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# Solubilities of $O_2$ , NO, and $N_2O_3$ in Liquid $N_2O_4$

### MAY 1965

Prepared by E. T. CHANG, N. A. GOKCEN, and C. D. ROE'SON Aerodynamics and Propulsion Research Laboratory

Prepared for BALLISTIC SYSTEMS AND SPACE SYSTEMS DIVISIONS AIR FORCE SYSTEMS COMMAND LOS ANGELES AIR FORCE STATION

Los Angeles, California





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### SOLUBILITIES OF $O_2$ , NO, AND $N_2O_3$ IN LIQUID $N_2O_4$

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Contract No. AF 04(695)-469

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BALLISTIC SYSTEMS AND SPACE SYSTEMS DIVISION AIR FORCE SYSTEMS COMMAND LOS ANGELES AIR FORCE STATION Los Angeles, California SSD-TR-65-61

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Report No. TDR-469(5210-10)-6

SOLUBILITIES OF 02, NO, AND N203 IN LIQUID N204

Prepared

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This technical documentary report has been reviewed and is approved for publication and dissemination. The conclusions and findings contained herein do no necessarily represent an official Air Force Position.

> For Space Systems Division Air Force Systems Command

ptain, USAF

### ABSTRACT

The solubilities of  $O_2$ , NO, and  $N_2O_3$  in liquid  $N_2O_4$  have been measured over a wide pressure range at -11.03, 0.0, and 25°C. The results show, conclusively, that Henry's law is obeyed for all pressures at each temperature for  $O_2$  and at low pressures for NO and  $N_2O_3$ . The standard free energy, enthalpy, and entropy of solution for each gas have been computed.

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### I. INTRODUCTION

The solubilities of a number of gases in propellants and oxidizers have been measured during the past two years (Refs. 1, 2). This report, a continuation of the foregoing effort, presents the experimental results and their interpretation for  $O_2$ , NO, and  $N_2O_3$  in liquid  $N_2O_4$  at various pressures and at -11.03, 0.0, and 25.0°C.

A literature search revealed that there were no data on the solubility of  $0_2$  in liquid  $N_20_4$ . Numerous investigations on systems containing NO,  $N_20_4$ ,  $N0_2$ , and  $N_20_3$  were reported, but the results were inconclusive and gave no direct solubility data for NO in liquid  $N_20_4$ . A systematic and reliable investigation of  $0_2$ , NO, and  $N_20_3$  in liquid  $N_20_4$  was therefore warranted. Previous page was blank, therefore not filmed.

### **II. EXPERIMENTAL PROCEDURE**

The apparatus and procedure for the solubility measurements are described in Ref. 2. In this work research grade  $N_2O_4$  of 99.5 percent minimum purity was further purified as follows: Oxygen was bubbled through  $N_2O_4$  to oxidize NO and NOC1. Then, liquid  $N_2O_4$  was repeatedly degassed, frozen with liquid  $N_2$ , evacuated, and melted, and this procedure was repeat. Until  $N_2O_4$  froze to a white solid. The solid was then melted and distilled under a vacuum into a sample container. Samples of approximately 100 g of liquid  $N_2O_4$  were used for the solubility measurements on  $O_2$  and samples of approximately 5 g for the measurements on NO. The gaseous  $O_2$  for the solubility measurements was of 99.99 percent minimum purity. The research grade NO gas had the following analysis in weight percent:  $0.68 N_2$ ,  $0.33 N_2O$ ,  $0.22 NO_2$ , and 98.74 NO. The gas was passed through a tube containing ascarite to remove  $NO_2$  before being used in the experiments.

