

**QUALITY AND RELIABILITY ASSURANCE
TECHNICAL REPORT**

TR 7

**FACTORS AND PROCEDURES FOR APPLYING
MIL-STD-105D SAMPLING PLANS TO LIFE
AND RELIABILITY TESTING**



D D C

MAY 2 1966

**CLEARER
FEDERAL
CIVILIAN**

— CSC 46 X

Code 1.24
21 MAY 1965

**OFFICE OF THE ASSISTANT SECRETARY OF DEFENSE
(INSTALLATIONS AND LOGISTICS)
WASHINGTON, D.C. 20301**



OFFICE OF THE ASSISTANT SECRETARY OF DEFENSE
WASHINGTON, D. C. 20301

INSTALLATIONS AND LOGISTICS

May 21, 1965

Factors and Procedures for Applying
MIL-STD-105D Sampling Plans to Life
and Reliability Testing

TR 7

Quality and Reliability Assurance

The content of this technical report was prepared by Professor Henry P. Goode of Cornell University under an Office of Naval Research contract. It was developed to meet a growing need for the use of mathematically sound sampling plans for life and reliability testing where the Weibull Distribution adequately approximates the test data.

The report is reproduced as a DoD Quality and Reliability Assurance Technical Report to permit ready dissemination of this material to Government and Industry personnel engaged in life and reliability testing.

FACTORS AND PROCEDURES FOR
APPLYING THE MIL-STD-105D PLANS IN
LIFE AND RELIABILITY INSPECTION

Summary

This report presents a procedure and related tables of factors for adapting the MIL-STD-105D sampling plans to acceptance sampling inspection when the item quality of interest is life length or reliability. Factors are provided for three alternative criteria for lot evaluation; mean life, hazard rate, and reliable life. Inspection of the sample is by attributes with testing truncated at the end of some preassigned period of time. The Weibull distribution, together with the exponential distribution as a special case, is used as the underlying statistical model.

Introduction

The procedure and tables presented in this report are based on recent work on the use of the Weibull distribution in acceptance sampling inspection. Details of this work, together with tables of sampling plans of other forms, have been published previously.^{(1),(2),(3)} However, with the introduction of the MIL-STD-105D Sampling Procedures and Tables the publication of tables of new factors for applying these new standard plans to life and reliability applications seemed to be a useful thing to do. Since the basic computations required have already been made, it has been quite easy to provide these new factors. No changes in method or details of application have been made over those described in the publications referenced above. For this reason the text portion of this report has been briefly written. Readers interested in further details are referred to these previous publications. Other sources of material on the underlying theory and approach are also available.^{(4),(5),(6)}

The Acceptance-Sampling Procedure

The procedure to be employed is essentially the same as the one normally used for attribute sampling inspection. The only difference is that sample items are tested for life or survival instead of for some other property. For single-sampling, the following are the required steps:

- (a) Using the tables of factors provided in this report, select a suitable sampling inspection plan from those tabulated in MIL-STD-105D.
- (b) Draw at random a sample of items of the size specified by the selected MIL-STD-105D plan.
- (c) Place the sample of items on life test for the specified period of time, t .
- (d) Determine the number of sample items that failed during the test period.
- (e) Compare the number of items that failed with the number allowed under the selected MIL-STD-105D plan.
- (f) If the number that failed is equal to or less than the acceptable number, accept the lot; if the number failing exceeds the acceptable number, reject the lot.

Note that both the sample sizes and the acceptance numbers used are those specified by the MIL-STD-105D plans. It will be assumed in the discussion and examples that follow that single-sampling plans will be used. However, the matching double-sampling and multiple-sampling plans provided in the 105D Standard can be used if desired. The corresponding sample sizes and acceptance and rejection numbers are employed in the usual way. The specified test truncation time, t , must be employed for all samples.

The probability of acceptance for a lot under this procedure depends only on the probability of a sample item failing before the end of the test truncation time, t . For this reason the actual life at failure need not be determined; only the number of items failing is of interest. It should be noted also that life requirements and test time specifications need not necessarily be measured in chronological terms such as minutes or hours. The life measure may be cycles of operation, revolutions, or miles of travel, for example.

Statistical Assumptions

The underlying lifelength distribution assumed is the Weibull distribution together with the exponential distribution as a special case of the Weibull. The Weibull distribution is a three parameter distribution. One parameter is a scale, or characteristic life parameter. For these plans and procedures the value for this parameter need not be known; the techniques

employed are independent of its magnitude. A second parameter is a location or "guaranteed life" parameter. In these plans and procedures it is assumed that this parameter has a value of zero; that there is some risk of item failure right from the start of life. If this is not the case for some application, a simple modification in procedure is available.

The third Weibull parameter, and the one of importance, is the shape parameter. The magnitude of the conversion factors used in the procedures described in this report depend directly on the value for this parameter. For this reason the magnitude of the parameter must be known through experience with the product or must be estimated from past research, engineering, or inspection data. Estimation procedures are available and are outlined in Reference (1). For the common case of random chance failures with the failure rate constant over time rather than failures due to "infant mortality" or wearout, a value of 1 for the shape parameter should be assumed. With this parameter value, the Weibull distribution reduces to the exponential. Tables of conversion factors are provided for ten selected shape parameter values ranging from $\frac{1}{2}$ to 4, the range commonly encountered in industrial and technical practice. The value 1 used for the exponential case is included. Factors for other required shape parameter values within this range may be obtained approximately by interpolation. A more complete discussion of the relationship between failure patterns and the Weibull parameters will be found in References (1), (2), and (3).

Mean Life Conversion Factors

One possible acceptance criterion is the mean life for items making up the lot (symbolized by the letter μ). Mean life conversion factors or values for the dimensionless ratio $100t/\mu$ have been determined to correspond to or replace all the p' or percent defective values associated with the 105D plans. In this factor the letter t represents the specified test truncation time and the letter μ the mean item life for the lot. For reliability or lifelength applications, these factors are used in place of the corresponding p' values normally employed in the use of the 105D plans for attribute inspection of other item qualities. The use of these factors will be demonstrated by several examples.

Table IA lists for each selected shape parameter value $100t/\mu$ ratios for each of the 105D Acceptable Quality Level [$p'(\%)$] values. With acceptance inspection plans selected in terms of these ratios, the probability of

acceptance will be high for lots whose mean life meets the specified requirement. The actual probability of acceptance will vary from plan to plan and may be read from the associated operating characteristic curves supplied in the 105D Standard. The curves are entered by using the corresponding $p'(\%)$ value. Table 1B lists $100t/\mu$ ratios at the Limiting Quality Level for the quality level at which the Consumer's Risk is 0.10. Table 1C lists corresponding $100t/\mu$ ratios for a Consumer's Risk of 0.05.

These ratios are to be used directly for the usual case for which the value for the Weibull location or threshold parameter (symbolized by the letter γ) can be assumed as zero. If γ is not zero but has some other known value, all that must be done is to subtract the value for γ from t to get t_0 and from μ to get μ_0 . These transformed values, t_0 and μ_0 , are then used in the employment of the tables and for all other computations. A solution in terms of μ_0 and t_0 can then be converted back to actual or absolute values by adding the value for γ to each.

Example (1)

A 105D acceptance sampling inspection plan is to be applied to incoming lots of product for which mean item life is the property of interest. An acceptable mean life of 2,000 hours has been specified and under the plan used lots with a mean life of this value or greater should have a high probability of acceptance. A testing truncation time of 250 hours has been specified. From past experience it has been determined that the Weibull distribution can be used as a lifelength model and a shape parameter value of $2\frac{1}{2}$ and a location or threshold parameter value of 0 can be assumed. Single sampling is to be employed. A sample of as many as 300 items or so can be tested at one time. An appropriate sampling inspection plan must be selected. Also, the consumer's risk under use of the selected plan must be determined.

Computation of the $100t/\mu$ ratio at the Acceptable Quality Level gives $100t/\mu = 100 \times 250/2,000 = 12.5$. Examination of the ratios in the column for a shape parameter of $2\frac{1}{2}$ in Table 1A discloses a value of 12.4 for an Acceptable Quality Level of 0.40 in $p'(\%)$ terms. A plan with this AQL is accordingly to be used. Reference now to the MIL-STD-105D indicates for Sample Size Code Letter M the sample size is 315; this value will accordingly be used. Examination of the Master Table for Normal Inspection (Single

Sampling) in the 105D Standard shows for Sample Size Code Letter M and an Acceptable Quality Level of 0.40, the Acceptance Number must be 3 and the rejection number 4. The acceptance procedure will thus be to draw at random a sample of 315 items and submit them to life test for 250 hours. At the end of that time the number that have failed will be determined. If 3 items or less have failed, the lot will be accepted; if 4 or more have failed, it will be rejected.

The consumer's risk at a probability level of 0.10 can be determined by use of Table 1B which gives $100t/\mu$ ratios at the Limiting Quality Level for the 0.10 risk value. For a shape parameter value of $2\frac{1}{2}$, a Sample Size Code Letter M, and an Acceptable Quality Level (AQL) of 0.40, the $100t/\mu$ ratio value is found to be 24. With $t = 250$, $100t/\mu = 24$ or $100 \times 250/\mu = 24$ which gives a value for μ of 1,040. Thus if the mean life for the items in the lot is 1,040 hours or less, the probability of acceptance will be 0.10 or less. If the lot quality for which the consumer's risk was 0.05 was desired instead, Table 1C might be used which gives ratios at the Limiting Quality Level for this risk value.

Example (2)

A MIL-STD-105D plan with Sample Size Code Letter F and an AQL of 4.0 has been specified for a product for which life length in terms of cycles of operation is the quality of interest. Acceptance is to be in terms of a mean life evaluation. The Weibull distribution can be assumed to apply with a shape parameter value of $\frac{2}{3}$ and a location parameter value of 0. Testing of sample items is to be truncated at 5,000 cycles. The operating characteristics in terms of mean life for this plan are required.

Reference to Table 1A which lists ratios at the Acceptable Quality Level gives a $100t/\mu$ value of .62 for an AQL of 4.0 and a shape parameter value of $\frac{2}{3}$. With $t = 5,000$, $100t/\mu = .62$ or $100 \times 5000/\mu = .62$ which gives $\mu = 810,000$. Thus if the mean item life for the lot is 810,000 or more the probability of acceptance will be high. Reference to Table 1C which gives ratios at the Limiting Quality Level for a consumer's risk of 0.05, provides a $100t/\mu$ value of 14 for Code Letter F, an AQL of 4.0, and a shape parameter value of $\frac{2}{3}$. Thus $100 \times 5,000/\mu = 14$ or $\mu = 36,000$. If mean item life for the lot is 36,000 cycles or less, the probability of acceptance will be 0.05 or less.

The sample size and acceptance number will be those specified by MIL-STD-105D for Code Letter F and an AQL of 4.0. For single sampling the sample size will be 20 items and the acceptance number 2. For this example, as in all cases, the matched 105D double-sampling and multiple-sampling plans may be elected instead. No additional changes in procedure are required. The specified test time, which in this case is 5,000 cycles, must be employed for all samples.

Example (3)

In another application it can be assumed the Weibull distribution applies with a shape parameter β value of $3\frac{1}{3}$ and a location or threshold parameter value, γ , of 3,000 hours. An 105D acceptance-inspection plan must be selected under which the probability of acceptance will be low (0.05 or less) if mean item life is 8,000 hours or less. The sample size will be kept large to reduce the testing period time but it cannot exceed 250 items. To further reduce testing time an acceptance number of 0 will be used. The required test truncation time must be determined; also, the Acceptable Quality Level.

Reference to MIL-STD-105D indicates the Code Letter L with a sample size of 200 items must be used. With this Code Letter and an acceptance number of 0, the AQL in 105D terms must be 0.065. Subtraction of the threshold parameter value, γ , of 3,000 hours from the required mean value, μ , of 8,000 hours gives as a converted value for the mean $\mu_0 = 8,000 - 3,000 = 5,000$ hours. This converted value must now be used in working with the tables of factors. Use of Table IC for $\beta = 3\frac{1}{3}$, Code Letter L, and an AQL of 0.065 gives a $100t/\mu$ value of 31 at the Limiting Quality Level [for $P(A) = 0.05$]. With $\mu_0 = 5,000$, $100 t_0/\mu_0 = 100 t_0/5,000 = 31$ or $t_0 = 1,550$ hours. Conversion of this to absolute terms gives $t = t_0 + \gamma = 1,550 + 3,000 = 4,550$ hours as the required test truncation time.

From Table IA the corresponding ratio at the Acceptable Quality Level may be found. For an AQL of 0.065 and $\beta = 3\frac{1}{3}$, it is 12.3. Thus $100 t_0/\mu_0 = 12.3$ or $100 \times 1,550/\mu_0 = 12.3$ or $\mu_0 = 12,600$. Converting this to absolute terms gives $\mu = \mu_0 + \gamma = 12,600 + 3,000 = 15,600$. Thus the mean item life for a lot must be 15,600 hours or more for its probability of acceptance to be high.

Hazard Rate Conversion Factors

Another measure of lot quality is hazard rate or instantaneous failure rate, symbolized by the letters $Z(t)$, at some specified period of time, t . Hazard rate conversion factors or values for the dimensionless product $100 + Z(t)$ have been determined for all of the p' values that characterize the collection of 105D plans. As for the mean life plans, these products may be used in place of the corresponding p' values when using the 105D plans for life length and reliability applications.

Table 2A lists for each selected value for the shape parameter $100 + Z(t)$ products for each 105D Acceptable Quality Level value. Table 2B lists corresponding $100 + Z(t)$ products at the Limiting Quality Level for a consumer's risk of 0.10. Table 2C lists products at the Limiting Quality Level for a consumer's risk of 0.05. Use of these tables of factors is similar to the method of use for the mean life ratios including the variation in method required when some non-zero value for the location or threshold parameter must be assumed.

One point of difference should be noted. This is that the products are for direct application only in cases for which the time t at which the hazard rate is specified or is to be evaluated is the same as the time t at which the lifetesting of sample items is to be truncated. However, a table of Hazard Rate Ratios has been prepared, Table 2D, to use in a simple modification of method which allows the test truncation time to differ from the time at which the hazard rate is specified. All that must be done is to determine the hazard rate at the test truncation time which corresponds to the hazard rate at the specification time. Table 2D provides ratios for making this conversion. It gives for various values of t_2/t_1 , the corresponding values for the ratio $Z(t_2)/Z(t_1)$ for all the shape parameter values for which conversion values have been provided. If the test truncation time is shorter than the time for hazard rate specification, t_1 is used to represent the test truncation time and $Z(t_1)$ the corresponding hazard rate at that time. In this case t_2 represents the time of hazard rate specification and $Z(t_2)$ the specified hazard rate. If the test truncation is longer instead, the meanings given the subscripts 1 and 2 are simply reversed.

Example (4)

An acceptance-inspection plan must be selected from the 105D collection for an application for which the Weibull distribution applies and for which

it may be assumed the shape parameter value is $\frac{2}{3}$ and the location parameter value is 0. A hazard rate of no more than .0005 per hr. at 1,000 hours of life can be tolerated so a plan under which the probability of acceptance will be low (0.10) if this rate will be exceeded at this life is required. The test truncation time is likewise to be 1,000 hours.

Computation of the $100 + Z(t)$ product gives $100 \times 1,000 \times .0005 = 50$. Thus a plan must be used for which this product is found at the Limiting Quality Level for which the consumer's risk is 0.10. Examination of the column for $\beta = \frac{2}{3}$ in Table 2B discloses several close possibilities. One is for a plan with Code Letter D and an AQL of 1.5 for which the product is 48; another is Code Letter F and an AQL of 4.0 for which the product is likewise 48; still another is Code Letter G and an AQL of 6.5 for which the product is 53. Any of these will provide fairly closely the required consumer's protection.

The last plan mentioned with its relatively large sample size and acceptance number will discriminate most sharply between good and bad lots and hence provide the most reasonable Acceptable Quality Level. This will be achieved at the expense of a relatively large number of item hours of inspection, of course. With this choice (Code Letter G and an AQL of 6.5) the Acceptable Quality Level can be easily determined. Reference to Table 2A gives a value for $100 + Z(t)$ of 11.2 for an AQL of 6.5. Thus $100 \times 1000 Z(t) = 11.2$ or $Z(t) = .000112$; the "acceptable" hazard rate is .000112 (per hour). If, alternatively, Code Letter D and an AQL of 1.5 had been used, the "acceptable" hazard rate would be .0000252 (per hour) instead.

Example (5)

Suppose the selected plan must have an acceptable hazard rate (a rate for which the probability of acceptance is high) of .0001 per hour at 500 hours of life. However the testing of sample items must be truncated at 200 hours. A value of β of $\frac{2}{3}$ and for γ of 0 can be assumed. A 105D plan must be selected.

In this case use must be made of Table 2D. Letting $t_2 = 500$ and $t_1 = 200$, $t_2/t_1 = 500/200 = 2.5$. Reference to this table with this ratio using the $\beta = \frac{2}{3}$ column, shows $Z(t_2)/Z(t_1)$ to be .734. With $Z(t_2) = .0001$, $.0001/Z(t_1) = .734$ or $Z(t_1) = .000136$. This failure rate figure must be used in selecting the plan. Thus $100 + Z(t) = 100 \times 200 \times .000136 = 2.72$ (note that the testing truncation time of 200 hours is used as t at this

point). Reference to Table 2A examining the column for $\beta = \frac{2}{3}$ shows that a 105D plan with an AQL of 4.0% precisely meets this need.

Reliable Life Conversion Factor

A third possible reliability and lifelength measure for the items in a lot or population is reliable life (which will be symbolized by the letters p_r). Reliable life can be defined as the life beyond which some specified proportion of the items in the lot or population will survive. The letter r is used to represent this specified proportion.

Tables of conversion factors have been prepared for two different proportions, $r = .90$ and $r = .99$. As for the mean life case, these reliable life conversion factors have been prepared in the form of values for the dimensionless ratio $100 t/p_r$. Ratio values have been determined for all the $p'(\%)$ values associated with the MIL-STD-105D plans. Table 3A gives $100 t/p_r$ values at each of the Acceptable Quality Levels for $r = .90$; Table 4A gives corresponding values for $r = .99$. Table 5B gives ratio values at the Limiting Quality Level for a consumer's risk of 0.10 for $r = .90$; Table 4B gives corresponding values for a consumer's risk of 0.10 and $r = .99$. Table 3C gives ratio values at the Limiting Quality Level for a consumer's risk of 0.05 and for $r = .90$; Table 4C gives similar ratio values at a consumer's risk of 0.05 and for $r = .99$. These conversion ratios are used in the same manner that mean life ratios are used, including the manner for application when the location parameter is not zero. An example follows.

Example (6)

A sampling inspection plan must be selected for a product for which item life in terms of feet of travel is the quality of interest. Experience indicates the Weibull distribution will serve well as a statistical model with a shape parameter value of approximately $1\frac{1}{2}$ and with a location parameter of 0. A lot will be considered "acceptable" if the reliable life is 40,000 feet and the probability of acceptance for such lots should be high. For lots for which reliable life is 10,000 feet or less the probability of acceptance should be low, namely 0.05 or less. Reliable life is defined as the life beyond which 90% of the items will survive; that is, r is to be .90. Testing of sample items is to be truncated at 5,000 feet.

