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RAY TRACING SYNTHESIS OF HF RADAR SIGNATURES FROM GAUSSIAN PLASMA CLOUDS

Raytheon Company, Sudbury Labs

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## RAY TRACING SYNTHESIS OF HF RADAR SIGNATURES FROM GAUSSIAN PLASMA CLOUDS

Pendyala B. Rao E. Michael Allen George D. Thome

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# PUBLICATION REVIEW

This technical report has been reviewed and is approved.

Micen O RADC Project Engineer

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#### ABSTRACT

The electron density distribution through ionized clouds produced by Barium releases is often taken to be Gaussian for want of direct evidence to the contrary. Multiple frequency hf radar observations (scattering cross-section and Doppler shift versus time) have been made during several releases for the primary purpose of measuring peak electron density as a function of time. Observations of this sort cannot be used to compute the electron density distribution directly because the cloud elongates along the Earth's magnetic field and thus the distribution is not one dimensional. These observations can however be used to test assumed distributions by ray tracing through a model cloud and comparing the predicted signatures with the observations. A detailed comparison of this nature has been made using a time-dependent Gaussian cloud and the ITSA three-dimensional ray tracing program. The ray tracing results have been compared also to that of a hard expanding ellipsoid model to study the effects of the ionization lying below the reflection level. Significant differences have been noted between the observed and the synthesized signatures from the ray tracing. The differences are of the nature to suggest that the electron density variation outward from the center of the cloud is more gradual than that in the adopted Gaussian model. Defocussing due to the underlying ionization is found to reduce the scattering cross-section by a factor that increases with time from 3 at the peak cross-section to 30 just prior to signal drop-out.

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### SECTION 1. INTRODUCTION

The generation of artificial ion clouds in the upper atmosphere has proven to be a useful technique for studying plasma interaction with the electric and magnetic field environment of the Earth's ionosphere and magnetosphere. The technique, originally developed at the Max Planck Institute in Germany, employs rocket releases of Barium vapor which, on being exposed to the solar ultraviolet radiation, becomes partially ionized (Haerendel and Lust, 1969). The ionized and the non-ionized components of the Barium vapor form into two distinct clouds, an ion and a neutral cloud. A number of radio and optical methods have been devised to study the following characteristics of the clouds:

- a. Size, shape, particle number densities and their distributions as a function of time
- b. Diffusion and drift motions including the dynamics associated with the gross deformation and the striated structure exhibited by the ion cloud
- c. Radio wave scattering in the hf and vhf regimes.

The knowledge of the electron (ion) density distribution in the ionized cloud is of fundamental importance for a proper understanding of the ion cloud interaction with the ionospheric environment. There have not been as yet any reliable experimental measurements that would directly provide this information. Some evidence has been gathered, however, which tends to suggest a Gaussian profile for the distribution. First, the Gaussian model has stemmed out of the theoretical work of Holway (1965) which is based on the ambipolar diffusion of the cloud in the geomagnetic field neglecting the presence of an external electric field. In a recent study by Simon (1970), it

was shown that taking the electric field into account would still lead to a Gaussian distribution, but in a transformed drift frame of reference. The experimental evidence that seems to favor the Gaussian model is derived from the optical intensity measurements of the resonant scattering and the Thomson scatter radar observations. The deductions from optical measurements are made by microdensitometer scans of the filter photographs of the cloud. The variations of the line integral of the ions along selected scans are found to fit well to Gaussian distributions. It does not, however, follow immediately that the ion density distribution itself is Gaussian. Thomson scatter radar observations provide electron density profiles along the antenna beam direction with a spatial resolution defined by the pulse length and temporal resolution determined by the integration time. The electron density profiles measured by this technique using the AIO radar during one of the SECEDE I tests suggest that the distribution is at least approximately Gaussian. The measurements with a resolution of 2 km are rather coarse, however, with respect to the cloud dimensions and are subject to the uncertainties involved due to possible energy leakage through the sidelobes. Further evidence in support of the Gaussian distribution has come from an analysis by Oetzel and Chang (1969) who found that the observed Faraday fading and the history of the center point electron density derived from hf measurements are consistent to a greater extent with the Gaussian model than with other distributions.

In spite of all the positive evidence in support of the Gaussian model, the true distribution is still a matter of speculation because of an unexpected behavior of the hf Doppler. It is expected that an expanding Gaussian cloud will lead to a Doppler trace that goes negative shortly before the signal dropout on a given operating frequency. The observed Doppler records, however, exhibit no such negative tail.

For this to occur, two possibilities suggest themselves immediately: one, of course, is that the distribution is unlike Gaussian, and the other, which seems more probable, is that the signal is too weak to be detected during the contracting phase of a given plasma frequency contour, thus washing off the expected negative tail.

The problem taken up in this report is to investigate the two possibilities by synthesizing the radar signatures both in Doppler and signal strength by means of a three dimensional ray tracing program and Gaussian modeled ion clouds. The results will show to what extent the sensitivity of the receiving system limits the Doppler trace, and how accurately a Gaussian model could simulate an ion cloud. The 3-D ray tracing program used here was developed at ESSA by Dr. R.M. Jones and has proven to be quite versatile in its scope. A summary description of this program is given in Section 2. Section 3 deals with the ion cloud modeling in the geomagnetic dipole coordinate system as desired by the ray tracing program. The results of the ray tracing are presented in Section 4 along with those derived for the case of an expanding hard ellipsoid model. Experimental results are described in Section 5. Section 6 is devoted to a comparison between the theory and observations with the summary and conclusions given in Section 7.

## SECTION 2. THREE DIMENSIONAL RAY TRACING PROGRAM

## 2.1 INTRODUCTION

A versatile computer program for tracing rays through a medium whose index of refraction varies in three dimensions has been developed by R. M. Jones at ESSA Laboratories in Boulder. The program was intended for ray tracing applications in the ionosphere and could successfully simulate a variety of radio propagation experiments. It was written in FORTRAN language and was made available on request to prospective users in two versions; one to run on a CDC 3600 and the other on an IBM 7090. A detailed description of the program along with instructions that include annotated listings of all routines, deck set-ups and the form of input and output has been published in the ESSA reports by Jones (1966, 1968). The efficiency of the program in computing the rays has been evaluated by Lemanski (1968).

## 2.2 GOVERNING EQUATIONS

The equations that govern ray paths in a three dimensional anisotropic medium have been derived using the method of Hamilton by Haselgrove (1954). The equations were expressed in a form suitable for integration by standard numerical methods using a digital computer. The Jones program calculates the ray paths by integrating the following six differential equations which are a slight modification to those described by Haselgrove.

$$\frac{dr}{dt} = \left[ V_r - \text{Real} \left( n \frac{\partial n}{\partial V_r} \right) \right] / \text{Real} \left( n n' \right)$$
(2-1)

$$\frac{d\theta}{dt} = \left[ V_{\theta} - \text{Real} \left( n \frac{\partial n}{\partial V_{\theta}} \right) \right] / r \text{ Real} \left( n n' \right)$$
(2-2)

$$\frac{d\phi}{dt} = V_{\phi} - \text{Real} \left(n \frac{\partial n}{\partial V_{\phi}}\right) / r \sin \theta \text{ Real} (n n') \qquad (2-3)$$

$$\frac{dV_{r}}{dt} = \frac{\text{Real } (n \frac{\partial n}{\partial r})}{\text{Real } (n n')} + V_{\theta} \frac{d\theta}{dt} + V_{\phi} \sin \theta \frac{d\phi}{dt}$$
(2-4)

2

$$\frac{dV_{\theta}}{dt} = \frac{1}{r} \left[ \frac{\text{Real} (n \frac{\partial n}{\partial \theta})}{\text{Real} (n n')} - V_{\theta} \frac{dr}{dt} + rV_{\phi} \cos \theta \frac{d\phi}{dt} \right]$$
(2-5)

$$\frac{dV_{\phi}}{dt} = \frac{1}{r \sin \theta} \left[ \frac{\text{Real } (n \frac{\partial n}{\partial \phi})}{\text{Real } (n n')} - V_{\phi} \sin \theta \frac{dr}{dt} - r V_{\phi} \cos \theta \frac{d\theta}{dt} \right]$$
(2-6)

The variables r,  $\theta$ , and  $\phi$  are the spherical polar coordinates of a point on the ray path;  $V_r$ ,  $V_{\theta}$ , and  $V_{\phi}$  are the components of the wave normal in the r,  $\theta$ , and  $\phi$  directions, normalized so that

$$v_r^2 + v_{\theta}^2 + v_{\phi}^2 = \text{Real} (n^2)$$
 (2-7)

where n and n' are the complex phase and group refractive indices which are based on Appleton-Hartree formula. The independent variable t is group path length in these equations whereas it is phase path length in Haselgrove equations. This change of independent variable has the advantage of speeding up the program by automatically decreasing the step length in real path near the reflection height. In addition to the six basic equations necessary to calculate the ray path, the program integrates the following to give the phase path, the absorption, and the Doppler shift, respectively.

$$\frac{dP}{dt} = \frac{\text{Real} (n^2)}{\text{Real} (n n')}$$
(2-8)

$$\frac{dA}{dt} = \frac{10}{\text{Log}_{e} 10} \frac{2\pi f}{C} \frac{|\text{imag} (n^2)|}{\text{Real} (n n')}$$
(2-9)

$$\frac{d\Delta f}{dt} = -\frac{f}{C} \frac{\text{Real} (n \frac{\partial n}{\partial t})}{\text{Real} (n n')}$$
(2-10)

#### 2.3 DESCRIPTION OF THE PROGRAM

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The program traces the path of a radio wave through the ionosphere when given along with the ionospheric models, the transmitter coordinates, the operating frequency, the direction of transmission, the height of the receiver and the maximum number of hops desired. The general set up of the program can take both the electron collisions and the Earth's magnetic field into account and trace the two types of ray paths (ordinary and extraordinary). It can, at our option, drop either or both of the collisions and the magnetic field. The automatic homing feature, common to some ray tracing programs, is not built into this program and it had to be achieved by trial and error, knowing the starting point for the approximate direction of transmission to the receiver.

The distributions of electron density, collision frequency and Earth's magnetic field constitute the input models that describe the ionosphere. Routines for several ionospheric models have been made available with the program. Five analytic models and tabular or true-height analysis profiles constitute the supplied electron density routines. Two collision frequency routines exist; one for tabular profiles and the other for a constant collision frequency. There are two routines that model the Earth's magnetic field; one is for an Earth-centered dipole, and the other is based on constant dip and gyro-frequency. The model routines are arranged in the programs in such a fashion that they can be replaced with any desired models with utmost ease provided, of course, the new routines follow the format already set.

The numerical integration of the ray tracing equations can be carried out by using either one of the two routines available; one based on Runge-Kutta method, and the other on Adams-Moulton method.

The integration routine by Adams-Moulton method has a built-in mechanism for checking errors and adjusting the integration step size accordingly. The maximum allowable error in any single step for any of the equations integrated in the routine is specified in the form of an input parameter. The step size is decreased to gain required accuracy if the error is larger than the specified maximum and in creased to reduce the computing time if the error is smaller. A value of  $10^{-4}$  is commonly used for the maximum allowable error as a compromise between cost and accuracy.

The program uses two spherical polar coordinate systems; one is geographic, and the other computational. The input data such as the location of the transmitter and the geomagnetic north pole is given in geographic coordinates; the transformation to the computational system is carried out within the program. When the dipole model is used for the Earth's magnetic field, the computational system is a geomagnetic coordinate system and both electron density and collision frequency must be defined in geomagnetic coordinates.

