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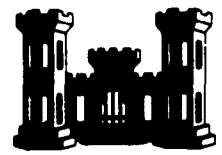
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GIMRADA Research Note No. 8  
FORMULAS FOR COMPUTING  
ATMOSPHERIC REFRACTION FOR OBJECTS  
INSIDE OR OUTSIDE THE ATMOSPHERE  
  
By Angel A. Baldini  
  
9 January 1963



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GEODESY, INTELLIGENCE AND MAPPING RESEARCH AND DEVELOPMENT AGENCY

Research Note No. 8

FORMULAS FOR COMPUTING ATMOSPHERIC REFRACTION  
FOR OBJECTS INSIDE OR OUTSIDE THE ATMOSPHERE

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9 January 1963

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## SUMMARY

This report presents the derivation of new equations for determining the changes in the direction of a ray of light as it passes through the atmosphere from an object to the observer. The equations are applicable to objects inside or outside the atmosphere.

Equations are also derived for obtaining the topocentric distance of the object as a function of the object's height and the observed zenith distance.

FORMULAS FOR COMPUTING ATMOSPHERIC REFRACTION  
FOR OBJECTS INSIDE OR OUTSIDE THE ATMOSPHERE

I. INTRODUCTION

Existing astronomic refraction equations cannot be satisfactorily applied to objects at distances up to a few thousands of miles from the earth because they were developed for a special use in which the object is at an infinite distance. In this paper, equations are derived that are applicable to objects both inside and outside the atmosphere.

II. INVESTIGATION

1. Fundamental Concepts. Refer to Fig. 1 and let

A = observing station

S = position of the object

h = height of the atmosphere over the station

C = earth's center

$\Delta$  = distance from the satellite to the station

$Z_0$  = observed zenith distance

AS = curve of the ray path

$S_1$  = any point on the curve AS

$\epsilon$  = astronomical refraction

AZ = vertical of the station through C

R = refraction to be determined

x,y = rectangular coordinate system



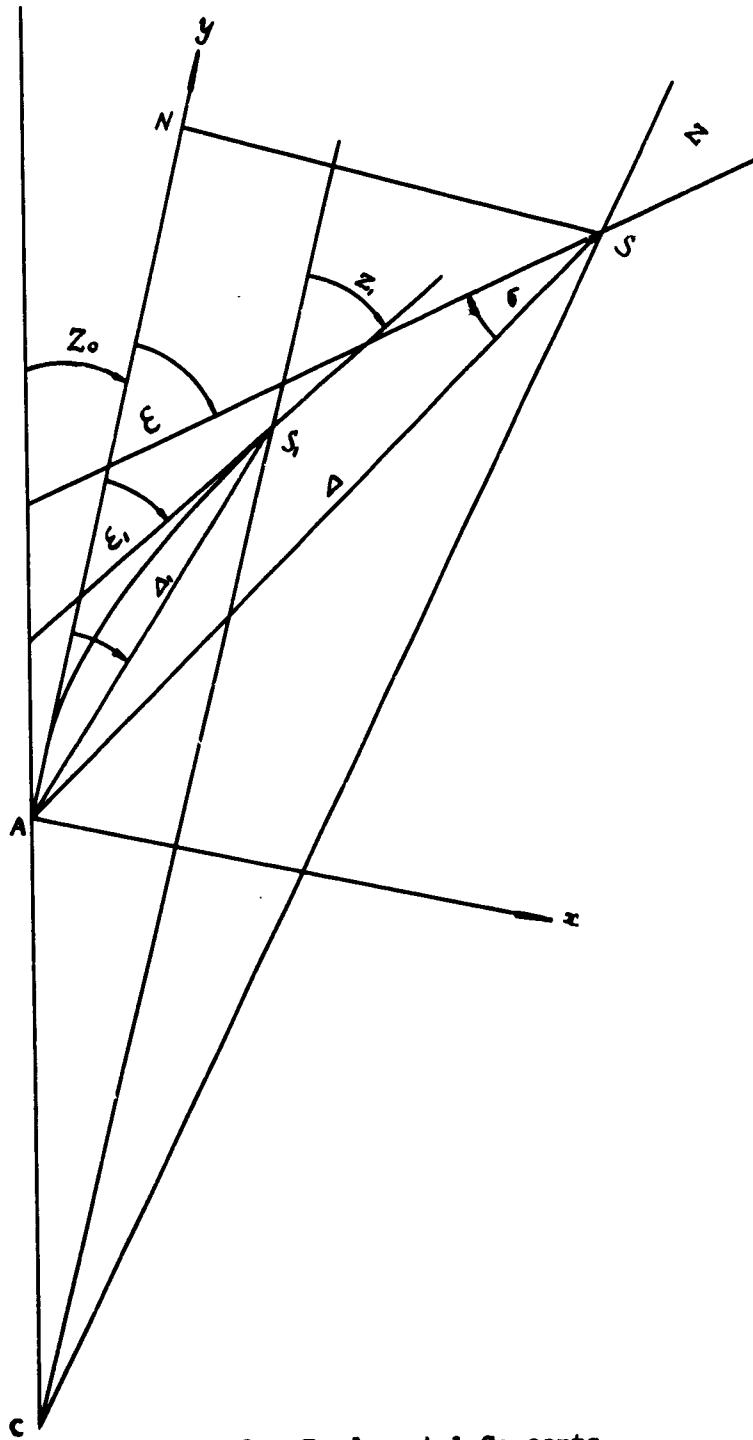


Fig. 1. Fundamental Concepts.

The observed zenith distance  $Z_o$  is the apparent zenith distance of the object when the ray reaches the observer. The true zenith distance is the angle  $Z_o + R$ , which the ray makes with the vertical of the observer's station before it enters the atmosphere.

The direction in which the observer sees the object is along the tangent to the curve at A. The origin of the x - y coordinate system is at A, the y-axis is oriented tangent to the ray path at A, and the x-axis is oriented  $90^\circ$  to the increasing zenith distances.

Let N be the point where the normal through S intersects the y-axis. The desired refraction is the angle NAS. It is obtained by equation

$$\sin R = \frac{SN}{\Delta} \quad (1)$$

We need to find SN, in order to obtain the refraction correction, R.

Because here we consider zenith distances less than  $75^\circ$ , R is always less than three minutes so it can be expressed as follows:

$$R = \frac{x}{\Delta \sin 1''}$$

in which

$$x = SN \quad (2)$$

We find x from

$$x = \int \epsilon \, dy \quad (3)$$

so that

$$R = \frac{1}{\Delta \sin 1''} \int \epsilon \, dy \quad (4)$$

in which  $\epsilon$  is the angle between the y-axis and the tangent at any point of the ray path.

Assume a spherical earth with the atmosphere arranged in spherical layers. If n indicates the index of refraction of one layer,  $n + dn$  is the refraction of the next layer.

If in the first layer we have a zenith distance Z, the next layer is  $Z + d\epsilon$ .

From the law of refraction we have

$$\frac{\sin (Z + d\epsilon)}{\sin Z} = \frac{n}{n + dn} \quad (5)$$

which we can transform as follows

$$1 + d\epsilon \cot Z = 1 - \frac{dn}{n}$$

so we obtain for  $d\epsilon$

$$d\epsilon = - \tan Z \frac{dn}{n} \quad (6)$$

Then

$$\epsilon = - \int \tan Z \frac{dn}{n} \quad (7)$$

Insert equation (7) into equation (4) and we obtain:

$$R = - \frac{1}{\sin 1''} \int \int \tan Z \frac{dn}{n} \cdot dy \quad (8)$$

To solve equation (8) we need an expression for  $\tan Z$  and another for  $\frac{dn}{n}$ .

To develop these we must first find expressions for the density of the atmosphere (on which refraction depends) as a function of the height.

2. Density of the Atmosphere As a Function of Height. The following symbols are used:

$\rho$ , the density of the atmosphere at any height

$\rho_0$ , the density at the earth's surface where the observer is located

$h$ , altitude above the observer's station

$n_0$ , index of refraction at the observer's station

$n$ , index of refraction at height  $h$ .

In order to determine the refraction it is necessary to have an expression for the density of the air as a function of the height.

We derive an empirical law of diminution of density from observations and take into consideration the fact that the power of reflecting light ceases at about 60 kilometers.\*

From the observed values of the density at different heights, we find that  $\rho$  decreases exponentially with altitude following the equation

$$\frac{\rho}{\rho_0} = e^{-\frac{h}{h_0}} \quad (9)$$

in which  $h_0$  is a constant.

The values of density  $\rho$  up to 20 kilometers follow equation (9) with accuracy. For heights over 20 km the equation is less accurate, but still sufficiently accurate because the refraction is small and the power of reflected light decreases rapidly at increasing heights (Fig. 2).

The constant  $h_0$ , was computed by weighting the observations proportionately to the power of reflected light at the height of observation. The value

$$h_0 = 9.240 \text{ km}$$

and

$$\frac{1}{h_0} = \frac{0.1082}{\text{km}} \quad (10)$$

Introduce this value into equation (9) and we obtain for the density  $\rho$

$$\rho = \rho_0 e^{-0.1082 h \text{ (km)}} \quad (11)$$

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\*The basic material for this development was obtained from The Handbook of Geophysics for Air Force Designers, Geophysics Research Directorate, Air Force Cambridge Research Center, Air Research and Development Command, Cambridge, Massachusetts 1957, and from available balloon observation data.

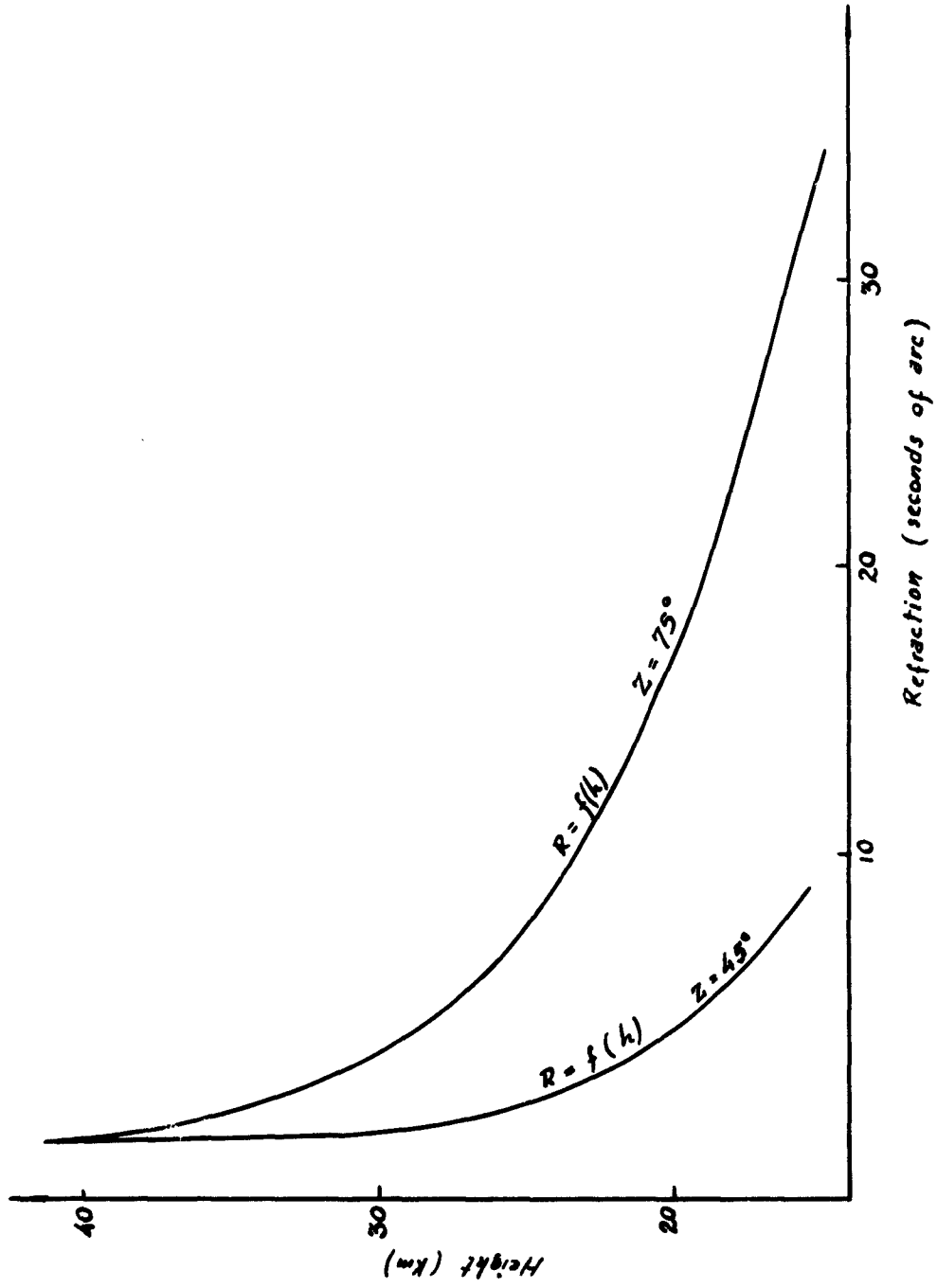


Fig. 2. Variation of refraction with height for  $Z = 75^\circ$  and  $Z = 45^\circ$ .