At the acceptable quality level the $100 t/p_r$ factor is $100 \times 5,000/40,000 = 12.5$. Examination of Table 3A shows that for $\beta = 1\frac{1}{2}$

the 100 t/p_r ratio for an AQL of 0.65 is 12.4 which is quite close to the desired ratio. Accordingly, a plan with this AQL is to be adopted. At the unacceptable or Limiting Quality Level the 100 t/p_r factor is $100 \times 5,000/10,000 = 50$. Reference to Table 3C which gives ratios at the Limiting Quality Level for $P(A) = 0.05$ shows that for Code Letter L, an AQL of 0.65 (which is required for this application, as indicated above), and $\beta = 1\frac{1}{2}$ the corresponding ratio is 48 which is close to the desired value of 50. Thus a 105D plan with Code Letter L and an AQL of 0.65 will meet the specified operating requirements. For single sampling the 105D Standard shows the sample size to be 200 items and the acceptance number 3.

Computation of the Conversion Factors

For the attribute acceptance procedure employed with these plans, the probability of acceptance for a lot depends only on the probability, p' , of item life being less than (or equal to) the test truncation time, t . With the magnitude of the shape parameter known, the magnitude of the location parameter taken as zero, and the value of test truncation time, t , pre-assigned, p' becomes a function only of the lot quality under evaluation (mean life, hazard rate, or reliable life). The means for the mathematical determination of the specific relationships are outlined below.

Evaluation in Terms of Mean Life (μ)

As noted, p' is a function of the test truncation time, t , and the mean item life, μ , for the lot. To make use of the MIL-STD-105D plans for mean life evaluation, it is necessary to find t and μ combinations equivalent to the p' (per cent defective) values associated with each of the 105D plans. To make the conversion factors available for general use rather than preparing them in terms of specific values of t and μ , the dimensionless ratio t/μ has been used (for ease in tabulation and use, 100 t/μ factors are provided).

The probability p' of an item failing prior to time t is the value of the cumulative density function at time t . For the Weibull distribution (with the location parameter equal to zero) this is given by,

$$p' = F(t) = 1 - \exp[-(t/\eta)^\beta] \quad (1)$$

where η is the scale or characteristic life parameter.

The formula for the mean of the Weibull distribution is,

$$\mu = \eta \Gamma(1/\beta + 1) . \quad (2)$$

By substitution of the value for η obtained from Equation (2) for η in Equation (1), the following equation is obtained,

$$p' = 1 - \exp\left\{-\left[\frac{t}{\mu} \Gamma(1/\beta + 1)\right]^\beta\right\} . \quad (3)$$

Solving for t/μ gives,

$$\frac{t}{\mu} = [-\ln(1-p')]^{1/\beta} / \Gamma(1/\beta + 1) . \quad (4)$$

Further details will be found in Reference (1) and Reference (4).

Evaluation in Terms of Hazard Rate [z(t)]

The instantaneous failure rate or the hazard rate at any specified time t , which is symbolized by $z(t)$, is given by the relationship,

$$z(t) = f(t)/[1-F(t)] , \quad (5)$$

where $f(t)$ is the population density function and $F(t)$ is the cumulative density function.

For the Weibull distribution (with the location parameter equal to zero) the expression for the population density function is,

$$f(t) = (\beta/\eta)(t/\eta)^{\beta-1} \exp[-(t/\eta)^\beta] \quad (6)$$

The expression for the cumulative density function is,

$$F(t) = 1 - \exp[-(t/\eta)^\beta] . \quad (7)$$

From Equations (6) and (7) the following expression for hazard rate may be obtained,

$$z(t) = (\beta/\eta)(t/\eta)^{\beta-1} . \quad (8)$$

A more useful form for the steps to follow is given if both sides of this equation are multiplied by (t/β) which gives,

$$\frac{tz(t)}{\beta} = (t/\eta)^\beta . \quad (9)$$

The probability, p' , of an item failing before the end of the testing time, t , is given by the cumulative density function, $F(t)$, as shown in Equation (7). By combining Equations (9) and (7), p' in terms of $Z(t)$ becomes,

$$p' = 1 - \exp[-\frac{tZ(t)}{\beta}] . \quad (10)$$

By transposing and taking the natural logarithm, the following required expression is found,

$$tZ(t) = -\beta \ln(1-p') . \quad (11)$$

Values for this dimensionless product, $tZ(t)$, may thus be found by use of this expression for all p' (per cent defective) values associated with the MIL-STD-105D plans. One should note that the time t at which the hazard rate is to be evaluated is the same as the test truncation time. Further details may be found in Reference (2) and Reference (5).

Evaluation in Terms of Reliable Life (ρ_r)

With the location parameter equal to zero, the value for reliable life, ρ_r , where r is the proportion of items surviving beyond a life of ρ_r , is given by the expression,

$$\rho_r = \eta (-\ln r)^{1/\beta} \quad (12)$$

The probability, p' , of an item failing prior to time t is given by,

$$p' = F(t) = 1 - \exp[-(t/\eta)] . \quad (13)$$

Substitution of the value for η given by Equation (12) for η in Equation (13) gives,

$$p' = 1 - \exp[-(t(-\ln r)^{1/\beta}/\rho_r)^{\beta}] .$$

This can be simplified to the following required form,

$$t/\rho_r = [\ln(1-p')/\ln(r)]^{1/\beta} .$$

Values for the dimensionless ratio t/ρ_r (actually, 100 t/ρ_r) have been determined for all the p' (percent defective) values associated with the MIL-STD-105D plans. Further details may be found in Reference (3) and Reference (6).

Bibliography

1. Quality Control and Reliability Technical Report TR3, Sampling Procedures and Tables for Life and Reliability Testing Based on the Weibull Distribution (Mean Life Criterion), Office of the Assistant Secretary of Defense (Installations and Logistics), U.S. Government Printing Office, September, 1961.
2. Quality Control and Reliability Technical Report TR4, Sampling Procedures and Tables for Life and Reliability Testing Based on the Weibull Distribution (Hazard Rate Criterion), Office of the Assistant Secretary of Defense (Installations and Logistics), U.S. Government Printing Office, February, 1962.
3. Quality Control and Reliability Technical Report TR6, Sampling Procedures and Tables for Life and Reliability Testing Based on the Weibull Distribution (Reliable Life Criterion), Office of the Assistant Secretary of Defense (Installations and Logistics), U.S. Government Printing Office, February, 1963.
4. Goode, Henry P. and Kao, John H.K., "Sampling Plans Based on the Weibull Distribution," Proceedings of the Seventh National Symposium on Reliability and Quality Control, 1961, pp. 24-40.
5. Goode, Henry P. and Kao, John H.K., "Sampling Procedures and Tables for Life and Reliability Testing Based on the Weibull Distribution (Hazard Rate Criterion)," Proceedings of the Eighth National Symposium on Reliability and Quality Control, 1962, pp. 37-58.
6. Goode, Henry P. and Kao, John H.K., "Weibull Tables for Bio-Assaying and Fatigue Testing," Proceedings of the Ninth National Symposium on Reliability and Quality Control, 1963, pp. 270-286.

TABLE 1A

100t/ μ Ratios at the Acceptable Quality Level (normal inspection)
for the MIL-STD-105D Plans

| Acceptable Quality Level $p'(\%)$ | Shape Parameter, β | | | | | | | | | |
|--|--------------------------|---------------|---------------|------|----------------|----------------|------|----------------|----------------|------|
| | $\frac{1}{3}$ | $\frac{1}{2}$ | $\frac{2}{3}$ | 1 | $1\frac{1}{3}$ | $1\frac{2}{3}$ | 2 | $2\frac{1}{2}$ | $3\frac{1}{3}$ | 4 |
| 0.010 | 17-12 | 50-8 | 75-6 | .010 | .11 | .45 | 1.13 | 2.83 | 7.03 | 11.0 |
| 0.015 | 56-12 | 11-7 | 14-5 | .015 | .15 | .57 | 1.38 | 3.32 | 7.94 | 12.2 |
| 0.025 | 26-11 | 31-7 | 30-5 | .025 | .22 | .77 | 1.78 | 4.08 | 9.26 | 13.9 |
| 0.040 | 11-10 | 80-7 | 60-5 | .040 | .31 | 1.02 | 2.26 | 4.93 | 10.7 | 15.6 |
| 0.065 | 46-10 | 21-6 | 13-4 | .065 | .44 | 1.37 | 2.88 | 5.98 | 12.3 | 17.6 |
| 0.10 | 17-9 | 50-6 | 25-4 | .10 | .61 | 1.78 | 3.57 | 7.11 | 14.0 | 19.6 |
| 0.15 | 56-9 | 11-5 | 44-4 | .15 | .83 | 2.26 | 4.37 | 8.36 | 15.8 | 21.7 |
| 0.25 | 26-8 | 31-5 | 94-4 | .25 | 1.22 | 3.08 | 5.64 | 10.3 | 18.5 | 24.7 |
| 0.40 | 11-7 | 80-5 | .019 | .40 | 1.73 | 4.07 | 7.14 | 12.4 | 21.3 | 27.8 |
| 0.65 | 46-7 | 21-4 | .040 | .65 | 2.50 | 5.46 | 9.12 | 15.1 | 24.6 | 31.4 |
| 1.0 | 17-6 | 51-4 | .076 | 1.01 | 3.45 | 7.08 | 11.3 | 17.9 | 28.0 | 34.9 |
| 1.5 | 59-6 | .011 | .14 | 1.51 | 4.69 | 9.07 | 13.9 | 21.1 | 31.7 | 38.7 |
| 2.5 | 27-5 | .032 | .30 | 2.53 | 6.91 | 12.3 | 18.0 | 25.9 | 37.0 | 44.0 |
| 4.0 | 11-4 | .083 | .62 | 4.08 | 9.88 | 16.4 | 22.8 | 31.4 | 42.7 | 49.6 |
| 6.5 | 51-4 | .23 | 1.31 | 6.72 | 14.4 | 22.2 | 29.3 | 38.3 | 49.6 | 56.2 |
| 10 | .019 | .56 | 2.57 | 10.5 | 20.1 | 29.0 | 36.6 | 45.8 | 56.7 | 62.9 |

The negative figure after a ratio shows the number of decimal points to provide. Thus 13-4 = .0013.

TABLE 1B

100t/ μ Ratios at the Limiting Quality Level
for the MIL-STD-105D Plans - Consumer's Risk = 0.10

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|------|--------------------------|---------------|---------------|-----|----------------|----------------|-----|----------------|----------------|-----|
| | | $\frac{1}{3}$ | $\frac{1}{2}$ | $\frac{2}{3}$ | 1 | $1\frac{1}{3}$ | $1\frac{2}{3}$ | 2 | $2\frac{1}{2}$ | $3\frac{1}{3}$ | 4 |
| A | 6.5 | 25 | 68 | 92 | 120 | 120 | 118 | 118 | 116 | 115 | 115 |
| B | 4.0 | 7.2 | 29 | 50 | 77 | 89 | 95 | 98 | 100 | 102 | 103 |
| C | 2.5 | 1.6 | 10 | 23 | 46 | 61 | 70 | 77 | 82 | 88 | 91 |
| C | 10 | 11 | 40 | 62 | 89 | 100 | 102 | 103 | 105 | 106 | 106 |
| D | 1.5 | .38 | 4.1 | 11.6 | 28 | 43 | 53 | 60 | 68 | 76 | 80 |
| D | 6.5 | 2.4 | 13 | 28 | 53 | 67 | 76 | 81 | 86 | 91 | 94 |
| D | 10 | 7.2 | 20 | 50 | 77 | 89 | 95 | 98 | 100 | 102 | 103 |
| E | 1.0 | .094 | 1 | 5.6 | 17 | 30 | 39 | 47 | 56 | 66 | 71 |
| E | 4.0 | .49 | 4.0 | 13 | 31 | 45 | 55 | 63 | 70 | 78 | 82 |
| E | 6.5 | 1.5 | 10 | 22 | 45 | 59 | 68 | 76 | 80 | 86 | 90 |
| E | 10 | 3.5 | 17 | 37 | 60 | 73 | 82 | 87 | 90 | 95 | 97 |
| F | 0.65 | .026 | .66 | 2.9 | 11 | 22 | 30 | 38 | 47 | 58 | 64 |
| F | 2.5 | .14 | 2.0 | 6.7 | 20 | 33 | 42 | 50 | 58 | 68 | 72 |
| F | 4.0 | .36 | 4.0 | 11 | 28 | 42 | 52 | 59 | 67 | 75 | 80 |
| F | 6.5 | .80 | 6.5 | 16 | 36 | 51 | 61 | 68 | 73 | 81 | 85 |
| F | 10 | 2.6 | 14 | 29 | 54 | 68 | 77 | 82 | 87 | 92 | 95 |
| G | 0.40 | 62-4 | .26 | 1.4 | 7.2 | 15 | 23 | 30 | 39 | 50 | 57 |
| G | 1.5 | .032 | .76 | 3.2 | 12 | 22 | 31 | 39 | 48 | 59 | 65 |
| G | 2.5 | .086 | 1.4 | 5.3 | 17 | 29 | 38 | 47 | 55 | 65 | 70 |
| G | 4.0 | .18 | 2.4 | 7.7 | 22 | 35 | 45 | 53 | 60 | 70 | 74 |
| G | 6.5 | .52 | 5.0 | 13 | 31 | 46 | 56 | 63 | 70 | 78 | 82 |
| G | 10 | 1.2 | 8.8 | 20 | 42 | 57 | 66 | 73 | 78 | 85 | 89 |
| H | 0.25 | 16-4 | .11 | .74 | 4.6 | 11 | 17 | 24 | 33 | 44 | 51 |
| H | 1.0 | 84-4 | .31 | 1.6 | 7.8 | 16 | 24 | 31 | 40 | 51 | 58 |
| H | 1.5 | .021 | .59 | 2.6 | 11 | 20 | 29 | 37 | 46 | 57 | 63 |
| H | 2.5 | .046 | .97 | 3.9 | 14 | 25 | 34 | 42 | 51 | 61 | 67 |
| H | 4.0 | .12 | 1.8 | 6.5 | 19 | 32 | 42 | 49 | 58 | 67 | 72 |
| H | 6.5 | .27 | 3.2 | 9.7 | 25 | 39 | 49 | 57 | 65 | 73 | 78 |
| H | 10 | .68 | 6.0 | 15 | 34 | 49 | 58 | 67 | 73 | 80 | 85 |
| J | 0.15 | 40-5 | .042 | .37 | 2.9 | 7.5 | 13 | 19 | 27 | 38 | 45 |
| J | 0.65 | 20-4 | .12 | .80 | 4.9 | 11 | 18 | 24 | 33 | 45 | 52 |
| J | 1.0 | 54-4 | .23 | 1.3 | 6.7 | 14 | 22 | 29 | 38 | 49 | 57 |
| J | 1.5 | .010 | .36 | 1.8 | 8.3 | 17 | 25 | 32 | 42 | 53 | 59 |
| J | 2.5 | .030 | .72 | 3.1 | 12 | 22 | 31 | 39 | 48 | 58 | 64 |
| J | 4.0 | .063 | 1.2 | 4.5 | 15 | 27 | 36 | 44 | 53 | 63 | 68 |
| J | 6.5 | .16 | 2.3 | 7.5 | 21 | 34 | 44 | 52 | 60 | 69 | 74 |
| J | 10 | .34 | 3.8 | 11 | 27 | 41 | 51 | 59 | 67 | 75 | 80 |

A negative figure after a ratio shows the number of decimal points to provide. Thus 62-4 = .0062.

TABLE 1B (Con.)

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | | |
|-------------|-------|--------------------------|---------------|---------------|------|----------------|----------------|-----|----------------|----------------|----|----|
| | | $\frac{1}{3}$ | $\frac{1}{2}$ | $\frac{2}{3}$ | 1 | $1\frac{1}{3}$ | $1\frac{2}{3}$ | 2 | $2\frac{1}{2}$ | $3\frac{1}{3}$ | 4 | |
| K | 0.10 | 10-5 | .017 | .19 | 1.8 | 5.5 | 10 | 15 | 23 | 33 | 40 | |
| | .40 | 50-5 | .049 | .41 | 3.1 | 8.0 | 14 | 20 | 28 | 39 | 46 | |
| | .65 | 13-4 | .093 | .67 | 4.3 | 10 | 17 | 23 | 32 | 43 | 50 | |
| | 1.0 | 27-4 | .15 | .94 | 5.4 | 12 | 19 | 26 | 35 | 46 | 53 | |
| | 1.5 | 76-4 | .29 | 1.5 | 7.6 | 15 | 23 | 31 | 40 | 51 | 58 | |
| | 2.5 | .015 | .47 | 2.2 | 9.8 | 19 | 27 | 35 | 44 | 55 | 61 | |
| | 4.0 | .039 | .85 | 3.5 | 13 | 23 | 33 | 41 | 50 | 60 | 66 | |
| | 6.5 | .092 | 1.5 | 5.5 | 17 | 29 | 39 | 47 | 56 | 65 | 70 | |
| | 10 | .27 | 3.2 | 9.7 | 25 | 39 | 49 | 57 | 65 | 73 | 78 | |
| | L | 0.065 | 25-6 | 67-4 | .093 | 1.1 | 3.8 | 7.7 | 12 | 19 | 29 | 36 |
| L | 0.25 | 12-5 | .019 | .20 | 1.9 | 5.7 | 10 | 15 | 23 | 34 | 41 | |
| | 0.40 | 33-5 | .036 | .33 | 2.7 | 7.2 | 12 | 18 | 26 | 37 | 45 | |
| | 0.65 | 66-5 | .058 | .47 | 3.4 | 8.5 | 14 | 20 | 29 | 40 | 47 | |
| | 1.0 | 18-4 | .11 | .79 | 4.8 | 11 | 18 | 24 | 33 | 44 | 52 | |
| | 1.5 | 40-4 | .18 | 1.1 | 6.0 | 13 | 20 | 27 | 36 | 48 | 55 | |
| | 2.5 | 91-4 | .32 | 1.7 | 8.0 | 16 | 24 | 32 | 40 | 52 | 59 | |
| | 4.0 | .020 | .56 | 2.6 | 10 | 20 | 29 | 36 | 45 | 56 | 62 | |
| | 6.5 | .060 | 1.1 | 4.4 | 15 | 26 | 36 | 44 | 52 | 62 | 68 | |
| | M | 0.040 | 60-7 | 26-4 | .047 | .73 | 2.7 | 5.8 | 9.6 | 16 | 25 | 32 |
| M | 0.15 | 30-6 | 78-4 | .10 | 1.2 | 4.0 | 8.0 | 12 | 19 | 30 | 37 | |
| | 0.25 | 80-6 | .015 | .17 | 1.7 | 5.1 | 9.7 | 14 | 22 | 33 | 40 | |
| | 0.40 | 16-5 | .023 | .23 | 2.1 | 6.0 | 11 | 16 | 24 | 35 | 42 | |
| | 0.65 | 45-5 | .045 | .39 | 3.0 | 7.8 | 13 | 19 | 27 | 38 | 46 | |
| | 1.0 | 95-5 | .074 | .56 | 3.8 | 9.3 | 15 | 22 | 30 | 42 | 49 | |
| | 1.5 | 22-4 | .12 | .85 | 5.0 | 11 | 18 | 25 | 34 | 45 | 52 | |
| | 2.5 | 51-4 | .22 | 1.3 | 6.6 | 14 | 22 | 29 | 38 | 49 | 56 | |
| | 4.0 | .013 | .45 | 2.1 | 9.4 | 18 | 27 | 34 | 43 | 54 | 61 | |
| | N | 0.025 | 14-7 | 10-4 | .024 | .46 | 1.9 | 4.4 | 7.6 | 13 | 22 | 28 |
| N | 0.10 | 72-7 | 31-4 | .052 | .79 | 2.8 | 6.1 | 10 | 16 | 26 | 32 | |
| | 0.15 | 19-6 | 56-4 | .082 | 1.0 | 3.5 | 7.3 | 11 | 18 | 28 | 35 | |
| | 0.25 | 40-6 | 92-4 | .11 | 1.3 | 4.3 | 8.4 | 13 | 20 | 30 | 37 | |
| | 0.40 | 11-5 | .017 | .19 | 1.8 | 5.5 | 10 | 15 | 23 | 33 | 40 | |
| | 0.65 | 22-5 | .028 | .27 | 2.4 | 6.6 | 12 | 17 | 25 | 36 | 43 | |
| | 1.0 | 50-5 | .049 | .41 | 3.1 | 8.0 | 14 | 20 | 28 | 39 | 46 | |
| | 1.5 | 12-4 | .083 | .62 | 4.0 | 9.8 | 16 | 22 | 31 | 42 | 49 | |
| | 2.5 | 35-4 | .17 | 1.0 | 5.9 | 13 | 20 | 27 | 36 | 47 | 54 | |
| | P | 0.015 | 35-8 | 40-5 | .012 | .29 | 1.3 | 3.3 | 6.0 | 11 | 19 | 25 |
| P | 0.065 | 17-7 | 12-4 | .026 | .49 | 2.0 | 4.6 | 7.8 | 13 | 21 | 29 | |
| | 0.10 | 44-7 | 22-4 | .041 | .67 | 2.5 | 5.5 | 9.2 | 15 | 25 | 31 | |
| | 0.15 | 92-7 | 34-4 | .057 | .84 | 3.0 | 6.3 | 10 | 17 | 26 | 33 | |
| | 0.25 | 25-6 | 68-4 | .094 | 1.1 | 3.8 | 7.7 | 12 | 19 | 29 | 36 | |
| | 0.40 | 51-6 | .011 | .13 | 1.4 | 4.6 | 8.9 | 13 | 20 | 31 | 38 | |
| | 0.65 | 12-5 | .019 | .20 | 1.9 | 5.7 | 10 | 15 | 23 | 34 | 41 | |
| | 1.0 | 28-5 | .033 | .30 | 2.5 | 6.9 | 12 | 18 | 26 | 37 | 44 | |
| | 1.5 | 77-5 | .063 | .50 | 3.5 | 8.8 | 15 | 21 | 29 | 41 | 48 | |

TABLE 1B (Con.)

