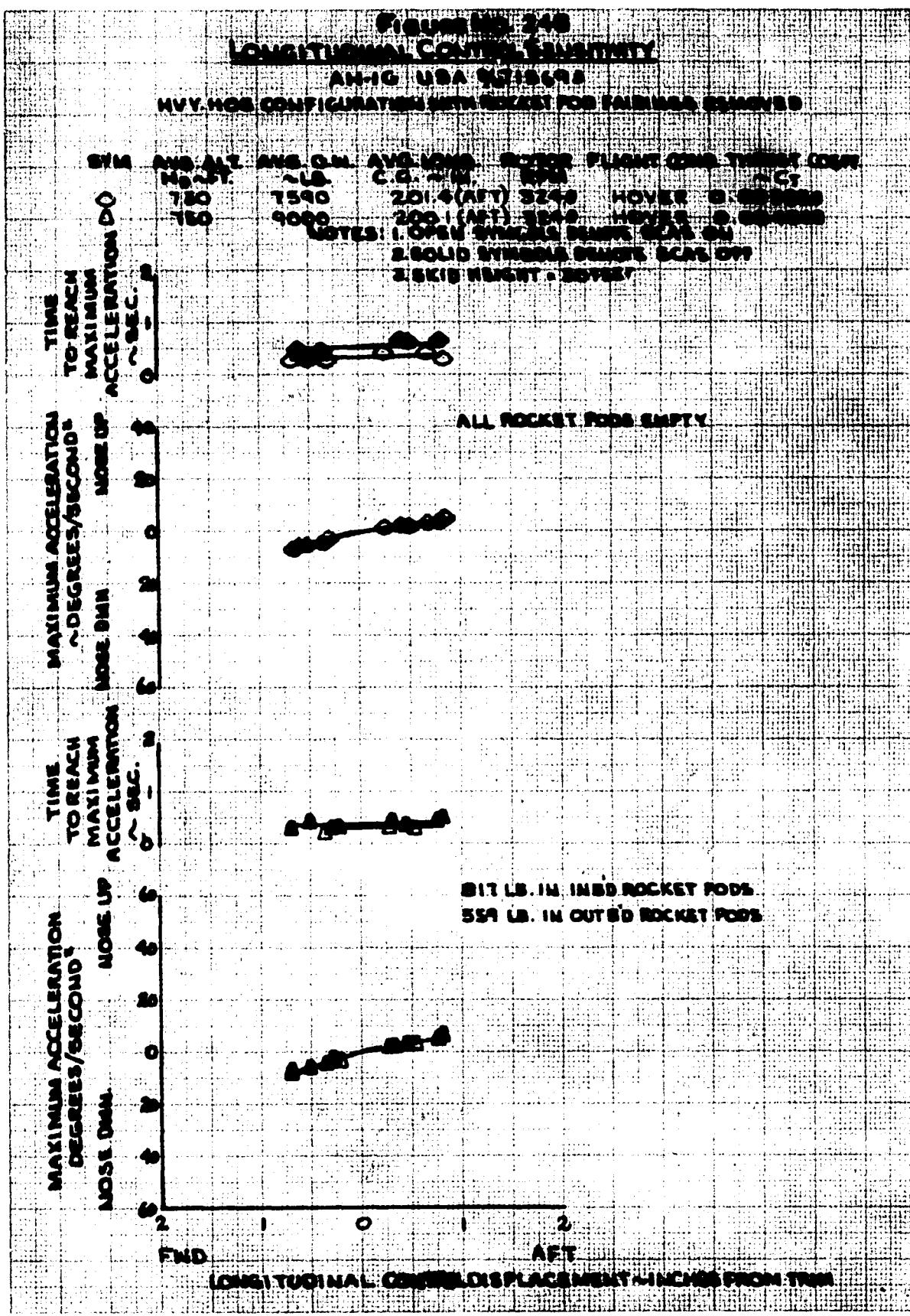


FIGURE NO 247
LONGITUDINAL CONTROL SENSITIVITY

AH-1G USA% 615507
HVY. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYMBOL AVE ALT. ANG. GAI. AVE. LONG. ROLL. PITCH. CRSS. THRUST. CRNT.
 Hr ~ ft. ~ deg. C.G. ~ in. RPM ~ C.P.
 D SEA LEVEL 8685 220.4 3010 10000 0.004341

NOTES: OPEN SYMBOLS DENOTE SEAS ON
 2. SOLID SYMBOLS DENOTE SEAS OFF
 3. ALL SEAS OFF VALUES READ AT ONE SECOND
 4. SKID HEIGHT RANGE = 3FT. → 15 FT.

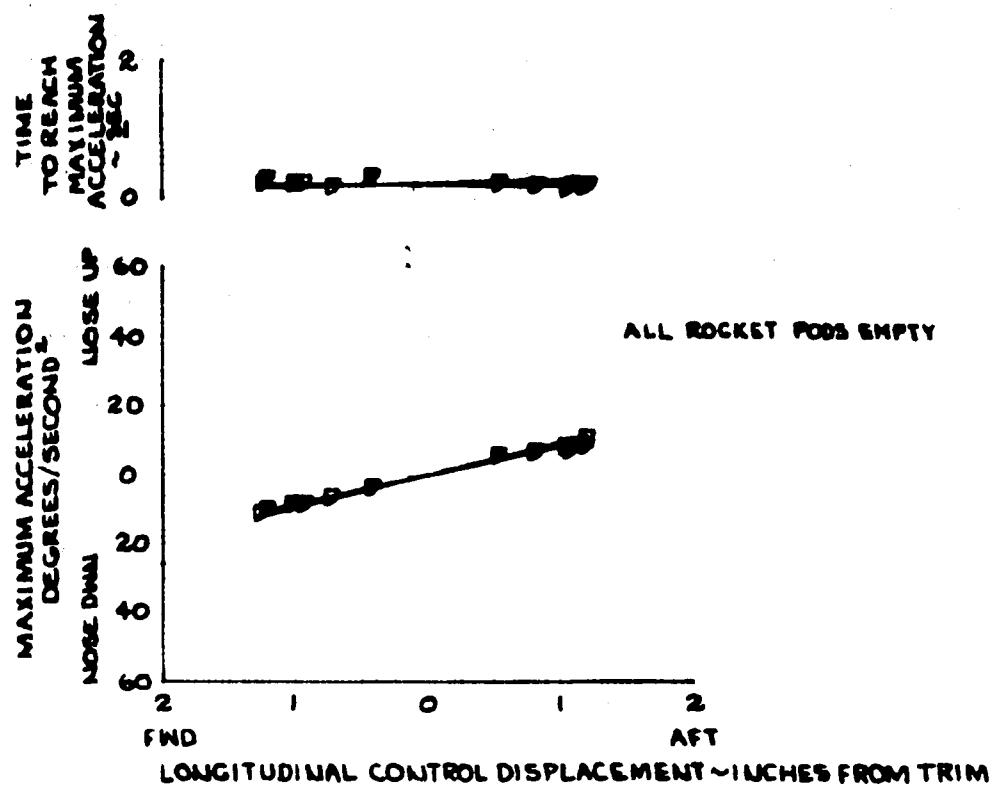


FIGURE NO. 250
 LONGITUDINAL CONTROL RESPONSE.
 AH-1G UBAK 6.080T
 CLEAN CONFIGURATION

SYMBOLS	Avg G-L ALTITUDE ~ FT.	Avg G-L. C.G. - IN.	Avg LONG. MOTOR RPM	FLIGHT COMD. THRUST COEF. ~ CT
0	4460	7590	195.9(MID)	0.000332
0	4650	8560	195.5(MID)	0.000345
0	8550	7810	195.5(MID)	0.000348
0	10320	7750	195.9(MID)	0.000326
0	610	1670	195.6(MID)	0.0003671

NOTES: 1. OPEN SYMBOLS DENOTE SCAS ON
 2. SOLID SYMBOLS DENOTE SCAS OFF
 3. ALL SCAS ON RESPONSE VALUES ARE MAXIMUMS
 4. ALL SCAS OFF RESPONSE VALUES READ AT ONE SECOND
 5. SKID HEIGHT (BNGT) = 5 FT. = 16 FT.

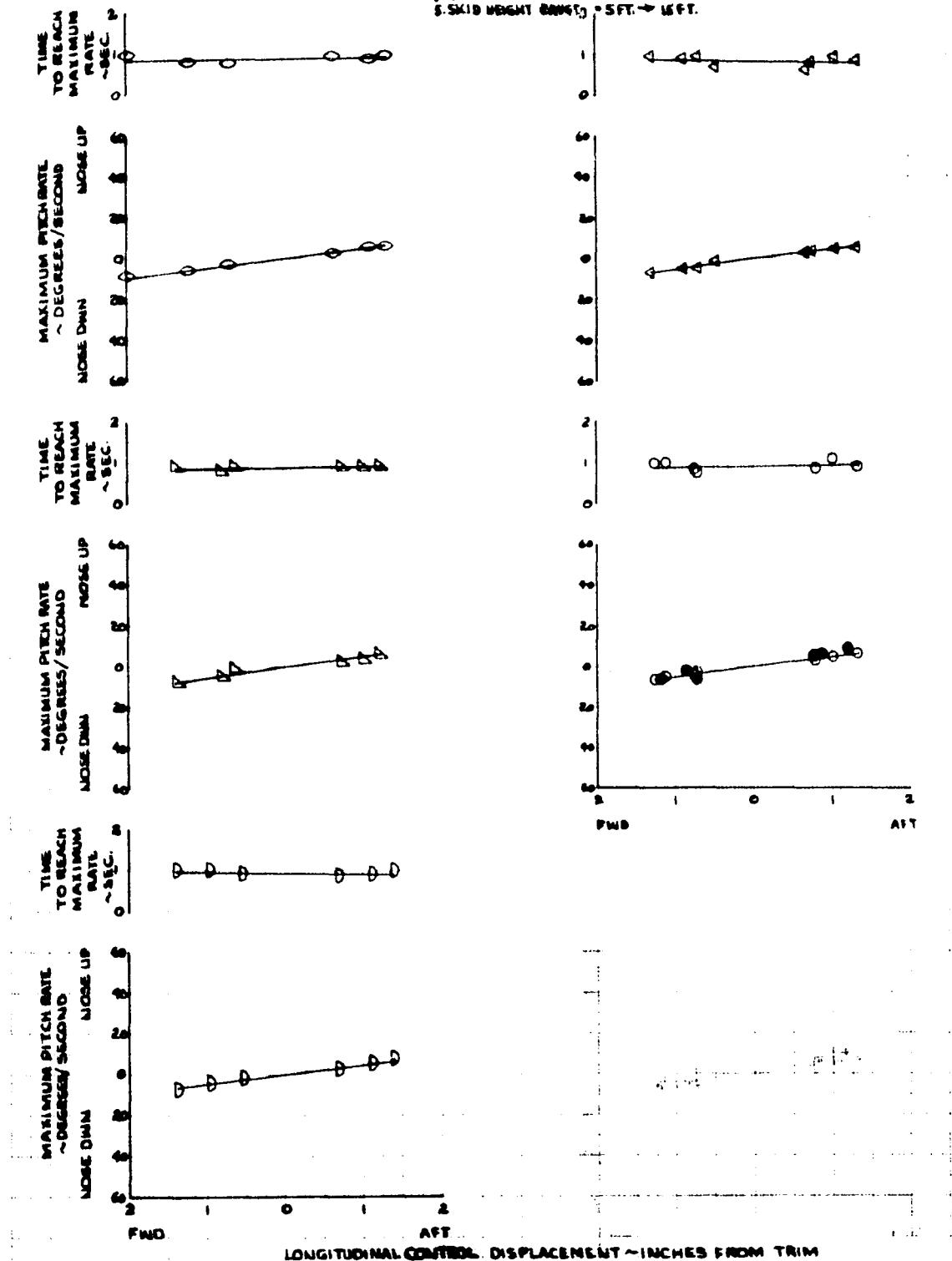


FIGURE NO. 251
LONGITUDINAL CONTROL RESPONSES

AH-1G USA #71568

HVV. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED
 SCAS ON

SYM. AVG. ALT. AVG. G.W. AVG. LONG. ROTOR FLIGHT COMP. THRUST COEFF.

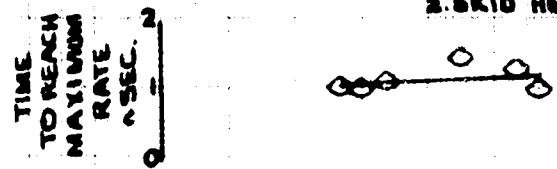
HGT-FT ~LB C.G. ~IN RPM ~CT

O 730 7590 201.4(AFT) 324.0 HOVER 0.005000

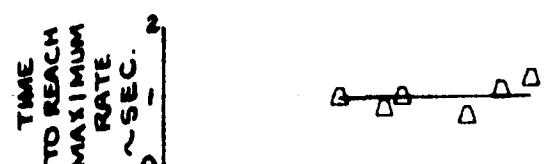
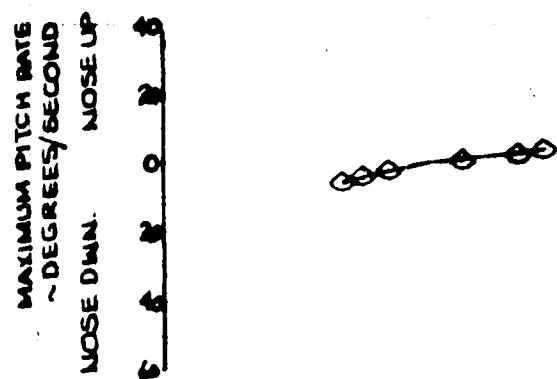
O 750 9000 200.1(AFT) 324.0 HOVER 0.004000

NOTES: 1. ALL SCAS VALUES ARE MAXIMUM

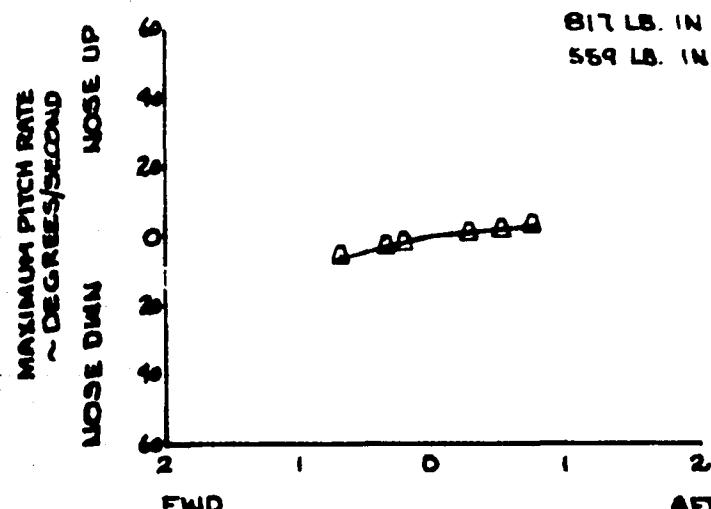
2. SKID HEIGHT = 30 FT.



ROCKET PODS EMPTY



817 LB. IN INBOARD ROCKET PODS
 559 LB. IN OUTBOARD ROCKET PODS



LONGITUDINAL CONTROL DISPLACEMENT ~ INCHES FROM TRIM

FIGURE No. 252
LONGITUDINAL RESPONSE AT ONE SECOND

AH-1G USA #15698
 HVY. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED
 SCAS OFF

SYM	Avg. Alt. Hg, ft.	Avg. G.W. ~LB.	Avg. Long. C.G. ~IN.	Rotor Flight Cond. 201.4 (AFT) 324.0	Thrust Off. RPM	~GT
○	730	7590	201.4 (AFT)	324.0		HOVER 0.003800
△	750	9000	200.1 (AFT)	324.0		HOVER 0.004800

NOTE: SKID HEIGHT = 30 FT.

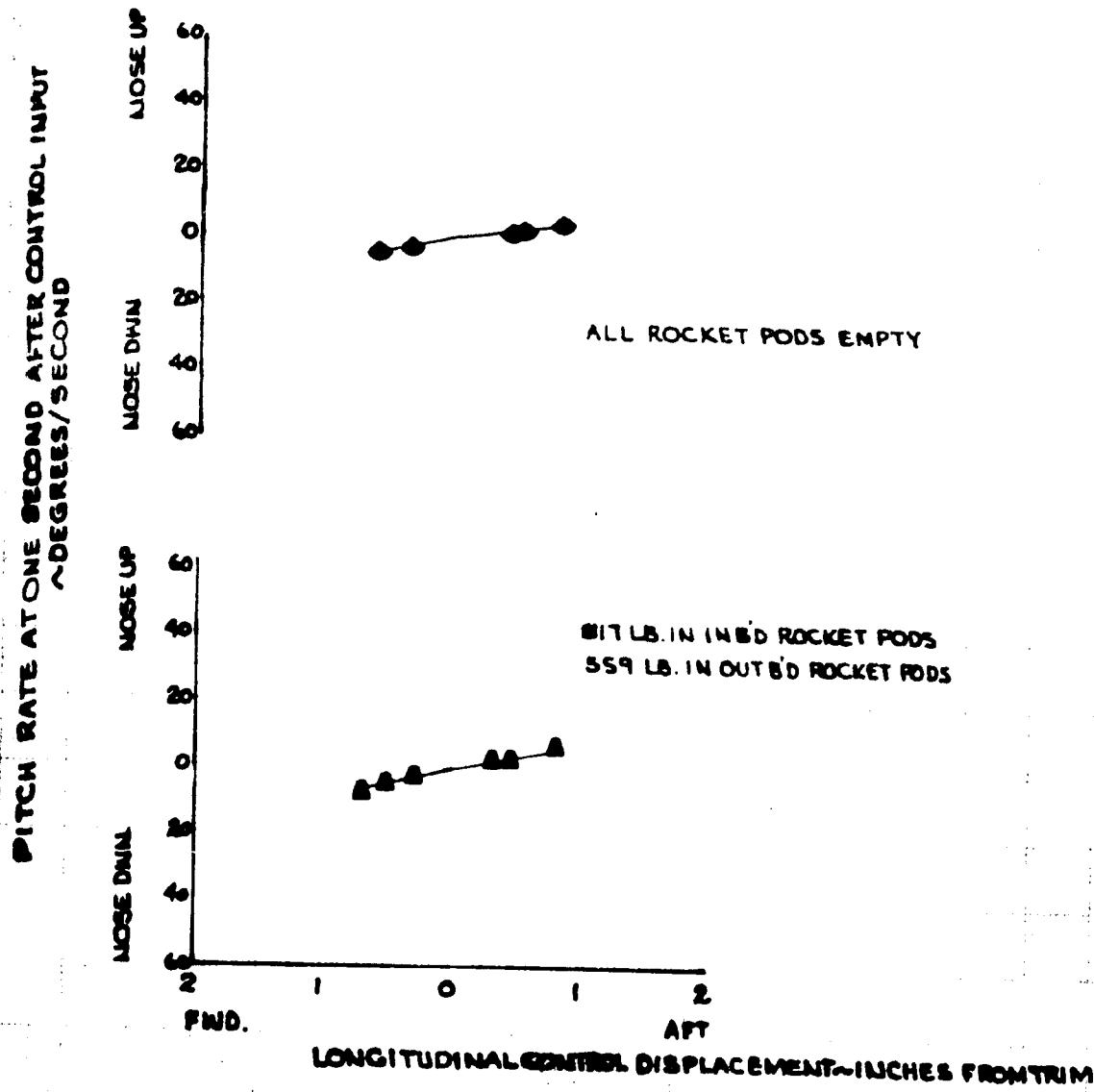


FIGURE No 253
LONGITUDINAL CONTROL RESPONSE
AH-1G USA 1/15/5993
HVV. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYMBOLS: AVG. ALI. AVG. G.M. AVG. LONG. ROTOR PLT. COMD. THRUST COEF.
 HGT. ~LD. C.D. ~IL. RPM ~CT
 D SEA LEVEL 8635 200.48FT) 322.0 HOVER 0.004261

- NOTES: 1. OPEN SYMBOLS DENOTE SCAS ON 4. ALL SCAS OF VALUES READ AT ONE SECOND
 2. SOLID SYMBOLS DENOTE SCAS OFF 5. SKID HEIGHT RANGE = 5FT → 15FT.
 3. ALL SCAS ON VALUES ARE MEANINGS

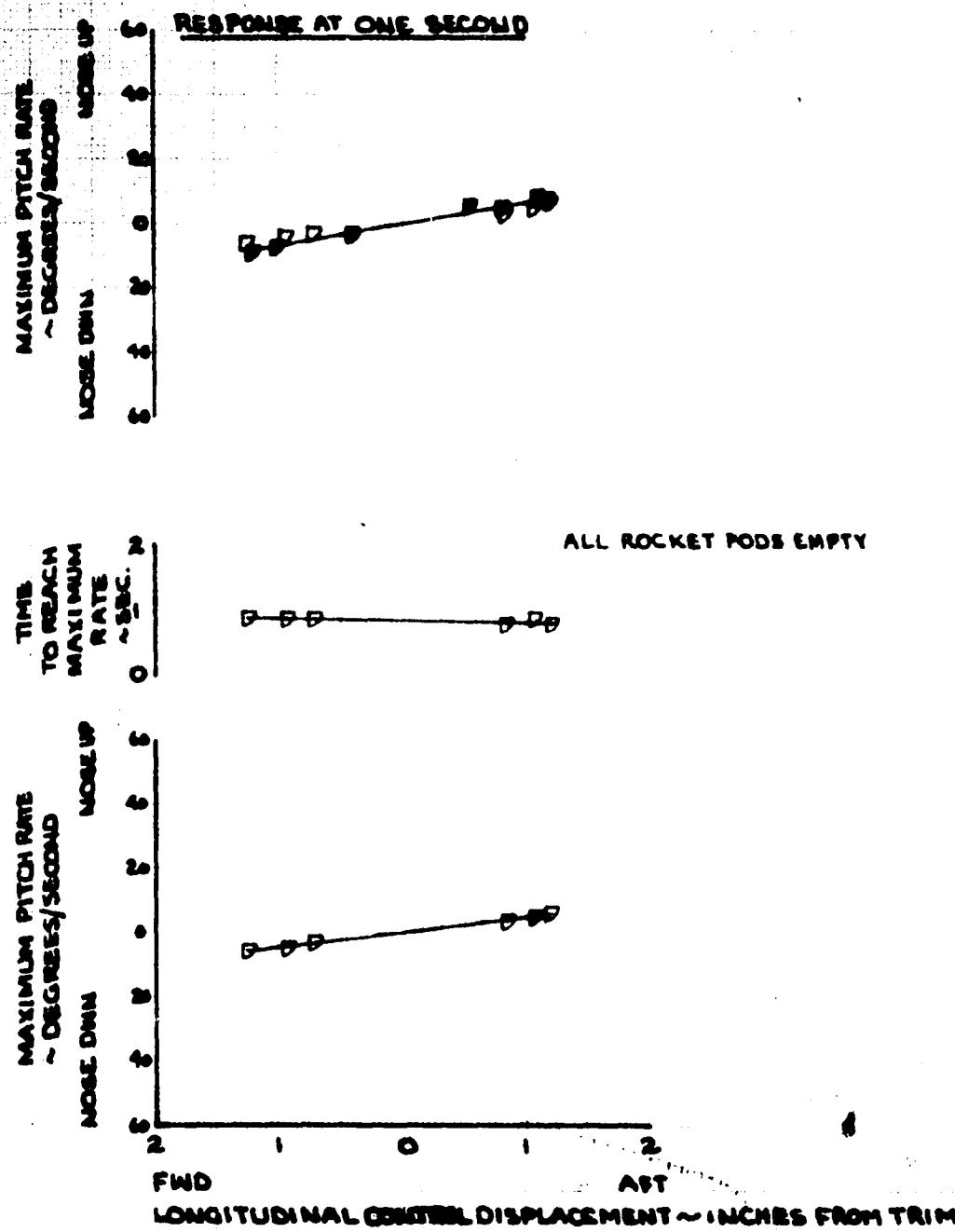
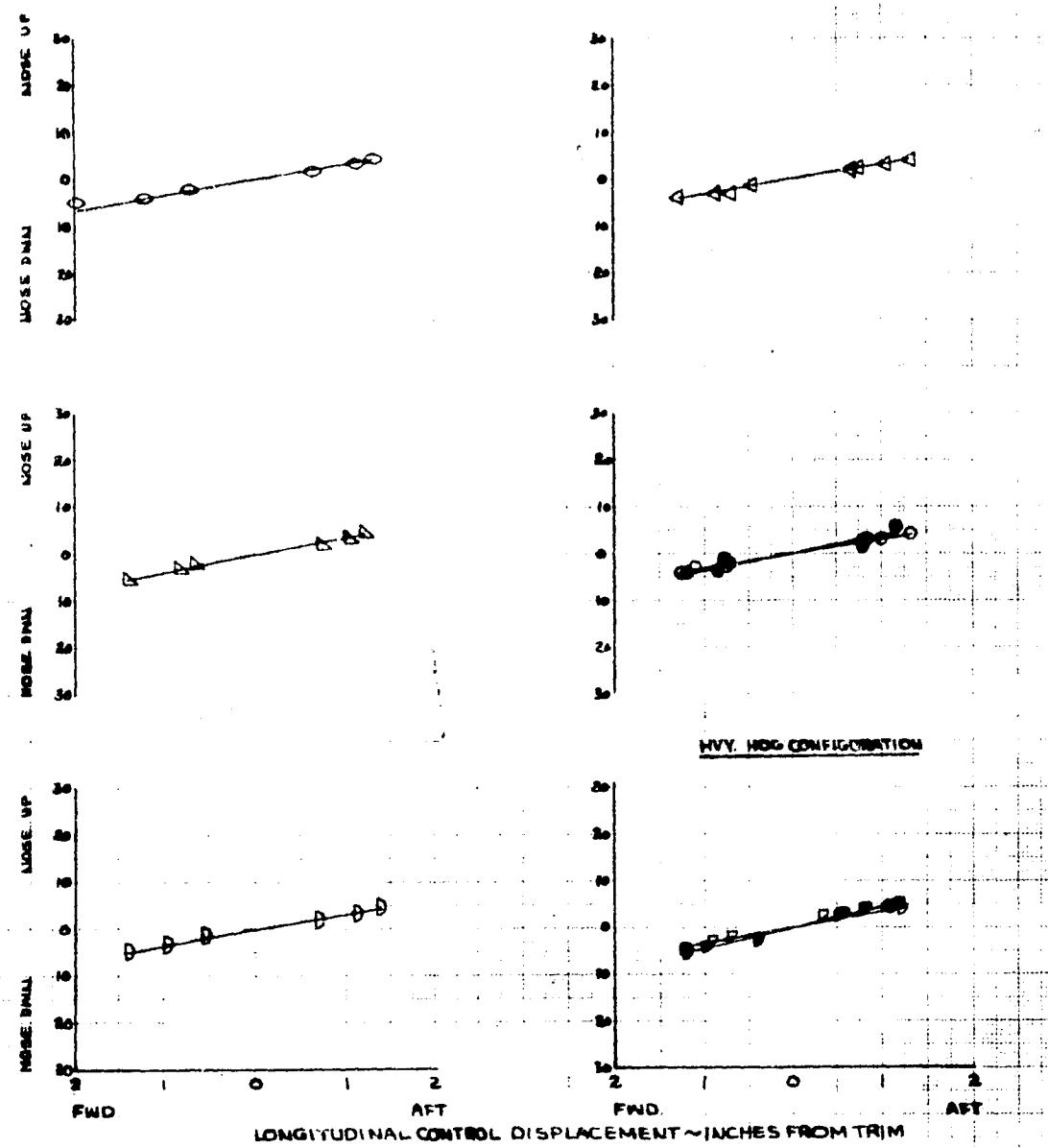


FIGURE NO. 254
 ANGULAR PITCH DISPLACEMENT
 AH-1G USAKA 847
 CLEAN CONFIGURATION

SYMBOLS AND ALTITUDE: AVG. G. W. ANG. LOME. ROTOR RPM. FLIGHT COND. TURBINE COADS
 $H_s \sim 77, 11$
 -LS C.G.-14L
 4450 7000 195.0 (H14) 328.0 HOVER D. G. 14L
 4850 7000 195.5 (H14) 328.5
 5250 7070 195.5 (H14) 328.0
 10250 7050 195.5 (H14) 328.0
 1450 7050 195.5 (H14) 328.0
 SEA LEVEL 9015 2004 (AFT) 328.0

NOTES: 1. OPEN SYMBOLS DENOTE SCAS ON
 2. SOLID SYMBOLS DENOTE SCAS OFF
 3. SKID HEIGHT RANGE = 5FT-18.5 FT

ANGULAR PITCH DISPLACEMENT AT ONE SECOND AFTER CONTROL INPUT ~ DEGREES FROM TRIM



HVV. HOG CONFIGURATION

Figure No. 255
ANGULAR PITCH DISPLACEMENT

AH-1C USAF TIGERS
 HVY. MOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM.	Avg. Alt. HO. FT	Avg. GM. ~LB.	Avg. Long. CG. ~IN.	ROTOR RPM	FLIGHT COND.	THRUST COEFF.
O	730	7290	2014(AFT)	3240	HOVER	0.00750
S	750	9000	2001(AFT)	3240	HOVER	0.00660

NOTES: 1. OPEN SYMBOLS DENOTE SCAS ON
 2. SOLID SYMBOLS DENOTE SCAS OFF
 3. SKID HEIGHT = 30FT.

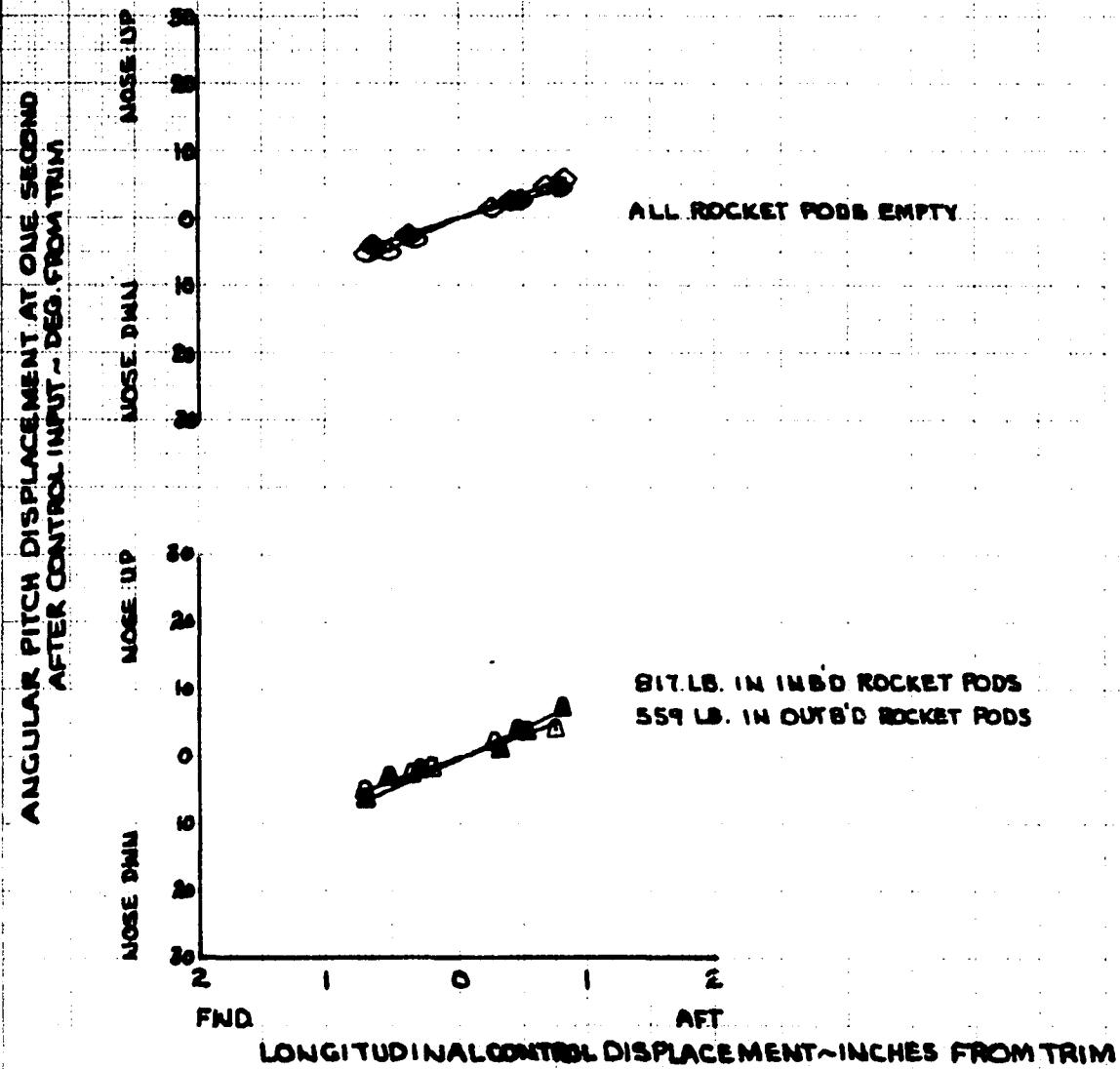


FIGURE NO. 256
ANGULAR PITCH DISPLACEMENT

AH-1G USA BN 615247

HVV. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYMBOL AVG. ALT. AVG.G.W. AVG.LONG. ROTOR FLT.COND. THRUST COEFF.
 H₀.FT. ~LB. C.G ~IN. RPM ~CT

D SEA LEVEL 8633 200.4 322.0 HOVER 0.00434

NOTES: 1. OPEN SYMBOLS DENOTE SCAS ON
 2. SOLID SYMBOLS DENOTE SCAS OFF
 3. SKID HEIGHT RANGE - 5 FT → 15 FT.

ANGULAR PITCH DISPLACEMENT AT ONE SECOND AFTER
 CONTROL INPUT ~ DEG. FROM TRIM

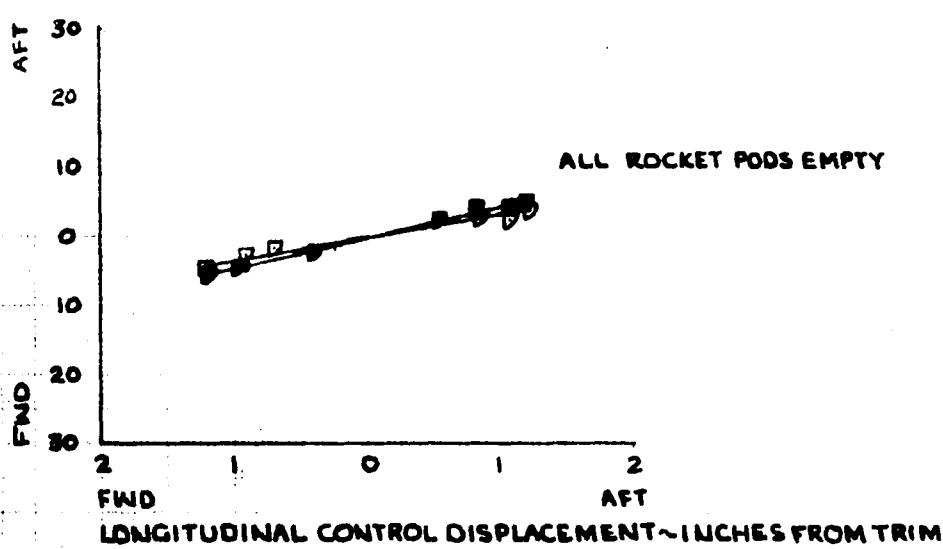


FIGURE NO. 257
LATERAL CONTROL SENSITIVITY
AH-1G USA #610847
CLEAN CONFIGURATION

SYMBOL	Avg. Altitude H ₀ ~ FT.	Avg. G.W. ~ LB.	Avg. Long. C.G. ~ IN.	RPM	FLIGHT COND.	THRUST COEFF. ~ CT
△	4460	7420	198.0(MID)	323.0	HOVER	0.004832
◆	4850	8400	198.3(MID)	320.5		0.004841
○	8330	7420	198.6(MID)	320.0		0.004768
▲	10320	7660	198.8(MID)	324.0		0.005282
□	550	7400	198.4 (MID)	324.0		0.003737

NOTES: 1. OPEN SYMBOLS DENOTE SCAS ON
2. SOLID SYMBOLS DENOTE SCAS OFF
3. SKID HEIGHT RANGE = 5FT. → 15FT.