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### III. RESULTS AND DISCUSSION

It is shown in the earlier reports (Refs. 1, 2) that the gases dissolved in liquids of interest obeyed Henry's law, i.e., the solubility is proportional to the partial pressure of dissolved gas. Thus, the process of dissolving a nonreacting gas in  $N_2O_4$  can be considered as the simple reaction

with its equilibrium constant K defined by

$$K = \frac{\text{mol fraction of dissolved gas}}{\text{partial pressure of gas}} = \frac{X}{P}$$
(2)

The data presented in this report show that Eq. (2) is valid for  $O_2$  at all pressures and for NO and  $N_2O_3$  at low pressures. When NO is admitted in the apparatus for the measurements of solubility, it reacts with gaseous  $NO_2$  (or  $N_2O_4$ ) to form  $N_2O_3$ , and large solubilities of NO and  $N_2O_3$  in liquid  $N_2O_4$  affect the concentrations of gaseous  $NO_2$  and  $N_2O_4$ . It is therefore necessary to account for the simultaneous reactions  $NO(g) + NO_2(g) = N_2O_3(g)$  and  $N_2O_4(g) = 2NO_2(g)$  in computing the partial pressures of each gas over the liquid and finding the composition of the solution.

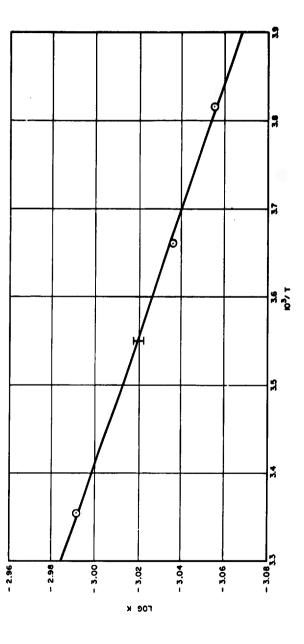
### A. OXYGEN

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The solubility values for  $O_2$  are listed in Table 1 and are represented in Fig. 1. Aside from a small degree of scattering, which is less than  $\pm 0.05 \times 10^{-4}$  in K (shown by  $\frac{1}{2}$  in Fig. 1), the temperature dependence of the equilibrium constant for solubility is linear. The equation representing this relationship is

		. 2	- 24	
Run No.	т, <sup>0</sup> к	P, atm	X(mol fr)x 10 <sup>3</sup>	$\begin{array}{l} \mathbf{K} = \mathbf{X}/\mathbf{P} \\ \mathbf{x} \ 10^3 \end{array}$
0 - 1	298.15	0.3728	0.376	1.01
0-2	298.15	0.4989	0.516	1.03
0-3	298.15	0.5745	0.597	1.04
0 - 4	298.15	0.9963	1.008	1.01
0 - 5	298.15	1.0809	1.070	<u>0.99</u>
			Avera	ge 1.02
0-6	273.15	0.2643	0.243	0.92
0 - 7	273.15	0.6275	0.578	0.92
0 - 8	273.15	1.1241	1.030	0.92
0-9	273.15	1.7950	1.637	<u>0.91</u>
			Avera	ge 0.92
0 - 10	262.02	0.6041	0.534	0.88
0 - 11	262.02	1.2017	1.058	0.88
0 - 12	262.02	1.3091	1.147	0.88
0 - 13	262.02	1.6119	1.423	0.88
0 - 14	262.02	1.9876	1.740	<u>0.88</u>
			Avera	uge 0.88

Table 1. Solubility of  $O_2$  in Liquid  $N_2O_4$ 





$$\log K = -\frac{139}{T} - 2.526$$

The corresponding change in the standard free energy MG° is

$$\Delta g^{o} = 636 + 11.56 \, \mathrm{T} \tag{4}$$

(3)

where  $\Delta H^{\circ} = 636$  cal/mole and  $\Delta S^{\circ} = -11.56$  cal/mole  $^{\circ}K$ .

A possible reaction of oxygen with  $N_2O_4$  is

$$O_2(g) + 2N_2O_4(1) \implies 2N_2O_5 \text{ (in liquid } N_2O_4)$$
 (5)

For this reaction the equilibrium constant is  $(2X)^2/p_0^2$ , where 2X is the mol fraction of N<sub>2</sub>O<sub>5</sub>. The dissolution process for O<sub>2</sub><sup>2</sup> in liquid N<sub>2</sub>O<sub>4</sub> is represented by (1) and not by (5) because  $X/p_{O_2}^2$  is a constant and not  $(2X)^2/p_{O_2}^2$  at various pressures for a given temperature.