The input data to the program is arranged in a one dimensional array (W array) and read in with one parameter on each card. This array provides all the information needed for the ray trace including the parameters associated with the analytic models for electron density, collision frequency and magnetic field. The output is available in various forms individually or in any combination. During the course of the ray trace the program will print information giving the position of the current ray path point, the wave normal direction and cummulative values of the quantities like group path, phase path, absorption, and Doppler shift. The main results of the program can be obtained, if desired, in the form of punched cards called ray-sets which can be used as input for other programs. The

ray paths can be plotted in two projection planes; a ground plane and any given vertical plane. It is possible to show the lateral deviations in a blown-up scale on the ground plane plot.

## 2.4 APPLICATION TO PLASMA CLOUDS

The ray tracing program has been used here to investigate the scattering behavior of an expanding Gaussian plasma cloud by synthesizing hf direct echo signatures both in Doppler shift and signal strength. The rays that have been traced are intended to simulate the signatures of test Mulberry (Pre-SECEDE) for which high quality Doppler data is available. The ultimate objective here is to compare the results with observation and thus test the validity of the Gaussian model for the ion cloud. The program has been used in the mode that takes the collisions and magnetic field into account as well as in the modes that neglect either one or both. The ray paths have been calculated for all the three types of rays, namely, ordinary, extraordinary and no-field.

The models adopted for the electron density of the cloud, the collision frequency and the magnetic field are all analytic throughout. The ion cloud model, discussed in detail in the next section, is represented by a Gaussian distribution cylindrically symmetric about the direction of Earth's magnetic field and governed by anisotropic diffusive expansion. The relevant Gaussian parameters that determine the electron density in time and space are based upon experimental measurements. The electron collisions are represented by a piece-wise exponential function with parameters that best fit the models published by Thrane and Piggot (1966). It turned out, however, that the collisional effects are negligible and never amount to more than a fraction of a dB in absorption. This is due to the fact that the ion cloud considered here was released in the F region where collisions are small and at twilight when the contribution from the

ambient ionosphere is still negligible. The dipole model is chosen for the Earth's magnetic field with the geomagnetic north pole located at  $78.3^{\circ}N$  and  $291^{\circ}E$  (geographic). The equatorial value of the gyrofrequency is taken to be 0.8 MHz and this together with the dipole model determines its value at any point in space.

The method of Adams-Moulton with relative error check was chosen out of the four options provided in the program for integrating the ray trace equations. The maximum allowable single step error was given a value in the range  $10^{-4}$  to  $10^{-6}$  depending on how stringent the ray tracing conditions are at a given time of the cloud's life. It was assigned a smaller value (5 x  $10^{-6}$  or  $10^{-6}$ ), to keep uniform accuracy as judged from the first column of the printout (see Appendix A), during the late phase when the plasma frequency contour supporting the signal return is small in size and rapidly collapsing to the center. Whenever this parameter was altered, suitable changes have also been made in other related parameters like initial integration step size and its minimum limit.

The ray tracing results were printed out in all cases, but plots in the two possible planes, vertical and ground, have been made only for some selected cases of interest. A sample plot and a printout are presented in Appendix A. The supplementary information on polarization, phase path and group path, obtained along with the Doppler results, will not be discussed here as they fall beyond the scope of this report.

#### SECTION 3. PLASMA CLOUD MODEL

#### 3.1 AMBIPOLAR DIFFUSION MODEL

The ion clouds of interest here are generated in the F region by means of rocket releases of metallic Barium vapor. The cloud, on formation, is subject as a whole to electrodynamic drift due to the presence of external electric field while at the same time expanding in a manner determined by diffusion. The charge neutrality, that is  $n_i = n_e$ , is satisfied in the cloud since the Debye shielding length is much smaller than the typical cloud dimensions and the diffusion is of ambipolar nature. The problem of ambipolar diffusion of the cloud in the geomagnetic field, neglecting the external electric field, has been studied by Holway (1965). The diffusion equation has been solved in cylindrical coordinate system (r,  $\phi$ , z) with z axis taken along the Earth's magnetic field. In this system, because of the cylindrical symmetry, the azimuthal component of the particle flux is non-divergent and it is, therefore, necessary to consider only the components in the z and r directions. Using the above criterian and a relation that the ion flux is the same as the electron flux in both the radial and logitudinal directions, Holway derives the equation for the ambipolar diffusion of the ionized cloud as:

$$\frac{\partial n}{\partial t} = \frac{D_{||}}{\Omega_{ie}} - \frac{1}{r} - \frac{\partial}{\partial r} - (r - \frac{\partial n}{\partial r}) + D_{||} - (\frac{\partial^2 n}{\partial r^2})$$
(3-1)

where n is the ion (electron) number density,  $\Omega_{ie} = (1 + \omega_i \omega_e / v_i v_e)$ , and  $D_{||} = D_i D_e (T_i + T_e) / (D_i T_e + D_e T_i)$  is the ambipolar diffusion coefficient.

The solution to Equation 3-1 for an ionized release of  $N_i$  ions, which is initially spherical with a Gaussian distribution of initial effective radius  $h_0$ , is:

n (r,z,t) = 
$$\left[\frac{N_{1}}{\pi^{3/2}z_{1}r_{1}^{2}}\right]$$
 exp $\left[-(z/z_{1})^{2} - (r/r_{1})^{2}\right]$  (3-2)

where

 $z_1 = (h_0^2 + 4D_{||}t)^{1/2}$  and  $r_1 = (h_0^2 + 4D_{||}t/\Omega_{ie})^{1/2}$  are the longitudinal and transverse Gaussian radii.

An extension has been made recently to the above solution by Simon (1970) by taking the presence of an external electric field into consideration. The diffusion equation in this case has been formulated, after making considerable simplification by Simon as:

$$\frac{\partial N}{\partial t} = \mathcal{D}_{\perp} \nabla_{\perp}^{2} N + \mathcal{D}_{\parallel} \nabla_{\parallel}^{2} N + \alpha \overrightarrow{U}_{0} \cdot \overrightarrow{\nabla}N + \beta \overrightarrow{U}_{0} \times b \cdot \overrightarrow{\nabla}N \quad (3-3)$$

The solution to Equation 3-3, assuming that the plasma is created at the origin at t = 0 and the total number of ions created at that time is  $S_0$ , is

$$N(\vec{x}, t) = \left[\frac{s_{o}}{4\pi p_{\perp} t (4\pi p_{\parallel} t)^{1/2}}\right]$$
$$exp\left[-\frac{(r_{\perp}^{2} + \vec{\alpha} v_{\parallel} + \beta v_{o} \times \vec{b} t)}{4 p_{\perp} t} - \frac{z^{2}}{4 p_{\parallel} t}\right] (3-4)$$

Note that Equations 3-3 and 3-4 retain Simon's notation. If the initial condition is changed from a  $\delta$  function to that of a spherical Gaussian distribution with radius  $h_0$ , the Gaussian radii of Equation 3-4 would transform to the same form as of Equation 3-2 in the manner discussed by Holway (1965). The solution given in Equation 3-4 is a cylindrically symmetric Gaussian moving with velocity ( $-\alpha U_0 - \beta U_0 \times b$ ). Since the Doppler associated with uniform drift velocity can be taken into account explicitly outside the ray tracing program, Equation 3-2 has been adopted here for the electron density distribution. The origin about which the expansion takes place was allowed to shift, however, on the basis of the trajectory information obtained from the optical measurements.

#### 3.2 MODEL TRANSFORMATION TO GEOMAGNETIC COORDINATE SYSTEM

The ray tracing program calls for electron densities and their gradients in terms of geomagnetic spherical dipole coordinates. This requires a correspondence between the cloud centered cylindrical coordinate system and the Earth-centered dipole coordinate system. The transformation can be made first by relating two Cartesian systems, one cloud centered (x, y, z) and the other Earth centered  $(x_m, y_m, z_m)$ , since they are directly related to respective polar systems. The system (x, y, z) is defined such that z is anti-parallel to the magnetic field direction and y is directed toward geomagnetic east in the northern hemisphere. In  $(x_m, y_m, z_m)$ ,  $z_m$  is along the dipole axis and directed toward the north pole,  $(x_m, z_m)$  defines a reference (0<sup>°</sup>) geomagnetic meridian plane and  $y_m$  is toward geomagnetic east. In general, it involves one translation and two rotations to bring correspondence between the two systems, as shown in Figure 3-1. The translation is along the vector joining the two origins and the rotations are in two orthogonal, geomagnetic latitude and meridian, planes. Let the cloud center in geomagnetic coordinates be



Figure 3-1 Illustration to Show the Coordinate Transformation from Earth Centered Geomagnetic Dipole System (x,y,z) to Cloud Centered System (x,y,z). The Correspondence Between the Two Systems Requires One Translation and Two Rotations.  $(R_{o}, \theta_{mo}, \phi_{mo}), \theta_{mo}$  being geomagnetic co-latitude. When the system  $(x_{m}, y_{m}, z_{m})$  is translated to the cloud center and rotated by  $\phi_{mo}$  about the  $Z_{m}$  axis, an intermediate system  $(x'_{m}, y'_{m}, z'_{m})$  with  $y'_{m}$  co-inciding with y, would result as shown in Figure 3-1.  $(x'_{m}, y'_{m}, z'_{m})$  is related to  $(x_{m'}, y_{m'}, z_{m})$  as:

$$\begin{bmatrix} x'_{m} \\ y'_{m} \\ z'_{m} \end{bmatrix} = \begin{bmatrix} a' \\ b' \\ c' \end{bmatrix} + \begin{bmatrix} \cos \phi_{mo} & \sin \phi_{mo} & 0 \\ -\sin \phi_{mo} & \cos \phi_{mo} & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} x_{m} \\ y_{m} \\ z_{m} \end{bmatrix}$$
(3-5)

The matrix elements a', b', and c' are the result of the translation. Now a rotation by an angle  $\chi_{mo}$ , which is equal to  $(90-I+\theta_{mo})$  as shown in Figure 3-1, in the plane  $(x'_m, z'_m)$  about the  $y'_m$  axis would bring the intermediate system to coincide with (x, y, z). The relation between the two systems is given as:

$$\begin{bmatrix} x \\ y \\ z \end{bmatrix} \begin{bmatrix} \cos \chi_{mo} & 0 & -\sin \chi_{mo} \\ 0 & 1 & 0 \\ \sin \chi_{mo} & 0 & \cos \chi_{mo} \end{bmatrix} \begin{bmatrix} x' \\ m \\ y'_{m} \\ z' \\ m \end{bmatrix}$$
(3-6)

combining Equations 3-5 and 3-6 we have

$$\begin{bmatrix} x \\ y \\ z \end{bmatrix} = \begin{bmatrix} a \\ b \\ c \end{bmatrix} + \begin{bmatrix} \cos \phi_{mo} \cos \chi_{mo} & \sin \phi_{mo} \cos \chi_{mo} & -\sin \chi_{mo} \\ -\sin \phi_{mo} & \cos \phi_{mo} & 0 \\ \cos \phi_{mo} \sin \chi_{mo} & \sin \phi_{mo} \sin \chi_{mo} & \cos \chi_{mo} \end{bmatrix} \begin{bmatrix} x \\ y \\ y \\ z \\ z \end{bmatrix}$$
(3-7)

The elements a, b and c denote the translation with respect to x, y, and z and can be evaluated by considering the origin of the cloud where:

$$\begin{bmatrix} x \\ y \\ z \end{bmatrix} = 0 \text{ and } y_{m} = y_{m0} = (R_{\oplus} + h) \sin \theta_{m0} \cos \phi_{m0}$$
(3-8)  
$$z_{m} = z_{m0} = (R_{\oplus} + h) \cos \theta_{m0}$$
(3-8)

 $R_{\oplus}$  is the radius of the Earth, h is the height and  $\theta_{mo}$ ,  $\phi_{mo}$  are the geomagnetic colatitude and longitude of the cloud center. Substituting Equation 3-8 into Equation 3-7 gives

$$a = -x \cos \phi \cos \chi_{mo} - y \sin \phi \cos \chi_{mo} + z \sin \chi_{mo}$$
(3-9a)

$$b = x_{mo} \sin \phi_{mo} - y_{mo} \cos \phi_{mo}$$
(3-9b)

$$c = x_{mo} \cos \phi_{mo} \sin \chi_{mo} - y_{mo} \sin \phi_{mo} \sin \chi_{mo} - z_{mo} \cos \chi_{mo}$$
(3-9c)

The position of the cloud center is made available usually in geographic coordinates and they are converted to geomagnetic coordinates using the following expressions:

$$\cos \theta_{mo} = \sin \theta_{o} \sin \theta_{n} + \cos \theta_{o} \cos \theta_{n} \cos (\phi_{o} - \phi_{n})$$
(3-10a)

$$\sin \phi_{mo} = \frac{\cos \theta_{o} \sin (\phi_{o} - \phi_{n})}{\sin \theta_{mo}}$$
(3-10b)

Where  $\begin{pmatrix} \theta_{0}, \phi_{0} \end{pmatrix}$  are the geographic latitude and longitude of the cloud center and  $\begin{pmatrix} \theta_{n}, \phi_{n} \end{pmatrix}$  are the geographic latitude and longitude of the geomagnetic north pole (note that  $\theta_{m0}$  is the geomagnetic colatitude).