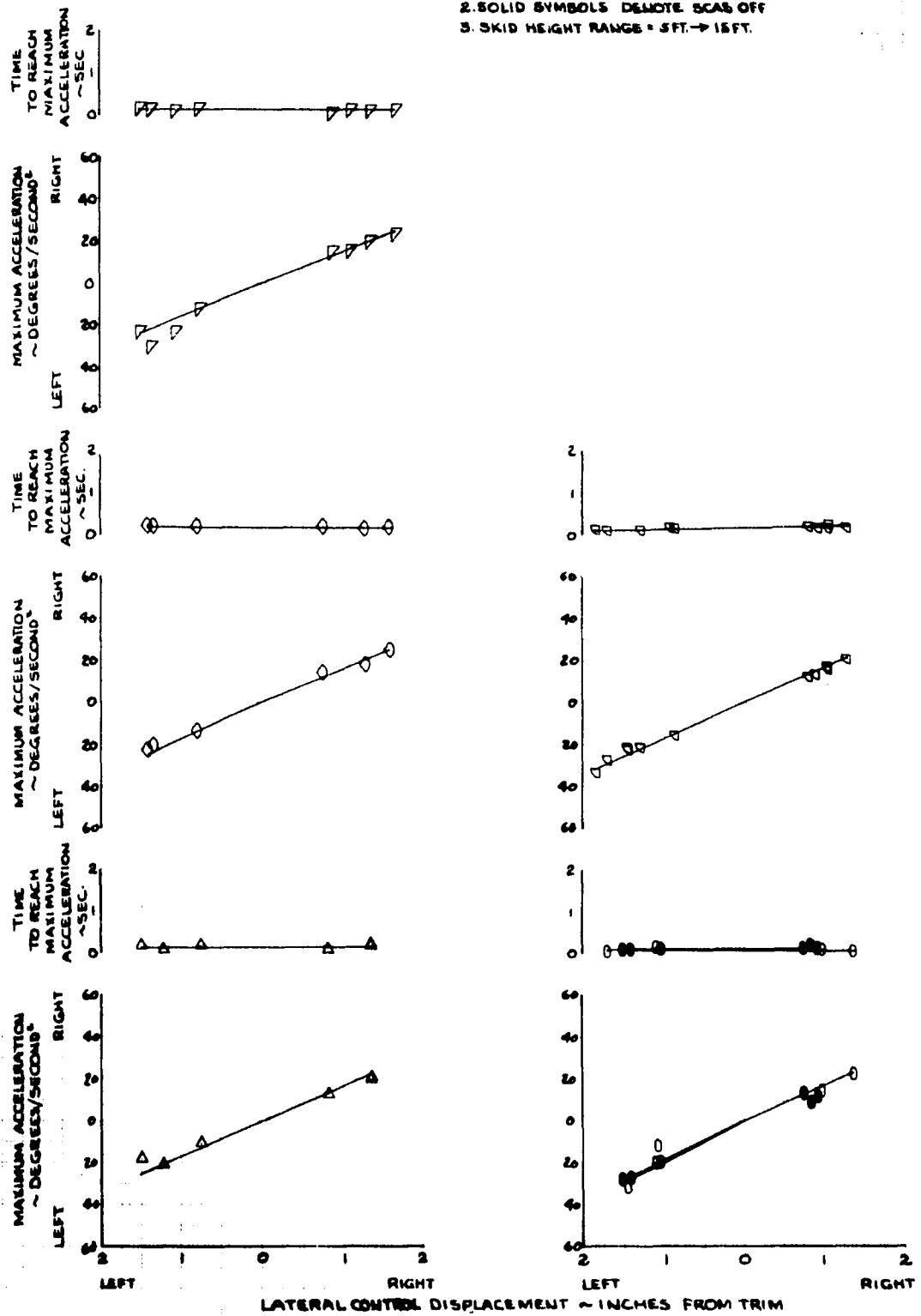


FIGURE NO 258
LATERAL CONTROL SENSITIVITY
 AH-1G USA # 715695
 HVY. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

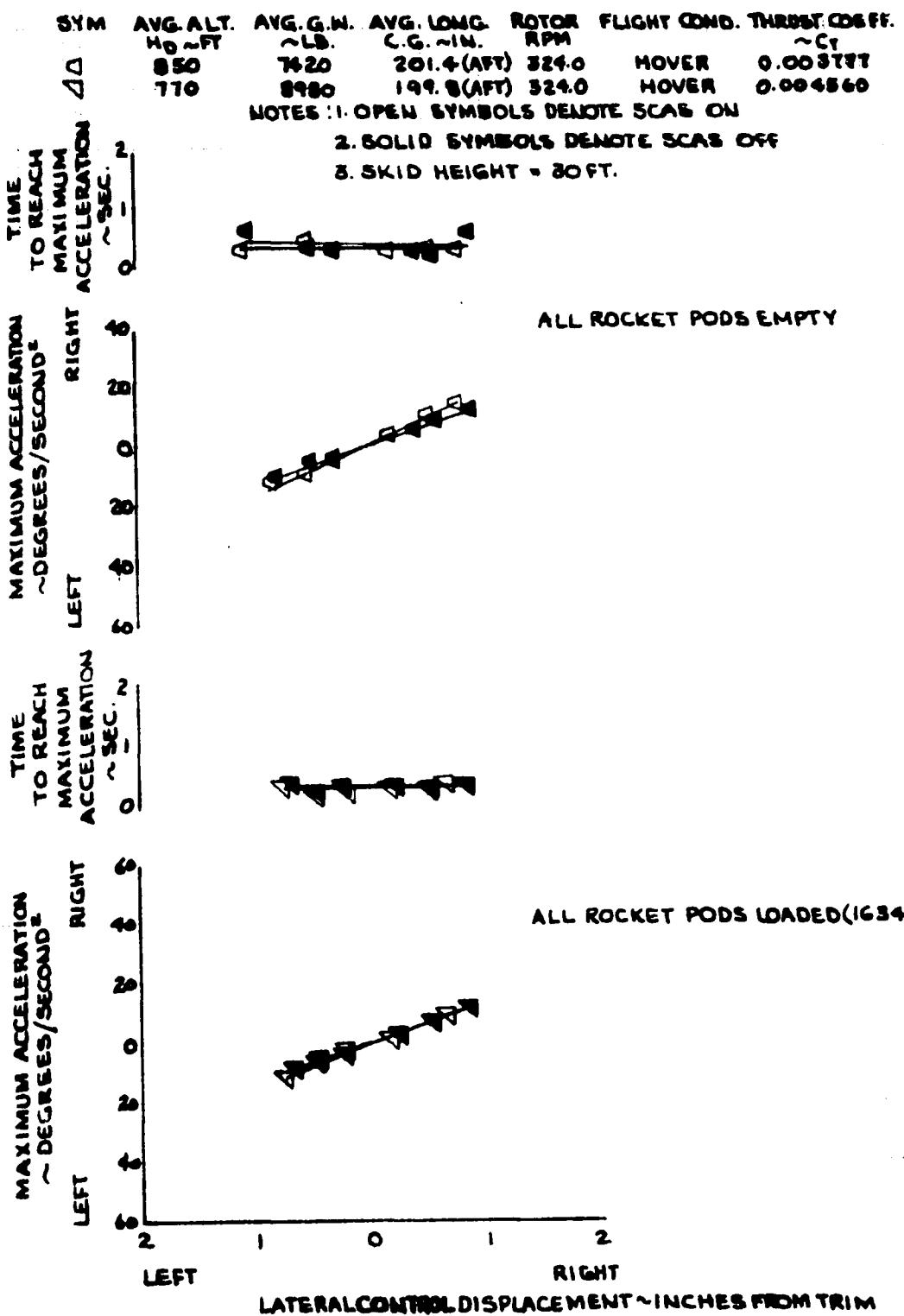


FIGURE No 259
LATERAL CONTROL RESPONSE
AH-1G USAF/NM8247
CLEAN CONFIGURATION

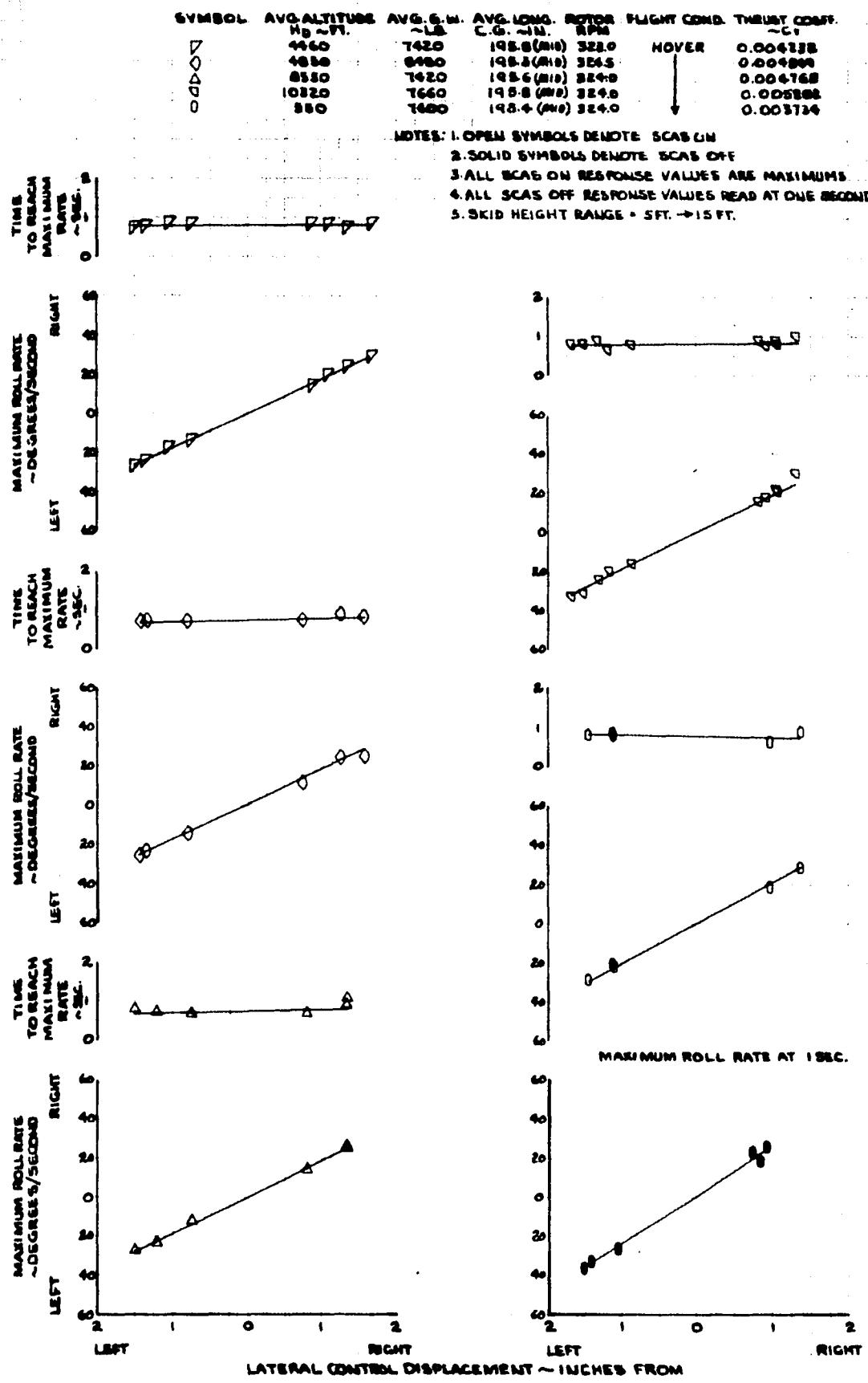


FIGURE No. 260
LATERAL CONTROL SENSITIVITY

AH-1G USA 161689T
 HVY. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYMBOL	Avg Altitude H _s ~FT.	Avg G.W. ~LB.	Avg Long. Motor C.G.-IN.	Flight Cond.	Thrust Coeff. ~C _T
○	-160	6400	1957(MID)	3225	HOVER 0.00400
●	400	6400	1958(AFT)	3220	HOVER 0.00400
○	030	8780	2020(AFT)	3225	HOVER 0.00400

NOTES: 1. OPEN SYMBOLS DENOTE SCAS ON
 2. SOLID SYMBOLS DENOTE SCAS OFF
 3. SKID HEIGHT RANGE = 5 FT. → 15 FT.

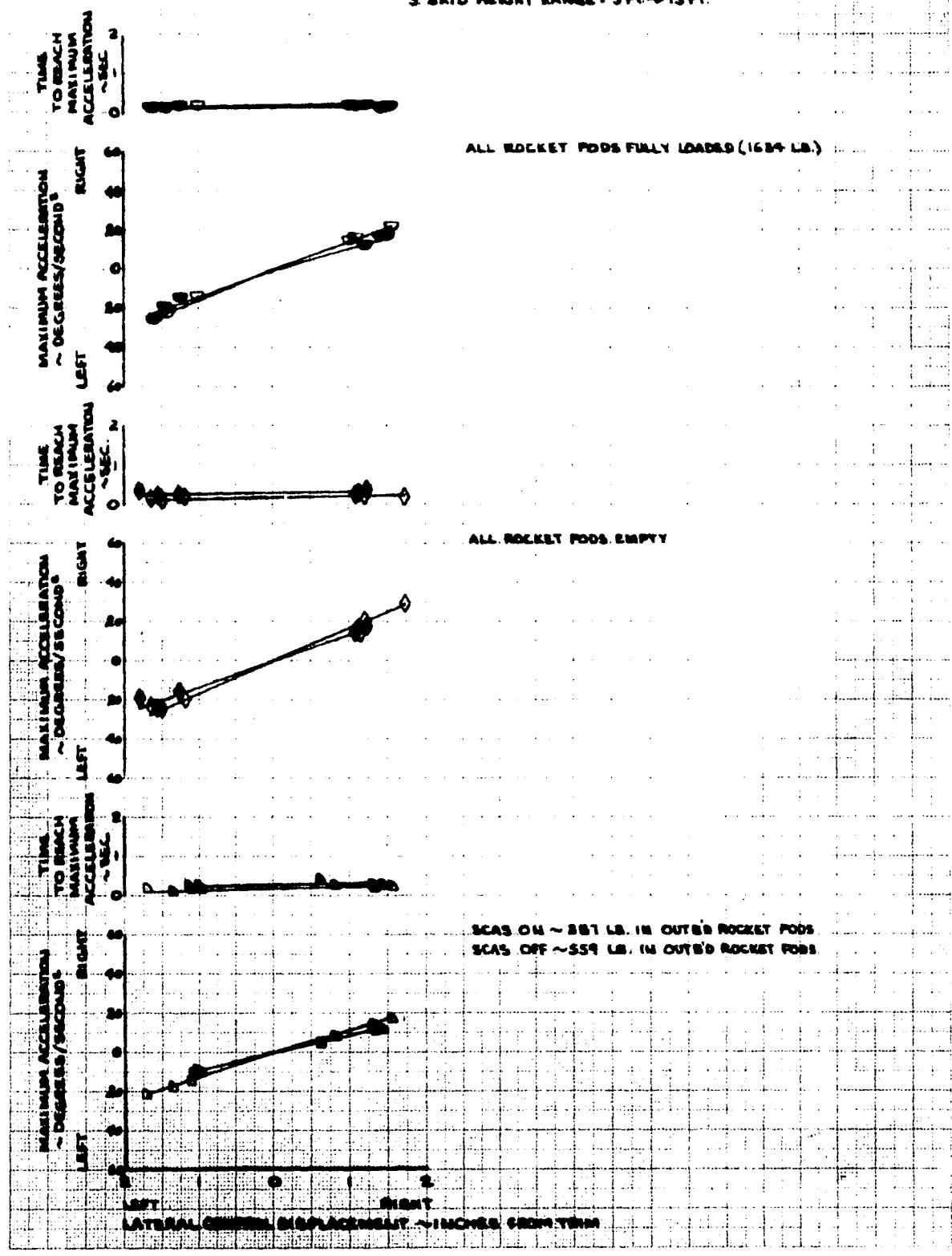


FIGURE NO 261
LATERAL CONTROL RESPONSE
 AM-1G USAF 88158847

HVY. HOG CONFIGURATION: WITH ROCKET POD FAIRINGS REMOVED

SYMBOL AVG ALTITUDE AVG. S.G. AVG. LONG. MOTOR FLIGHT COND. THRUST COEFF.
 $H_{\text{ft}} \sim \text{FT}$ ~LB. C.G. ~IN. RPM ~CT
 O - 160 6600 166.3(MIN) 8225 HOVER 0.004200
 D - 480 6600 198.0(Avg) 8280 HOVER 0.004887
 O - 630 6780 2000(Avg) 8228 HOVER 0.004487

NOTES: 1. OPEN SYMBOLS DENOTE SCAS ON.
 2. SOLID SYMBOLS DENOTE SCAS OFF.
 3. ALL SCAS ON RESPONSE VALUES ARE MAXIMUMS.
 4. ALL SCAS OFF RESPONSE VALUES READ AT ONE SECOND.
 5. SKID HEIGHT RANGE: 8FT → 16FT.

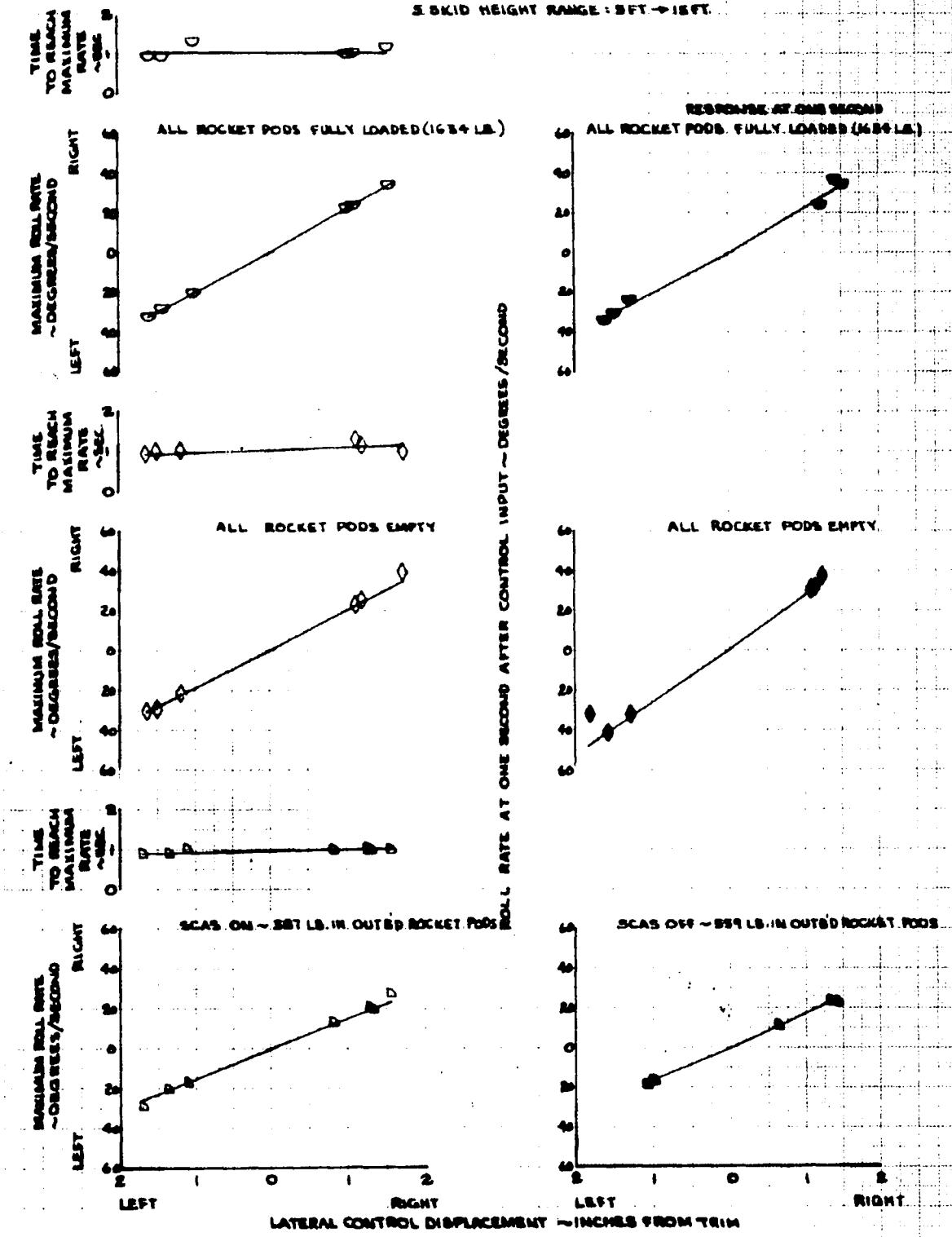


FIGURE NO. 262
ANGULAR ROLL DISPLACEMENT
AH-1S USAF/NBBST
HVV/HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYMBOLS: AVG. ALTITUDE AVG. G-D. AVG. LOAD. MOTOR FLIGHT COND. THRUST COEF.
 $H_0 \sim 5\text{ft}$ ~L.S. C.G. ~14° RPM ~C_T
 -100 8000 1000 (14) 3200 HOVER 0.004292
 000 8000 1000 (14) 3200 HOVER 0.004292
 100 8000 1000 (14) 3200 HOVER 0.004292

NOTES: 1. OPEN SYMBOLS DENOTE SCAS ON
 2. SOLID SYMBOLS DENOTE SCAS OFF
 3. SKID HEIGHT RANGE = 5FT. → 15FT.

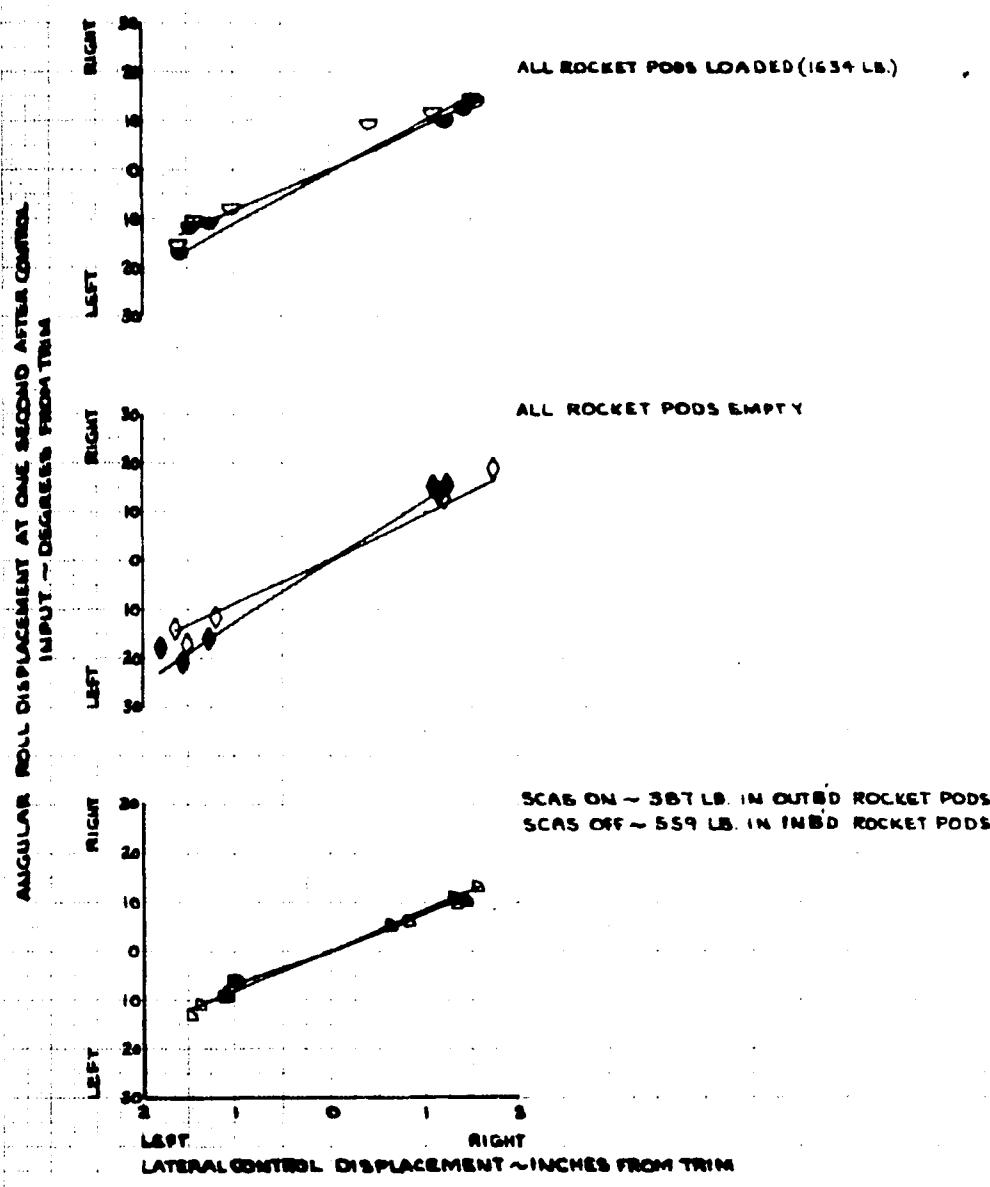


FIGURE NO. 263
LATERAL CONTROL RESPONSE
AH-1G USA #715645

HVV/HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM.	Avg. Alt. ft.	Avg. G.W. lb.	Avg. Long. C.G. in.	Rotor Thrust RPM	Flight Cond. ~CT
D	650	7420	201.4 (AFT)	324.0	HOVER 0.003773
D	770	6490	199.8 (AFT)	324.0	HOVER 0.004860

NOTE: SKID HEIGHT = SOFT.

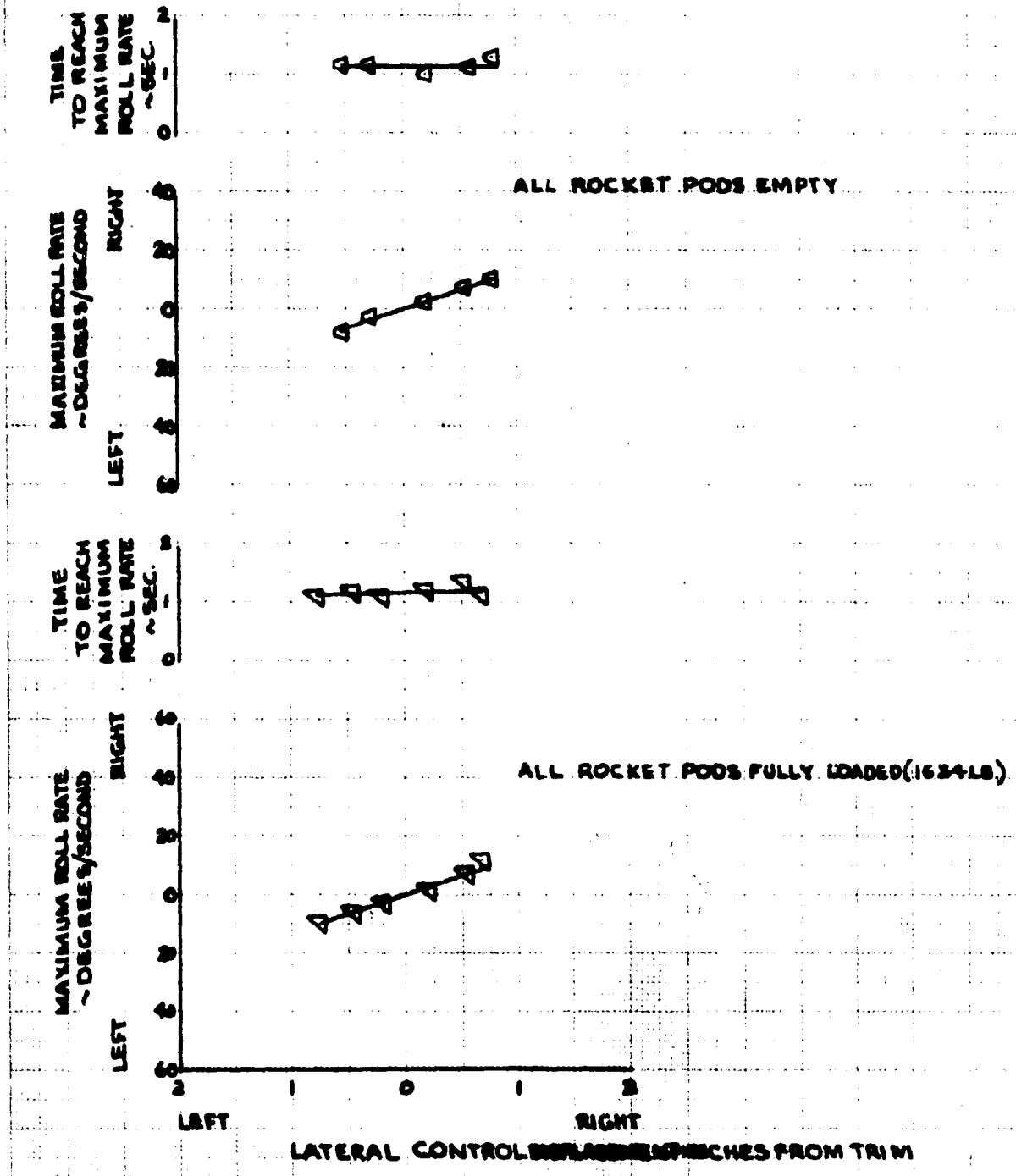


FIGURE NO. 264
LATERAL RESPONSE AT ONE SECOND

AH-1S USA XTISCRS
 HVY. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYN. ANG. ALT. ANG. G.H. ANG. LONG. ROTOR FLIGHT COND. THRUST DEPS.
 $H_0 \sim 1\text{ft}$ ~15° C.G. ~14° RPM ~CT
 C 860 T620 201.0(FT) 3300 HOVER 0000000
 V 770 0720 197.0(FT) 3310 HOVER 0000000
 NOTE: EXC'D. HEIGHT = 20FT.

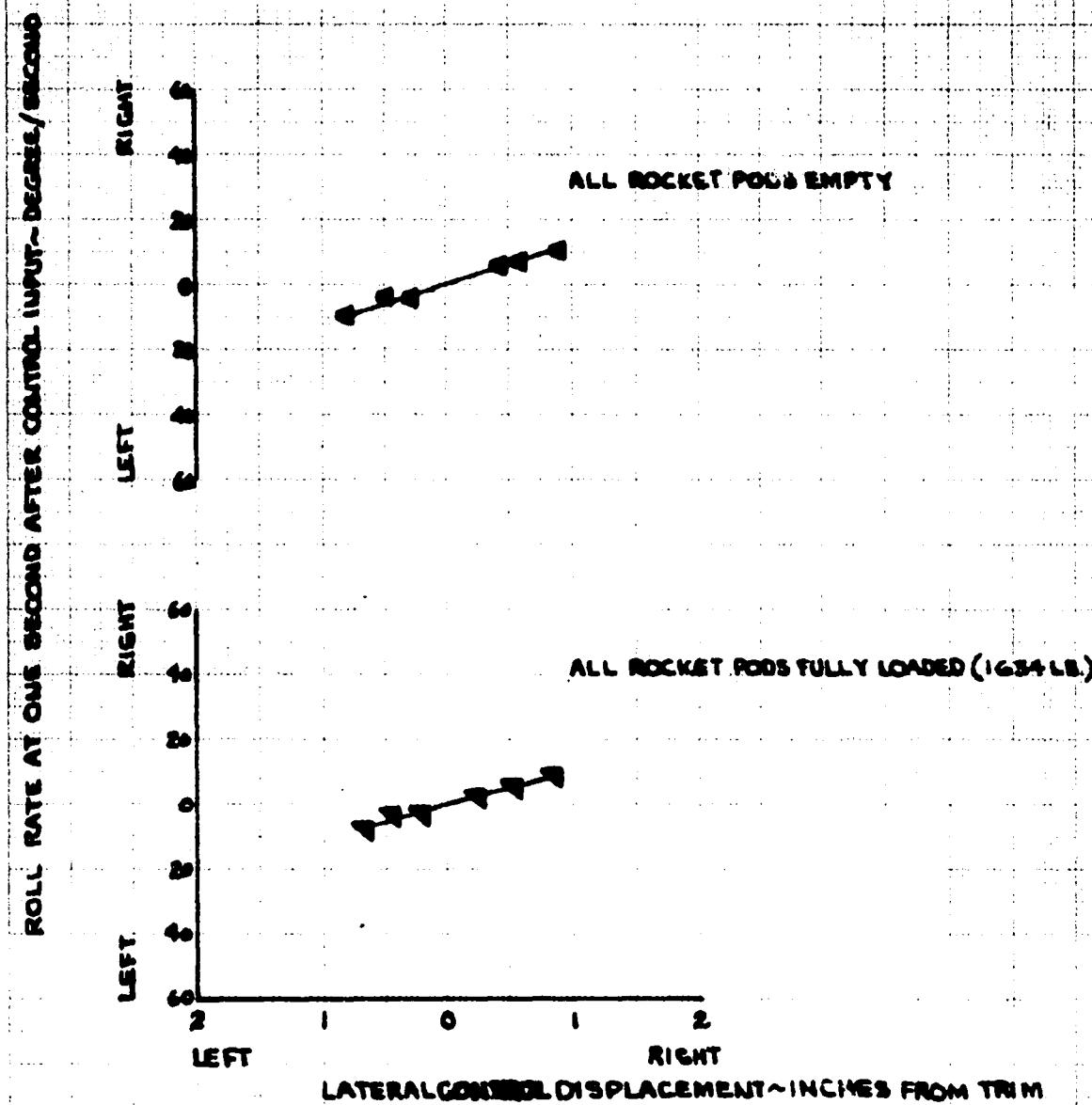


FIGURE NO 265
ANGULAR ROLL DISPLACEMENT
 AN-IG USA 4018803
 CLEAN CONFIGURATION

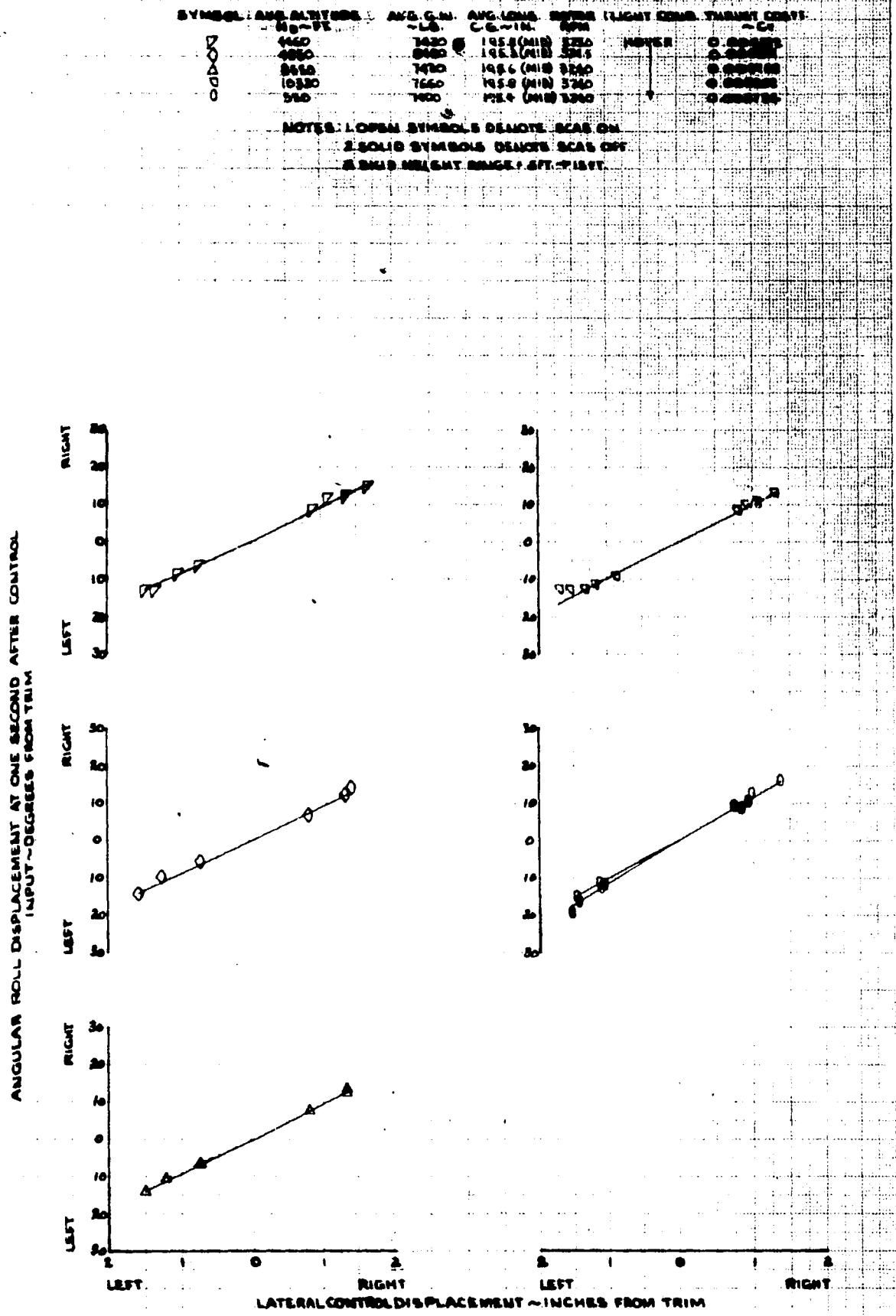


FIGURE NO. 266
ANGULAR ROLL DISPLACEMENT

HVY. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM. AVG. ALI. AVG.G.W. AVG.LONG. SECTOR. FLIGHT.CYC. THRUST COEFF.
M_s~FT. ~LBS. C.G.~IN RPM ~CP