### B. NITRIC OXIDE AND DINITROGEN TRIOXIDE

In order to determine the partial pressures of the various species over liquid  $N_2O_4$  from the measurement of total pressure it is necessary to consider the two side reactions. Gaseous  $N_2O_4$  dissociates reversibly into two molecules of  $NO_2$  in the gas phase, i.e.,

$$N_{0}O_{\mu}(g) \rightleftharpoons 2NO_{0}(g) \tag{6}$$

In the liquid state  $N_2^{0}_{4}$  dissociates so little that it may safely be considered as entirely  $N_2^{0}_{4}$  (Ref. 3). In addition NO reacts with  $N_2^{0}$  to form  $N_2^{0}_{3}$  as follows:

$$NO(g) + NO_{p}(g) \rightleftharpoons N_{2}O_{3}(g)$$
 (7)

-8-

At equilibrium in this system, the molecular species NO, NO<sub>2</sub>, N<sub>2</sub>O<sub>4</sub>, and N<sub>2</sub>O<sub>3</sub> are present. The arount of each species present in the gas phase is determined by the following equilibrium constants for (6) and (7):

$$\kappa_{N_2^{O_4}} = \frac{F_{N_{O_2}}^2}{F_{N_2^{O_4}}}$$
(8)

$$K_{N_2O_3} = \frac{P_{NO}P_{NO_2}}{P_{N_2O_3}}$$
(9)

The evaluation of partial pressure of NO and mol fraction of NO dissolved is not straightforward. However, an analytical expression can be obtained in the following manner: Reaction (6) can be written as the difference of the reactions

$$N_2O_4(1) - 2NO_2(g)$$
 (10)

$$N_2 C_{l_4}(1) \stackrel{\text{def}}{=} N_2 O_{l_4}(g) \tag{11}$$

Their respective equilibrium constants are

$$K_{1} = \frac{P_{NO_{2}}^{2}}{X_{N_{2}O_{4}}}$$
(12)

$$K_{2} = \frac{P_{N_{2}O_{4}}}{X_{N_{2}O_{4}}}$$
(13)

where  $X_{N_2O_4}$  is the mole fraction of  $N_2O_4$  in the liquid phase.

The experimentally measured total pressure over the liquid phase of this system is the sum of the partial pressures:

$$P_{\text{total}} = P_{N_2O_4} + P_{NO_2} + P_{NO} + P_{N_2O_3}$$
(14)

From (12), (13), (9), and (14) the partial pressures are, respectively,

$$P_{NO_2} = \left( K_1 X_{N_2 O_4} \right)^{1/2}$$
(15)

$$P_{N_2O_4} = K_2 X_{N_2O_4}$$
(16)

$$P_{N_2O_3} = \frac{P_{NO}P_{NO_2}}{K_{N_2O_3}} = \frac{P_{NO}x(K_1X_{N_2O_4})^{1/2}}{K_{N_2O_3}}$$
(17)

$$P_{NO} = \frac{P_{total} - K_2 X_{N_2O_{l_4}} - (K_1 X_{N_2O_{l_4}})^{1/2}}{1 + \left[ (K_1 X_{N_2O_{l_4}})^{1/2} / K_{N_2O_{l_3}} \right]}$$
(18)

The equilibrium constants can be calculated from thermodynamic data in the JANAF Tables (Ref. 4). The calculated values used are listed in Table 2.

T, <sup>o</sup> C	ĸı	K <sub>2</sub>	к <sub>N2<sup>0</sup>3</sub>
25.0	0.1238	0.8454	2.358
0	$4.914 \times 10^{-3}$	0.2765	0.5437
-11.03	9.629 x 10 <sup>-4</sup>	0.1556	0.2604

Table 2. Values of Equilibrium Constants

Finally, by the method of successive approximation, the partial pressures and the mol fractions of the solute gas are evaluated. For the first approximation, the mol fraction of  $N_2O_4$ ,  $X_{N_2O_4}$ , is set to unity in Eqs. (15)-(18) to obtain the partial pressures of all four species. These values and the known volume above the liquid yield the mass of each constituent, the mol fraction  $X_{N_2O_4}$  of liquid  $N_2O_4$ . Substitution of  $X_{N_2O_4}$  in Eqs. (15)-(18) yields a second set of values for the partial pressures from which  $X_{N_2O_4}$  is recalculated. The procedure may be repeated to obtain the third approximation for  $X_{N_2O_4}$  which differs from the second approximation by less than 0.1 percent.

