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TRAFFICABILITY OF SOILS

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TESTS ON COARSE-GRAINED SOILS WITH SELF-PROPELLED AND TOWED VEHICLES, 1956 AND 1957



TECHNICAL MEMORANDUM NO. 3-240 FIFTEENTH SUPPLEMENT

June 1959

U. S. Army Engineer Waterways Experiment Station CORPS OF ENGINEERS

Vicksburg, Mississippi

ARMY-MRC VICKSBURG MISS

PREFACE

The tests reported herein are part of the studies conducted by the U. S. Army Engineer Waterways Experiment Station under Corps of Engineers Subproject 8-70-05-400, "Trafficability of Soils as Related to the Mobility of Military Vehicles," and were also financed in part by the Bureau of Yards and Docks, Department of the Navy.

Acknowledgment is made to the consultants for trafficability studies and to the representatives of the Bureau of Yards and Docks, Department of Agriculture, Detroit Arsenal, and Office, Chief of Engineers, who participated in a conference at the Waterways Experiment Station on 12 May 1955 and offered suggestions for conducting the tests reported herein. Special acknowledgment is made to Dr. A. A. Warlam, consultant, for his participation in the Pacific islands test program.

These tests were performed by personnel of the Army Mobility Research Center, Soils Division, Waterways Experiment Station, under the supervision of Messrs. W. J. Turnbull, C. R. Foster, and S. J. Knight. Engineers actively engaged in the study were Messrs. A. A. Rula and E. S. Rush. This report was prepared by Mr. Rush.

Directors of the Waterways Experiment Station during the conduct of this study and preparation of this report were Col. A. P. Rollins, Jr., CE, and Col. Edmund H. Lang, CE. Mr. J. B. Tiffany was Technical Director.

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SUMMARY

Three types of vehicle tests (self-propelled, towing, and towed) were conducted with several military vehicles over a range of vehicle weights, tire pressures, and sand strengths and conditions for the following purposes:

- a. To determine whether the trafficability characteristics of coral and volcanic sands differ from those of quartz sands previously tested.
- b. To establish more definitive relations between sand condition and vehicle mobility by testing vehicles on softer sands than previously tested.
- <u>c</u>. To determine towing abilities of self-propelled vehicles over a range of sand conditions.
- <u>d</u>. To determine towing-force requirements of various vehicles over a range of sand conditions.

Single self-propelled wheeled vehicles were tested on undisturbed coral and velcanic sands on Pacific islands, and on quartz sand (dese.t and beach) in the United States. Towing tests with self-propelled vehicle. were conducted on harrowed desert quartz sands near Yuma, Arizona. Toured wheeled trailers were tested on disturbed and undisturbed quartz sand at Camp Lejeune, North Carolina. Principal conclusions were that: (a) performance of single self-propelled wheeled vehicles can be expressed in cone indexslope climbing ability terms; (b) wet sands are more trafficable than dry-to-moist sands; (c) performance, as defined by the cone index-slope climbing curves, is the same regardless of sand source (quartz, volcanic, or coral) or location (beach or desert); (d) towing ability of selfpropelled vehicles (wheeled and tracked) on harrowed sand slopes can be computed with reasonable accuracy from performance measurements obtained in tests of the respective vehicles on level harrowed sand; and (e) towingforce requirements of wheeled trailers can be correlated with cone index and tire pressure.

TRAFFICABILITY OF SOILS <u>TESTS ON COARSE-GRAINED SOILS</u> <u>WITH SELF-PROPELLED AND TOWED VEHICLES</u>

1956 AND 1957

PART I: INTRODUCTION

Purpose and Scope of Test Inogram

1. The tests reported herein are part of a study to establish relations between coarse-grained soils and the ability of military vehicles to negotiate them. These tests had the following specific objectives:

- <u>a</u>. To determine whether the trafficability characteristics of coral and volcanic sands differ from those of quartz sands previously tested.
- b. To establish more definitive relations between sand condition and vehicle mobility by testing vehicles on softer sands than previously tested.

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- c. To determine towing abilities of self-propelled vehicles over a range of sand conditions.
- <u>d</u>. To determine towing-force requirements of various vehicles over a range of sand conditions.

2. Objectives <u>a</u> and <u>b</u> were accomplished by tests on the beaches of certain islands in the Pacific Ocean. Objective <u>c</u> was partially accomplished by tests on desert sands near Yuma, Arizona, and objective <u>d</u> was partially accomplished by tests at Camp Lejeune, North Carolina. Testing of additional vehicles on a wider range of sand conditions will be necessary to complete these latter two objectives.

Previous Investigations

3. Since 1945 the Waterways Experiment Station has conducted a large number of traffic tests with military vehicles on a variety of soil conditions. Results of this work have been published in a series of reports with the general title "Trafficability of Soils," Technical Memorandum No. 3-240, which are listed on the inside of the front cover of this volume. Most of the tests were conducted on fine-grained soils, as these were believed to cause the greatest trafficability problems. The development of instruments and techniques for measuring the trafficability of these soils is considered to be essentially completed. Work to develop methods of measuring trafficability of coarse-grained soils is continuing.

Pilot Study of Coarse-grained Soils

4. In October 1953, a joint Army-Navy ad hoc committee assigned the responsibility for studying means of determining the trafficability of beaches (particularly those with coarse-grained soils) to the Waterways Experiment Station. The first phase of this project was a pilot study to provide background information concerning mobility problems on coarsegrained soils, and to determine whether instruments and techniques that have been successful in defining trafficability of fine-grained soils would also be successful in coarse-grained soils. This study was accomplished in 1954 and is reported in Technical Memorandum 3-240, 13th Supplement. All the vehicle tests reported in the 13th Supplement were conducted on quartztype sands found on inland areas and beaches of the United States. The important findings of this pilot study are summarized as follows:

- <u>a.</u> <u>Sand categories.</u> Two distinct sand categories, each requiring a different technique for the determination of its trafficability, were recognized: (1) clean sands that reacted in a frictional manner to traffic, and (2) sand with fines, poorly drained, that reacted in a more plastic manner.
- b. <u>Instruments.</u> The cone penetrometer was found to be as accurate an instrument for measuring sand trafficability as any tested, and was recommended for future use in sands, mainly on the basis of its ability to determine profile conditions but also because it had been previously accepted for use in fine-grained soils.
- c. <u>Remolding effects.</u> No necessity was found for predicting strength changes under vehicle traffic for most sands (see subparagraph <u>d</u>). For sands with fines, poorly drained, strength changes had to be estimated and a technique for doing this was developed.
- d. <u>Repetition of traffic.</u> In general, the first pass was found to be the most difficult for a wheeled vehicle in a sand area. Succeeding passes were made with increasingly less difficulty and smaller and smaller increases in rut depth. An exception to this occurred in some crusted sand. The surface crust supported the vehicle for one pass (or a few)

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but suddenly broke on a subsequent pass, causing the vehicle to become immobilized or making operation more difficult in the much softer sand and deeper ruts. Because only a few tests were conducted on crusted sands, no attempt was made to devise a means of predicting break-through.

- e. <u>Tire pressure</u>. Among individual vehicle characteristics, tire pressure was the most influential single factor in the performance of wheeled vehicles in sand.
- <u>f.</u> <u>Critical layer</u>. For all vehicles tested, the critical layer of the various sands appeared to be the top 6 in.

Definitions

5. Certain soil, beach, test-media, and vehicle terms used in this report are defined for the convenience of the reader.

Soil terms

<u>Fine-grained soil (fines).</u> A soil of which more than 50% of the grains, by weight, will pass a No. 200 U. S. standard sieve (smaller than 0.074 mm in diameter).

<u>Coarse-grained soil.</u> A soil of which more than 50% of the grains, by weight, will be retained on a No. 200 sieve (larger than 0.074 mm in diameter).

<u>Sand.</u> A coarse-grained soil with the greater percentage of the coarse fraction (larger than 0.074 mm) passing the No. 4 sieve (4.76 mm).

<u>Sand with fines, poorly drained.</u> A sand that contains some finegrained soil and is slow-draining. When wet, such sands behave similarly to very wet fine-grained soils under vehicular traffic.

<u>D</u>. Particle diameter, in millimeters, that is larger than the grain diameter of n per cent by weight of the sample (e.g., $D_{60} = 0.30$ means that 60% of the sample, by weight, has a grain diameter less than 0.30 mm).

Effective size. The effective size of a soil is that particle diameter, in millimeters, that is larger than the grain diameter of 10% by weight of the sample (D_{10}) .

Uniformity coefficient $(C_u) = \frac{D_{60}}{D_{10}}$. An index reflecting the shape of the grain-size curve. A material composed entirely of grains of the same d'uneter would have a uniformity coefficient of 1.0. <u>Median diameter.</u> The median diameter is that particle diameter that is larger (or smaller) than the grain diameter of 50% by weight of the sample (D_{50}) .

<u>Density.</u> The unit weight of the soil in pounds per cubic foot. Unless otherwise stated, the density is the dry unit weight.

Moisture content or water content. The ratic, expressed as a percentage, of the weight of water in the soil to the dry weight of the solid particles.

<u>Cone index.</u> An index of the shearing resistance of soil obtained with the cone penetrometer. The value is a dimensionless number representing the resistance of the soil to penetration of a 30-deg cone of 0.5sq-in. base or projected area. The number, although considered dimensionless, actually denotes pounds of force on the handle divided by the area of the cone base in square inches.

<u>T</u> <u>ficability</u>. The capacity of a soil to support the traffic of military vehicles.

<u>Bearing capacity.</u> The ability of a soil to support a vehicle without undue settlement.