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|-------|--------------------------|---------------|---------------|-----|----------------|----------------|-----|----------------|----------------|----|
| | | $\frac{1}{3}$ | $\frac{1}{2}$ | $\frac{2}{3}$ | 1 | $1\frac{1}{3}$ | $1\frac{2}{3}$ | 2 | $2\frac{1}{2}$ | $3\frac{1}{3}$ | 4 |
| Q | 0.010 | 90-9 | 16-5 | 63-4 | .18 | .96 | 2.5 | 4.9 | 9.0 | 16 | 23 |
| Q | 0.040 | 44-8 | 48-5 | .013 | .31 | 1.4 | 3.5 | 6.2 | 11 | 19 | 26 |
| Q | 0.065 | 11-7 | 90-5 | .021 | .43 | 1.8 | 4.2 | 7.4 | 12 | 21 | 28 |
| Q | 0.10 | 22-7 | 14-4 | .029 | .53 | 2.1 | 4.8 | 8.2 | 14 | 23 | 30 |
| Q | 0.15 | 62-7 | 28-4 | .048 | .75 | 2.7 | 5.9 | 9.7 | 16 | 25 | 32 |
| Q | 0.25 | 13-6 | 45-4 | .069 | .95 | 3.3 | 6.8 | 11 | 17 | 27 | 34 |
| Q | 0.40 | 30-6 | 78-4 | .10 | 1.2 | 4.1 | 8.0 | 12 | 19 | 30 | 37 |
| Q | 0.65 | 70-6 | .013 | .15 | 1.6 | 4.9 | 9.4 | 14 | 22 | 32 | 39 |
| Q | 1.0 | 19-5 | .026 | .26 | 2.3 | 6.4 | 11 | 17 | 25 | 35 | 43 |
| R | 0.025 | 10-8 | 18-5 | 68-4 | .19 | 1.0 | 2.6 | 5.0 | 9.3 | 17 | 23 |
| R | 0.040 | 26-8 | 35-5 | .010 | .26 | 1.2 | 3.2 | 5.8 | 10 | 18 | 25 |
| R | 0.065 | 54-8 | 55-5 | .015 | .33 | 1.5 | 3.6 | 6.5 | 11 | 20 | 26 |
| R | 0.10 | 15-7 | 11-4 | .024 | .47 | 1.9 | 4.5 | 7.7 | 13 | 22 | 29 |
| R | 0.15 | 30-7 | 17-4 | .034 | .59 | 2.3 | 5.1 | 8.7 | 14 | 24 | 30 |
| R | 0.25 | 70-7 | 30-4 | .051 | .78 | 2.8 | 6.0 | 10 | 16 | 26 | 33 |
| R | 0.40 | 17-6 | 52-4 | .075 | 1.0 | 3.4 | 7.1 | 11 | 18 | 28 | 35 |
| R | 0.65 | 46-6 | .010 | .12 | 1.4 | 4.5 | 8.7 | 13 | 20 | 31 | 38 |

TABLE 1C

100t/ μ Ratios at the Limiting Quality Level
for the MIL-STD-105D Plans -- Consumers Risk = 0.05

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|------|--------------------------|---------------|---------------|-----|----------------|----------------|-----|----------------|----------------|-----|
| | | $\frac{1}{3}$ | $\frac{1}{2}$ | $\frac{2}{3}$ | 1 | $1\frac{1}{3}$ | $1\frac{2}{3}$ | 2 | $2\frac{1}{2}$ | $3\frac{1}{3}$ | 4 |
| A | 6.5 | 55 | 120 | 130 | 140 | 140 | 130 | 130 | 120 | 120 | 120 |
| B | 4.0 | 16 | 50 | 73 | 100 | 110 | 110 | 110 | 110 | 110 | 110 |
| C | 2.5 | 3.5 | 18 | 35 | 60 | 74 | 82 | 87 | 90 | 96 | 97 |
| C | 10 | 20 | 59 | 84 | 110 | 120 | 110 | 110 | 110 | 110 | 110 |
| D | 1.5 | .84 | 6.9 | 17 | 36 | 52 | 61 | 69 | 76 | 82 | 86 |
| D | 6.5 | 4.3 | 20 | 37 | 64 | 77 | 85 | 90 | 93 | 97 | 99 |
| D | 10 | 13 | 43 | 65 | 93 | 100 | 100 | 100 | 110 | 100 | 100 |
| E | 1.0 | .22 | 2.8 | 8.6 | 23 | 37 | 47 | 55 | 63 | 72 | 76 |
| E | 4.0 | .95 | 7.4 | 18 | 39 | 53 | 63 | 70 | 76 | 83 | 87 |
| E | 6.5 | 2.5 | 14 | 28 | 53 | 67 | 76 | 82 | 86 | 92 | 95 |
| E | 10 | 5.5 | 24 | 43 | 69 | 82 | 89 | 94 | 97 | 99 | 100 |
| F | 0.65 | .059 | 1.1 | 4.4 | 15 | 26 | 35 | 43 | 52 | 62 | 68 |
| F | 2.5 | .25 | 3.1 | 9.3 | 25 | 38 | 48 | 56 | 64 | 73 | 77 |
| F | 4.0 | .60 | 5.4 | 14 | 33 | 48 | 57 | 65 | 72 | 79 | 83 |
| F | 6.5 | 1.2 | 8.6 | 20 | 42 | 57 | 66 | 73 | 78 | 85 | 89 |
| F | 10 | 3.8 | 19 | 36 | 62 | 75 | 83 | 88 | 92 | 96 | 98 |
| G | 0.40 | .013 | .43 | 2.1 | 9.3 | 18 | 27 | 34 | 43 | 54 | 61 |
| G | 1.5 | .059 | 1.1 | 4.4 | 15 | 26 | 35 | 43 | 52 | 62 | 68 |
| G | 2.5 | .13 | 1.9 | 6.7 | 20 | 32 | 42 | 50 | 58 | 67 | 72 |
| G | 4.0 | .29 | 3.4 | 10 | 26 | 30 | 50 | 57 | 65 | 74 | 78 |
| G | 6.5 | .76 | 6.3 | 16 | 35 | 50 | 60 | 67 | 74 | 81 | 85 |
| G | 10 | 1.6 | 10 | 23 | 47 | 61 | 70 | 77 | 82 | 88 | 91 |
| H | 0.25 | 37-4 | .18 | 1.1 | 5.9 | 13 | 20 | 27 | 36 | 47 | 54 |
| H | 1.0 | .014 | .46 | 2.2 | 9.6 | 18 | 27 | 34 | 42 | 55 | 61 |
| H | 1.5 | .034 | .82 | 3.4 | 12 | 23 | 32 | 40 | 49 | 60 | 66 |
| H | 2.5 | .070 | 1.3 | 4.9 | 16 | 27 | 37 | 45 | 54 | 64 | 70 |
| H | 4.0 | .18 | 2.5 | 7.9 | 22 | 35 | 45 | 53 | 61 | 71 | 75 |
| H | 6.5 | .40 | 4.1 | 11 | 28 | 43 | 53 | 60 | 68 | 76 | 80 |
| H | 10 | .93 | 7.4 | 18 | 39 | 54 | 63 | 70 | 76 | 83 | 87 |
| J | 0.15 | 90-5 | .072 | .55 | 3.7 | 9.3 | 15 | 22 | 30 | 41 | 49 |
| J | 0.65 | 37-4 | .18 | 1.1 | 5.9 | 13 | 20 | 27 | 36 | 47 | 54 |
| J | 1.0 | 92-4 | .32 | 1.7 | 8.0 | 16 | 24 | 32 | 40 | 52 | 58 |
| J | 1.5 | .016 | .48 | 2.3 | 9.9 | 19 | 28 | 35 | 44 | 57 | 61 |
| J | 2.5 | .046 | .95 | 3.9 | 14 | 25 | 34 | 42 | 51 | 61 | 67 |
| J | 4.0 | .089 | 1.5 | 5.5 | 17 | 29 | 39 | 47 | 55 | 65 | 70 |
| J | 6.5 | .18 | 2.5 | 7.9 | 22 | 35 | 45 | 53 | 61 | 71 | 75 |
| J | 10 | .45 | 4.6 | 12 | 30 | 44 | 54 | 62 | 69 | 77 | 81 |

A negative figure after a ratio shows the number of decimal points to provide. Thus 92-4 = .0092

1C (Con.)

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|-------|--------------------------|---------------|---------------|-----|----------------|----------------|-----|----------------|----------------|----|
| | | $\frac{1}{3}$ | $\frac{1}{2}$ | $\frac{2}{3}$ | 1 | $1\frac{1}{3}$ | $1\frac{2}{3}$ | 2 | $2\frac{1}{3}$ | $3\frac{1}{3}$ | 4 |
| K | 0.10 | 24-5 | .029 | .28 | 2.4 | 6.6 | 12 | 17 | 25 | 36 | 43 |
| K | 0.40 | 10-4 | .076 | .58 | 3.8 | 9.4 | 16 | 22 | 30 | 42 | 49 |
| K | 0.65 | 23-4 | .13 | .87 | 5.1 | 11 | 18 | 25 | 34 | 45 | 52 |
| K | 1.0 | 46-4 | .20 | 1.2 | 6.4 | 13 | 21 | 28 | 37 | 49 | 56 |
| K | 1.5 | .011 | .38 | 1.9 | 8.7 | 17 | 26 | 33 | 42 | 53 | 60 |
| K | 2.5 | .030 | .72 | 3.1 | 12 | 22 | 31 | 39 | 48 | 58 | 64 |
| K | 4.0 | .059 | 1.1 | 4.4 | 15 | 26 | 35 | 43 | 52 | 62 | 68 |
| K | 6.5 | .12 | 1.8 | 6.5 | 19 | 32 | 42 | 49 | 58 | 67 | 72 |
| K | 10 | .34 | 3.8 | 11 | 27 | 41 | 51 | 59 | 67 | 75 | 80 |
| L | 0.065 | 56-6 | .011 | .14 | 1.5 | 4.7 | 9.0 | 13 | 21 | 31 | 38 |
| L | 0.25 | 24-5 | .029 | .28 | 2.4 | 6.6 | 12 | 17 | 25 | 36 | 43 |
| L | 0.40 | 58-5 | .053 | .44 | 3.2 | 8.3 | 14 | 20 | 28 | 39 | 47 |
| L | 0.65 | 11-4 | .082 | .60 | 4.0 | 9.7 | 16 | 22 | 31 | 42 | 49 |
| L | 1.0 | 28-4 | .15 | .95 | 5.5 | 12 | 19 | 26 | 35 | 46 | 53 |
| L | 1.5 | 56-4 | .24 | 1.3 | 5.8 | 14 | 22 | 29 | 38 | 49 | 57 |
| L | 2.5 | .012 | .40 | 2.0 | 8.9 | 17 | 26 | 33 | 42 | 53 | 60 |
| L | 4.0 | .027 | .67 | 3.0 | 11 | 22 | 30 | 38 | 47 | 58 | 64 |
| L | 6.5 | .070 | 1.3 | 4.9 | 16 | 27 | 37 | 45 | 54 | 64 | 70 |
| M | 0.040 | 13-6 | 46-4 | .070 | .96 | 3.3 | 6.8 | 11 | 17 | 27 | 34 |
| M | 0.15 | 56-6 | .011 | .14 | 1.5 | 4.7 | 9.0 | 13 | 21 | 31 | 38 |
| M | 0.25 | 13-5 | .020 | .21 | 2.0 | 5.8 | 10 | 16 | 23 | 34 | 41 |
| M | 0.40 | 27-5 | .032 | .30 | 2.5 | 6.9 | 12 | 18 | 25 | 37 | 44 |
| M | 0.65 | 64-5 | .057 | .46 | 3.3 | 8.5 | 14 | 20 | 29 | 40 | 47 |
| M | 1.0 | 13-4 | .093 | .67 | 4.3 | 10 | 17 | 23 | 32 | 43 | 50 |
| M | 1.5 | 30-4 | .15 | .99 | 5.6 | 12 | 19 | 26 | 35 | 46 | 53 |
| M | 2.5 | 68-4 | .27 | 1.4 | 7.3 | 15 | 23 | 30 | 39 | 50 | 57 |
| M | 4.0 | .017 | .51 | 2.4 | 10 | 19 | 28 | 35 | 45 | 56 | 62 |
| N | 0.025 | 33-7 | 18-4 | .035 | .60 | 2.3 | 5.2 | 8.7 | 14 | 24 | 31 |
| N | 0.10 | 13-6 | 46-4 | .070 | .96 | 3.3 | 6.8 | 11 | 17 | 27 | 34 |
| N | 0.15 | 40-6 | 92-4 | .11 | 1.3 | 4.3 | 8.4 | 13 | 20 | 30 | 37 |
| N | 0.25 | 68-6 | .013 | .15 | 1.6 | 4.9 | 9.3 | 14 | 22 | 32 | 39 |
| N | 0.40 | 16-5 | .022 | .23 | 2.1 | 6.0 | 11 | 16 | 24 | 35 | 42 |
| N | 0.65 | 30-5 | .035 | .32 | 2.6 | 7.0 | 12 | 18 | 26 | 37 | 45 |
| N | 1.0 | 70-5 | .061 | .48 | 3.4 | 8.7 | 14 | 21 | 29 | 40 | 48 |
| N | 1.5 | 16-4 | .10 | .70 | 4.5 | 10 | 17 | 23 | 32 | 44 | 51 |
| N | 2.5 | 44-4 | .20 | 1.2 | 6.3 | 13 | 21 | 28 | 37 | 48 | 55 |

1C (Con.)

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|-------|--------------------------|---------------|---------------|------|----------------|----------------|-----|----------------|----------------|----|
| | | $\frac{1}{3}$ | $\frac{1}{2}$ | $\frac{2}{3}$ | 1 | $1\frac{1}{3}$ | $1\frac{2}{3}$ | 2 | $2\frac{1}{2}$ | $3\frac{1}{3}$ | 4 |
| P | 0.015 | 80-8 | 72-5 | .018 | .38 | 1.6 | 3.9 | 6.9 | 12 | 21 | 27 |
| P | 0.065 | 30-7 | 17-4 | .034 | .59 | 2.3 | 5.1 | 8.7 | 14 | 24 | 30 |
| P | 0.10 | 67-7 | 31-4 | .053 | .80 | 2.8 | 6.1 | 10 | 16 | 26 | 32 |
| P | 0.15 | 14-6 | 47-4 | .072 | .98 | 3.3 | 7.0 | 11 | 17 | 27 | 34 |
| P | 0.25 | 40-6 | 92-4 | .11 | 1.3 | 4.3 | 8.4 | 13 | 20 | 30 | 37 |
| P | 0.40 | 68-6 | .013 | .15 | 1.6 | 4.9 | 9.3 | 14 | 22 | 32 | 39 |
| P | 0.65 | 16-5 | .022 | .23 | 2.1 | 6.0 | 11 | 16 | 24 | 35 | 42 |
| P | 1.0 | 33-5 | .036 | .33 | 2.7 | 7.2 | 12 | 18 | 26 | 37 | 45 |
| P | 1.5 | 10-4 | .076 | .58 | 3.8 | 9.4 | 16 | 22 | 30 | 42 | 49 |
| Q | 0.010 | 19-8 | 28-5 | 92-4 | .024 | 1.1 | 3.0 | 5.5 | 10 | 18 | 24 |
| Q | 0.040 | 80-8 | 72-5 | .018 | .38 | 1.6 | 3.9 | 6.9 | 12 | 21 | 27 |
| Q | 0.065 | 18-7 | 12-4 | .026 | .50 | 2.0 | 4.6 | 8.0 | 13 | 22 | 29 |
| Q | 0.10 | 35-7 | 19-4 | .036 | .63 | 2.4 | 5.3 | 8.9 | 15 | 24 | 31 |
| Q | 0.15 | 92-7 | 34-4 | .057 | .84 | 3.0 | 6.3 | 10 | 17 | 26 | 33 |
| Q | 0.25 | 21-6 | 62-4 | .087 | 1.1 | 3.7 | 7.5 | 12 | 18 | 29 | 35 |
| Q | 0.40 | 46-6 | .010 | .12 | 1.4 | 4.5 | 8.7 | 13 | 20 | 31 | 38 |
| Q | 0.65 | 10-5 | .017 | .18 | 1.8 | 5.3 | 10 | 15 | 22 | 33 | 40 |
| Q | 1.0 | 24-5 | .029 | .28 | 2.4 | 6.6 | 12 | 17 | 25 | 36 | 43 |
| R | 0.025 | 19-8 | 28-5 | 92-4 | .024 | 1.1 | 3.0 | 5.5 | 10 | 18 | 24 |
| R | 0.040 | 44-8 | 50-5 | .014 | .32 | 1.4 | 3.6 | 6.4 | 11 | 20 | 26 |
| R | 0.065 | 88-8 | 76-5 | .018 | .39 | 1.7 | 4.0 | 7.1 | 12 | 21 | 27 |
| R | 0.10 | 22-7 | 14-4 | .029 | .53 | 2.1 | 4.8 | 8.2 | 14 | 23 | 30 |
| R | 0.15 | 44-7 | 22-4 | .041 | .67 | 2.5 | 5.5 | 9.2 | 15 | 25 | 31 |
| R | 0.25 | 10-6 | 36-4 | .059 | .85 | 3.0 | 6.4 | 10 | 17 | 26 | 33 |
| R | 0.40 | 21-6 | 62-4 | .087 | 1.1 | 3.7 | 7.5 | 12 | 18 | 29 | 35 |
| R | 0.65 | 56-6 | .011 | .14 | 1.5 | 4.7 | 9.0 | 13 | 21 | 31 | 38 |