The solubility values for NO in liquid  $N_2O_4$  are listed in Table 3 and are represented in Figs. 2-4.

Figure 2 presents the solubility, as mol fraction  $X_{NO}$ , of NO in liquid  $N_2O_4$  vs the partial pressure of NO. It is assumed that only the species NO and  $N_2O_4$  are present in the liquid phase. The plot shows that only in the dilute solution region, i.e., when  $X_{NO} < 0.1$ , Henry's law is obeyed. The solubility of NO in liquid  $N_2O_4$  decreases as temperature increases. Log  $X_{NO}/P_{NO}$ = log K' is presented vs  $X_{N_2}^2$  in Fig. 3 to facilitate the extrapolation of the solubility constant K', to the limiting value of zero concentration of NO. The decrease in K' with increase in pressure is probably due to the deviation of the gases from the ideal gas laws. Figure 4 represents log K' vs 1/T with mol fraction  $X_{NO} = 0.2$ . The equation representing the linear plots of Fig. 4 and the curves in the linear portions of Fig. 3 is

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Run No.	т, <sup>с</sup> К	Ptotal' <sup>atma</sup>	X <sub>NO</sub>	X <sub>N2</sub> 04	$(x_{N_2O_4})^2$	PNO, atm	K	Log K'
I -ON	262.12	1402.0	- <del>η</del> τ <u>5</u> 0.0	0.9486	0.8998	0.0236	2.1780	1966.0
NO- 2	262.12	0.2597	0.1705	0.8295	0.6881	0.0924	1.8452	0.2660
NO- 3	262.12	0.3282	0.2799	0.7201	0.5185	0.1724	1.6235	0.2104
NO- 4	262.12	0.4343	0.3830	0.6170	0.3807	0.2870	1.3346	<b>₩</b> \$21.0
NO- 5	262.12	0.8120	0.5424	0.4576	0.2094	0.6661	0.8143	-0.0892
			0.625 <sup>8</sup>			1.000		
NO- 6	273.15	0.4097	0.0807	0.9193	0.8451	0.0786	1.0267	<b>4110.0</b>
No- 7	273.15	0.5488	0.2211	0.7789	0.6067	0.2438	0.9069	-0.0426
No- 8	213.15	0.7530	0.3513	0.6487	0.4208	0.4684	0.7500	-0.12H9
No- 9	213.15	1.0913	0.4653	0.5347	0.2859	0.8152	0.5708	-0.2435
			0.516 <sup>8</sup>			1.000		
OT-ON	298.15	1.2507	4620.0	0.9766	0.9537	0.0674	0.3472	-0.4597
TT-ON	298.15	1.6583	0.1551	0.8449	0.7139	0.5456	0.2842	-0.5464
SI-ON	298.15	2140.5	0.2541	0.7459	0.5564	0.9805	0.2592	-0.5864
NO-13	298.15	1.2721	0.0305	0.9695	0.9399	0.0926	0.3293	-0.1824
412-ON	298.15	1.5124	0.1097	0.8903	0.7926	0.3748	0.2927	-0.5340
NO-15	298.15	1.7799	0.1877	0.8123	0.6598	0.6840	0.2744	-0.5616
9 <b>T-</b> 0N	208.15	2.0346	0.2501	0.7499	0.5624	0.9704	0.2577	-0.5889
			0.257			1.000		
arne val	ue of X	The value of X at P = 1						

Table 3. Solubility of NO in Liquid  $M_2O_{f h}$ 

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The value of  $X_{NO}$  at  $P_{NO} = 1$ .