From Gladstone and Dale's law the values of the indexes of refraction, in terms of the atmospheric density, are given by equation

$$\frac{n - 1}{\rho} = c = \text{constant} \quad (12)$$

in which

$$c = 0.226$$

Use for  $\rho$  the value given by equation (11), and the index of refraction from equation (12) can be expressed as follows:

$$n = 1 + 0.226 \rho_0 e^{-0.1082 h} \quad (13)$$

in which the height  $h$  must be expressed in km.

From equation (13) we obtain

$$\frac{dn}{n} = - \frac{0.226 \rho_0 e^{-0.1082 h}}{1 + 0.226 \rho_0 e^{-0.1082 h}} 0.1082 dh \quad (14)$$

but from equation (12)

$$0.226 \rho_0 = n_0 - 1 \quad (15)$$

and because

$$0.1082 = \frac{1}{h_0}$$

We can rewrite equation (14) as follows:

$$\frac{dn}{n} = \frac{(n_0 - 1) e^{-\frac{h}{h_0}} dh}{h_0 [1 + (n_0 - 1) e^{-\frac{h}{h_0}}]} \quad (16)$$

3. Expression for  $\tan Z$ . To find an expression for  $\tan Z$  we must consider:

a. The maximum height of the stratus over which the reflecting power can be assumed zero.

b. The maximum zenith distance  $Z_0$ .

For (a) we find

$$h < 64 \text{ km} \quad (17)$$

and for (b) we adopt

$$Z_0 \leq 75^\circ \quad (18)$$

With these values for  $h$  and  $Z_0$ , the maximum value of  $Z$  should be:

$$Z = Z_0 - \xi \quad (19)$$

in which

$$\xi < 2.2$$

We can then express  $\tan Z$  as follows:

$$\tan Z = \tan Z_0 + \Delta \quad (20)$$

in which

$$\Delta = f(x) \quad (21)$$

Expand  $f(x)$  using the McLaurin's series. Then, we have

$$\Delta = f(0) + x f'(0) + \frac{x^2}{2} f''(0) + \frac{x^3}{6} f'''(0) + \dots (22)$$

Differentiating equation (20), we have

$$(1 + \tan^2 Z_0) \frac{dZ}{dx} = f'(x) \quad (23)$$

After the second differentiation

$$\frac{d^2 Z}{dx^2} (1 + \tan^2 Z) + 2 \left( \frac{dZ}{dx} \right)^2 \tan Z (1 + \tan^2 Z) = f''(x) \quad (24)$$

and from the third differentiation

$$\begin{aligned} \frac{d^3 Z}{dx^3} [1 + \tan^2 Z] + 6 \tan Z (1 + \tan^2 Z) \frac{d^2 Z}{dx^2} \frac{dZ}{dx} \\ + 2 \left( \frac{dZ}{dx} \right)^3 (1 + \tan^2 Z)^2 (1 + 3 \tan^2 Z) = f'''(x) \end{aligned} \quad (25)$$

To find the  $\frac{dZ}{dx}$ ,  $\frac{d^2 Z}{dx^2}$ ,  $\frac{d^3 Z}{dx^3}$ , we use Snell's law

$$nr \sin Z = n_0 r_0 \sin Z_0 = \text{constant}$$

Because we can express r as follows:

$$r = r_0 \left( 1 + \frac{h}{r_0} \right) \quad (26)$$

and for n

$$n = 1 + (n_0 - 1) e^{-\frac{h}{h_0}}$$

Snell's law can be rewritten in the form

$$\sin Z = \frac{n_0 \sin Z_0}{\left( 1 + \frac{h}{r_0} \right) \left[ (n_0 - 1) e^{-\frac{h}{h_0}} + 1 \right]} \quad (27)$$

Place

$$x = \frac{h}{n_0 r_0} + (n_0 - 1) \left[ \frac{e^{-\frac{h}{h_0}}}{n_0} \left( 1 + \frac{h}{r_0} \right) - 1 \right] \text{ and} \quad (28)$$

we obtain

$$\sin Z = \sin Z_0 (1 + x)^{-1} \quad (29)$$



It follows from equation (26) when  $h = 0$

$$r = r_0$$

$$n = n_0$$

then, from equation (28)

$$x = 0$$

and from equation (29)

$$Z = Z_0$$

from which  $f'(0) = 0$

From equation (29) we obtain for  $x = 0$

$$\left( \frac{dz}{dx} \right)_0 = -\tan Z_0 \quad (30)$$

$$\left( \frac{d^2z}{dx^2} \right)_0 = 2 \tan Z_0 + \tan^3 Z_0 \quad (31)$$

$$\left( \frac{d^3z}{dx^3} \right)_0 = -3 \tan Z_0 (1 + \tan^2 Z_0) (2 + \tan^2 Z_0) + 2 \tan^3 Z_0 \quad (32)$$

For  $x = 0$ , equations (23), (24), and (25) become

$$f'(0) = (1 + \tan^2 Z_0) \left( \frac{dz}{dx} \right)_0$$

$$f''(0) = \left( \frac{d^2z}{dx^2} \right)_0 (1 + \tan^2 Z_0) + 2 \left( \frac{dz}{dx} \right)_0^2 \tan Z_0 (1 + \tan^2 Z_0) \quad (33)$$

$$r'''(0) = [1 + \tan^2 z_0] \left[ \left( \frac{d^3 z}{dx^3} \right)_0 + 6 \tan z_0 \left( \frac{d^2 z}{dx^2} \right)_0 \left( \frac{dz}{dx} \right)_0 \right. \\ \left. + 2 \left( \frac{dz}{dx} \right)_0^3 (1 + 3 \tan^2 z_0) \right]$$

Insert the values of equations (30), (31), and (32) in the groups of equations (33) and we obtain finally

$$r'(0) = -\tan z_0 (1 + \tan^2 z_0)$$

$$r''(0) = (2 \tan z_0 + 3 \tan^2 z_0) (1 + \tan^2 z_0) \quad (34)$$

$$r'''(0) = -3 \tan z_0 (1 + \tan^2 z_0) [2 + \tan^2 z_0 (7 + 5 \tan^2 z_0)]$$

Now, introduce the values of equation (34) into equation (22) and equation (20) becomes

$$\tan z = \tan z_0 - x \tan z_0 (1 + \tan^2 z_0) + \frac{x^2}{2} \tan z_0 (1 + \tan^2 z_0) (2 + 3 \tan^2 z_0) \\ - \frac{x^3}{2} \tan z_0 (1 + \tan^2 z_0) [2 + \tan^2 z_0 (7 + 5 \tan^2 z_0)] + \dots \quad (35)$$

If we introduce

$$A = \tan z_0 (1 + \tan^2 z_0)$$

$$B = \frac{1}{2} A (2 + 3 \tan^2 z_0) \quad (36)$$

$$C = A \left[ 1 + \frac{1}{2} \tan^2 z_0 (7 + 5 \tan^2 z_0) \right]$$

equation (35) can then be rewritten as follows:

$$\tan z = \tan z_0 - x A + x^2 B - x^3 C + \dots \quad (37)$$

This equation (37) and the equation (16) which can also be written in the form

$$\frac{dn}{n} = (n_0 - 1) e^{-\frac{h}{h_0}} \left[ 1 - (n_0 - 1) e^{-\frac{h}{h_0}} \right] \frac{dh}{h_0} \quad (38)$$

are the two expressions which must be inserted into equation #(8).

dy remains unknown but can be obtained from

$$dy = \frac{dh}{\cos Z}$$

Its value is found later. Let us first solve equation (7)

4. Solution for  $\int \tan Z \frac{dn}{n}$ . Introduce into equation (7) the values given by equations (37) and (38), and we have

$$\begin{aligned} \epsilon = & - \tan Z_0 \int \frac{dn}{n} - (n_0 - 1) A \int x e^{-\frac{h}{h_0}} \left[ 1 - (n_0 - 1) e^{-\frac{h}{h_0}} \right] \frac{dh}{h_0} \\ & + (n_0 - 1) B \int x^2 e^{-\frac{h}{h_0}} \left[ 1 - (n_0 - 1) e^{-\frac{h}{h_0}} \right] \frac{dh}{h_0} \\ & - (n_0 - 1) C \int x^3 e^{-\frac{h}{h_0}} \left[ 1 - (n_0 - 1) e^{-\frac{h}{h_0}} \right] \frac{dh}{h_0} \end{aligned} \quad (39)$$

The solution of the first integral is

$$- \int_{n_0}^n \frac{dn}{n} = \left[ \frac{1}{2n^2} \right]_{n_0}^n = \frac{n_0^2 - n^2}{2n_0^2 n^2} \quad (40)$$

The indexes of refraction differ from unity by a small quantity

$$n < 1.0003$$

Indicate the small quantity .0003, by  $\gamma$  and we have

$$n = 1 + \gamma \quad (41)$$

in which  $\gamma$  has the values given by equation (26)

$$\gamma = (n_0 - 1) e^{-\frac{h}{h_0}} \quad (42)$$

so we can rewrite equation (40) as follows:

$$\frac{n_0^2 - n^2}{2 n_0^2 n^2} = [\gamma_0 - \gamma] \left[ 1 + \frac{\gamma_0 + \gamma}{2} \right] [1 - 2(\gamma_0 + \gamma)]$$

Neglect terms of the second power and we have

$$\frac{n_0^2 - n^2}{2 n_0^2 n^2} = (\gamma_0 - \gamma) \left[ 1 - \frac{3}{2} (\gamma_0 + \gamma) \right] \quad (43)$$

$\gamma_0$  is the value for  $h = 0$ . From equation (41)

$$\gamma_0 = n_0 - 1 \quad (44)$$

Introduce the values of  $\gamma$  given by equations (44) and (42), and equation (43) becomes

$$\frac{n_0^2 - n^2}{2 n_0^2 n^2} = (n_0 - 1) (1 - e^{-\frac{h}{h_0}}) \left[ 1 - \frac{3}{2} (n_0 - 1) (1 + e^{-\frac{h}{h_0}}) \right] \quad (45)$$

With this value the first integral of equation (39) is

$$-\ln Z \int \frac{dn}{n} = (n_0 - 1) \ln Z_0 (1 - e^{-\frac{h}{h_0}}) \left[ 1 - \frac{3}{2} (n_0 - 1) (1 + e^{-\frac{h}{h_0}}) \right] \quad (46)$$

Solve the second integral

$$II = \int x e^{-\frac{h}{h_0}} \left[ 1 - (n_0 - 1) e^{-\frac{h}{h_0}} \right] \frac{dh}{h_0} \quad (47)$$

in which  $x$  is determined by equation (28)

$$x = - (n_0 - 1) + \frac{(n_0 - 1)}{n_0} e^{-\frac{h}{h_0}} + \frac{h}{n_0 r_0} + (n_0 - 1) \frac{h}{n_0 r_0} e^{-\frac{h}{h_0}}$$

Introduce the value of  $x$  into this integral (47) and we have

$$\begin{aligned} \text{II} = & - (n_0 - 1) \int e^{-\frac{h}{h_0}} \left[ 1 - (n_0 - 1) e^{-\frac{h}{h_0}} \right] \frac{dh}{h_0} \\ & + \frac{(n_0 - 1)}{n_0} \int e^{-2\frac{h}{h_0}} \left[ 1 - (n_0 - 1) e^{-\frac{h}{h_0}} \right] \frac{dh}{h_0} \\ & + \frac{1}{n_0 r_0} \int h e^{-\frac{h}{h_0}} \left[ 1 - (n_0 - 1) e^{-\frac{h}{h_0}} \right] \frac{dh}{h_0} \\ & + \frac{n_0 - 1}{n_0 r_0} \int h e^{-\frac{h}{h_0}} \left[ 1 - (n_0 - 1) e^{-\frac{h}{h_0}} \right] \frac{dh}{h_0} \end{aligned} \quad (48)$$