When the ray tracing program refers to the electron density subroutine with geomagnetic coordinates  $(R, \theta_m, \phi_m)$ , they are transformed to corresponding (x, y, z) through  $(x_m, y_m, z_m)$ . Further, by converting the cylindrical coordinates of Equation 3-2 to corresponding (x, y, z) we have:

$$n(R, \theta_{m}, \phi_{m}) = n(x, y, z) = \left[ \left( \frac{N_{i}}{\pi^{3/2} z_{1} r_{1}^{2}} \right) \right] \exp \left[ \frac{\left( \frac{x^{2} + y^{2}}{r_{1}^{2}} - \frac{z^{2}}{z_{1}^{2}} \right)}{r_{1}^{2} z_{1}^{2}} \right]$$
(3-11)

#### 3.2.1 DENSITY GRADIENT FIELD

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The electron density partial derivatives are evaluated by using the following matrix relations.

$$\begin{bmatrix} \frac{\partial n}{\partial R} \\ \frac{\partial n}{\partial R} \\ \frac{\partial n}{\partial \theta_{m}} \\ \frac{\partial n}{\partial \phi_{m}} \end{bmatrix} = \begin{bmatrix} \frac{\partial x_{m}}{\partial R} & \frac{\partial y_{m}}{\partial R} & \frac{\partial z_{m}}{\partial R} \\ \frac{\partial x_{m}}{\partial \theta_{m}} & \frac{\partial y_{m}}{\partial \theta_{m}} & \frac{\partial z_{m}}{\partial \theta_{m}} \\ \frac{\partial n}{\partial \theta_{m}} & \frac{\partial y_{m}}{\partial \theta_{m}} & \frac{\partial z_{m}}{\partial \theta_{m}} \end{bmatrix} \begin{bmatrix} \frac{\partial n}{\partial x_{m}} \\ \frac{\partial n}{\partial y_{m}} \\ \frac{\partial n}{\partial y_{m}} \end{bmatrix}$$
(3-12)

$$\frac{\partial x_{m}}{\partial R} = \frac{\partial y_{m}}{\partial R} = \frac{\partial z_{m}}{\partial R}$$

$$\frac{\partial x_{m}}{\partial \theta_{m}} = \frac{\partial y_{m}}{\partial \theta_{m}} = \begin{bmatrix} \sin \theta \cos \phi_{m} & \sin \theta_{m} \sin \phi_{m} & \cos \theta_{m} \\ R \cos \phi_{m} & \cos \phi_{m} & R \cos \theta_{m} \sin \phi_{m} & -R \sin \theta_{m} \\ R \cos \theta_{m} \cos \phi_{m} & R \cos \theta_{m} \sin \phi_{m} & -R \sin \theta_{m} \\ -R \sin \theta_{m} \sin \phi_{m} & R \sin \theta_{m} \cos \phi_{m} & 0 \end{bmatrix}$$

$$(3-13)$$

$$\begin{bmatrix} \frac{\partial n}{\partial x} \\ \frac{\partial n}{\partial x} \\ \frac{\partial n}{\partial y} \\ \frac{\partial n}{\partial z} \\ \frac{\partial n}{\partial z}$$



(3-15)

$$\begin{bmatrix} \frac{\partial n}{\partial x} \\ \frac{\partial n}{\partial y} \\ \frac{\partial n}{\partial z} \end{bmatrix} = \begin{bmatrix} n(R, \theta_{m}, \phi_{m}) \begin{bmatrix} -2x/r_{1}^{2} \end{bmatrix} \\ n(R, \theta_{m}, \phi_{m}) \begin{bmatrix} -2y/r_{1}^{2} \end{bmatrix} \\ n(R, \theta_{m}, \phi_{m}) \begin{bmatrix} -2y/r_{1}^{2} \end{bmatrix} \end{bmatrix}$$
(3-16)

The time derivative  $\partial n/\partial t$  is evaluated by writing n as

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$$n(x,y,z,t) = \frac{N_{1}}{\pi^{3/2}} \underbrace{\frac{(1-e^{-t/\tau})}{z_{1}}}_{f(t)} \underbrace{e^{-\left(\frac{x^{2}+y^{2}}{r_{1}^{2}}\right)}}_{g(t)} \underbrace{e^{-\left(\frac{z^{2}}{z_{1}^{2}}\right)}}_{H(t)} \underbrace{e^{-\left(\frac{z^{2}}{z_{1}^{2}}\right)}}_{g(t)} \underbrace{e^{-\left(\frac{z^{2}}{z_{1}^{2}}\right)}}_{H(t)} \underbrace{e^{-\left(\frac{z^{2}}{z_{1}^{2}}\right)}}_{g(t)} \underbrace{e^{-\left(\frac{z^{2}}{z_{1}^{$$

$$\frac{\partial n}{\partial t} = \frac{N_{i}}{\pi^{3/2}} \left[ \frac{\partial n}{\partial f} \quad \frac{\partial f}{\partial t} + \frac{\partial n}{\partial g} \quad \frac{\partial g}{\partial t} + \frac{\partial n}{\partial H} \quad \frac{\partial H}{\partial t} \right]$$

$$= \frac{N_{i}}{\pi^{3/2}} \left[ gH \quad \frac{\partial f}{\partial t} + fH \quad \frac{\partial g}{\partial t} + fg \quad \frac{\partial H}{\partial t} \right]$$
(3-18)

$$\frac{\partial f}{\partial t} = \frac{e^{-t/\tau}}{\tau z_{1}r_{1}^{2}} - \frac{f}{z_{1}r_{1}^{2}} (4 z_{1}^{2} D_{1} + 2D_{1} r_{1}^{2}) \quad (3-19a)$$

$$\frac{\partial g}{\partial t} = 4 D_{\perp} g \left[ \left( x^2 + y^2 \right) / r_{\perp}^4 \right]$$
(3-19b)

$$\frac{\partial H}{\partial t} = 4 D_{||} H (z^2/z_1^4)$$
 (3-19c)

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#### 3.3 ION CLOUD INPUT PARAMETERS

The coordinates of the center of the ion cloud and the parameters, total ion content  $N_i$ , ionization time constant  $\tau$ , initial Gaussian radius  $h_o$ , and longitudinal and transverse diffusion coefficients  $D_{||}$  and  $D_{\perp}$  form the input to set up the electron density distribution for the ray tracing. The numerical values of the parameters are appropriate to test Mulberry of Pre-SECEDE and are taken from Minkoff (1970). The positional data obtained by photographic means was available in the form of look angles (azimuth and elevation) from different observation sites. These observations taken from pairs of stations have been used to determine the coordinates of the cloud following a vector method described in Appendix B. The trajectory information is shown in Figure 3-2 for the period of interest of ray tracing.

The total ion content N is obtained by integrating Equation 3-2 over all space, from which:

 $N_i = n_p (t) \pi^{3/2} (h_o^2 + 4D_{||} t)^{1/2} (h_o^2 + 4D_{\perp} t)$  (3-20) The peak electron (ion) density  $n_p (t)$  is taken from hf radar measurements. The Gaussian radii  $(h_o^2 + 4D_{||} t)^{1/2}$  and  $(h_o^2 + 4D_{\perp} t)^{1/2}$  are determined by means of microdensitometer scans of the filter photographs of the cloud. Figure 3-2 also presents the peak electron density variation with time and the results from the densitometer scans. The numerical values obtained for the parameters are given in Table 3-1.



Figure 3-2 The Trajectory, the Peak Electron Density and the Results From Microdensitometer Scans of the Filter Photographs of the Cloud. (Filled and Open Circles in the Trajectory Data Represent Determinations from Two Pairs of Optical Stations).

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## TABLE 3-1

## NUMERICAL VALUES FOR ION CLOUD PARAMETERS

| Test     | h (KM)<br>O | D (KM <sup>2</sup> /SEC) | D <sub>⊥</sub> (KM <sup>2</sup> /SEC) | N<br>i               |
|----------|-------------|--------------------------|---------------------------------------|----------------------|
| Mulberry | 3.0         | 0.13                     | 0.045                                 | $3.0 \times 10^{24}$ |

The reader is referred to Minkoff (1970) for details on how these parameters are deduced.

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## SECTION 4. SYNTHESIS OF RADAR SIGNATURES

Two methods have been used for synthesizing radar signatures for the test Mulberry; one involves the rigorous ray tracing technique, and the other, an approximate technique meant primarily for the purpose of comparison, is based on an expanding hard ellipsoid model. This section is devoted to a description of the two methods and to a discussion of the results obtained.

#### 4.1 RAY TRACING METHOD

There are two steps involved in synthesizing a radar signature. The first step is to determine the ray that homes in on the receiver when the transmitter-cloud-receiver configuration is given. The Doppler shift of interest is the one associated with this ray and it is listed in the output of the ray tracing program as a cumulative sum along the ray path. The next step is to determine the signal strength associated with this ray. It is evaluated in terms of radar scattering cross section of the cloud since it is a convenient parameter to compare different models and to gain some insight into the scattering behavior of the ion clouds. The process of homing-in on the receiver proceeds in steps and is as follows: First, the elevation and azimuth of the cloud center is calculated with respect to the transmitter location. This provides the initial guess for the direction of transmission at the starting time. Using this as reference direction, a matrix of nine rays (3 x 3 in elevation and azimuth) defining a rectangular solid angle are shot normally as a first trial. The angular increments in elevation and azimuth are selected such that the impact points form a contour that encloses the receiver location. The points, in general, describe a skewed quadrilateral because of the nonlinear nature of the cloud defocussing.