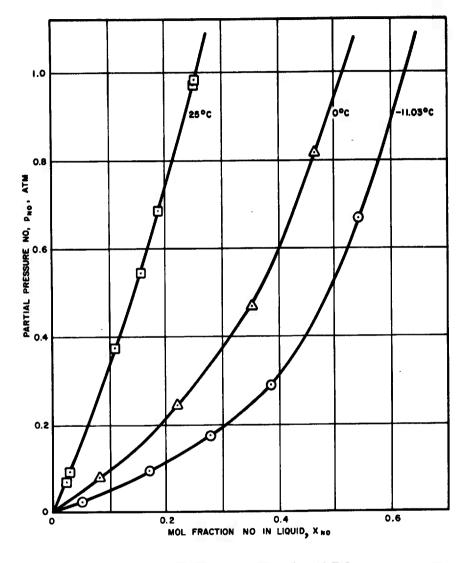
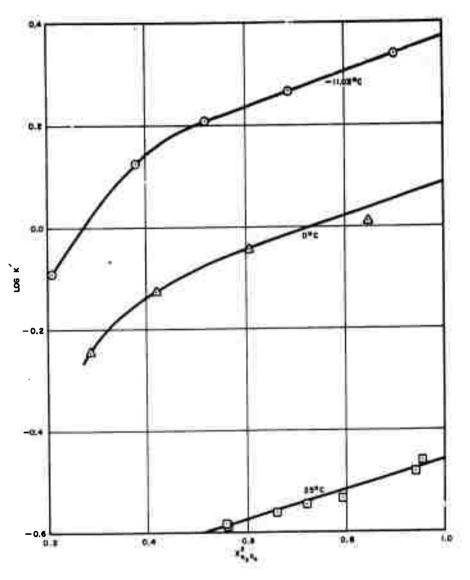


Fig. 2. Solubility of NO in Liquid N<sub>2</sub>0<sub>4</sub>

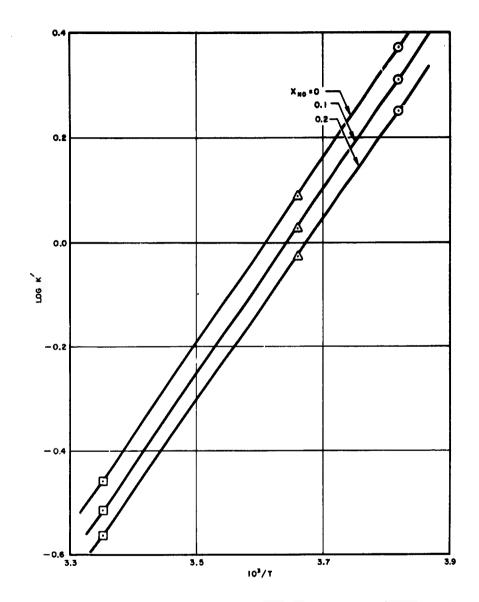


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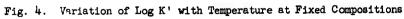
Fig. 3. Variation of Log K' with  $X_{N_2O_{l_1}}^2$  in Liquid



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Tana T	0.2011	0.2597	0.300	C.h3h3	0.6120	0.4097	0.5466	0.7530	1.0913	1.2507	1.872	1.512	1.6583	1.7799	2.0346	2.0412
7e	1.966	1.743	1.35	1.437	1-232	1.869	1.657	6113	1.32	1.973	1-950	1.26	1.747	J.691	1.600	1.60
<b>1</b> 203	0.013	0.039	0.053	0.062	0.066	0.00	0.051	0.065	0.071	0.00	0.01	0.0 <del>35</del>	0.045	0.44	0.062	0.062
<sup>₽</sup> #203	0.0027	0.0100	0.027	0.0269	0.0537	0.0097	0.0277	0.0487	0.0770	0.0099	0.036	0.0528	0.0748	0.0980	0.1254	0.1263
<b>1</b>	911.0	0.356	0.525	0.661	0.020	0.192	11.0	0.622	0.747	0.054	0.073	0.240	0.329	0.0	TTA-0	0.480
0	0.0236	0.0924	0.1724	0.2870	0.6661	0.0786	0.2436	0.460	0.8152	0.0674	0.0926	0.3748	0.5456	0.680	0.9704	0.9805
¥ <sup>®</sup>	BAL.O	601.0	0.000	0.056	0.05	0.164	0.113	0.075	0.047	0.278	0.272	0.220	0.195	0.178	0.150	04T.0
P. mo2	0.0302	0.0283	0.0263	0.0014	0.0210	0.0672	0.0619	0.0565	0.0513	0.347	0.3463	0.3320	0.3234	0.317	C.30k7	0. 303B
<b>≴</b> _0,	0.723	0.497	0.342	0.221	0.088	0.620	0.392	0.238	0.135	0.660	0.644	0.496	0.431	0.306	0.312	6.3.3
PII204	0.14TG	0.1290	12TT-0	0.0960	0.0TL2	0.2542	0.2154	0.1794	0.1478	0.8256	0.8196	0.7526	o. TJAA	0.6868	0.6341	0.6306
ĸ	1.974	1.907	1.837	1.763	1.628	1.958	1.876	1.787	1.697	1.988	1.965	1.942	1.916	1.896	1.857	1.854
X∎0	0.051	0.17	0.200	0.383	0.542	0.081	0.22	0.351	0.1465	0.023	0:030	011.0	0.155	0.188	0.250	0.25
х, <sub>2</sub> 0,	0.949	0.829	0.720	0.617	0.458	0.919	0.779	0.649	0.535	0.977	0.970	0.890	0.845	0.612	0.750	0.746
ц Ч	E0-11-					0.0				2 <del>5</del> .0						