20 **900** **T020** **2004 (AFT) 3000** **W002** **C-003701**
 T10 **0700** **1900 (AFT) 3000** **W003** **C-004500**

NOTES:

- 1. OPEN SYMBOLS DENOTE SCAS ON
- 2. SOLID SYMBOLS DENOTE SCAS OFF
- 3. SKID HEIGHT = 20 FT

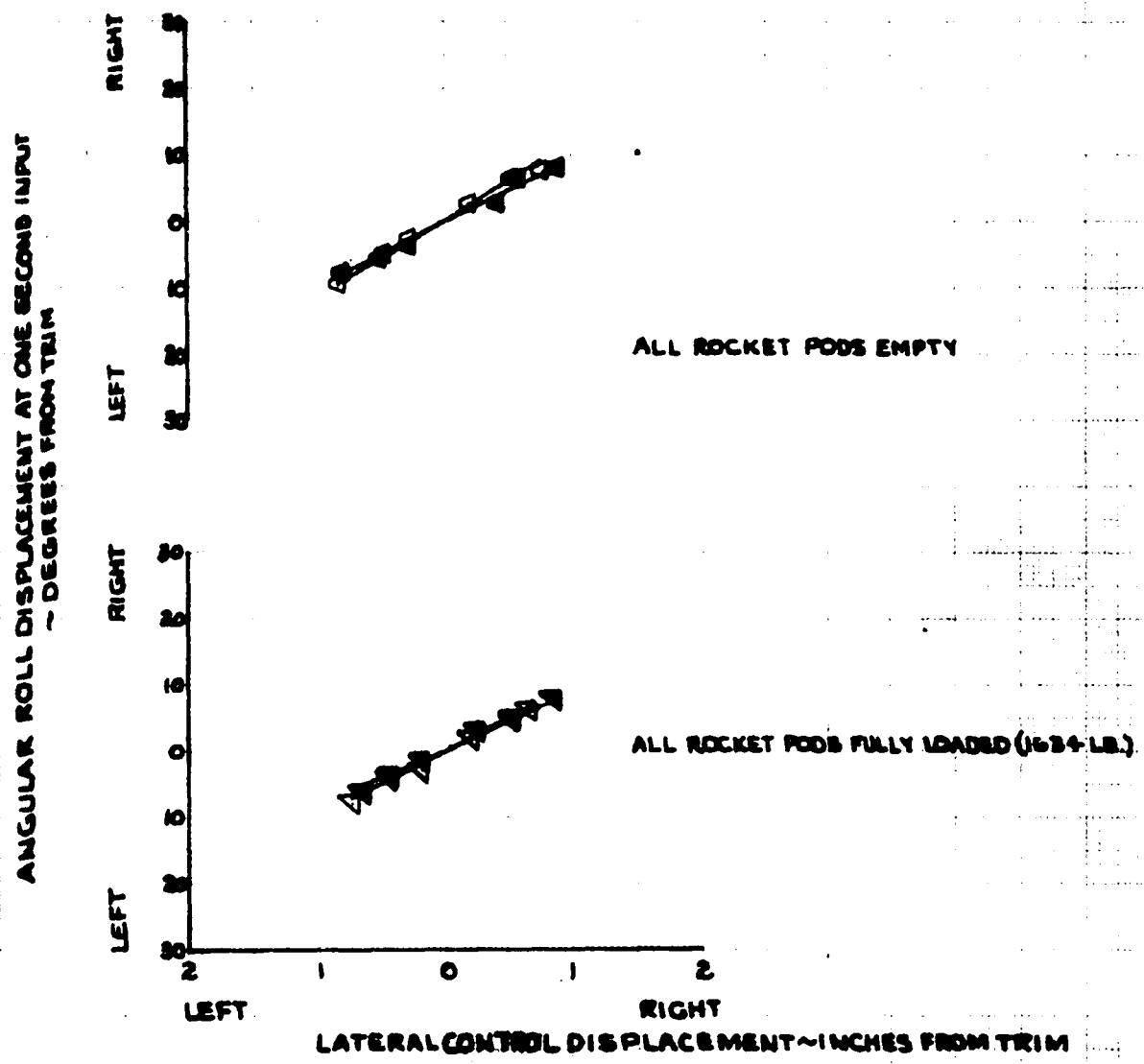


FIGURE NO. 267
 DIRECTIONAL CONTROL SENSITIVITY
 AM-1G USA X615847
 CLEAN CONFIGURATION
 SCAS ON

SYMBOL	Avg Altitude Hg ~ FT.	Avg S.W. ~ LB.	Avg Long. Rotor RPM	Flight Cond.	Thrust Coeff.
	C.G. ~ IN.				
○	4780	7280	195.6(MD) 3230	HOVER	0.00468
△	4580	7220	195.6(MD) 314.5		0.00426
○	4790	6680	195.4(MD) 324.5		0.00476
○	4860	6400	195.2(MD) 314.5		0.005116
○	5550	7370	195.5(MD) 324.0		0.004716
○	5550	7270	195.4(MD) 314.5		0.004486

NOTES: 1. SKID HEIGHT RANGE 3FT TO LEFT.
 2. DIRECTIONAL CONTROL AVAILABLE
 TO THE LEFT IS LESS THAN ONE INCH
 ABOVE A CT OF 0.004680

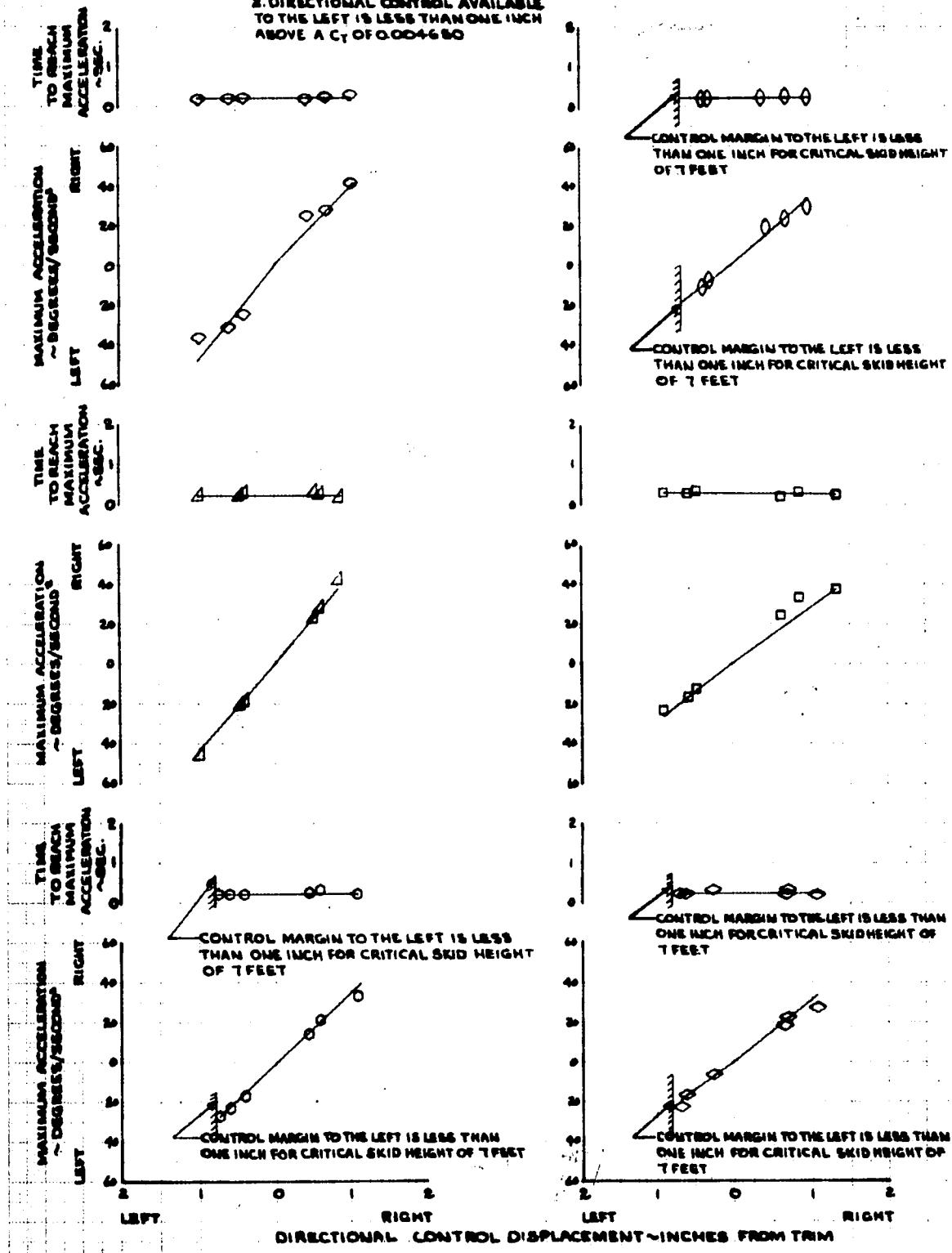


FIGURE NO. 268
DIRECTIONAL CONTROL SENSITIVITY
AH-1G USA 4/615847
CLEAN CONFIGURATION

SYMBOL	Avg. ALTITUDE H _D ~ FT.	Avg. G.W. ~ LB	Avg. LONG. MOTOR C.G. MIN.	FLIGHT COND. RPM	THRUST COEF.
○	10520	7560	195.7(MIN)	324.0	0.005134
○	10320	7490	195.6(MIN)	313.5	0.005023
○	560	7170	195.2(MIN)	324.0	0.005220
○	550	7160	195.1(MIN)	313.5	0.005187
○	570	6980	194.9(MIN)	303.5	0.004016

HOVER
↓

- NOTES:
 1. OPEN SYMBOLS DENOTE SCAS ON
 2. SOLID SYMBOLS DENOTE SCAS OFF
 3. SKID HEIGHT RANGE = 5FT - 15FT
 4. DIRECTIONAL CONTROL AVAILABLE TO THE
 LEFT IS LESS THAN ONE INCH ABOVE A
 C.Y OF 0.004650

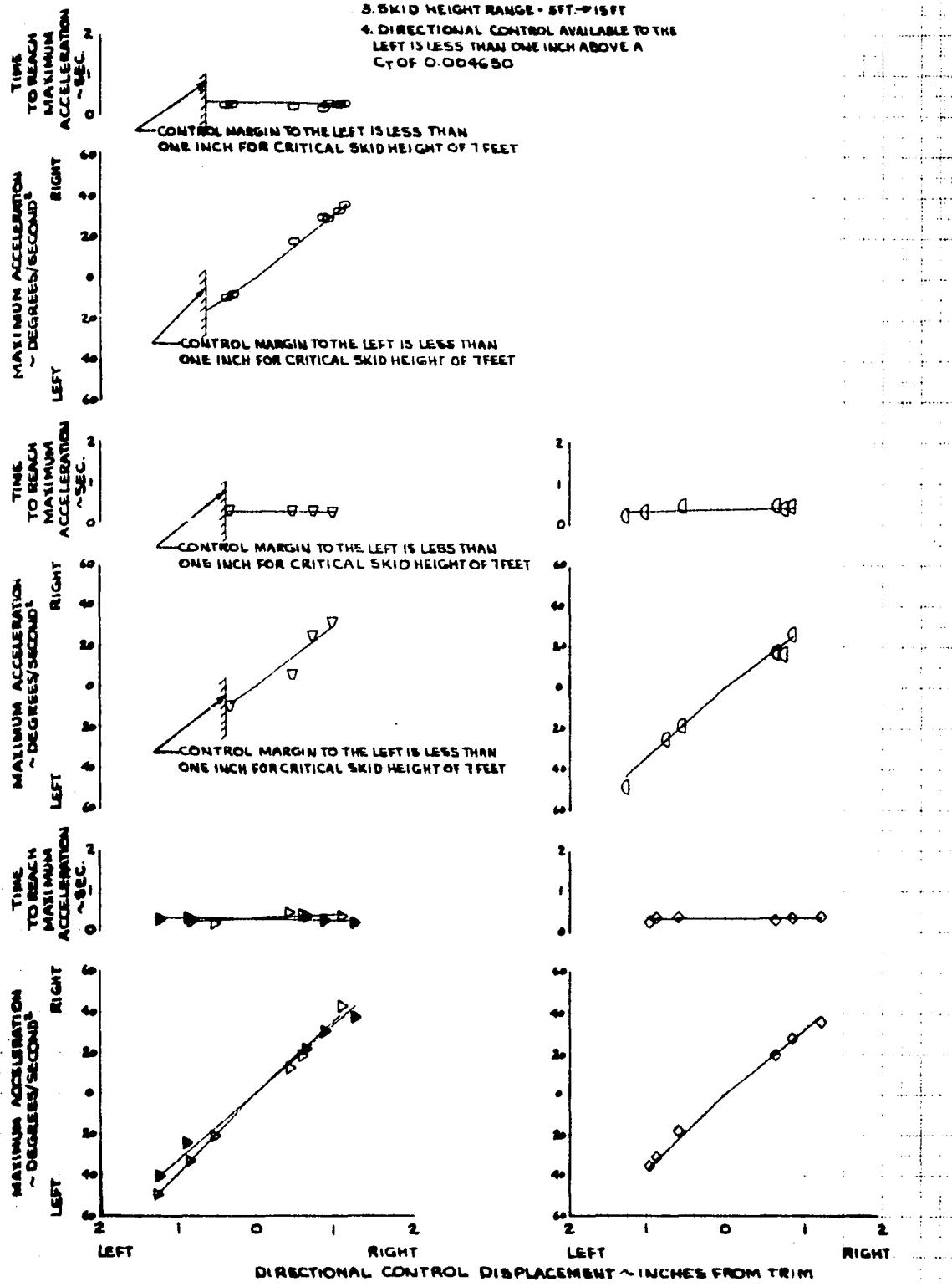


FIGURE NO. 269
DIRECTIONAL CONTROL SENSITIVITY
 AH-1G USA #616867
 HVY. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYMBOL	Avg Altitude H _b - FT.	Avg G.W. ~LB.	Avg Long. C.G. ~IN.	Rotor RPM	Flight Cond.	Thrust Coeff. ~C _T
△	-480	8460	195.9 (AF)	323.0	HOVER	0.004160
○	-490	8400	195.8 (H)	313.5		0.004161
□	SEA LEVEL	8770	200.4 (AF)	313.5		0.004081
○	060	8600	199.9 (AF)	323.0		0.004207

NOTES: 1. OPEN SYMBOLS DENOTE SCAS ON
 2. SOLID SYMBOLS DENOTE SCAS OFF
 3. SKID HEIGHT RANGE = 8FT. → 15FT

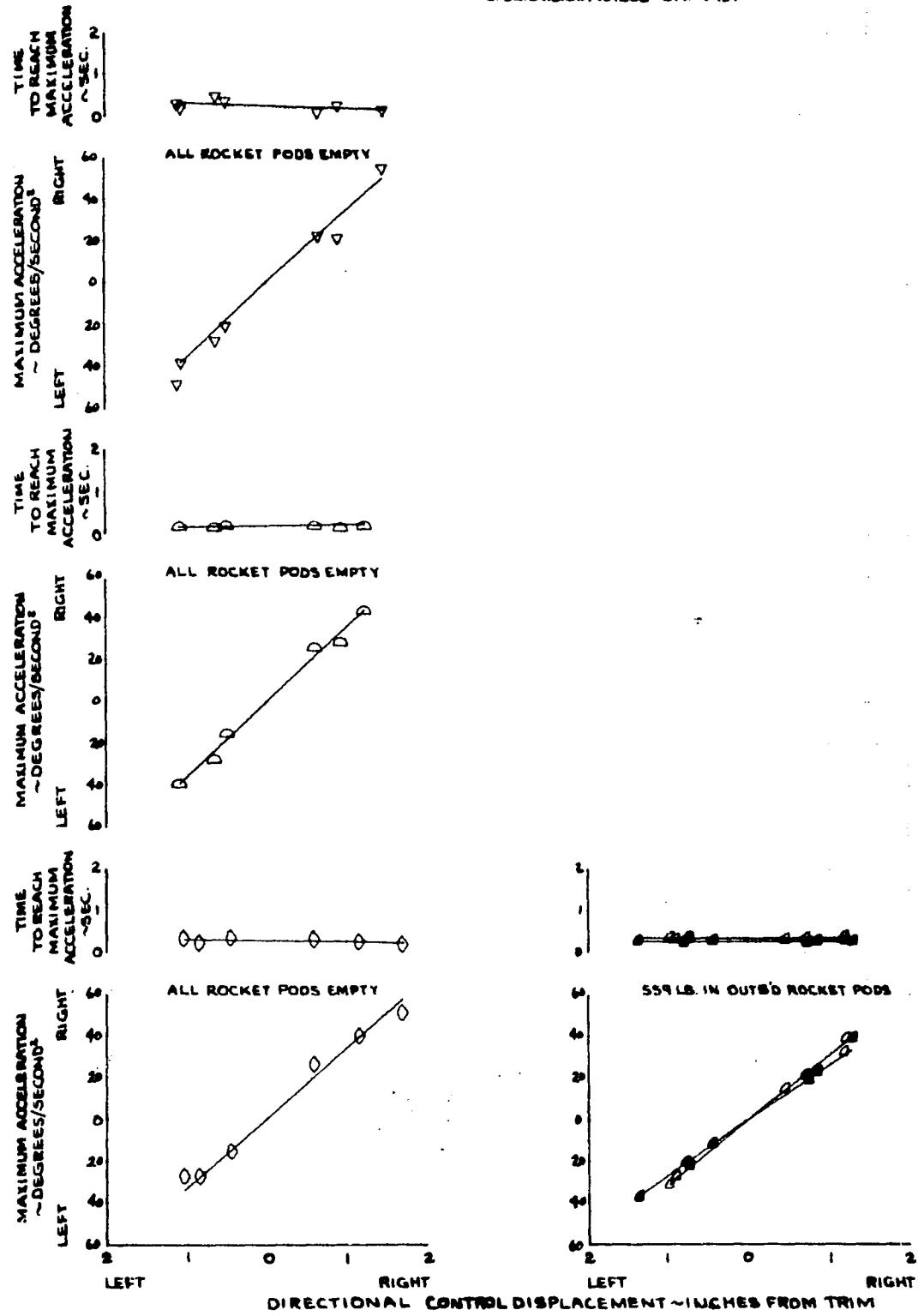


FIGURE NO. 270
DIRECTIONAL CONTROL SENSITIVITY

AH-1G USA #715695

HVV. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM.	Avg. Alt.	Avg. G.W.	Avg. Long.	Rotor Flight Cond.	Thrust Coeff.
O	Hg-ft.	~lb.	C.G. ~in.	RPM	~ct
O	980	7260	201.4 (AFT)	324.0	HOVER 0.003710
D	450	8970	200.5 (AFT)	324.0	HOVER 0.004818

NOTES: 1. OPEN SYMBOLS DENOTE SCAS ON
 2. SOLID SYMBOLS DENOTE SCAS OFF
 3. SKID HEIGHT = 30 FEET

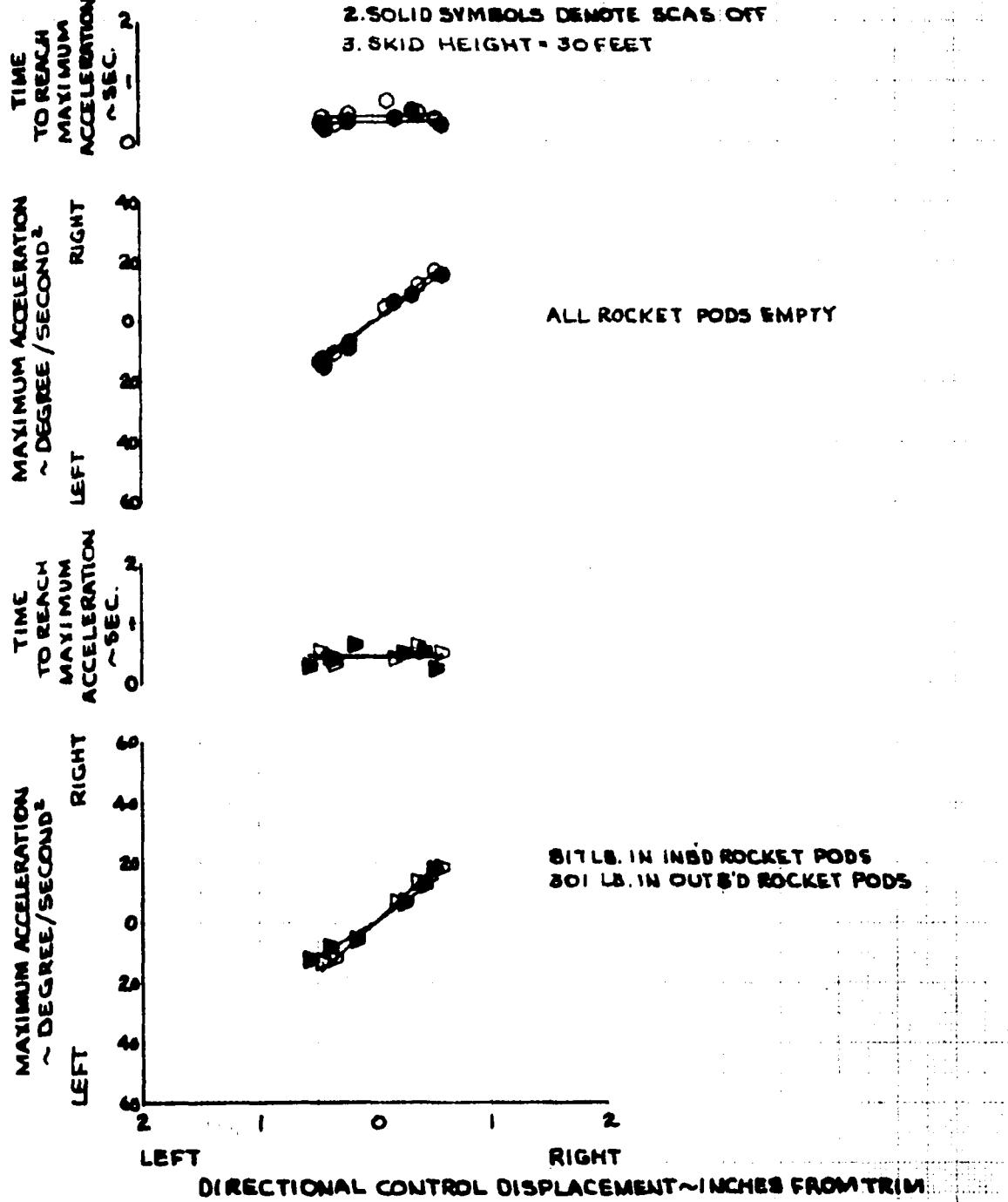


FIGURE NO. 271
DIRECTIONAL CONTROL RESPONSE
AH-1G USA #616247
CLEAN CONFIGURATION

SYMBOL	Avg. ALTITUDE HO ~ FEET	Avg. G.M. ~ LB.	Avg. LONG. MOTOR C.G. MIN. RPM	FLIGHT COND.	THRUST COEFF.
○	4580	7280	195.6(10)3230	CT	0.004168
○	4580	7220	193.6(10)3165		0.004368
○	4710	8630	195.4(10)3245		0.004926
○	4850	8400	195.2(10)3145		0.005116
○	8550	1830	195.5(10)3260	HOVER	0.006718
○	8550	7270	195.4(10)3145		0.004488

NOTES: 1. OPEN SYMBOLS DENOTE SCAB ON
2. SOLID SYMBOLS DENOTE SCAB OFF
3. DIRECTIONAL CONTROL AVAILABLE TO THE LEFT IS LESS THAN ONE INCH ABOVE ACT OF 0.004650

CONTROL MARGIN TO THE LEFT IS LESS THAN ONE INCH FOR CRITICAL SKID HEIGHT OF 7 FEET

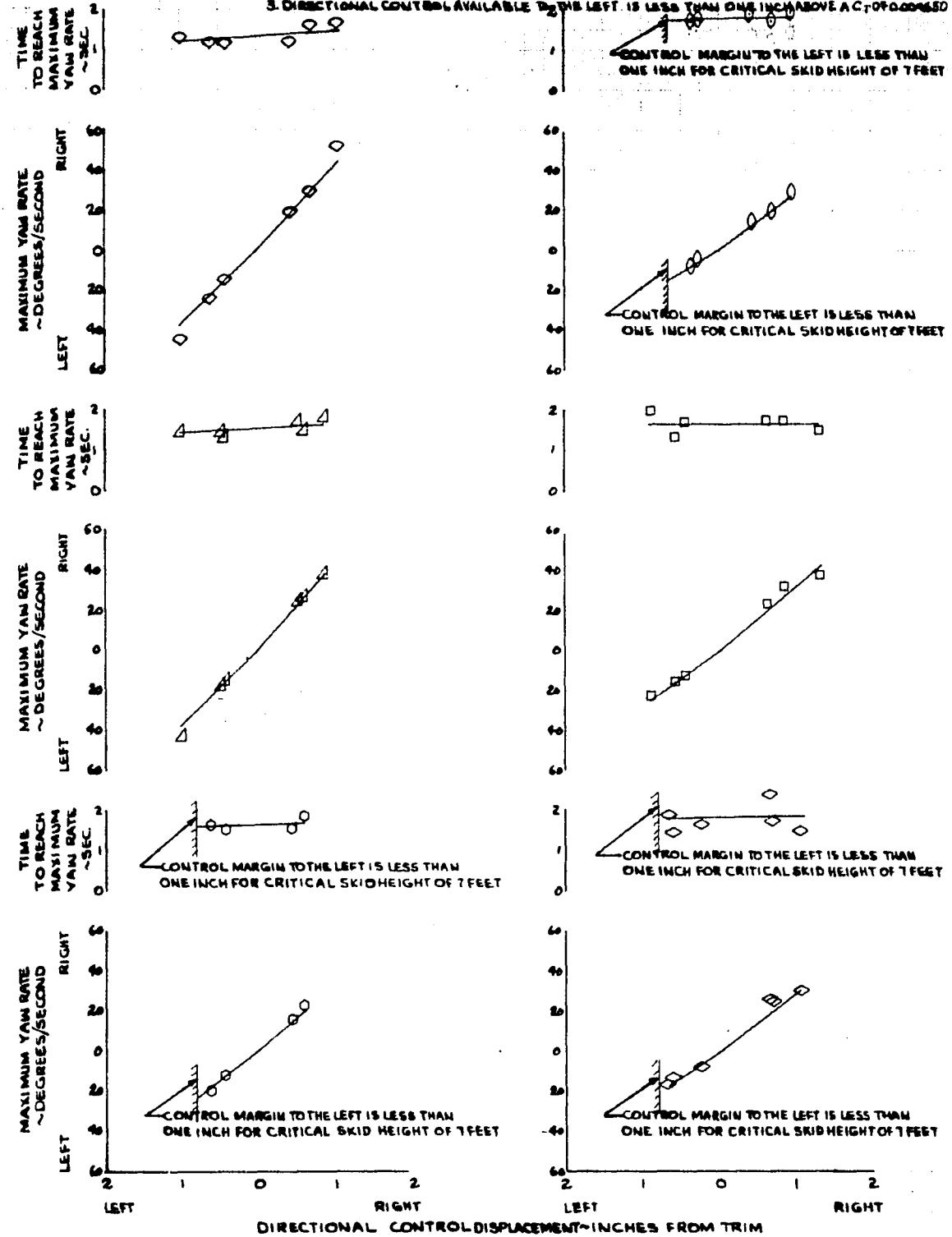


FIGURE NO 272
DIRECTIONAL CONTROL RESPONSE
 AH-1G USAF 84-8007
 CLEAN CONFIGURATION

SYMBOL	ANG. ALTITUDE	Avg. G-M.	Avg. L-M.	ROTORS	FLIGHT CRDS.	THRUST CRDS.
O	Hs ~67°	-1.6	0.6	8100	~C	
O	10320	7.660	1.9	TURBO	2.240	HOVER
O	10320	7.640	1.8	GEAR DOWN	2.11.8	0.000000
O	560	11.10	1.8	GEAR UP	3.24.0	0.000000
O	550	11.60	1.8	GEAR DOWN	2.11.5	0.000000
O	6180	14.700	2.1	GEAR UP	2.01.5	0.000000

NOTES: 1. OPEN SYMBOLS DENOTE SCAS ON
 2. SOLID SYMBOLS DENOTE SCAS OFF
 3. ALL SCAS OFF MEASURED VALUES READ AT ONE SECOND

4. ALL SCAS ON MEASURED VALUES READ AT ONE SECOND
 5. CRASH HEIGHT BARRIER = 8FT -> 15FT
 6. DIRECTIONAL CONTROL ANALOGUE TO THE LEFT IS ABOVE THAN ONE INCH ABOVE A/C OF 0.000000

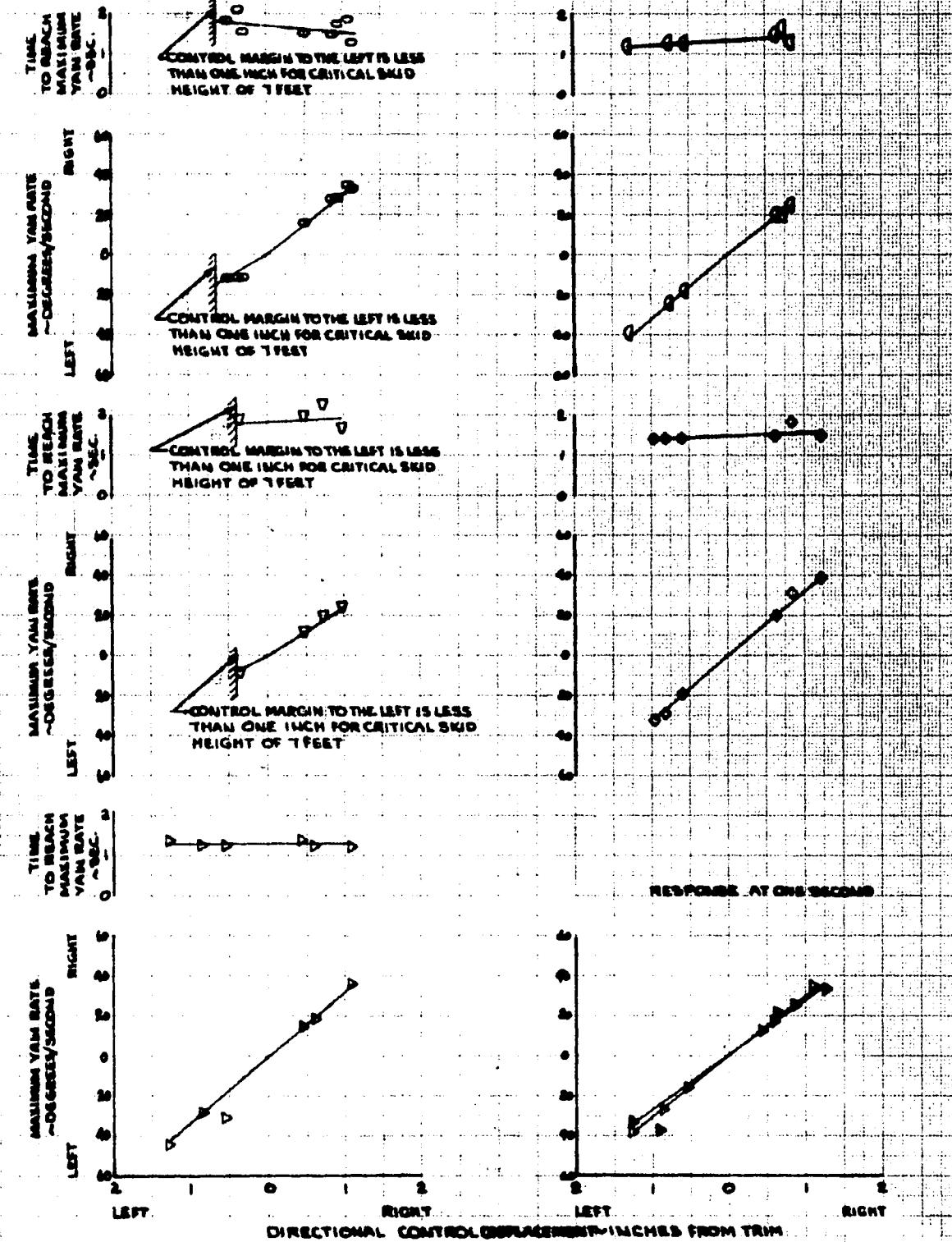


FIGURE NO 273
DIRECTIONAL CONTROL RESPONSE
AH-1G USA 10/86
HVY HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYMBOL	Avg. ALTITUDE Hg ~ ft.	Avg. G.W. ~ LB.	CD. ~ IN.	RPM	FLIGHT COND.	THRUST COEFF
○	7900	6460	196.9(AM)	323.0	HOVER	0.00028
○	7400	6400	196.8(MM)	313.5		0.00031
○	SEA LEVEL 060	6770	200.4(MT)	313.5		0.00031
○	060	6600	199.9(MT)	323.0		0.00032

NOTES:
 1. OPEN SYMBOLS DENOTE SCAS ON
 2. SOLID SYMBOLS DENOTE SCAS OFF
 3. ALL SCAS ON RESPONSE VALUES ARE MAXIMUMS
 4. ALL SCAS OFF RESPONSE VALUES READ AT ONE SECOND
 5. SKID HEIGHT RANGE = 8 FT. → 15 FT.