The next trial uses, in general, four rays for which the elevation and azimuth angles are arrived at by interpolating between the constant elevation and constant azimuth lines associated with the impact points. The rays, in this trial, converge toward the receiver to come usually within 25 km. Proceeding along the same lines, the next set of four trial rays shrink the impact area to typically a 5 km square. The 'homing in' ray is determined, finally, on the basis of the last set of four impact points. The ray is considered to have successfully 'homed in' if it returns to within 1 km of the receiver location. The 'homing in' ray for an initial time serves as a guide to arrive at the first guess trial rays for a subsequent time. Figure 4-1 illustrates the sequence of trials used to accomplish the homing of an extraordinary ray of 16.078 MHz transmitted at 70 seconds after the release of the cloud. It was found that, in practice, it is often easier to guess the bound rays in elevation than in azimuth and consequently instead of  $(3 \times 3)$ , a  $(2 \times 3)$  initial matrix of rays as shown in the figure was found sufficient to enclose the receiver. In selecting the next set of four rays, some account is made for the skewness of the elevation and azimuth lines instead of choosing the angles associated with four evenly spaced points around the receiver. The final set of four trial rays, however, are selected evenly to center the receiver. The sequence shown in the figure represent a shrink in the elevation angle increment from 0.08 to 0.0008° and azimuthal increment from 0.3 to 0.0052. On obtaining the homing ray, the scattering cross section presented by the cloud to this ray is determined as described below.

## 4.1.1 RADAR CROSS SECTION OF THE CLOUD

The scattering cross section of the cloud  $\sigma$ , defined in terms of an equivalent isotropic scatter, is given by the bistatic radar equation as:
MULBERRY FEIG.078 MH2 XTRACEDINARY RAY

A. S. Tarris musicer at



Figure 4-1 Illustrates the Method for Determination of the 'Homing' Ray. A,B, C,D, etc. are the Ground Impact Points When a Bundle of Rays Incremented in Azimuth and Elevation are Transmitted

$$\sigma = \frac{16\pi^2 R_1^2 R_2^2}{P_t G_t A_r} \cdot P_r$$
(4-1)

where

 $P_t$  = Transmitted power  $G_t$  = Effective gain of the transmitting antenna  $R_1$  = Range to the scattering volume from the transmitter  $R_2$  = Range to the scattering volume from the receiver  $P_r$  = Received power  $A_r$  = Effective collecting area of the receiving antenna

 $A_r$  can be expressed as  $G_R \lambda^2 / 4\pi$ , where  $G_R$  is the effective gain of the receiving antenna and  $\lambda$  is the wavelength of the received signal. The scattering cross section of the cloud can be calculated from Equation 4-1 following the technique developed by Croft (1967) and generalized recently by Georges and Stephenson (1969) for 3D ray tracing simulation of hf ground backscatter signatures. The method derives an expression for the received power  $P_r$  which results in an expression for  $\sigma$  free of system parameters. This makes it possible to calculate  $\sigma$  solely on the basis of the ray tracing results. The method in brief is as follows:

A bundle of rays are transmitted about the direction of the homing ray in a small solid angle defined by an elevation angle increment of  $\Delta\beta$  and azimuth angle increment of  $\Delta\phi$ . The flux of energy leaving in this solid angle will refract through the cloud and strike the ground on return over an area denoted as A. The amount of power reaching the impact area is a fraction K times the power fed into the flux tube of transmission where the fraction is determined by the

dissipation losses in the medium. When the transmission is centered at an elevation angle of  $\beta$ , then the solid angle into which the energy is injected becomes  $\Delta\beta \ \Delta\phi \ \cos\beta$ . The power leaving this solid angle is given as:

$$\Delta P_{t} = \frac{P_{t} G_{t} \Delta \beta \Delta \phi \cos \beta}{4\pi}$$
(4-2)

when this power approaches the impact area A at the elevation angle  $\Psi$ , then the received power P<sub>r</sub> is given as:

$$P_{r} = \frac{P_{t} G_{t} \Delta \beta \Delta \phi \cos \beta A_{r} K}{4\pi A \sin \Psi}$$
(4-3)

The fraction K is given as exp (-X/4.343) where X is the total absorption in dB suffered by the homing ray. The Equation 4-3 for P<sub>r</sub> applies strictly to a cw radar and in the case of a pulse radar it should be multiplied by a correction factor to take account of the pulse spreading in time. If  $\tau$  and  $\tau + \Delta \tau$  are the pulse lengths of the transmitted and received signals the correction factor is given approximately as  $(\tau/\tau+\Delta\tau)$ . This correction is considered small and neglected.

Substituting for  $P_r$  in Equation 4-1 leads to

$$\sigma = \frac{4\tau R_1^2 R_2^2 \Delta\beta \Delta\phi \cos\beta K}{A \sin\Psi}$$
(4-4)

In the Equation 4-4 for  $\sigma$ , the parameters  $\beta$ ,  $\Delta\beta$  and  $\Delta\phi$  are the specified input to the ray tracing program. The output provides  $\Psi$ , K and all the information necessary to compute R<sub>1</sub>, R<sub>2</sub> and A. The geometry involved

to calculate A is the same as described by Goerges and Stephenson (1969) and is as shown in Figure 4-2. Consider a set of four rays that constitute a rectangular flux tube. The rays while passing through the cloud undergo lateral deviations and on hitting the ground form a spherical quadrilateral. The area of the quadrilateral can be calculated from the coordinates of the four corners supplied by the ray tracing program. In practice, the four rays of the flux tube



Figure 4-2 Geometry of an Electromagnetic Flux Tube Illuminating a Patch of Ground on Reflection from the Plasma Cloud

are so closely packed that the quadrilateral can be considered plane and a simple formula for the area can be applied. If  $r_1$ ,  $r_2$ ,  $r_3$  and  $r_4$  are the ground ranges to the four landing points and  $\theta_1$ ,  $\theta_2$ ,  $\theta_3$ and  $\theta_4$  are their azimuths then,

$$A \approx \frac{1}{2} \left| \frac{r_3 - r_1}{\sin \alpha} \right| \left| \frac{r_4 - r_2}{\sin \gamma} \right| \sin (\alpha + \gamma)$$
(4-5a)

where

$$\tan \alpha = \left| \frac{r_3 - r_1}{\theta_3 - \theta_1} \right| \left[ R_E \sin \frac{r_3 + r_1}{2R_E} \right]^{-1}$$
(4-5b)

$$\tan \gamma = \left| \frac{r_4 - r_2}{\theta_4 - \theta_2} \right| \left[ R_E \sin \frac{r_4 + r_2}{2R_E} \right]^{-1}$$
(4-5c)

and  $R_E$  is the radius of the Earth. This amounts to calculating the area of a quadrilateral by one-half the product of its diagonals times the sine of the angle between them. The area is calculated using the final set of trial rays such as shown in Figure 4-1 provided it is less than about 5 km square and the receiver is reasonably well centered. Otherwise, a new set of four rays closely spaced about the homing ray are used to meet the requirement.

The ranges  $R_1$  and  $R_2$  to the reflection point from the transmitter and the receiver are calculated by forming two triangles as shown in Figure 4-3. Considering the triangle TSO, the range  $R_1$  is obtained as:

$$R_{1} = \left[ R_{E} \sin \xi_{1} / \cos(\xi_{1} + \beta) \right]$$
(4-6)

The ground range to the subreflection point TS' taken from the ray tracing output provides the central Earth angle  $\xi_1$ .

The range  $R_{2}$  is obtained, considering the Triangle RSO, as:

$$R_{2} = \left[ \left( R_{E} \sin \xi_{2} \right)^{2} + \left( R_{E} - R_{E} \sin \xi_{2} + h \right)^{2} \right]^{1/2}$$
(4-7)

The ground range  $RS_1$  which provides  $\xi_2$  is calculated from the spherical triangle  $TRS_1$  knowing the ranges TR and  $TS_1$  and the azimuth of the subreflection point with respect to TR.

The scattering cross section  $\sigma$  is calculated by substituting the Equations 4-5, 4-6 and 4-7 in 4-4.



Figure 4-3 Illustration to Evaluate the Ranges  $R_1$  and  $R_2$  to the Reflection Point from the Transmitter and the Receiver

#### 4.2 HARD EXPANDING ELLIPSOID METHOD

#### 4.2.1 RADAR CROSS SECTION (RCS)

The radar cross section of a smooth body is given from considerations of geometric optics as (Crispin and Maffett, 1968):

$$\sigma \approx \pi R_1 R_2 \tag{4-8}$$

Where  $R_1$  and  $R_2$  are the principal radii of curvature at the specular reflection point and are both assumed to be large in comparison with the operating wavelength. If the equation of the target surface is expressed in the form z = f(x, y), then

$$R_{1}R_{2} = \frac{\left(1 + f_{x}^{2} + f_{y}^{2}\right)^{2}}{\left|f_{xx}f_{xy} - f_{xy}^{2}\right|}$$
(4-9)  
where  $f_{x} = \frac{\partial z}{\partial x}$ ,  $f_{y} = \frac{\partial z}{\partial y}$ ,  $f_{xx} = \frac{\partial^{2} z}{\partial x^{2}}$ ,  $f_{yy} = \frac{\partial^{2} z}{\partial y^{2}}$  and  $f_{xy} = \frac{\partial^{2} z}{\partial x \partial y}$ 

The surface of interest here is that of an ellipsoid for which the equation can be written as:

$$\left(\frac{x}{a}\right)^{2} + \left(\frac{y}{b}\right)^{2} + \left(\frac{z}{c}\right)^{2} = 1$$
(4-10)

Using the coordinate system shown in Figure 4-4, the following expression can be derived for monostatic radar cross section of the general ellipsoid.

$$\sigma = \frac{\pi a^2 b^2 c^2}{\left[a^2 \sin^2 \theta \cos^2 \phi + b^2 \sin^2 \theta \sin^2 \phi + c^2 \cos^2 \theta\right]^2}$$
(4-11)

The Equation 4-11 for the case of Barium ion clouds, which can be approximated to a prolate spheroid (a = b), can be reduced to



Figure 4-4 Coordinate System Adopted to Obtain An Expression for the Radar Cross Section of the Ellipsoid

$$\sigma = \frac{\pi b^4 c^2}{\left[b^2 \sin^2 \theta + c^2 \cos^2 \theta\right]^2}$$
(4-12)

The radar configuration in the experiment of interest here (test Mulberry) is approximately monostatic and, therefore, the Equation 4-12 can be used to calculate the cross section. The parameters c and b, the major and minor axes of the cloud, and the aspect angle  $\theta$  to the specular point from the radar are evaluated at any given time as described in the following paragraphs.