Equilibrium Compositions of Liquid and Gas Phases for Mixtures of  $\mathbb{N}_2 \mathcal{O}_{l_1}$  and RO Table 4.

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$$\log K' = \log \frac{X_{NO}}{P_{NO}} = \frac{1682.6 + 87.4X_{N_2O_4}^2}{T} - 6.388$$
(19)

The corresponding change in the standard free energy for the limiting case when  $X_{N_2O_4} \longrightarrow 1$  is

$$\Delta G^{\circ} = -RT \ln K' = -8100 + 29.23 T$$
 (20)

where  $\Delta H^{\circ} = -8100 \text{ cal/mol}$ , and  $\Delta S^{\circ} = -29.23 \text{ cal/mol}^{\circ} K$ .

The values for the equilibrium composition of the liquid and gas phases and equilibrium partial pressures at -11.03, 0, and 25°C and at various total pressures are listed in Table 4. Figure 5 presents the equilibrium partial pressures of the molecular species NO,  $N_2O_3$ ,  $N_2O_4$ , and  $NO_2$  over the liquid. Since there are no data on the liquid phase equilibria,  $NO(1) + NO_2(1) \rightleftharpoons N_2O_3(1)$  and  $NO(1) + 1/2 N_2O_4(1) \oiint N_2O_3(1)$ , the liquid phase compositions are computed on the basis that only NO and  $N_2O_4$  exist in the liquid. The compositions are also expressed as a function of  $y_1$  and  $y_g$ , the total oxygen to total nitrogen ratio in the formula  $NO_v$  of the liquid and of the gas phase, respectively.

The partial pressure of  $N_2O_3$  over the liquid  $N_2O_4$  containing dissolved species from the gas phase have been computed and listed in Table 4. A possible reaction for the dissolution process of gaseous  $N_2O_3$  in liquid  $N_2O_4$  may be assumed as follows:

$$N_2O_3(g) \rightleftharpoons NO(in liq. N_2O_4) + 1/2 N_2O_4(1)$$
 (21)

Then, the solubility constant  $K'' = X_{NO}/P_{N_2O_3}$  of gaseous  $N_2O_3$  in liquid  $N_2O_4$  may be represented by

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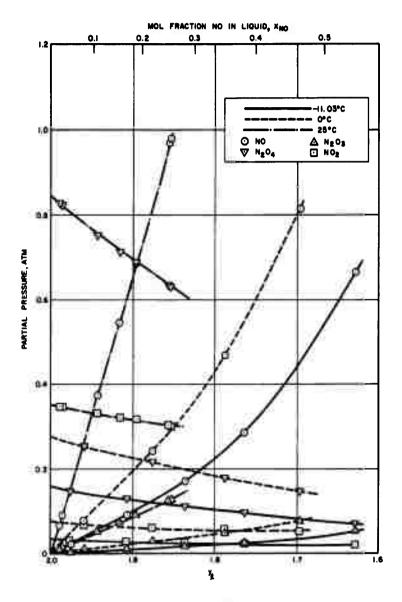