After rearrangement and because  $(n_0 - 1)$  is less than 0.0003,

$$\frac{1}{n_0} + (n_0 + 1) = \frac{1}{(n_0 - 1) + 1} + (n_0 - 1) = 1$$

and

$$\frac{1}{n_0} = 1 - (n_0 - 1)$$

we obtain

$$\text{II} = - \frac{(n_0 - 1)}{h_0} \int_0^h e^{-\frac{h}{h_0}} dh + \frac{(n_0 - 1)}{h_0} \int_0^h e^{-2\frac{h}{h_0}} dh$$

$$\begin{aligned}
& + \frac{1}{n_o r_o h_o} \int_0^h h e^{-\frac{h}{h_o}} dh - \frac{(n_o - 1)^2}{n_o h_o} \int_0^h e^{-3 \frac{h}{h_o}} dh \\
& - \frac{(n_o - 1)^2}{n_o h_o} \int_0^h h e^{-3 \frac{h}{h_o}} dh
\end{aligned}$$

Integrate to obtain

$$\begin{aligned}
\text{II} = & - (n_o - 1) \left[ 1 - e^{-\frac{h}{h_o}} \right] + \frac{(n_o - 1)}{2} \left( 1 - e^{-2 \frac{h}{h_o}} \right) \\
& + \frac{h_o}{n_o r_o} \left[ 1 - e^{-\frac{h}{h_o}} \left( \frac{h}{h_o} + 1 \right) \right] - \frac{(n_o - 1)^2}{3 n_o} \left[ 1 - e^{-3 \frac{h}{h_o}} \right] \quad (49) \\
& - \frac{(n_o - 1)^2 h_o}{9 n_o} \left[ 1 - e^{-3 \frac{h}{h_o}} \left( 1 + 3 \frac{h}{h_o} \right) \right]
\end{aligned}$$

which is the solution of the integral of equation (47)

Solve the third integral of equation (39)

$$\int x^2 e^{-\frac{h}{h_o}} \left[ 1 - (n_o - 1) e^{-\frac{h}{h_o}} \right] \frac{dh}{h_o} = \text{III} \quad (50)$$

From equation (36), for the maximum zenith distance  $Z = 75$ ,  $\tan Z = 3.7$ , so taking  $\tan Z = 4$ , we have from equation (36)

$$A = \tan Z_o (1 + \tan^2 Z_o) = 68$$

$$B = \frac{1}{2} A (2 + 3 \tan^2 Z_o) = 1630$$

but because

$$(n_o - 1) < 0.0003$$

all terms containing  $(n_0 - 1)^3$  can be neglected, and we have for the maximum value

$$B (n_0 - 1)^3 < 0.003$$

$$x^2 = -2 \frac{(n_0 - 1)h}{n_0 r_0} + \frac{h^2}{n_0^2 r_0^2} \quad (51)$$

Substitute equation (51) into (50) and we obtain

$$\begin{aligned} \text{III} = & - \frac{2(n_0 - 1)}{n_0 r_0 h_0} \int h e^{-\frac{h}{h_0}} dh + \frac{1}{n_0^2 r_0^2 h_0} \int h^2 e^{-\frac{h}{h_0}} dh \\ & - \frac{(n_0 - 1)}{n_0 r_0^2 h_0} \int h^2 e^{-2\frac{h}{h_0}} dh \end{aligned} \quad (52)$$

The solution of these integrals is

$$\int_0^h h e^{-\frac{h}{h_0}} dh = h_0^2 \left[ 1 - e^{-\frac{h}{h_0}} \left( \frac{h}{h_0} - 1 \right) \right] \quad (53)$$

$$\int_0^h h^2 e^{-\frac{h}{h_0}} dh = h_0^3 \left[ 2 - e^{-\frac{h}{h_0}} \left( \frac{h^2}{h_0^2} + 2 \frac{h}{h_0} + 2 \right) \right] \quad (54)$$

$$\int_0^h h^2 e^{-2\frac{h}{h_0}} dh = \frac{h_0^3}{4} \left[ 1 - e^{-2\frac{h}{h_0}} \left( 2 \frac{h^2}{h_0^2} + 2 \frac{h}{h_0} + 1 \right) \right] \quad (55)$$

Introduce equations (53), (54) and (55) into equation (52), and we have

$$\text{III} = - \frac{2(n_0 - 1) h_0}{n_0 r_0} \left[ 1 - e^{-\frac{h}{h_0}} \left( \frac{h}{h_0} + 1 \right) \right]$$

$$\begin{aligned}
& + \frac{1}{n_0^2} \frac{h_0^2}{r_0^2} \left[ 2 - e^{-\frac{h}{h_0}} \left( \frac{h^2}{h_0^2} + 2 \frac{h}{h_0} + 2 \right) \right] \\
& - \frac{(n_0 - 1) h_0^2}{4 n_0 r_0^2} \left[ 1 - e^{-\frac{2h}{h_0}} \left( 2 \frac{h^2}{h_0^2} + 2 \frac{h}{h_0} + 1 \right) \right]
\end{aligned} \tag{56}$$

The last term equation of (56) has no influence in the refraction correction. By introducing this term into equation (39) its influence is given by

$$dR_3 = \frac{B (n_0 - 1)^2}{4 n_0} \frac{h_0^2}{r_0^2} \left[ 1 - e^{-2 \frac{h}{h_0}} \left( 2 \frac{h^2}{h_0^2} + 2 \frac{h}{h_0} + 1 \right) \right] \tag{57}$$

The maximum value corresponds to a maximum value of  $h = h_0$ .

It follows that

$$\left[ 1 - e^{-\frac{2h}{h_0}} \left( 2 \frac{h^2}{h_0^2} + 2 \frac{h}{h_0} + 1 \right) \right]_{\max.} = 0.14$$

For  $\tan Z = 6$  ( $Z = 80^\circ 5'$ )

$$B = 4218$$

Retaining

$$\frac{h_0}{n_0 r_0} = 0.01$$

$$(n_0 - 1) < 0.0003$$

we obtain

$$dR_3 < 0''001$$



Similar computations for the second term give

$$\begin{aligned} \text{for } Z = 75^\circ & \quad dR_2 < 0''06 \\ \text{for } Z = 81^\circ5 & \quad dR_2 < 3''8 \end{aligned} \quad (58)$$

For the third integral we make

$$x^3 = \frac{h^3}{n_o^3 r_o^3} \quad (59)$$

$$IV = \int x^3 e^{-\frac{h}{h_o}} \left[ 1 - (n_o - 1) e^{-\frac{h}{h_o}} \right] \frac{dh}{h_o}$$

$$IV = \frac{1}{n_o^3 h_o r_o^3} \int h^3 e^{-\frac{h}{h_o}} dh \quad (60)$$

neglecting the second term. The solution is

$$IV = -\frac{h_o^3}{n_o r_o^3} e^{-\frac{h}{h_o}} + 3 \frac{h_o^3}{n_o r_o^3} \left[ 2 - e^{-\frac{h}{h_o}} \left( \frac{h^2}{h_o^2} + 2 \frac{h}{h_o} + 2 \right) \right] \quad (61)$$

Multiply equation (61) by  $-C(n_o - 1)$ , equation (49) by  $-A(n_o - 1)$ , the first two terms of equation (56) by  $B(n_o - 1)$ , and add to equation (46). Then, equation (39) can be written as follows:

$$\begin{aligned} \epsilon &= (n_o - 1) \tan Z_o \left( 1 - e^{-\frac{h}{h_o}} \right) \left[ 1 - \frac{3}{2} (n_o - 1) \left( 1 + e^{-\frac{h}{h_o}} \right) \right] \\ &+ (n_o - 1)^2 A \left[ 1 - e^{-\frac{h}{h_o}} \right] - \frac{(n_o - 1)^2}{2} A \left( 1 - e^{-2\frac{h}{h_o}} \right) \\ &- \frac{(n_o - 1) A h_o}{n_o r_o} \left[ 1 - e^{-\frac{h}{h_o}} \left( \frac{h}{h_o} + 1 \right) \right] + A \frac{(n_o - 1)^3}{3n_o} \left[ 1 - e^{-3\frac{h}{h_o}} \right] \end{aligned}$$

$$\begin{aligned}
& + \frac{h_0 (n_0 - 1)^3}{9 n_0} A \left[ 1 + \frac{1}{r_0} \right] \left[ 1 - e^{-3 \frac{h}{h_0}} \left( 1 + 3 \frac{h}{h_0} \right) \right] \\
& - \frac{2 (n_0 - 1)^2 h_0}{n_0 r_0} B \left[ 1 - e^{-\frac{h}{h_0}} \left( \frac{h}{h_0} + 1 \right) \right] \\
& + \frac{(n_0 - 1)}{n_0^2} B \frac{h_0^2}{r_0^2} \left[ 2 - e^{-\frac{h}{h_0}} \left( \frac{h^2}{h_0^2} + 2 \frac{h}{h_0} + 2 \right) \right] \\
& + \frac{(n_0 - 1) C h_0^3}{n_0 r_0^3} e^{-\frac{h}{h_0}} \\
& - \frac{3(n_0 - 1) C h_0^3}{n_0 r_0^3} \left[ 2 - e^{-\frac{h}{h_0}} \left( \frac{h^2}{h_0^2} + 2 \frac{h}{h_0} + 2 \right) \right]
\end{aligned} \tag{62}$$

Collect the constant terms in A, and we have

$$C_A = (n_0 - 1) \left[ \frac{n_0 - 1}{n_0} - \frac{n_0 - 1}{2} - \frac{h_0}{n_0 r_0} + \frac{h_0}{9} \frac{(n_0 - 1)^2}{n_0} \right] \tag{63}$$

Let  $C_B$  be the constant terms of B. We then find

$$C_B = 2(n_0 - 1) \left[ \frac{h_0^2}{n_0^2 r_0^2} - (n_0 - 1) \frac{h_0}{n_0 r_0} \right] \tag{64}$$

$$C_C = 6 \frac{(n_0 - 1)}{n_0} \frac{h_0^3}{r_0^3}$$

Let  $E_1$ , be the summation of terms in  $e^{-\frac{h}{h_0}}$ ;  $E_2$  of the  $e^{-\frac{2h}{h_0}}$ , and  $E_3$

be of the  $e^{-\frac{3h}{h_0}}$ . We then obtain

$$E_1 = - (n_0 - 1) \tan Z_0 + A \left[ (n_0 - 1) \frac{h_0}{n_0 r_0} - \frac{(n_0 - 1)^2}{n_0} \right] + \frac{6 C (n_0 - 1) h_0^3}{n_0 r_0^3} \quad (65)$$

$$+ 2 B \left[ (n_0 - 1)^2 \frac{h_0}{n_0 r_0} - \frac{(n_0 - 1) h_0^2}{n_0^2 r_0^2} \right]$$

$$E_2 = \frac{(n_0 - 1)^2}{2} A + \frac{3}{2} (n_0 - 1)^2 \tan Z_0 \quad (66)$$

$$E_3 = A \frac{h_0 (n_0 - 1)^3}{9 n_0} \left( 1 + \frac{1}{r_0} \right) \quad (67)$$

Let  $M_1$  be the sum of terms of  $\frac{h}{h_0} e^{-\frac{h}{h_0}}$  and  $M_3$  the sum of terms of  $\frac{h}{h_0} e^{-3\frac{h}{h_0}}$ . We then have

$$M_1 = (n_0 - 1) \frac{h_0}{n_0 r_0} A + 2 B \left[ (n_0 - 1)^2 \frac{h_0}{n_0 r_0} + \frac{(n_0 - 1) h_0^2}{n_0^2 r_0^2} \right] \quad (68)$$

$$M_3 = \frac{1}{9} A \frac{h_0 (n_0 - 1)^2}{n_0} \left( 1 + \frac{1}{r_0} \right) \quad (69)$$

and letting  $N$  be

$$N = \frac{3 (n_0 - 1) h^3}{n_0 r_0^3} C - \frac{(n_0 - 1) h_0^2 B}{n_0^2 r_0^2} \quad (70)$$