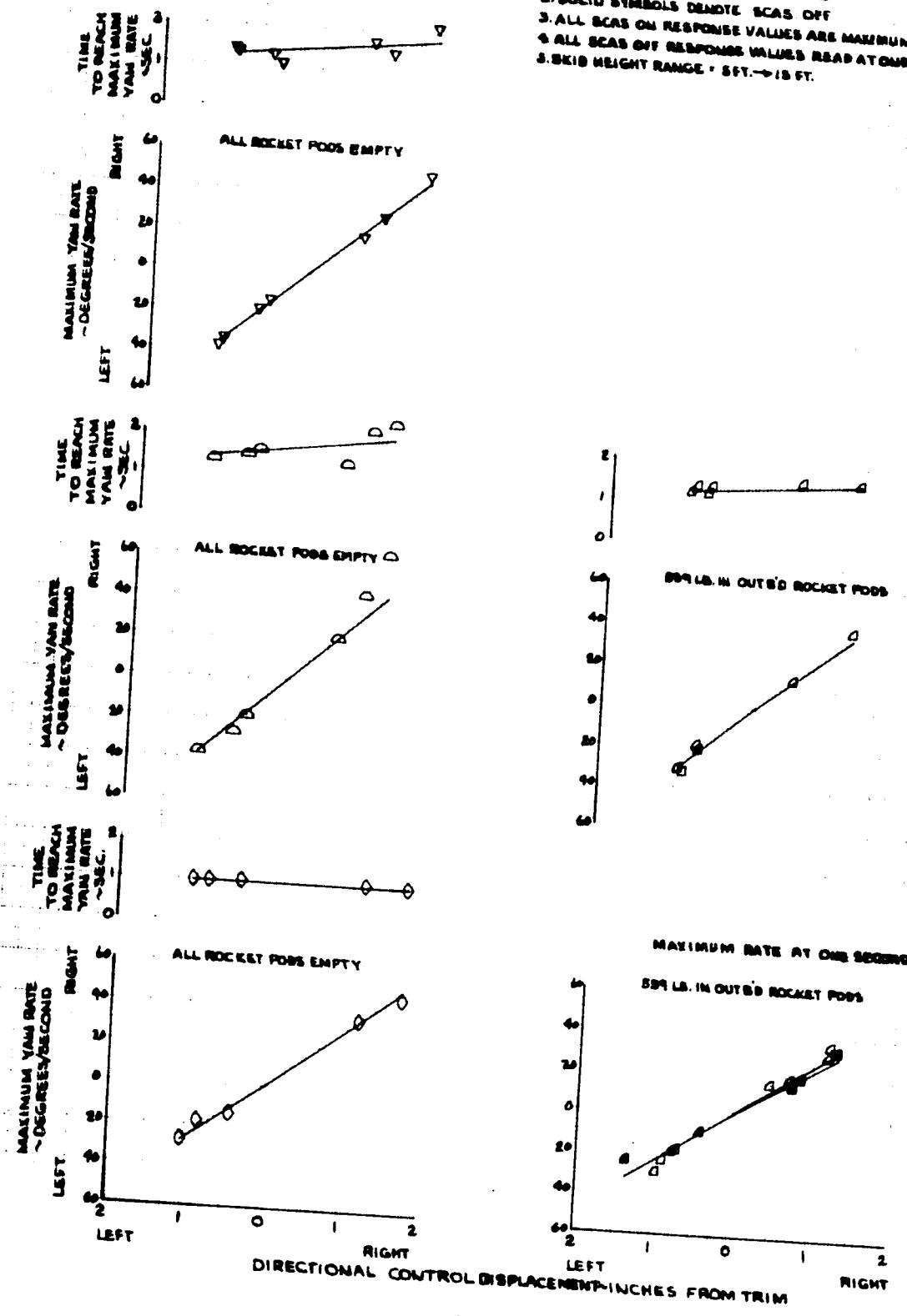


FIGURE NO. 274
DIRECTIONAL CONTROL RESPONSE

AH-1G USA 47156AS

HVT. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED
 SCAS ON

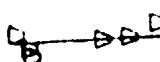
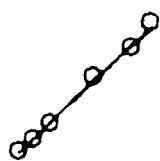
SYM	Avg. Alt. Hr-ft.	Avg. G-in. ~10	Avg. Long. CG. ~1M	RPM	ROTOR FLIGHT COND.	THRUST COEFF.
980	7260	201.4(4ft)	324.0	HOVER	0.00370	
480	8970	200.5(AFT)	324.0	HOVER	0.004513	

0

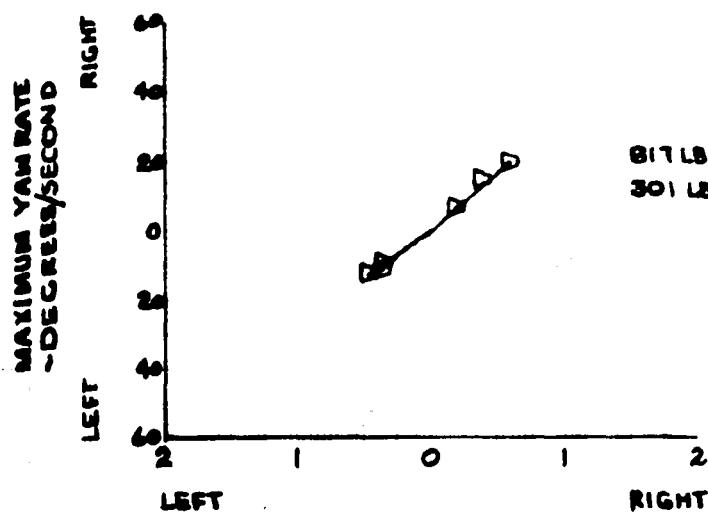
NOTE: SKID HEIGHT = 30 FEET



ALL SOCKET PODS EMPTY



817 LB. IN INBOARD ROCKET PODS
 301 LB. IN OUTBOARD ROCKET PODS



DIRECTIONAL CONTROL DISPLACEMENT-INCHES FROM TRIM

FIGURE NO. 275
DIRECTIONAL RESPONSE AT ONE SECOND
 AH-1G USA #6715695

HVV. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM.	Avg. Alt. Hd~FT.	Avg. G.I.L. ~LB.	Avg. Long. C.G. ~IN.	ROTOR FLIGHT COND. RPM	THRUST COEFF. ~CT
O	980	7260	201.4(AFT)	324.0	HOVER 0.003710
D	450	8970	200.5(AFT)	324.0	HOVER 0.004513

NOTE: SKID HEIGHT = 30 FEET

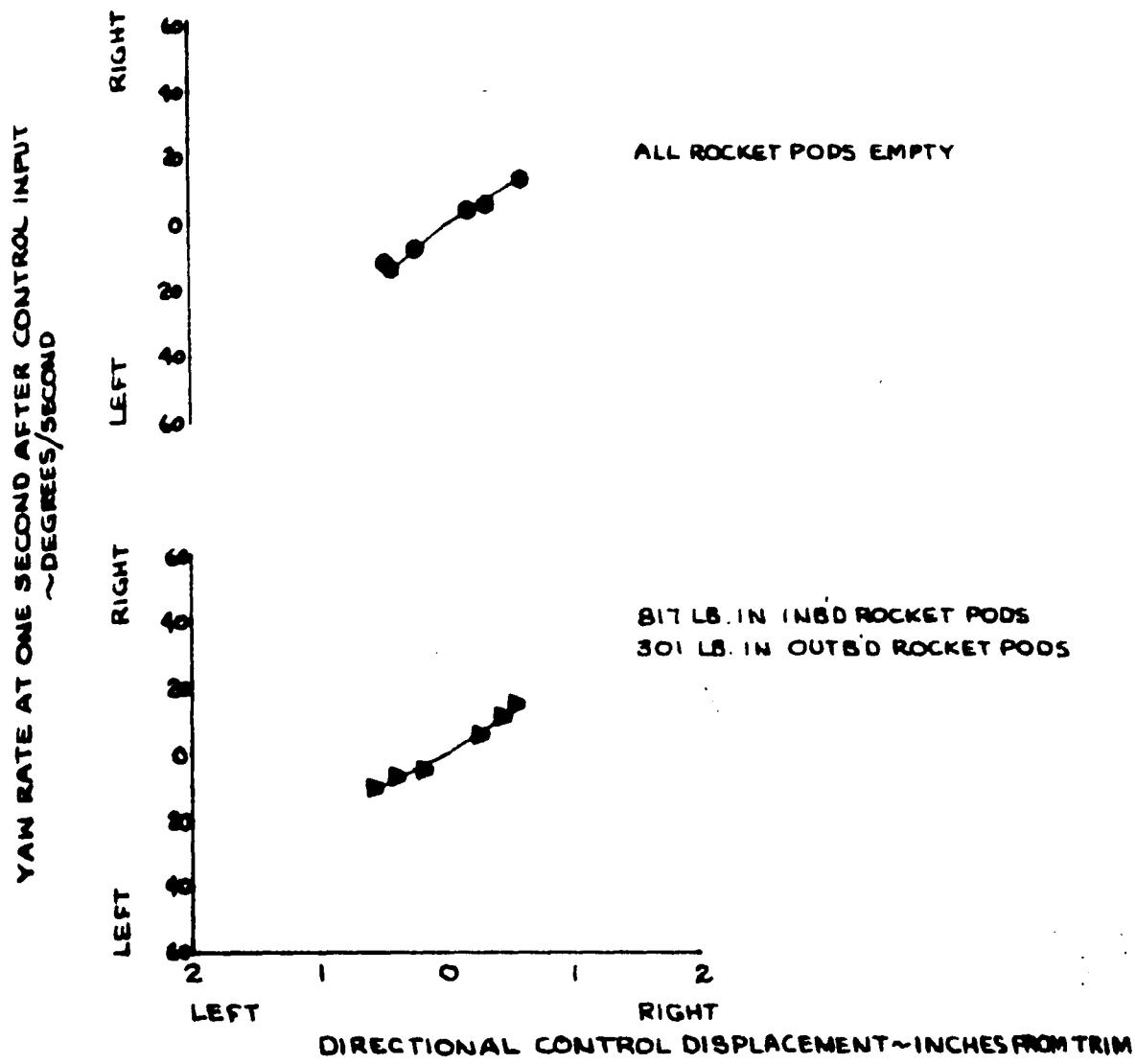


FIGURE NO. 27G
ANGULAR YAW DISPLACEMENT
 AH-1G USA #61897
 CLEAN CONFIGURATION

SYMBOL	Avg. Altitude HO - FT	Avg. G.W. ~LB.	Avg. Long. C.G. ~IN.	ROTOR RPM	FLIGHT COND.	THRUST COEF. ~C _T
○	10220	7560	1957(MID)	322.0	HOVER	0.001317
●	10220	7490	1956(MID)	311.5		0.001317
○	560	7170	1952(MID)	322.0		0.001317
○	550	7160	1951(MID)	313.5		0.001317
○	570	6980	1949(MID)	303.5		0.001316

NOTES: 1. OPEN SYMBOLS DENOTE SCAS ON
 2. SOLID SYMBOLS DENOTE SCAS OFF
 3. SKID HEIGHT RANGE = 5FT. → 15FT.
 4. DIRECTIONAL CONTROL AVAILABLE TO
 THE LEFT IS LESS THAN ONE INCH
 ABOVE A C_T OF 0.004650

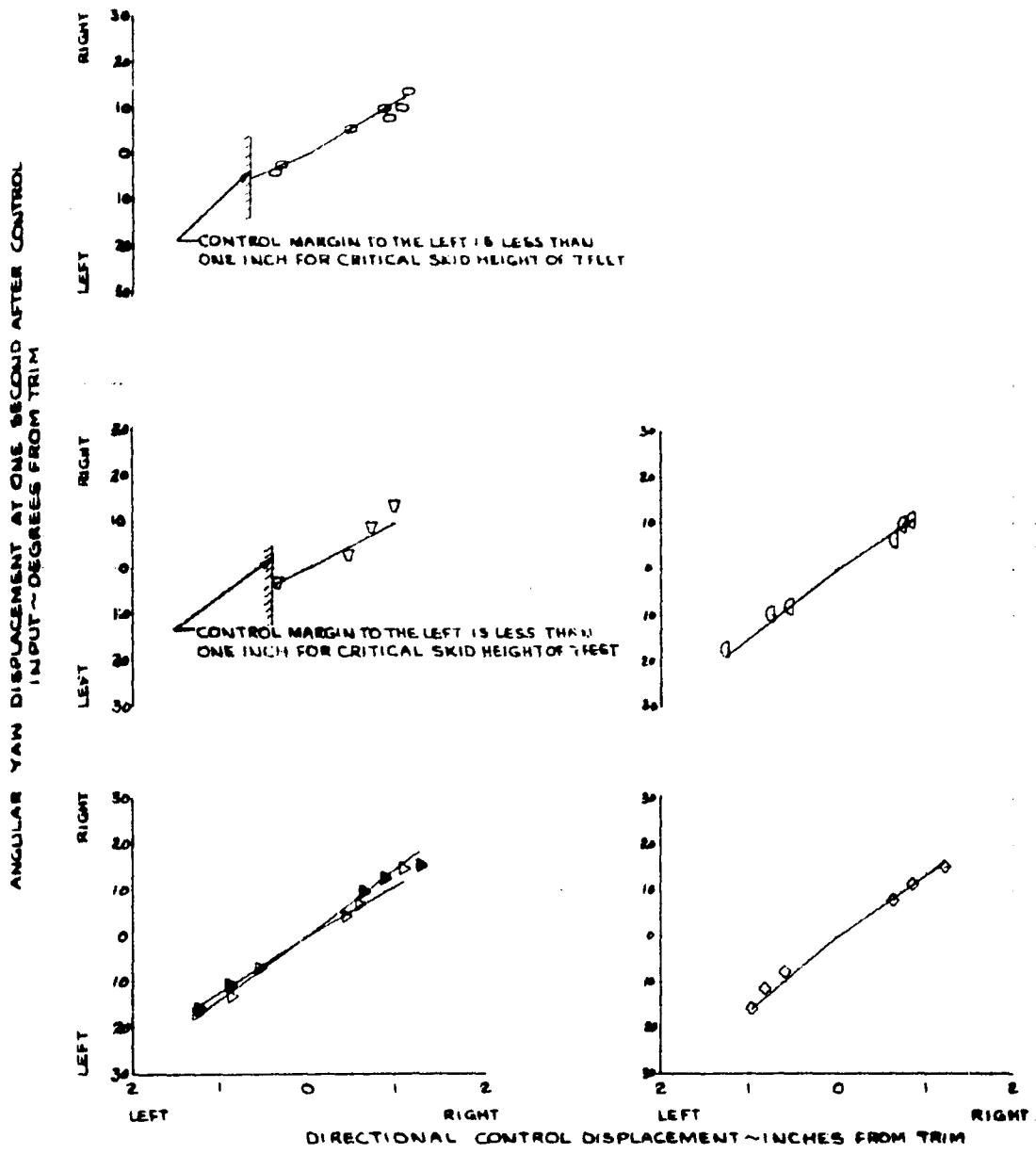


FIGURE NO. 277
ANGULAR YAW DISPLACEMENT
 AH-1G USA %018847
 CLEAN CONFIGURATION
 SCAS ON

SYMBOL	Avg. ALTITUDE H ₀ ~ FT.	Avg. G.N. ~ LB.	Avg. LONG. C.G. ~ IN.	ROTIN FLIGHT RPM	COMB. THRUST COEFF. ~ CT
0	7200	195.6 (MIN)	325.0	NOVER	0.004160
00	7200	196.6 (MIN)	316.5		0.004160
000	6630	195.4 (MIN)	324.5		0.004160
0000	5900	195.2 (MIN)	314.5		0.004160
00000	7830	195.5 (MIN)	330.0		0.004160
000000	7270	191.6 (MIN)	314.5		0.004160

NOTES: 1. SKID HEIGHT RANGE = 5 FT. -> 15 FT.
 2. DIRECTIONAL CONTROL AVAILABLE TO THE LEFT IS LESS THAN ONE INCH ABOVE A CT OF 0.004160

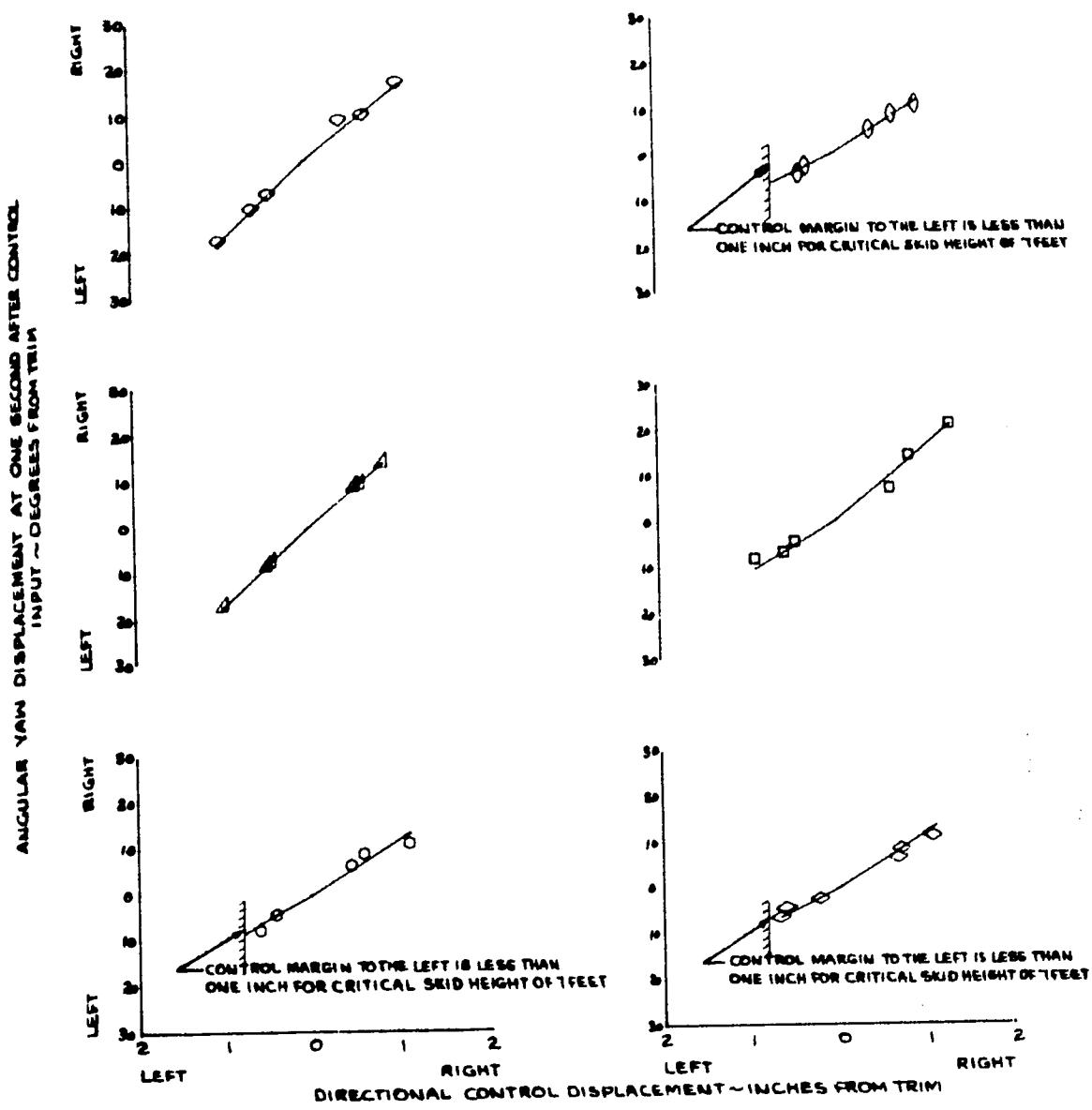


FIGURE NO. 278
ANGULAR YAW DISPLACEMENT
 AH-1G USA 4618847
 HVY HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYMBOL	Avg. Altitude H ₀ - FT.	Avg. G.W. LBS.	Avg. Long. C.G. - IN.	Rotor RPM	Flight Cond.	Thrust Coeff. ~CT
△	6400	195.9 (MAX)	228.0	348.5	HOVER	0.000168
○	8400	195.8 (MIN)	218.5	348.5		0.000081
◆	8710	206.4 (APT)	218.5	348.5		0.000081
◆	8600	199.9 (APT)	228.0	348.5		0.000081

NOTES : 1. OPEN SYMBOLS DENOTE SCAS ON
 2. SOLID SYMBOLS DENOTE SCAS OFF
 3. SKID HEIGHT RANGE = 5 FT. ~ 15 FT.

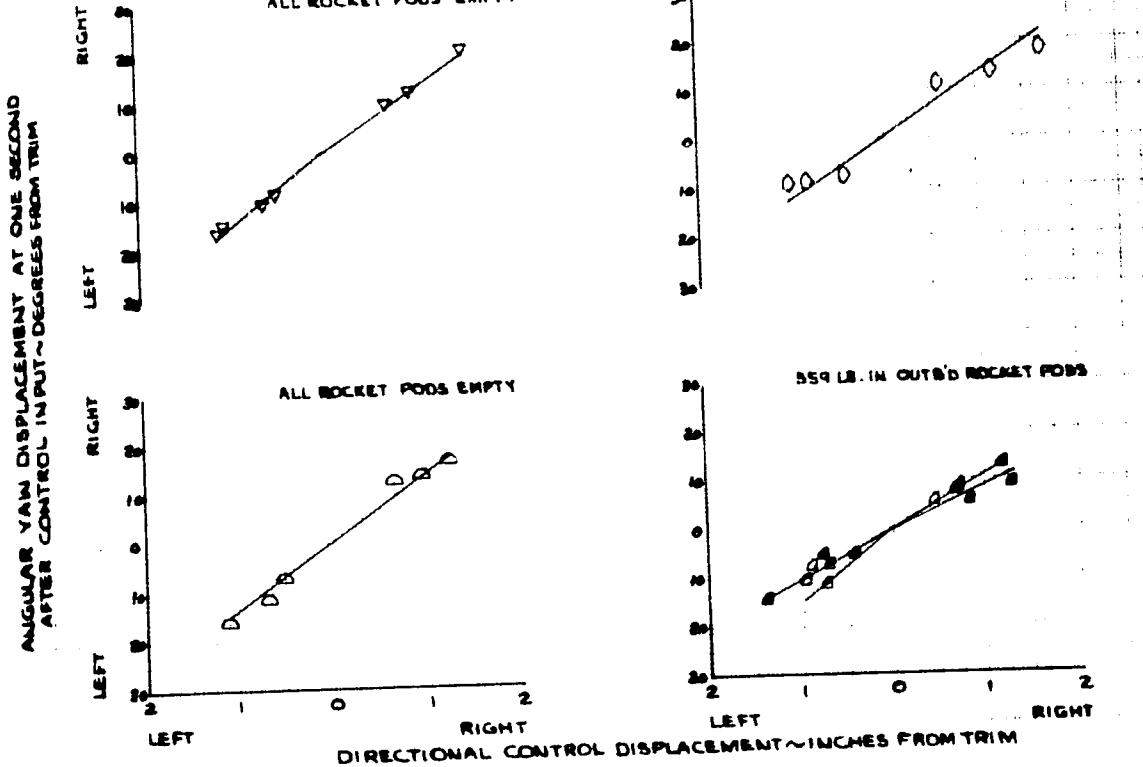


FIGURE NO. 279
ANGULAR YAW DISPLACEMENT
 AH-1G USAF 715695

HVV. HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

SYM. AVG. ALT. AVG.G.W. AVG.LONG. ROTOR FLIGHT COND. THRUST COEFF.
 HD~FT. ~LB. C.G. ~IN. RPM ~CT
 O 980 7260 20.4(AFT) 324.0 HOVER 0.008710
 D 450 8970 2005(AFT) 324.0 HOVER 0.009815

NOTES: 1. OPEN SYMBOLS DENOTE SCAS ON
 2. SOLID SYMBOLS DENOTE SCAS OFF
 3. SKID HEIGHT = 30 FEET

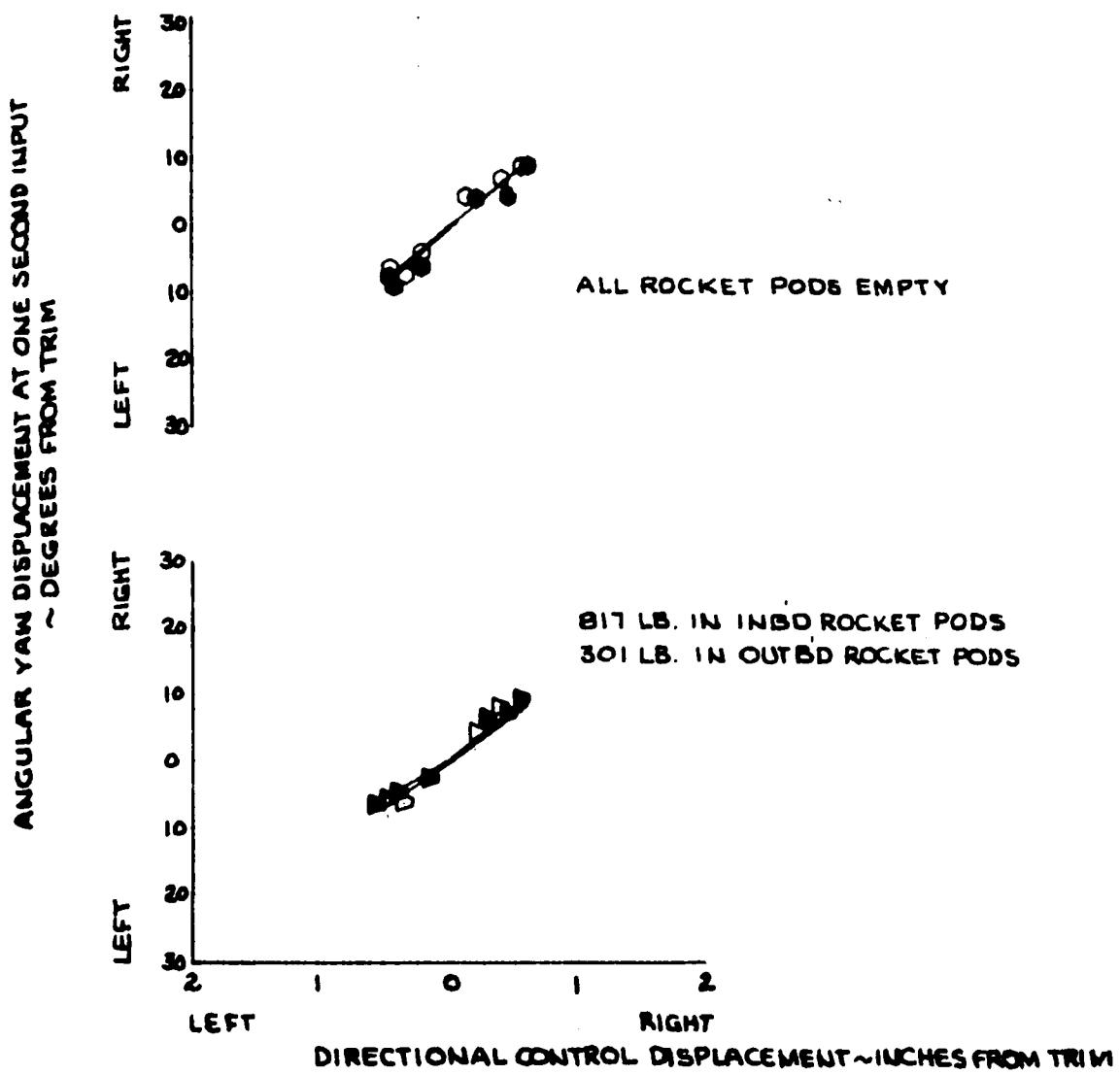
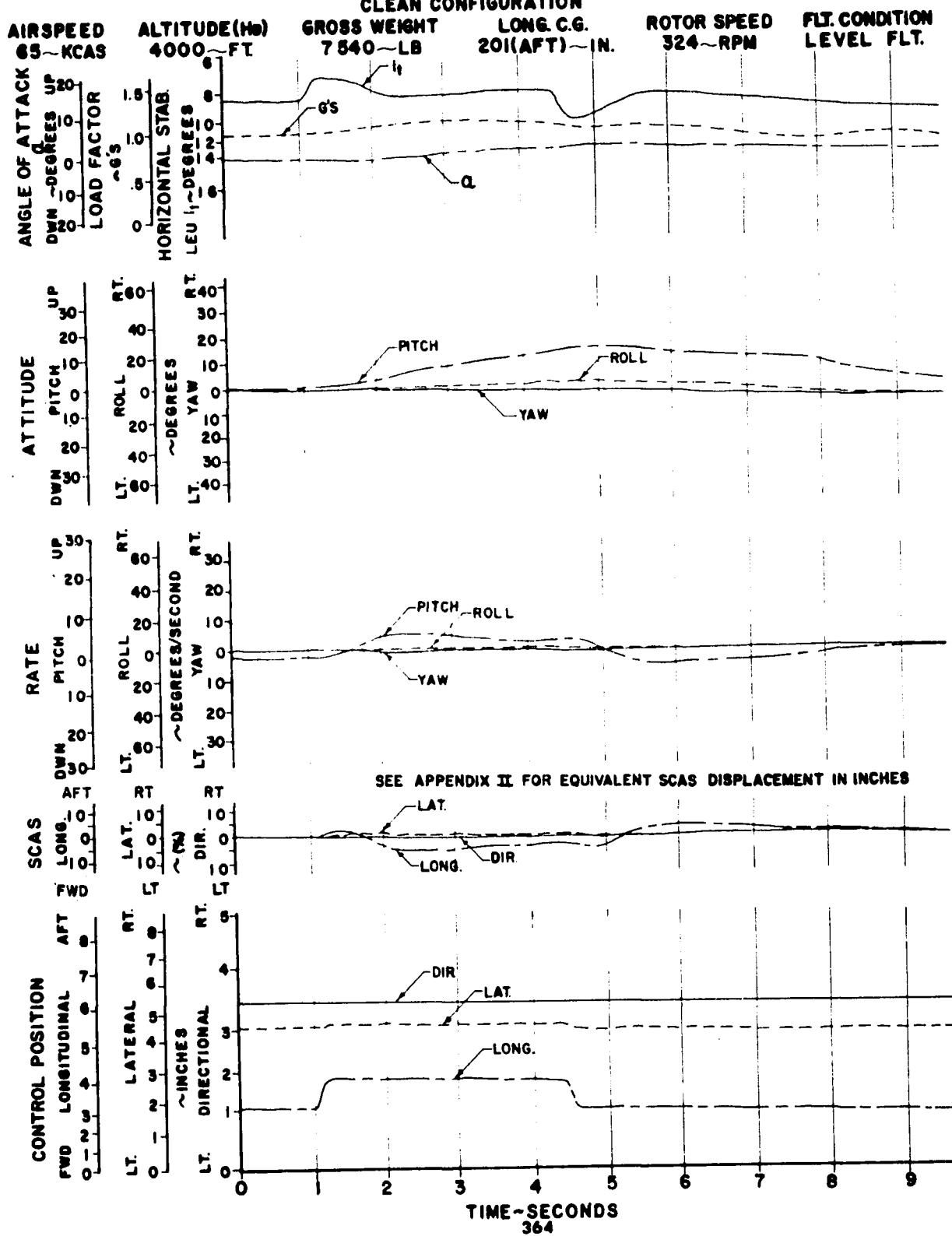


FIGURE NO. 280
AFT LONGITUDINAL STEP SCAS ON

AH-1G USA #6715695
 CLEAN CONFIGURATION



TIME-SECONDS
364

FIGURE NO. 281
FWD. LONGITUDINAL STEP SCAS ON

AH-1G USA # 6715695
CLEAN CONFIGURATION

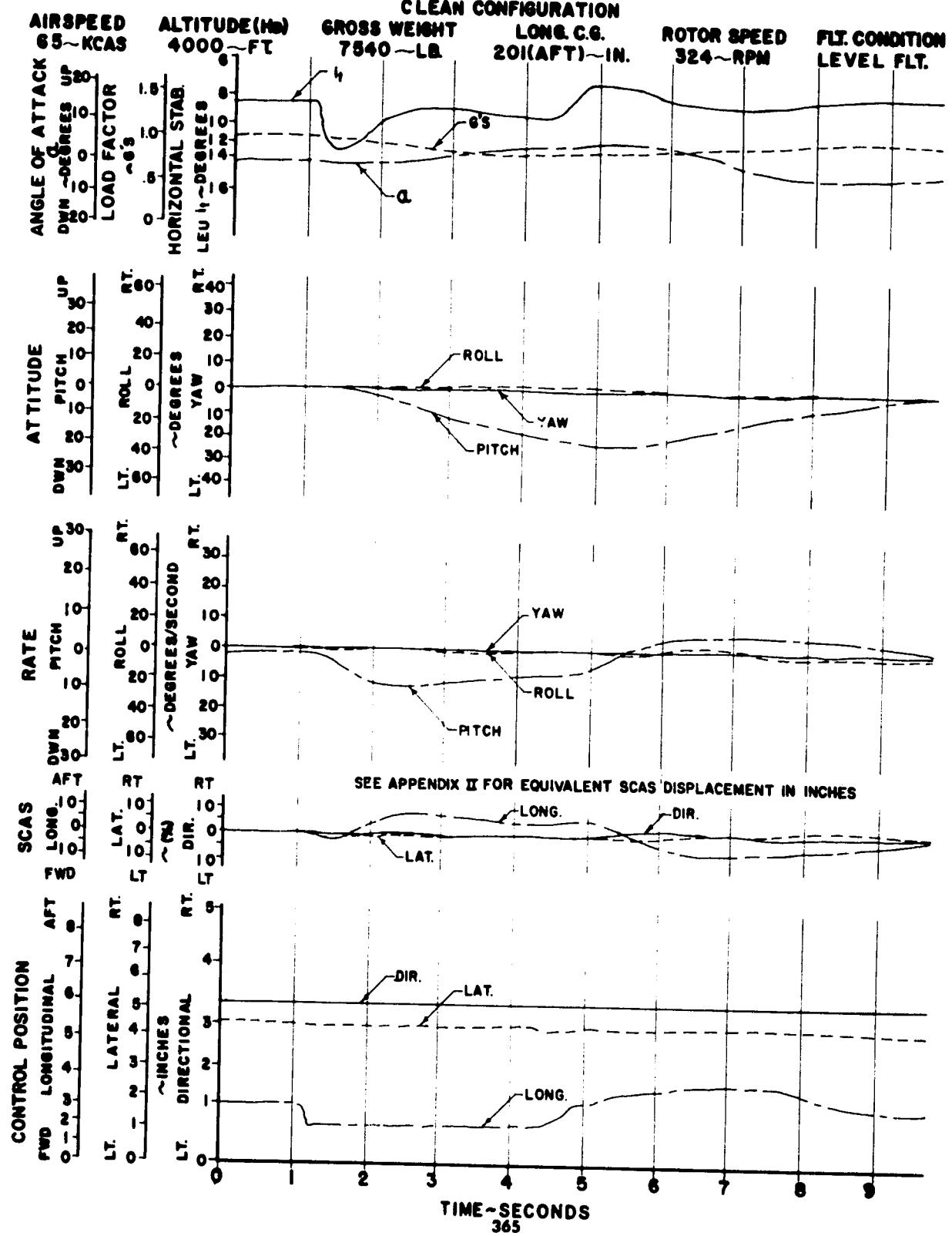


FIGURE NO. 282
RIGHT LATERAL STEP SCAS ON

AH-1G USA #6715695

HEAVY HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

AIRSPEED 105-KCAS	ALTITUDE(H) 3700-FT	GROSS WEIGHT 7620-LB	LONG. C.G. 20'(AFT)-IN.	ROTOR SPEED 324-RPM	FLT. CONDITION LEVEL FLT.
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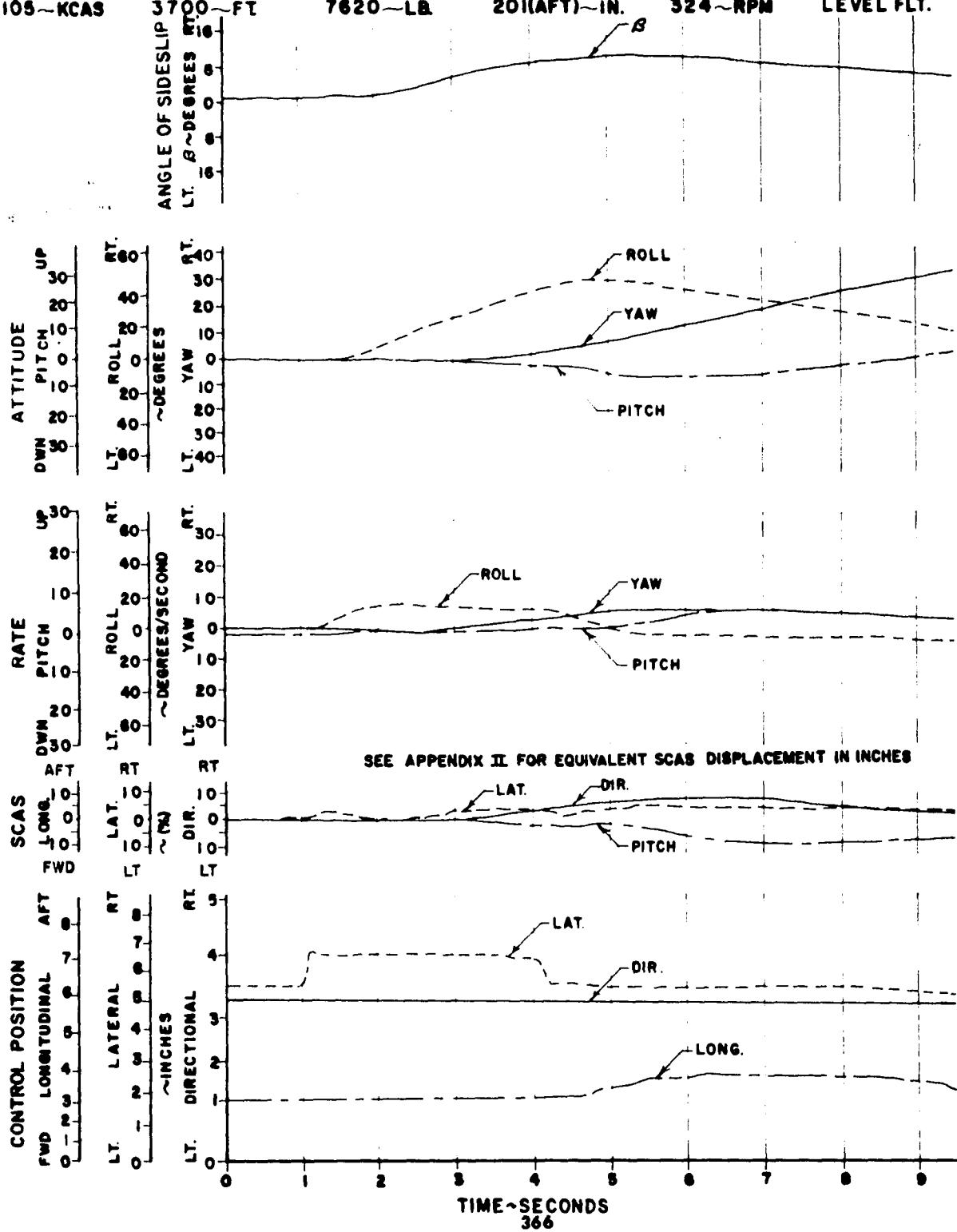


FIGURE NO. 283
LEFT LATERAL STEP SCAS ON

AH-1G USA #6715695

HEAVY HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

AIRSPEED 105~KCAS	GROSS WEIGHT 7130~LB	LONG. C.G. 201(AFT)~IN.	ROTOR SPEED 324~RPM	FLT. CONDITION LEVEL FLT.
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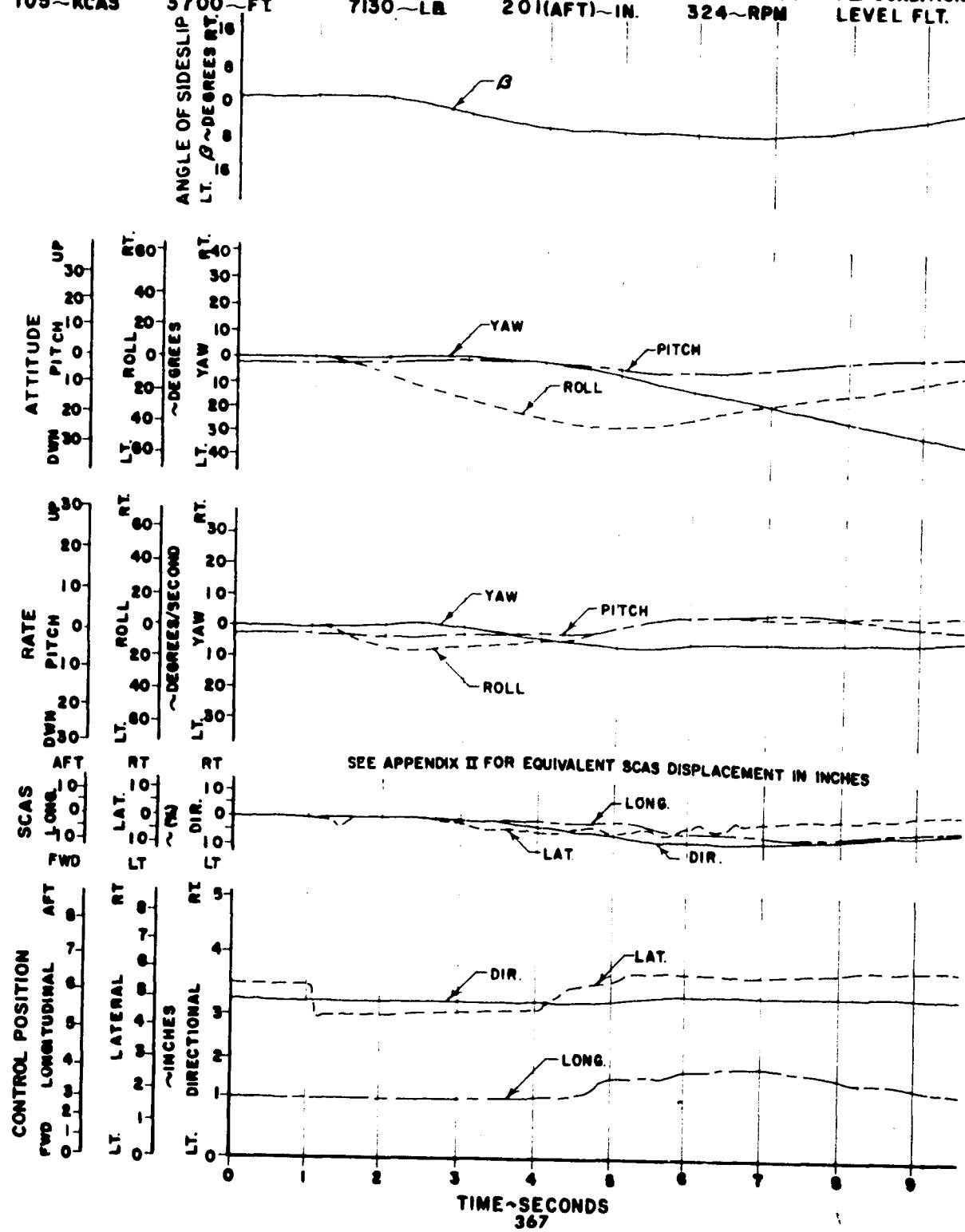


FIGURE NO. 284
RIGHT DIRECTIONAL STEP SCAS ON

AH-1G USA #6715695

HEAVY HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

AIR SPEED 55-KCAS ALTITUDE(Ho) 15400 FT GROSS WEIGHT 7620 LB LONG. C.G. 201(AFT)-IN. ROTOR SPEED 324-RPM FLT. CONDITION LEVEL FLT.