TABLE 2A

100t Z(t) Products at the Acceptable Quality Level (normal inspection)
for the MIL-STD-105D Plans

| Acceptable Quality Level $p'(\%)$ | Shape Parameter, β | | | | | | | | | |
|--|--------------------------|---------------|---------------|------|----------------|----------------|------|----------------|----------------|------|
| | $\frac{1}{3}$ | $\frac{1}{2}$ | $\frac{2}{3}$ | 1 | $1\frac{1}{3}$ | $1\frac{2}{3}$ | 2 | $2\frac{1}{2}$ | $3\frac{1}{3}$ | 4 |
| 0.010 | 33-4 | 50-4 | 67-4 | .010 | .013 | .017 | .020 | .025 | .033 | .040 |
| 0.015 | 50-4 | 75-4 | .010 | .015 | .020 | .025 | .030 | .038 | .050 | .060 |
| 0.025 | 83-4 | .012 | .017 | .025 | .033 | .042 | .050 | .06 | .083 | .10 |
| 0.040 | .013 | .020 | .027 | .040 | .053 | .067 | .080 | .10 | .13 | .16 |
| 0.065 | .022 | .032 | .043 | .065 | .087 | .11 | .13 | .16 | .22 | .26 |
| 0.10 | .033 | .050 | .067 | .10 | .13 | .17 | .20 | .25 | .33 | .40 |
| 0.15 | .050 | .075 | .10 | .15 | .20 | .25 | .30 | .38 | .50 | .60 |
| 0.25 | .083 | .13 | .17 | .25 | .33 | .42 | .50 | .63 | .83 | 1.00 |
| 0.40 | .13 | .20 | .27 | .40 | .54 | .67 | .80 | 1.00 | 1.34 | 1.60 |
| 0.65 | .22 | .33 | .44 | .65 | .87 | 1.09 | 1.30 | 1.63 | 2.17 | 2.61 |
| 1.0 | .34 | .50 | .67 | 1.01 | 1.34 | 1.68 | 2.01 | 2.51 | 3.35 | 4.02 |
| 1.5 | .50 | .76 | 1.01 | 1.51 | 2.02 | 2.52 | 3.02 | 3.78 | 5.04 | 6.04 |
| 2.5 | .84 | 1.27 | 1.69 | 2.53 | 2.38 | 4.22 | 5.06 | 6.33 | 8.44 | 10.1 |
| 4.0 | 1.36 | 2.04 | 2.72 | 4.08 | 5.44 | 6.80 | 8.16 | 10.2 | 13.6 | 16.3 |
| 6.5 | 2.24 | 3.36 | 4.48 | 6.72 | 8.96 | 11.2 | 13.4 | 16.8 | 22.4 | 26.9 |
| 10 | 3.51 | 5.27 | 7.02 | 10.5 | 14.0 | 17.6 | 21.1 | 26.3 | 35.1 | 42.1 |

The negative figure after a ratio shows the number of decimal points to provide.
Thus 83-4 = .0083

TABLE 2B

100t Z(t) Products at the Limiting Quality Level
for the MIL-STD-105D Plans - Consumer's Risk = 0.10

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|------|--------------------------|---------------|---------------|-----|----------------|----------------|-----|----------------|----------------|-----|
| | | $\frac{1}{3}$ | $\frac{3}{8}$ | $\frac{2}{3}$ | 1 | $1\frac{1}{3}$ | $1\frac{2}{3}$ | 2 | $2\frac{1}{2}$ | $3\frac{1}{3}$ | 4 |
| A | 6.5 | 37 | 54 | 76 | 110 | 150 | 180 | 220 | 280 | 380 | 470 |
| B | 4.0 | 25 | 38 | 50 | 77 | 100 | 130 | 150 | 190 | 260 | 310 |
| C | 2.5 | 15 | 22 | 30 | 46 | 61 | 76 | 92 | 110 | 150 | 180 |
| C | 10 | 28 | 43 | 57 | 86 | 110 | 140 | 170 | 210 | 290 | 350 |
| D | 1.5 | 9.6 | 14 | 19 | 29 | 38 | 48 | 57 | 72 | 96 | 110 |
| D | 6.5 | 17 | 26 | 35 | 53 | 71 | 88 | 100 | 130 | 170 | 210 |
| D | 10 | 25 | 38 | 50 | 77 | 100 | 130 | 150 | 190 | 260 | 310 |
| E | 1.0 | 5.8 | 8.7 | 11 | 17 | 23 | 29 | 35 | 42 | 58 | 70 |
| E | 4.0 | 10 | 15 | 21 | 31 | 42 | 53 | 63 | 78 | 100 | 120 |
| E | 6.5 | 14 | 22 | 29 | 45 | 60 | 75 | 90 | 110 | 150 | 180 |
| E | 10 | 19 | 28 | 38 | 59 | 77 | 97 | 110 | 140 | 190 | 230 |
| F | 0.65 | 3.9 | 5.7 | 7.8 | 11 | 15 | 19 | 23 | 29 | 38 | 47 |
| F | 2.5 | 6.6 | 9.9 | 13 | 20 | 26 | 33 | 40 | 50 | 66 | 80 |
| F | 4.0 | 9.6 | 14 | 19 | 29 | 38 | 48 | 57 | 72 | 96 | 110 |
| F | 6.5 | 12 | 18 | 24 | 35 | 47 | 59 | 71 | 89 | 120 | 140 |
| F | 10 | 18 | 27 | 36 | 55 | 73 | 92 | 110 | 130 | 180 | 220 |
| G | 0.40 | 2.3 | 3.5 | 4.7 | 7.2 | 9.5 | 12 | 14 | 18 | 23 | 28 |
| G | 1.5 | 4.3 | 6.4 | 8.5 | 13 | 17 | 21 | 25 | 32 | 42 | 51 |
| G | 2.5 | 5.8 | 8.7 | 11 | 17 | 23 | 29 | 35 | 42 | 58 | 70 |
| G | 4.0 | 7.4 | 11 | 15 | 22 | 30 | 37 | 44 | 56 | 74 | 89 |
| G | 6.5 | 10 | 15 | 21 | 31 | 42 | 53 | 63 | 78 | 100 | 120 |
| G | 10 | 13 | 20 | 27 | 42 | 58 | 70 | 85 | 100 | 140 | 170 |
| H | 0.25 | 1.5 | 2.3 | 3.0 | 4.7 | 6.1 | 7.6 | 9.3 | 11 | 15 | 18 |
| H | 1.0 | 2.6 | 3.9 | 5.3 | 7.9 | 10 | 13 | 16 | 19 | 26 | 31 |
| H | 1.5 | 3.5 | 5.2 | 7.0 | 10 | 14 | 17 | 21 | 26 | 35 | 42 |
| H | 2.5 | 4.7 | 6.9 | 9.3 | 14 | 18 | 23 | 28 | 35 | 46 | 56 |
| H | 4.0 | 6.6 | 9.9 | 13 | 20 | 26 | 33 | 40 | 50 | 66 | 80 |
| H | 6.5 | 8.3 | 12 | 16 | 25 | 33 | 41 | 50 | 62 | 81 | 100 |
| H | 10 | 11 | 17 | 22 | 34 | 46 | 57 | 69 | 86 | 110 | 130 |
| J | 0.15 | .95 | 1.4 | 1.8 | 2.8 | 3.7 | 4.7 | 5.7 | 7.1 | 9.5 | 11 |
| J | 0.65 | 1.6 | 2.4 | 3.2 | 4.9 | 6.5 | 8.2 | 9.9 | 12 | 16 | 19 |
| J | 1.0 | 2.2 | 3.3 | 4.5 | 6.7 | 8.9 | 11 | 13 | 17 | 22 | 27 |
| J | 1.5 | 2.8 | 4.2 | 5.7 | 8.6 | 11 | 14 | 17 | 21 | 28 | 34 |
| J | 2.5 | 3.9 | 5.7 | 7.8 | 11 | 15 | 19 | 23 | 29 | 38 | 47 |
| J | 4.0 | 5.0 | 7.5 | 10 | 15 | 20 | 25 | 30 | 37 | 50 | 61 |
| J | 6.5 | 7.0 | 10 | 14 | 21 | 28 | 34 | 42 | 53 | 70 | 86 |
| J | 10 | 9.1 | 13 | 18 | 27 | 36 | 45 | 55 | 69 | 90 | 110 |

TABLE 2B (Con.)

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|-------|--------------------------|---------------|---------------|-----|----------------|----------------|-----|----------------|----------------|-----|
| | | $\frac{1}{3}$ | $\frac{1}{2}$ | $\frac{2}{3}$ | 1 | $1\frac{1}{3}$ | $1\frac{2}{3}$ | 2 | $2\frac{1}{2}$ | $3\frac{1}{3}$ | 4 |
| K | 0.10 | .60 | .90 | 1.2 | 1.8 | 2.4 | 3.0 | 3.6 | 4.5 | 6.0 | 7.2 |
| | 0.40 | 1.0 | 1.5 | 2.0 | 3.1 | 4.2 | 5.3 | 6.3 | 7.8 | 10 | 12 |
| | 0.65 | 1.4 | 2.2 | 2.9 | 4.4 | 5.8 | 7.3 | 8.9 | 11 | 14 | 17 |
| | 1.0 | 1.8 | 2.7 | 3.6 | 5.6 | 7.3 | 9.2 | 11 | 13 | 18 | 21 |
| | 1.5 | 2.5 | 3.8 | 5.1 | 7.6 | 10 | 13 | 15 | 19 | 25 | 30 |
| | 2.5 | 3.2 | 4.9 | 6.6 | 9.8 | 13 | 16 | 19 | 23 | 32 | 39 |
| | 4.0 | 4.2 | 6.4 | 8.5 | 13 | 17 | 21 | 25 | 32 | 42 | 51 |
| | 6.5 | 5.8 | 8.7 | 11 | 17 | 23 | 29 | 35 | 42 | 58 | 70 |
| | 10 | 8.7 | 13 | 17 | 26 | 35 | 43 | 53 | 66 | 86 | 100 |
| | | | | | | | | | | | |
| L | 0.065 | .40 | .60 | .80 | 1.2 | 1.6 | 2.0 | 2.4 | 3.0 | 4.0 | 4.8 |
| | 0.25 | .67 | 1.0 | 1.3 | 2.0 | 2.7 | 3.3 | 4.0 | 5.0 | 6.7 | 8.1 |
| | 0.40 | .91 | 1.3 | 1.8 | 2.7 | 3.6 | 4.6 | 5.5 | 6.8 | 9.1 | 11 |
| | 0.65 | 1.1 | 1.6 | 2.2 | 3.3 | 4.4 | 5.5 | 6.7 | 8.4 | 11 | 13 |
| | 1.0 | 1.5 | 2.3 | 3.1 | 4.3 | 6.3 | 7.8 | 9.5 | 11 | 15 | 19 |
| | 1.5 | 2.0 | 3.0 | 4.0 | 6.1 | 8.1 | 10 | 12 | 15 | 20 | 24 |
| | 2.5 | 2.6 | 3.9 | 5.3 | 8.0 | 10 | 13 | 16 | 20 | 26 | 32 |
| | 4.0 | 3.5 | 5.2 | 7.0 | 10 | 14 | 17 | 21 | 26 | 35 | 42 |
| | 6.5 | 5.0 | 7.5 | 10 | 15 | 20 | 25 | 30 | 37 | 50 | 61 |
| | | | | | | | | | | | |
| M | 0.040 | .24 | .36 | .49 | .73 | .96 | 1.2 | 1.4 | 1.8 | 2.4 | 2.9 |
| | 0.15 | .40 | .60 | .80 | 1.2 | 1.6 | 2.0 | 2.4 | 3.0 | 4.0 | 4.8 |
| | 0.25 | .56 | .84 | 1.1 | 1.7 | 2.3 | 2.8 | 3.4 | 4.2 | 5.7 | 6.8 |
| | 0.40 | .70 | 1.0 | 1.4 | 2.1 | 2.8 | 3.5 | 4.2 | 5.3 | 7.0 | 8.5 |
| | 0.65 | .98 | 1.4 | 1.9 | 2.9 | 3.9 | 4.9 | 6.0 | 7.4 | 9.8 | 11 |
| | 1.0 | 1.2 | 1.9 | 2.5 | 3.8 | 5.0 | 6.4 | 7.6 | 9.4 | 12 | 15 |
| | 1.5 | 1.6 | 2.5 | 3.3 | 5.0 | 6.7 | 8.4 | 10 | 12 | 16 | 20 |
| | 2.5 | 2.2 | 3.3 | 4.4 | 6.6 | 8.7 | 11 | 13 | 16 | 21 | 26 |
| | 4.0 | 3.1 | 4.6 | 6.3 | 9.4 | 12 | 15 | 19 | 23 | 31 | 38 |
| | | | | | | | | | | | |
| N | 0.025 | .15 | .23 | .31 | .46 | .60 | .76 | .92 | 1.1 | 1.5 | 1.8 |
| | 0.10 | .26 | .39 | .52 | .78 | 1.0 | 1.3 | 1.5 | 1.9 | 2.6 | 3.1 |
| | 0.15 | .37 | .55 | .74 | 1.1 | 1.4 | 1.8 | 2.2 | 2.7 | 3.7 | 4.4 |
| | 0.25 | .44 | .65 | .88 | 1.3 | 1.7 | 2.2 | 2.6 | 3.2 | 4.4 | 5.2 |
| | 0.40 | .63 | .95 | 1.2 | 1.9 | 2.5 | 3.2 | 3.8 | 4.8 | 6.3 | 7.6 |
| | 0.65 | .80 | 1.2 | 1.6 | 2.4 | 3.2 | 4.0 | 4.8 | 6.0 | 8.1 | 9.7 |
| | 1.0 | 1.0 | 1.5 | 2.0 | 3.1 | 4.2 | 5.3 | 6.3 | 7.8 | 10 | 12 |
| | 1.5 | 1.3 | 2.0 | 2.7 | 4.1 | 5.4 | 6.8 | 8.1 | 10 | 13 | 16 |
| | 2.5 | 1.9 | 2.8 | 3.8 | 5.8 | 7.7 | 9.5 | 11 | 14 | 19 | 23 |
| | | | | | | | | | | | |
| P | 0.015 | .096 | .14 | .19 | .29 | .36 | .48 | .58 | .72 | .95 | 1.1 |
| | 0.065 | .16 | .24 | .32 | .49 | .65 | .81 | .98 | 1.2 | 1.6 | 1.9 |
| | 0.10 | .22 | .33 | .45 | .67 | .89 | 1.1 | 1.3 | 1.6 | 2.2 | 2.7 |
| | 0.15 | .28 | .42 | .56 | .84 | 1.1 | 1.4 | 1.7 | 2.1 | 2.8 | 3.4 |
| | 0.25 | .40 | .60 | .80 | 1.2 | 1.6 | 2.0 | 2.4 | 3.0 | 4.0 | 4.8 |
| | 0.40 | .50 | .75 | 1.0 | 1.5 | 2.0 | 2.5 | 3.0 | 3.7 | 5.0 | 6.0 |
| | 0.65 | .64 | .95 | 1.3 | 1.9 | 2.5 | 3.2 | 3.8 | 4.8 | 6.4 | 7.6 |
| | 1.0 | .84 | 1.2 | 1.6 | 2.5 | 3.3 | 4.2 | 5.0 | 6.3 | 8.4 | 10 |
| | 1.5 | 1.2 | 1.8 | 2.3 | 3.5 | 4.7 | 6.0 | 7.2 | 8.9 | 12 | 14 |
| | | | | | | | | | | | |

TABLE 2B (Con.)

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|-------|--------------------------|---------------|---------------|-----|----------------|----------------|-----|----------------|----------------|-----|
| | | $\frac{1}{3}$ | $\frac{1}{2}$ | $\frac{2}{3}$ | 1 | $1\frac{1}{3}$ | $1\frac{2}{3}$ | 2 | $2\frac{1}{2}$ | $3\frac{1}{3}$ | 4 |
| Q | 0.010 | .060 | .090 | .12 | .18 | .24 | .30 | .36 | .45 | .60 | .71 |
| Q | 0.040 | .10 | .15 | .20 | .31 | .40 | .51 | .62 | .77 | 1.0 | 1.2 |
| Q | 0.065 | .14 | .21 | .29 | .43 | .56 | .71 | .87 | 1.0 | 1.4 | 1.7 |
| Q | 0.10 | .17 | .26 | .35 | .53 | .70 | .87 | 1.0 | 1.3 | 1.7 | 2.1 |
| Q | 0.15 | .25 | .37 | .50 | .74 | .97 | 1.2 | 1.4 | 1.8 | 2.4 | 3.0 |
| Q | 0.25 | .31 | .47 | .63 | .94 | 1.2 | 1.5 | 1.9 | 2.3 | 3.2 | 3.8 |
| Q | 0.40 | .40 | .60 | .80 | 1.2 | 1.6 | 2.0 | 2.4 | 3.0 | 4.0 | 4.8 |
| Q | 0.65 | .54 | .80 | 1.1 | 1.6 | 2.1 | 2.7 | 3.2 | 4.0 | 5.4 | 6.4 |
| Q | 1.0 | .77 | 1.1 | 1.5 | 2.3 | 3.1 | 3.9 | 4.7 | 5.8 | 7.7 | 9.3 |
| R | 0.025 | .067 | .10 | .13 | .20 | .26 | .33 | .40 | .50 | .66 | .80 |
| R | 0.040 | .089 | .13 | .18 | .27 | .35 | .45 | .54 | .67 | .89 | 1.1 |
| R | 0.065 | .11 | .16 | .22 | .33 | .43 | .54 | .66 | .82 | 1.1 | 1.3 |
| R | 0.10 | .15 | .23 | .31 | .46 | .60 | .76 | .92 | 1.1 | 1.5 | 1.8 |
| R | 0.15 | .19 | .29 | .39 | .59 | .78 | .97 | 1.2 | 1.4 | 2.0 | 2.4 |
| R | 0.25 | .26 | .38 | .52 | .77 | 1.0 | 1.2 | 1.5 | 1.9 | 2.5 | 3.1 |
| R | 0.40 | .33 | .50 | .67 | 1.0 | 1.3 | 1.6 | 2.0 | 2.5 | 3.3 | 4.0 |
| R | 0.65 | .47 | .70 | .94 | 1.4 | 1.8 | 2.3 | 2.8 | 3.5 | 4.7 | 5.6 |

TABLE 2C

100t Z(t) Products at the Limiting Quality Level
for the MIL-STD-105D Plans - Consumer's Risk = 0.05