Substitute equations (63) to (70) in (62)

$$\begin{aligned} \epsilon &= (n_0 - 1) \tan Z_0 \left[ 1 - \frac{3}{2} (n_0 - 1) \right] A C_A + B C_B - C C_C \\ &+ E_1 e^{-\frac{h}{h_0}} + E_2 e^{-2\frac{h}{h_0}} - E_3 e^{-3\frac{h}{h_0}} \\ &+ M_1 \frac{h}{h_0} e^{-\frac{h}{h_0}} - M_3 \frac{h}{h_0} e^{-3\frac{h}{h_0}} \\ &+ N \frac{h^2}{h_0^2} e^{-\frac{h}{h_0}} \end{aligned} \quad (71)$$

This equation (71) gives  $\epsilon$  as a function of the height  $h$ , which we must introduce in equation (3) to find  $x$ . Then

$$\begin{aligned} x &= \left\{ (n_0 - 1) \tan Z_0 \left[ 1 - \frac{3}{2} (n_0 - 1) \right] + A.C_A + B.C_B - C.C_C \right\} \int_0^y dy \\ &+ E_1 \int_0^y e^{-\frac{h}{h_0}} dy + E_2 \int_0^y e^{-2\frac{h}{h_0}} dy - E_3 \int_0^y e^{-3\frac{h}{h_0}} dy \\ &+ M_1 \int_0^y \frac{h}{h_0} e^{-\frac{h}{h_0}} dy - M_3 \int_0^y \frac{h}{h_0} e^{-3\frac{h}{h_0}} dy \\ &+ N \int_0^y \frac{h^2}{h_0^2} e^{-\frac{h}{h_0}} dy \end{aligned} \quad (72)$$

The first integral is

$$\int_0^y dy = y$$

To solve the other integrals we need an expression for  $dy$ . We find

$$dy = \frac{dh}{\cos Z} \quad (73)$$

To find  $\frac{1}{\cos Z}$  we use equations (37) and (29).

$$\begin{aligned} \tan Z &= \tan Z_0 - x A + B x^2 - C x^3 \\ \sin Z &= \sin Z_0 (1 + x)^{-1} \end{aligned}$$

By division we obtain

$$\frac{1}{\cos Z} = \frac{1+x}{\cos Z_0} - \frac{x(1+x)A}{\sin Z_0} + \frac{(1+x)x^2 B}{\sin Z_0} \dots \quad (74)$$

Because in all the integrals the exponential  $e^{-m \frac{h}{h_0}}$  ( $m = 1, 2, 3$ ) decreases with increasing  $h$  we consider only terms containing  $x^2$  and neglect the other terms containing  $x^3$  and so on.

From equations (36) we obtain

$$\begin{aligned} \frac{A}{\sin Z_0} &= \frac{1 + \tan^2 Z_0}{\cos Z_0} \\ \frac{B}{\sin Z_0} &= \frac{1}{2} \frac{(1 + \tan^2 Z_0)}{\cos Z_0} (2 + 3 \tan^2 Z_0) \end{aligned} \quad (75)$$

By introducing (75) into (74) we have

$$\frac{1}{\cos Z} = \frac{1}{\cos Z_0} - x \frac{\tan^2 Z_0}{\cos Z_0} + \frac{3}{2} \frac{x^2}{\cos Z_0} \tan^2 Z_0 (1 + \tan^2 Z_0) + (76)$$

Multiply this equation (76) by dh, and equation (73) can be written as follows:

$$dy = \frac{dh}{\cos Z_0} - x \frac{\tan^2 Z_0}{\cos Z_0} dh + \frac{3}{2} x^2 \frac{\tan^2 Z_0 (1 + \tan^2 Z_0)}{\cos Z_0} dh \quad (77)$$

Because all the corrections are small ones and decrease with increasing height, it is sufficiently accurate to retain

$$x = \frac{h}{n_0 r_0} - (n_0 - 1)$$

$$x^2 = \frac{h^2}{n_0^2 r_0^2} \quad (78)$$

Substitute equation (78) into (77) and we have

$$\begin{aligned} dy = & \frac{dh}{\cos Z_0} + (n_0 - 1) \frac{\tan^2 Z_0}{\cos Z_0} dh - \frac{\tan^2 Z_0}{\cos Z_0} \cdot \frac{h}{n_0 r_0} dh \\ & + \frac{3}{2} \tan^2 Z_0 \frac{(1 + \tan^2 Z_0)}{\cos Z_0} \cdot \frac{h^2}{n_0^2 r_0^2} dh \end{aligned} \quad (79)$$

Introduce equation (79) into each integral of equation (72) and we have for the second one

$$\begin{aligned}
E_1 \int_0^y e^{-\frac{h}{h_0}} dy &= \frac{E_1}{\cos Z_0} \left[ 1 + (n_0 - 1) \tan^2 Z_0 \right] \int_0^h e^{-\frac{h}{h_0}} dh \\
&\quad - \frac{E_1 \tan^2 Z_0}{n_0 r_0 \cos Z_0} \int_0^h h e^{-\frac{h}{h_0}} dh \\
&\quad + \frac{3}{2} \frac{E_1 \tan^2 Z_0 (1 + \tan^2 Z_0)}{n_0^2 r_0^2 \cos Z_0} \int_0^h h^2 e^{-\frac{h}{h_0}} dh
\end{aligned} \tag{80}$$

Integrate and we have

$$\begin{aligned}
E_1 \int_0^y e^{-\frac{h}{h_0}} dy &= \frac{E_1 h_0}{\cos Z_0} \left[ 1 + (n_0 - 1) \tan^2 Z_0 \right] \left[ 1 - e^{-\frac{h}{h_0}} \right] \\
&\quad + \frac{E_1 \tan^2 Z_0 h_0^2}{n_0 r_0 \cos Z_0} \left[ e^{-\frac{h}{h_0}} \left( \frac{h}{h_0} + 1 \right) - 1 \right] \\
&\quad + \frac{3E_1 \tan^2 Z_0 (1 + \tan^2 Z_0)}{n_0^2 r_0^2 \cos Z_0} h_0^3 \left[ 1 - e^{-\frac{h}{h_0}} \left( \frac{h^2}{2h_0^2} + \frac{h}{h_0} + 1 \right) \right]
\end{aligned} \tag{81}$$

For the third integral we have

$$\begin{aligned}
E_2 \int_0^y e^{-\frac{2h}{h_0}} dy &= E_2 \frac{\left[ 1 + (n_0 - 1) \tan^2 Z_0 \right]}{\cos Z_0} \int_0^h e^{-\frac{2h}{h_0}} dh \\
&\quad - E_2 \frac{\tan^2 Z_0}{\cos Z_0} \frac{1}{n_0 r_0} \int_0^h e^{-2\frac{h}{h_0}} h dh \\
&\quad + \frac{3}{2} E_2 \tan^2 Z_0 \frac{(1 + \tan^2 Z_0)}{\cos Z_0} \frac{1}{n_0^2 r_0^2} \int_0^h h^2 e^{-2\frac{h}{h_0}} dh
\end{aligned} \tag{82}$$

the solution of which is

$$\begin{aligned}
E_2 \int_0^y e^{-2 \frac{h}{h_0}} dy &= E_2 \frac{[1 + (n_0 - 1) \tan^2 Z_0]}{\cos Z_0} \frac{h_0}{2} [-e^{-2 \frac{h}{h_0}} + 1] \\
&+ E_2 \frac{\tan^2 Z_0}{\cos Z_0} \frac{h_0^2}{4 r_0 n_0^2} [e^{-2 \frac{h}{h_0}} (2 \frac{h}{h_0} + 1) - 1] \\
&+ \frac{3}{8} E_2 \tan^2 Z_0 \frac{(1 + \tan^2 Z_0)}{\cos Z_0} \frac{h_0^3}{n_0 r_0^2} [1 - e^{-2 \frac{h}{h_0}} (2 \frac{h^2}{h_0^2} + 2 \frac{h}{h_0} + 1)]
\end{aligned} \tag{83}$$

Solve for the fourth integral and we have

$$\begin{aligned}
E_3 \int_0^y e^{-3 \frac{h}{h_0}} dy &= -\frac{E_3}{\cos Z_0} [1 + (n_0 - 1) \tan^2 Z_0] \int_0^h e^{-3 \frac{h}{h_0}} dh \\
&+ \frac{E_3 \tan^2 Z_0}{n_0 r_0 \cos Z_0} \int_0^h e^{-\frac{3h}{h_0}} \cdot h dh \\
&- \frac{3}{2} E_3 \tan^2 Z_0 \frac{(1 + \tan^2 Z_0)}{\cos Z_0} \frac{1}{n_0^2 r_0^2} \int_0^h e^{-3 \frac{h}{h_0}} h^2 dh
\end{aligned} \tag{84}$$

the solution of which is:

$$\begin{aligned}
-E_3 \int_0^y e^{-3 \frac{h}{h_0}} dy &= \frac{E_3 h_0}{3 \cos Z_0} [1 + (n_0 - 1) \tan^2 Z_0] [e^{-3 \frac{h}{h_0}} - 1] \\
&+ \frac{E_3 \tan^2 Z_0 h_0^2}{9 n_0 r_0 \cos Z_0} [1 - e^{-\frac{3h}{h_0}} (3 \frac{h}{h_0} + 1)] \\
&- \frac{3E_3 \tan^2 Z_0 (1 + \tan^2 Z_0)}{54 n_0 r_0^2 \cos Z_0} h_0^3 [2 - e^{-3 \frac{h}{h_0}} (9 \frac{h^2}{h_0^2} + 6 \frac{h}{h_0} + 2)]
\end{aligned} \tag{85}$$



For the fifth integral we have

$$\begin{aligned}
 M_1 \int_0^y \frac{h}{h_0} e^{-\frac{h}{h_0}} dy &= M_1 \frac{[1 + (n_0 - 1) \tan^2 Z_0]}{\cos Z_0} \int_0^h \frac{h}{h_0} e^{-\frac{h}{h_0}} dh \\
 &- \frac{M_1 \tan^2 Z_0}{n_0 r_0 \cos Z_0} \int_0^h \frac{h^2}{h_0} e^{-\frac{h}{h_0}} dh \\
 &+ \frac{3 M_1 \tan^2 Z_0 (1 + \tan^2 Z_0)}{2 n_0^2 r_0^2 \cos Z_0} \int_0^h \frac{h^3}{h_0} e^{-\frac{h}{h_0}} dh
 \end{aligned} \tag{86}$$

the solution of which is:

$$\begin{aligned}
 M_1 \int_0^y \frac{h}{h_0} e^{-\frac{h}{h_0}} dh &= \frac{M_1 \cdot h_0}{\cos Z_0} [1 + (n_0 - 1) \tan^2 Z_0] [1 - e^{-\frac{h}{h_0}} (\frac{h}{h_0} + 1)] \\
 &- \frac{M_1 \tan^2 Z_0}{n_0 r_0 \cos Z_0} h_0^2 [2 - e^{-\frac{h}{h_0}} (\frac{h^2}{h_0^2} + 2 \frac{h}{h_0} + 2)] \\
 &+ \frac{3 M_1 \tan^2 Z_0 (1 + \tan^2 Z_0)}{2 n_0^2 r_0^2 \cos Z_0} h_0^3 [6 - e^{-\frac{h}{h_0}} (\frac{h^3}{h_0^3} + 3 \frac{h^2}{h_0} + 6 \frac{h}{h_0} + 6)]
 \end{aligned} \tag{87}$$