#### 4.2.1.1 Determination of c and b

The electron density in the cloud is given according to the Equation 3-2. The parameters c and b are the major and minor axes of the ellipsoidal contour with the electron density critical to the

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operating frequency of the radar. If n denotes the critical density, it is given by considering the variation along the axis (r = 0) as:

$$n_{p} = \frac{N_{i} (1 - e^{-t/\tau}) \exp \left[-c^{2} (h_{o}^{2} + 4D_{||}t)\right]}{\pi^{3/2} (h_{o}^{2} + 4D_{||}t)^{1/2} (h_{o}^{2} + 4D_{|}t)}$$
(4-13)

From Equation 4-13 one obtains

$$c = (h_{o}^{2} + 4D_{||}t)^{1/2} \left[ ln \frac{N_{i} (1 - e^{-t/\tau})}{n_{p} \pi^{3/2} (h_{o}^{2} + 4D_{||}t)^{1/2} (h_{o}^{2} + 4D_{1}t)} \right]^{1/2}$$

$$(4-14)$$

similarly considering the variation along a radius vector at z = 0, one gets

$$b = (h^{2} + 4D_{1}t)^{1/2} \left[ ln \frac{N_{i} (1 - e^{-t/\tau})}{n_{p} \pi^{3/2} (h^{2} + 4D_{||}t)^{1/2} (h^{2} + 4D_{1}t)} \right]^{1/2}$$
(4-15)

# 4.2.1.2 Determination of the Aspect Angle $\theta$

Consider a cloud centered Cartesian system (x, y, z) as defined in Section 3 with z axis anti-parallel to the direction of the Earth's magnetic field. Let the coordinates of the radar in this system be  $(x_1, y_1, z_1)$  and those of the specular point be denoted as  $(x_0, y_0, z_0)$ . The coordinates of the specular point are evaluated by considering a unit vector normal to the surface at that point. The equations for the ellipsoid and the unit normal vector are:

$$z = \left[ c^{2} - c^{2} \left( \frac{x^{2} + y^{2}}{b^{2}} \right) \right]^{1/2}$$
(4-16)

$$\vec{N} = \frac{\vec{1} \cdot \vec{f}_{x0} + \vec{j} \cdot \vec{f}_{y0} - \vec{k}}{(\vec{f}_{x0}^2 + \vec{f}_{y0}^2 + 1)^{1/2}}$$
(4-17)

Where i, j, k are the unit vectors along x, y, z and  $f_{xo}$ ,  $f_{yo}$ , are the partial derivatives  $\frac{\partial z}{\partial x}$  and  $\frac{\partial z}{\partial y}$  at the point  $(x_0, y_0, z_0)$ . Since the normal vector is along the line joining the specular point to the radar, the unit vector  $\vec{N}$  can also be expressed, using the geometry shown in Figure 4-5, as:

$$\vec{N} = \frac{\vec{PR}}{PR} = \frac{\vec{i} (x_1 - x_0) + \vec{j} (y_1 - y_0) + \vec{k} (z_1 - z_0)}{\left[ (x_1 - x_0)^2 + (y_1 - y_0)^2 + (z_1 - z_0)^2 \right]^{1/2}}$$
(4-18)

Equating 4-17 and 4-18 and substituting  $\left(-\frac{c^{2}}{b^{2}}, \frac{c^{0}}{z_{0}}\right)$  for f and 2

$$\begin{pmatrix} -\frac{c^{2}}{b^{2}} & \frac{y_{0}}{z_{0}} \end{pmatrix} \text{ for } f_{y0} \text{ leads to}$$

$$x_{1} = x_{0} \begin{bmatrix} 1 - \frac{c^{2}}{b^{2}} + \frac{c^{2}}{b^{2}} \frac{z_{1}}{z_{0}} \end{bmatrix}$$

$$y_{1} = y_{0} \begin{bmatrix} 1 - \frac{c^{2}}{b^{2}} + \frac{c^{2}}{b^{2}} \frac{z_{1}}{z_{0}} \end{bmatrix}$$

$$(4-19)$$

$$(4-20)$$



Figure 4-5 The Geometry to Express Unit Vector Normal to the Cloud Surface at the Specular Point from the Radar

Equations 4-19 and 4-20 are squared and then added to yield, on substitution of  $\begin{bmatrix} b^2 - (b^2/c^2)z_0^2 \end{bmatrix}$  for  $x_0^2 + y_0^2$ , a quartic in  $z_0$  of the form

$$Az_{o}^{4} + Bz_{o}^{3} + Cz_{o}^{2} + Dz_{o} + E = 0$$
 (4-21)

where

$$A = \left[\frac{b^2}{c^2} + \frac{c^2}{b^2} - 2\right]$$

$$B = \left[2z_1 - 2\frac{c^2}{b^2}z_1\right]$$

$$C = \left[x_1^2 + y_1^2 + \frac{c^2}{b^2}z_1^2 - b^2 - \frac{c^4}{b^2} + 2c^2\right]$$

$$D = \left[2\frac{c^4}{b^2}z_1 - 2c^2z_1\right]$$

$$E = \left[-\frac{c^4}{b^2}z_1^2\right]$$

Since the dimensions of the cloud are very small compared to the distance between the radar and the cloud, a good approximation to the solution of the Equation 4-21 can be obtained by dropping the higher order terms with coefficients A and B. The resulting equation is solved for  $z_0$  and of the two possible values, the one with favorable geometry for specular reflection is taken and substituted, in turn, in Equations 4-19 and 4-20 to get  $x_0$  and  $y_0$ . The coordinates of the radar that are used to calculate the specular point are given by:

$$\begin{bmatrix} x_{1} \\ y_{1} \\ z_{1} \end{bmatrix} = \begin{bmatrix} a \\ b \\ c \end{bmatrix} + \begin{bmatrix} \cos \phi_{mo} \cos \chi_{mo} & \sin \phi_{mo} \cos \chi_{mo} & -\sin \chi_{o} \\ -\sin \phi_{mo} & \cos \phi_{mo} & 0 \\ \cos \phi_{mo} \sin \chi_{mo} & \sin \phi_{mo} \sin \chi_{mo} & \cos \chi_{mo} \end{bmatrix} \begin{bmatrix} x_{m1} \\ y_{m1} \\ z_{m1} \end{bmatrix}$$

$$(4-22)$$

The elements a, b\* and c\* and the transformation matrix are the same as in Equation 3-7.  $(x_{ml}, y_{ml}, z_{ml})$  are the coordinates of the radar in the geomagnetic dipole coordinate system defined in paragraph 3.2. Knowing the coordinates of the specular point, the aspect angle  $\theta$  can be calculated by taking the scalar product of the unit vector  $\vec{N}$  and a unit vector along the magnetic field  $\vec{B}$ .

Let

$$\vec{\mathbf{N}} = \boldsymbol{l}_{1} \hat{\mathbf{i}} + \boldsymbol{l}_{2} \hat{\mathbf{j}} + \boldsymbol{l}_{3} \hat{\mathbf{k}}$$
$$\vec{\mathbf{B}} = \boldsymbol{m}_{1} \hat{\mathbf{i}} + \boldsymbol{m}_{2} \hat{\mathbf{j}} + \boldsymbol{m}_{3} \hat{\mathbf{k}}$$

then

$$\cos \theta = \ell_1 m_1 + \ell_2 m_2 + \ell_3 m_3$$

The direction cosines are given as:  $m_1 = m_2 = 0$ ,  $m_3 = -1$ and  $\ell_3 = -\left[f_{xo}^2 + f_{yo}^2 + 1\right]^{-1/2}$ 

Not to be confused with major and minors axes of the ellipsoid.

substituting for f and f one obtains:

$$\cos \theta = \left[ \frac{\frac{c^4}{c^4}}{\frac{b^4}{b^2}} - \frac{(x_0^2 + y_0^2)}{\frac{c^2}{c^2}} + 1 \right]^{-1/2}$$
(4-23)

# 4.2.2 DETERMINATION OF DOPPLER SHIFT

Let  $(x_{01}, y_{01}, z_{01})$  and  $(x_{02}, y_{02}, z_{02})$  be the coordinates of the specular reflection points on the cloud at times t and t +  $\Delta$ t as shown in Figure 4-6. The corresponding ranges to these reflection points from the radar are given as:



Figure 4-6 Illustrate the Position of the Specular Point at Two Instants of Time to Calculate the Path Difference to it from the Radar

$$R_{1} = \left[ (x_{1} - x_{01})^{2} + (y_{1} - y_{01})^{2} + (z_{1} - z_{01})^{2} \right]_{1}^{\frac{1}{2}}$$
(4-24)

$$R_{2} = \left[ (x_{1} - x_{02})^{2} + (y_{1} - y_{02})^{2} + (z_{1} - z_{02})^{2} \right]^{\overline{2}}$$
(4-25)

Since the signal traverses in free space the difference between the two ranges  $\Delta R (=R_2 - R_1)$  represents the difference in the phase path length to the reflection point. Hence the Doppler shift of the reflected signal at the radar is obtained by

$$\Delta f = \frac{-2\Delta R}{\lambda \Delta t}$$
 (4-26)

The Doppler shift given in the Equation 4-26 is smeared over the time interval  $\Delta t$ . The time increment should, therefore, be made as small as possible without running into computer round off errors in calculating  $\Delta R$ . Figure 4-7 shows a typical case to illustrate how the Doppler shift approaches its true value in an asymptotic manner as  $\Delta t$  is decreased from 0.5 to 0.01 seconds. If  $\Delta t$  is allowed to take lower values, it would result in a fluctuation in  $\Delta f$ . Since the lower limit of  $\Delta t$  is time dependent, it is allowed to vary over an interval at each time and the asymptotic value such as shown in the Figure 4-7 is picked for the Doppler shift.

# 4.3 RESULTS AND DISCUSSION

# 4.3.1 RAY TRACING RESULTS

Figure 4-8 shows ray path projection plots in both vertical and ground planes at 100 seconds after release for all the three modes namely, the no-field the ordinary and the extraordinary. The ray path segments close to the reflection level where there is an appreciable bending are plotted on an enlarged scale for the vertical plane in Figure 4-9 to show how the three modes refract in the denser regions of the cloud.





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Figure 4-8 Ray Path Projection Plots in Both Vertical and Ground Planes at 100 Seconds After Release for the Three Modes, No Field, Ordinary and Extraordinary, at F = 10.31 MHz



Figure 4-9 The Vertical Ray Path Segments Close to the Reflection Level to Show How the Three Modes Refract Through the Denser Regions of the Cloud

The movement of the reflection point with respect to the center of the cloud and the refraction suffered by the rays as function of time are shown in Figures 4-10a, b and c and 4-11a and b in terms of the azimuth and elevation angles of the cloud center, the reflection point and of transmission. It can be seen that the direction of the reflection point walks away from the center during the expansion phase as the cloud becomes elongated and walks back at later times as the reflection surface recedes toward the center. The deviations in azimuth and elevation due to refraction are of some importance and are therefore plotted separately in Figure 4-12. The refraction in the case of no-field ray is entirely due to the density gradients in the ionization at levels below the height of reflection. The deviation is nearly zero at the beginning and increases continuously at a rate that builds up rapidly with time. The O and X rays undergo refraction that is partly due to density gradients and partly due to the magnetic field. The refraction effects due to density gradients and the magnetic field are found to act in the same direction for the X ray while they get cancelled partially for the O ray. The curves for the O ray pass through zero indicating the time when the two effects cancel each other exactly. The refraction is found to be the highest for the X ray with azimuth and elevation deviations of 1.65° and -0.35° respectively (the  $\Delta \varphi$  is in the ground plane and should be multiplied with  $\cos \beta$  to obtain it in the transmission plane). The cross over of the curves for the no-field and the X ray is due to the fact that the deviations increase most rapidly at the time of penetration which comes slightly earlier for the no-field ray.

The defocussing nature of the cloud is illustrated in Figures 4-13 to 4-16. The ray plots shown are for the frequency of 10.31 MHz and for the time of 180 seconds after release. The plots are projections of the ray paths on the ground and the vertical plane





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Figure 4-12 The Azimuth and Elevation Angle Deviations Suffered by the Three Modes Due to Refraction up to the Reflection Level at F = 10.31 MHz



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Figure 4-13 Ray Path Projections in Vertical Plane of a Fine Bundle of Eleven Rays (Appears as Thick Line on the Plot) Transmitted Over an Elevation Scan Interval of 0.02<sup>°</sup>. The Spread of the Rays on Reflection Illustrate the Defocussing Effects of the Cloud



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Figure 4-14 Ray Path Projections in Vertical Plane of a Fine Bundle of Eleven Rays (Appears as Thick Line on the Plot) Transmitted over an Azimuth Scan of Size 0.025°. The Spread of the Rays on Reflection Illustrate the Defocussing Effects of the Cloud







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Figure 4-16 Ray Path Projections on the Ground Plane of a Fine Bundle of Eleven Rays (Thick Line on the Plot from TX) for an Azimuth Scan of Size 0.025<sup>0</sup>

connecting the transmitter and the receiver. They describe how a narrow beam of incident energy confined either to an elevation plane or an azimuth plane become defocussed on reflection from the cloud. The beam sizes  $\Delta \phi \cos \beta$  and  $\Delta \beta$  represented by the scans in azimuth and elevation are respectively 0.025 degrees and 0.02 degrees. They are so narrow in extent that they could be seen only as a thick line on the plots. The energy dispersion on the ground is found to be to an extent of about 130 km and 160 km corresponding to the elevation and azimuth scans of the ground plane plots. The spreading of the revs due to the defocussing effects of the cloud in this case are greater by a factor of about 8 x  $10^5$  relative to free space spreading. The defocussing effects are not uniform over the entire illuminated area since the rays, while equally incremented in the scan, seem to bunch closer in certain areas. It should be mentioned that some of the bunching effect seen especially with the azimuthal scan in the vertical plane is due to the distortion resulting from the projection. The cloud is found to become increasingly more defocussing with time as it gets more and more elongated. On the basis of the impact area calculation described in paragraph 4.1, it is found that the defocussing factor (relative to free space) for the X ray at 10.31 MHz increases from 7.6 x  $10^3$  to 1.85 x  $10^7$  over the interval 5 to 190 seconds. It will increase from 2.27 x  $10^4$  to 1.47 x  $10^8$  in the interval 10 to 85 seconds for 16.078 MHz.