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|------|--------------------------|---------------|---------------|-----|----------------|----------------|-----|----------------|----------------|-----|
| | | $\frac{1}{3}$ | $\frac{1}{2}$ | $\frac{2}{3}$ | 1 | $1\frac{1}{3}$ | $1\frac{2}{3}$ | 2 | $2\frac{1}{2}$ | $3\frac{1}{3}$ | 4 |
| A | 6.5 | 50 | 77 | 100 | 150 | 200 | 250 | 300 | 380 | 510 | 610 |
| B | 4.0 | 32 | 50 | 67 | 99 | 130 | 160 | 200 | 250 | 330 | 400 |
| C | 2.5 | 20 | 30 | 40 | 60 | 80 | 100 | 120 | 150 | 200 | 240 |
| C | 10 | 36 | 53 | 72 | 110 | 140 | 180 | 210 | 270 | 360 | 440 |
| D | 1.5 | 12 | 18 | 24 | 37 | 49 | 62 | 75 | 93 | 120 | 150 |
| D | 6.5 | 21 | 33 | 42 | 65 | 85 | 100 | 130 | 160 | 210 | 250 |
| D | 10 | 30 | 46 | 61 | 93 | 120 | 150 | 180 | 230 | 310 | 370 |
| E | 1.0 | 7.9 | 11 | 15 | 24 | 31 | 39 | 48 | 59 | 78 | 95 |
| E | 4.0 | 12 | 19 | 25 | 38 | 51 | 64 | 77 | 96 | 120 | 150 |
| E | 6.5 | 17 | 26 | 35 | 54 | 70 | 88 | 100 | 130 | 170 | 210 |
| E | 10 | 23 | 34 | 46 | 69 | 92 | 110 | 140 | 170 | 230 | 280 |
| F | 0.65 | 5.0 | 7.5 | 10 | 15 | 20 | 25 | 30 | 37 | 50 | 60 |
| F | 2.5 | 8.3 | 12 | 16 | 25 | 33 | 41 | 50 | 63 | 82 | 100 |
| F | 4.0 | 11 | 16 | 21 | 33 | 44 | 55 | 65 | 83 | 110 | 130 |
| F | 6.5 | 13 | 20 | 27 | 42 | 56 | 70 | 84 | 100 | 120 | 160 |
| F | 10 | 20 | 30 | 40 | 62 | 82 | 100 | 120 | 150 | 200 | 240 |
| G | 0.40 | 3.1 | 4.6 | 6.2 | 9.2 | 12 | 15 | 18 | 23 | 31 | 37 |
| G | 1.5 | 5.0 | 7.5 | 10 | 15 | 20 | 25 | 30 | 37 | 50 | 60 |
| G | 2.5 | 6.6 | 9.8 | 13 | 20 | 26 | 33 | 39 | 50 | 66 | 80 |
| G | 4.0 | 8.7 | 13 | 17 | 26 | 35 | 43 | 52 | 65 | 86 | 100 |
| G | 6.5 | 12 | 17 | 23 | 35 | 47 | 59 | 71 | 89 | 120 | 140 |
| G | 10 | 15 | 23 | 30 | 47 | 62 | 77 | 93 | 110 | 150 | 180 |
| H | 0.25 | 2.0 | 3.0 | 3.9 | 6.0 | 7.9 | 9.9 | 12 | 15 | 19 | 24 |
| H | 1.0 | 3.2 | 4.7 | 6.3 | 9.5 | 12 | 16 | 19 | 24 | 31 | 38 |
| H | 1.5 | 4.2 | 6.4 | 8.5 | 12 | 17 | 21 | 25 | 32 | 42 | 51 |
| H | 2.5 | 5.4 | 8.1 | 10 | 16 | 21 | 27 | 32 | 40 | 54 | 65 |
| H | 4.0 | 7.4 | 11 | 15 | 22 | 29 | 37 | 44 | 55 | 74 | 89 |
| H | 6.5 | 9.6 | 14 | 19 | 28 | 38 | 48 | 57 | 72 | 95 | 110 |
| H | 10 | 12 | 19 | 25 | 38 | 51 | 65 | 77 | 97 | 120 | 150 |
| J | 0.15 | 1.2 | 1.8 | 2.5 | 3.8 | 5.0 | 6.3 | 7.6 | 9.4 | 12 | 15 |
| J | 0.65 | 2.0 | 3.0 | 3.9 | 6.0 | 7.9 | 9.9 | 12 | 15 | 19 | 24 |
| J | 1.0 | 2.6 | 4.0 | 5.3 | 7.9 | 10 | 13 | 16 | 19 | 26 | 32 |
| J | 1.5 | 3.3 | 4.9 | 6.5 | 9.7 | 13 | 16 | 19 | 24 | 32 | 39 |
| J | 2.5 | 4.6 | 6.9 | 9.2 | 14 | 18 | 23 | 28 | 35 | 46 | 56 |
| J | 4.0 | 5.8 | 8.5 | 11 | 17 | 23 | 29 | 35 | 43 | 58 | 70 |
| J | 6.5 | 7.4 | 11 | 15 | 22 | 29 | 37 | 44 | 55 | 74 | 89 |
| J | 10 | 10 | 15 | 20 | 30 | 40 | 50 | 60 | 76 | 100 | 120 |

TABLE 2C (Con't)

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|-------|--------------------------|---------------|---------------|-----|----------------|----------------|-----|----------------|----------------|-----|
| | | $\frac{1}{3}$ | $\frac{1}{2}$ | $\frac{2}{3}$ | 1 | $1\frac{1}{3}$ | $1\frac{2}{3}$ | 2 | $2\frac{1}{2}$ | $3\frac{1}{3}$ | 4 |
| K | 0.10 | .80 | 1.2 | 1.6 | 2.4 | 3.2 | 4.0 | 4.9 | 6.0 | 8.2 | 9.7 |
| | 0.40 | 1.3 | 1.9 | 2.6 | 3.9 | 5.2 | 6.5 | 7.8 | 9.7 | 13 | 15 |
| | 0.65 | 1.7 | 2.5 | 3.4 | 5.1 | 6.8 | 8.5 | 10 | 12 | 17 | 20 |
| | 1.0 | 2.1 | 3.2 | 4.2 | 6.4 | 8.5 | 10 | 12 | 16 | 21 | 26 |
| | 1.5 | 2.9 | 4.3 | 5.8 | 8.7 | 11 | 14 | 17 | 22 | 29 | 35 |
| | 2.5 | 3.9 | 5.7 | 7.7 | 11 | 15 | 19 | 23 | 29 | 38 | 47 |
| | 4.0 | 5.0 | 7.5 | 10 | 15 | 20 | 25 | 30 | 37 | 50 | 60 |
| | 6.5 | 6.6 | 9.9 | 13 | 20 | 26 | 33 | 40 | 50 | 66 | 80 |
| | 10 | 9.2 | 13 | 18 | 27 | 36 | 45 | 55 | 69 | 90 | 110 |
| | | | | | | | | | | | |
| L | 0.065 | .50 | .75 | 1.0 | 1.5 | 2.0 | 2.5 | 3.0 | 3.7 | 5.0 | 6.0 |
| | 0.25 | .80 | 1.2 | 1.6 | 2.4 | 3.2 | 4.0 | 4.9 | 6.0 | 8.2 | 9.7 |
| | 0.40 | 1.0 | 1.6 | 2.1 | 3.2 | 4.4 | 5.4 | 6.5 | 8.0 | 11 | 13 |
| | 0.65 | 1.3 | 2.0 | 2.6 | 4.0 | 5.3 | 6.7 | 8.0 | 10 | 13 | 16 |
| | 1.0 | 1.8 | 2.7 | 3.6 | 5.5 | 7.3 | 9.0 | 11 | 13 | 18 | 22 |
| | 1.5 | 2.2 | 3.4 | 4.5 | 6.8 | 9.0 | 11 | 13 | 17 | 22 | 27 |
| | 2.5 | 2.9 | 4.4 | 5.9 | 8.8 | 11 | 14 | 17 | 22 | 29 | 35 |
| | 4.0 | 3.9 | 5.7 | 7.7 | 11 | 15 | 19 | 23 | 29 | 38 | 47 |
| | 6.5 | 5.4 | 8.1 | 10 | 16 | 21 | 27 | 32 | 40 | 54 | 65 |
| | | | | | | | | | | | |
| M | 0.040 | .31 | .47 | .64 | .95 | 1.2 | 1.5 | 1.9 | 2.3 | 3.2 | 3.8 |
| | 0.15 | .50 | .75 | 1.0 | 1.5 | 2.0 | 2.5 | 3.0 | 3.7 | 5.0 | 6.0 |
| | 0.25 | .67 | 1.0 | 1.3 | 2.0 | 2.7 | 3.3 | 4.0 | 5.0 | 6.7 | 8.0 |
| | 0.40 | .84 | 1.2 | 1.6 | 2.5 | 3.3 | 4.2 | 5.0 | 6.3 | 8.4 | 10 |
| | 0.65 | 1.1 | 1.6 | 2.2 | 3.3 | 4.5 | 5.6 | 6.7 | 8.4 | 11 | 13 |
| | 1.0 | 1.4 | 2.1 | 2.8 | 4.3 | 5.7 | 7.2 | 8.7 | 10 | 14 | 17 |
| | 1.5 | 1.8 | 2.7 | 3.6 | 5.6 | 7.4 | 9.2 | 11 | 13 | 18 | 22 |
| | 2.5 | 2.4 | 3.6 | 4.8 | 7.3 | 9.5 | 12 | 14 | 18 | 23 | 29 |
| | 4.0 | 3.3 | 5.0 | 6.7 | 10 | 13 | 16 | 20 | 25 | 33 | 40 |
| | | | | | | | | | | | |
| N | 0.025 | .20 | .30 | .40 | .60 | .80 | 1.0 | 1.2 | 1.5 | 2.0 | 2.4 |
| | 0.10 | .31 | .47 | .64 | .95 | 1.2 | 1.5 | 1.9 | 2.3 | 3.2 | 3.8 |
| | 0.15 | .43 | .65 | .87 | 1.3 | 1.7 | 2.1 | 2.6 | 3.3 | 4.3 | 5.2 |
| | 0.25 | .54 | .80 | 1.0 | 1.6 | 2.1 | 2.7 | 3.2 | 4.0 | 5.3 | 6.4 |
| | 0.40 | .70 | 1.0 | 1.4 | 2.1 | 2.8 | 3.5 | 4.2 | 5.3 | 7.0 | 8.4 |
| | 0.65 | .88 | 1.3 | 1.7 | 2.6 | 3.5 | 4.4 | 5.3 | 6.5 | 8.8 | 10 |
| | 1.0 | 1.1 | 1.7 | 2.2 | 3.5 | 4.6 | 5.8 | 7.0 | 8.6 | 11 | 13 |
| | 1.5 | 1.5 | 2.2 | 3.0 | 4.5 | 6.0 | 7.5 | 9.1 | 11 | 15 | 18 |
| | 2.5 | 2.1 | 3.1 | 4.1 | 6.2 | 8.4 | 10 | 12 | 15 | 20 | 25 |
| | | | | | | | | | | | |
| P | 0.015 | .12 | .19 | .25 | .38 | .50 | .63 | .76 | .95 | 1.3 | 1.5 |
| | 0.065 | .20 | .29 | .39 | .59 | .78 | .97 | 1.1 | 1.4 | 1.9 | 2.4 |
| | 0.10 | .26 | .39 | .53 | .79 | 1.0 | 1.3 | 1.6 | 2.0 | 2.6 | 3.2 |
| | 0.15 | .32 | .48 | .65 | .96 | 1.3 | 1.6 | 1.9 | 2.4 | 3.2 | 3.9 |
| | 0.25 | .44 | .65 | .88 | 1.3 | 1.7 | 2.2 | 2.6 | 3.2 | 4.4 | 5.2 |
| | 0.40 | .54 | .80 | 1.1 | 1.6 | 2.1 | 2.7 | 3.2 | 4.0 | 5.4 | 6.4 |
| | 0.65 | .70 | 1.0 | 1.4 | 2.1 | 2.8 | 3.5 | 4.2 | 5.3 | 7.0 | 8.5 |
| | 1.0 | .91 | 1.3 | 1.8 | 2.7 | 3.6 | 4.6 | 5.5 | 6.8 | 9.1 | 11 |
| | 1.5 | 1.3 | 1.9 | 2.6 | 3.9 | 5.2 | 6.5 | 7.8 | 9.7 | 13 | 15 |
| | | | | | | | | | | | |

TABLE 2C (Con.)

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|-------|--------------------------|---------------|---------------|-----|----------------|----------------|-----|----------------|----------------|-----|
| | | $\frac{1}{3}$ | $\frac{1}{2}$ | $\frac{2}{3}$ | 1 | $1\frac{1}{3}$ | $1\frac{2}{3}$ | 2 | $2\frac{1}{2}$ | $3\frac{1}{3}$ | 4 |
| Q | 0.010 | .080 | .12 | .16 | .24 | .32 | .39 | .48 | .59 | .79 | .95 |
| | 0.040 | .12 | .19 | .25 | .38 | .50 | .63 | .76 | .95 | 1.3 | 1.5 |
| | 0.065 | .16 | .25 | .33 | .50 | .66 | .83 | 1.0 | 1.2 | 1.6 | 2.0 |
| | 0.10 | .20 | .31 | .42 | .62 | .81 | 1.0 | 1.2 | 1.5 |) | 2.5 |
| | 0.15 | .28 | .42 | .56 | .84 | 1.1 | 1.4 | 1.7 | 2.1 | 3 | 3.4 |
| | 0.25 | .37 | .55 | .74 | 1.1 | 1.4 | 1.8 | 2.2 | 2.7 |) | 4.4 |
| | 0.40 | .47 | .70 | .94 | 1.4 | 1.8 | 2.3 | 2.8 | 3.5 | 4.7 | 5.6 |
| | 0.65 | .60 | .90 | 1.2 | 1.8 | 2.4 | 3.0 | 3.6 | 4.5 | 6.0 | 7.2 |
| | 1.0 | .80 | 1.2 | 1.6 | 2.4 | 3.2 | 4.0 | 4.8 | 6.0 | 8.1 | 9.7 |
| R | 0.025 | .080 | .12 | .16 | .24 | .32 | .39 | .48 | .59 | .79 | .95 |
| | 0.040 | .10 | .16 | .21 | .32 | .42 | .53 | .64 | .79 | 1.0 | 1.3 |
| | 0.065 | .13 | .19 | .26 | .39 | .51 | .65 | .78 | .97 | 1.3 | 1.5 |
| | 0.10 | .17 | .26 | .35 | .53 | .70 | .87 | 1.0 | 1.3 | 1.7 | 2.1 |
| | 0.15 | .22 | .33 | .44 | .66 | .88 | 1.1 | 1.3 | 1.6 | 2.2 | 2.6 |
| | 0.25 | .28 | .42 | .57 | .85 | 1.1 | 1.4 | 1.7 | 2.1 | 2.8 | 3.4 |
| | 0.40 | .37 | .55 | .74 | 1.1 | 1.4 | 1.8 | 2.2 | 2.7 | 3.7 | 4.4 |
| | 0.65 | .50 | .75 | 1.0 | 1.5 | 2.0 | 2.5 | 3.0 | 3.7 | 5.0 | 6.0 |

TABLE 2D
Table of Hazard Rate Ratios for t_2/t_1

| t_2/t_1 | $z(t_2)/z(t_1)$ | | | | | | | | | |
|-----------|--------------------------|------|------|------|-------|-------|------|-------|-------|------|
| | Shape Parameter, β | | | | | | | | | |
| | 1/3 | 1/2 | 2/3 | 1 | 1 1/3 | 1 2/3 | 2 | 2 1/2 | 3 1/3 | 4 |
| 1.25 | .862 | .894 | .928 | 1.00 | 1.08 | 1.16 | 1.25 | 1.40 | 1.68 | 1.95 |
| 1.50 | .763 | .816 | .873 | 1.00 | 1.14 | 1.31 | 1.50 | 1.84 | 2.57 | 3.38 |
| 1.75 | .689 | .756 | .823 | 1.00 | 1.21 | 1.45 | 1.75 | 2.32 | 3.69 | 5.36 |
| 2.00 | .630 | .707 | .794 | 1.00 | 1.26 | 1.59 | 2.00 | 2.83 | 5.04 | 8.00 |
| 2.25 | .583 | .667 | .763 | 1.00 | 1.31 | 1.72 | 2.25 | 2.38 | 6.64 | 11.4 |
| 2.50 | .543 | .632 | .734 | 1.00 | 1.36 | 1.84 | 2.50 | 3.95 | 8.49 | 15.6 |
| 2.75 | .510 | .603 | .714 | 1.00 | 1.40 | 1.96 | 2.75 | 4.56 | 10.6 | 20.8 |
| 3.00 | .481 | .577 | .694 | 1.00 | 1.44 | 2.08 | 3.00 | 5.20 | 13.0 | 27.0 |
| 3.25 | .456 | .555 | .675 | 1.00 | 1.48 | 2.19 | 3.25 | 5.86 | 15.6 | 34.3 |
| 3.50 | .434 | .534 | .659 | 1.00 | 1.52 | 2.30 | 3.50 | 6.55 | 18.4 | 42.9 |
| 3.75 | .414 | .516 | .644 | 1.00 | 1.55 | 2.42 | 3.75 | 7.26 | 21.8 | 52.7 |
| 4.00 | .397 | .500 | .630 | 1.00 | 1.59 | 2.52 | 4.00 | 8.00 | 25.4 | 64.0 |
| 4.25 | .381 | .485 | .617 | 1.00 | 1.62 | 2.62 | 4.25 | 8.76 | 29.3 | 76.8 |
| 4.50 | .367 | .472 | .606 | 1.00 | 1.65 | 2.73 | 4.50 | 9.54 | 33.4 | 91.1 |
| 4.75 | .354 | .459 | .595 | 1.00 | 1.68 | 2.83 | 4.75 | 10.4 | 37.9 | 107 |
| 5.00 | .342 | .447 | .585 | 1.00 | 1.71 | 2.92 | 5.00 | 11.2 | 42.8 | 125 |

TABLE 3A

100t/p Ratios at the Acceptable Quality Level (normal inspection)

for the MIL - STD - 105D Plans r = .90

| Acceptable Quality Level p' (%) | Shape Parameter, β | | | | | | | | | |
|---------------------------------|--------------------------|------|-------|------|-------|-------|------|-------|-------|------|
| | 1/3 | 1/2 | 2/3 | 1 | 1 1/3 | 1 2/3 | 2 | 2 1/2 | 3 1/3 | 4 |
| .010 | 86-9 | 90-6 | .0029 | .095 | .54 | 1.54 | 3.08 | 6.18 | 12.4 | 17.6 |
| .015 | 29-8 | 20-5 | .0054 | .14 | .91 | 1.96 | 3.77 | 7.27 | 14.0 | 19.4 |
| .025 | 13-7 | 56-5 | .016 | .24 | 1.08 | 2.66 | 4.87 | 8.92 | 16.3 | 22.1 |
| .040 | 55-7 | 14-4 | .023 | .38 | 1.53 | 3.53 | 6.16 | 10.8 | 18.8 | 24.8 |
| .065 | 24-6 | 38-4 | .048 | .62 | 2.20 | 4.72 | 7.85 | 13.1 | 21.7 | 28.0 |
| 0.10 | 86-6 | 90-4 | .092 | .95 | 3.04 | 6.12 | 9.74 | 15.5 | 24.7 | 31.2 |
| 0.15 | 29-5 | .020 | .17 | 1.42 | 4.12 | 7.80 | 11.9 | 18.3 | 27.9 | 34.5 |
| 0.25 | 13-4 | .056 | .37 | 2.37 | 6.04 | 10.6 | 15.4 | 22.4 | 32.6 | 39.2 |
| 0.40 | 55-4 | .15 | .74 | 3.81 | 8.62 | 14.1 | 19.5 | 27.1 | 37.5 | 44.2 |
| 0.65 | .024 | .38 | 1.54 | 6.19 | 12.4 | 18.8 | 24.9 | 32.9 | 43.4 | 49.9 |
| 1.0 | .087 | .91 | 2.95 | 9.54 | 17.2 | 24.4 | 30.9 | 39.1 | 49.4 | 55.6 |
| 1.5 | .30 | 2.06 | 5.43 | 14.3 | 23.3 | 31.2 | 37.9 | 46.0 | 55.8 | 61.5 |
| 2.5 | 1.39 | 5.78 | 11.8 | 24.0 | 34.3 | 42.5 | 49.0 | 56.5 | 56.2 | 70.0 |
| 4.0 | 5.82 | 15.0 | 24.1 | 38.7 | 49.1 | 56.6 | 62.2 | 68.4 | 75.2 | 78.9 |
| 6.5 | 26.0 | 40.7 | 50.9 | 63.8 | 71.4 | 76.4 | 79.9 | 83.6 | 87.4 | 89.4 |
| 10 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |

The negative figure after a ratio shows the number of decimal points to provide. Thus 56-5 = .00056.