<u>Traction capacity.</u> The ability of a soil to provide sufficient resistance to the push of the track or wheel of the vehicle to furnish the necessary thrust to move it.

<u>Critical layer.</u> The layer of soil regarded as being most pertinent to establishing the relation between soil strength and vehicle performance. (For coarse-grained soils, this appears to be the 0- to 6-in. layer.)

Liquefaction. The puddling and drastic reduction in strength of saturated (although initially firm) soil under the action of repetitive loading.

<u>Erosion.</u> The washing away of soil particles by water moving under and around that portion of a wheel or track in contact with the soil. <u>Beach terms</u>

Foreshore (FS).* That part of the beach ordinarily traversed by the uprush and downrush of waves as the tide rises and falls.

^{*} The beach terms noted with an asterisk were extracted from Appendix A, Beach Erosion Board Bulletin, Special Issue No. 2, March 1953. Other terms pertain to specific areas in which vehicular tests were conducted but which are not defined in the above-mentioned reference.

Backshore (BS).* That part of the beach between the foreshore and the forward dune apron (if present) or the coast line.

<u>Berm crest (BC) or beach berm.</u> The seaward limit of the backshore; usually a relatively flat area paralleling the foreshore and occasionally wetted by waves at high tide.

Berm backslope (BBS). A backshore area between the berm crest and the forward dune apron, usually sloping gently downward and landward.

Forward dune apron (FDA). The concave seaward slope of a line of dunes.

Dune area (DA), coastal. An area of wind-deposited sand between the forward dune apron and the coast line. Coastal dunes may be active or partially stabilized by vegetation.

Dune area, desert. An area of active sand dunes with little or no vegetation present. Desert dunes are much higher and much larger in area than coastal dunes.

<u>Cusp.</u>* One of a series of naturally formed low mounds of sand separated by crescent-shaped troughs spaced at more or less regular intervals along the foreshore.

Scarp, beach.* A line of steep slopes facing seaward, caused by wave erosion of the beach.

Test-media terms

<u>Harrowed sand.</u> Sand that has been harrowed to at least a 12-in. depth and the surface smoothed with a light drag.

Disturbed sand. Sand disturbed by traffic.

<u>Undisturbed sand.</u> A sand that apparently has not been recently disturbed.

Vehicle terms

Pass. One trip of the vehicle over the test course.

<u>Immobilization.</u> In this report, failure of a self-propelled vehicle to travel forward over sand, although it could possibly back up in its ruts. In this report, immobilizations of wheeled vehicles also were considered to take occurred whenever the drive wheels began to jerk violently and the vehicle began to make very labored, slow progress. <u>Maximum drawbar pull.</u> The maximum amount of sustained towing effort a self-propelled vehicle can produce at its drawbar under given test conditions.

<u>Towing-force requirements.</u> The amount of force required to tow a given vehicle under given test conditions.

<u>Tractive coefficient.</u> The ratio of the maximum drawbar pull to the gross weight of a vehicle.

<u>Slip.</u> The percentage of track or tire movement ineffective in thrusting the vehicle forward.

<u>Ply rating (PR).</u> A term used to identify a given tire w^{i+h} its maximum recommended load when used in a specific type of service. It is an index of tire strength and does not necessarily represent the number of cord plies in the tire.

PART II: TEST PROGRAMS

6. As stated earlier, tests were conducted on a number of Pacific islands, at Yuma, Arizona, and at Camp Lejeune, North Carolina. The test program on the Pacific islands consisted in operating single selfpropelled, rubber-tired vehicles across level and sloping sand beaches. At Yuma, both rubber-tired and tracked vehicles were tested as single selfpropelled and towing vehicles on level and sloping natural sand and harrowed sand lanes. At Camp Lejeune, single self-propelled or towing, and trailer or towed-type wheeled vehicles were tested on disturbed and undisturbed sand, and asphalt. Measurements and/or observations of vehicle performance and pertinent sand data were made for each test. Details of the program are described in the following paragraphs. Locations of test sites on the various Pacific islands are shown in plates 1 and 2. Plate 3 shows the locations of the Yuma and Camp Lejeune sites used in tests reported herein, as well as the sites used in the pilot study reported in TM 3-240, 13th Supplement.

Pacific Island Test Areas

7. Brief descriptions of the islands visited and beaches tested are contained in the following paragraphs. All the beaches tested are of correand shell origin except the following four: Kalapana Beach on Hawaii, Talofofo Beach on Guam, and the famed Red and Yellow Beaches on Iwo Jima, all of which are of volcanic origin. Representative grain-size curves for the sands at the various test sites are shown in plate 4; supplementary physical property data are presented in table 1. Average beach profiles and cone index isopleths are shown in the figures accompanying the text descriptions. Isopleths show the general strength profile of each beach to assist in a more complete beach description; however, they are not considered in the actual analysis.

Oahu, T. H.

8. Onhu, the third largest island in the Havaiian Islands chain, is of volcanic origin, but there is no volcano activity there at the present time. The ocean beaches on Onhu are of three types: sand, rocky or

cliffed, and silty clay with vegetation growing down to the water's edge. Only the sand beaches were tested. They consist mainly of coral sands deposited by wind and wave action, but they also include seashell fragments and sand eroded from rock formations which can be seen just below the waterline at low tide on some of the beaches. Vehicle tests were run on five beaches, and cone index profiles and sand samples were obtained on four others. The locations of the beaches are shown in plate 1; they are described in the following paragraphs.

9. Mokuleia Beach. This beach, located on the northwestern shore of



Oahu approximately one and one-half miles west of Mokuleia Station, is about 1000 ft long and 250 ft wide (fig. 1). A profile of the beach is shown in fig. 2. The foreshore averages 15 ft in width, has a 30% slope, and is entirely covered with water at high tide and partly covered at low tide.

Fig. 1. Oahu, T. H., Mokuleia Beach

Above the foreshore is a flat berm crest (which comprises all of the backshore) averaging 12 ft in width, frequently wetted by wave action. Beyond the berm crest is a



Fig. 2. Beach profile and cone index isopleths,* Mokuleia Beach

^{*} This and all subsequent beach profiles include cone index isopleths, which are lines of equal cone index and denoted by ---25---. Slevations are referred to mean low tide. Cone indexes were measured at the surface and at 3-in. vertical increments to a maximum depth of 34 in.

forward dune apron averaging 25 ft in width, with a 24% slope, on which 1-1/2 in. of dry, loose sand overlies deep, moist sand. The dune area, some 200 ft in width, is relatively flat with 4 in. of dry, loose sand overlying deep, moist sand. On the landward side of the dune area, where the beach sand has mixed with alluvium, there is some vegetation.

10. Vehicle tests were run on the berm-crest and dune-area portions of Mokuleia Beach. The foreshore was too short and the forward-dune-apron slopes too irregular to be suitable test areas. Vehicle tests were run parallel to the shore line on the berm crest, and both parallel and perpendicular to the shore line in the dune area. A representative sample revealed the soil to be a poorly graded (SP) medium sand (plate 4, fig. 1). The cone index for the 0- to 6-in. depth ranged from 14 to 51. Characteristics of the sand are listed in table 1.

11. Drone Beach. Drone Beach is on the same coast as Mokuleia Beach and approximately 3/4 mile farther west (plate 1). This beach is approximately 800 ft long and averages 200 ft in width. A profile of the beach is shown in fig. 3. The foreshore averages 20 ft in width, has a 30% slope,

and is entirely covered with water at high tide and partly covered at low tide. Rock outcrops can be seen underneath the water at the foot of the foreshore. Above





the foreshore is a berm crest (which comprises all of the backshore) approximately 15 ft wide and fairly flat, which is frequently wetted by waves at high tide. Beyond the berm crest is a forward dune apron that averages 50 ft in width, has a 15% slope, and .s covered with loose, fairly dry sand. The dune area is relatively flat near the forward dune apron but ...bopes downward as it extends inland.

12. Vehicle tests were run parallel to the shore on the berm crest and perpendicular to the shore on the forward dune apron. No tests were run on the foreshore because of its narrow width, or in the dune area

because of vegetation and irregularity of the surface. The sand was uniform in gradation over the entire beach; a representative sample revealed poorly graded sand (SP), medium-textured (plate 4, fig. 1). The cone index for the 0- to 6-in. depth ranged from 21 to 48. Characteristics of the sand are listed in table 1.

13. <u>Makua Beach</u>. This beach is located on the western shore of Oahu, 3 miles south along the coast from Kaena Point (see plate 1), and is



Fig. 4. [^]ahu, T. H., Makua Beach

approximately 3/4 mile long and averages 200 ft in width (fig. 4). A profile of the beach is shown in fig. 5. The foreshore is approximately 30 ft wide and has an average slope of 25%. At high tide the foreshore is almost covered with water. Most of the foreshore is underlain by rock, which

can be seen as outcrops some distance out from the water's edge. Occasionally, the shore line is broken by crescent-shaped troughs which extend to the forward dune

apron. The berm crest averages 15 ft in width, is relatively flat, and is occasionally wetted by wave action. Landward of the berm crest is the berm backslope, which averages 50 ft in



Fig. 5. Beach profile, Makua Beach

width; its slope averages 6% downward as it continues inland. The berm backslope is seldom wetted by surf except when the waves are unusually high. Beyond the berm slope is the forward dune apron, which averages 25 ft in width and has an uneven surface that is partly due to an old railroad bed over which beach sand has been deposited by wind. Some portions of the dune area were suitable for testing.

14. Vehicle tests were run on all areas of Makua Beach. The tests on the berm creat were run parallel to the shore line, and most of the tests on the forward dune apron were run perpendicular to the shore line. Only a small portion of the foreshore was suitable for vehicle tests. The sand was poorly graded (SP) and fine to medium in texture (plate 4, fig. 1, and table 1); in the dune area the sand was darker in appearance than that of the other areas and had little or no fines. The cone index for the 0- to 6-in. depth ranged from 22 to 136.