Fig. 5. Partial Pressures of NO,  $N_2O_3$ ,  $N_2O_4$ , and  $NO_2$  vs Atomic Ratio O/N =  $y_1$  in Liquid

$$\log K'' = \log \frac{X_{NO}}{P_{N_2O_3}} = \frac{199.2}{T} - 6.33$$
(22)

for the limiting case when  $X_{NO} \longrightarrow 0$ . This equation is also valid up to  $X_{NO} = 0.2$  within ±2 percent.

The corresponding change in the standard free energy for the limiting case is

$$\Delta G^{0} = -RT \ln K'' = -911.5 + 29.19T$$
(23)

where  $\Delta H^{\circ} = -911.5$  cal/mol, and  $\Delta S^{\circ} = -29.19$  cal/mol  $^{\circ}K$ .

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### IV. COMPARISON OF AVAILABLE DATA

During the past 30 years numerous investigators have studied various aspects of the  $N_2O_4$ -NO system. Verhoek and Daniels (Ref. 5) investigated the dissociation constants of  $N_2O_4$  and of  $N_2O_3$ . Giauque and Kemp (Ref. 6) measured the entropy of  $N_2O_4$  and  $NO_2$  and the equilibria in  $N_2O_4(g)$  $\implies 2NO_2(g) \implies 2NO(g) + O_2(g)$ . Whittaker, et al., (Ref. 7) investigated the vapor pressure and freezing points of the system,  $N_2O_4$ -NO in the composition range 0 to 16.85 percent by weight of NO and in the temperature range -40 to +15°C. Beattie, et al., (Refs. 8-11) made a series of investigations on  $N_2O_3$ . They studied the stability of  $N_2O_3$  in the gaseous phase and reported equilibrium constants for the reaction  $N_2O_3(g) \implies NO(g) + NO_2(g)$ at 5, 15, 25, 35 and 45°C (Ref. 8). They reported freezing-point data for the  $NO_2-N_2O_3$  system and pure  $N_2O_3$  (Ref. 9). They measured the vapor pressure of mixtures of  $NO_2$  and NO and expressed their results as

$$\log_{10} P$$
 (pressure in man) = 8.95 -  $\frac{f(X)}{T}$ 

where f(X) is a function dependent only on the composition of the mixture (Ref. 10). They also determined the composition of the vapor in equilibrium with liquid mixtures of NO<sub>2</sub> and NO (Ref. 11). They found that the vapor in equilibrium with a liquid containing equimolar amounts of NO<sub>2</sub> and NO is almost exclusively NO and that the composition of the vapor above liquid mixtures of NO and NO<sub>2</sub> is nearly independent of temperature for a particular liquid composition.

The results of this investigation are compared in Table 5 and in Fig. 6 with those of other investigations. Both Whittaker, et al., and Beattie, et al., reported their measurements as total pressure vs composition. Whittaker, et al., expressed their composition of liquid phase as the weight percent of NO, and Beattie, et al., as a function of the quantity  $y_1$  in the