The Doppler and the scattering cross section results synthesized by the ray tracing technique are presented in Figures 4-17 and 4-18 for the two operating frequencies 10.31 MHz and 16.078 MHz. In addition to the ordinary and extraordinary modes, results have been obtained also for the no-field case for 10.31 MHz to study the magnetic field effects. The shapes of the curves showing the variation of the Doppler and the cross section with time are found to be



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Figure 4-17 The Time History of the Doppler Shift and the Scattering Cross Section Synthesized by the Ray Tracing Method for No-Field, Ordinary and Extraordinary Modes at F = 10.31 MHz



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Figure 4-18 The Time History of the Doppler Shift and the Scattering Cross Section Synthesized by the Ray Tracing Method for Ordinary and Extraordinary Modes at F = 16.078 MHz

identical for all the three modes. The Doppler and the cross with 20 variations for the X mode lag in time to that of the 0 mode. The lag in Doppler widens as the cutoff times are approached. The variations for the 'no field' (N) fall in between that of the 0 and X, but closer to the 0 mode. The differences between the 0 and X modes are primarily due to the fact that they are supported by two plasma frequency surfaces whose expansion rates are changing relative to each other with time. The plasma frequency contour supporting the 0 and N modes being the same, the differences between these two indicate the effects due to the magnetic field. At the operating frequency of 10.31 MHz the Doppler shift falls from 17 to -5 Hz in the time interval of 5 seconds after release to the cutoff. The cross-over from positive to the negative Doppler occurs roughly halfway in the time interval, The scattering cross section reaches a maximum of about 2 x  $10^7$  m<sup>2</sup> within 20 to 30 seconds after release and thereafter falls continuously at a rate that increases rapidly with time. It implies that the signal drops out rather abruptly. The results for 16.078 MHz share all the basic features observed for 10.31 MHz. The peak scattering cross section at 16.078 MHz is found to be smaller than at 10.31 MHz by a factor 5 for the ordinary ray and 4 for the extraordinary ray.

4.3.2 COMPARISON WITH ELLIPSOID MODEL

The Doppler and the scattering cross section have been calculated also for the field aligned ellipsoid model using the method described in paragraph 4.2. The results are presented in Figures 4-19 and 4-20. The curves denoted by 0 and X in these figures represent two slightly different operating frequencies which correspond to the plasma frequencies appropriate to the ordinary and the extraordinary modes. The comparison between the ellipsoid model and the ray tracing is intended to bring out the effects on the Doppler and the scattering cross section due to magnetic field and the ionization lying below



Figure 4-19

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4-19 The Time History of the Doppler Shift and the Scattering Cross Section Synthesized by the Hard Ellipsoid Method for F = 10.31 and 9.902 MHz. (The Two Frequencies Correspond to the Plasma Frequencies that Support the 0 and X Modes)



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Figure 4-20 The Time History of the Doppler Shift and the Scattering Cross Section Synthesized by the Hard Ellipsoid Method for F = 16.078 and 15.673 MHz. (The Two Frequencies Correspond to the Plasma Frequencies that Support the 0 and X Modes)

the reflection level. The general shapes of the curves showing the temporal variations of the two parameters are similar for both the models. Considering in detail, the Doppler variations are significantly steeper for the ellipsoid model than for the ray tracing. The negative phase of the Doppler is much more pronounced for the ellipsoid model with the transition from positive to negative occurring significantly earlier than for ray tracing. The transition occurs for the ellipsoid model at about the same time as the scattering cross section begins to decrease whereas it lags a short while with ray tracing. This suggests that an effect of the underlying ionization is to hold the Doppler positive for a short duration even after the contraction phase of the reflection surface is initiated. It causes also the tailing effect of the Doppler to be significantly inhibited. The defocussing effects of the underlying ionization which enhance with time cause a remarkable reduction in the scattering cross section of the cloud. The ray tracing technique yields a cross section which is smaller by a factor that increases with time from 3 at the peak to 30 at the time just prior to penetration. The comparison thus leads to the conclusion that the simple hard ellipsoid model is inadequate for an accurate synthesis of the hf radar signatures.

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### SECTION 5. EXPERIMENTAL RESULTS

#### 5.1 TEST GEOMETRY AND INSTRUMENTATION

The Pre-SECEDE Series of Barium release tests were conducted during the fall of 1969 at White Sands Missile Range, New Mexico. The releases were observed by nine hf radar systems of which eight (6 pulse and 2 cw) had been operated by Raytheon with transmitters located at Paxton Siding and receivers located at Twin Butes. Figure 5-1 shows the geometry of the radar sites with respect to the



Figure 5-1 Illustration to Show the Cloud Geometry With Respect to the Transmitting (TX) and Receiving (RX) Stations
position of the plasma cloud at release for the test Mulberry. The discussion of the results presented in this section is limited to the pulse measurements made at 10.31 and 16.078 MHz for which the ray tracing synthesis has been done.

The radars employed in the experiments are the conventional Phase Path Sounders with the transmitting and the receiving systems phase locked to stable frequency standards at each site. This enables both phase and amplitude of the received signal to be obtained from the observations. The pulse radars had been operated at a 40 pps rate with a pulse width of 150  $\mu$ s. For receiving, a bandwidth 10 kHz was used and the output signal was recorded on analog magnetic tape at a 15 kHz i-f level for later processing. The antennas used for transmitting 10.31 and 16.078 MHz were vertically directed deltas. At the receiving site, a delta antenna was used for receiving at 10.31 MHz and a vertically directed log periodic antenna for receiving at 16.078 MHz.

## 5.2 EXPERIMENTAL DATA

The experimental data recorded on the tape is reduced to the form of doppler spectra. The signature display format is such that the time runs from left to right, Doppler shift runs from bottom to top and the strength of the echo is represented by the darkness of the trace. The signal processing involves phase detection of the i-f signal run off from the tape which is then range gated and sampled at the pulse repetition rate. The sampled signal results in a boxcarved waveform which is fed into a UA-6A spectrum analyzer to obtain the desired Doppler signature display. The unambiguous window of the Doppler spectrum is equal to half the pulse repetition frequency which

in this case is 20 Hz. The Doppler components that fall outside the range fold back into the window and cause images to appear along with the real spectral components. Figure 5-2 shows the Doppler signatures obtained on 10.31 and 16.078 MHz for the test Mulberry. The true signature is simply a single monotonically descending tone and during the first few seconds when the Doppler falls outside the unambiguous window an image appears as labeled on the figure. The frequency folding takes place about 10 Hz instead of 20 Hz since the signal is phase detected with an offset frequency of 10 Hz. The periodic notches that appear on the traces were identified as due to Faraday fading of the received signal.

The spectrally analyzed signal can be displayed also in the form of amplitude spectral cuts in time to measure the received power of the signal and thereby determine the scattering cross section of the cloud as function of time. The sequence of spectra obtained have a time resolution of 1.5 seconds for both 10.31 and 16.078 MHz. Figures 5-3 and 5-4 show the spectral sweeps for selected times for the two The signal spikes appear in pairs because of the imaging frequencies. of the spectral components about the folding frequency of 10 Hz. The signal amplitudes are subject to nonuniform weighting in frequency imposed by the method of sampling. The weighting function is sin X/X where X is equal to  $\omega \tau / 2$  while  $\omega$  is the angular frequency and au is the sampling time. The amplitudes scaled from the spectra are corrected for the nonuniform response. A test signal injected into the receiver at the operating frequency in 5 dB steps from a reference power level is used for calibrating the amplitude scale. Figure 5-5 shows the calibration curves constructed for 10.31 and 16.078 MHz for converting the arbitrary amplitude readings to absolute signal power.







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Figure 5-3 Selected Scans of the Amplitude Spectra of the Signal at F = 10.31 MHz for Test Mulberry. (The Folding of the Spectral Components Lying Outside the Unambiguous Doppler Window Causes Images to Appear on the Display.)



Figure 5-4 Selected Scans of the Amplitude Spectra of the Signal at F = 16.078 MHz for Test Mulberry. (The Folding of the Spectral Components Lying Outside the Unambiguous Doppler Window Causes Images to Appear on the Display.)



Figure 5-5 The Calibration Curves Used to Convert the Arbitrary Units of Amplitude to Absolute Signal Power

The amplitude and power plots for the two frequencies are presented in Figures 5-6 and 5-7. The dashed horizontal lines shown on the plots correspond to the average noise level and the minimum detectable signal level which is arbitrarily set at one standard deviation above the noise level. The systematic fading observed in the signal amplitude is considered as due to the interference between the ordinary and extraordinary modes of the echo. The power plots are constructed from the envelopes of the amplitude curves and hence represent the sum of the powers returned in the two modes.

# 5.3 <u>RESULTS</u>

The power measurements of the received signal are converted to the scattering cross sections of the plasma cloud using the radar equation

$$\sigma = \frac{64 \pi^{3} R_{1}^{2} R_{2}^{2} P_{r}}{P_{t} G_{t} G_{r} \lambda^{2}}$$
(5-1)

The parameters of Equation 5-1 are the same as defined in paragraph 4.1.1. The gains  $G_t$  and  $G_r$  include the system losses and are given as  $(g_t \gamma_t)$  and  $(g_r \gamma_r)$  where g's and  $\gamma$ 's represent respectively the antenna gains and the efficiency factors. The system parameters used to calculate the scattering cross sections are listed in Table 5-1.

### TABLE 5-1

SYSTEM PARAMETERS

| $\lambda$ (Meters) | P <sub>t</sub> (Watts) | gt   | a <sup>r</sup> | $\gamma_t$ | $\gamma_r$ |
|--------------------|------------------------|------|----------------|------------|------------|
| 18.66              | $1.24 \times 10^4$     | 4.60 | 6.31           | 0.295      | 0.617      |
| 29.40              | $1.50 \times 10^4$     | 3.70 | 4.39           | 0.490      | 0.414      |



Figure 5-6 The Amplitude (Arbitrary Scale) and the Power Variations of the Signal at 10.31 MHz. The Power Curve is Constructed from the Envelope of the Amplitude Plot. The Horizontal Dashed Lines Indicate the Average Noise and the Minimum Detectable Signal Levels.



Figure 5-7 The Amplitude (Arbitrary Scale) and the Power Variations of the Signal at F = 16.078 MHz. The Power Curve is Constructed from the Envelope of the Amplitude Plot. The Horizontal Dashed Lines Indicate the Average Noise and the Minimum Detectable Signal Levels.