15. Crescent Beach. Crescent Beach (fig. 6), located approximately

l mile southeast of Makua Beach, is not as uniform throughout its length as the beaches described previously and thus is represented by two different profiles, one through a crescentshaped trough area betucen cusps, designated area one (fig. 7), and



the other through an Fig. 6. Oahu, T. H., Crescent Beach area with no cusps, designated area two (fig. 8).

16. An average profile through area one shows a foreshore that is long and relatively flat for foreshores in this area. It averages



50 ft in width, has a 6% slope, and is entirely covered by surf during periods of high tides and occasionally wetted during low tides. Rocks are exposed at the toe of the foreshore

Fig. 7. Beach profile, Crescent Beach, area one



during low tide. Landward of the foreshore is the berm crest, which averages 20 ft in width. No berm backslope is evident, and the forward dune apron rises directly from the berm crest. It averages 75 ft in width and has an

Fig. 8. Beach profile, Crescent Beach, area two

8% slope. The dune area on this beach is a mixture of sand and silt and supports vegetation to such an extent that it was impractical to run vehicle tests on it.

17. An average profile of beach area two is similar to the profile c^{r} Makua Beach. The foreshore averages 25 ft in width, has a 25% slope, and leads up to a berm crest approximately 15 ft in width. Landward of the berm crest is the berm backslope, which averages 30 ft in width and slopes downward toward the forward dune apron on an average slope of 4%. The forward dune apron averages 30 ft in width, has a 10% slope, and leads up to a dune area on which are found vegetation such as trees and underbrush.

18. Vehicle tests were run on all portions of Crescent Beach except the dune area. Foreshore tests in the vicinity of the crescent-shaped troughs were run both parallel and perpendicular to the shore line. Tests on the berm crest were run parallel to the shore line, and tests on the berm backslore were run perpendicular to the shore line. A representative sample of sand from Crescent Beach shows a poorly graded (SP), fine-textured material (plate 4, fig. 1, and table 1). The cone index for the 0- to 6in. depth ranged from 18 to 66.

19. <u>Bunker Beach.</u> This beach (fig. 9), adjacent to the southeast end of Crescent Beach, is approximately 2000 ft long and has two distinct profiles, one of which is similar to the profile of Makua Beach.

20. Area one profile (fig. 10) shows a foreshore averaging 30 ft in width, with an average clope of 25%. The berm crest is about 20 ft wide and is wetted occasionally by high waves. Beyond the berm crest is the berm backslope, averaging 50 ft in width; it has an average slope of 5% downward as it extends inland. The forward dune apron is about 25 ft wide, and has a 15% slope leading up to a dune area on which some vegetation is growing.

21. Area two profile (fi 11) represents an area in which the berm backslope slopes downward, leaving a low area behind the beach in which water no doubt stands for some time after



Fig. 9. Oahu, T. H., Burker Beach



heavy rains. The foreshore of this profile resembles other beaches mentioned in that it averages 30 ft in width and has a 25% slope. The berm crest averages 20 ft in width and is relatively flat. Landward, the berm backslope

Fig. 10. Beach profile, Bunker Beach, area one the berm backslope averages 100 ft in width and slopes downward on an average slope of 6%.

22. Vehicle tests were run on the berm creat (parallel to the shore line), the berm backslope (perpendicular to the shore line), and on the forward dune apron (perpendicular to the shore line). The foreshore slope was too steep for



Fig. 11. Beach profile, Bunker Beach, area two

vehicle tests, and the dune area contained too much vegetation. The sand



Fig. 12. Beach profiles and cone index isopleths, Oahu

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was poorly graded (SP), with almost equal amounts of medium and fine sizes (plate 4, fig. 2, and table 1). The cone index for the 0- to 6-in. depth ranged from 39 to 85.

23. Other beaches. Only cone index and sand data were obtained on the beaches at Pokai Bay 1, Pokai Bay 2, Naval Ammunition Depot (NAD), and Last Beaches. Profiles of these beaches are shown in fig. 12. The sands from these beaches were all poorly graded (SP) and ranged in texture from medium for Last and Pokai Bay 1 Beaches, to fine-to-medium for NAD and Pokai Bay 2 Beaches (see table 1). The cone index for the 0- to 6-in. depth ranged from 28 to 31 for Pokai Bay 1 Beach, 22 to 52 for Pokai Bay 2 Beach, 26 to 51 for NAD Beach, and 11 to 27 for Last Beach.

Havaii, T. H.

24. Hawaii is the largest island of the Hawaiian Islands chain and,

like Oahu, is of volcanic origin. It is the only island of this chain that has an active volcano at the present time. For the most part the shores of Hawaii are rocky and cliffed, but there are a few sand beaches.

25. The beach tested on Hawaii is covered with bear is sand derived from lava rock



Fig. 13. Hawaii, T. H., Kalapana Beach



Fig. 14. Beach profile, Hawaii, Kalapana Beach

(fig. 13). A beach profile is shown in fig. 14. Because the beach itself is almost inaccessible by vehicle, no trafficability tests were performed; however, cone index profiles and sand samples were obtained. Kalapana

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Beach is approximately 1/4 mile long and about 150 ft wide. The foreshore is approximately 30 ft wide and has a 12% slope. Bedrock can be seen at the toe of the slope and is partially exposed at low tide. The entire foreshore is wetted during high tide. A berm crest at the top of the foreshore averages 10 ft in width, and the backshore slopes gently downward as it continues inland, with palm trees growing near the berm crest. The sand was poorly graded (SP), fine- to medium-textured (plate 4, fig. 3, and table 1). The cone index for the 0- to 6-in. depth ranged from 25 to 68. <u>Kwajalein Atoll</u>

26. Kwajalein Atoll (plate 1), one of the largest atolls in exist-

ence, is approximately 75 miles long from the western to the southern tip. It consists of coral reefs and small sand bars surrounding a lagoon. Kvajalein, its largest island, is located on the southern tip of the atoll and is approximately 3 miles long and 1/2 mile wide; most of this area is



Fig. 15. Kwajalein Atoll, ocean side



Fig. 16. Najalein Atoll, lagoon side

used for an airfield. A profile across the island shows the beaches on the ccean side to be prinarily gravel (fig. 15) and somewhat steeper than the coral sand beaches on the lagoon side (fig. 16). The sand on the ocean-side beaches is only a few inches deep and overlies bedrock. Also, it should be noted that the ending foreshore and beginning of backshore on the lagoon beaches of Kwe' lein are not as well defined as on Oahu, where berm crests were present on nearly every beach. Nine wehicle tests were run on three beaches (designated numbers 5, 6, and 7) on the lagoon side of the island where American landings were made in 1944; in addition, cone index and sand data were obtained on another lagoon beach (designated number 1). These four beaches are described in the following paragraphs, and profiles of each are shown in fig. 17. Gradation and characteristics of the sand found on them are given in plate 4 (figs. 3 and 4) and table 1, respectively.

27. Beach No. 1. This beach is located approximately midway along the lagoon coast line of the island. As shown in fig. 17a, the foreshore is 60 ft wide and has a slope of 14%; it is underlain by coral rock at a depth of about 7 in. The backshore extends 60 ft inland and is fairly flat.







b. Beach No. 5



The sand from this beach was poorly graded (SP) and finetextured. Range of cone index for the 0- to 6-in. depth was 47-52.

28. <u>Beach No. 5.</u> This beach is located about 1000 ft west of Beach No. 1. Its foreshore averages 60 ft in width and has a 13% slope (fig. 17b). The backshore extends 60 ft inland, rising slightly. The sand was poorly graded (SP), fine- to medium-textured. Cone index for the 0- to 6-in. depth ranged from 107 to 128.

29. <u>Beach No. 5.</u> Located about 2000 ft west of the northernmost tip of the island, this beach has been modified by a hydraulic fill which was pumped in from the lagoon. As shown in fig. 17c, the





Beach No. 7 **d.**

Fig. 17c and d. Beach profiles and cone index isopleths, Kwajalein

beach revealed the sand to be poorly graded (SP), medium- to fine-textured, with some silt. Cone index for the O- to 6-in. depth ranged from 50 to 153.

Beach No. 7. Located 30. on the northern tip of the island, this beach has a foreshore that averages 75 ft in width and has an average slope of 13% (fig. 17d). The backshore extends 65 ft inland and is fairly flat. The sand was poorly graded (SP), medium- to finetextured. Cone index for the 0- to 6-in. depth ranged from 62 to 136.

Guam

31. The island of Guam (plate 2) is approximately 30

miles long, 4 to 8 miles wide, and about 275 square miles in area. It consists essentially of volcanic rock and coral limestone, with a fringing reef of coral around most of the island. All beaches tested were coral except Talofofo, which was made up of volcanic materials. In the beach descriptions, the backshore areas are not separated into berm crest and berm backslope since these beach areas on Quan were not as pronounced as on Cahu. Seven vehicle tests were run on four beaches, and sand and cone index data were obtained on two additional beaches. The beaches are described in the following paragraphs, and gradation and characteristics of the beach materials are shown in plate 4 and table 1, respectively.

32. <u>Mimits Beach</u> is located on the west coast of Guam approximately wile south of New Agat. A beach profile is shown in fig. 18. The foreshow in the vicinity of the test area slopes of and is approximately 25 ft wide. The backshore is relatively flat and extends 80 ft inland (fig. 18a). The sand on this beach was poorly graded (SP) and fine-textured. The cone index for the 0- to 6-in. depth ranged from 52 to 68.