For the sixth integral we have

$$- M_3 \int_0^y \frac{h}{h_0} e^{-3 \frac{h}{h_0}} dh = - \frac{M_3}{\cos Z_0} [1 + (n_0 - 1) \tan^2 Z_0] \int_0^h \frac{h}{h_0} e^{-3 \frac{h}{h_0}} dh$$

$$\frac{M_3 \tan^2 Z_0}{n_0 r_0 \cos Z_0} \int_0^h \frac{h^2}{h_0} e^{-3 \frac{h}{h_0}} dh \quad (88)$$

$$- \frac{3 M_3 \tan^2 Z_0 (1 + \tan^2 Z_0)}{2 n_0^2 r_0^2 \cos Z_0} \int_0^h \frac{h^3}{h_0} e^{-3 \frac{h}{h_0}} dh$$

the solution of which is:

$$\begin{aligned} -M_3 \int_0^y \frac{h}{h_0} e^{-\frac{3h}{h_0}} dy &= \frac{h_0 M_3}{9 \cos Z_0} \left[ 1 + (n_0 - 1) \tan^2 Z_0 \right] \left[ e^{-3 \frac{h}{h_0}} \left( 3 \frac{h}{h_0} + 1 \right) - 1 \right] \\ &+ \frac{M_3 \tan^2 Z_0 \cdot h_0^2}{27 n_0 r_0 \cos Z_0} \left[ 2 - e^{-3 \frac{h}{h_0}} \left( 9 \frac{h^2}{h_0^2} + 6 \frac{h}{h_0} + 2 \right) \right] \quad (89) \\ &+ \frac{3M_3 \tan^2 Z_0 (1 + \tan^2 Z_0)}{162 n_0^2 r_0^2 \cos Z_0} h_0^3 \left[ e^{-3 \frac{h}{h_0}} \left( 27 \frac{h^3}{h_0^3} + 27 \frac{h^2}{h_0^2} \right. \right. \\ &\left. \left. + 18 \frac{h}{h_0} + 6 \right) - 6 \right] \end{aligned}$$

and finally, for the last integral we have

$$\begin{aligned} N \int_0^y \frac{h^2}{h_0^2} e^{-\frac{h}{h_0}} dy &= \frac{N}{\cos Z_0} \left[ 1 + (n_0 - 1) \tan^2 Z_0 \right] \int_0^h \frac{h^2}{h_0^2} e^{-\frac{h}{h_0}} dh \\ &- \frac{N \tan^2 Z_0}{n_0 r_0 \cos Z_0} \int_0^h \frac{h^3}{h_0^3} e^{-\frac{h}{h_0}} dh \quad (90) \end{aligned}$$

$$+ \frac{3 N \tan^2 Z_0 (1 + \tan^2 Z_0)}{2 n_0^2 r_0^2 \cos Z_0} \int_0^h \frac{h^4}{h_0^2} e^{-\frac{h}{h_0}} dh$$

the solution of which is:

$$\begin{aligned} N \int_0^y \frac{h^2}{h_0^2} e^{-\frac{h}{h_0}} dy &= \frac{h_0 N}{\cos Z_0} [1 + (n_0 - 1) \tan^2 Z_0] \left[ 2 - e^{-\frac{h}{h_0}} \left( \frac{h^2}{h_0^2} + 2\frac{h}{h_0} + 2 \right) \right] \\ &+ \frac{N \tan^2 Z_0 h_0^2}{n_0 r_0 \cos Z_0} \left[ e^{-\frac{h}{h_0}} \left( \frac{h^3}{h_0^3} + 3 \frac{h^2}{h_0^2} + 6 \frac{h}{h_0} + 6 \right) - 6 \right] \quad (91) \\ &+ \frac{3N h_0^3 \tan^2 Z_0 (1 + \tan^2 Z_0)}{2 n_0^2 r_0^2 \cos Z_0} \left[ 24 - e^{-\frac{h}{h_0}} \left( \frac{h^4}{h_0^4} + 4 \frac{h^3}{h_0^3} \right. \right. \\ &\left. \left. + 12 \frac{h^2}{h_0^2} + 24 \frac{h}{h_0} + 24 \right) \right] \end{aligned}$$

Use the abbreviation

$$t = \tan Z_0$$

and add the equations (81), (83), (85), (87), (89), and (91). Then equation (72) becomes:

$$\begin{aligned} x = \int \epsilon dy &= \left\{ (n_0 - 1) t \left[ 1 - \frac{3}{2} (n_0 - 1) \right] + A.C_A + B.C_B + C.C_C \right\} y \\ &+ E_1 \frac{h_0}{\cos Z_0} [1 + (n_0 - 1) t^2] \left[ 1 - e^{-\frac{h}{h_0}} \right] + \frac{E_1 t^2 h_0^2}{n_0 r_0 \cos Z_0} \left[ e^{-\frac{h}{h_0}} \left( \frac{h}{h_0} + 1 \right) - 1 \right] \end{aligned}$$

$$\begin{aligned}
& + 3 \frac{E_1 t^2 (1+t^2) h_0^3}{n_0^2 r_0^2 \cos Z_0} \left[ 1 - e^{-\frac{h}{h_0}} \left( \frac{1}{2} \frac{h^2}{h_0^2} + \frac{h}{h_0} + 1 \right) \right] \\
& + \frac{1}{2} E_2 \frac{h_0 [1 + (n_0 - 1)t^2]}{\cos Z_0} (1 - e^{-2\frac{h}{h_0}}) + \frac{1}{4} E_2 \frac{t^2 h_0^2}{n_0 r_0 \cos Z_0} \left[ e^{-2\frac{h}{h_0}} (2\frac{h}{h_0} - 1) \right] \\
& + \frac{3}{8} E_2 \frac{t^2 (1+t^2) h_0^3}{\cos Z_0 n_0 r_0^2} \left[ 1 - e^{-2\frac{h}{h_0}} \left( 2\frac{h^2}{h_0^2} + 2\frac{h}{h_0} + 1 \right) \right] \\
& + \frac{1}{3} E_3 \frac{h_0}{\cos Z_0} [1 + (n_0 - 1)t^2] \left[ e^{-3\frac{h}{h_0}} - 1 \right] \\
& + \frac{1}{9} E_3 \frac{t^2 h_0^2}{n_0 r_0 \cos Z_0} \left[ 1 - e^{-\frac{3h}{h_0}} \left( 3\frac{h}{h_0} + 1 \right) \right] \\
& + \frac{1}{18} E_3 \frac{t^2 (1+t^2)}{\cos Z_0} \cdot \frac{h_0^3}{n_0 r_0^2} \left[ e^{-3\frac{h}{h_0}} \left( 9\frac{h^2}{h_0^2} + 6\frac{h}{h_0} + 2 \right) - 2 \right] \\
& + M_1 \frac{h_0}{\cos Z_0} [1 + (n_0 - 1)t^2] \left[ 1 - e^{-\frac{h}{h_0}} \left( \frac{h}{h_0} + 1 \right) \right] \quad (92) \\
& + \frac{M_1 t^2 h_0^2}{\cos Z_0 n_0 r_0} \left[ e^{-\frac{h}{h_0}} \left( \frac{h^2}{h_0^2} + 2\frac{h}{h_0} + 2 \right) - 2 \right] \\
& + \frac{3}{2} M_1 \frac{t^2 (1+t^2) h_0^3}{n_0^2 r_0^2 \cos Z_0} \left[ 6 - e^{-\frac{h}{h_0}} \left( \frac{h^3}{h_0^3} + 3\frac{h^2}{h_0^2} + 6\frac{h}{h_0} + 6 \right) \right]
\end{aligned}$$

$$\begin{aligned}
& + \frac{M_3}{9} \frac{h_0}{\cos Z_0} [1 + (n_0 - 1) t^2] [e^{-3 \frac{h}{h_0}} (3 \frac{h}{h_0} + 1) - 1] \\
& + \frac{M_3}{27 n_0 r_0} \frac{t^2 h_0^2}{\cos Z_0} [2 - e^{-3 \frac{h}{h_0}} (9 \frac{h^2}{h_0^2} + 6 \frac{h}{h_0} + 2)] \\
& + \frac{3}{162} M_3 \frac{t^2 (1 + t^2) h_0^3}{n_0^2 r_0^2 \cos Z_0} [e^{-3 \frac{h}{h_0}} (27 \frac{h^3}{h_0^3} + 27 \frac{h^2}{h_0^2} + 18 \frac{h}{h_0} + 6) - 6] \\
& + \frac{N}{\cos Z_0} h_0 [1 + (n_0 - 1) t^2] [2 - e^{-\frac{h}{h_0}} (\frac{h^2}{h_0^2} + 2 \frac{h}{h_0} + 2)] \\
& + \frac{N}{n_0 r_0} \frac{t^2 h_0^2}{\cos Z_0} [e^{-\frac{h}{h_0}} (\frac{h^3}{h_0^3} + 3 \frac{h^2}{h_0^2} + 6 \frac{h}{h_0} + 6) - 6] \\
& + \frac{3}{2} N \frac{h_0^3 t^2 (1 + t^2)}{n_0^2 r_0^2 \cos Z_0} [24 - e^{-\frac{h}{h_0}} (\frac{h^4}{h_0^4} + 4 \frac{h^3}{h_0^3} + 12 \frac{h^2}{h_0^2} + 24 \frac{h}{h_0} + 24)]
\end{aligned}$$

To obtain the refraction correction we divide the value of  $x$  by the distance  $\Delta$ , as was indicated in equation (4).

In order to consider the terms necessary for  $Z = 75^\circ$  we must compute the values of  $E_1$ ,  $E_2$ ,  $E_3$ ,  $M_1$ ,  $M_3$ , and  $N$ . We find for  $Z = 75^\circ$

$$E_1 = 213''$$

$$E_2 = 0.6$$

$$E_3 = 0$$

$$M_1 = 5.0$$

$$M_3 = 1.0$$

$$N = -0.05$$

The term in the right hand of equation (65) can be neglected because its maximum value reaches

$$6 C (n_0 - 1) \frac{h_0^3}{n_0 r_0^3} < 0.03$$

and each coefficient of  $E_1$  is less than unity.

Since we hold as maximum zenith distance  $Z_0 = 75^\circ$ ,  $R_{\max}$  does not reach more than 3 minutes which permits us to retain

$$\Delta = y$$

with an error less than 0.1 meter for the maximum value of  $\Delta$  (when the object is at the limit of the atmosphere).

Then, the final formula for computing the refraction for an object inside the atmosphere is as follows:

$$R = A_0 (n_0 - 1) \tan Z_0 + A_1 (n_0 - 1) \tan^3 Z_0 + A_2 (n_0 - 1) \tan^5 Z_0$$

$$+ \frac{E_1 h_0}{\Lambda \cos Z_0} \left[ (1 + (n_0 - 1) \tan^2 Z_0) \left( 1 - e^{-\frac{h}{h_0}} \right) \right]$$

$$+ \frac{E_1 h_0^2 \tan^2 Z_0}{n_0 r_0 \Lambda \cos Z_0} \left[ e^{-\frac{h}{h_0}} \left( \frac{h}{h_0} + 1 \right) - 1 \right]$$

$$\begin{aligned}
& + \frac{1}{2} \frac{h_0 E_2}{\Delta \cos Z_0} \left[ 1 - e^{-\frac{h}{h_0}} \right] \\
& + \frac{M_1 h_0}{\Delta \cos Z_0} \left[ 1 - e^{-\frac{h}{h_0}} \left( \frac{h}{h_0} + 1 \right) \right] \\
& + \frac{M_3 h_0}{9 \Delta \cos Z_0} \left[ e^{-3 \frac{h}{h_0}} \left( 3 \frac{h}{h_0} + 1 \right) - 1 \right] \\
& + N \frac{h_0}{\Delta \cos Z_0} \left[ 1 + (n_0 - 1) \tan^2 Z_0 \right] \left[ 2 - e^{-\frac{h}{h_0}} \left( \frac{h^2}{h_0^2} + 2 \frac{h}{h_0} + 2 \right) \right]
\end{aligned} \tag{93}$$

in which

$$A_0 = +0.99827$$

$$A_1 = -0.00130$$

$$A_2 = +0.000006$$

If we express  $\Delta$  in kilometers, and holding

$$h_0 = 9.24 \text{ km}$$

$$\frac{h_0^2}{n_0 r_0} = 0.0134 \text{ km}$$

$$\frac{1}{2} h_0 = 4.62 \text{ km}$$

$$\frac{1}{9} h_0 = 1.027 \text{ km}$$

The height of the station  $h_a$ , does not affect the results except for extreme heights. If this is so, we replace  $h$  and  $r_o$  as follows:

$$h = h_s - h_a$$

$$n_o r_o = 6372 + h_a$$

where

$$h_s = \text{height of the object}$$

$$h_a = \text{height of the station}$$

both  $h_s$  and  $h_a$  are expressed in kilometers.