TABLE 3B

100t/p Ratios at the Limiting Quality Level

for the MIL - STD - 105D Plans - r = .90 - Consumer's Risk = 0.10

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|------|--------------------------|-----|-----|-----|-------|-------|-----|-------|-------|-----|
| | | 1/3 | 1/2 | 2/3 | 1 | 1 1/3 | 1 2/3 | 2 | 2 1/2 | 3 1/3 | 4 |
| A | 6.5 | --- | --- | --- | --- | 600 | 420 | 330 | 260 | 200 | 180 |
| B | 4.0 | --- | --- | --- | 720 | 440 | 330 | 270 | 220 | 180 | 160 |
| C | 2.5 | --- | --- | 880 | 430 | 300 | 240 | 200 | 180 | 150 | 140 |
| C | 10 | --- | --- | --- | 810 | 480 | 350 | 290 | 230 | 180 | 160 |
| D | 1.5 | --- | 740 | 450 | 270 | 210 | 180 | 160 | 140 | 130 | 120 |
| D | 6.5 | --- | --- | --- | 490 | 330 | 260 | 220 | 190 | 160 | 140 |
| D | 10 | --- | --- | --- | 720 | 440 | 330 | 270 | 220 | 180 | 160 |
| E | 1.0 | 450 | 270 | 210 | 160 | 140 | 130 | 120 | 120 | 110 | 110 |
| E | 4.0 | --- | 920 | 500 | 290 | 220 | 190 | 170 | 150 | 130 | 130 |
| E | 6.5 | --- | --- | 850 | 420 | 290 | 230 | 200 | 170 | 150 | 140 |
| E | 10 | --- | --- | --- | 540 | 350 | 280 | 230 | 190 | 160 | 150 |
| F | 0.65 | 130 | 120 | 110 | 110 | 100 | 100 | 100 | 100 | 100 | 100 |
| F | 2.5 | 680 | 350 | 250 | 180 | 160 | 140 | 130 | 130 | 120 | 110 |
| F | 4.0 | --- | 740 | 450 | 270 | 210 | 180 | 160 | 140 | 130 | 120 |
| F | 6.5 | --- | --- | 620 | 330 | 250 | 200 | 180 | 160 | 140 | 130 |
| F | 10 | --- | --- | --- | 510 | 340 | 260 | 220 | 190 | 160 | 150 |
| G | 0.40 | 30 | 46 | 56 | 68 | 74 | 78 | 82 | 85 | 88 | 90 |
| G | 1.5 | 180 | 140 | 130 | 120 | 110 | 110 | 110 | 100 | 100 | 100 |
| G | 2.5 | 450 | 270 | 210 | 160 | 140 | 130 | 120 | 120 | 110 | 110 |
| G | 4.0 | 950 | 440 | 300 | 210 | 170 | 150 | 140 | 130 | 120 | 120 |
| G | 6.5 | --- | 920 | 500 | 290 | 220 | 190 | 170 | 150 | 130 | 130 |
| G | 10 | --- | --- | 760 | 390 | 280 | 220 | 190 | 170 | 150 | 130 |

TABLE 3B (Con.)

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|------|--------------------------|-----|-----|-----|-------|-------|-----|-------|-------|-----|
| | | 1/3 | 1/2 | 2/3 | 1 | 1 1/3 | 1 2/3 | 2 | 2 1/2 | 3 1/3 | 4 |
| H | 0.25 | 8.3 | 19 | 28 | 43 | 53 | 60 | 66 | 71 | 77 | 80 |
| H | 1.0 | 41 | 56 | 64 | 75 | 79 | 83 | 86 | 89 | 91 | 93 |
| H | 1.5 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| H | 2.5 | 220 | 170 | 150 | 130 | 120 | 110 | 110 | 110 | 100 | 100 |
| H | 4.0 | 680 | 350 | 250 | 180 | 160 | 140 | 130 | 130 | 120 | 110 |
| H | 6.5 | --- | 560 | 350 | 230 | 190 | 160 | 150 | 140 | 120 | 120 |
| H | 10 | --- | --- | 570 | 320 | 240 | 200 | 170 | 160 | 140 | 130 |
| J | 0.15 | 1.9 | 7.3 | 14 | 27 | 37 | 45 | 52 | 59 | 67 | 71 |
| J | 0.65 | 10 | 22 | 31 | 46 | 55 | 63 | 68 | 74 | 79 | 82 |
| J | 1.0 | 26 | 40 | 50 | 63 | 71 | 76 | 79 | 83 | 87 | 89 |
| J | 1.5 | 53 | 66 | 73 | 80 | 83 | 86 | 88 | 91 | 93 | 95 |
| J | 2.5 | 130 | 120 | 110 | 110 | 100 | 100 | 100 | 100 | 100 | 100 |
| J | 4.0 | 280 | 200 | 170 | 140 | 130 | 120 | 120 | 110 | 110 | 100 |
| J | 6.5 | 810 | 400 | 280 | 200 | 170 | 150 | 140 | 130 | 120 | 110 |
| J | 10 | --- | 680 | 410 | 260 | 200 | 170 | 160 | 140 | 130 | 120 |

TABLE 3B (Con.)

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | | |
|-------------|-------|--------------------------|-----|-----|-----|-------|-------|-----|-------|-------|-----|--|
| | | 1/3 | 1/2 | 2/3 | 1 | 1 1/3 | 1 2/3 | 2 | 2 1/2 | 3 1/3 | 4 | |
| K | 0.10 | .50 | 3.0 | 7.1 | 17 | 26 | 35 | 41 | 49 | 59 | 64 | |
| K | 0.40 | 2.6 | 9.0 | 16 | 29 | 40 | 48 | 55 | 62 | 69 | 74 | |
| K | 0.65 | 7.3 | 17 | 27 | 41 | 51 | 59 | 65 | 70 | 76 | 80 | |
| K | 1.0 | 14 | 28 | 38 | 53 | 61 | 67 | 72 | 77 | 82 | 85 | |
| K | 1.5 | 38 | 53 | 62 | 73 | 78 | 82 | 85 | 88 | 90 | 92 | |
| K | 2.5 | 81 | 88 | 90 | 93 | 94 | 95 | 95 | 96 | 97 | 98 | |
| K | 4.0 | 180 | 140 | 130 | 120 | 110 | 110 | 110 | 100 | 100 | 100 | |
| K | 6.5 | 450 | 270 | 210 | 160 | 140 | 130 | 120 | 120 | 110 | 110 | |
| K | 10 | --- | 620 | 380 | 240 | 190 | 170 | 150 | 140 | 130 | 120 | |
| L | 0.065 | .15 | 1.3 | 3.8 | 11 | 19 | 27 | 33 | 42 | 52 | 58 | |
| L | 0.25 | .70 | 3.6 | 8.4 | 19 | 29 | 37 | 43 | 51 | 60 | 66 | |
| L | 0.40 | 1.7 | 6.7 | 13 | 26 | 36 | 44 | 51 | 58 | 66 | 71 | |
| L | 0.65 | 3.1 | 10 | 18 | 31 | 42 | 50 | 57 | 63 | 70 | 74 | |
| L | 1.0 | 9.0 | 20 | 30 | 44 | 54 | 61 | 67 | 72 | 78 | 81 | |
| L | 1.5 | 19 | 33 | 43 | 57 | 65 | 71 | 76 | 80 | 84 | 87 | |
| L | 2.5 | 43 | 58 | 66 | 76 | 80 | 84 | 87 | 90 | 92 | 93 | |
| L | 4.0 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | |
| L | 6.5 | 280 | 200 | 170 | 140 | 130 | 120 | 120 | 110 | 110 | 100 | |
| M | 0.040 | .033 | .47 | 1.8 | 7.0 | 13 | 20 | 26 | 34 | 44 | 51 | |
| M | 0.15 | .15 | 1.3 | 3.8 | 11 | 19 | 27 | 33 | 42 | 52 | 58 | |
| M | 0.25 | .42 | 2.6 | 6.5 | 16 | 25 | 33 | 40 | 48 | 57 | 63 | |
| M | 0.40 | .82 | 4.0 | 9.0 | 20 | 30 | 38 | 45 | 53 | 61 | 66 | |
| M | 0.65 | 2.1 | 7.7 | 14 | 27 | 38 | 46 | 53 | 60 | 67 | 72 | |
| M | 1.0 | 4.5 | 12 | 21 | 35 | 46 | 54 | 60 | 66 | 73 | 77 | |
| M | 1.5 | 10 | 22 | 32 | 47 | 56 | 64 | 69 | 74 | 80 | 83 | |
| M | 2.5 | 24 | 39 | 47 | 62 | 69 | 75 | 79 | 82 | 86 | 86 | |
| M | 4.0 | 70 | 79 | 85 | 89 | 90 | 92 | 94 | 95 | 96 | 97 | |

TABLE 3 B (Con.)

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | | |
|-------------|-------|--------------------------|------|-----|-----|-------|-------|----|-------|-------|----|--|
| | | 1/3 | 1/2 | 2/3 | 1 | 1.1/3 | 1 2/3 | 2 | 2 1/2 | 3 1/3 | 4 | |
| N | 0.025 | .0082 | .19 | .90 | 4.3 | 9.3 | 15 | 21 | 28 | 38 | 45 | |
| N | 0.10 | .040 | .54 | 2.0 | 7.4 | 14 | 21 | 27 | 35 | 45 | 52 | |
| N | 0.15 | .11 | 1.1 | 3.4 | 10 | 18 | 25 | 32 | 40 | 50 | 56 | |
| N | 0.25 | .19 | 1.5 | 4.4 | 12 | 21 | 28 | 35 | 43 | 53 | 59 | |
| N | 0.40 | .60 | 3.3 | 7.7 | 18 | 27 | 36 | 43 | 50 | 59 | 65 | |
| N | 0.65 | 1.2 | 5.3 | 11 | 23 | 33 | 41 | 48 | 55 | 64 | 68 | |
| N | 1.0 | 2.6 | 9.0 | 16 | 29 | 40 | 48 | 55 | 62 | 69 | 74 | |
| N | 1.5 | 5.8 | 15 | 24 | 38 | 49 | 56 | 62 | 68 | 75 | 78 | |
| N | 2.5 | 16 | 30 | 40 | 55 | 63 | 69 | 74 | 78 | 83 | 86 | |
| P | 0.015 | 21-4 | .076 | .45 | 2.7 | 6.6 | 11 | 16 | 23 | 33 | 40 | |
| P | 0.065 | 0.10 | .21 | 1.0 | 4.6 | 10 | 15 | 21 | 29 | 39 | 46 | |
| P | 0.10 | .025 | .40 | 1.6 | 6.3 | 12 | 19 | 25 | 33 | 43 | 50 | |
| P | 0.15 | .050 | .63 | 2.2 | 8.0 | 15 | 22 | 28 | 36 | 46 | 53 | |
| P | 0.25 | .15 | 1.3 | 3.8 | 11 | 19 | 27 | 33 | 42 | 52 | 58 | |
| P | 0.40 | .29 | 2.0 | 5.4 | 14 | 23 | 31 | 37 | 46 | 55 | 61 | |
| P | 0.65 | .60 | 3.3 | 7.7 | 18 | 27 | 36 | 43 | 50 | 59 | 65 | |
| P | 1.0 | 1.3 | 5.7 | 11 | 24 | 34 | 42 | 49 | 56 | 65 | 70 | |
| P | 1.5 | 3.8 | 11 | 19 | 33 | 44 | 52 | 58 | 65 | 72 | 76 | |
| Q | 0.010 | 52-5 | .029 | .22 | 1.7 | 46 | 8.7 | 13 | 19 | 29 | 36 | |
| Q | 0.040 | 25-4 | .086 | .50 | 2.9 | 7.0 | 12 | 17 | 24 | 34 | 41 | |
| Q | 0.065 | 68-4 | .16 | .81 | 4.1 | 8.9 | 14 | 20 | 27 | 38 | 44 | |
| Q | 0.10 | .012 | .25 | 1.1 | 5.0 | 10 | 16 | 22 | 30 | 40 | 46 | |
| Q | 0.15 | .034 | .49 | 1.8 | 7.1 | 13 | 20 | 26 | 34 | 44 | 51 | |
| Q | 0.25 | .071 | .78 | 2.6 | 9.0 | 16 | 23 | 30 | 38 | 48 | 54 | |
| Q | 0.40 | .15 | 1.3 | 3.8 | 11 | 19 | 27 | 33 | 42 | 52 | 58 | |
| Q | 0.65 | .35 | 2.3 | 6.0 | 15 | 24 | 32 | 39 | 47 | 56 | 62 | |
| Q | 1.0 | 1.0 | 4.9 | 10 | 22 | 32 | 40 | 47 | 54 | 63 | 68 | |

TABLE 3B (Con.)

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|-------|--------------------------|------|-----|-----|-------|-------|----|-------|-------|----|
| | | 1/3 | 1/2 | 2/3 | 1 | 1 1/3 | 1 2/3 | 2 | 2 1/2 | 3 1/3 | 4 |
| R | 0.025 | 70-5 | .036 | .26 | 1.9 | 5.1 | 9.2 | 13 | 20 | 30 | 37 |
| R | 0.040 | 16-4 | .065 | .40 | 2.5 | 6.3 | 11 | 16 | 23 | 33 | 39 |
| R | 0.065 | 30-4 | .098 | .55 | 3.1 | 7.3 | 12 | 17 | 25 | 35 | 42 |
| R | 0.10 | 82-4 | .19 | .90 | 4.3 | 9.3 | 15 | 21 | 29 | 38 | 45 |
| R | 0.15 | .017 | .31 | 1.3 | 5.6 | 11 | 17 | 23 | 31 | 42 | 48 |
| R | 0.25 | .039 | .53 | 2.0 | 7.3 | 14 | 20 | 27 | 35 | 45 | 52 |
| R | 0.40 | .087 | .91 | 2.9 | 9.5 | 17 | 24 | 30 | 39 | 49 | 55 |
| R | 0.65 | .24 | 1.8 | 4.9 | 13 | 22 | 30 | 36 | 44 | 54 | 60 |

The negative figure after a ratio shows the number of decimal points to provide. Thus, 21-4 = .0021.

TABLE 3C

100t/ ρ Ratios at the Limiting Quality Level for the

MIL-STD-105D Plans - r = .90 - Consumer's Risk = 0.05

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|------|--------------------------|------|-----|------|-------|-------|-----|-------|-------|-----|
| | | 1/3 | 1/2 | 2/3 | 1 | 1 1/3 | 1 2/3 | 2 | 2 1/2 | 3 1/3 | 4 |
| A | 6.5 | --- | --- | --- | --- | 730 | 490 | 380 | 280 | 220 | 190 |
| B | 4.0 | --- | --- | --- | 930 | 540 | 380 | 310 | 240 | 190 | 170 |
| C | 2.5 | --- | --- | --- | 550 | 360 | 280 | 230 | 200 | 160 | 150 |
| C | 10 | --- | --- | --- | 1000 | 570 | 410 | 320 | 250 | 200 | 180 |
| D | 1.5 | --- | --- | 640 | 350 | 250 | 210 | 180 | 160 | 140 | 130 |
| D | 6.5 | --- | --- | --- | 590 | 380 | 290 | 240 | 200 | 170 | 150 |
| D | 10 | --- | --- | --- | 860 | 500 | 370 | 290 | 240 | 190 | 170 |
| E | 1.0 | --- | 500 | 320 | 220 | 180 | 160 | 140 | 130 | 120 | 120 |
| E | 4.0 | --- | --- | 680 | 360 | 260 | 210 | 190 | 160 | 140 | 130 |
| E | 6.5 | --- | --- | --- | 490 | 330 | 260 | 220 | 190 | 160 | 140 |
| E | 10 | --- | --- | --- | 660 | 410 | 310 | 250 | 210 | 170 | 160 |
| F | 0.65 | 280 | 200 | 170 | 140 | 130 | 120 | 120 | 110 | 110 | 100 |
| F | 2.5 | --- | 560 | 360 | 230 | 190 | 160 | 150 | 140 | 120 | 120 |
| F | 4.0 | --- | 1000 | 540 | 310 | 230 | 200 | 170 | 150 | 140 | 130 |
| F | 6.5 | --- | --- | 760 | 390 | 280 | 220 | 190 | 170 | 150 | 130 |
| F | 10 | --- | --- | --- | 570 | 370 | 290 | 240 | 200 | 170 | 150 |
| G | 0.40 | 68 | 79 | 83 | 88 | 90 | 92 | 93 | 94 | 96 | 97 |
| G | 1.5 | 280 | 200 | 170 | 140 | 130 | 120 | 120 | 110 | 110 | 100 |
| G | 2.5 | 680 | 350 | 250 | 180 | 160 | 140 | 130 | 130 | 120 | 110 |
| G | 4.0 | --- | 620 | 380 | 240 | 190 | 170 | 150 | 140 | 130 | 120 |
| G | 6.5 | --- | --- | 620 | 340 | 250 | 200 | 180 | 160 | 140 | 130 |
| G | 10 | --- | --- | 880 | 430 | 300 | 240 | 200 | 180 | 150 | 140 |
| H | 0.25 | 18 | 32 | 42 | 57 | 65 | 70 | 75 | 79 | 84 | 86 |
| H | 1.0 | 74 | 82 | 87 | 90 | 91 | 92 | 94 | 95 | 96 | 97 |
| H | 1.5 | 180 | 140 | 130 | 120 | 110 | 110 | 110 | 100 | 100 | 100 |
| H | 2.5 | 360 | 230 | 190 | 150 | 130 | 130 | 120 | 120 | 110 | 110 |
| H | 4.0 | 950 | 440 | 300 | 210 | 170 | 150 | 140 | 130 | 120 | 120 |
| H | 6.5 | --- | 740 | 450 | 270 | 210 | 180 | 160 | 150 | 130 | 120 |
| H | 10 | --- | --- | 680 | 360 | 260 | 210 | 190 | 160 | 140 | 130 |

TABLE 3C (Con.)