33. Jones Beach, located on the east coast of Guam approximately 1-1/2 miles north of Talofofo Bay, has a foreshore approximately 40 ft in width, with a 14% slope. As shown by the profile in fig. 18b, the back-shore is 110 ft wide and fairly flat. Sparse vegetation grows on the back-shore. The sand was poorly graded (SP) and medium-textured. The cone index for the 0- to 6-in. depth ranged from 31 to 52.



a. Nimitz Beach



b. Jones Beach

Fig. 18a and b. Beach profiles and cone index isopleths, Guam

34. <u>Tarague Beach</u>, located on the northern coast, midway between Ritidian Point and Pati Point, is about 180 ft wide. The foreshore averages 70 ft in width and has a 20% slope; the backshore is flat (fig. 18c). The sand was poorly graded (SP), medium- to fine-textured. Come index for the O- to 6-in. depth was 40 to 41. Fig. 19 is a view of this beach.



d. NCS Beach

e. Talofofo Bay Beach

Fig. 18c, d, and e. Beach profiles and cone index isopleths, Guam

35. <u>NCC Beach</u> is located on the western shore about 1 mile south of Haputo Point. The foreshore is about 60 ft wide with a 20% slope. The backshore is flat and 70 ft in withth (fig. 18a). The sand was poorly graded (SP), fineto medium-textured. Cone index for the 0- to 6-in. depth ranged from 79 to 86.



Fig. 19. Guan, Tarague Beach

36. <u>Talofofo Beach</u> is located on the eastern shore near the neck of Talofofo Bay. The foreshows is about 20 ft wide with a 10% slope. Beyond it is a 4-ft-high scarp (fig. 18e), exposed to erosion by waves during high vide. Above the scarp is a fairly level backshore, 40 ft wide. This back is inaccessible to wheeled vehicles. A representative sample of soil

showed it to be a poorly graded (SF), medium- to fine-textured sand containing some silt. Range of cone index for the 0- to 6-in. depth was 32-61.

37. Tumon Beach is located on the western shore of Guam, near the southern end of Tumon Bay. As shown in fig. 20, the foreshore averages 60 ft in width and has a 20% slope. The backshore also averages 60 ft in width and slopes downward from the foreshore. Some vegetation is growing on the backshore. The cand is poorly graded (SP), medium- to fine-textured. The cone index for the O- to 6-in. depth ranged from 102 to 144.



Fig. 20. Beach profile, Tumon Beach



Fig. 21. Luzon, P. I., Lido Beach

Luzcn, P. I.

38. Luzon, the largest island of the Philippine Islands group, measures some 40,420 square miles in area. Beaches are numerous but ecause of the great distance between most beaches and any military reservation, only one beach, Lido, was tested. Lido (fig. 21) is located

approximately 20 miles south of Manila on Manila Bay. The foreshore area

tested averages 60 ft in width and has a slope of 18%. The backshore extends 100 ft inland and slopes gently downward (see fig. 22). The Lido Beach grainsize curve showed a poorly graded (SP), fine to medium sand (plate 4, fig. 6, and table 1). Cone index for the 0- to 6-in. depth ranged from 97 to 131.



Fig. 22. Beach profile; Lido Beach

Midway Atoll

the Hawaiian chain. It is circular in shape, the diameter within the encircling reef being about 6 miles. The atoll includes two islands, Sand and Eastern, which have a combined area of approximately 2 square miles. Tests were performed only on Officers' Club Beach (fig. 23), which is located on the northern shore of the lagoon side of Sand Island.

Fig. 23. Midway Atoll, Officers' Club Beach

The foreshore averages 60 ft in width and has a slope of 12%. The backshore is fairly flat and is 75 ft wide (fig. 24). A representative sample showed a poorly graded (SP), fine- to medium-textured sand (plate 4, fig. 6, and table 1). The cone index for the 0- to 6-in. depth ranged from 34 to 72.



Fig. 24. Beach profile, Officers' Club Beach

Ivo Jima

40. Ivo Jima, the central one of three small islands that make up the Volcano Islands chain, is 5 miles long and 2-1/2 miles wide. The northern portion of the island is a ravine-cut dome, which descends southward through a rough plateau and is connected to Mount Suribachi by an isthmus. Vehicle tests were performed on the two beaches on Iwo Jima on which severe military losses were suffered in 1945, Red Beach and Yellow Beach. Both beaches consisted of weathered volcanic ash.

39. Midway Atoll is located 1300 miles west of Oahu, near the end of

41. Red Peach. Red Beach (fig. 25) is located on the west shore of Ivo Jima, and extends approximately 2-1/2 miles northward from Mount



Suribachi. The foreshore averages 75 ft in width and has a 20% slope. The backshore extends 125 ft inland and has two berms (see fig. 26). Beyond the backshore the forward dune apron extends 800 ft, and its slope averages 15%. The dune area is partially stabilized by vegetation. The Red Beach

grain-size curve showed a poorly graded (SP), fine to medium sand (plate 4, fig. 6, and table 1). The cone index for the 0- to 6in. depth ranged from 24 to 141.

42. <u>Yellow Beach.</u> This beach (fig. 27) is located on the east shore of Iwo Jima and



Fig. 27. Ivo Jims, Yellow Beach



extends approximately 1-1/2 miles northward from Mount Suribachi. The foreshore is 75 ft in width and has a 20% slope. Beyond the foreshore the backshore averages 45 ft in width and slopes slightly downward. The forward dune apron extends 450 ft inland, and its slope averages 12%

Fig. 28. Beach profile, Yellow Beach

(fig. 28). The sand was poorly graded (SP), and medium-textured (plate 4, fig. 6, and table 1). The cone index for the 0- to 6-in. depth ranged from 18 to 88.

Yuma, Arizona, Test Areas

Test Station area

43. Testing at the Yuma Test Station (plate 3), located approximately 25 miles north of Yuma, Arizona, on the east bank of the Colorado River, was confined to prepared test lanes. The test lanes are shown in fig. 29. Towing tests were performed on the prepared lanes, but no single self-propelled vehicle tests.

44. The test lanes, approximately 300 ft long and 40 ft wide, were

prepared by harrowing to a depth of 20 in. and smoothing the surface with an aluminum I-beam attached behind the harrow. The test sites included one level area and three slopes with grades of approximately 10, 15, and 20%, respectively. Analyses of samples revealed the



Fig. 2). Yuma Test Station area

sand to be medium- to fine-textured, with a small percentage of fines (see table 1). A representative grain-size curve is shown in fig. 7 of plate 4. Dune_area

45. Tests were also conducted in a sand dune area referred to herein as the Yuma dune area, although it is actually located in California, ap-

proximately 20 miles west of Yuma, Arizona (see plate 3). Fig. 30 shows the general appearance of the test area, which consists of active sand dunes, some as high as 300 ft, although the majority are less than 100 ft high. Analyses of samples from the test area showed the sand to be medium- to fine-



Fig. 30. Yuma dune area

grained. A representative grain-size curve is shown in plate 4, and supplementary sand data are presented in table 1. Cone index for the 0- to 6-in. depth ranged from 21 to 141. The moisture content of the 0- to 6-in. depth during the test period was approximately 2.0% by weight, unusually high for this area. This was attributed to the fact that the first general rain in about two years occurred at the beginning of testing.

Camp Lejeune, N. C., Test Area

46. Tests were conducted on Onslow Beach (fig. 31) which is located on he Atlantic Coast within the reservation boundaries of Camp Lejeune, N. C. (see plate 3 for location). It is approximately 5 miles long and consists of firm quartz sand. A beach profile is shown in fig. 32. The foreshore ranges in width from 15 to 20 ft at high tide to as much as 100 ft during low tide. The average foreshore slope is about $G_{\rm P}$. Cone index for the 0- to 6-in. depth ranged from 50 to 167. Beyond the foreshore was a very short forward dune apron with dune area sand extending to the



Fig. 31. Onslow Beach, Camp Lejeune



Fig. 32. Beach profile, Camp Lejeune

foreshore in some areas. Dune area slopes were short and steep, with only a few low passages through the dunes. Gradation curves for the 0- to 6-in. depth show a poorly graded (SP), fine-textured sand. A representative grain-size curve is shown in plate 4, and supplementary sand data are presented in table 1. All towed-vehicle tests were conducted on the foreshore, parallel to the water's edge. Tests of self-propelled vehicles were conducted on the forward dune apron and dune area.

Instruments Used to Obtain Test Data

47. The cons penetrometer for measuring strength and a hand level for measuring slope were used throughout the three test programs. Tire pressures were checked with laboratory-type test gages during all three test programs. Dynamometers were used only during the Yuma and Camp Lejeune tests; the slip meter was used only at Yuma. These various items of equipment are described in the following paragraphs.

Sand data

48. <u>Cone penetrometer</u>. The cone penetrometer is a field instrument consisting of a 30-deg cone with a 0.5-sq-in. base area mounted on one end

of a shaft in such a way that it can be forced into the soil by hand. The penetrometer in use is illustrated in fig. 33. A proving ring and calibrated-dial assembly are mounted on the other end of the shaft and are used to measure the load applied. The penetration resistance (read from the dial) is termed



Fig. 33. Cone penetrometer in use

cone index (see "Definitions"). This is the same instrument used to measure the trafficability of fine-grained soils.

49. <u>Han' level.</u> A hand level accurate to 0.5% was used for determining the slope prior to each vehicle test. Slope readings were made by placing the hand level in the center of a 6-ft plank adjacent to the vehicle and parallel to the vehicle path. Slope measurements recorded were the average of several measurements around the vehicle.