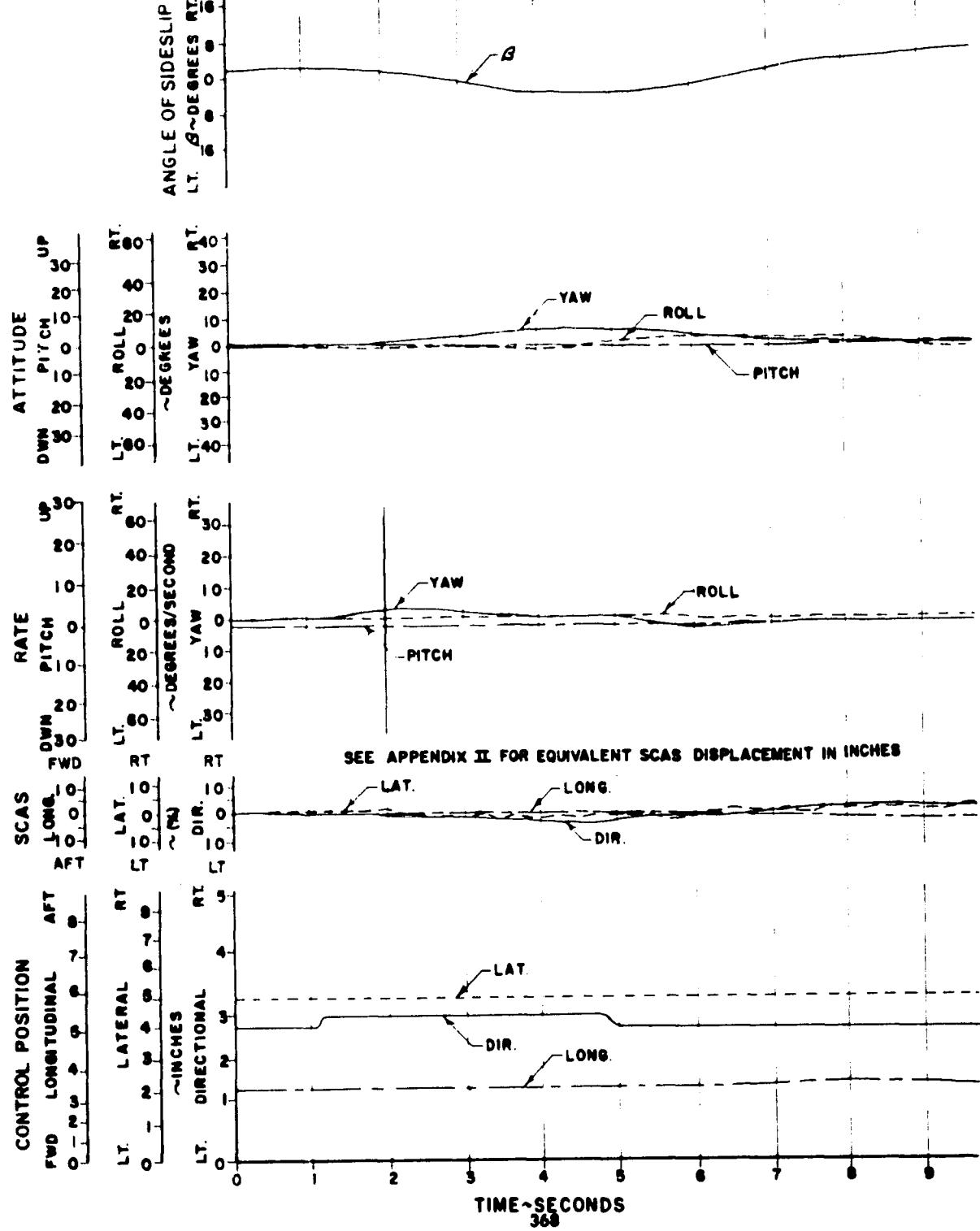


FIGURE NO. 285
LEFT DIRECTIONAL STEP SCAS ON

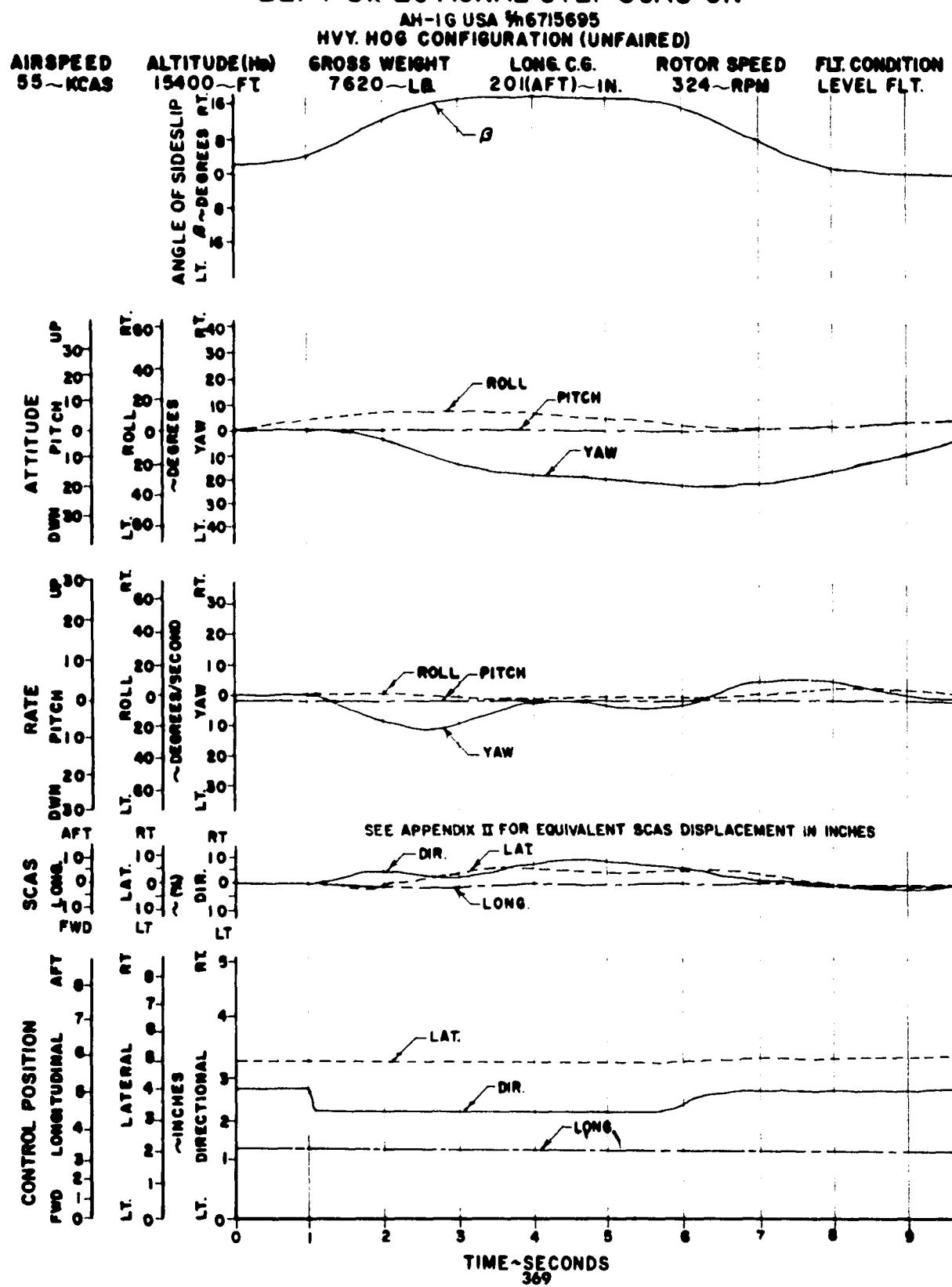


FIGURE NO. 286
LEFT DIRECTIONAL STEP SCAS ON

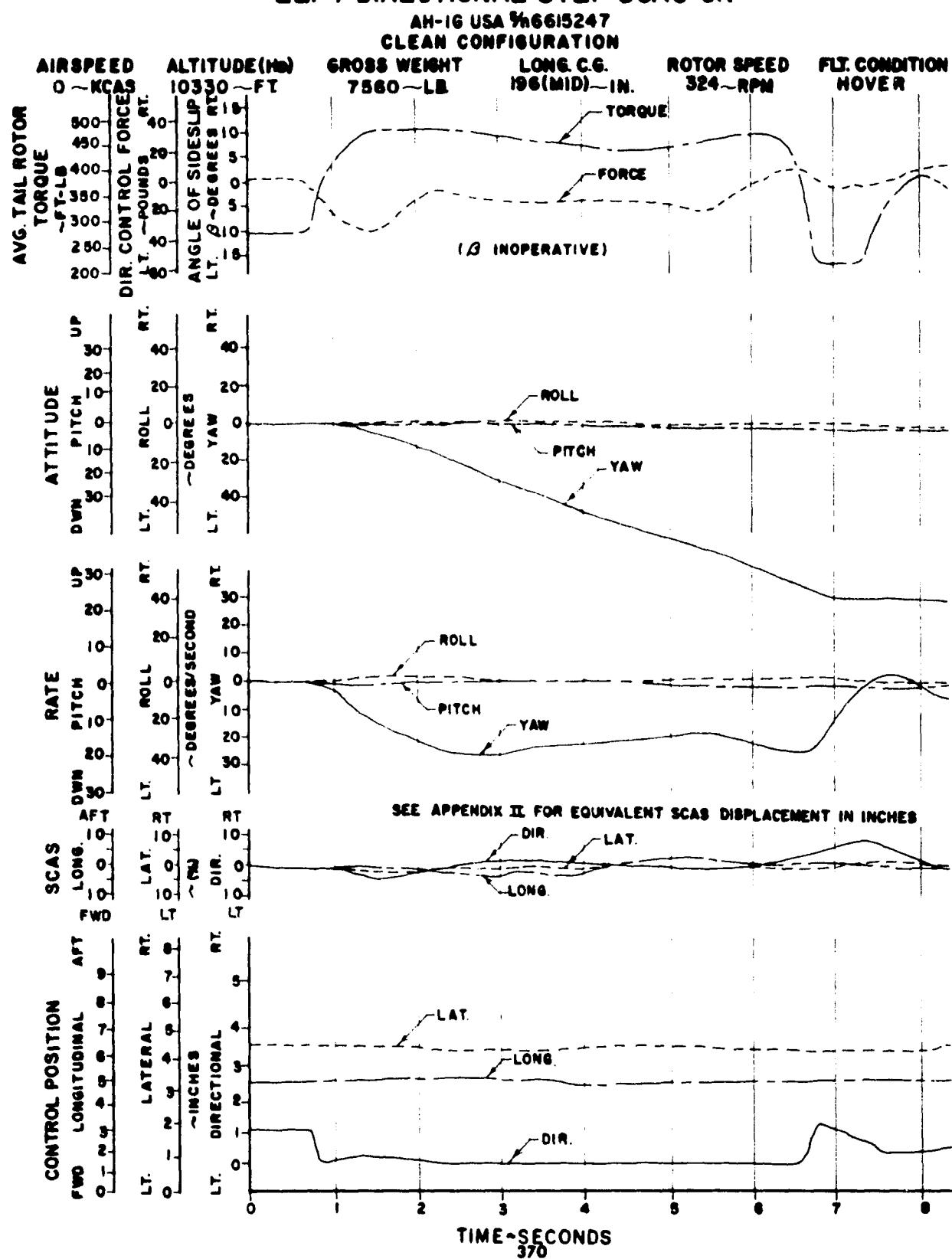


FIGURE No. 287
 DIFFERENTIAL TAIL ROTOR HORSEPOWER ENCOUNTERED DURING DIRECTIONAL INPUTS
 AH-1G USA 6615247
 CLEAN CONFIGURATION

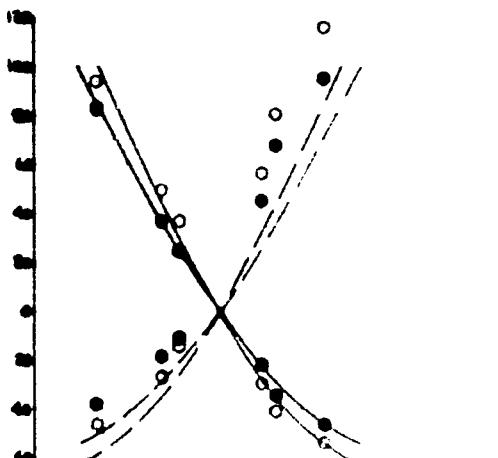
SYM	DENSITY HO ~ FT.	ALTITUDE ~ FT.	GROSS WEIGHT ~ LB.	LONG CG ~ IN.	ROTOR RPM	FLT. COND.	THRUST COEFF. ~ CT
O	6700	5650	1954(MID)	3245	HOVER	0.004921	
O	4650	6400	1952(MID)	3145		0.005116	
O	10320	1860	1957(MID)	3260		0.005188	
O	10320	7690	1956(MID)	3185		0.005484	

NOTES:
 1. ALL DATA GATHERED WITH AIRCRAFT IN GROUND EFFECT
 2. SKID HEIGHT RANGE = 5FT -> 15FT
 3. SOLID SYMBOLS DENOTE AVERAGE TAIL ROTOR HORSEPOWER
 4. OPEN SYMBOLS DENOTE PEAK TAIL ROTOR HORSEPOWER
 5. SOLID LINES DENOTE DIFFERENTIAL TAIL ROTOR HORSEPOWER
 RESULTING FROM INITIAL CONTROL INPUT
 6. DASHED LINES DENOTE DIFFERENTIAL TAIL ROTOR HORSEPOWER
 RESULTING FROM RECOVERY INPUT
 7. DIFFERENTIAL TAIL ROTOR HORSEPOWER IS EQUAL TO TAIL ROTOR
 HORSEPOWER, RESULTING FROM INPUT MINUS TAIL ROTOR HORSEPOWER
 FOR A TRIMMED HOVER CONDITION

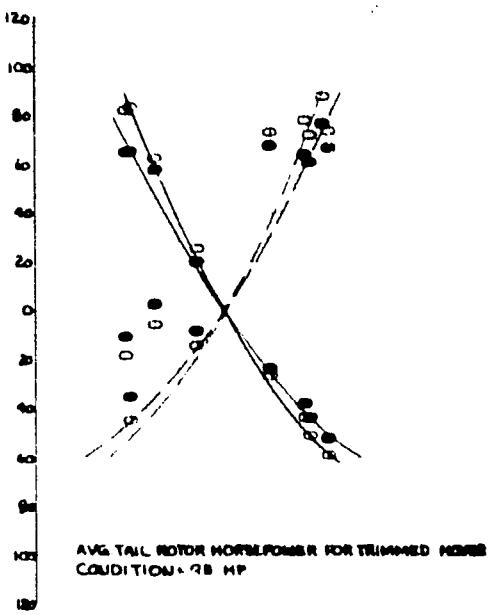
SCAS ON

SCAS ON

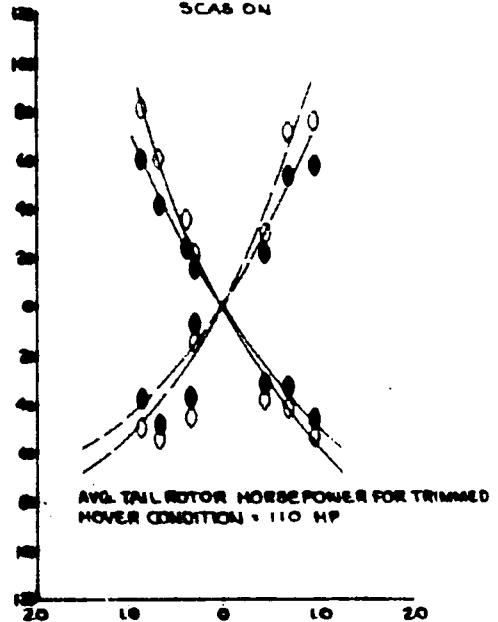
Differential Tail Rotor Horsepower



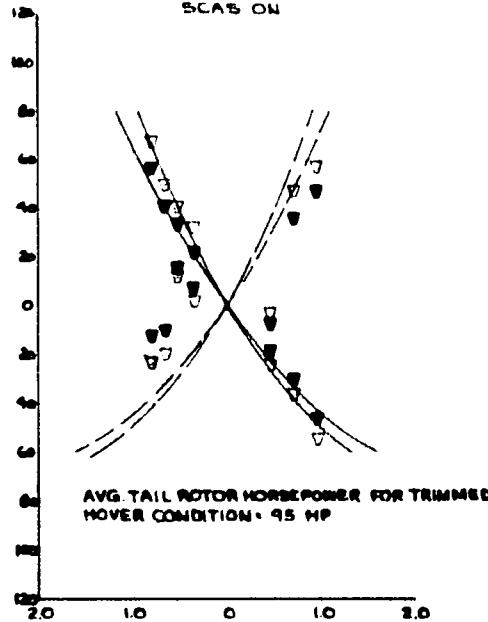
Avg. TAIL ROTOR HORSEPOWER FOR TRIMMED HOVER
CONDITION = 101 HP



Avg. TAIL ROTOR HORSEPOWER FOR TRIMMED HOVER
CONDITION = 98 HP



Avg. TAIL ROTOR HORSEPOWER FOR TRIMMED
HOVER CONDITION = 110 HP



Avg. TAIL ROTOR HORSEPOWER FOR TRIMMED
HOVER CONDITION = 95 HP

DIRECTIONAL CONTROL DISPLACEMENT ~ INCHES FROM TRIM

FIGURE NO. 288
DIFFERENTIAL TAIL ROTOR HORSEPOWER ENCOUNTERED DURING DIRECTIONAL INPUTS
 AH-1G USA #618247
 CLEAN CONFIGURATION

SYN.	DENSITY ALTITUDE Hg ~ FT.	GROSS WEIGHT ~ LB.	LNG.C. ~ IN.	ROTOR RPM	FLY. COND.	THRUST COEFF. ~ CT
○	4500	7200	1856 (MID)	3250	HOVER	0.004168
○	4500	7200	1856 (MID)	3145		0.004160
○	5500	7200	1856 (MID)	3260		0.004166
○	6500	7200	1856 (MID)	3145		0.004167

NOTES:
 1. ALL DATA GATHERED WITH AIRCRAFT IN GROUND EFFECT
 2. SKID HEIGHT RANGE = 5FT. - 15 FT.
 3. SOLID SYMBOLS DENOTE AVERAGE TAIL ROTOR HORSEPOWER
 4. OPEN SYMBOLS DENOTE PEAK TAIL ROTOR HORSEPOWER
 5. SOLID LINES DENOTE DIFFERENTIAL TAIL ROTOR HORSEPOWER RESULTING
 FROM INITIAL CONTROL INPUT
 6. DASHED LINE DENOTE DIFFERENTIAL TAIL ROTOR HORSEPOWER
 RESULTING FROM RECOVERY
 7. DIFFERENTIAL TAIL ROTOR HORSEPOWER IS EQUAL TOTAL TAIL ROTOR HORSEPOWER
 RESULTING FROM INPUT MINUS TAIL ROTOR HORSEPOWER FOR A TRIMMED
 HOVER CONDITION

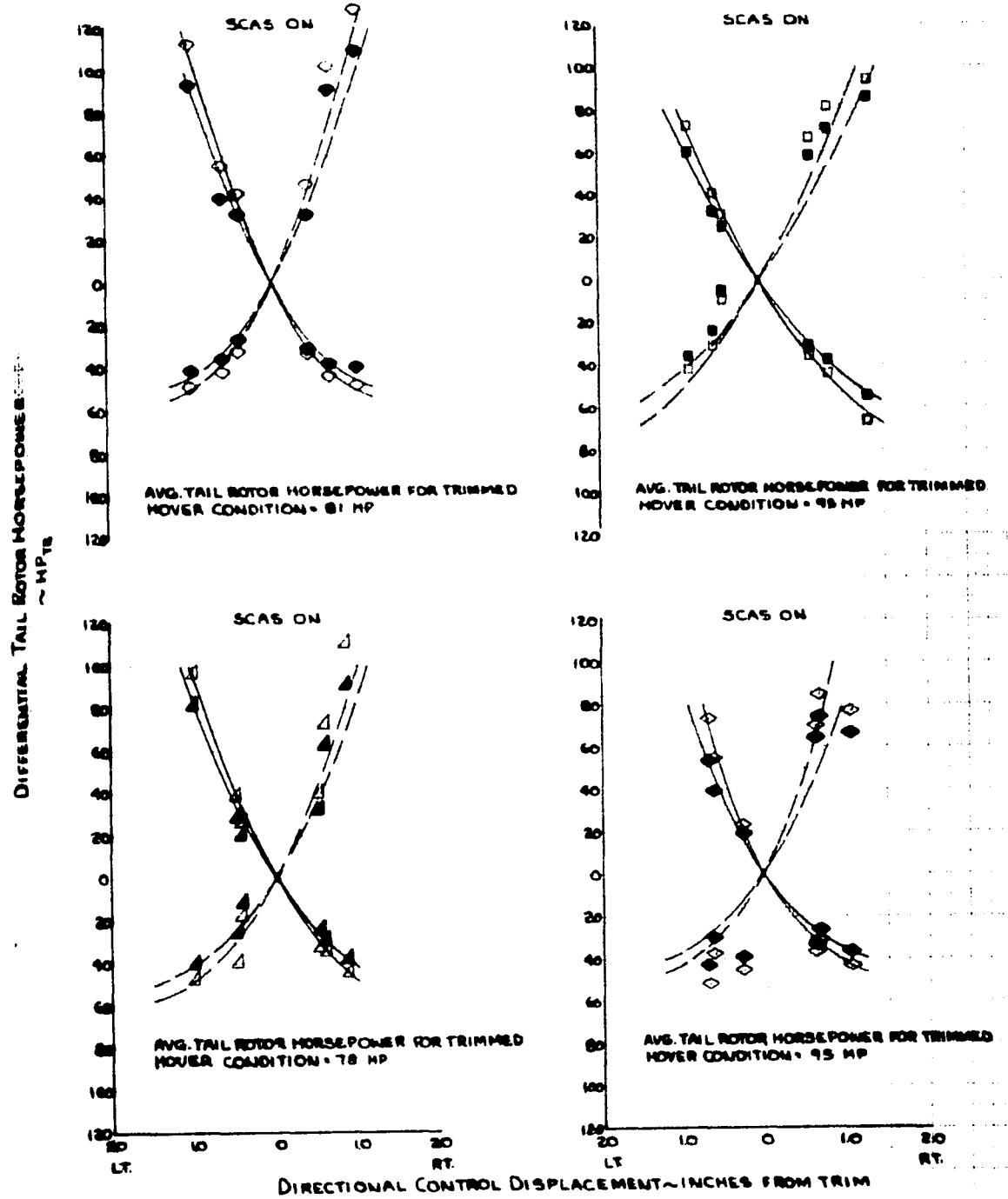


FIGURE NO. 209
 DIFFERENTIAL TAIL ROTOR HORSEPOWER ENCOUNTERED DURING DIRECTIONAL INPUTS
 AH-1G USAF 619267
 CLEAN CONFIGURATION

SYM	DENSITY ALTITUDE GROSS WEIGHT LBS/IN. HD ~ FT.	BLDG. ~LB.	ROTOR BLDG.	FLOWD. ~CT	THRUST COEF.
▲	360	7160	195.2 (HUB)	2160	HOVER 0.00414
▲	360	7160	195.2 (HUB)	2260	0.00418
○	660	7160	195.1 (HUB)	3165	0.00389
○	670	6960	195.9 (HUB)	3265	0.004017

NOTES: 1. ALL DATA GATHERED WITH AIRCRAFT IN GROUND EFFECT
 2. SKID HEIGHT RANGE = 5FT - 15FT.
 3. SOLID SYMBOLS DENOTE AVERAGE TAIL ROTOR HORSEPOWER
 4. OPEN SYMBOLS DENOTE PEAK TAIL ROTOR HORSEPOWER
 5. SOLID LINES DENOTE DIFFERENTIAL TAIL ROTOR HORSEPOWER
 RESULTING FROM INITIAL CONTROL INPUT
 6. DASHED LINES DENOTE DIFFERENTIAL TAIL ROTOR HORSEPOWER
 RESULTING FROM RECOVERY
 7. DIFFERENTIAL TAIL ROTOR HORSEPOWER IS EQUAL TO TAIL ROTOR
 HORSEPOWER RESULTING FROM INPUT MINUS TAIL ROTOR HORSEPOWER
 FOR A TRIMMED HOVER CONDITION

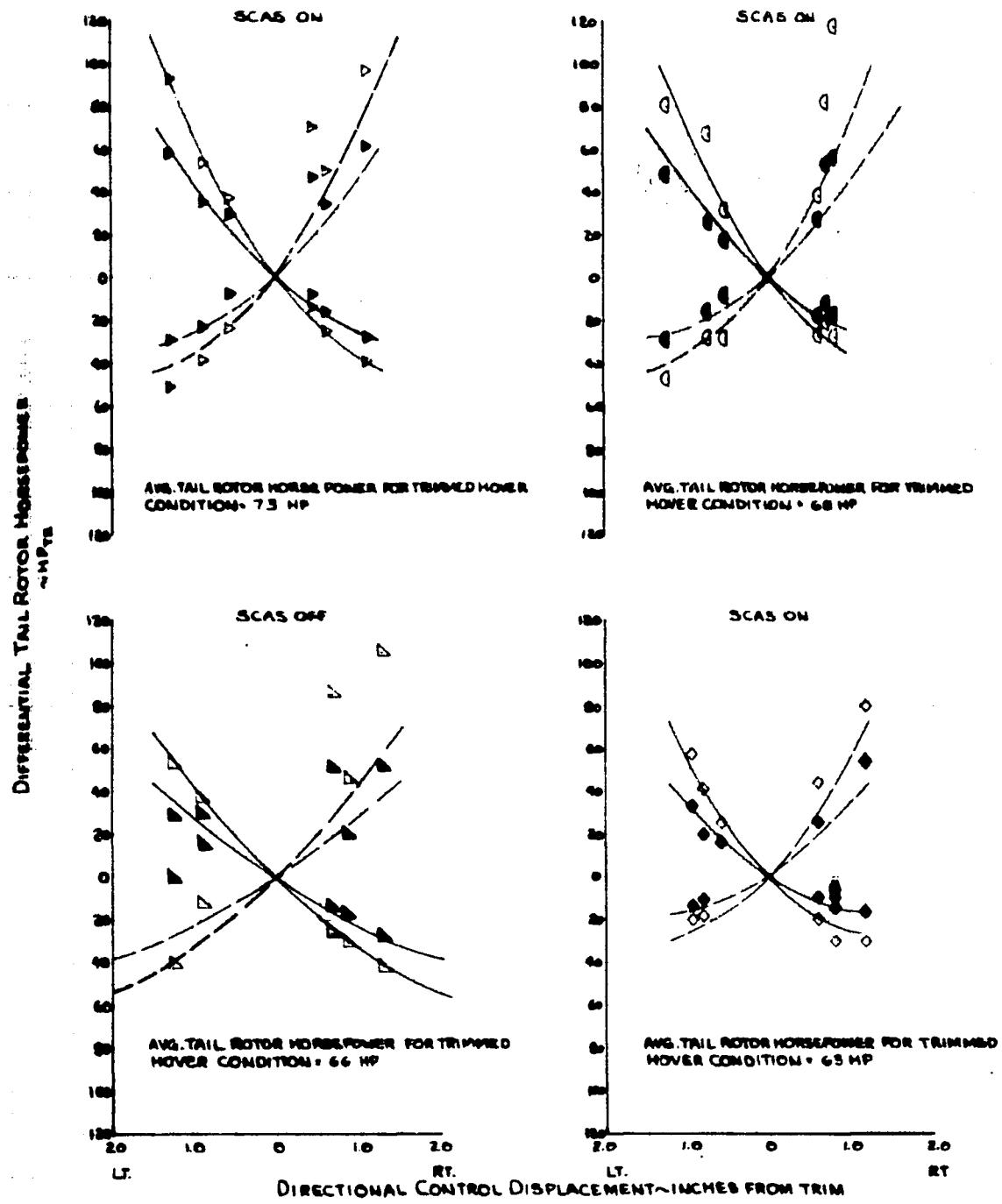


FIGURE No. 290
SUMMARY OF STICK FIXED AND STICK FREE
MANEUVERING STABILITY
AH-1G USA 4/N615247
CLEAN CONFIGURATION

SYM	AVG. AIRSPEED $V_c \sim$ KCAS	AVG. GROSS WEIGHT ~ LB
○	138	7800
□	138	7000
△	117	7800
△	117	7000

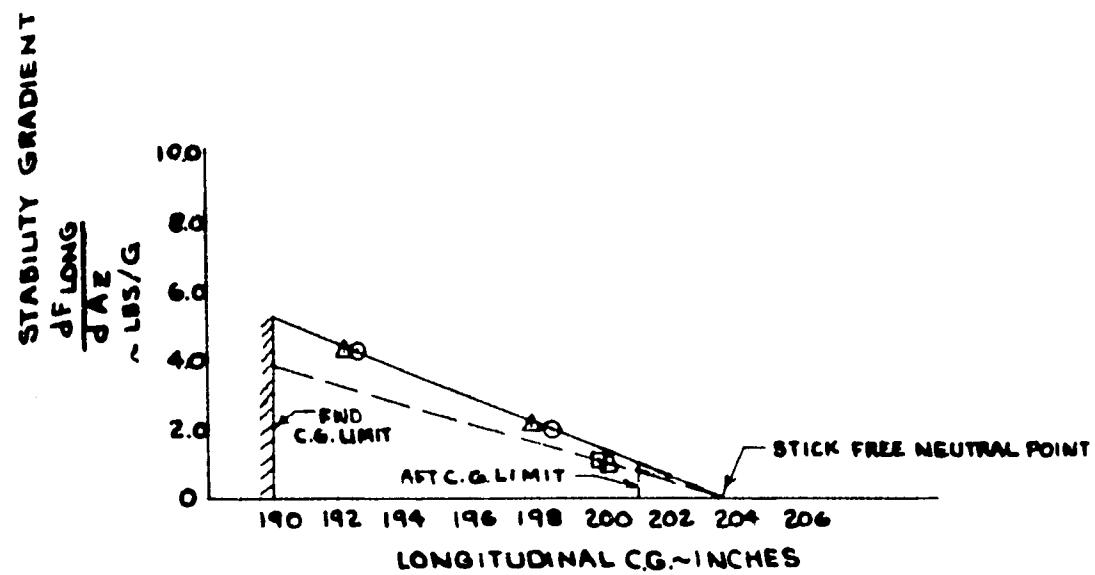
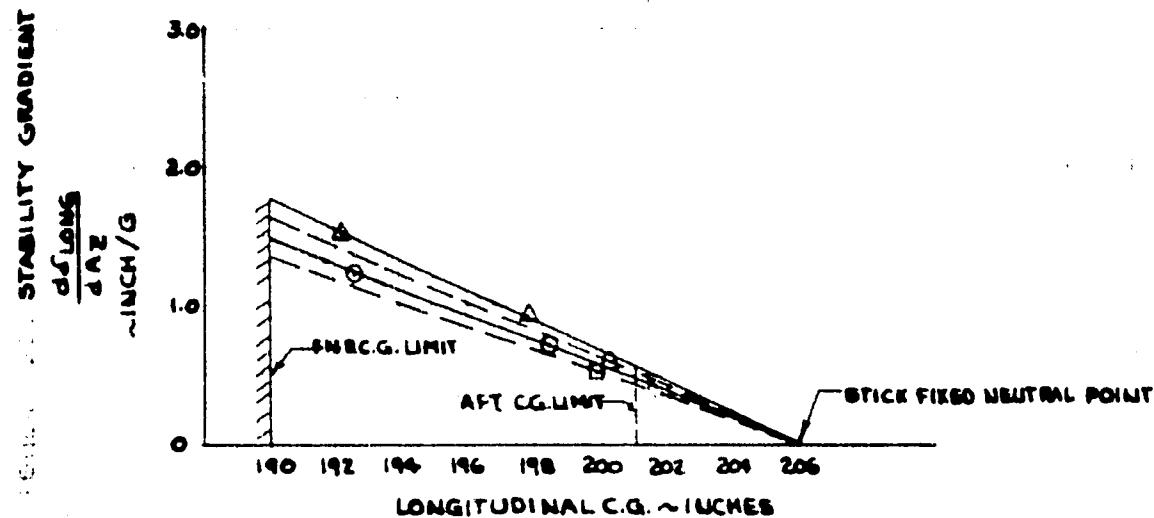


FIGURE NO. 291
MANEUVERING STABILITY
AH-1G USA #615247
CLEAN CONFIGURATION

NOTES:
 1 □ DENOTES LEFT MIND-UP TURN
 2 □ DENOTES RIGHT MIND-UP TURN
 3 △ DENOTES SYMMETRICAL PULL-UP
 4 CYCLIC FORCE TRIM ON
 5 LONGITUDINAL CONTROL FORCE
 MEASURED AT CENTER OF HAND GRIP