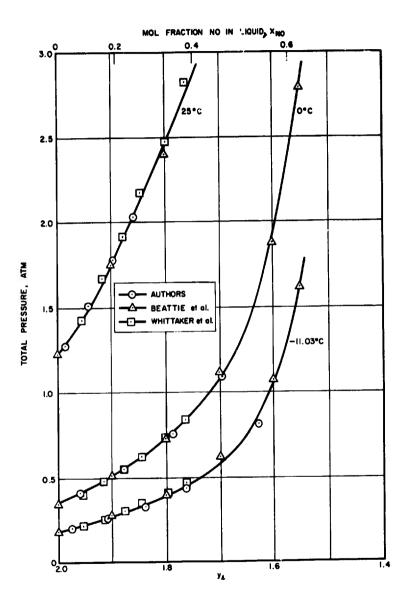
	Wt \$ NO			Total	Pressure, 1	m Hg at
Investigator	in liq.	XNO	у	-11.03°C	<b>5°</b> 0	25 °C
Whittaker,	2.89	0.087	1.954	163.3	306.3	1083
et al.	5.55	0.155	1.915	198.4	363.2	1268
	8.30	0.220	1.875	229.6	419.5	1458
	10.67	0.270	1.843	256.4	471.0	1655
	14.11	0.336	1.798	309.2	557.1	1861
	16.85	0.384	1.763	353.7	636.6	2146
Beattie,		0	2.000	140.5	264.5	932.8
et al.		0.180	1.900	210.5	389.9	1331
		0.333	1.800	301.8	550.8	1826
		0.464	1.700	472.3	846.6	2708
		0.575	1.600	814.3	1428.0	_
	-	0.623	1.550	1231.0	2122.0	
		0.646	1.525	1749.0	2973.0	l
Authors		0.051	1.974	155.1		
		0.171	1.907	197.3		
		0.280	1.837	249.3		
		0.383	1.763	330.0		
		0.542	1.628	617.0		
		0.081	1.958		311.4	
		0.221	1.876		417.1	
		0.351	1.787		572.3	
		0.465	1.697		829.4	
		0.023				950.5
		0.031	1.985			966.8
		0.110	1.942			1149
		0.155				1260
		0.188	1.896			1352
1		0.250	1.857			1546
		0.254				1551

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Table 5. Comparison of Available Data

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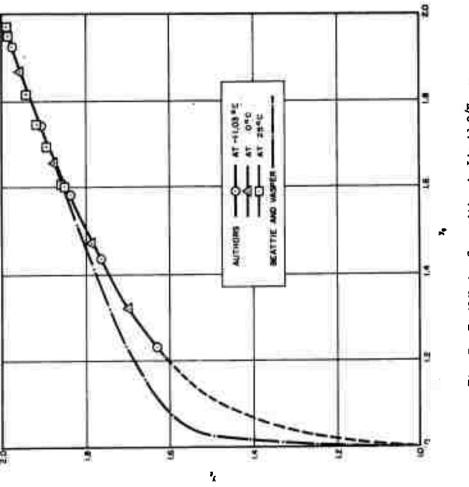


Fig. 7. Equilibrium Composition in Liquid  $0/N = y_1$ and in Gas  $0/N = y_g$  ſ

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formula NO<sub>y</sub> in the liquid phase. Therefore all the data were extrapolated to the same temperature and converted to the common units of total pressure vs  $y_1$  in Fig. 6. The scale for the mol fraction of NO,  $X_{NO}$ , in the liquid phase, i.e., assuming that in the liquid phase the only species present are NO and N<sub>2</sub>O<sub>4</sub>, is also shown in this figure. The agreement among the various investigations is good at 25, 0, and -ll.03°C and at pressures less than 2 atm.

Figure 7 is a comparison of the authors' data with those of Beattie et al., showing the equilibrium composition of the vapor  $y_g$  vs the composition of the liquid  $y_1$  for mixtures of NO and  $N_2O_4$ ;  $y_g$  and  $y_1$  are as indicated before, in terms of the formula NO<sub>y</sub> in the gas and liquid phases, respectively. The authors' data for Fig. 7 (Table 4) are in agreement with the extrapolated values of Beattie, et al., when the concentration of NO is low, i.e., y is close to 2 and poor at high NO concentrations. It appears from these results that the composition of the vapor is nearly independent of temperature for a given liquid composition, in agreement with the conclusion of Beattie, et al. The authors' results cover the range that have never been investigated, i.e., the range of  $y_1 = 1.6$  to 2.0 and  $y_g = 1.2$  to 2, whereas Beattie, et al., covered the range  $y_1 = 1.5$  to 1.8 and  $y_g = 1.0$  to 1.5.

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El Segundo, California	2 b. GROUP
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Security Classification

# UNCLASSIFIED Security Classification

14.

Oxygen Nitric Oxide Dinitrogen Trioxide Dinitrogen Tetroxide Triaminoguanidine Reactions

Abstract (Continued)

KEY WORDS

UNCLASSIFIED Security Classification (