Vehicle data

50. <u>Tire-pressure gage.</u> The laboratory-type test gages used to regulate tire-inflation pressures during the tests were accurate to 0.25 psi throughout the range of tire pressures tested. Fig. 34 shows a tirepressure check being made on one of the test vehicles.

51. <u>Dynamometers</u>. The dynamometers used were electrically recording load cells suitable for measuring forces in tension by translating changes in force into changes in electrical energy. These load cells are hermetically sealed and operate without mechanically moving parts. The sensing element is a high-strength load-carrying member to which are bonded special (R-4 strain gages that undergo resistance changes precisely proportional to applied strain. The dynamometers, used to measure drawbar pulls during the



Fig. 34. Tire-pressure check before testing

towing and towed tests, were connected between the test vehicle and the load vehicle, and measured the amount of pull exerted by the towing vehicle. Dynamometers ranged in capacity from 1000 to 50,000 lb, depending upon the amount of force to be measured.

52. <u>Slip meter.</u> The distance a point on the periphery of a wheel or track traveled during a given time and the distance the vehicle traveled during the same time were determined by a slip meter. The meter recorded the number of revolutions the vehicle wheel made while propelling the vehicle, and the number of revolutions made by a nonslipping bicycle wheel trailing the test vehicle and attached to it.

53. <u>Recorder for dynamometer and slip measurements</u>. During the drawbar-slip tests the force exerted on the dynamometer, and the events experienced by the slip meter were amplified and recorded simultaneously as traces on paper tape moving through a six-channel direct-inking recorder. Tests with the 2-1/2-ton M135 utilized all six channels, since electrical contacts were placed on four rear wheels and the bicycle wheel, and one channel was required for recording the dynamometer measurements. Togedvehicle tests utilized a smaller recorder of the same type since only one channel for recording dynamometer measurements was needed.

54. The complex system of measuring drawbar slip required "instrumenting" an M29C weasel with a recorder, amplifiers, and power supply; this vehicle traveled alongside the test vehicle during testing as shown in



Fig. 35. Towing tests, drawbar pull

fig. 35. Electric cables, connecting the test vehicle and the instrumented vehicle, transmitted the measurements to the recorder. For the simple to red-vehicle tests, recorder, amplifier, and power supply were mounted in the towing vehicle.

Vehicles Tested

Tacific islands

55. The vehicles tested were furnished by military units on each island. They included the 1/4-ton M38A1 4x4 truck, the 3/4-ton H37 4x4 truck, the 2-1/2-ton M211 6x6 truck, the 2-1/2-ton H215 6x6 truck, and an unnumbered 2-1/2-ton 6x6 truck. These vehicles are shown in figs. 36 and 37. The test vehicles were equipped with standard equipment and tires, except that the 2-1/2-ton H215 was tested with six 11.00x20 12-ply tires, single tandem (this vehicle normally is equipped with ten 9.00x20 tires). All the vehicles were tested at their rated off-highway payload (nominal capacity) and, in addition, the H215 was tested at one-half the rated payload, and the H211 was tested empty. Vehicle weights, test loads, and tire descriptions are shown in the tabulation on page 32; additional vehicle data are given in table 2.



Fig. 36. Self-propelled wheeled vehicles used in tests
a. 2-1/2-ton 6x6 truck







c. 5-ton M41 6x6 truck



d. 5-ton M54 6x6 truck



Fig. 37. Self-propelled wheeled vehicles used in tests

	Veh	icle Wt.	1b	Tire Data				
		Approx			Ply			
Vehicle	Empty	Load	Gross	Size	Rating	No.		
1/4-ton M38A1 4x4 truck	2,625	500	3,125	7 .00x1 6	6	4		
3/4-ton M37 4x4 truck	5,917	1,500	7,417	9 .00x1 6	8	4		
2-1/2-ton M211 6x6 truck	13,120	0	13,120	9.00x20	8	10		
	13,120	5,000	18,120	9 .00x2 0	8	10		
2-1/2-ton M215 6x6 truck	14,820	2,500	17,320	11 .00x 20	12	6		
	14,820	5,000	19,820	11.00x20	12	6		
2-1/2-ton 6x6 truck	11,000	4,800	15,800	8 .25x 20		6		

56. The truck weights were taken from the identification-data plates inside the cab; however, the 2-1/2-ton 6x6 truck used on Kwajalein had no identification data and its weight was estimated. This truck was very old but still functioned well. Its tire size was 8.25x20, which apparently was not standard for the truck. The drive shaft of the 3/4-ton truch used on Guam broke during a difficult maneuver on the foreshore of NCS Beach. Otherwise, all vehicles tested appeared to be in very good mechanical condition, and were able to spin their wheels when immobilized. The tires on most of the vehicles tested were worn, but otherwise in good condition (no large cuts or bulges).

Yuma, Arizona

57. The vehicles tested where furnished by the Yuma Test Station and are shown in figs. 36, 37, and 38. All wheeled vehicles were equipped with standard military, nondirectional, cross-country tires. The following table lists the vehicles tested and pertinent vehicle data; additional vehicle data are given in table 2.

	!/heeled	Vehicle	5			
	Veh	icle Wt,	1b	Ti	e Data	
		pprox				
Vehicle	Empty	Load	Gross	Size	Rating	No.
1/4-ton 138A1 4x4 truc:	2,475	500	2,975	7 .00x1 6	6	1:
3/4-ton 1137 4x4 truck	5, 645	0 750 1,500 2,300	5,045 6,275 7,085 7,805	9 .00x1 6	8	ł
2-1/2-ton 1135 6x6 truck	12,450 (Con	0 2,500 5,000 7,500 10,000	12,450 15,000 17,330 20,500 22, 7 05	11.00x20	12	6

32



a. 1/4-ton M29C cargo carrier (weasel)



speed tractor

b. 18-ton M4A2 h...

c. 38-ton M6 hispeed tractor

Fig. 38. Self-propelled tracked vehicles used in tests

	Wheeled Veh	icles (C	ont'd)			
	Vel	icle Wt.	16	Tir	e Data	
		Approx	Ply			
Vehicle	Empty	Load	Gross	Size	Rating	<u>No.</u>
5-ton M41 6x6 truck	18,115	0 5,000 10,000 15,000	18,115 24,275 28,175 32,380	14 .00x2 0	12	6
5-ton M54 6x6 truck	20,635	10,000	30,6 35	11.00x20	12	10

		racked V	ehicles			
	Veh	icle Wt,	16	Track	Dim.	Average
Vehicle	Empty	Approx Load	Gross	Length in.	Wilth in.	Contact <u>Pressure, psi</u>
1/4-ton M29C weasel	5 ,97 0	0 1,000	5,970 6,970	78	20	1.9 2.2
18-ton M4A2 hi-speed tractor	36,910	0	36,9 _0	126	24	6.1
38-ton M6 hi-speed tractor	76,000	C	76 ,0 00	17 6	22	9.8

58. All vehicles appeared to be in good mechanical condition and, with the exception of the M135 when loaded with 10,000 lb, each vehicle was able to spin its wheels or tracks when immobilized while operating under full load. Testing with the M41 loaded with 15,000 lb was limited because severe side-wall buckling of the tires occurred when the truck was operated with tires inflated to 10-psi pressure.

Camp Lejeune, N. C.

59. The wheeled trailers tested were furnished by the Motor Officer at Camp Lejeune and are shown in fig. 39. The self-propelled tests were conducted with vehicles of the types shown in figs. 36a and b, and fig. 37b. The following table lists the vehicles tested and pertinent vehicle data; additional vehicle data are given in table 2.

	Veh	icle Wt.	<u>Tire Data</u> Ply			
99-b-1 - 5 -		Approx				
Venicie	<u>P 0.57</u>		01088	<u>512e</u>	Mating	NO.
3	elf-prope	lled Vel	icles			
1/4-ton M38A1 4x4 truck	2,775	200	2,075	7.00x16	6	4
3/4-ton M37 4x4 truck	6,067	0	6,067	9.00x16	8	4
2-1/2-ton M135 6x6 truck	12,450	5,000	17,450	11.00x20	12	6

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- a. 1/4-ton M100 cargo trailer

b. 3/4-ton M101 cargo trailer



c. 1-1/2-ton XM105 cargo trailer



d. 37.5-kv generator trailer

e. 6-ton cargo trailer



and a second second

à

Fig. 39. Wheeled trailers used in towed-vehicle tests at Camp Lejoune, N. C.

	Vel	icle Wt,	Tile Data			
Vehicle	Empty	Approx Load	Gross	Size	Ply <u>Rating</u>	<u>No.</u>
z	Towed Whee	led Vehi	cles			
1/4-ton M100 cargo trailer	569	0 250 500	569 782 1,127	7.00x1 6	6	2
3/4-ton M101 cargo trailer	1,339	750 750 1,500 2,250	1,211 2,089 2,960 3,679	9 .00x1 6	8	2
1-1/2-ton XM105 cargo trailer	2,450	1,500 3,000 4,500	4,110 5,648 7,482	9 .00x2 0	8	2
37.5-kw generator trailer	7,153	0	7, 153	7.00x20	8	l;
6-ton cargo trailer	10,960	0 6,000	10,960 17,160	10.00x20 (front)	10	4
		12,000	25,520	11.00x20 (rear)	12	<u>}.</u>

60. All vehicles tested were in good condition. The three twowheeled trailers were equipped with standard military tires, and the two four-wheeled trailers were equipped with standard commercially available tires.