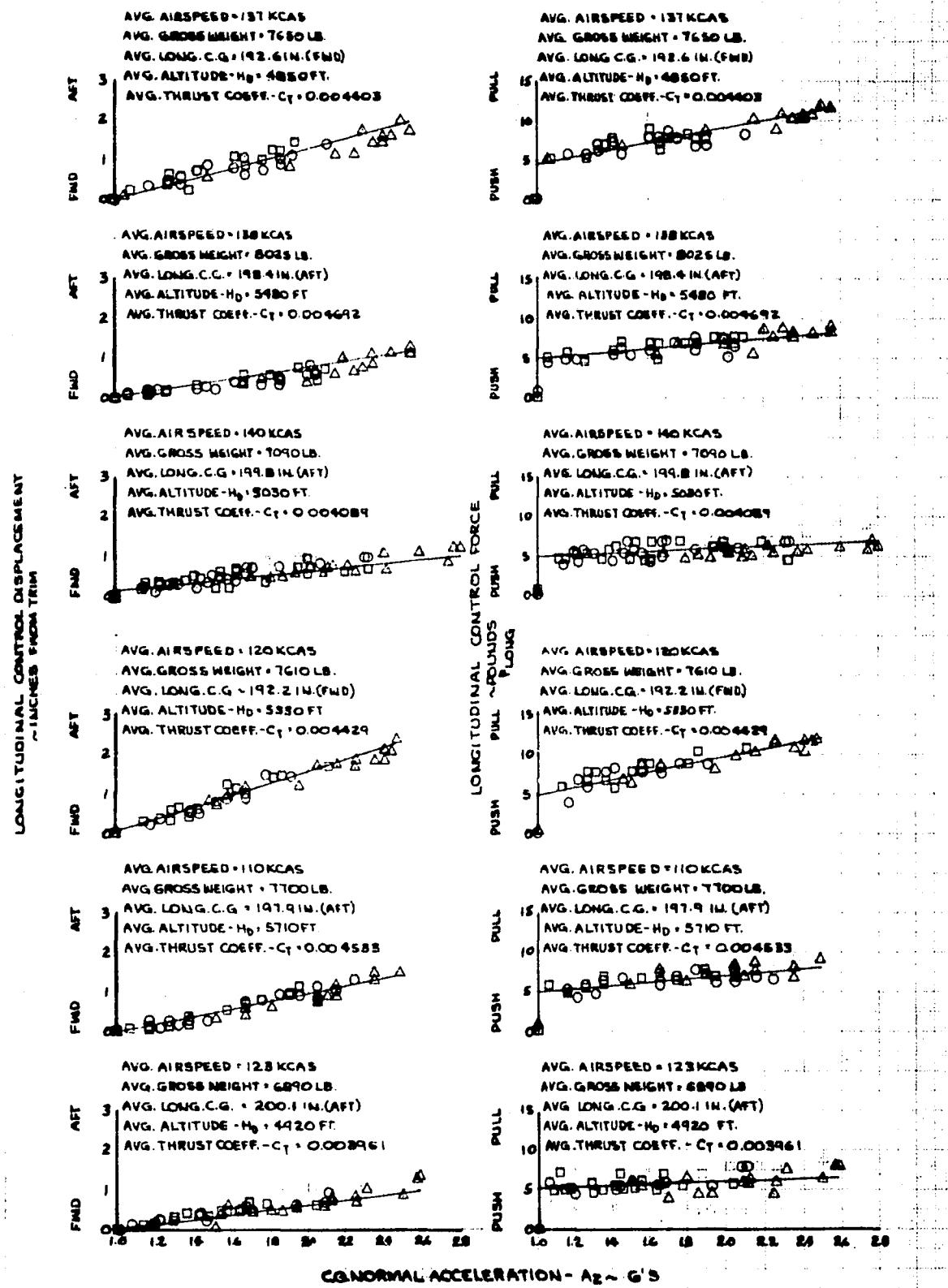


FIGURE NO. 292
LATERAL CYCLIC CONTROL VARIATION WITH AIRCRAFT LOAD FACTOR

AH-1G USA #615247
 CLEAN CONFIGURATION
 MOTOR SPEED: 820 RPM
 NOTES:
 ○ DENOTES LEFT WING UP TURN
 □ DENOTES RIGHT WING UP TURN
 △ DENOTES SYMMETRICAL PULL-UP

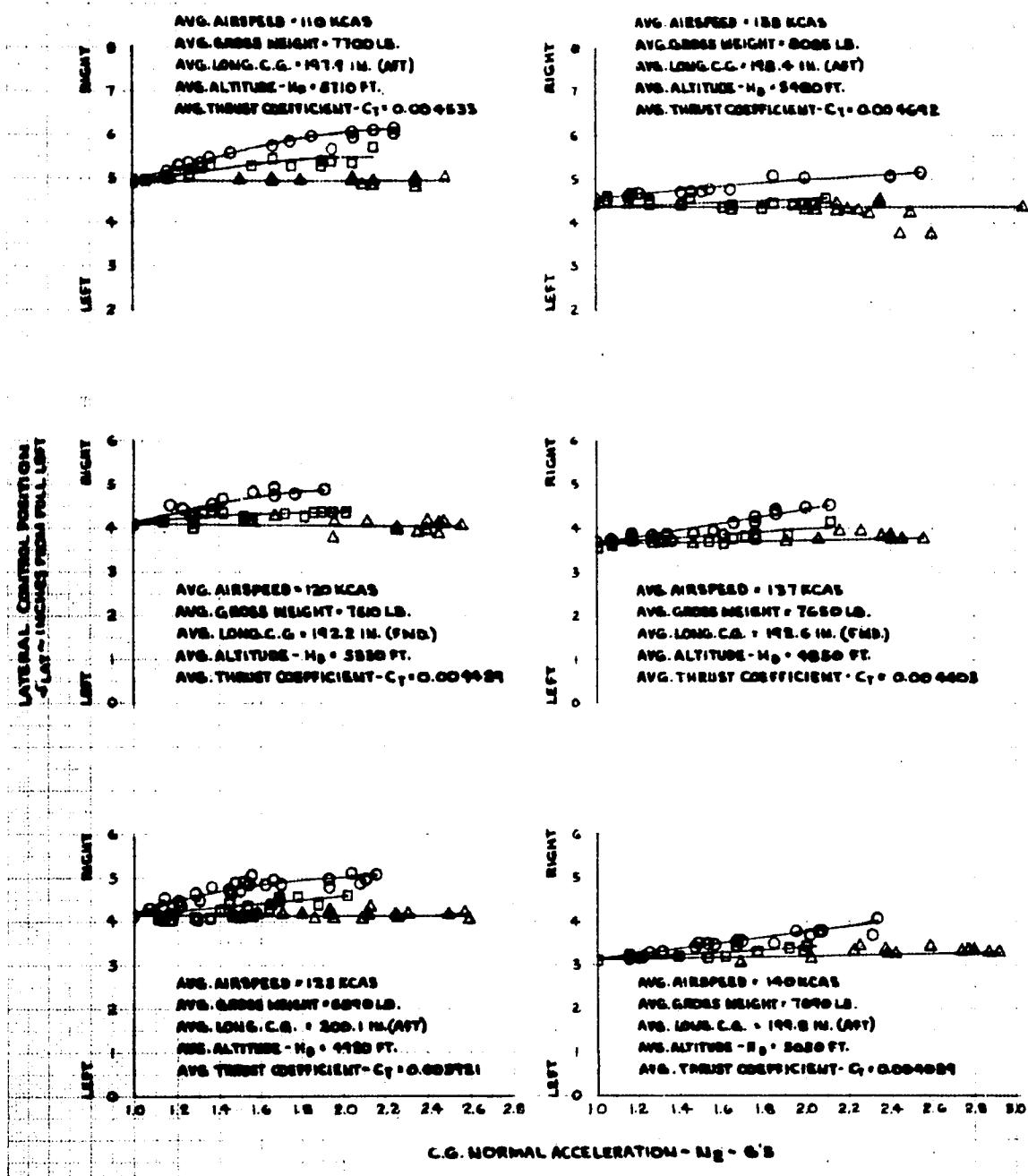


FIGURE NO 293
SUMMARY OF AIRCRAFT REACTION AND RECOVERY FOLLOWING A SIMULATED ENGINE FAILURE

AH-1G USA 46615247
CLEAN CONFIGURATION

AVG. TRIM CONDITIONS:

SYM. DENSITY ALT.	GWEIGHT	LONG CG	ROTOR SPEED	CONFIGURATION OF LANDING
H ₀ - FT.	- LB.	- IN.	- RPM	GEAR CROSS TUBE FAIRINGS
○ 5000	7260	201.0 (AFT)	8240	INSTALLED
□ 5000	7060	201.0 (AFT)	8240	NOT INSTALLED

NOTE: 1. FLAGGED SYMBOLS DENOTE CLIMBING FLIGHT AT 1100 RPM ORENGINE TOPPING POWER WHICH EVER IS LESS
2. AVG. ENGINE SHAFT HORSEPOWER IN A DIVE WAS 1050 SHP AT 5000 FT.

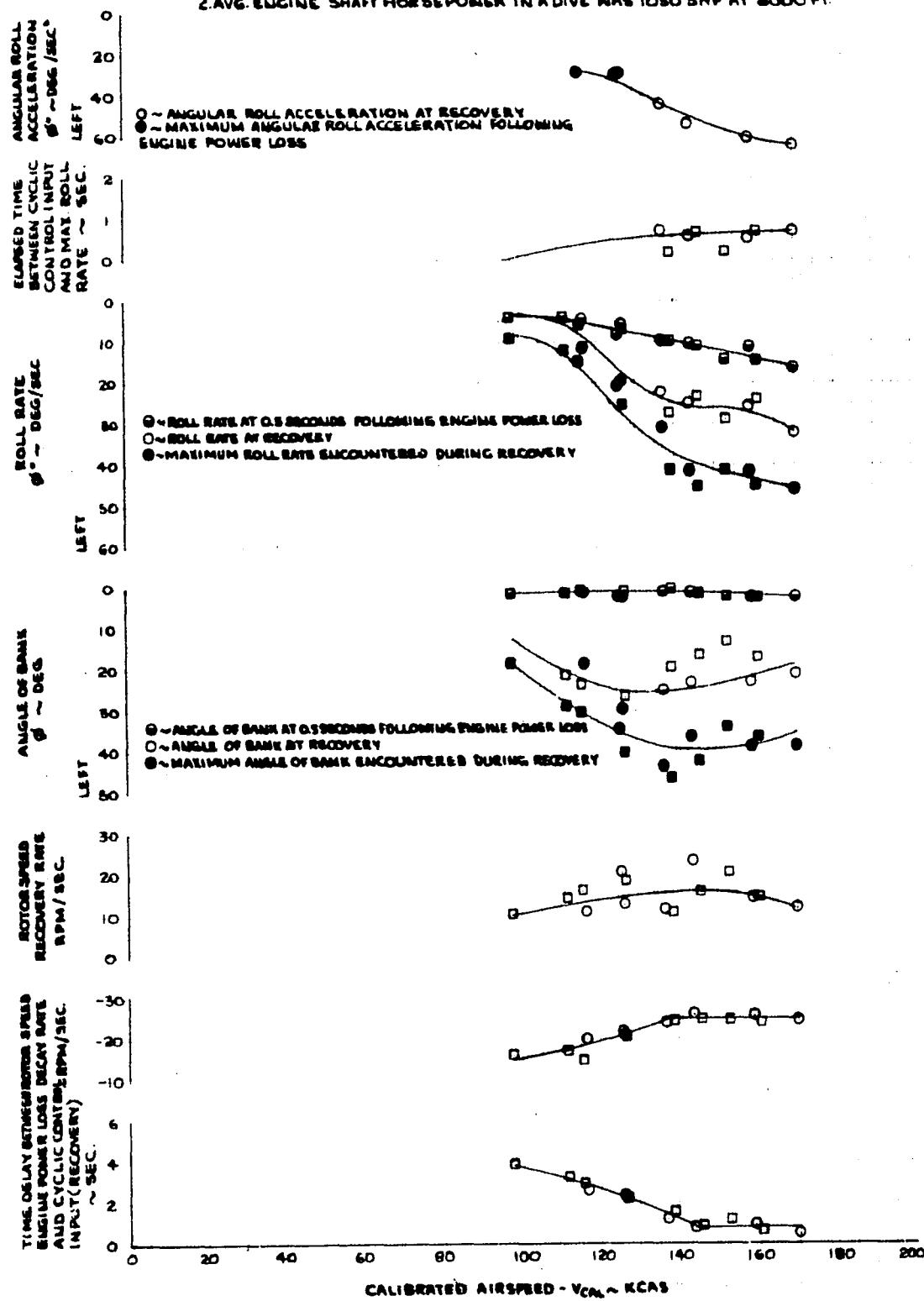


FIGURE No 293 (CONTINUE)

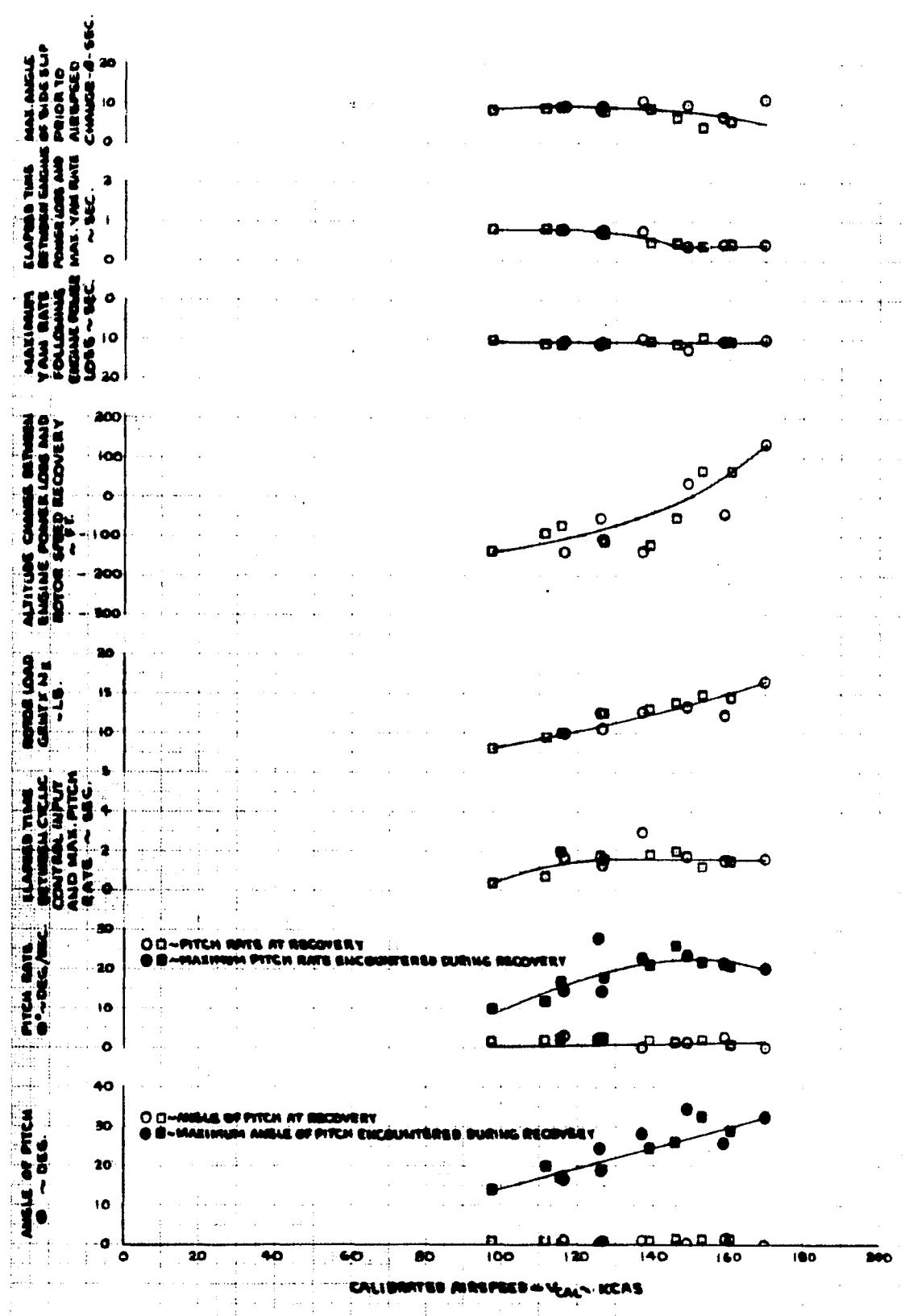


FIGURE NO. 294
SUMMARY OF AIRCRAFT REACTION AND RECOVERY FOLLOWING A SIMULATED ENGINE FAILURE

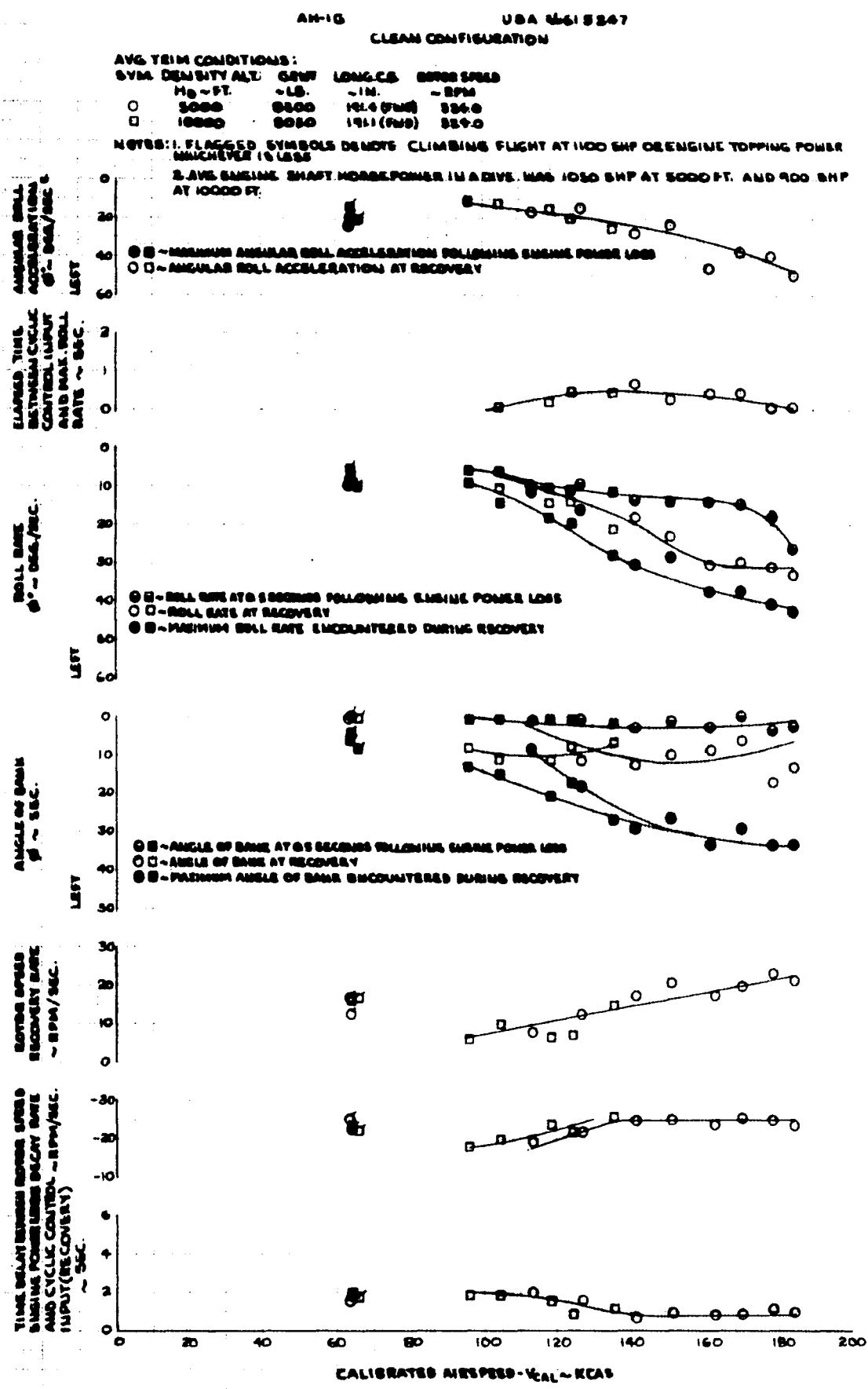


FIGURE No 294 (continued)

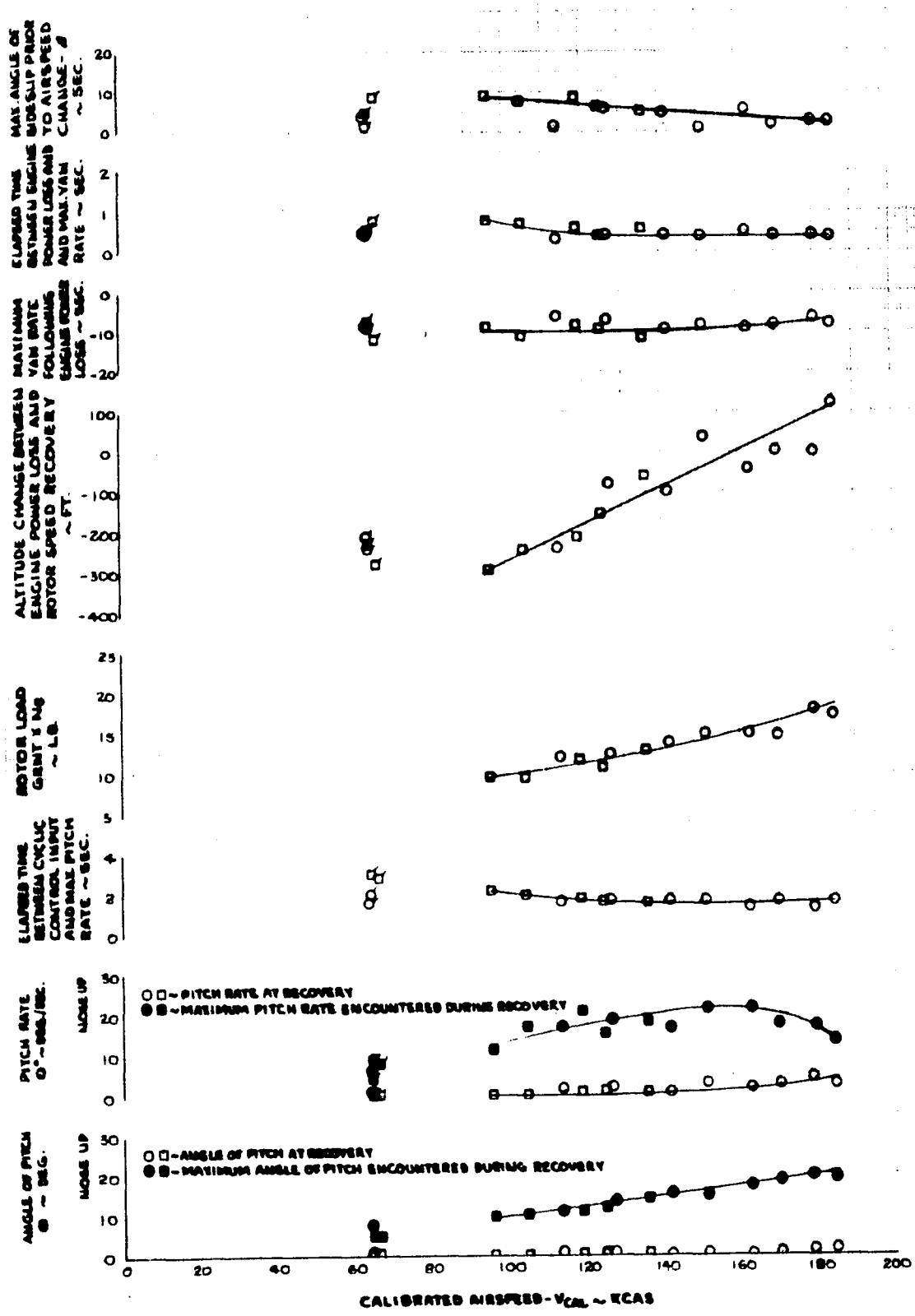


FIGURE NO. 295
SUMMARY OF AIRCRAFT REACTION AND RECOVERY FOLLOWING A SIMULATED ENGINE FAILURE

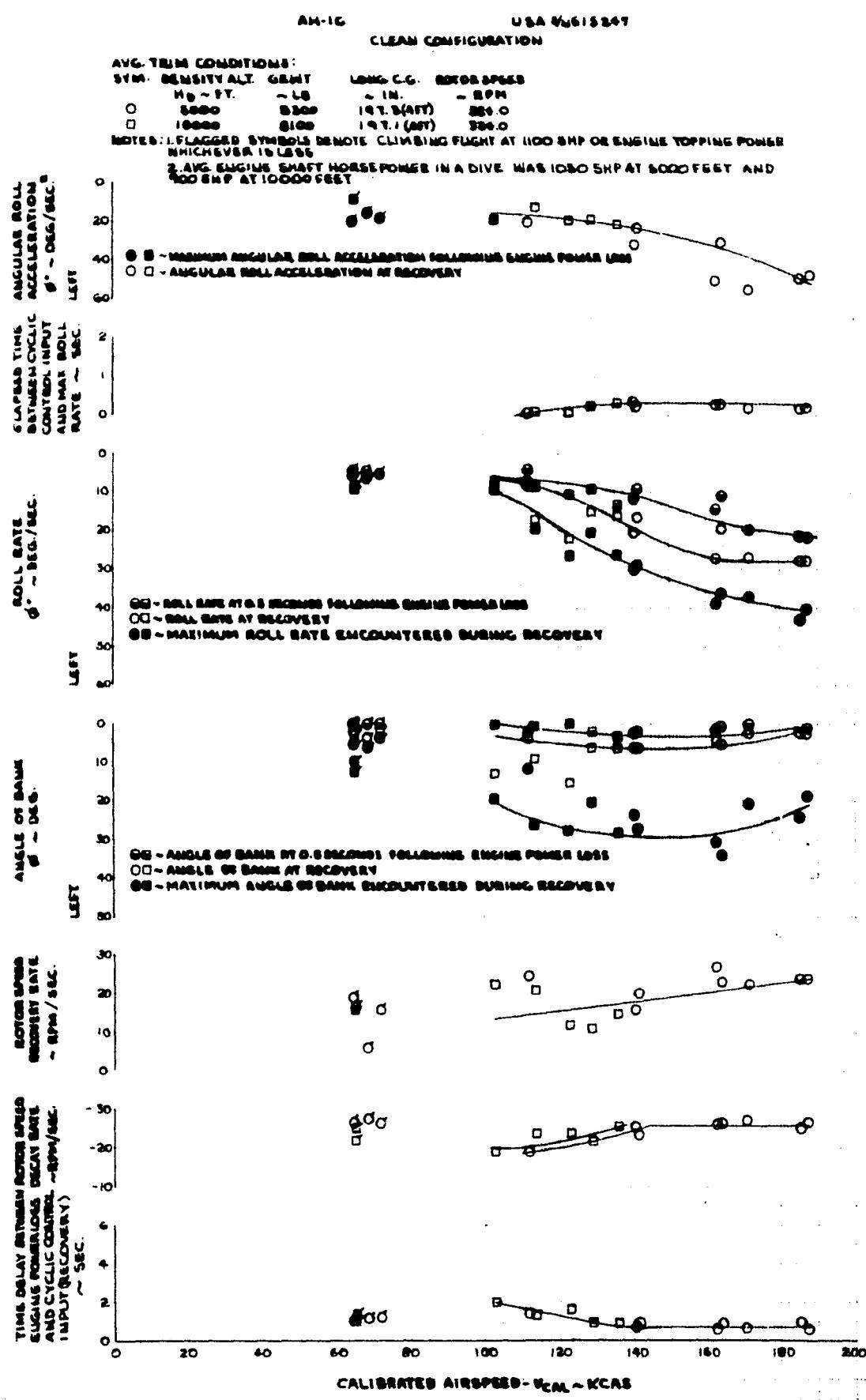


FIGURE NO 245 (CONTINUED)

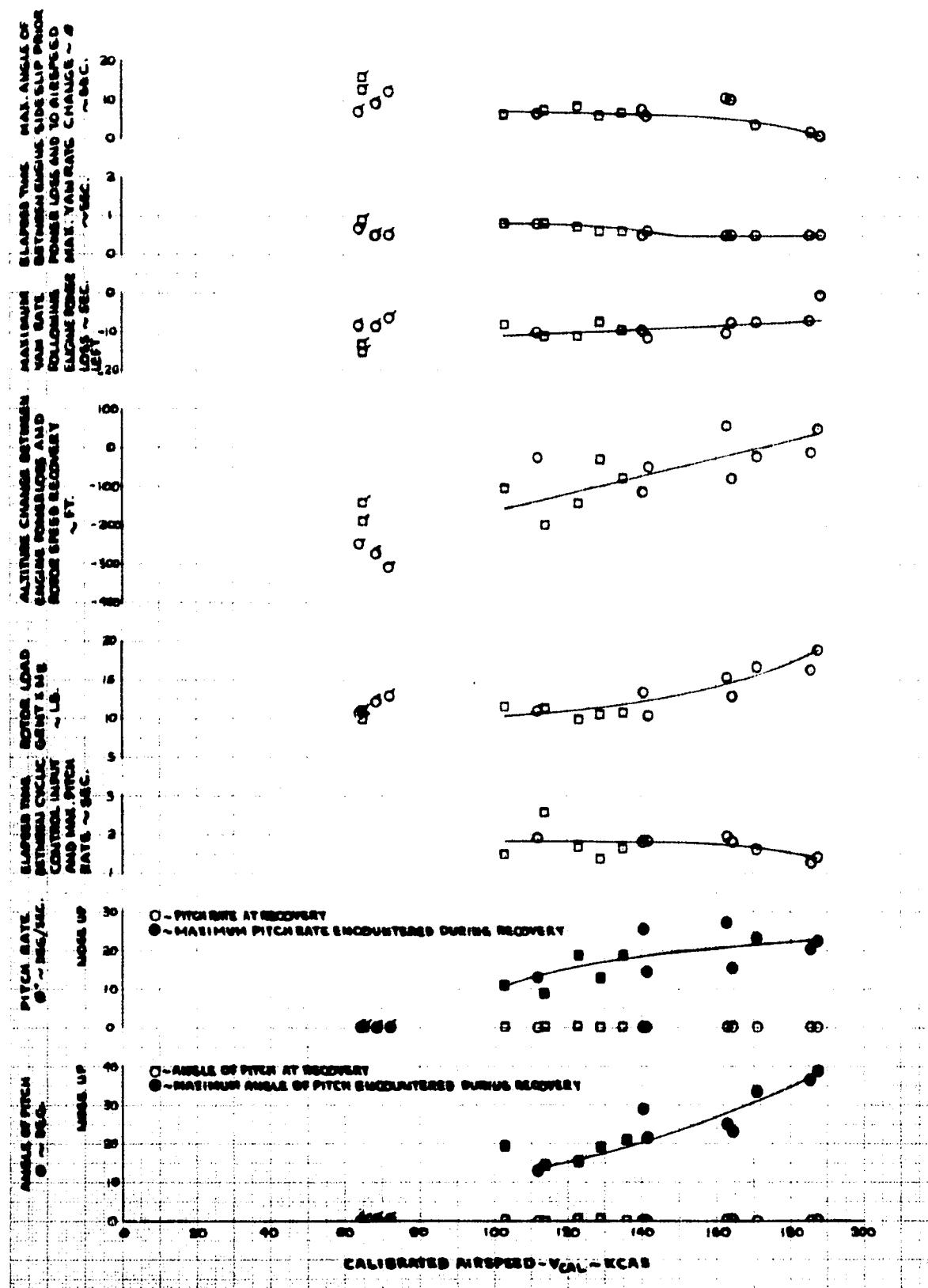


FIGURE NO. 296

SUMMARY OF AIRCRAFT REACTION AND RECOVERY FOLLOWING A SIMULATED ENGINE FAILURE

AM-1G USA #615267

MVY. MOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

Avg. TBM CONDITIONS:

AVG. TURBINE POWER - 1000000000
SYM. DENSITY ALT. GRANT LONG. C.S. MOTOR SPEED
HO - FT. "LB. - IN. - RPM
5000 2.50 192.8(FWD) 324.0

NOTES: 1. FLAGGED SYMBOLS DENOTE CLIMBING FLIGHT AT 100 MPH OR ENGINE TIPPING POWER
WHICHEVER IS LESS

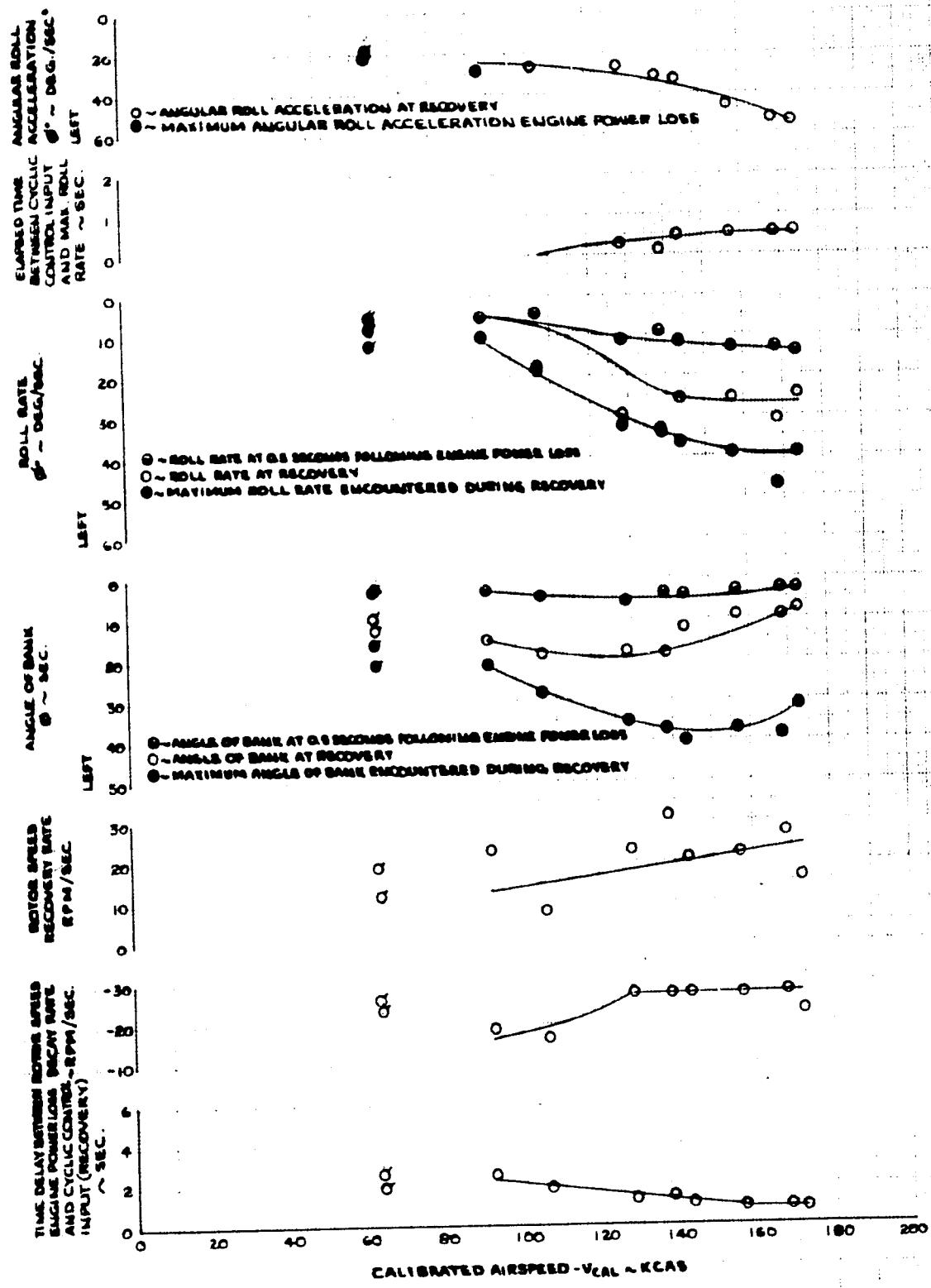


FIGURE NO. 296 (CONTINUED)