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|-------|--------------------------|-----|-----|-----|-------|-------|-----|-------|-------|-----|
| | | 1/3 | 1/2 | 2/3 | 1 | 1 1/3 | 1 2/3 | 2 | 2 1/2 | 3 1/3 | 4 |
| J | 0.15 | 4.5 | 12 | 21 | 35 | 46 | 54 | 60 | 66 | 73 | 77 |
| J | 0.65 | 18 | 32 | 42 | 57 | 65 | 70 | 75 | 79 | 84 | 89 |
| J | 1.0 | 43 | 58 | 66 | 76 | 80 | 84 | 87 | 90 | 92 | 93 |
| J | 1.5 | 81 | 88 | 90 | 93 | 94 | 95 | 95 | 96 | 97 | 98 |
| J | 2.5 | 220 | 170 | 150 | 130 | 120 | 110 | 110 | 110 | 100 | 100 |
| J | 4.0 | 450 | 270 | 210 | 160 | 140 | 130 | 120 | 120 | 110 | 110 |
| J | 6.5 | 950 | 450 | 300 | 210 | 170 | 150 | 140 | 130 | 120 | 120 |
| J | 10 | --- | 840 | 470 | 280 | 220 | 180 | 160 | 150 | 130 | 120 |
| K | 0.10 | 1.2 | 5.3 | 11 | 23 | 33 | 41 | 48 | 55 | 64 | 68 |
| K | 0.40 | 4.9 | 13 | 22 | 36 | 47 | 55 | 60 | 67 | 74 | 77 |
| K | 0.65 | 11 | 23 | 34 | 48 | 58 | 64 | 69 | 75 | 80 | 83 |
| K | 1.0 | 22 | 37 | 47 | 60 | 68 | 73 | 78 | 81 | 85 | 88 |
| K | 1.5 | 57 | 70 | 75 | 83 | 86 | 88 | 90 | 92 | 94 | 95 |
| K | 2.5 | 130 | 120 | 110 | 110 | 100 | 100 | 100 | 100 | 100 | 100 |
| K | 4.0 | 280 | 200 | 170 | 140 | 130 | 120 | 120 | 110 | 110 | 100 |
| K | 6.5 | 680 | 350 | 250 | 180 | 160 | 140 | 130 | 130 | 120 | 110 |
| K | 10 | --- | 680 | 410 | 260 | 200 | 170 | 160 | 140 | 130 | 120 |
| L | 0.065 | .29 | 2.0 | 5.4 | 4 | 23 | 31 | 37 | 46 | 55 | 61 |
| L | 0.25 | 1.2 | 5.3 | 11 | 23 | 33 | 41 | 48 | 55 | 64 | 68 |
| L | 0.40 | 3.0 | 9.5 | 17 | 30 | 41 | 49 | 56 | 62 | 70 | 74 |
| L | 0.65 | 5.4 | 14 | 23 | 37 | 48 | 55 | 62 | 67 | 74 | 78 |
| L | 1.0 | 13 | 27 | 37 | 51 | 60 | 67 | 72 | 76 | 81 | 84 |
| L | 1.5 | 27 | 42 | 52 | 64 | 71 | 76 | 80 | 84 | 87 | 90 |
| L | 2.5 | 59 | 71 | 76 | 84 | 87 | 89 | 90 | 92 | 94 | 95 |
| L | 4.0 | 130 | 120 | 110 | 110 | 100 | 100 | 100 | 100 | 100 | 100 |
| L | 6.5 | 360 | 230 | 190 | 150 | 130 | 130 | 120 | 120 | 110 | 110 |

TABLE 3C (Con.)

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|-------|--------------------------|-----|-----|-----|-------|-------|----|-------|-------|----|
| | | 1/3 | 1/2 | 2/3 | 1 | 1 1/3 | 1 2/3 | 2 | 2 1/2 | 3 1/3 | 4 |
| M | 0.040 | .073 | .81 | 2.7 | 9.1 | 16 | 23 | 30 | 38 | 48 | 55 |
| M | 0.15 | .29 | 2.0 | 5.4 | 4 | 23 | 31 | 37 | 46 | 55 | 61 |
| M | 0.25 | .70 | 3.6 | 8.4 | 19 | 29 | 37 | 43 | 51 | 60 | 66 |
| M | 0.40 | 1.3 | 5.7 | 11 | 24 | 34 | 42 | 49 | 56 | 65 | 70 |
| M | 0.65 | 3.1 | 10 | 18 | 31 | 42 | 50 | 57 | 63 | 70 | 74 |
| M | 1.0 | 6.7 | 16 | 26 | 40 | 50 | 58 | 64 | 70 | 76 | 80 |
| M | 1.5 | 14 | 28 | 38 | 53 | 61 | 67 | 72 | 77 | 82 | 85 |
| M | 2.5 | 32 | 47 | 57 | 69 | 74 | 78 | 82 | 86 | 88 | 90 |
| M | 4.0 | 87 | 91 | 93 | 95 | 96 | 97 | 97 | 98 | 98 | 98 |
| N | 0.025 | .018 | .32 | 1.3 | 5.7 | 11 | 18 | 24 | 31 | 42 | 48 |
| N | 0.10 | .074 | .80 | 2.7 | 9.1 | 16 | 23 | 30 | 38 | 48 | 54 |
| N | 0.15 | .19 | 1.5 | 4.4 | 12 | 21 | 28 | 35 | 43 | 53 | 59 |
| N | 0.25 | .35 | 2.3 | 6.0 | 15 | 24 | 32 | 39 | 47 | 56 | 62 |
| N | 0.40 | .82 | 4.0 | 9.0 | 20 | 30 | 38 | 45 | 53 | 61 | 66 |
| N | 0.65 | 1.5 | 6.2 | 12 | 25 | 35 | 43 | 50 | 57 | 65 | 70 |
| N | 1.0 | 3.5 | 10 | 18 | 32 | 43 | 51 | 57 | 64 | 71 | 75 |
| N | 1.5 | 7.8 | 18 | 27 | 42 | 52 | 59 | 65 | 71 | 77 | 80 |
| N | 2.5 | 21 | 36 | 46 | 59 | 67 | 73 | 77 | 81 | 85 | 88 |
| P | 0.015 | 47-4 | .13 | .68 | 3.6 | 8.1 | 13 | 19 | 26 | 36 | 43 |
| P | 0.065 | .017 | .31 | 1.3 | 5.6 | 11 | 17 | 23 | 31 | 42 | 48 |
| P | 0.10 | .042 | .56 | 2.0 | 7.5 | 14 | 21 | 27 | 35 | 45 | 52 |
| P | 0.15 | .080 | .84 | 2.8 | 9.3 | 16 | 24 | 30 | 38 | 48 | 55 |
| P | 0.25 | .19 | 1.5 | 4.4 | 12 | 21 | 28 | 35 | 43 | 53 | 59 |
| P | 0.40 | .35 | 2.3 | 6.0 | 15 | 24 | 32 | 39 | 47 | 56 | 62 |
| P | 0.65 | .82 | 4.0 | 9.0 | 20 | 30 | 38 | 45 | 53 | 61 | 66 |
| P | 1.0 | 1.7 | 6.7 | 13 | 26 | 36 | 44 | 51 | 58 | 66 | 71 |
| P | 1.5 | 4.9 | 13 | 22 | 36 | 47 | 55 | 60 | 67 | 74 | 77 |

TABLE 3C (Con.)

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | | |
|-------------|-------|--------------------------|------|-----|-----|-------|-------|----|-------|-------|----|--|
| | | 1/3 | 1/2 | 2/3 | 1 | 1 1/3 | 1 2/3 | 2 | 2 1/2 | 3 1/3 | 4 | |
| Q | 0.010 | 12-4 | .052 | .34 | 2.2 | 5.8 | 10 | 15 | 22 | 32 | 38 | |
| Q | 0.040 | 47-4 | .13 | .68 | 3.6 | 8.1 | 13 | 19 | 26 | 36 | 43 | |
| Q | 0.065 | .011 | .22 | 1.0 | 4.7 | 10 | 16 | 21 | 29 | 40 | 46 | |
| Q | 0.10 | .020 | .34 | 1.5 | 5.9 | 12 | 18 | 24 | 32 | 42 | 49 | |
| Q | 0.15 | .050 | .63 | 2.2 | 8.0 | 15 | 22 | 28 | 36 | 46 | 53 | |
| Q | 0.25 | .11 | 1.1 | 3.4 | 10 | 18 | 25 | 32 | 40 | 50 | 56 | |
| Q | 0.40 | .24 | 1.8 | 4.9 | 13 | 22 | 30 | 36 | 44 | 54 | 60 | |
| Q | 0.65 | 50 | 3.0 | 7.1 | 17 | 26 | 35 | 41 | 49 | 59 | 64 | |
| Q | 1.0 | 1.2 | 5.3 | 11 | 23 | 33 | 41 | 48 | 55 | 64 | 68 | |
| R | 0.025 | 12-4 | .052 | .34 | 2.2 | 5.8 | 10 | 15 | 22 | 32 | 38 | |
| R | 0.040 | 28-4 | .091 | .52 | 3.0 | 7.1 | 12 | 17 | 24 | 35 | 41 | |
| R | 0.065 | 50-4 | .13 | .70 | 3.7 | 8.3 | 14 | 19 | 26 | 37 | 43 | |
| R | 0.10 | .012 | .25 | 1.1 | 5.0 | 10 | 16 | 22 | 30 | 40 | 46 | |
| R | 0.15 | .025 | .39 | 1.5 | 6.3 | 12 | 19 | 25 | 33 | 43 | 50 | |
| R | 0.25 | .053 | .65 | 2.3 | 8.0 | 15 | 22 | 28 | 36 | 46 | 53 | |
| R | 0.40 | .11 | 1.1 | 3.4 | 10 | 18 | 25 | 32 | 40 | 50 | 56 | |
| R | 0.65 | .29 | 2.0 | 5.4 | 14 | 23 | 31 | 37 | 45 | 55 | 61 | |

The negative figure after a ratio shows the number of decimal points to provide. Thus, 47-4 = .0047

TABLE 4A
 100t/p Ratios at the Acceptable Quality Level (normal inspection)
 for the MIL-STD-105D Plans r = .99

| Acceptable Quality Level p (%) | Shape Parameter, β | | | | | | | | | |
|--------------------------------|--------------------------|-------|------|------|-------|-------|------|-------|-------|------|
| | 1/3 | 1/2 | 2/3 | 1 | 1 1/3 | 1 2/3 | 2 | 2 1/2 | 3 1/3 | 4 |
| .010 | 99.6 | .010 | .10 | .99 | 3.15 | 6.29 | 9.98 | 15.8 | 25.1 | 31.6 |
| .015 | 33.5 | .022 | .18 | 1.49 | 4.26 | 8.02 | 12.2 | 18.6 | 28.3 | 34.9 |
| .025 | 15.4 | .062 | .39 | 2.49 | 6.26 | 10.9 | 15.8 | 22.8 | 33.0 | 39.7 |
| .040 | 63.4 | .16 | .79 | 3.98 | 8.91 | 14.5 | 20.0 | 27.5 | 38.0 | 44.7 |
| .065 | 027 | .42 | 1.64 | 6.47 | 12.8 | 19.3 | 25.4 | 33.4 | 44.0 | 50.4 |
| 0.10 | .10 | .99 | 3.14 | 9.95 | 17.7 | 25.0 | 31.5 | 39.7 | 50.0 | 56.2 |
| 0.15 | .33 | 2.23 | 5.76 | 14.9 | 24.0 | 31.9 | 38.6 | 46.7 | 56.5 | 62.2 |
| 0.25 | 1.54 | 6.19 | 12.4 | 24.9 | 35.2 | 43.4 | 49.9 | 57.3 | 65.9 | 70.6 |
| 0.40 | 6.35 | 15.9 | 25.2 | 39.9 | 50.2 | 57.6 | 63.2 | 69.2 | 75.9 | 79.5 |
| 0.65 | 27.3 | 42.1 | 52.2 | 64.9 | 72.3 | 77.1 | 80.6 | 84.1 | 87.8 | 89.8 |
| 1.0 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| 1.5 | 340 | 226 | 184 | 150 | 136 | 128 | 123 | 118 | 113 | 111 |
| 2.5 | 1600 | 635 | 400 | 252 | 200 | 174 | 159 | 145 | 132 | 126 |
| 4.0 | 6700 | 1650 | 818 | 406 | 286 | 232 | 202 | 175 | 152 | 142 |
| 6.5 | 29900 | 4470 | 1730 | 669 | 416 | 313 | 259 | 214 | 177 | 161 |
| 10 | 116000 | 11000 | 3390 | 1050 | 582 | 410 | 324 | 256 | 202 | 180 |

The negative figure after a ratio shows the number of decimal points to provide. Thus, 33.5 = .00033.

TABLE 4B
 100t/p Ratios at the Limiting Quality Level for the
 MIL-STD-105D Plans - r = .99 - Consumer's Risk = 0.10

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|------|--------------------------|------|------|------|-------|-------|------|-------|-------|-----|
| | | 1/3 | 1/2 | 2/3 | 1 | 1 1/3 | 1 2/3 | 2 | 2 1/2 | 3 1/3 | 4 |
| A | 6.5 | --- | --- | --- | --- | 3300 | 1700 | 1000 | 660 | 410 | 320 |
| B | 4.0 | --- | --- | --- | 7700 | 2500 | 1300 | 880 | 560 | 360 | 290 |
| C | 2.5 | --- | --- | --- | 4600 | 1700 | 980 | 680 | 460 | 310 | 250 |
| C | 10 | --- | --- | --- | 8700 | 2700 | 1400 | 930 | 590 | 380 | 300 |
| D | 1.5 | --- | --- | --- | 2800 | 1200 | 740 | 530 | 380 | 270 | 230 |
| D | 6.5 | --- | --- | --- | 5300 | 1900 | 1000 | 720 | 480 | 350 | 260 |
| D | 10 | --- | --- | --- | 7700 | 2500 | 1300 | 880 | 560 | 360 | 290 |
| E | 1.0 | --- | --- | 7300 | 1700 | 840 | 540 | 410 | 310 | 230 | 200 |
| E | 4.0 | --- | --- | --- | 3100 | 1300 | 770 | 560 | 390 | 280 | 230 |
| E | 6.5 | --- | --- | --- | 4400 | 1700 | 960 | 660 | 450 | 310 | 250 |
| E | 10 | --- | --- | --- | 5800 | 2000 | 1100 | 760 | 500 | 330 | 270 |
| F | 0.65 | --- | --- | 3900 | 1100 | 620 | 410 | 330 | 260 | 210 | 180 |
| F | 2.5 | --- | --- | 8800 | 1900 | 930 | 590 | 440 | 320 | 240 | 210 |
| F | 4.0 | --- | --- | --- | 2800 | 1200 | 740 | 530 | 380 | 270 | 230 |
| F | 6.5 | --- | --- | --- | 3500 | 1400 | 850 | 590 | 410 | 290 | 240 |
| F | 10 | --- | --- | --- | 5500 | 1900 | 1000 | 730 | 490 | 330 | 270 |
| G | 0.40 | --- | 5000 | 1800 | 710 | 430 | 320 | 260 | 210 | 180 | 160 |
| G | 1.5 | --- | --- | 4500 | 1200 | 670 | 460 | 350 | 270 | 210 | 180 |
| G | 2.5 | --- | --- | 7300 | 1700 | 840 | 540 | 410 | 310 | 230 | 200 |
| G | 4.0 | --- | --- | --- | 2200 | 1000 | 640 | 470 | 340 | 250 | 210 |
| G | 6.5 | --- | --- | --- | 3100 | 1300 | 770 | 560 | 390 | 280 | 230 |
| G | 10 | --- | --- | --- | 4100 | 1600 | 920 | 640 | 440 | 300 | 250 |

TABLE 4B (Con.)

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|------|--------------------------|------|------|------|-------|-------|-----|-------|-------|-----|
| | | 1/3 | 1/2 | 2/3 | 1 | 1 1/3 | 1 2/3 | 2 | 2 1/2 | 3 1/3 | 4 |
| H | 0.25 | 9400 | 2100 | 960 | 450 | 310 | 250 | 210 | 180 | 150 | 140 |
| H | 1.0 | --- | 6100 | 2200 | 790 | 460 | 340 | 270 | 220 | 180 | 160 |
| H | 1.5 | --- | --- | 3300 | 1000 | 580 | 410 | 320 | 250 | 200 | 180 |
| H | 2.5 | --- | --- | 5100 | 1400 | 7.0 | 480 | 370 | 280 | 220 | 190 |
| H | 4.0 | --- | --- | 8800 | 1900 | 930 | 590 | 440 | 320 | 240 | 210 |
| H | 6.5 | --- | --- | --- | 2500 | 1100 | 670 | 500 | 360 | 260 | 220 |
| H | 10 | --- | --- | --- | 3400 | 1400 | 820 | 580 | 400 | 290 | 240 |
| J | 0.15 | 2300 | 800 | 460 | 280 | 210 | 180 | 160 | 150 | 130 | 130 |
| J | 0.65 | --- | 2400 | 1000 | 490 | 320 | 260 | 210 | 180 | 160 | 150 |
| J | 1.0 | --- | 4400 | 1700 | 660 | 410 | 310 | 250 | 210 | 170 | 160 |
| J | 1.5 | --- | 7300 | 2500 | 860 | 490 | 360 | 290 | 230 | 190 | 170 |
| J | 2.5 | --- | --- | 3900 | 1100 | 620 | 410 | 330 | 260 | 210 | 180 |
| J | 4.0 | --- | --- | 5800 | 1500 | 750 | 500 | 380 | 290 | 220 | 190 |
| J | 6.5 | --- | --- | 9400 | 2100 | 970 | 610 | 460 | 330 | 250 | 210 |
| J | 10 | --- | --- | --- | 2700 | 1100 | 710 | 520 | 370 | 270 | 220 |
| K | 0.10 | 600 | 320 | 240 | 180 | 150 | 140 | 130 | 120 | 120 | 110 |
| K | 0.40 | 3100 | 980 | 540 | 310 | 230 | 200 | 170 | 150 | 140 | 130 |
| K | 0.65 | 8200 | 1900 | 900 | 440 | 300 | 240 | 200 | 180 | 150 | 140 |
| K | 1.0 | --- | 3000 | 1200 | 550 | 350 | 280 | 230 | 190 | 160 | 150 |
| K | 1.5 | --- | 5800 | 2100 | 760 | 450 | 340 | 270 | 220 | 180 | 160 |
| K | 2.5 | --- | 9500 | 3000 | 980 | 550 | 390 | 310 | 250 | 190 | 170 |
| K | 4.0 | --- | --- | 4500 | 1200 | 670 | 460 | 350 | 270 | 210 | 180 |
| K | 6.5 | --- | --- | 7300 | 1700 | 840 | 540 | 410 | 310 | 230 | 200 |
| K | 10 | --- | --- | --- | 2600 | 1100 | 690 | 510 | 360 | 260 | 220 |

TABLE 4B (Con.)