Tests Conducted

61. The tests were of three types: single self-propelled vehicle tests, towing tests, and towed-wehicle tests. A single self-propelled vehicle test indicated the ability of the vehicle to negotiate various sand conditions and slopes. Towing tests were made for two general purposes: to determine the maximum dravbar (towing) force the test vehicle could exert while moving slowly forward over a range of soil conditions and slopes, and to develop dravbar pull-slip relations. The towed-vehicle tests were made to measure the force required to tow a given vehicle. The following paragraphs enumerate the types of tests and number of each type conducted with each vehicle for each of the three general test areas, Pacific islands, Yuma, and Camp Lejeune.

Pacific islands

62. In this test program, 24 beaches located on 7 islands were visited. Vehicle tests were not conducted on 10 of these beaches, but soil classification and come index data were collected. The vehicle tests on the other 14 beaches were all of the single, self-propelled vehicle type.

63. <u>Single self-propelled tests.</u> The following table shows the number of tests conducted at each beach with each wheeled vehicle.

			Number of Vehicle Tests						
				Veh	icle				
Island	Beach	1438A1	<u>M37</u>	M211	14215	2-1/2-TT	Total		
Oahu	Mokuleia	7	6		2	-	17		
	Drone	8	••			-	8		
	Melcua	12	5 7	41	43	-	153		
Ę	Crescent		40	14	7	-	61		
	Bunker	14	••	20	3	-	37		
Kwajalein	5		1			-	l		
	6	••	4	• •		3	7		
	7	-	**			1	1		
Guam	Nimitz		Ţ			-	1		
	Jones		2			-	2		
	Tarague	• •	3			-	3		
Luzon	Lido		1			-	1		
Total at and	Red	34	20	34		-	38		
	Yellow	• •	15	2	••	•	17		
Total		75	150	111	57	24	307		

64. <u>Other tests</u>. The beaches on which cone index and soil data were obtained but no vehicle tests performed are as follows:

Island	<u></u> Beach	Island	Beach
Oahu	Pokai Bay 1	Kvajalein	1
	Pokai Bay 2 NAD Last	Cuan	Talofofo NCS Tumon
Mawaii	Kalapana	Hidray Atoll	Officers' Club

Yuma, Arizona

65. <u>Single self-propelled tests.</u> Four wheeled vehicles (M38A1, M37, M135, and M41) were tested at various tire pressures on slopes in the natural dune area. All the vehicles, with the exception of the M38A1, were also tested at various payloads. The following tabulation shows the number of tests conducted with each vehicle.

Num				
With	Each	Vehicle		Total
M38A1	<u>M37</u>	M135	<u>M41</u>	Tests
14	102	122	167	405

66. Towing tests. Maximum-drawbar-pull tests (D) were conducted on natural and prepared level and sloping terrain with five wheeled vehicles (M38A1, M37, M135, M41, and M5⁴) and three tracked vehicles (M29C, M4A2, and M6); drawbar pull-slip (S) characteristics were determined only for the M135 2-1/2-ton truck and the M29C weasel. The number of tests conducted with each vehicle on prepared lanes and in the sand dunes is listed below.

				-			Numb	er of	<u>Veh</u>	<u>icle</u>	Tea	ts		_				
	Wheeled Vehicles									Tr	ack	ed	Veh	icl	.68			
Test	M36	<u>A1</u>	M	17	M	35	141	M54	Tot	al	M	90	M	A2	M	6	Tot	al
Area	D	S	D	S	D	S	DS	DS	D	S	D	S	D	S	D	S	D	S
Pre- pared lanes	6	0	5	0	31	50	15 0	7 0	64	50	13	32	4	0	3	0	20	32
Sand du ne s	4	0	10	0	2	0	00	00	16	0	3	0	5	0	0	0	8	0
Total	10	0	15	0	33	50	15 0	70	80	50	16	32	9	0	3	0	28	32

Camp Lejeune, N. C.

67. At Camp Lejeune, single self-propelled terts were conducted on slopes with three vehicles. Towed-vehicle tests were conducted with five trailers, at various loads and tire pressures, on undisturbed sand (by towing the trailer with a long cable, see fig. 40, page 41), and disturbed sand (by towing a trailer coupled directly behind the towing vehicle, see fig. 39). No towing tests were conducted.

-68. <u>Single self-propelled tests</u>. Three wheeled vehicles (M38A1, M37, and M135) loaded to nominal capacities were tested at various tire

pressures on dune slopes. The number of tests made with each vehicle is as follows:

Numbe:	r of T	ests	
With E	Total		
M38A1	<u>M37</u>	M135	Tests
17	29	37	83

69. <u>Towed-vehicle tests.</u> Tests with wheeled trailers were conducted on undisturbed sand, disturbed sand, and asphalt pavement. The following tabulation shows the number of tests conducted with each vehicle.

	Mumber of Tests with Each Trailer								
Test Surface	1/4-ton <u>M100</u>	3/4-ton M101	1-1/2-ton XV105	37.5-kw Generator	6-ton	Total			
Undisturbed sand	16	12	12	4	12	56			
Disturbed sand	16	12	12	4	12	56			
Asphalt pavement	16	12	12	4	12	56			
0 .4.)						-			
10041	48	36	36	12	36	168			

Vehicle-test Procedures and Data Obtained

Single self-propelled tests

70. All single self-propelled tests were performed in the same manner insofar as possible. Most of the tests on the Pacific islands were performed with vehicles loaded to their off-road payload capacities; the loads were secured to prevent shifting. The tests at Yuma were performed with vehicles empty and loaded to 1/2, 1, and 1-1/2 times their off-road payload capacities. Tire pressures were carefully regulated and checked before each test. The same driver was used with the same vehicle insofar as possible. Each test was made with the vehicle traveling in a straightline path in low gear, low range, at slow, steady speed, and with all wheels driving. Since previous tests had indicated that the first pass was the most difficult one to make in sand, the tests reported herein were concerned only with one-pass traffic. Test areas were selected on the basis of accessibility, surface smoothness, and ab. mos of vegetation or litter. The tests conducted on beaches were run both parallel and perpendicular to the water's edge. Soils data were obtained, wehicle performance was observed, and pertiment notes were recorded.

39

Towing tests

71. The vehicle-performance data obtained in these tests consisted of notes concerning immobilizations, general ease or difficulty with which the vehicle traversed the test area, spinning or jerking of wheels, and other pertinent observations. These data are included in tables 3-7.

72. <u>Maximum drawbar pull.</u> The maximum-drawbar-pull tests were performed on prepared lanes and dune slopes at Yuma with the test vehicle towing a second vehicle by means of a cable. As the train moved slowly forward, the load was gradually increased (by application of the brakes on the towed vehicle) until a load condition was established that was thought to be just short of that which would cause immobilization of the test vehicle. This maximum drawbar pull was verified if a slight increase in load caused a halt in the forward progress.

73. The data obtained consisted of continuous measurements of drawbar pull recorded on an oscillograph. The maximum drawbar pull for each test was noted and is given in table 8.

74. <u>Drawbar slip.</u> Drawbar-slip tests were conducted in the same way as the maximum-drawbar-pull tests, except that at several stages between no drawbar pull and maximum drawbar pull records were obtained of the forward speed of the vehicle and the absolute speed of the track or wheel as well as of drawbar pull. The first two measurements permitted the computation of slip. These data are also given in table 8.

Towed tests

75. In these tests, conducted on asphalt pavement and sand at Camp Lejeune, a dynamometer attached to a cable between the towing and towed, trailer-type vehicles was used to measure the towing force. Repetitive tests in the same path were not performed.

76. The vehicle data obtained consisted of towing force required to move the towed vehicle at a slow, steady speed; these data are given in table 9.

77. Long-coulled tests. Tests in which a long cable was used between the two vehicles permitted the offsetting of the towing vehicle slightly so that the towed vehicle straddled the ruts created by the towing vehicle and thus traveled on undisturbed sand. A specially built sled was used to support the tongue of a two-wheel trailer in these tests. This



Fig. 40. Long-coupled hitch for towed tests, Camp Lejeune

sled also contained the dynamometer, which was positioned to the rear of the sled so that it measured only the force required to pull the trailer (see fig. 40).

78. <u>Short-coupled tests.</u> The force required to tow a trailer connected to the drawbar pintle of the towing vehicle in normal fashion also was measured by means of a dynamometer between the two vehicles. In these tests the towed vehicle usually operated in sand that had been disturbed by the towing vehicle.

Sand Data Obtained

Cone index

79. In the self-propelled tests, when a vehicle had successfully traversed a given area, it was halted, and a number of cone index measurements were made along its path. The measurements were made fairly close to the ruts but at a distance believed to be outside the zone of soil actually disturbed by the vehicle. When a vehicle was immobilized, the cone index readings were made in the undisturbed areas along both sides of the vehicle. These readings were made at the surface and at 3-in. vertical increments to a depth of at least 15 in. Ten sets of cone index readings usually were made for each test. Average cone indexes for each depth and

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each test are shown in tables 3-8. The cone index averages for the 0- to 6-, 6- to 12-, and 0- to 12-in. depths are also shown.

80. For the towing tests, cone indexes representative of the area in which the maximum drawbar pull occurred are shown in table 8. In the tables of data obtained in the towing and towed-vehicle tests, tables 8 and 9, cone index is given only for the 0- to 6-in. depth.

81. In towed-vehicle tests cone indexes were determined before traffic and in the ruts after passage of the vehicle. This was not done in the single self-propelled tests since previous studies on coarse-grained soils have shown that trafficability of the soil usually improves with traffic even though the cone index does not necessarily increase. Average cone indexes for each test are shown in table 9.

Moisture content

82. Quantitative moisture-content determinations were not made for each individual test because the small variation in moisture content that might have occurred between tests on the same component of a beach did not justify the time required to make such measurements. However, a qualitative moisture content in one of the five categories defined below was selected for each test on the basis of appearance and feel of the sand and is shown in tables 3-8. Quantitative measurements of moisture content were made for each major test area, and are tabulated in paragraph 84.