The antenna gains in the direction of the cloud for the deltas are obtained by computing the patterns for the configurations used in the experiments. An estimate of 8 dB is adopted, however, for the log periodic antenna. The efficiency factors  $\gamma_{t}$  and  $\gamma_{r}$  account for the cable and impedance mismatch losses. The ranges  $R_1$  and  $R_2$  to the reflection point of the cloud from the transmitter and the receiver are taken from the results of the ray tracing program. Figure 5-8 shows how the ranges vary with time as the reflection point moves out and then recedes toward the center of the cloud. The scattering cross sections, calculated on the basis of the above parameters and the power measurements of the received signals, are presented for the two frequencies in Figures 5-9 and 5-10 along with the Doppler information read out of the amplitude spectra. The minimum detectable cross section  $\sigma_{\min}$  is also indicated on the plots and it is about  $3 \times 10^3 \text{ m}^2$  for 10.31 MHz and 4.4 x  $10^2 \text{ m}^2$  for 16.078 MHz. The initial maximum observed in the scattering cross sections on the two frequencies is believed to be due to thermal ionization that appears immediately on release. The following minimum which was reported to be more pronounced at higher frequencies is caused apparently by the decay of the thermal ionization before the photoionization builds up significantly. The maximum that is associated with the photoionization occurs at about 110 seconds for 10.31 MHz and 50 seconds for 16.078 MHz. The observed Doppler behavior is characteristic of an expanding cloud with the rate of expansion decreasing continuously with time. Further discussion of the results is deferred to the next section where they are compared with those synthesized by ray tracing through Gaussian clouds.



Figure 5-8 The Variation With Time Of The Ranges R<sub>1</sub> and R<sub>2</sub> To The Reflection Point Respectively From The Transmitter And Receiver



Figure 5-9 Time History of the Doppler Shift and the Scattering Cross-Section Derived from the HF Measurements at F = 10.31 MHz



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Figure 5-10 Time History of the Doppler Shift and the Scattering Cross-Section Derived from the HF Measurements at F = 16.078 MHz

SECTION 6. COMPARISON BETWEEN EXPERIMENTAL AND RAY TRACING RESULTS

The time dependent Gaussian model adopted for the ray tracing, while permitted to change its origin from one time to another on the basis of the optical trajectory data, had been kept stationary at any given time as the rays were traced. Since the cloud was observed to drift continuously in position, there is a Doppler component associated with this bodily motion which should be added to that computed for the expanding stationary cloud to allow a comparison between the theory and the observations. A computer program is available which calculates the drift Doppler when the coordinates of the cloud as a function of time and the operating frequency are given. Figure 6-1 shows the drift Dopplers as function of time at 10.31 and 16.078 MHz for the test Mulberry. Using these values, the computed Dopplers have been



Figure 6-1 The Doppler Shift Associated With the Drift of the Plasma Cloud for F = 10.31 and 16.078 MHz

corrected and are presented along with the scattering cross sections and the corresponding experimental results in Figures 6-2 and 6-3. The synthesized curves of the extraordinary mode are selected for comparison since they represent the actual conditions at the time of the signal drop-out which is of maximum importance. There is an apparent discrepancy in the cutoff times indicated by the experimental and the synthesized curves. This seems to be due to the fact that the parameters, the total ion content and the diffusion coefficients, which determine the lifetime of the cloud for different operating frequencies have been kept constant in ray tracing synthesis where in fact they change with time. The discrepancy can be removed by adjusting the time scales of the synthesized curves to match with that of the experimental curves. The adjustment is not made, however, in Figures 6-2 and 6-3.

The Doppler and the scattering cross section synthesized by ray tracing are found to differ quite significantly from those measured experimentally. The differences are consistent for both the operating frequencies, 10.31 and 16.078 MHz. The most important difference in the Doppler behavior is that the synthesized Doppler based on a Gaussian model has a tail at the time of signal drop-out which is not experimentally observed. It has been speculated that the signal might be below the level of system sensitivity and could have been lost in the background noise at the time when the Doppler tail is expected to be seen. The estimated minimum detectable cross section  $\sigma_{\min}$  and the ray tracing results, however, clearly show that the signal level is above the system sensitivity and the doppler tail should have been observed if the distribution were truly Gaussian. Even if  $\sigma_{\min}$ 



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Figure 6-2 Comparison Between The Experimental And The Synthesized Time Histories Of The Doppler Shift And The Scattering Cross Section At F = 10.31 MHz



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Figure 6-3 Comparison Between the Experimental And The Synthesized Time Histories Of The Doppler Shift And The Scattering Cross Section At F = 16.078 MHz

should be detectable over a significant portion of the Doppler tail. Since the uncertainties in the system losses are not likely to be greater than 20 dB, the ray tracing results lead to the conclusion that the electron density distribution is unlike Gaussian during the late time evolution of the cloud. Considering the general behavior, the experimental Doppler is found to be consistently greater than that synthesized. It was noted earlier from a comparison of the Dopplers by hard ellipsoid and ray tracing methods that the effect of the 'softness' of the cloud is to contribute some positive Doppler. In analogy to that, the comparison between the experimental and the ray tracing Doppler suggests that the cloud is softer than that implied by the adopted Gaussian distribution. The scattering cross sections synthesized by ray tracing are 10 to 20 dB greater than those derived from the experimental data. Since the uncertainties in antenna gains and system losses are not likely to add up to this magnitude, the true cross sections of the cloud seem to be lower than that predicted by the Gaussian model. This suggests that the cloud is softer than the Gaussian causing a greater defocusing and thereby a reduction in the cross section which is consistent with the Doppler behavior. The general trend in the variation with time is such that the experimental cross sections hold up closer to the peak for longer time than the synthesized. This could happen if the expansion phase of the plasma frequency contour supporting the reflection lasts longer than that associated with the Gaussian model. The defocussing effects of the underlying ionization which build up in time are expected to offset to some extent the increase in the cross section associated with the extended phase of expansion and thus can lead to the observed slow variation. It emerges from the comparison that the true distribution of the cloud tends to become flatter in the sense that the density falls off much more gradually from the center than that in the adopted Gaussian model as the time progress towards the signal drop-out.

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## SECTION 7. SUMMARY AND CONCLUSIONS

A three dimensional ray tracing program has been used to synthesize hf radar signatures from Gaussian plasma clouds. The prime objective of the investigation is to test the validity of the assumed Gaussian model by comparing the synthesized signatures with the experimental observations. The ray tracing results have been compared also to that computed for the case of a hard expanding ellipsoid model to study the effects of the ionization lying below the level of reflection.

The 3D ray tracing program used in this study has been developed at ESSA by Dr. R.M. Jones and is based on a set of six partial differential equations similar to that of Haselgrove (1954). The program can take the electron collisions and the Earth's magnetic field into account and trace ray paths for both ordinary and extraordinary modes.

The Gaussian distribution of electron (ion) density in the plasma cloud used for synthesizing the radar signatures is based on the ambipolar diffusion model given by Holway (1965). The Gaussian parameters adopted for the synthesis are that appropriate to the test Mulberry of Pre-SECEDE series conducted at White Sands, New Mexico (Minkoff, 1970).

The ray tracing method of synthesizing a radar signature from the cloud involves first the determination of the 'homing' ray when the transmitter-cloud-receiver configuration is given. The Doppler shift of interest is the one associated with this ray and it is recorded. The next step is to evaluate the scattering cross section of the cloud which has been done by following the technique described by Croft (1967) and Georges and Stephenson (1969). It involves transmission of a narrow bundle of rays and the determination of the area

of their impact on the ground. The radar signature synthesis by the hard ellipsoid method involves the determination of the specular point from the radar. A method to find the specular point on the cloud and to evaluate the Doppler shift and the scattering cross section has been described.

The experimental data for which the ray tracing simulation has been made was collected by operating hf phase path sounders at 10.31 and 16.078 MHz during test Mulberry of Pre-SECEDE series. The data has been reduced to the form of power spectra to measure the Doppler shifts and to estimate the radar scattering cross sections of the cloud.

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The following conclusions can be drawn from the foregoing study of the synthesized and the observed radar signatures from the plasma clouds:

The radar signatures synthesized by ray tracing for the Gaussian plasma clouds are found to be significantly different from those observed experimentally. The synthesized Doppler shifts are somewhat lower and reveal a negative tail in contrast to the observed Doppler behavior. The scattering cross sections, however, are 10 to 20 dB greater than those derived from the observations. These differences tend to suggest that the electron density variation outward from the center of the cloud is more gradual than that in the adopted Gaussian model.

The comparison between the signatures synthesized by the ray tracing and the hard ellipsoid model shows that the effect of the ionization below the reflection level is to introduce a significant positive shift in Doppler and a considerable reduction in the scattering cross section by way of defocusing. The factor by which the scattering cross section is reduced is found to vary from about 3 at the time

cf Peak cross section to 30 just prior to the signal dropout. It is, therefore, concluded that a simple hard ellipsoid model is inadequate for a satisfactory synthesis of hf radar signatures.

# APPENDIX A. GAUSS X ROUTINE AND SAMPLE RAY TRACE

The subroutine Gauss X listed here calculated the Appleton Parameter X (=  $f_n^2/f^2$ ) and its time and spatial derivatives in geomagnetic dipole coordinate system. The table that follows the routine shows the sample printout of the ray tracing program. The results are for the homing extraordinary ray at the operating frequency of 10.31 MHz and at the time 180 seconds after the release of the cloud. Figure A-l shows the corresponding ray plot in the vertical plane defined by the line joining the transmitter and the receiver. The portion of the ray path within the cloud where there is significant bending is shown alongside on an enlarged scale.

| 1  | SUBROUTINE GAUSSX                                                            |
|----|------------------------------------------------------------------------------|
| 2  | DATA PI/3.14159265/                                                          |
| 3  | REAL NO.K. I.N.D(15) NLO.NLN                                                 |
| 4  | COMMON R(6)/WW/1 <sub>D</sub> (14) <sub>*D</sub> UM*W(400)/XX/X*PXPR(3)*PXPT |
| 5  | EQUIVALENCE (F, W(3)), (PHN+W(13)), (THN+W(15)), (RE+W(19)), (NO+W(201)      |
| 6  | 1), (T, w(202)), (TAU, w(203)), (H0, w(204)), (DR, w(205)), (D2, w(206)),    |
| 7  | 2(K,W(207)),(THO,W(208)),(PHO,W(209)),(1,W(210)),(H,H(211))                  |
| 8  | ENTRY ELECTX                                                                 |
| 9  | 1F(W(3011.GT.0.) GO TO 1                                                     |
| 10 | w(301)=1.                                                                    |
| 11 | KCUSQ#HD*+2+4++DR+T                                                          |
| 12 | ZCO=5QRT(H0++2+4.+DZ+T)                                                      |
| 13 | <u>CTHMD=SIN(THU)+SIN(THN)+COS(THO)+COS(THN)+COS(PHO+PHN)</u>                |
| 14 | STHMD=SQRT(1+DD=CTHMO++2)                                                    |
| 15 | SPHMO=CQS1THU)+ <u>Sin1PhO</u> =PHN1/STHMO                                   |
| 16 | CPHND=SQRT(1+DD=SPHMD++2)                                                    |
| 17 | XMO#(RE+H) #STHMD#CPHMD                                                      |
| 18 | YMO≖(RE+H)#STHM0#SPHM0                                                       |
| 19 | 7MD=(RE+H) #CTHHD                                                            |
| 20 | CHIMU=PI/2.=I+ACOS(CTHMO)                                                    |
| 21 | CCHIMB=COSICHIMD1                                                            |
| 22 | SCHIMD=SIN(CHIMD)                                                            |
| 23 | CPCX=CPHMD+CCH1MD                                                            |
| 24 | SPCX=SPHMU+CCH1MD                                                            |
| 25 | CPSX=CPHMO+SCH1MO                                                            |