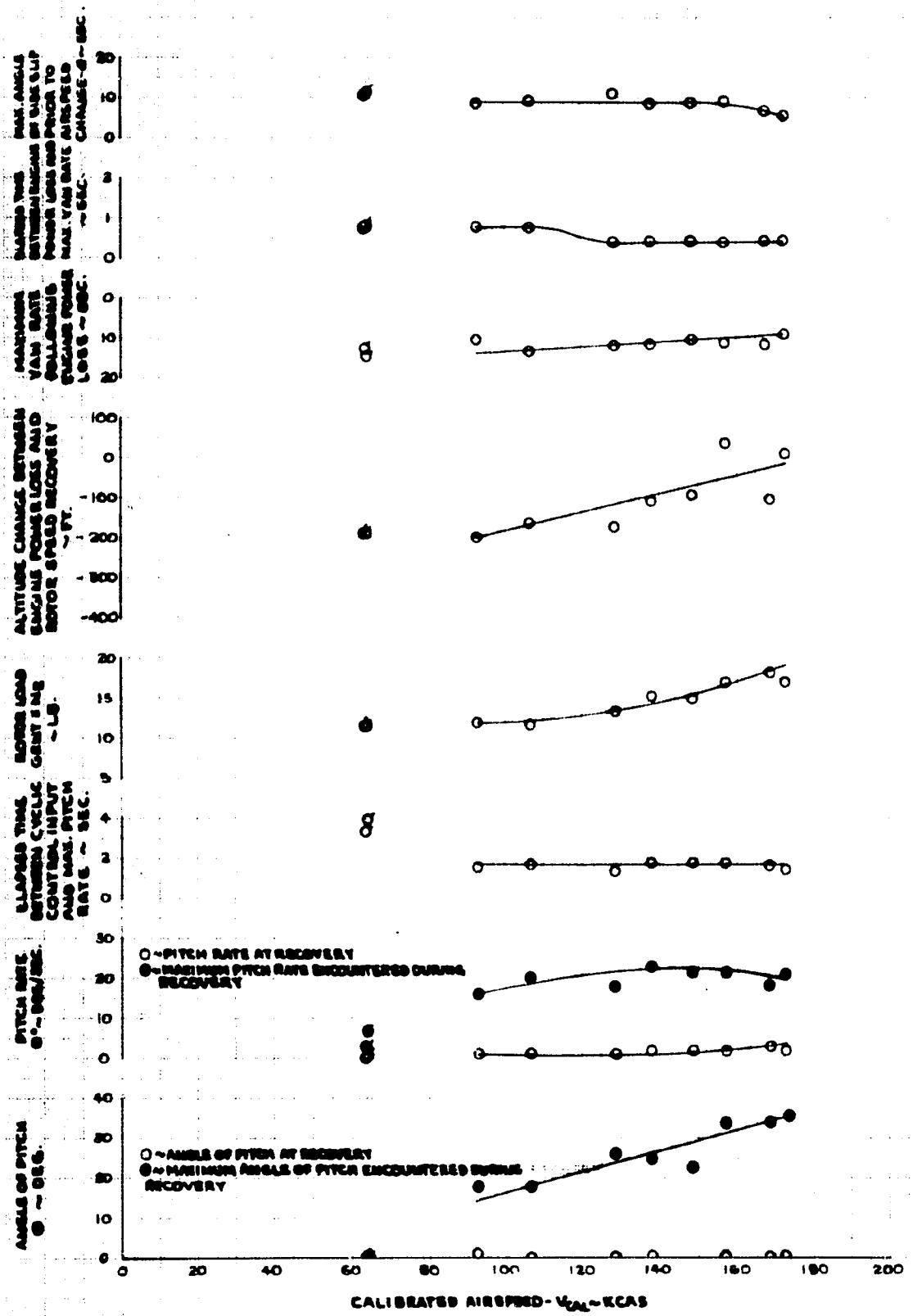


FIGURE NO. 297
SUMMARY OF AIRCRAFT REACTION AND RECOVERY FOLLOWING A SIMULATED ENGINE FAILURE

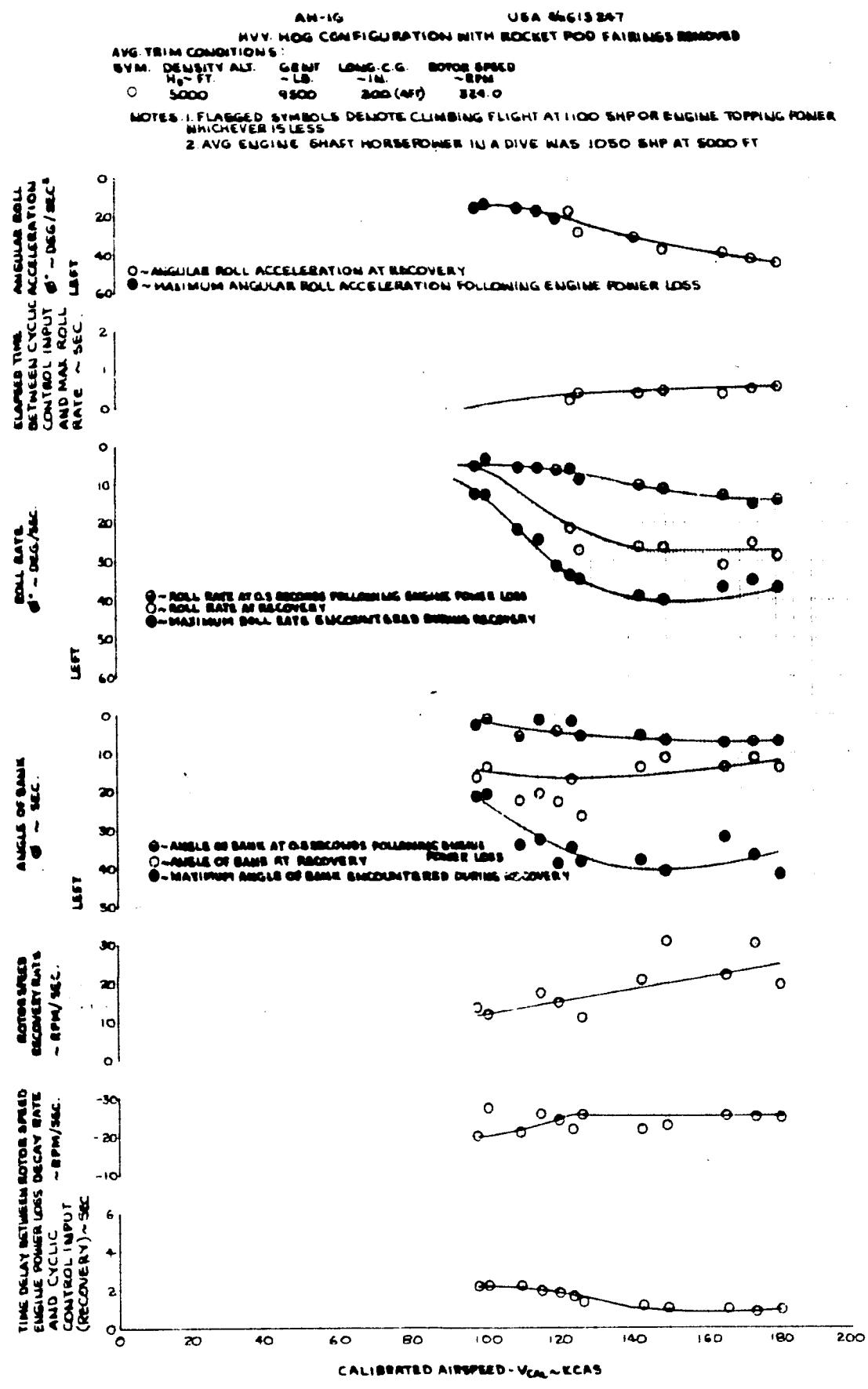


FIGURE NO. 297 (CONTINUED)

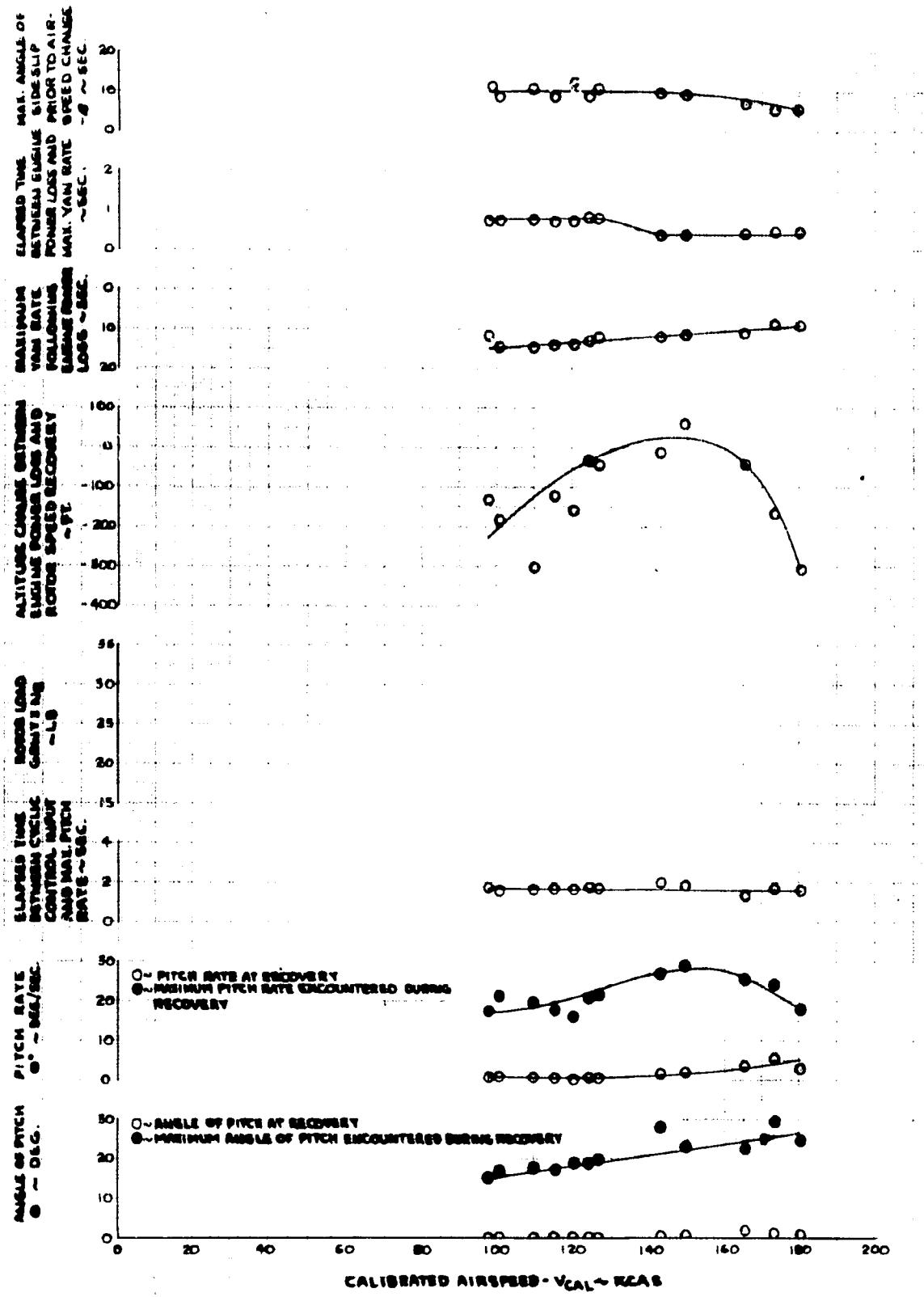
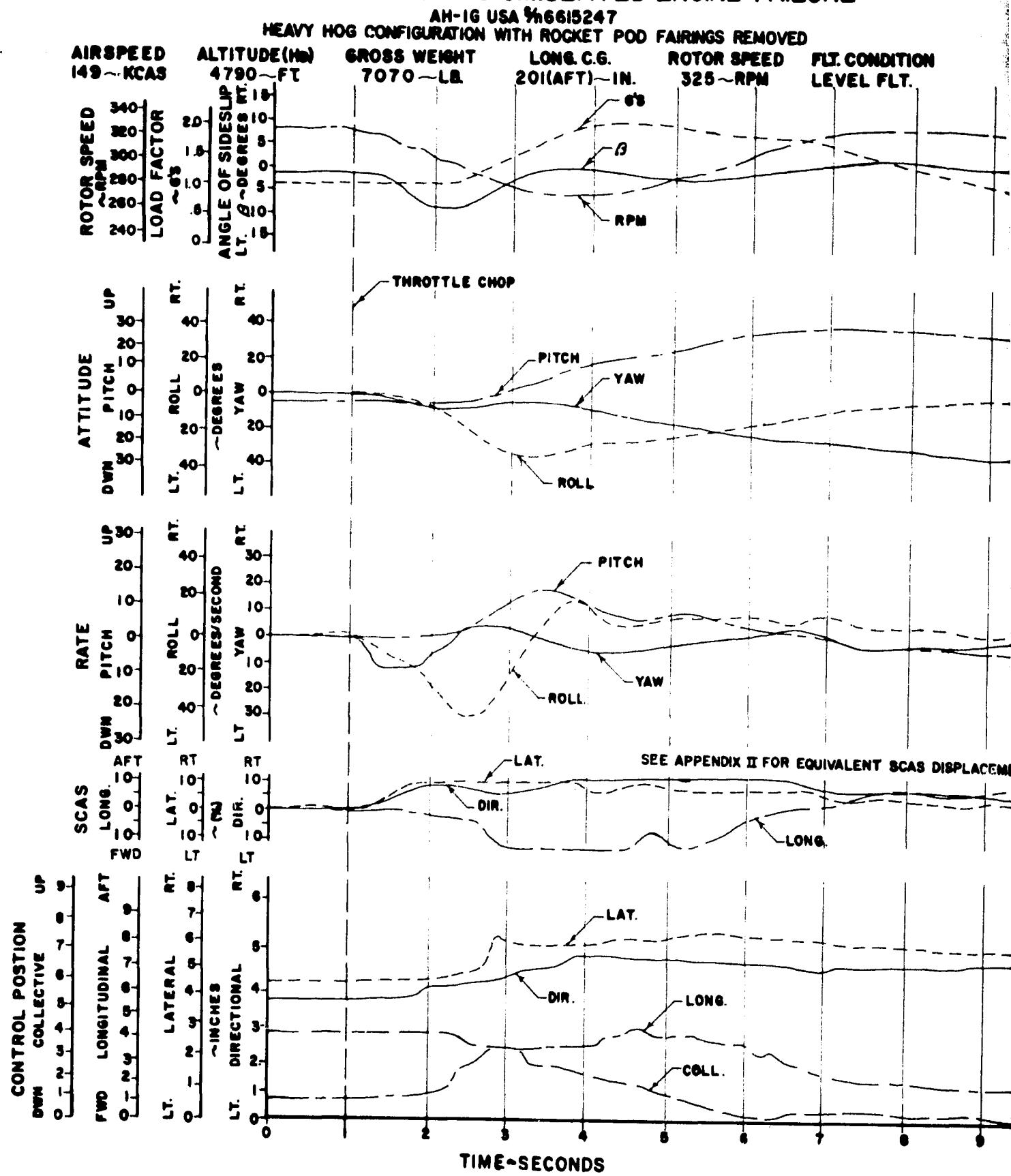


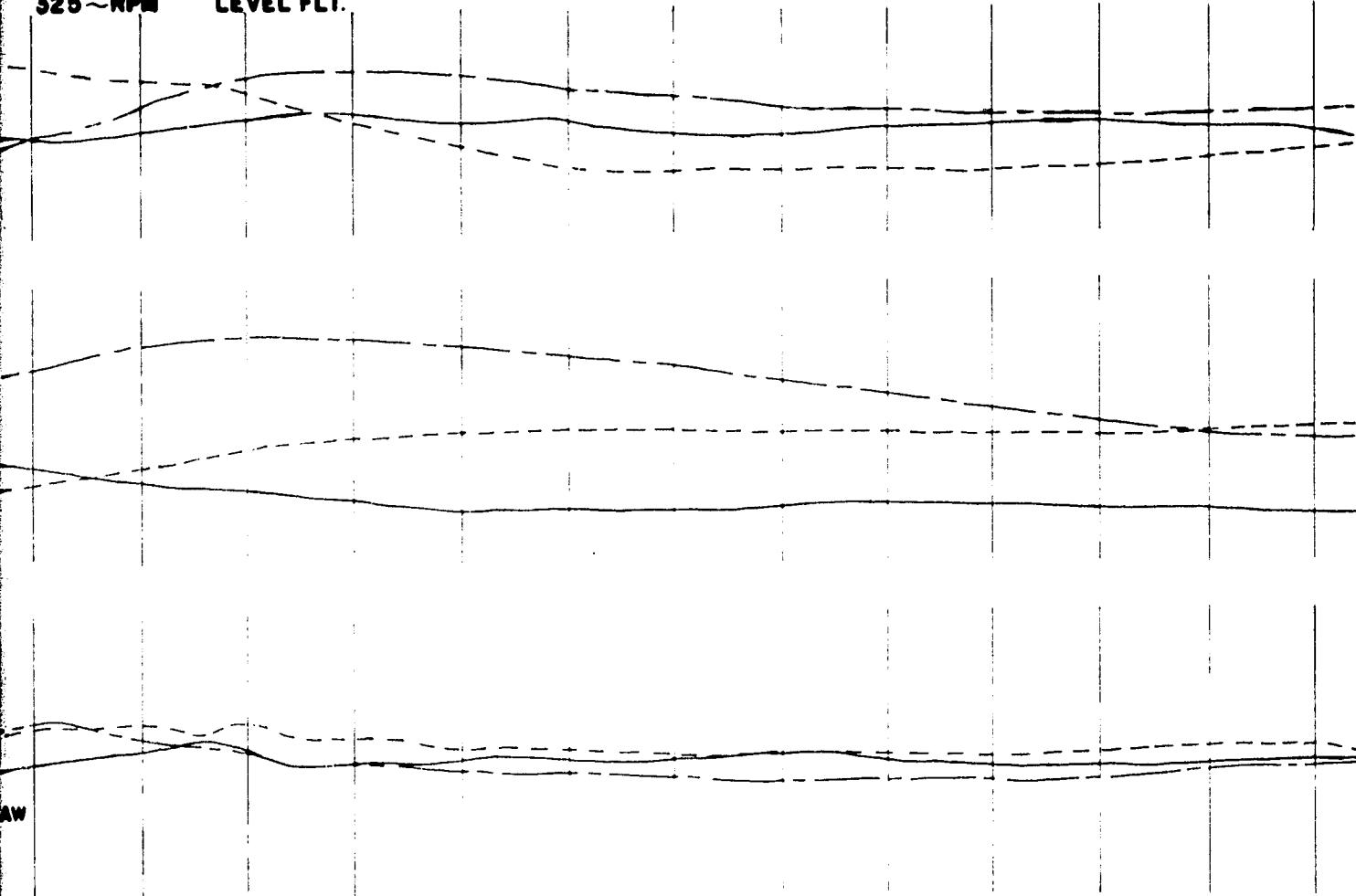
FIGURE NO. 298
AIRCRAFT REACTION TO SIMULATED ENGINE FAILURE



ENGINE FAILURE

FAIRINGS REMOVED

ROTOR SPEED FLI. CONDITION
325~RPM LEVEL FLT.



SEE APPENDIX II FOR EQUIVALENT SCAS DISPLACEMENT IN INCHES

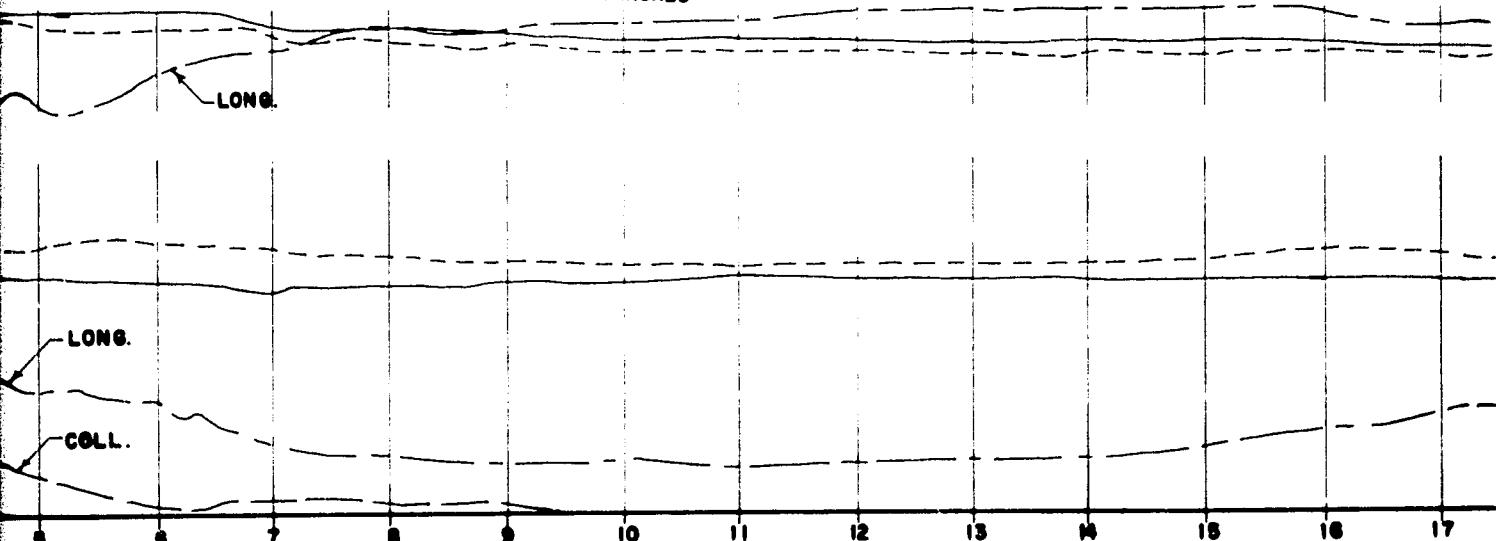
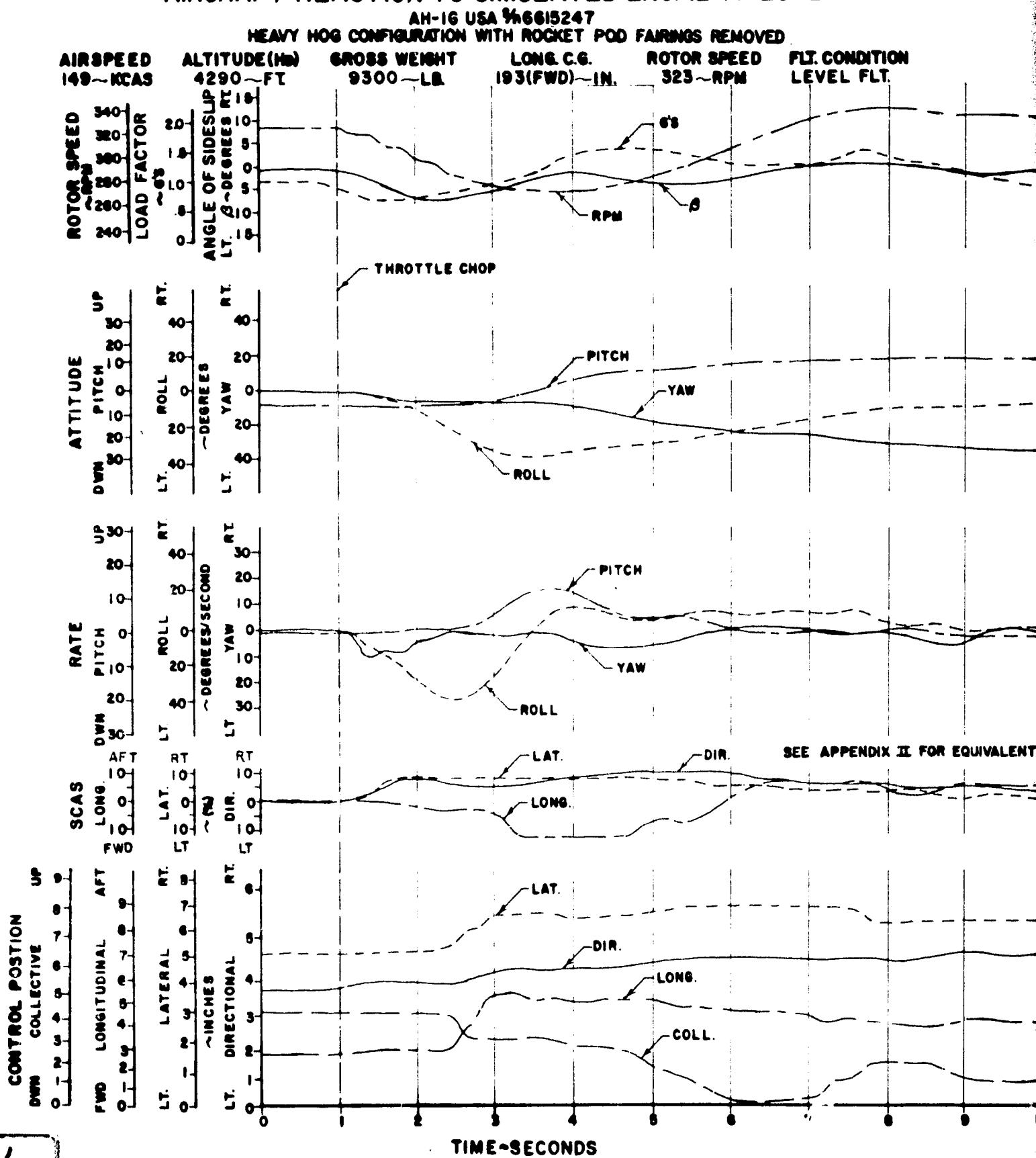
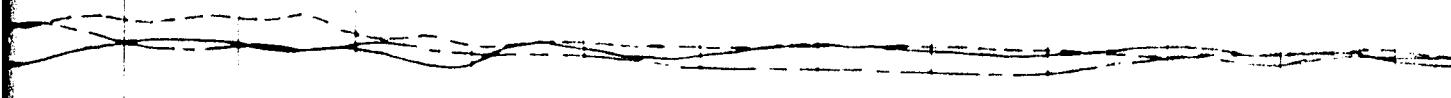
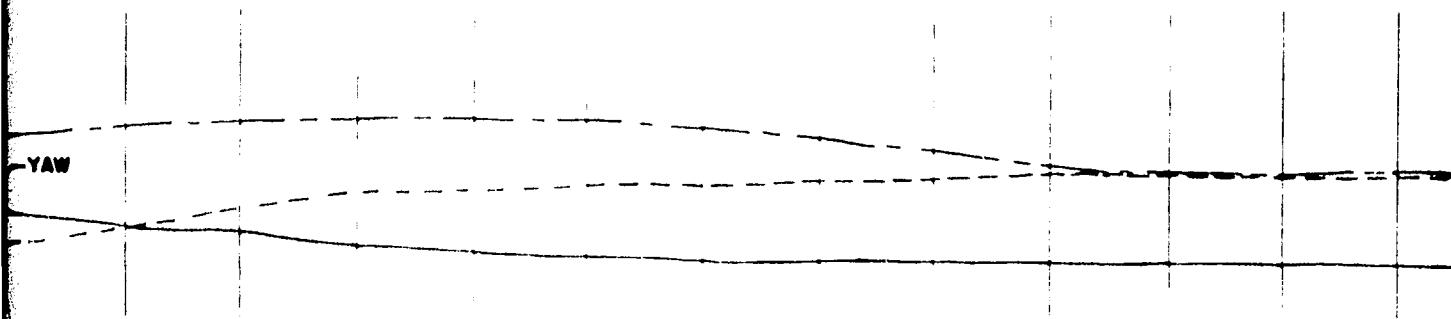
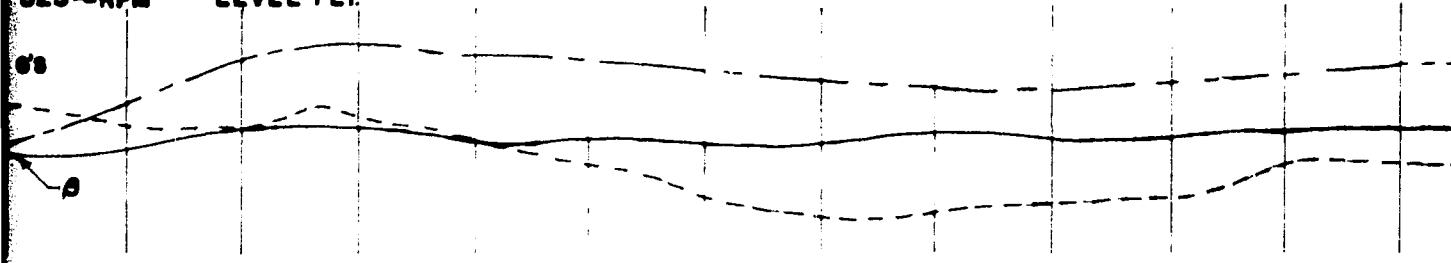


FIGURE NO. 299
AIRCRAFT REACTION TO SIMULATED ENGINE FAILURE



GINE FAILURE

WINGS REMOVED
OTOR SPEED PI. CONDITION
323~RPM LEVEL FLT.



DIR. SEE APPENDIX II FOR EQUIVALENT SCAS DISPLACEMENT IN INCHES

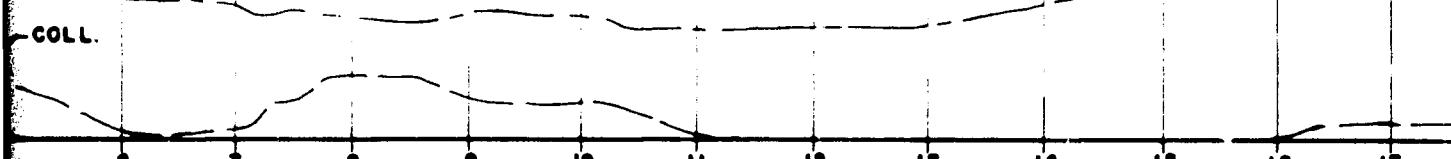
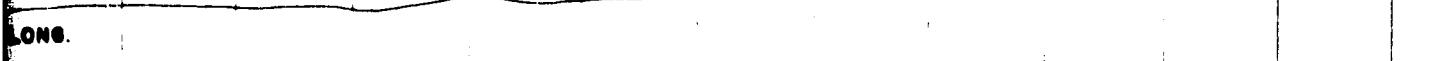
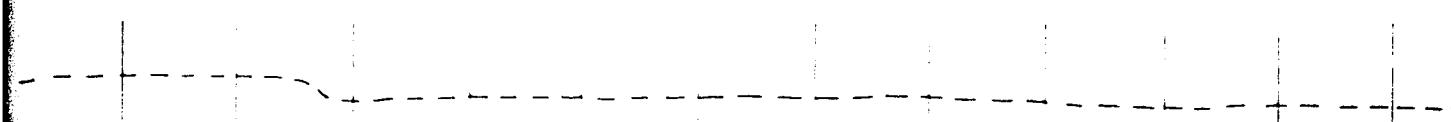
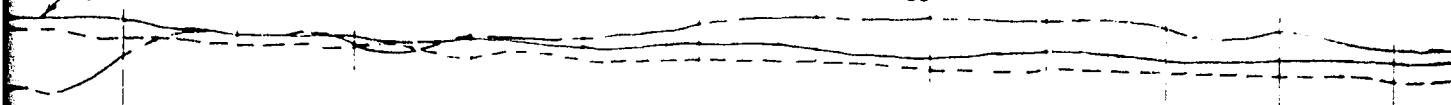
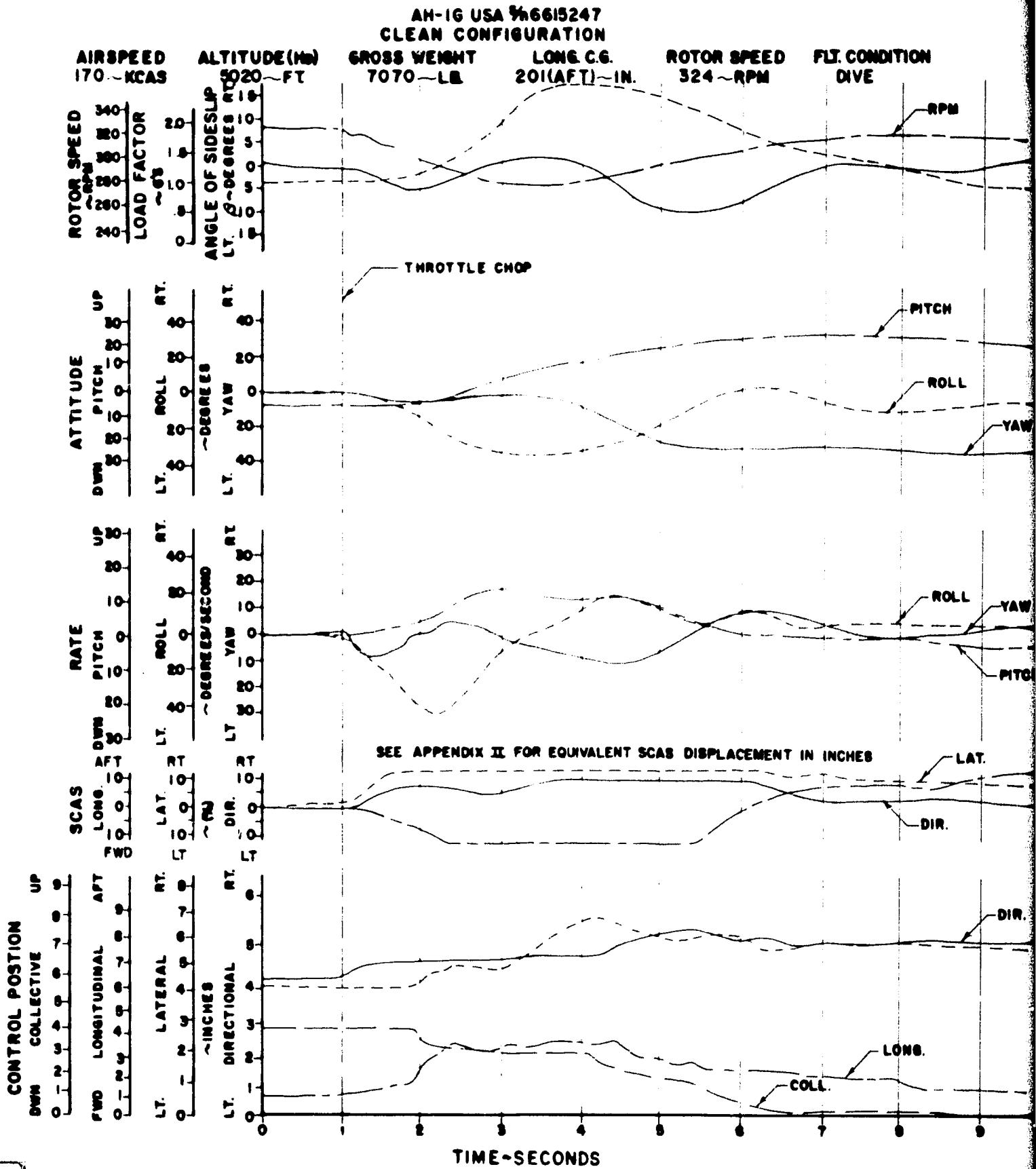