83. The five categories of qualitative moisture contents are defined as follows:

- a. <u>Dry scuid.</u> Sand that was light-colored, loose, and freeflowing when poured from the hand was termed "dry." Dry sand usually occurred on the surface of all components of the beaches except the foreshore, but seldom extended deeper than 5 in. before becoming moist. Where test data are available for comparison, sand classed as dry on the basis of visual observation contained less than 1.5% moisture by weight.
- b. <u>Moist sand.</u> "Moist" sand usually lay directly beneath the dry sand layer. It was usually durker in color, showed slight cohesion, and was cooler to the touch. In general, moist sand was found to contain about 1.5 to 5.0 per cent moisture by weight when actual moisture-content determinutions were made.
- c. <u>Net sand</u>. Sand on the foreshore that was being wetted by waves but was not under a finite depth of water during the

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time of testing was termed "wet." Wet sand exhibited a considerable amount of cohesion, and free water could be squeezed out of it.

- d. <u>Inundated sand</u>. Sand covered by water during the time of testing was termed "inundated." This term refers to that portion of the foreshore at the time actually covered by water from wave action. NOIE: A spot on the foreshore "inundated" at one moment during the uprush of a wave might become "wet" a few seconds later when the wave receded.
- e. Quick-condition sand. Loose, yielding, wet, or more commonly, inundated sand that had water flowing through it vertically and became liquefied under the moving wheels of a vehicle (thereby causing immobilization of the vehicle) was termed "quick." (Erosion of the sand away from the wheels contributed to the immobilization.)

A discussion of the effect of sand in these five moisture categories on vehicle performance is presented in paragraphs 90 and 91.

84. Quantitative moisture contents for beaches on Oahu and the Yuma Test Station and dune areas are shown in the following table. Moisture contents for Camp Lejeune tests are shown in table 9 and are averages of several moisture-content values obtained in a series of tests on the same area of beach.

<u>M</u>	oisture	conte	nt (Pe	r Cent)	
Tocation	0-3	Dept	h. in.	12-18	Remerika
		d			
varsu					
Makua Beach					
Foreshore	5.9	7.2	8.4	6.8	
Berm crest	3.8	4.6	4.9	5.3	
Berm backslope	2.2	3.6	4.6	4.4	
Forward dune apron	2.2	3.2	4.4	4.6	
Dune area	1.2	3.4	4.1	7.2	12- to 18-in. depth con- tained some silt
Mokuleia Beach					
1 eshore	6.0	7.8	7.6		
Bern crest	5.7	6.0	6.7		
Forward dune apron	1.1	1.9	4.5		
Dune area	0.7	2.6	5.5		
Crescent Beach. Area 1					
Foreshore					
(near vater)	25.1	24.1	26.0		Free veter
Poreshore (inland)	7.1	13.9	23.6		3- to 12-in. depth con-
		(Conti	(been		ANTTOM TIME MERCE.
		•			

Molstur	e Cont	ent (F	er Cen	t) (Con	t'd)
Location	0-3	3-6	<u>6-12</u>	12-18	Remarks
Oahu (Cont'd)					
Crescent Beach, Area 1 (Cont'd)					
Berm crest Forward dune apron	5•7 0•9	7•3 3•4	8.3 4.8	10.1 3.9	
Crescent Beach, Area 2					
Foreshore	10.5	13.6	20.5	24.4	6- to 18-in. depth con- tained free water
Berm crest	11.3	8.1	17.1	20.3	6- to 18-in. depth con- tained free water
Berm backslope Forward dune apron	5.5 1.8	8.3 2.8	4.4	7∙8 3∙3	
Bunker Beach, Area 1					
Foreshore Berm crest Berm backslope Forward dune apron	4,6 4.1 1.1 0.9	6.5 4.3 1.9 1.9	8.5 5.2 3.6 4.3	3.4 6.7 4.2 4.1	
Bunker Beach, Area 2					
Foreshore Berm crest Berm backslope	5.2 9.6 3.8	7•9 8•3 4•6	10.4 8.8 5.6	7•3 8•1 7•3	
Drone Beach					
Foreshore Berm crest Forward dune apron Dune area	4.2 4.8 0.5 0.5	5.9 6.2 1.0 2.7	8.4 6.6 5.1 4.5	• • • • • • • • • •	
	<u>0</u>	<u>-6 6</u>	-12		
Yuma, Arizona					
Test Station area Dune arca	h 1	.0 1 .9 1	•6 •1		

Slopes

85. The slope for each test area was determined as described in paragraph 49. If a vehicle negotiated a slope, several slope readings were made in the area of maximum slope; however, if the vehicle was immobilized, slope readings were made along both sides of the vehicle at the site of the immobilization. Clope measurements for each test are shown in tables 3-8.

Rut depth

86. Rut-depth measurements were made for most tests; however, they are not reliable as a measure of vehicle performance in cases of immobilization or difficult travel because in some immobilizations the vehicle was allowed to spin its wheels longer than in others. In tests where the vehicle left a smooth rut, the rut depth was measured as the vertical distance from the original sand surface to the bottom of the rut. Where spinning occurred and the rut surface was not easily distinguishable, the rut depth was determined by measuring from the center of the wheel to the original sand surface and then subtracting that distance from the distance between the center of the wheel and the bottom of the tire, which was determined while the wheel was resting on a flat rigid surface. Rut-depth measurements for each test are shown in tables 3-9, and several rut configurations are shown in figs. 41 and 42.



a. Dry sand, Makum Beach, 3/4-ton M37 truck

b. 2-in. dry sand, moist below, Makus Beach, 3/4-ton M37 truck



c. Moist sand, Makus Beach, 2-1/2-tot M211 truck

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Fig. 41. One-pass sut designs



a. Moist sand dunc area, Yuma, Arizona, 2-1/2ton M135 truck



b. Wet sand, Crescent Beach 2-1/2-ton M215 truck



c. Wet sand, Crescent Beach, liquefaction in one rut, 2-1/2-ton M215 truck



PART III: ANALYSIS OF DATA

87. The data collected in this test program are analyzed under four headings: Single Self-propelled Tests, Towing Tests, Towed-vehicle Tests, and Notes and Observations. The conditions and assumptions upon which the analysis is based are described in the following section.

Basis of Analysis

Sand types

88. Three principal types of sand were tested in this program: coral, volcanic, and quartz. The coral and volcanic sands were tested in the Pacific islands, and the quartz sand was tested in the vicinities of Yuma and Camp Lejeune. Field observations and preliminary analysis of the data revealed no significant difference in the performance of the test vehicles as a result of sand type; therefore, all similar vehicle tests on sand are grouped together for analysis purposes.

Sand-trafficability categories

By. In the pilot study, TM 3-240, 13th Supplement, two broad categories of sands were recognized from a trafficability standpoint, clean sands, and sands with fines, poorly drained. Sand in the latter category, when nearly saturated, reacts to traffic in a manner similar to finegrained soils. It generally contains more than 7% fines. From the sand data reported herein it is apparent that all soils tested were in the clean-sand category. The sand in the Yuam dune area contains about 7% fines and may possibly react as a sand with fines, poorly drained, but it is in a desert area where the moisture content of the soil does not attain a high enough level to permit a poorly drained condition to develop. Moisture categories

90. These categories are defined in paragraph 83. It was expected that the moisture content of a sand would play an important part in its trafficability characteristics. Dry sands were expected to be loose and yielding at the surface under the horizontal shearing action of a wheel and thus have poor traction capacity. Hoist sands were expected to have bearing capacities at least as high as that of dry sand and higher traction

capacities because of increased cohesion between grains due to capillary pressures. Some increase in trafficability was expected with further increase in moisture content for the same reason. However, at some stage of increasing moisture content (at or near seturation), it was expected that the intergranular pressure would be partially relieved by the development of pressure in the pore water and that the bearing and traction capacities would be reduced. This condition was anticipated in inundated or submerged sands because of buoyancy. In sands with a definite flow of water through them, and especially an upward flow or gradient, liquefaction of the sand and immobilization of the vehicle were expected. It was further anticipated that the various degrees of trafficability described above could be measured with the cone penetrometer.

91. As will be brought out subsequently, the general pattern of expected behavior described above did occur in these tests. However, the variation in trafficability with moisture content was such that the sands could be grouped into two categories according to their moisture content, with a third category representing high moisture and a pressure condition of the void pore water. The two categories according to moisture content are "dry-to-moist" and "wet-to-inundated." The third category is referred to as a "quick condition."

92. As will be discussed later, separate curves of cone index vs vehicle performance were drawn for the two categories, and results of the tests conducted on quick-condition sands were plotted with the results of tests of the wet-to-inundated category sands.

Immobilization

93. <u>Dry-to-moist sands</u>, During this test program no immobilizations in which a vehicle had to be towed away by another vehicle occurred on dry and moist sands. In cases in which a vehicle could no longer move forward, it was always able to back out in its own tracks. In some cases a wheeled vehicle was almost immobilized but was able to inch itself forward slowly with violent jerks and a great amount of wheel slip. However, for analysis purposes, these two conditions were considered to be immobilizations.

94. <u>Het-to-inundated sends.</u> Several wheeled-vehicle ismobilizations occurred because of the liquefaction of sand under the tires when the vehicle operated in the surf. (These sand conditions are referred to as

quick conditions in this report.) These vehicles were completely immobilized and had to be towed from the test area.