Equation (93) can be rewritten as follows:

$$\begin{aligned}
 R = & A_0 (n_o - 1) \tan Z_o + A_1 (n_o - 1) \tan^3 Z_o + A_2 (n_o - 1) \tan^5 Z_o \\
 & + \frac{9.24 E_1}{\Delta \cos Z_o} \left[ 1 + (n_o - 1) \tan^2 Z_o \right] \left[ 1 - e^{-\frac{h}{h_o}} \right] \\
 & + 0.0134 \frac{E_1 \tan^2 Z_o}{\Delta \cos Z_o} \left[ e^{-\frac{h}{h_o}} \left( \frac{h}{h_o} + 1 \right) - 1 \right] \\
 & + \frac{4.620 E_2}{\Delta \cos Z_o} \left[ 1 - e^{-\frac{h}{h_o}} \right] \\
 & + \frac{9.240 M_1}{\Delta \cos Z_o} \left[ 1 + (n_o - 1) \tan^2 Z_o \right] \left[ 1 - e^{-\frac{h}{h_o}} \left( \frac{h}{h_o} + 1 \right) \right] \\
 & + \frac{1.026 M_3}{\Delta \cos Z_o} \left[ 1 + (n_o - 1) \tan^2 Z_o \right] \left[ e^{-3 \frac{h}{h_o}} \left( 3 \frac{h}{h_o} + 1 \right) - 1 \right]
 \end{aligned} \tag{94}$$



$$+ \frac{9.240 N}{\Delta \cos Z_0} \left[ 1 + (n_0 - 1) \tan^2 Z_0 \right] \left[ 2 - e^{-\frac{h}{h_0}} \left( \frac{h^2}{h_0^2} + 2 \frac{h}{h_0} + 2 \right) \right]$$

$$A_0 = +0.99827$$

$$A_1 = -0.00130$$

$$A_2 = +0.000006$$

5. Refraction Viewed from an Object Inside the Atmosphere.  
The refraction viewed from the object is the angle

$$\sigma = NSA$$

of Figure 1. We see that

$$\sigma = \epsilon - R \quad (95)$$

The angle  $\epsilon$  can be computed by using equation (71).

Then the refraction  $\sigma$  can be computed as follows:

$$\begin{aligned} \sigma = & E_1 e^{-\frac{h}{h_0}} - \frac{9.240 E_1}{\Delta \cos Z_0} \left[ 1 + (n_0 - 1) \tan^2 Z_0 \right] \left[ 1 - e^{-\frac{h}{h_0}} \right] \\ & + 0.0134 \frac{E_1 \tan^2 Z_0}{\Delta \cos Z_0} \left[ 1 - e^{-\frac{h}{h_0}} \left( \frac{h}{h_0} + 1 \right) \right] \\ & + E_2 e^{-2 \frac{h}{h_0}} - \frac{4.620}{\Delta \cos Z_0} E_2 \left[ 1 - e^{-\frac{h}{h_0}} \right] \end{aligned} \quad (96)$$

$$\begin{aligned}
& + M_1 \frac{h}{h_0} e^{-\frac{h}{h_0}} \cdot \frac{9.240 M_1}{\Delta \cos Z_0} [1 + (n_0 - 1) \tan^2 Z_0] \left[1 - e^{-\frac{h}{h_0}} \left(\frac{h}{h_0} + 1\right)\right] \\
& - M_3 \frac{h}{h_0} e^{-3\frac{h}{h_0}} \cdot \frac{1.026 M_3}{\Delta \cos Z_0} [1 + (n_0 - 1) \tan^2 Z_0] \left[e^{-3\frac{h}{h_0}} \left(3\frac{h}{h_0} + 1\right) - 1\right] \\
& + N \frac{h^2}{h_0^2} e^{-\frac{h}{h_0}} \cdot \frac{9.240}{\Delta \cos Z_0} [1 + (n_0 - 1) \tan^2 Z_0] \left[2 - e^{-\frac{h}{h_0}} \left(\frac{h^2}{h_0^2} + 2\frac{h}{h_0} + 1\right)\right]
\end{aligned}$$

As always  $\Delta$  must be expressed in kilometers. The refraction  $\sigma$  is always less than  $R$ , consequently

$$\epsilon > R > \frac{\epsilon}{Z}$$

6. Computation of the Distance  $\Delta$  of an object inside the Atmosphere. When the distance  $\Delta$  is unknown it can be obtained as follows:

$$dy = \frac{dh}{\cos Z}$$

From

$$\frac{1}{\cos Z} = \frac{\tan Z}{\sin Z}$$

we have found

$$\frac{1}{\cos Z} = \frac{1}{\cos Z_0} - x \frac{\tan^2 Z_0}{\cos Z_0} + \frac{3}{2} x^2 \frac{\tan^2 Z_0}{\cos Z_0}$$

$$+ \frac{3}{2} x^2 \frac{\tan^4}{\cos Z_0} + x^3 \frac{\tan^2 Z_0}{\cos Z_0} (1 + \tan^2 Z_0) + \dots$$

where

$$x = \frac{h}{n_0 r_0} + (n_0 - 1) e^{-\frac{h}{h_0}} \left(1 + \frac{h}{r_0}\right)$$

$$x^m = \left(\frac{h}{n_0 r_0}\right)^m \quad m = 2, 3, \dots$$

After these values are replaced and integrated we find

$$\begin{aligned} \Delta = & \frac{h}{\cos Z_0} - \frac{1}{2} \frac{h^2}{n_0 r_0} \frac{\tan^2 Z_0}{\cos Z_0} + (n_0 - 1) h \frac{\tan^2 Z_0}{\cos Z_0} \\ & - \frac{(n_0 - 1) h_0}{n_0} \frac{\tan^2 Z_0}{\cos Z_0} - (n_0 - 1) \frac{h_0^2 \tan^2 Z_0}{n_0 r_0 \cos Z_0} \\ & - \frac{3}{2} \frac{(n_0 - 1)}{n_0 r_0} h^2 \frac{\tan^2 Z_0}{\cos Z_0} (1 + \tan^2 Z_0) \\ & + 3 \frac{(n_0 - 1)}{n_0 r_0} h_0^2 \frac{\tan^2 Z_0}{\cos Z_0} (1 + \tan^2 Z_0) \\ & + \frac{1}{2} \frac{h^3}{n_0^2 r_0^2} \frac{\tan^2 Z_0}{\cos Z_0} (1 + \tan^2 Z_0) \\ & + (n_0 - 1) \frac{h_0}{n_0} \frac{\tan^2 Z_0}{\cos Z_0} e^{-\frac{h}{h_0}} \end{aligned} \tag{97}$$

$$\begin{aligned}
& + \frac{3}{2} \frac{h^2 (n_o - 1)}{n_o r_o} \frac{\tan^2 Z_o}{\cos Z_o} e^{-\frac{h}{h_o}} \left( \frac{h}{h_o} + 1 \right) \\
& - 3 \frac{(n_o - 1)}{n_o r_o} h_o^2 e^{-\frac{h}{h_o}} \left( \frac{h}{h_o} + 1 \right) \frac{\tan^2 Z_o}{\cos Z_o} (1 + \tan^2 Z_o)
\end{aligned}$$

7. Working Equations to Obtain Coefficients  $E_1$ ,  $E_2$ ,  $E_3$ ,  $M_1$ ,  $M_3$ , and  $N$ . These coefficients can be computed from the following working equations:

$$E_1 = - (n_o - 1) \tan Z_o + [0.0680 - 0.00010 \tan^2 Z_o] \tan Z_o (1 + \tan^2 Z_o)$$

$$E_2 = + 0.033 \tan Z_o + 0.0081 \tan^3 Z_o$$

$$E_3 = + 0.000005 \tan Z_o (1 + \tan^2 Z_o)$$

(98)

$$M_1 = + [0.0849 + 0.00044 \tan^2 Z_o] \tan Z_o (1 + \tan^2 Z_o)$$

$$M_3 = + 0.0168 \tan Z_o (1 + \tan^2 Z_o)$$

$$N = - 0.000006 \tan Z_o (1 + \tan^2 Z_o) (2 + 3 \tan^2 Z_o)$$

8. Computation of  $(n_o - 1)$ . The refractive index ( $n$ ) of standard air at optical frequencies can be obtained from that given by Barrel and Sears

$$(n_o - 1) 10^7 = 2876.04 + \frac{16.288}{\lambda^2} + \frac{0.136}{\lambda^4} \quad (99)$$

where

$\lambda$  = the light group wavelength in microns. This equation agrees to 1 in  $10^8$  over the visible spectrum.

$$(n_0 - 1) = \frac{n_c - 1}{1 + \alpha t} \frac{P}{760} - \frac{0.000000055 e}{1 + \alpha t} \text{ where} \quad (100)$$

$n_0$  = refractive index under ambient conditions

$n_c$  = refractive index in dry air with 0.03 %  $\text{CO}_2$  at NTP ( $0^\circ \text{C}$ , 760 mm Hg) for light of the group wavelength employed, as calculated here

$t$  = temperature in centigrade

$P$  = atmospheric pressure in mm Hg

$\alpha$  = coefficient of expansion of air ( $\alpha = 0.00367$ )

$e$  = partial vapor pressure in mm Hg

Table I gives the vapor pressure corresponding to saturation at various temperatures

Table I. Pressure of Saturated Water Vapor

Temp.in $0^\circ \text{C}$	mm of Hg
-5	3.02
0	4.58
5	6.54
10	9.21
15	12.79
20	17.55
25	23.78
30	31.86
35	42.23
40	55.40

Let us compute an example

The following conditions are chosen as being in effect at the observing site:

$\varphi$ = latitude	38°
P = atmosphere pressure	760 mm Hg
t = temperature	+10° C
RH = relative humidity =	60%
$\lambda$ = effective wave length	0.578
hs = height of the object =	13.96 km
$Z_0$ = observed zenith distance =	70°
$h_a$ = height of the station above sea level	0.1 km

Computation of the Refractive Index

$$(n_0 - 1) 10^7 = 2876.04 + \frac{16.288}{\lambda^2} + \frac{0.136}{\lambda^4}$$

$$(n_0 - 1) = \frac{(n_0 - 1)}{1 + \alpha t} \frac{P}{760} - \frac{0.00000055 e}{1 + \alpha t}$$

$\lambda = 0.578$	$\frac{16.288}{\lambda^2}$ .....	49.264
$\lambda^2 = 0.330625$	$\frac{0.136}{\lambda^4}$	1.244
$\lambda^4 = 0.109313$	$(n_0 - 1) 10^7 =$	$\frac{2876.04}{2926.55}$

$$n_0 - 1 = 0.000292655$$

$$\alpha = 0.00367$$

From Table I, for 60 % R. H. and temperature = 10°

$$e = 5.53$$

so

$$n_0 - 1 = 0.00028180$$

$$(n_0 - 1)'' = 58''1254$$

Computation of the Distance  $\Delta$

$h = h_s - h_a$	13.86	km
$s_0 = \frac{h_0}{n_0 r_0}$	0.001450	"
$s = \frac{h}{n_0 r_0}$	0.002176	"
$\frac{h}{h_0} =$	1.5	"
$\frac{h}{\cos Z_0}$	40.5239	"
$-\frac{1}{2} s h \frac{\tan^2 Z_0}{\cos Z_0}$	-0.3328	"
$+ (n_0 - 1) h \frac{\tan^2 Z_0}{\cos Z_0}$	+0.0862	"
$- (n_0 - 1) h_0 \frac{\tan^2 Z_0}{\cos Z_0}$	-0.0575	"
$- s_0 \cdot h_0 (n_0 - 1) \frac{\tan^2 Z_0}{\cos Z_0}$	-0.0001	"
$-\frac{3}{2} s h (n_0 - 1) \frac{\tan^2 Z_0}{\cos Z_0} (1 + \tan^2 Z_0)$	-0.0024	"

$$\begin{aligned}
& + 3 s_0 h_0 (n_0 - 1) \frac{\tan^2 Z_0}{\cos Z_0} (1 + \tan^2 Z_0) && +0.0022 \text{ km} \\
& + \frac{1}{2} h s^2 \frac{\tan^2 Z_0}{\cos Z_0} (1 + \tan^2 Z_0) && +0.0062 \text{ ''} \\
& + (n_0 - 1) h_0 \frac{\tan^2 Z_0}{\cos Z_0} e^{-\frac{h}{h_0}} && +0.0128 \text{ ''} \\
& + \frac{3}{2} (n_0 - 1) h_0 s_0 \frac{\tan^2 Z_0}{\cos Z_0} e^{-\frac{h}{h_0}} \left( \frac{h}{h_0} + 1 \right) && +0.0001 \text{ ''} \\
& - 3 (n_0 - 1) h_0 s_0 e^{-\frac{h}{h_0}} \left( \frac{h}{h_0} + 1 \right) (1 + \tan^2 Z_0) \frac{\tan^2 Z_0}{\cos Z_0} && -0.0012 \text{ ''} \\
\hline
& && \Delta = 40.2374 \text{ km}
\end{aligned}$$