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|-------|--------------------------|------|------|------|-------|-------|-----|-------|-------|-----|
| | | 1/3 | 1/2 | 2/3 | 1 | 1 1/3 | 1 2/3 | 2 | 2 1/2 | 3 1/3 | 4 |
| L | 0.065 | 170 | 140 | 130 | 120 | 110 | 110 | 110 | 100 | 100 | 100 |
| L | 0.25 | 810 | 400 | 280 | 200 | 160 | 150 | 140 | 130 | 120 | 110 |
| L | 0.40 | 2000 | 740 | 440 | 270 | 210 | 180 | 160 | 140 | 130 | 120 |
| L | 0.65 | 3700 | 1100 | 590 | 330 | 240 | 200 | 180 | 160 | 140 | 130 |
| L | 1.0 | 9900 | 2200 | 1000 | 470 | 310 | 250 | 210 | 180 | 150 | 140 |
| L | 1.5 | --- | 3600 | 1400 | 610 | 380 | 290 | 240 | 200 | 170 | 150 |
| L | 2.5 | --- | 6300 | 2200 | 800 | 470 | 350 | 280 | 220 | 180 | 160 |
| L | 4.0 | --- | --- | 3300 | 1000 | 580 | 410 | 320 | 250 | 200 | 180 |
| L | 6.5 | --- | --- | 5800 | 1500 | 750 | 500 | 380 | 290 | 220 | 190 |
| M | 0.040 | 38 | 53 | 62 | 72 | 78 | 82 | 84 | 87 | 90 | 92 |
| M | 0.15 | 170 | 140 | 130 | 120 | 110 | 110 | 110 | 100 | 100 | 100 |
| M | 0.25 | 500 | 290 | 220 | 170 | 150 | 130 | 130 | 120 | 110 | 110 |
| M | 0.40 | 950 | 440 | 300 | 210 | 170 | 150 | 140 | 130 | 120 | 120 |
| M | 0.65 | 2500 | 870 | 490 | 290 | 220 | 190 | 170 | 150 | 130 | 130 |
| M | 1.0 | 5300 | 1400 | 710 | 370 | 260 | 220 | 190 | 160 | 140 | 140 |
| M | 1.5 | --- | 2500 | 1100 | 500 | 330 | 260 | 220 | 180 | 160 | 150 |
| M | 2.5 | --- | 4200 | 1600 | 660 | 400 | 310 | 250 | 210 | 170 | 160 |
| M | 4.0 | --- | 8800 | 2800 | 940 | 530 | 380 | 300 | 240 | 190 | 170 |
| N | 0.025 | 9.7 | 21 | 30 | 45 | 55 | 62 | 67 | 72 | 79 | 82 |
| N | 0.10 | 47 | 60 | 68 | 77 | 82 | 86 | 88 | 90 | 92 | 94 |
| N | 0.15 | 130 | 120 | 110 | 110 | 110 | 100 | 100 | 100 | 100 | 100 |
| N | 0.25 | 220 | 170 | 150 | 130 | 120 | 110 | 110 | 110 | 100 | 100 |
| N | 0.40 | 700 | 360 | 260 | 190 | 160 | 140 | 130 | 120 | 120 | 110 |
| N | 0.65 | 1400 | 580 | 370 | 240 | 190 | 170 | 150 | 140 | 130 | 120 |
| N | 1.0 | 3100 | 980 | 540 | 310 | 230 | 200 | 170 | 150 | 140 | 130 |
| N | 1.5 | 6700 | 1600 | 810 | 400 | 280 | 230 | 200 | 170 | 150 | 140 |
| N | 2.5 | --- | 3200 | 1300 | 580 | 360 | 280 | 230 | 200 | 160 | 150 |

TABLE 4B (Con.)

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|-------|--------------------------|------|-----|-----|-------|-------|-----|-------|-------|-----|
| | | 1/3 | 1/2 | 2/3 | 1 | 1 1/3 | 1 2/3 | 2 | 2 1/2 | 3 1/3 | 4 |
| P | 0.015 | 2.4 | 8.2 | 15 | 28 | 39 | 47 | 53 | 60 | 69 | 73 |
| P | 0.065 | 11 | 24 | 34 | 48 | 57 | 64 | 69 | 74 | 80 | 83 |
| P | 0.10 | 30 | 44 | 54 | 66 | 73 | 78 | 80 | 84 | 88 | 90 |
| P | 0.15 | 59 | 70 | 76 | 83 | 87 | 89 | 90 | 92 | 94 | 95 |
| P | 0.25 | 170 | 140 | 130 | 120 | 110 | 110 | 110 | 100 | 100 | 100 |
| P | 0.40 | 340 | 220 | 180 | 150 | 130 | 120 | 120 | 110 | 110 | 110 |
| P | 0.65 | 700 | 360 | 260 | 190 | 160 | 140 | 130 | 120 | 120 | 110 |
| P | 1.0 | 1600 | 630 | 400 | 250 | 200 | 170 | 150 | 140 | 130 | 120 |
| P | 1.5 | 4500 | 1200 | 650 | 350 | 250 | 210 | 180 | 160 | 140 | 130 |
| Q | 0.010 | .58 | 3.2 | 7.5 | 18 | 27 | 35 | 42 | 50 | 59 | 64 |
| Q | 0.040 | 2.9 | 9.3 | 17 | 30 | 41 | 49 | 55 | 62 | 70 | 74 |
| Q | 0.065 | 8.0 | 18 | 28 | 42 | 52 | 60 | 64 | 70 | 77 | 80 |
| Q | 0.10 | 15 | 28 | 38 | 52 | 61 | 68 | 72 | 77 | 82 | 85 |
| Q | 0.15 | 40 | 54 | 63 | 73 | 78 | 82 | 85 | 88 | 91 | 93 |
| Q | 0.25 | 80 | 87 | 90 | 92 | 94 | 95 | 96 | 97 | 98 | 98 |
| Q | 0.40 | 170 | 140 | 130 | 120 | 110 | 110 | 110 | 100 | 100 | 100 |
| Q | 0.65 | 410 | 250 | 200 | 160 | 140 | 130 | 120 | 110 | 110 | 110 |
| Q | 1.0 | 1200 | 530 | 340 | 230 | 180 | 160 | 150 | 140 | 120 | 120 |
| R | 0.025 | .80 | 3.9 | 8.8 | 20 | 29 | 37 | 44 | 52 | 61 | 66 |
| R | 0.040 | 1.9 | 7.0 | 14 | 26 | 37 | 45 | 51 | 59 | 67 | 72 |
| R | 0.065 | 3.6 | 11 | 18 | 32 | 43 | 51 | 56 | 64 | 71 | 75 |
| R | 0.10 | 9.7 | 21 | 30 | 45 | 55 | 62 | 67 | 72 | 79 | 82 |
| R | 0.15 | 20 | 34 | 45 | 58 | 66 | 72 | 76 | 80 | 85 | 87 |
| R | 0.25 | 45 | 59 | 66 | 76 | 81 | 84 | 86 | 89 | 92 | 94 |
| R | 0.40 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| R | 0.65 | 270 | 190 | 160 | 140 | 120 | 120 | 110 | 110 | 110 | 100 |

TABLE 4C

100t/ ρ Ratios at the Limiting Quality Level for the

MIL-STD-105D Plans - r = .99 - Consumer's Risk = 0.05

| Code Letter | AQL | Shape Parameter, β | | | | | | | | | |
|-------------|-----|--------------------------|------|------|------|-----------------|-----------------|------|-----------------|-----------------|-----|
| | | 1/3 | 1/2 | 2/3 | 1 | 1 $\frac{1}{3}$ | 1 $\frac{2}{3}$ | 2 | 2 $\frac{1}{2}$ | 3 $\frac{1}{3}$ | 4 |
| A | 6.5 | --- | --- | --- | --- | 4200 | 2000 | 1200 | 740 | 450 | 350 |
| B | 4.0 | --- | --- | --- | 9900 | 3000 | 1500 | 990 | 620 | 390 | 310 |
| C | 2.5 | --- | --- | --- | 6000 | 2100 | 1100 | 760 | 510 | 340 | 270 |
| C | 10 | --- | --- | --- | --- | 3200 | 1600 | 1000 | 640 | 400 | 320 |
| D | 1.5 | --- | --- | --- | 3700 | 1400 | 850 | 610 | 420 | 290 | 240 |
| D | 6.5 | --- | --- | --- | 6400 | 2200 | 1100 | 790 | 520 | 340 | 280 |
| D | 10 | --- | --- | --- | 9200 | 2800 | 1500 | 950 | 600 | 380 | 300 |
| E | 1.0 | --- | --- | --- | 2300 | 1000 | 650 | 480 | 350 | 250 | 220 |
| E | 4.0 | --- | --- | --- | 3800 | 1500 | 870 | 620 | 420 | 290 | 240 |
| E | 6.5 | --- | --- | --- | 5300 | 1900 | 1000 | 720 | 480 | 350 | 260 |
| E | 10 | --- | --- | --- | 6900 | 2300 | 1200 | 830 | 540 | 350 | 280 |
| F | .65 | --- | --- | 5800 | 1500 | 750 | 500 | 380 | 290 | 220 | 190 |
| F | 2.5 | --- | --- | 2500 | 1100 | 670 | 500 | 360 | 260 | 220 | |
| F | 4.0 | --- | --- | 3200 | 1300 | 790 | 570 | 400 | 280 | 230 | |
| F | 6.5 | --- | --- | 4100 | 1600 | 930 | 640 | 440 | 300 | 250 | |
| F | 10 | --- | --- | 6200 | 2100 | 1100 | 780 | 510 | 340 | 270 | |
| G | .40 | --- | 8500 | 2800 | 920 | 530 | 380 | 300 | 240 | 190 | 170 |
| G | 1.5 | --- | 5800 | 1500 | 750 | 500 | 380 | 290 | 220 | 190 | |
| G | 2.5 | --- | 8800 | 1900 | 930 | 590 | 440 | 320 | 240 | 210 | |
| G | 4.0 | --- | --- | 2600 | 1100 | 690 | 510 | 360 | 260 | 220 | |
| G | 6.5 | --- | --- | 3500 | 1400 | 850 | 590 | 410 | 290 | 240 | |
| G | 10 | --- | --- | 4600 | 1700 | 980 | 680 | 460 | 310 | 250 | |
| H | .25 | --- | 3500 | 1400 | 600 | 370 | 290 | 240 | 200 | 170 | 150 |
| H | 1.0 | --- | 9000 | 2900 | 960 | 540 | 380 | 300 | 240 | 190 | 170 |
| H | 1.5 | --- | 4500 | 1200 | 670 | 460 | 350 | 270 | 210 | 180 | |
| H | 2.5 | --- | 6500 | 1600 | 800 | 530 | 400 | 300 | 230 | 200 | |
| H | 4.0 | --- | --- | 2200 | 1000 | 640 | 470 | 340 | 250 | 210 | |
| H | 6.5 | --- | --- | 2800 | 1200 | 740 | 530 | 380 | 270 | 230 | |
| H | 10 | --- | --- | 3800 | 1500 | 880 | 620 | 420 | 290 | 240 | |
| J | .15 | 5300 | 1400 | 710 | 370 | 260 | 220 | 190 | 160 | 140 | 140 |
| J | .65 | --- | 3500 | 1400 | 600 | 370 | 290 | 240 | 200 | 170 | 150 |
| J | 1.0 | --- | 6300 | 2200 | 800 | 470 | 350 | 280 | 220 | 180 | 160 |
| J | 1.5 | --- | 9500 | 3000 | 980 | 550 | 390 | 310 | 250 | 190 | 170 |
| J | 2.5 | --- | 5100 | 1400 | 710 | 480 | 370 | 280 | 220 | 190 | |
| J | 4.0 | --- | 7300 | 1700 | 840 | 540 | 410 | 310 | 230 | 200 | |
| J | 6.5 | --- | --- | 2200 | 1000 | 640 | 470 | 340 | 250 | 210 | |
| J | 10 | --- | --- | 3000 | 1200 | 750 | 540 | 390 | 270 | 230 | |

TABLE 4C (Con.)

| Code Letter | AQL | Shape Parameter β | | | | | | | | | |
|-------------|-------|-------------------------|------|------|------|-----------------|-----------------|-----|-----------------|-----------------|-----|
| | | 1/3 | 1/2 | 2/3 | 1 | 1 $\frac{1}{3}$ | 1 $\frac{2}{3}$ | 2 | 2 $\frac{1}{2}$ | 3 $\frac{1}{3}$ | 4 |
| K | 0.10 | 1400 | 580 | 370 | 240 | 190 | 170 | 150 | 140 | 130 | 120 |
| K | 0.40 | 5700 | 1500 | 740 | 380 | 270 | 220 | 190 | 170 | 150 | 140 |
| K | 0.65 | --- | 2600 | 1100 | 510 | 330 | 260 | 220 | 190 | 160 | 150 |
| K | 1.0 | --- | 3900 | 1500 | 640 | 390 | 300 | 250 | 200 | 170 | 160 |
| K | 1.5 | --- | 7600 | 2500 | 870 | 500 | 360 | 290 | 230 | 190 | 170 |
| K | 2.5 | --- | --- | 3900 | 1100 | 620 | 410 | 330 | 260 | 210 | 180 |
| K | 4.0 | --- | --- | 5800 | 1500 | 750 | 500 | 380 | 290 | 220 | 190 |
| K | 6.5 | --- | --- | 8800 | 1900 | 930 | 590 | 440 | 320 | 240 | 210 |
| K | 10 | --- | --- | --- | 2700 | 1100 | 710 | 520 | 370 | 270 | 220 |
| L | 0.065 | 340 | 220 | 180 | 150 | 130 | 120 | 120 | 110 | 110 | 110 |
| L | 0.25 | 1400 | 580 | 370 | 240 | 190 | 170 | 150 | 140 | 130 | 120 |
| L | 0.40 | 3400 | 1000 | 560 | 320 | 230 | 200 | 170 | 150 | 140 | 130 |
| L | 0.65 | 6100 | 1500 | 770 | 400 | 270 | 230 | 190 | 170 | 150 | 140 |
| L | 1.0 | --- | 2900 | 1200 | 540 | 350 | 270 | 230 | 190 | 160 | 150 |
| L | 1.5 | --- | 4600 | 1700 | 680 | 410 | 310 | 250 | 210 | 170 | 160 |
| L | 2.5 | --- | 7700 | 2600 | 880 | 500 | 370 | 290 | 230 | 190 | 170 |
| L | 4.0 | --- | --- | 3900 | 1100 | 620 | 410 | 330 | 260 | 210 | 180 |
| L | 6.5 | --- | --- | 6500 | 1600 | 800 | 530 | 400 | 300 | 230 | 200 |
| M | 0.040 | 85 | 89 | 92 | 94 | 95 | 96 | 96 | 97 | 98 | 98 |
| M | 0.15 | 340 | 220 | 180 | 150 | 130 | 120 | 120 | 110 | 110 | 110 |
| M | 0.25 | 810 | 400 | 280 | 200 | 160 | 150 | 140 | 130 | 120 | 110 |
| M | 0.40 | 1600 | 630 | 400 | 250 | 200 | 170 | 150 | 140 | 130 | 120 |
| M | 0.65 | 3700 | 1100 | 590 | 330 | 240 | 200 | 180 | 160 | 140 | 130 |
| M | 1.0 | 7700 | 1800 | 850 | 430 | 290 | 240 | 200 | 170 | 150 | 140 |
| M | 1.5 | --- | 3000 | 1200 | 550 | 350 | 280 | 230 | 190 | 160 | 150 |
| M | 2.5 | --- | 5200 | 1900 | 730 | 440 | 330 | 260 | 220 | 180 | 160 |
| M | 4.0 | --- | 9900 | 3100 | 1000 | 560 | 400 | 310 | 250 | 200 | 170 |
| N | 0.025 | 21 | 36 | 46 | 59 | 67 | 73 | 76 | 80 | 85 | 88 |
| N | 0.10 | 85 | 89 | 92 | 94 | 95 | 96 | 96 | 97 | 98 | 98 |
| N | 0.15 | 220 | 170 | 150 | 130 | 120 | 110 | 110 | 110 | 100 | 100 |
| N | 0.25 | 410 | 250 | 200 | 160 | 140 | 130 | 120 | 120 | 110 | 110 |
| N | 0.40 | 950 | 440 | 300 | 210 | 170 | 150 | 140 | 130 | 120 | 120 |
| N | 0.65 | 1800 | 680 | 410 | 260 | 200 | 180 | 160 | 140 | 130 | 120 |
| N | 1.0 | 4100 | 1200 | 620 | 340 | 250 | 210 | 180 | 160 | 140 | 130 |
| N | 1.5 | 8800 | 2000 | 930 | 450 | 300 | 240 | 210 | 180 | 150 | 140 |
| N | 2.5 | --- | 3900 | 1500 | 630 | 380 | 300 | 240 | 200 | 170 | 150 |

TABLE 4C (Con.)

| Code Letter | AQL | Shape Parameter β | | | | | | | | | |
|-------------|-------|-------------------------|------|-----|-----|-----------------|-----------------|-----|-----------------|-----------------|-----|
| | | 1/3 | 1/2 | 2/3 | 1 | 1 $\frac{1}{3}$ | 1 $\frac{2}{3}$ | 2 | 2 $\frac{1}{2}$ | 3 $\frac{1}{3}$ | 4 |
| P | 0.015 | 5.5 | 14 | 23 | 37 | 48 | 55 | 60 | 67 | 74 | 78 |
| P | 0.065 | 20 | 34 | 45 | 58 | 66 | 72 | 76 | 80 | 85 | 87 |
| P | 0.10 | 49 | 62 | 69 | 78 | 83 | 86 | 88 | 90 | 92 | 94 |
| P | 0.15 | 90 | 92 | 94 | 96 | 96 | 96 | 97 | 97 | 97 | 98 |
| P | 0.25 | 220 | 170 | 150 | 130 | 120 | 110 | 110 | 110 | 100 | 100 |
| P | 0.40 | 410 | 250 | 200 | 160 | 140 | 130 | 120 | 120 | 110 | 110 |
| P | 0.65 | 950 | 440 | 300 | 210 | 170 | 150 | 140 | 130 | 120 | 120 |
| P | 1.0 | 2000 | 740 | 440 | 270 | 210 | 180 | 160 | 140 | 130 | 120 |
| P | 1.5 | 5700 | 1500 | 740 | 380 | 270 | 220 | 190 | 170 | 150 | 140 |
| Q | 0.010 | 1.4 | 5.7 | 11 | 24 | 34 | 42 | 48 | 56 | 64 | 80 |
| Q | 0.040 | 5.5 | 14 | 23 | 37 | 48 | 55 | 60 | 67 | 74 | 78 |
| Q | 0.065 | 12 | 24 | 35 | 49 | 59 | 65 | 70 | 75 | 81 | 84 |
| Q | 0.10 | 23 | 38 | 48 | 61 | 69 | 74 | 77 | 82 | 86 | 88 |
| Q | 0.15 | 59 | 70 | 76 | 83 | 87 | 89 | 90 | 92 | 94 | 95 |
| Q | 0.25 | 130 | 120 | 110 | 110 | 110 | 100 | 100 | 100 | 100 | 100 |
| Q | 0.40 | 270 | 190 | 160 | 140 | 120 | 120 | 110 | 110 | 110 | 100 |
| Q | 0.65 | 600 | 320 | 240 | 180 | 150 | 140 | 130 | 120 | 120 | 110 |
| Q | 1.0 | 1400 | 580 | 370 | 240 | 190 | 170 | 150 | 140 | 130 | 120 |
| R | 0.025 | 1.4 | 5.7 | 11 | 24 | 34 | 42 | 48 | 56 | 64 | 80 |
| R | 0.040 | 3.2 | 10 | 17 | 31 | 42 | 50 | 55 | 63 | 70 | 75 |
| R | 0.065 | 6.0 | 15 | 24 | 38 | 49 | 56 | 61 | 68 | 75 | 79 |
| R | 0.10 | 15 | 28 | 38 | 52 | 61 | 68 | 72 | 77 | 82 | 85 |
| R | 0.15 | 28 | 43 | 52 | 65 | 72 | 78 | 80 | 84 | 88 | 90 |
| R | 0.25 | 60 | 71 | 77 | 84 | 88 | 89 | 90 | 93 | 95 | 96 |
| R | 0.40 | 130 | 120 | 110 | 110 | 110 | 100 | 100 | 100 | 100 | 100 |
| R | 0.65 | 340 | 220 | 180 | 150 | 130 | 120 | 110 | 110 | 110 | 110 |

* U.S. GOVERNMENT PRINTING OFFICE 1965 O-779-805