| 26  | SPSX#SPHMD+SCHIMD                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  |
|-----|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| 27  | FT=(1e=EXP(=T/TAU))/(2CO+RCDSQ)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    |
| 28  | DFDT=1./(TAU+ZCO+RCDSQ )-FT+(1./TAU+4.+DR/RCDSQ+2.+D2/ZCO++2)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      |
| 29  | CONST K/F . 2                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      |
| 30  | CNST1=NO/P1*+1.5                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |
| 31  | CNST2=CONST*CNST1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  |
| 32  | 1 CR2=COS(R(2))                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    |
| 33  | SR2#SIN(R(2))                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      |
| 34  | CR3=COS(R(3))                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      |
| 35  | SR3#SIN(R(3))                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      |
| 36  | XM=R(1)*SR2*CR3                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    |
| 37  | YM#R(1) + SR2#SR3                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  |
| 38  | ZM*R(1) + CR2                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      |
| 39  | XC=CPCX+(XM=XMO)+SPCX+(YM=YHO)=SCH1MO+(ZM+ZMO)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |
| 40  | YC=-SPHMO+(XM-XMO)+CPHHO+(YM-YMO)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  |
| 41  | $zc=cpsx \bullet (xm-xho) + spsx \bullet (Ym-Ymo) + cchimo + (zm-zmo)$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |
| 42  | GT=EXP(-(xc++2+Yc++2)/RCOSQ)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |
| 43  | HT=EXP(-(ZC/ZCO)++2)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               |
| 44  | N=CNST1=FT=GT=HT                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |
| 45  | X=CONST+N                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |
| 46  | D(10)==N#2·*XC/RCOSW                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               |
| 47  | $D(11) = N \bullet 2_2 \bullet Y C / R C O S Q$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    |
| 48  | D(12)==N*2+*ZC/ZCD+*2                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |
| 49  | $D(13)=CPC_X+D(10)=SPHM0+D(11)+CPSX+D(12)$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |
| 50  | D(14)=SPCX+D(1n)+CPHMO+D(11)+SPSX+D(12)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |
| 51  | D(15) = SCH1HD + D(1D) + CCH1HD + D(12)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |
| 52  | D(1)*SR2*CR3                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |
| 53  | D(2) = R(1) + CR2 + CR3                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |
| 54  | D(3)==R(1)=SR2=SR3                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |
| _55 | D(4)=SR2+SR3                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |
| 56  | D(5)=R(1)+CR2+SR3                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  |
|     |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    |
| 57  | n(6) = R(1) + 5R2 + cR3                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |
| 58  | n(7)=rR2                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |
| 59  | D(8)==R(1)=SR2                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |
| 60  | c D(9)=0.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |
| 61  | PyPR(1)=CONST (0(13)+0(1)+0(14)+0(4)+0(15)+0(7))                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |
| 62  | $PXPR(2) \neq ConSte(0(13) + D(2) + D(14) + D(5) + D(15) + D(8))$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  |
| 63  | PXPR(3)#CONSTC(D(13)+D(3)+D(3)+D(4)+D(4)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |
| 64  | D(2) = GT = 4 + OR = ( (xC = 2 + YC = 2) / RCD = 2)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |
| 65  | D(3)#HT#4.0DZ#(2C/2CD##2)##2                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |
| 66  | PXPT#CNST2#(GT+HT+DFDT+FT+HT+D(2)+FT+GT+D(3))                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      |
| 67  | nnin sistema nya salahan anakana ang kanakana kanakana kanakana kanakana kanakana                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  |
| 68  | END                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |
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Figure A-1 A Sample Ray Trace Projection Plot In A Vertical Plane Defined By The Line Joining The Transmitter And The Receiver. The Boxed Segment Where The Ray Suffers Significant Bending Is Shown On An Enlarged Scale

# APPENDIX B. A VECTOR METHOD TO CALCULATE CLOUD TRAJECTORY

The vector method described below determines the coordinates of the cloud using the line of sight data given in azimuth and elevation angles from a pair of observing stations. The cloud position is defined ideally by the intersection point of the lines of sight from the two sites. In practice, however, slight errors in sighting cause the two lines to miss each other and in this case the midpoint of the common perpendicular to the two lines of sight is taken to be the best estimate for the cloud position.

Let I and J be the unit vectors along the two lines of sight and N be the unit vector along the common perpendicular to the two lines such that

$$\vec{N} = \frac{\vec{I} \times \vec{J}}{\left|\vec{I} \times \vec{J}\right|}$$
(B-1)

 $\vec{R_1}$  and  $\vec{R_2}$  represent the vectors to the two observing sites from the center of the earth;  $\vec{X}$  denote the vector to the cloud center.  $B_1$  and  $B_2$  are the scalar distances from the two sites to the points joined by the common perpendicular. D is the distance between the two lines along the perpendicular. Then from the geometry shown in Figure B-1 we have:

$$\vec{R}_1 + B_1 \vec{I} + \frac{D}{2} N = \vec{X}$$
(B-2)

$$\vec{R}_2 + \vec{B}_2 \vec{J} - \frac{\vec{D}}{2} \vec{N} = \vec{X}$$
(B-3)

Taking the scalar product of Equations B-2 and B-3 with N and subtracting one from the other would result in the relation

$$(\overline{R_1} - \overline{R_2}) \cdot (\overline{N}) = D \tag{B-4}$$



Figure B-1 Geometry for the Vector Determination of the Cloud Coordinates

It is required now to evaluate either  $B_1$  or  $B_2$  to obtain the position vector  $\vec{X}$  of the cloud. This can be done, for example, by vector multiplication of Equations B-2 and B-3 with the unit vector  $\vec{I}$  which yields the following expression for  $B_2$  on making use of Equation B-1.

$$B_{2} | \vec{I} \times \vec{J} | \vec{N} = \vec{I} \times [\vec{R}_{1} - \vec{R}_{2}] - D[\vec{N} \times \vec{I}]$$
(B-5)

Using Equations B-4 and B-5, the vector  $\vec{X}$  can be expressed in terms of  $\vec{I}$ ,  $\vec{J}$ ,  $\vec{N}$ ,  $\vec{R}_1$  and  $\vec{R}_2$  which can be evaluated from the known quantities, the coordinates of the observing sites and the look angles to the cloud, as follows:

Let  $(\alpha_1, \phi_1)$  and  $(\theta_2, \phi_2)$  be the co-latitude and east longitude of the two stations in the geographic co-ordinate system. The azimuth and elevation angles to the cloud from the two stations are

denoted as  $\binom{\alpha}{1}$ ,  $\binom{\beta}{1}$  and  $\binom{\alpha}{2}$ ,  $\binom{\beta}{2}$ , respectively. Define two Cartesian coordinate systems, (x, y, z) an Earth centered system and  $(x_1, y_1, z_1)$ with its origin at one of the observing stations (say site 1) as shown in Figure B-2. (x, y, z) is such that z is pointed toward north and (x, z) defines the reference meridian plane.  $(x_1, y_1, z_1)$  is tilted with respect to (x, y, z) by  $\phi_1$  in longitude and  $(90 - \theta_1)$  in latitude.  $(\hat{1}, \hat{1}, \hat{k})$  and  $(\hat{1}_1, \hat{1}_1, \hat{k}_1)$  are the unit vectors along (x, y, z) and  $(x_1, y_1, z_1)$ , respectively. They are related by a transformation matrix as:



Figure B-2 The coordinate systems involved in the transformation of various vectors.(x, y, z) is an Earth centered system and  $(x_1, y_1, z_1)$  is centered at an observation site.

The unit vector  $\vec{I}$  along the line of sight from station 1 is given in  $(x_1, y_1, z_1)$  system in terms of the look angles as:

$$\vec{I} = \sin \beta_1 \quad \hat{i}_1 + \cos \beta_1 \sin \alpha_1 \quad \hat{j}_1 + \cos \beta_1 \cos \alpha_1 \quad \hat{k}_1 \quad (B-7)$$

substituting Equation B-6 into B-7 leads to:

$$I = (\sin \beta_{1} \sin \theta_{1} \cos \phi_{1} - \cos \beta_{1} \sin \alpha_{1} \sin \phi_{1} - \cos \beta_{1} \cos \alpha_{1} \cos \theta_{1})\hat{1} + (\sin \beta_{1} \sin \theta_{1} \sin \phi_{1} + \cos \beta_{1} \sin \alpha_{1} \cos \phi_{1} - \cos \beta_{1} \cos \alpha_{1} \cos \theta_{1} \sin \phi_{1})\hat{1} + (\sin \beta_{1} \cos \alpha_{1} \cos \theta_{1} \sin \phi_{1})\hat{1} + (\sin \beta_{1} \cos \theta_{1} + \cos \beta_{1} \cos \alpha_{1} \sin \theta_{1})\hat{k} = a_{1}\hat{1} + b_{1}\hat{1} + c_{1}\hat{k}$$

$$(B-8)$$

 $\vec{J}$ , the unit vector from the second site, can be similarly expressed; replacing the subscript 1 in Equation B-8 by 2 one gets:

$$J = a_2 \hat{i} + b_2 \hat{j} + c_2 \hat{k}$$
 (B-9)

From Equation B-1

$$\vec{N} = \begin{bmatrix} \hat{1} & \hat{j} & \hat{k} \\ a_1 & b_1 & c_1 \\ a_2 & b_2 & c_2 \end{bmatrix} \begin{bmatrix} \vec{I} & \vec{J} \\ \vec{I} & \vec{J} \end{bmatrix}^{-1} = N_1 \hat{1} + N_2 \hat{j} + N_3 \hat{k} \quad (B-10)$$

The vectors  $\overline{R_1}$  and  $\overline{R_2}$  are given in terms of the coordinates of the stations as

$$\vec{R}_{1} = R_{E} \left[ \sin \theta_{1} \cos \phi_{1} \hat{i} + \sin \theta_{1} \sin \phi_{1} \hat{j} + \cos \theta_{1} \hat{k} \right] (B-11)$$

 $R_2 = R_E (\sin \theta_2 \cos \phi_2 \hat{1} + \sin \theta_2 \sin \phi_2 j + \cos \theta_2 \hat{k}) (B-12)$ 

using Equations B-4, B-5, and B-8 to B-12, the position vector of the cloud can be expressed in the Earth centered coordinate system in the form:

$$\overline{X} = U\hat{1} + V\hat{j} + W\hat{k}$$
 (B-13)

Where U, V and W are functions of the parameters  $\theta_1$ ,  $\theta_2$ ,  $\phi_1$ ,  $\phi_2$ ,  $\alpha_1$ ,  $\alpha_2$ ,  $\beta_1$  and  $\beta_2$  and can be calculated. If h,  $\theta$ , and  $\phi$  denote the altitude, latitude and longitude of the cloud position, they are given as:

$$h = (U^{2} + V^{2} + W^{2})^{1/2} - R_{E}$$
  

$$\theta = s_{...}^{-1} (W(U^{2} + V^{2} + W^{2})^{-1/2})$$
  

$$\phi = tan^{-1} (V/U)$$

The method described here has been used to calculate the trajectory of the cloud shown in Figure 3-2.

## ACKNOWLEDGMENTS

We are grateful to Dr. R.M. Jones and Mrs. Judith J. Stephenson of ESSA for supplying us with a FORTRAN deck of the 3D ray tracing program and the instructions to use it. We would like to thank Tom Boak for adapting the program to Univac 1108, Dave Blood for the help in preparing the section on experimental results and Bill Russell for the assistance at the time of publication.

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