Computation of the Coefficients  $E_1$ ,  $E_2$ ,  $M_1$ ,  $M_3$ , and  $N$

Equation (98)

$$\tan Z_0 = 2.747477$$

$$\tan^2 Z_0 = 7.5486$$

$$\tan^3 Z_0 = 20.74$$

$$2 + 3 \tan^2 Z_0 = 24.65$$

$$\tan Z_0 (1 + \tan^2 Z_0) = 23.49$$

$$E_1 = -(n_0 - 1) \tan Z_0 + [0''0680 - 0''00010 \tan^2 Z_0] \tan Z_0 (1 + \tan^2 Z_0)$$

$$\underline{E_1 = -157'' \ 118}$$

$$E_2 = +0''033 \tan Z_0 + 0''0081 \tan^3 Z_0$$

$$\underline{E_2 = 0''259}$$



$$M_1 = +[0''0168 + 0''00044 \operatorname{tn}^2 Z_0] \operatorname{tn} Z_0 (1 + \operatorname{tn}^2 Z_0)$$

$$\underline{M_1 = + 2''072}$$

$$M_3 = +0''0168 \operatorname{tn} Z_0 (1 + \operatorname{tn}^2 Z_0)$$

$$\underline{M_3 = + 0''395}$$

$$N = -0''00006 \operatorname{tn} (1 + \operatorname{tn}^2 Z_0) (2 + 3 \operatorname{tn}^2 Z_0)$$

$$\underline{N = -0''035}$$

#### Computation of Refraction R

##### Equation (94)

$A_0 = +0.99827$	$\cos Z_0$	$= 0.34202$
$A_1 = -0.00130$	$\operatorname{tn} Z_0$	$= 2.747477$
$A_2 = +0.000006$	$\operatorname{tn}^3 Z_0$	$= 20.74$
$h = 13.86$	$\operatorname{tn}^5 Z_0$	$= 156.6$
$h_0 = 9.24$	$e^{-\frac{h}{h_0}}$	$= 0.2231$
$\Delta = 40.2374$	$e^{-3 \frac{h}{h_0}}$	$= 0.0111$
$\Delta \cos Z_0 = 13.7620$	$1 + (n_0 - 1) \operatorname{tn}^2 Z_0$	$= 1.0021$

$$E_1 = -157.118$$

$$E_2 = +0.259$$

$$M_1 = +2.072$$

$$M_3 = +0.395$$

$$N = -0.035$$

$$1 - e^{-\frac{h}{h_0}} = 0.7769$$

$$e^{-\frac{h}{h_0}} \left( \frac{h}{h_0} + 1 \right) - 1 = -0.4422$$

$$e^{-3\frac{h}{h_0}} \left( 3\frac{h}{h_0} + 1 \right) - 1 = -0.9390$$

$$2 - e^{-\frac{h}{h_0}} \left( \frac{h^2}{h_0^2} + 2\frac{h}{h_0} + 2 \right) = +0.3825$$

$$(n_0 - 1) A_0 \tan Z_0 \quad 159.422$$

$$+ (n_0 - 1) A_1 \tan^3 Z_0 \quad -1.568$$

$$+ (n_0 - 1) A_2 \tan^5 Z_0 \quad +0.055$$

$$+ \frac{9.24 E_1}{\Delta \cos Z_0} \left[ 1 + (n_0 - 1) \tan^2 Z_0 \right] \left[ 1 - e^{-\frac{h}{h_0}} \right] \quad -82.126$$

$$+ 0.0134 E_1 \frac{\tan^2 Z_0}{\Delta \cos Z_0} \left[ e^{-\frac{h}{h_0}} \left( \frac{h}{h_0} + 1 \right) - 1 \right] \quad +0.511$$

$$+ \frac{4.620 E_2}{\Delta \cos Z_0} \left[ 1 - e^{-\frac{h}{h_0}} \right] \quad +0.068$$

$$\begin{aligned}
& + \frac{9.24 M_1}{\Delta \cos Z_0} [1 + (n_0 - 1) \tan^2 Z_0] \left[ 1 - e^{-\frac{h}{h_0}} \left( \frac{h}{h_0} + 1 \right) \right] & +0.616 \\
& + \frac{1.026 M_3}{\Delta \cos Z_0} [1 + (n_0 - 1) \tan^2 Z_0] \left[ e^{-3 \frac{h}{h_0}} \left( 3 \frac{h}{h_0} + 1 \right) - 1 \right] & +0.028 \\
& + \frac{9.24 N}{\Delta \cos Z_0} [1 + (n_0 - 1) \tan^2 Z_0] \left[ 2 - e^{-\frac{h}{h_0}} \left( \frac{h^2}{h_0^2} + 2 \frac{h}{h_0} + 2 \right) \right] & +0.009 \\
\hline
& & 77.02
\end{aligned}$$

$$R = 77.02$$

Computation of the Refraction  $\epsilon$

Equation (71)

$$\begin{aligned}
\frac{h}{h_0} = 1.5 & & e^{-\frac{h}{h_0}} & = 0.2231 \\
& & e^{-2 \frac{h}{h_0}} & = 0.050 \\
& & e^{-3 \frac{h}{h_0}} & = 0.011 \\
(n_0 - 1) A_0 \tan Z_0 & & & 159.422 \\
+ (n_0 - 1) A_1 \tan^3 Z_0 & & & - 1.568 \\
+ (n_0 - 1) A_2 \tan^5 Z_0 & & & + 0.065 \\
+ E_1 e^{-\frac{h}{h_0}} & & & -35.053 \\
+ E_2 e^{-2 \frac{h}{h_0}} & & & + 0.013
\end{aligned}$$

$$\begin{aligned}
& - E_3 e^{-3 \frac{h}{h_0}} && 0.000 \\
& + M_1 \frac{h}{h_0} e^{-\frac{h}{h_0}} && + 0.693 \\
& - M_3 \frac{h}{h_0} e^{-3 \frac{h}{h_0}} && - 0.007 \\
& + N \left( \frac{h}{h_0} \right)^2 e^{-\frac{h}{h_0}} && - 0.018 \\
\hline
& && 123.537
\end{aligned}$$

$$e = 2' 03.54$$

Computation of the Refraction  $\sigma$

$$\begin{aligned}
& E_1 e^{-\frac{h}{h_0}} && - 35.053 \\
& - \frac{9.240}{\Delta \cos Z_0} \left[ 1 + (n_0 - 1) \tan^2 Z_0 \right] \left[ 1 - e^{-\frac{h}{h_0}} \right] && + 82.126 \\
& + 1.0134 \frac{E_1 \tan^2 Z_0}{\Delta \cos Z_0} \left[ 1 - e^{-\frac{h}{h_0}} \left( \frac{h}{h_0} + 1 \right) \right] && - 0.511 \\
& + E_2 e^{-2 \frac{h}{h_0}} && + 0.013 \\
& - \frac{4.620 E_2}{\Delta \cos Z_0} \left[ 1 - e^{-\frac{h}{h_0}} \right] && - 0.068 \\
& + M_1 \frac{h}{h_0} e^{-\frac{h}{h_0}} && + 0.693
\end{aligned}$$

$$\begin{aligned}
& - \frac{9.240 M_1}{\Delta \cos Z_0} \left[ 1 + (n_0 - 1) \tan^2 Z_0 \right] \left[ 1 - e^{-\frac{h}{h_0}} \left( \frac{h}{h_0} + 1 \right) \right] & -0.616 \\
& - M_1 \frac{h}{h_0} e^{-3 \frac{h}{h_0}} & -0.007 \\
& - \frac{1.026 M_3}{\Delta \cos Z_0} \left[ 1 + (n_0 - 1) \tan^2 Z_0 \right] \left[ e^{-3 \frac{h}{h_0}} \left( 3 \frac{h}{h_0} + 1 \right) - 1 \right] & -0.028 \\
& + N \left( \frac{h}{h_0} \right)^2 e^{-\frac{h}{h_0}} & -0.018 \\
& - \frac{9.240}{\Delta \cos Z_0} \left[ 1 + (n_0 - 1) \tan^2 Z_0 \right] \left[ 2 - e^{-\frac{h}{h_0}} \left( \frac{h^2}{h_0^2} + 2 \frac{h}{h_0} + 1 \right) \right] & -0.009 \\
& & \underline{\hspace{10em}} \\
& & 46''.52
\end{aligned}$$

$$\sigma = 46''.52$$

$$\sigma = \epsilon - R$$

$$\sigma = 46''.52$$

Astronomical Refraction

$$\epsilon_a = (n_0 - 1) A_0 \tan Z_0 + (n_0 - 1) A_1 \tan^3 Z_0 + (n_0 - 1) A_2 \tan^5 Z_0$$

$$\epsilon_a = 157''.91$$

The set of values obtained are as follows:

$$\epsilon_a = 2'37''.91$$

$$\epsilon = 2'03''.54$$

$$R = 1\ 17.02$$

$$\sigma = 46.52$$

$$R > \frac{1}{2} \epsilon$$

$$1'17''02 > 1'01''8$$

9. Refraction Viewed from an Object Outside the Atmosphere.

The foregoing equations are correctly applied to an object inside the atmosphere for zenith distances less than  $75^\circ$  and with the height of the atmosphere of 65 kilometers, which may be regarded as the limit beyond which the air does not produce any appreciable refraction. For such conditions we have expanded  $\ln Z$  in series. An object outside the atmosphere can be treated as follows:

In Figure 3 let S be the object. There is a point  $S_0$  at which the ray coming from S reaches the upper layer of the atmosphere after which following the curve  $S_0A$ , it reaches the point A.

The x and y coordinates have the same meaning as before.

At the limit of the atmosphere, formula (94) gives  $R_0$ .

$\epsilon_a = TNS$  is only the astronomic refraction.

The refraction we are looking for is  $R_s = TAS$ .

From Figure 3 it follows that

$$\sin R_s = \frac{x_s}{\Delta_s} \tag{101}$$

$$\sin R_0 = \frac{x_0}{R_0}$$

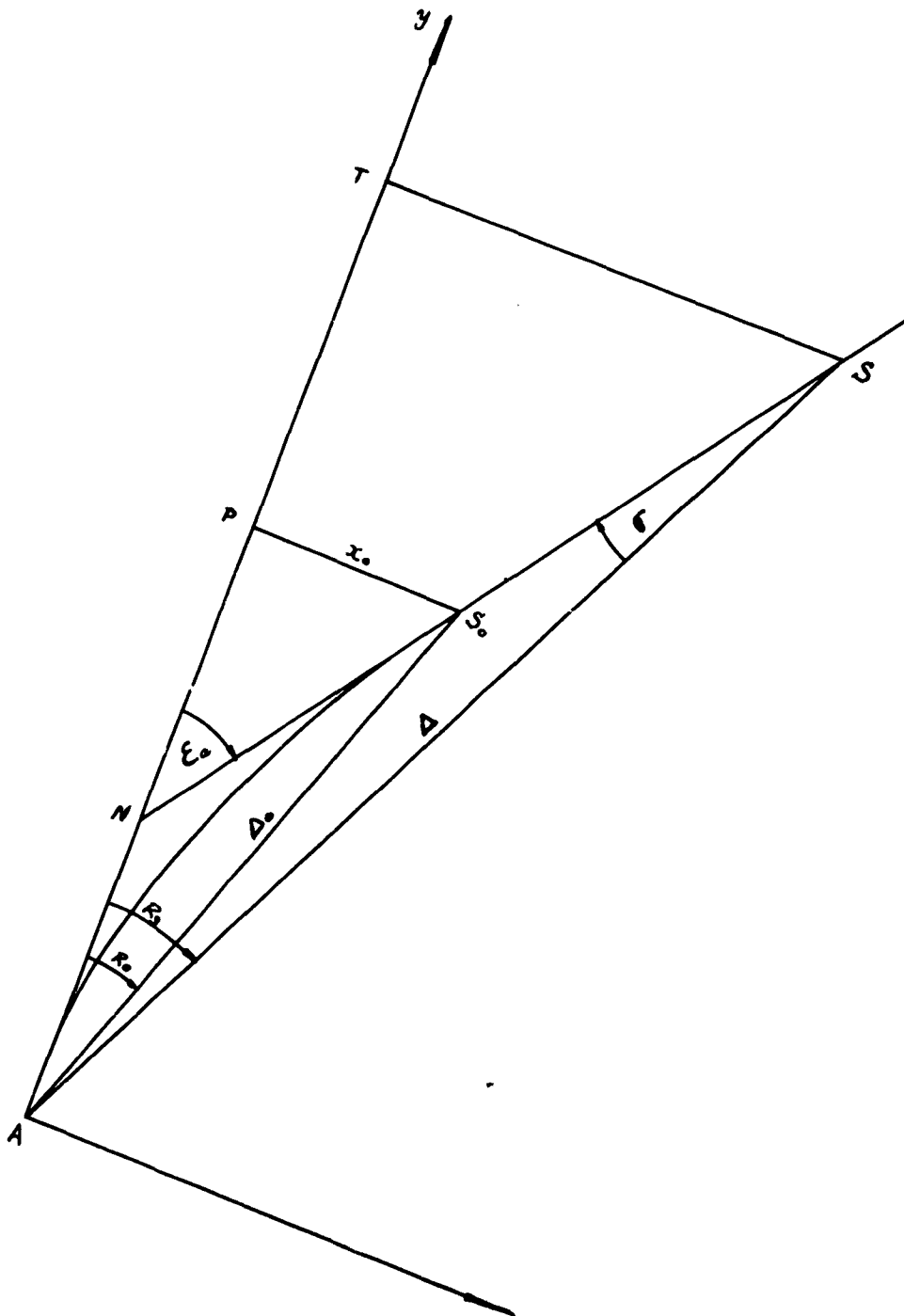


Fig. 3. Fundamental concepts in relation to Fig. 1.