FIGURE NO. 300
AIRCRAFT REACTION TO SIMULATED ENGINE FAILURE



ENGINE FAILURE

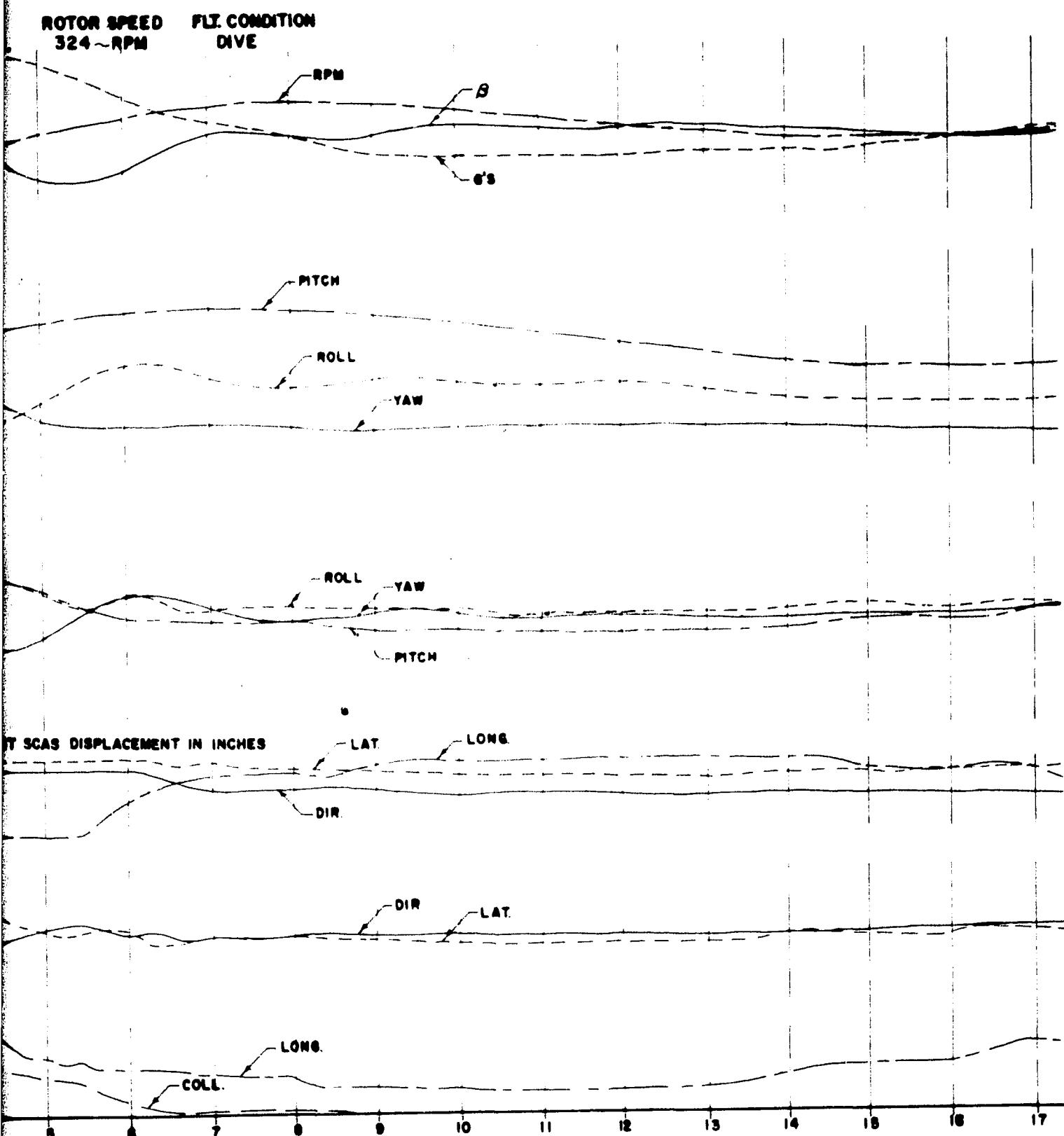
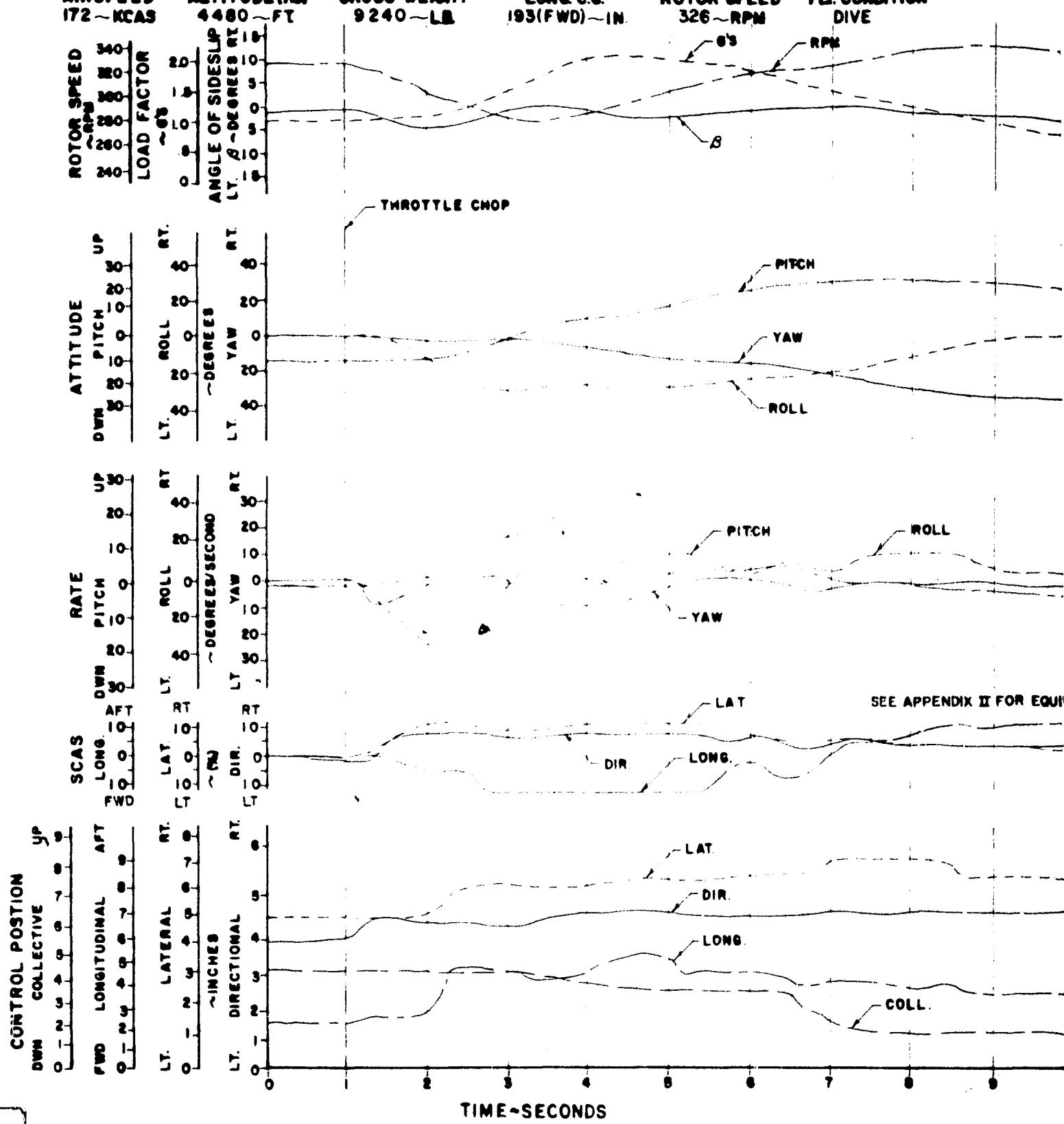


FIGURE NO. 301
AIRCRAFT REACTION TO SIMULATED ENGINE FAILURE

AH-1G USA #6615247

HEAVY HOG CONFIGURATION WITH ROCKET POD FAIRINGS REMOVED

AIRSPEED 172-KCAS ALTITUDE(AGL) 4480-FT GROSS WEIGHT 9240-LB LONG. C.G. 193(FWD)-IN. ROTOR SPEED 326-RPM FLT. CONDITION DIVE



D. 301
ATED ENGINE FAILURE

247

NET POD FAIRINGS REMOVED

L.C.G.
10)-IN. ROTOR SPEED FLG CONDITION
326-RPM DIVE

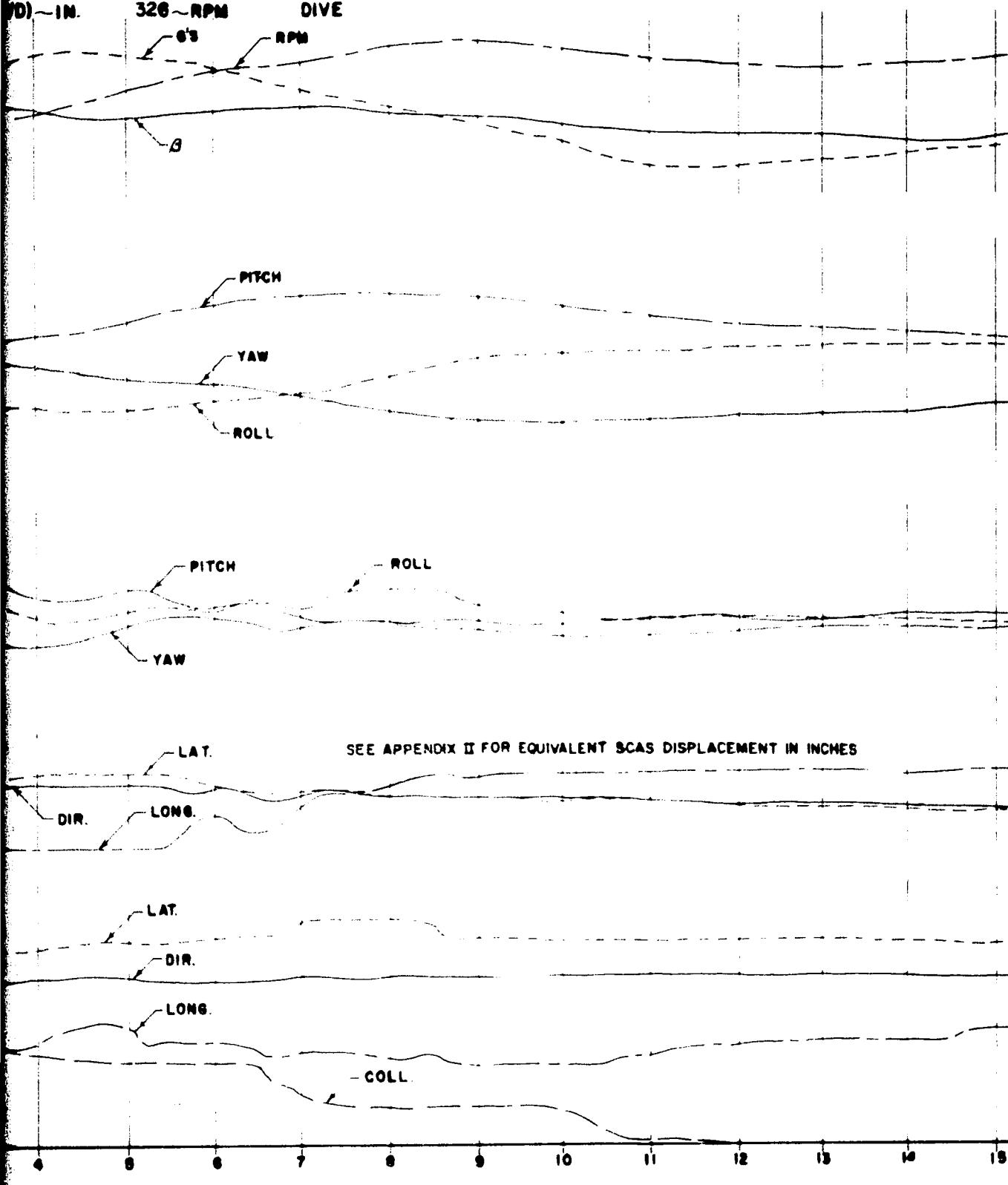


FIGURE NO. 302
AIRSPEED CALIBRATION
AH-1G TSB-L-15
STANDARD AIRSPEED SYSTEM

SYM	AIRCRAFT S/N	CONFIGURATION	GRAVITY ~ IN.	DEENSITY ~ FT.	ROTOR SPEED ~ RPM	LONG.C.G. ~ IN.	SOURCE OF DATA
O	615247	CLEAN	7810	5500	324	191.7(FW8) PHASE D TEST PROG.	
□	615246	BASIC	8280	5360	324	188.3(FW8) REF. 2 APP.I	
△	615248	BASIC	8170	4920	324	199.2(MID) REF. 4 APP.I	
◊	615243	OUTED ALTERNATE	8290	3100	324	199.1(AFT) REF. 5 APP.I	

CONNECTION TO BE MADE TO ROTOR



AUTOROTATIVE FLIGHT AT ROTOR
SPEED OF 324 RPM



CLIMBING FLIGHT AT MILITARY RATED POWER



LEVEL AND DIVING FLIGHT

NOTES: 1. SOLID SYMBOLS DENOTE AIRCRAFT DESCENDING
 2. OPEN SYMBOLS DENOTE AIRCRAFT IN LEVEL FLIGHT

INDICATED AIRSPEED - V_{IND} ~ KNOTS
 (CORRECTED FOR INSTRUMENT ERROR)

FIGURE NO 303
AIRSPEED CALIBRATION
AH-1G USA WNG15247
BOOM SYSTEM

SYM.	GROSS WEIGHT ~LBS.	CG STATION ~IN.	DENSITY ~FT.	ALTITUDE ~FT.	ROTOR SPEED ~RPM	CONFIGURATION
□	7265	1935	1020FT	1000FT	324	CLEAN
△	7176	1933	5300FT	5300FT	324	CLEAN
△	7200	1933	6000FT	6000FT	324	CLEAN

NOTES: 1. □ DATA COLLECTED USING THE GROUND SPEED METHOD.

2. △ DATA COLLECTED USING THE PACER AIRCRAFT METHOD.

3. △ DATA COLLECTED USING THE TRAILING BOMB METHOD.

4. SHADeD SYMBOLS DENOTE CLIMB AT LIMIT POWER

5. FLAGGED SYMBOLS DENOTE AUTOROTATION

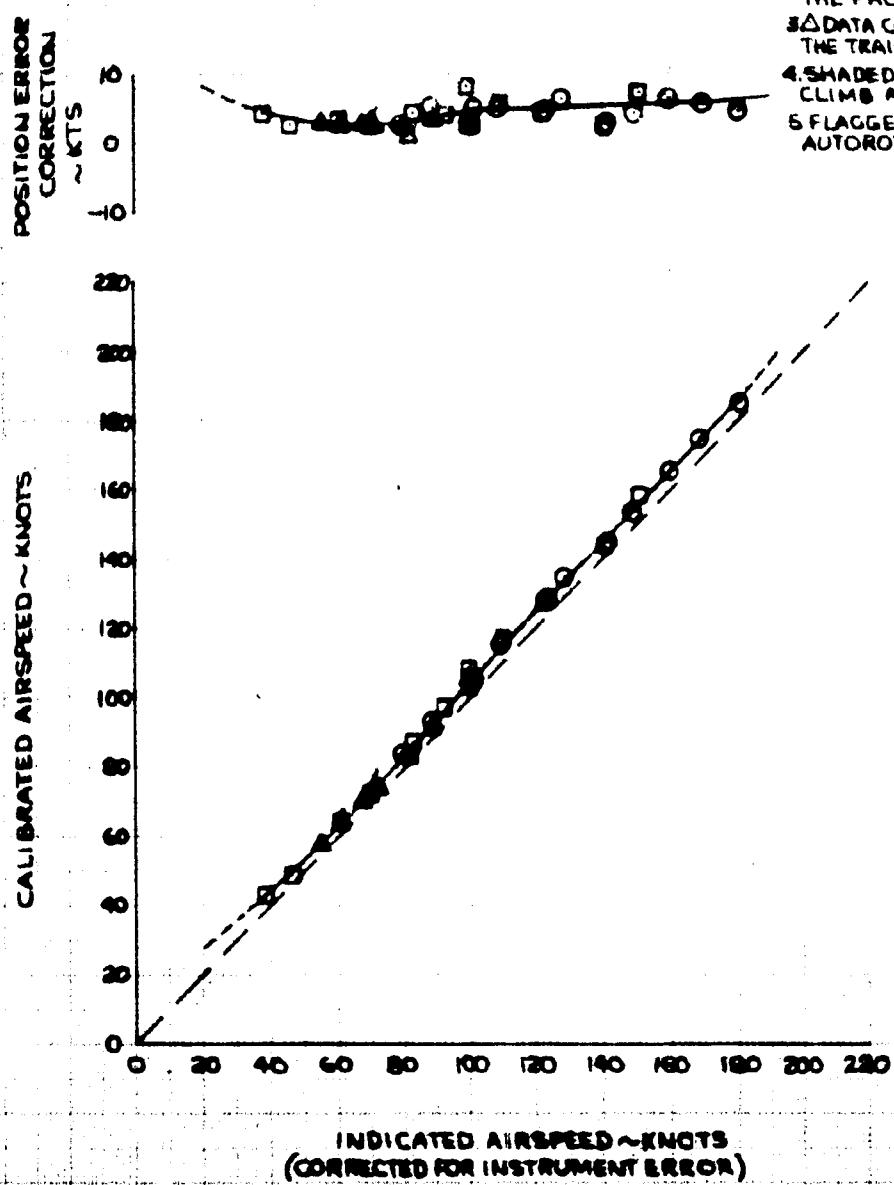


FIGURE NO. 304
AIR SPEED CALIBRATION
AH-1G USA SW 718673

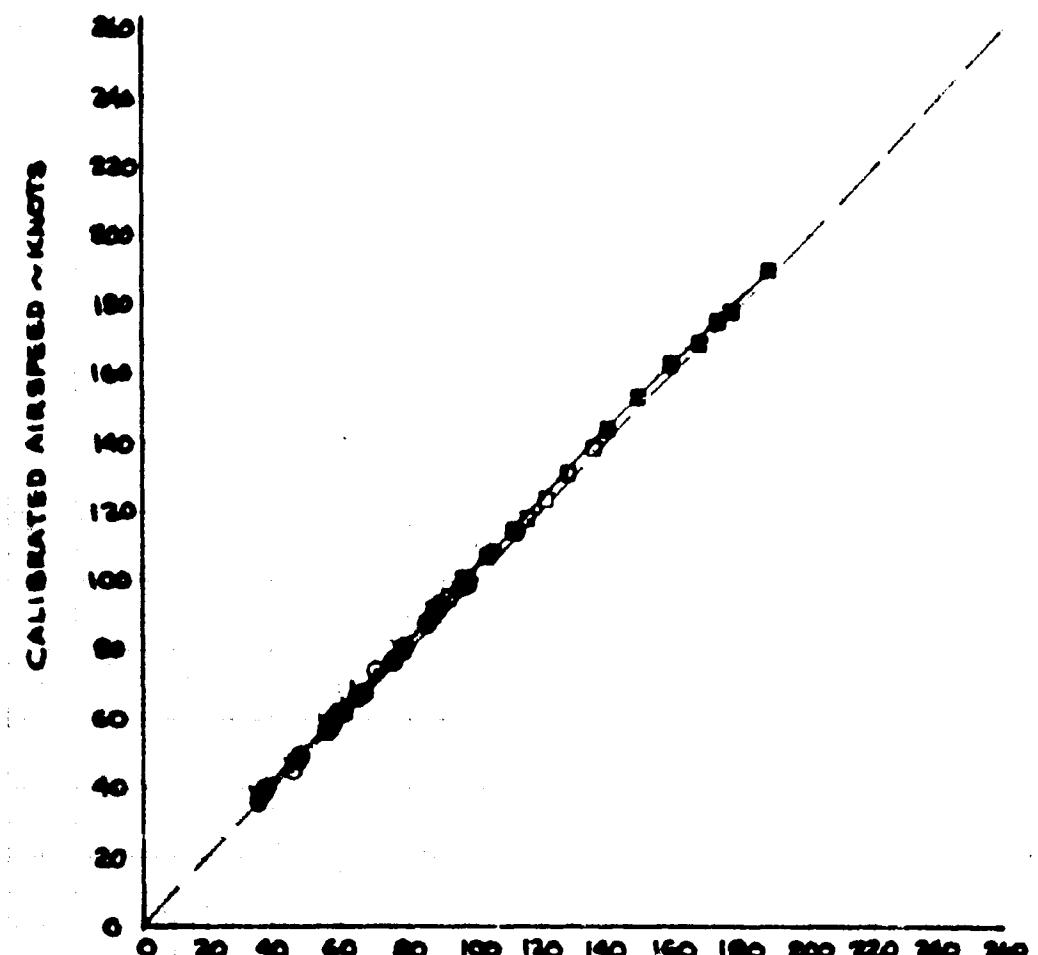
SYM.	GROSS WEIGHT	CG	STATION	DENSITY ALTITUDE	ROTOR SPEED	CONFIGURATION
○	~ LBS	~ IN.	~ FT.	~ RPM	3240	CLEAN
□	16000	1915	1650	7250	3240	CLEAN
■	16500	1914				

NOTE: OPEN SYMBOLS DENOTE LEVEL FLIGHT; SOLID SYMBOLS DENOTE AUTO-ROTATIONAL DESCENT; FLAGGED SYMBOLS DENOTE CLIMB; & CROSS SYMBOLS DENOTE DIVES.

○ TRAILING BOMB
 □ PACER

POSITION ERROR
 CORRECTION ± 10

CALIBRATED AIRSPEED ~ KNOTS



INDICATED AIRSPEED ~ KNOTS
 (CORRECTED FOR INSTRUMENT ERROR)

APPENDIX VIII. TEST CONDITIONS

Table 1. Static Trim Stability.

Rotor speed = 324 rpm				
Configuration	Flight Condition	Gross Weight (lb)	Density Altitude (ft)	Longitudinal Center of Gravity (in.)
Clean ¹	Level Flight and Dive	8665	3080	199.8 (aft)
Clean	Level Flight and Dive	8450	4540	200.8 (aft)
		8470	4980	191.4 (fwd)
		8420	14100	200.9 (aft)
	Climb	8170	5470	201.1 (aft)
		8240	5000	191.2 (fwd)
Outboard Alternate ²	Auto-rotation	8170	4950	201.1 (aft)
		8290	5000	191.2 (fwd)
	Level Flight and Dive	8500	3720	200.8 (aft)
Heavy scout ²		9430	6480	200.0 (aft)
		8410	13800	200.9 (aft)
Heavy hog ²	Level Flight and Dive	8370	4040	201.0 (aft)
		9555	3500	200.0 (aft)
	Level Flight and Dive	8530	5360	200.8 (aft)
		9580	4440	200.0 (aft)
		8620	4960	191.8 (fwd)
		8600	14760	200.7 (aft)
	Climb	9320	5470	200.2 (aft)
		8280	6000	201.0 (aft)
Auto-rotation	8350	5650	191.2 (fwd)	
	9290	4950	200.1 (aft)	
	8310	5920	201.0 (aft)	
	8340	5770	191.5 (fwd)	

¹Landing gear cross-tube fairings removed.

²Rocket pod fairings removed

Table 2. Static Longitudinal Collective Fixed Stability.

Rotor speed = 324 rpm				
Configuration	Gross Weight (lb)	Density Altitude (ft)	Longitudinal Center of Gravity (in.)	Trim Airspeeds
Clean ¹	8490	4630	199.7 (aft)	$0.8V_H, V_H, V_L$
Clean	8460	5310	200.8 (aft)	V for min R/D
Clean	8100	6750	191.0 (fwd)	V for R/C
Heavy hog ²	8100	5730	201.1 (aft)	V for min pwr rq'd
Heavy hog ²	8220	5940	191.1 (fwd)	$0.8V_H, V_H$ and V_L
Outboard Alternate ²	8190	4970	201.0 (aft)	V for min pwr rq'd
Heavy scout ²	8015	5320	201.0 (aft)	$0.8V_H, V_H,$ and V_L
Outboard Alternate ²	9010	5730	200.4 (aft)	
Heavy scout ²	9240	5320	200.2 (aft)	
Heavy hog ²	9140	5310	200.3 (aft)	
Clean	8150	15420	201.1 (aft)	V for min pwr rq'd
Outboard Alternate ²	8180	14650	201.7 (aft)	V_H
Heavy hog ²	8570	14640	200.7 (aft)	V_L

¹Landing gear cross-tube fairings removed.

²Rocket pod fairings removed.

Table 3. Static Lateral-Directional Stability.

Rotor speed = 324 rpm				
Configuration	Gross Weight (lb)	Density Altitude (ft)	Longitudinal Center of Gravity (in.)	Trim Airspeeds
Clean ¹	8770	3700	200.6 (aft)	$0.8V_H, V_H, V_L$
Clean	8290	5400	199.2 (aft)	V for min R/L
Outboard Alternate ²	8680	6080	200.7 (aft)	V for min R/D
Heavy scout ²	8330	6750	201.0 (aft)	V for min pwr rq'd $0.8V_H$
Heavy hog ²	8310	6080	200.9 (aft)	V_H and V_L
Heavy hog ²	8080	6070	191.1 (fwd)	
Heavy hog ²	9465	5170	200.0 (aft)	
Heavy hog ²	7745	4730	201.3 (aft)	
Heavy hog ²	8510	14640	200.8 (aft)	V for min pwr rq'd V_H and V_L

¹Landing gear cross-tube fairings removed.

²Rocket pod fairings removed.

Table 4. Longitudinal Dynamic Stability.

	Control Inputs Forward and Aft				
	Rotor speed = 324 rpm				
Configuration	Average Gross Weight (lb)	Average Density Altitude (ft)	Average Longitudinal Center of Gravity (in.)	Stability and Control Augmentation System	Trim Airspeeds
Clean	7660	5000	190.5 (fwd)	ON and OFF	V for min pwr rq'd
Clean	7540	4000	201 (aft)	ON and OFF	V for max R/C V for min R/D 0.8V _H , V _H and V _L
Heavy hog ¹	7740	4300	201 (aft)	ON and OFF	V for min pwr rq'd
Heavy hog ¹	9340	4400	200 (aft)	ON	0.8 V _H , V _H , V for max A/C
				OFF	V _H , V for max R/C
Heavy scout ¹	9310	4500	200 (aft)	ON	V for max R/C 0.8V _H , V _H , V _L
Heavy hog ¹	7730	15000	201 (aft)	ON and OFF	V for max R/L 0.8V _H , V _H

¹Rocket pod fairings removed.

Table 5. Lateral Dynamic Stability.

Inputs Right and Left					
Rotor speed = 324 rpm					
Configuration	Average Gross Weight (lb)	Average Density Altitude (ft)	Average Longitudinal Center of Gravity (in.)	Stability and Control Augmentation System	Trim Airspeeds
Clean	7300	4100	201 (aft)	ON and OFF	V for min pwr rq'd
Heavy hog ^{1,2}	8360	4500	195 (mid)	ON and OFF	V for max R/C V for min R/D $0.8V_H, V_H, V_L$
Heavy hog ^{1,3}	8680	3600	195 (mid)		
Heavy hog ^{1,2}	7620	3700	201 (aft)	ON and OFF	V for min pwr rq'd $0.8V_H, V_H, V_L$
Heavy hog ^{1,2}	7690	15060	201 (aft)	ON OFF	V for min pwr rq'd $1.8V_H, V_L$ $0.8V_H, V_H$
Heavy scout ^{1,3}	9000	5000	200 (aft)	ON	$0.8V_H, V_H$
Clean ⁴	8630	3700	199.5 (aft)	ON OFF	$0.8V_H, V_H, V_L, V_H, V_L$

¹Rocket pod fairings removed.

²Rocket pods empty.

³Rocket pods loaded with rockets.

⁴Landing gear cross-tube fairings removed.

Table 6. Directional Dynamic Stability.

Configuration	Control Inputs Left and Right		Rotor speed = 324 rpm	Stability and Control Augmentation System	Trim Airspeeds
	Average Gross Weight (lb)	Average Density Altitude (ft)			
Clean	7210	4200	201 (aft)	ON and OFF	V for min pwr rq'd V for max R/C V for min R/D $0.8V_H, V_H, V_L$
Heavy hog ^{1, 2}	7490	5000	201 (aft)	ON and OFF	V for max R/C V for max R/D $0.8V_H, V_L$
Heavy hog ^{1, 3}	9180	4600	200 (aft)	ON OFF	V for min pwr rq'd $0.8V_H, V_H, V_L$ V_H, V_L
Heavy hog ^{1, 2}	7620	15400	201 (aft)	ON OFF	V for min pwr rq'd $0.8V_H, V_H, V_H$
Clean ⁴	8650	3700	199.5 (aft)	ON OFF	$0.8V_H, V_H, V_L$ $0.8V_H, V_H$

¹Rocket pod fairings removed.²Rocket pods empty.³Rocket pods loaded with rockets.⁴Landing gear cross-tube fairings removed.

Table 7. Longitudinal Controllability in Forward Flight.

Control Inputs Forward and Aft				
Rotor speed = 324 rpm				
Configuration	Average Gross Weight (lb)	Average Density Altitude (ft)	Average Longitudinal Center of Gravity (in.)	Trim Airspeeds
Clean	6200	7610	190 (fwd)	$V_{min}, 0.8V_H, V_H, V_L$ $V_{min}, R/D, V_{max}, R/C$
Clean	5440	7780	201 (aft)	$V_{min}, 0.8V_H, V_H, V_L$ $V_{min}, R/D, V_{max}, R/C$
Heavy scout ¹	5000	9500	200 (aft)	$0.8V_H, V_H, V_L$ $V_{max}, R/C$
Heavy hog ¹	5060	7910	201 (aft)	$V_{min}, 0.8V_H, V_H, V_L$ $V_{min}, R/D, V_{max}, R/C$
Heavy hog ¹	5470	9490	200 (aft)	$V_{min}, 0.8V_H, V_H, V_L$ $V_{max}, R/C$
Heavy hog ¹	5530	7840	201 (aft)	$V_{min}, 0.8V_H, V_H$

¹Rocket pod fairings not installed.

Table 8. Lateral Controllability in Forward Flight.

Configuration	Control Inputs Right and Left			
	Average Gross Weight (lb)	Average Density Altitude (ft)	Average Longitudinal Center of Gravity (in.)	Trim Airspeeds
Clean	4270	7590	201 (aft)	V_{min} , $0.8V_H$, V_H , V_L V_{min} , R/D, V_{max} , R/C
Clean ¹	4070	7390	199.5 (aft)	$0.8V_H$, V_H , V_L
Heavy scout ²	5000	9500	200 (aft)	$0.8V_H$, V_H , V_L , V_{max} R/C
Heavy hog ^{2,3}	5180	8580	195 (mid)	V_{min} , $0.8V_H$, V_H , V_L V_{min} , R/D, V_{max} R/C
Heavy hog ^{2,4}	4030	8830	195 (mid)	V_{min} , $0.8V_H$, V_H , V_L V_{min} , R/D, V_{max} , R/C
Heavy hog ²	5270	9390	200 (aft)	V_{min} , $0.8V_H$, V_H , V_L V_{max} , R/C
Heavy hog ²	5290	7800	201 (aft)	V_{min} , $0.8V_H$, V_H , V_L V_{max} , R/C, V_{min} , R/D
Heavy hog ²	16150	7730	201 (aft)	V_{min} , $0.8V_H$, V_H , V_L V_{max} , R/C, V_{min} , R/D

¹Landing gear cross-tube fairings removed.

²Rocket pod fairings not installed.

³All rocket pods empty.

⁴All rocket pods fully loaded (1634 lb).

Table 9. Directional Controllability in Forward Flight.

Control Inputs Right and Left				
Rotor speed = 324 rpm				
Configuration	Average Gross Weight (lb)	Average Density Altitude (ft)	Average Longitudinal Center of Gravity (in.)	Trim Airspeeds
Clean	7480	5900	201 (aft)	$V_{min}, 0.8V_H, V_H, V_L$ $V_{min} R/D, V_{max} R/C$
Clean ¹	8680	4330	199.5 (aft)	$0.8V_H, V_H, V_L$
Heavy hog ²	9280	6060	200 (aft)	$V_{min}, 0.8V_H, V_H, V_L$ $V_{min} R/D, V_{max} R/C$
Heavy hog ²	7640	4650	201 (aft)	$V_{min}, 0.8V_H, V_H, V_L$ $V_{min} R/D, V_{max} R/C$
Heavy hog ²	7640	16460	201 (aft)	$V_{min}, 0.8V_H, V_H$

¹Landing gear cross-tube fairings removed.

²Rocket pod fairings not installed.

Table 10. Longitudinal Controllability in a Hover.

Control Inputs Forward and Aft				
Configuration	Average Gross Weight (lb)	Average Density Altitude (ft)	Average Longitudinal Center of Gravity (in.)	Rotor Speed (rpm)
Clean	7670	610	196 (mid)	324
	7590	4460	195 (mid)	323
	8635	Sea Level	195.5 (mid)	322
	7370	8550	196 (mid)	324
	8560	4850	195.5 (mid)	324.5
	7750	10320	200.0 (aft)	324
Heavy hog	7590	730	201 (aft)	324
	9000	750	200 (aft)	324

Table 11. Lateral Controllability in a Hover.

Control Inputs Right and Left				
Configuration	Average Gross Weight (lb)	Average Density Altitude (ft)	Average Longitudinal Center of Gravity (in.)	Rotor Speed (rpm)
Clean	7400	550	195.5 (mid)	324
	7420	4460	196 (mid)	324.5
	8550	7420	195.5 (mid)	324
	8480	4850	195.5 (mid)	324.5
	7660	10320	196.0 (mid)	324
Heavy hog	7420	850	201 (aft)	324
	8600	-160	196.5 (mid)	322.5
	8600	480	198.0 (aft)	323
	8780	030	200.0 (aft)	322.5
	8980	770	200.0 (aft)	324

Table 12. Directional Controllability in a Hover

Control Inputs Right and Left				
Configuration	Average Gross Weight (lb)	Average Density Altitude (ft)	Average Longitudinal Center of Gravity (in.)	Rotor Speed (rpm)
Clean	7170	560	195 (mid)	324
	7160	550	195 (mid)	313.5
	6980	570	195.5 (mid)	303.5
	7280	4580	195.5 (mid)	323
	7220	4580	195.5 (mid)	314.5
	7330	8550	195.5 (mid)	324
	8630	4790	195.5 (mid)	324.5
	7270	8550	195.0 (mid)	314.5
	8400	4850	195.5 (mid)	314.5
	7560	10320	195.5 (mid)	324
Heavy hog	7490	10320	195.5 (mid)	313.5
	7260	980	201 (aft)	324
	8460	-480	195.5 (mid)	323
	8600	060	200 (aft)	323
	8400	-490	196 (mid)	313.5
	8970	450	200.5 (aft)	324
	8770	Sea Level	200 (aft)	313.5

Table 13. Aircraft Reaction to Engine Failure.

Configuration	Gross Weight (lb)	Center of Gravity (in.)	Density Altitude (ft)
Clean	8500	Aft	5000, 10,000
Clean	8500	Fwd	5000, 10,000
Heavy hog	9500	Aft	5000
Heavy hog	9500	Fwd	5000
Clean ¹	7500	Aft	5000

¹Tests conducted with landing gear cross-tube fairings installed and with them removed.

APPENDIX IX. SYMBOLS AND ABBREVIATIONS

<u>Abbreviation</u>	<u>Definition</u>	<u>Unit</u>
ALT	Altitude	foot
AVG	Average	--
COEFF	Coefficient	--
CG, cg	Center of gravity	--
COLL	Collective	--
COND	Condition	--
CONF	Configuration	--
CPS, cps	Cycles per second	--
DEG, deg	Degrees	degree
DESCRIPT	Description	--
DIR	Directional	--
DWN	Down	--
FLT	Flight	--
FT	Feet	foot
FS	Fuselage station	inch
FWD, fwd	Forward	--
GRWT, grwt	Gross weight	pound
HQRS	Handling qualities rating scale	--
HP	Horsepower	--
IFR	Instrument flight rules	--
IGE	In ground effect	--

<u>Abbreviation</u>	<u>Definition</u>	<u>Unit</u>
in.	Inch, inches	inch
KCAS	Knots calibrated airspeed	knot
KIAS	Knots indicated airspeed	knot
KTAS	Knots true airspeed	knot
LB, lb	Pound, pounds	pound
LAT	Lateral	--
LEU	Leading edge Up	--
LN	Natural log	--
LT	Left	--
LONG.	Longitudinal	--
MAX, max	Maximum	--
MIN, min	Minimum	--
ND	Nose down	--
NU	Nose up	--
NO., no.	Number	--
PSI, psi	Pound(s) per square inch	lb/in. ²
REF, ref	Reference, referred	--
RPM, rpm	Revolution(s) per minute	rpm
RT	Right	--
SCAS	Stability and control augmentation system	--
SEC, sec	Second	--
SHP, shp	Shaft horsepower	--
SL	Sea level	--

<u>Abbreviation</u>	<u>Definition</u>	<u>Unit</u>
S/N	Serial number	--
STD, std	Standard	--
SYM	Symbol	--

<u>Symbol</u>	<u>Definition</u>	<u>Unit</u>
A	Rotor disc area	ft ²
C _T	Thrust coefficient	--
F _{LAT}	Lateral control force	pound
F _{LONG}	Longitudinal control force	pound
F _{DIR}	Directional control force	pound
H _D	Density altitude	foot
H _P	Pressure altitude	foot
i _t	Horizontal stabilizer position	degree
R	Rotor radius	foot
R/C	Rate of climb	ft/min
R/D	Rate of descent	ft/min
V _{cal}	Calibrated airspeed	knot
V _H	Maximum airspeed for level flight	knot
V _L	Limit airspeed	knot
%	Percent	--
α	Angle of attack	degree
β	Angle of sideslip	degree
δ_{COLL}	Collective control position	inch

<u>Symbol</u>	<u>Definition</u>	<u>Unit</u>
δ_{DIR}	Directional control position	inch
δ_{LAT}	Lateral cyclic control position	inch
δ_{LONG}	Longitudinal cyclic control position	inch
ζ	Damping ratio	--
θ	Angle of pitch	degree
$\dot{\theta}$	Pitch rate	deg/sec
$\ddot{\theta}$	Pitch acceleration	deg/sec ²
ρ	Air mass density	slug/ft ³
ϕ	Angle of bank	degree
$\dot{\phi}$	Roll rate	deg/sec
$\ddot{\phi}$	Roll acceleration	deg/sec ²
Ω	Rotor rotational frequency	rad/sec
ψ	Yaw attitude	degree
$\dot{\psi}$	Yaw rate	deg/sec
$\ddot{\psi}$	Yaw acceleration	deg/sec ²
ω_d	Damped natural frequency	cycle/sec
ω_n	Undamped natural frequency	cycle/sec
P	Period of oscillation	second
X	Amplitude	inch
m	Number of half cycles	--
$<$	Less than	--
$>$	Greater than	--

<u>Subscript</u>	<u>Definition</u>
a	Ambient
std, s	Standard
t	Test

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13. ABSTRACT The Phase D, Part 1 airworthiness and qualification handling qualities tests of the AH-1G helicopter were conducted at Edwards Air Force Base, California, and auxiliary test sites during the period 13 June 1968 through 29 July 1969. Handling qualities were quantitatively evaluated to determine model specification compliance and to obtain mission suitability information for inclusion in technical manuals and other publications. The AH-1G met all contractual requirements of MIL-H-8501A except for paragraphs 3.2.4 (cyclic force gradients), 3.2.7 (cyclic breakout forces), 3.5.4.1 (takeoff and landing in winds), 3.5.5 (autorotational entry) and 3.5.5.1 (aircraft reaction to engine failure). Tests were not conducted to verify compliance with paragraphs 3.5.4.3 (autorotational landings), 3.5.4.4 (autorotational landings) and 3.5.4.5 (autorotational landing with flotation gear) of MIL-H-8501A. By contractual agreement, the handling qualities requirements presented in paragraphs 3.3 (directional and lateral handling qualities) and 3.6 (handling qualities during instrument flight) of MIL-H-8501A were not applicable. The handling qualities of the AH-1G are acceptable throughout the flight envelope except for the four deficiencies for which correction is mandatory for mission accomplishment: excessive cyclic control breakout forces; inadequate directional control; inability to achieve maximum tail rotor blade angle (19 deg) when full left directional control is applied for all conditions with the present directional control/yaw SCAS geometry; and excessive tail rotor horsepower required for hovering and translational flight. In addition, there were five shortcomings for which corrective action is desirable.		

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