but

$$x_B = NT \tan \epsilon_a$$

$$NT = NP + PT$$

and

$$NP = \frac{x_0}{\tan \epsilon_a}$$

so

$$x_B = x_0 + PT \tan \epsilon_a$$

then

$$\sin R_B = \frac{x_0}{\Delta_B} + \frac{PT}{\Delta_B} \tan \epsilon_a \quad (102)$$

Because  $R_B$  or  $R_0$  is a small angle of about 3 minutes for  $Z_0 = 75^\circ$

$$PT = \Delta_B - \Delta_0$$

so

$$\sin R_B = \frac{x_0}{\Delta_B} + \frac{\Delta_B - \Delta_0}{\Delta_B} \tan \epsilon_a \quad (103)$$

The refraction  $R_0$  can be obtained from equation (94) without considering the terms which contain  $e^{-\frac{h}{h_0}}$  and  $e^{-3\frac{h}{h_0}}$ , because at the height of  $S_0$ , they become extremely small. Since we can write

$$\epsilon_a = (n_0 - 1) \tan \left[ 1 - \frac{3}{2} (n_0 - 1) \right] + A.C_A + B.C_B + C.C_C$$

We can write equation (93) as follows:

$$R_0 = \epsilon_a + \frac{E_1}{\Delta_0} \left[ \frac{h_0}{\cos Z_0} (1 + (n_0 - 1) \tan^2 Z_0 - \frac{h_0 \tan^2 Z_0}{n_0 r_0}) \right]$$



but

$$x_s = NT \tan \epsilon_a$$

$$NT = NP + PT$$

and

$$NP = \frac{x_o}{\tan \epsilon_a}$$

so

$$x_s = x_o + PT \tan \epsilon_a$$

then

$$\sin R_s = \frac{x_o}{\Delta_s} + \frac{PT}{\Delta_s} \tan \epsilon_a \quad (102)$$

Because  $R_s$  or  $R_o$  is a small angle of about 3 minutes for  $Z_o = 75^\circ$

$$PT = \Delta_s - \Delta_o$$

so

$$\sin R_s = \frac{x_o}{\Delta_s} + \frac{\Delta_s - \Delta_o}{\Delta_s} \tan \epsilon_a \quad (103)$$

The refraction  $R_o$  can be obtained from equation (94) without considering the terms which contain  $e^{-\frac{h}{h_o}}$  and  $e^{-3\frac{h}{h_o}}$ , because at the height of  $S_o$ , they become extremely small. Since we can write

$$\epsilon_a = (n_o - 1) \tan \left[ 1 - \frac{3}{2} (n_o - 1) \right] + A.C_A + B.C_B + C.C_C$$

We can write equation (93) as follows:

$$R_o = \epsilon_a + \frac{E_1}{\Delta_o} \left[ \frac{h_o}{\cos Z_o} \left( 1 + (n_o - 1) \tan^2 Z_o - \frac{h_o \tan^2 Z_o}{n_o r_o} \right) \right]$$

$$+ \frac{1}{2} \frac{E_2}{\Delta_0} \frac{h_0}{\cos Z_0} + \frac{M_1}{\Delta_0} \frac{h_0}{\cos Z_0} - \frac{M_3}{\Delta_0} \frac{h_0}{9 \cos Z_0} \quad (104)$$

Because

$$x_0 = \Delta_0 \cdot \sin R_0 = \Delta \cdot R_0$$

it follows that

$$x_0 = \epsilon \cdot \Delta_0 + E_1 \left[ \frac{h_0}{\cos Z_0} (1 + (n_0 - 1) \tan^2 Z_0 - \frac{h_0 \tan^2 Z_0}{n_0 r_0}) \right] \quad (105)$$

$$+ \frac{1}{2} E_2 \frac{h_0}{\cos Z_0} + M_1 \frac{h_0}{\cos Z_0} - M_3 \frac{h_0}{9 \cos Z_0}$$

Indicate by  $\Sigma$  all the terms of the right hand free of  $\Delta_0$  and we have

$$x_0 = \epsilon \cdot \Delta_0 + \Sigma \quad (106)$$

Now, introduce this value  $x_0$  into equation (103) and we obtain

$$R_B = \epsilon_a \frac{\Delta_0}{\Delta_B} + \frac{\Sigma}{\Delta_B} + \frac{\Delta_B - \Delta_0}{\Delta_B} \epsilon_a \quad (107)$$

which simplifies to

$$R_B = \epsilon_a + \frac{\Sigma}{\Delta_B} \quad (108)$$

because

$$\epsilon = \epsilon_a$$

Equation (108) shows that the refraction outside the atmosphere is obtained by introducing a correction to the astronomical refraction, by an amount given by  $\frac{\Sigma}{\Delta_S}$ .

Since  $\Delta_S$  can be any distance, for an object at infinity

$$\frac{\Sigma}{\Delta_S} = 0$$

consequently,

$$R_S = \epsilon_a$$

which is the astronomical refraction.

10. Computation of the Distance  $\Delta$  of an Object Outside the Atmosphere. Equation (97) is not good now for computing the distance of an object outside the atmosphere because it was developed to be used inside the atmosphere. For a height over 65 kilometers the following equation must be used:

$$\Delta = \frac{1}{2} s r_0 \frac{1 + \cos \theta}{\cos \frac{1}{2} \theta \cos (\gamma - \sigma)} \quad (109)$$

where

$$s = \frac{h_S}{r_0}$$

$$\theta = Z_0 + \epsilon_a - Z$$

$\epsilon_a$  = astronomical refraction

$$Z = \arcsin \left( \frac{n_0}{1+s} \sin Z_0 \right)$$

$$\epsilon_a = (n_0 - 1) A_0 \tan Z_0 + (n_0 - 1) A_1 \tan^3 Z_0 + (n_0 - 1) A_2 \tan^5 Z_0$$

$$\gamma = \frac{1}{2} (Z_0 + \epsilon_a + Z)$$

$\sigma$  always is a small angle (a few seconds) so we can assume  $\sigma = 0$  for computing the distance  $\Delta$ , with sufficient accuracy for obtaining R or  $\sigma$ . To obtain an error  $dR = 0''01$  the error  $\delta\Delta$  in  $\Delta$  reaches the following values for a zenith distance  $Z_0 = 70^\circ$ :

$$H = 100 \text{ km} \quad \text{is } \delta\Delta = 200 \text{ meters}$$

$$H = 1000 \text{ km} \quad \text{is } \delta\Delta = 10,000 \text{ meters}$$

If it is required to obtain  $\Delta$  with higher accuracy, in equation (109) the value of  $\sigma$  computed from equation (111) must be introduced.

Then, the refraction R can be obtained by using the following equation:

$$\begin{aligned} R = & (n_0 - 1) A_0 \tan Z_0 + (n_0 - 1) A_1 \tan^3 Z_0 + (n_0 - 1) A_2 \tan^5 Z_0 \\ & + \frac{9.24 E_1}{\Delta \cos Z_0} \left[ 1 + (n_0 - 1) \tan^2 Z_0 \right] \\ & - 0.0134 \frac{E_1 \tan^2 Z_0}{\Delta \cos Z_0} + \frac{4.62 E_2}{\Delta \cos Z_0} \quad (110) \\ & + \frac{9.24 M_1}{\Delta \cos Z_0} \left[ 1 + (n_0 - 1) \tan^2 Z_0 \right] \\ & - 1.026 \frac{M_3 \left[ 1 + (n_0 - 1) \tan^2 Z_0 \right]}{\Delta \cos Z_0} + \frac{18.48 N}{\Delta \cos Z_0} \end{aligned}$$

11. Computation of the Refraction Angle  $\sigma$  of an Object outside the Atmosphere. This refraction is the angle  $\sigma$ . It can be obtained by using the following equation:

$$\sigma = - \frac{9.24 E_1}{\Delta \cos Z_0} \left[ 1 + (n_0 - 1) \tan^2 Z_0 \right] + 0.0134 \frac{E_1 \tan^2 Z_0}{\Delta \cos Z_0}$$

$$\begin{aligned}
& - \frac{4.62 E_2}{\Delta \cos Z_0} - 9.24 \frac{M_1 [1 + (n_0 - 1) \tan^2 Z_0]}{\Delta \cos Z_0} \\
& + 1.026 \frac{M_3 [1 + (n_0 - 1) \tan^2 Z_0]}{\Delta \cos Z_0} - \frac{18.48 N}{\Delta \cos Z_0}
\end{aligned} \tag{111}$$

### Example of Computation

We assume the same data as used for computing  $R$  and  $\sigma$  for an object inside the atmosphere, and change  $h_g$  to:

$$h_g = 100 \text{ kilometers}$$

$$h_g = 1,000 \text{ kilometers}$$

as before

$$Z_0 = 70^\circ$$

and assuming

$$h_a = 0$$

the constants used are:

$$E_1 = - 157''.118$$

$$E_2 = + 0.259$$

$$M_1 = + 2.072$$

$$M_3 = + 0.395$$

$$N = - 0.035$$

$$\gamma_0 = 6370.06 \text{ km}$$

Computation of the Distance

$$\sin Z = \frac{n_0}{(1 + s)} \sin Z_0$$

	H = 100 km	H = 1,000 km
s	0.0156984	0.1569840
sin Z <sub>0</sub>	0.9396926	
n <sub>0</sub>	1.0002818	
sin Z	0.9254296	0.8124204
Z	67° 43' 59.6	54° 19' 59.0
Z <sub>0</sub>	70°	70°
ε <sub>a</sub>	2' 37.9	2 37.9
γ	68 53 18.7	62 11 18.4
θ	2 18 38.3	15 42 38.9
$\frac{1}{2} \theta$	1 09 19.2	7 51 19.4
1 + cos θ	1.999 1868	1.962 6407
cos γ	0.36018 36	0.466 5650
Δ	277.579	2123.206
Δ .cos Z <sub>0</sub>	94.938	
γ - σ	58° 53' 03.6	62° 11' 16.3
cos (γ - σ)	0.360 2519	0.466 5741
Δ	277.5264	2123.1698
Δ cos Z <sub>0</sub>	94.920	726.167

Computation of the Refraction  $\sigma$

	H = 100	H = 1,000
- 9.24 $\frac{E_1 [1 + (n_0 - 1) \tan^2 Z_0]}{\Delta \cos Z_0}$	+15.422	+2.016
+ 0.0134 $\frac{E_1 \tan^2 Z_0}{\Delta \cos Z_0}$	-0.167	-0.022
- $\frac{4.62 E_2}{\Delta \cos Z_0}$	-0.013	-0.002
- $\frac{9.24 M_1 [1 + (n_0 - 1) \tan^2 Z_0]}{\Delta \cos Z_0}$	-0.202	-0.026
+ 1.026 $\frac{M_3 [1 + (n_0 - 1) \tan^2 Z_0]}{\Delta \cos Z_0}$	+0.043	+0.001
- $\frac{18.48 N}{\Delta \cos Z_0}$	+0.006	+0.001
$\sigma =$	+15"083	1.968

Now, introduce these values of  $\sigma$ , and the new values of  $\Delta$  are:

$$H = 100 \text{ km: } \Delta = 277.5264 \text{ km}$$

$$H = 1000 \text{ km: } \Delta = 2123.1698 \text{ km}$$

These new values do not alter the preceding value.

Then, the results are as follows:

$$H = 100 \text{ km}$$

$$H = 1000 \text{ km}$$

$$R = \epsilon_a - R$$

$$\epsilon_a = 2'37".9$$

$$\sigma = 15".1$$

$$R = 2'22".8$$

$$\epsilon_a = 2'37".9$$

$$\sigma = 2".0$$

$$R = 2'35".9$$



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