95. Yuma dune sand. Tests at the Yuma dune area presented a problem not previously encountered in that a vehicle occasionally could travel over an area for which the cone index-slope combination previously determined indicated that the vehicle should become immobilized. In such tests slight shear planes usually appeared in the ruts, indicating that immobilization was imminent. When this happened the tests were rerun as follows: the vehicle was allowed to come to a complete stop on the slope, and if it could not progress from this stopped position, the vehicle was considered to be immobilized. Cone index criteria for vehicle performance on sand dunes are, therefore, somewhat conservative. The fact that the vehicle could traverse an area the first time was probably due to the momentum it developed on the gradually increasing slopes typical of the sand dunes. Critical soil layer

96. Previous tests on coarse-grained soils (TM 3-240, 13th Supplement) indicated that the best correlations of vehicle performance with cone index measurements were obtained for the 0- to 6-in. sand layer. Other layers were considered in this analysis but none showed better correlations; hence, the 0- to 6-in. layer is used as the critical layer in this analysis also.

Single Self-propelled Tests

Data used and method of analysis

97. The single self-propelled vehicle test program included a total of 885 tests. A summary of data and test results is presented in tables 3-7.

98. Where applicable, test data reported in TM 3-240, 13th Supplement, were also used in this analysis. The data used were results of tests on three trucks, a 3/4-ton with 9.00x16 tires, a 2-1/2-ton with 9.00x20 tires (dual), and a 2-1/2-ton with 11.00x20 tires (single), since these data were considered comparable to data collected during the current test program. Some of the 13th Supplement data on these vehicles were reevaluated on the basis of sand condition. Data were not used from tests

conducted on (1) prepared sand slopes, (2) sands with more than 75 fines, and (3) crusted desert sands where immobilizations were reported to have occurred after the first pass was completed. Crusted sands were not tested in the current test program. The curves of cone index vs slope reported herein differ only slightly from corresponding curves presented in the 13th Supplement.

99. The method of analysis and the factors considered in this analysis are the same as those described in TM 3-2., 13th Supplement. In brief, the factors considered were soil strength, slope, and vehicle characteristics. Soil strength is important in that it reflects the soil's bearing capacity as well as its capability to permit a vehicle to develop the necessary traction force to propel the vehicle forward. In this report soil strength is expressed in terms of cone index. Slope was considered as a factor because of the increased soil strength required for a given vehicle to negotiate a slope as compared to that required on level terrain. Furthermore, no level, dry or moist sand condition was found that would cause complete immobilization of the vehicles tested; therefore, slopes were used to obtain vehicle immobilizations. A change in tire pressure materially affects the performance of wheeled vehicles; therefore, this vehicle characteristic was also considered as a factor.

100. The method of analysis consisted in plotting the slope and cone index pertinent to all tests with the same vehicle at the same tire pressure, and indicating whether or not immobilization occurred. A line was then drawn that essentially separated the immobilizations and nonimmobilizations. This line thus represented the maximum slope that the vehicle at the given tire pressure could climb, over a range of cone index conditions. Clear-cut separation of immobilizations and nonimmobilizations was not always possible. Consequently, the line was drawn so that the majority of immobilizations would plot above and to the left of the line. In so doing, many nonimmobilizations also plot above and to the left of the separation line. The curve is therefore somewhat conservative. The final position of the line was also influenced by similar lines for the same vehicle at other tire pressures. Curves for the same vehicle at various loads and tire pressures were combined into a family of curves.

Cone index-slope-tire pressure correlations

101. Cone index-slope-tire pressure relations were established for five trucks having tire sizes ranging from 7.00x16, 6-ply rating, to 14.00x20, 12-ply rating. The tire pressures used in the test program ranged from 10 to 45 psi. A maximum of 40-45 psi was used because little or no change in contact area occurred at tire pressures greater than 40 psi and hence little or no change in vehicle performance. Ten psi was used as a lower limit because at pressures less than this, the tire was subject to rim slippage or excessive tire buckling. The relations established for the various vehicles and tires tested are described in the following paragraphs.

102. <u>1/4-ton, 4x4, M38Al with 7.00x16 6 PR tires.</u> The following tabulation gives the number of tests of the M38Al at the various tire pressures shown for which data were taken from table 3 and plotted in plate 5 or 6 according to sand moisture conditions.

	No. of Tests Plotted							
Tire Pressure, psi	Plate 5, Wet- to-inundated Sand	Plate 6, to-moist	Dry- Sand					
30	11	10						
20	3	19						
15	Ο	25						
10	13	19						
Total	27	73						

The results of the five tests at 25 psi and one test at 5 psi are not plotted because of the small number of tests performed at these tire pressures.

103. Twenty-seven tests were run on the wet-to-inundated sand, with a gross vehicle weight of 2975 lb and three tire pressures. An examination of the data plots in plate 5 shows that four tests in which immobilization occurred do not plot on the proper side of the curve. Plotted in fig. 1, test 3-49* (cone index of 39 and slope of 6%) was an immobilization that occurred while the vehicle was traveling at about a 45-deg angle to the slope face, causing a vehicle side tilt of 10%. Had the vehicle been

* First number refers to table number, and second number refers to item number in that table.

operated perpendicular to the slope, it probably would not have been immobilized, as indicated by the location of the plotted point in regard to the separation line. No explanation can be given for test 3-55 (cone index of 62 and slope of 10%) plotting incorrectly in fig. 2. In fig. 3, tests 3-71 (cone index of 62 and slope of 17%) and 3-40 (cone index of 22 and slope zero) plot incorrectly. These were tests in which the vehicle was operating on the foreshore and when the sand was inundated by surf, the vehicle began to sink although cone index measurements indicated that it should have traveled with ease. In test 3-71 the vehicle was operating perpendicular to the water's edge, and it is believed that excessive sinkage was probably due to a combination of liquefaction beneath the wheels and erosion of sand around the wheels by the surf. In the case of test 3-40, the vehicle was operating parallel to the water's edge, causing it to assume a side tilt of 13%.

104. The results of the 73 tests run on dry-to-moist sand with test vehicles operating at 2975 and 3125 lb, at four tire pressures, are shown in plate 6. Two immobilizations plot with the nonimmobilizations: in fig. 2, test 3-8 (cone index of 62 and slope of 6%), and in fig. 3, test 3-18 (cone index of 76 and slope of 10%), both of which were run on Bunker Beach, Oahu. No reason can be given for these tests plotting as outliers. Eleven other tests on Bunker Beach plot on the correct side of the curve.

105. A comparison of plates 5 and 6 indicates that the 1/4-ton M38Al performs better on wet sands than on moist or any sands. For example, at 20-psi tire pressure and on soil having a cone index of 40, it can climb a 16% slope on wet sands but only a 3% slope on dry sands.

106. On the basis of one test at 5-psi tire pressure (3-41, not plotted), the M38A1 performance was improved by lowering the tire pressure below 10 psi, but tire life would probably be greatly reduced because of side-wall buckling and rim slippage.

107. <u>3/4-ton. 4x4. M37 with 9.00x16 8 PR tires.</u> The tabulation on the following page gives the number of tests of the M37 at the various tire pressures shown for thich data were taken from table 4 and the 13th Supplement, and rlotted in plates 7 and 8 according to sand moisture. Pourteen of the tests listed in table 4 are not plotted in plates 7 and C. Four of these tests (two at 40-psi, one at 30-psi, and one at 15-psi tire pressure)

were run on negative slopes. Nine were run at miscellaneous tire pressures and do not justify extra plots. One test (4-108) on wet sand at 20 psi was not plotted because it is obviously in error.

Tire Pres-	No. of Tes 13th Suppleme	ts From nt Plotted	No. of Tests From Table 4 Plotted			
sure psi	Plate 7, Met- to-inundated Sand	Plate 8, Dry- to-moist Sand	Plate 7, Net- to-imundated Sand	Plate 8, Dry- to-moist Sand		
45	0	0	0	15		
40	0	7	0	16		
30	0	Ò	0	49		
20	2	3	7	50		
15	0	5	Ğ	56		
10	0	14	17	51		
	-					
Total	1 2	19	30	237		

108. Thirty-six tests were run on wet-to-inundated sands at tire pressures of 40, 30, 20, 15, 10, and 8 psi. Data plots (plate 7) were made only for the 20-, 15-, and 10-psi tire pressures since only one test was run at each of the other tive pressures. Two hundred and forty-five tests were run on dry-to-moist sand (only 237 tests are plotted in plate 8), mainly at tire pressures of 45, 40, 30, 20, 15, and 10 psi. Curves separating the immobilizations from the nonimmobilizations for both wet-toinuncated sands and dry-to-moist sands are shown for each pressure for which chough data are available.

109. For the vet and inundated sands (plate 7), three tests resulted in immobilizations where the vehicle should have traveled. Test 4-75 (cone index of 23 and slope of zero), plotted in fire. 2 of plate 7, was an immobilization due to liquefaction, and cone indexes taken around the vehicle did not actually indicate the very soft conditions that probably existed when the wehicle became immobilized.

110. Fig. 3, plate 7, reveals three tests on wet-to-inundated sand that are not on the proper side of the curve. Test 4-94 (cone index of 23 and slope of 5%) was another immobilization due to liquefaction. No explanation can be given for the other two tests plotting incorrectly.

111. On dry and moist sands the M37 was tested at four gross weights, 5645, 6067-6275, 7085-7417, and 7805 1b (see plate 8). All tests are plotted together since a variation in weight apparently did not significantly affect vehicle performance. Seven tests, one each at tire pressures

of 40, 30, 20, and 10 psi and three tests at 15 psi, indicate immobilizations where they should not have occurred according to the separation curve. Four of these occurred at the Yuma dune area: tests 4-176 and 4-244 at 15 psi, test 4-234 at 30 psi, and test 4-239 at 20 psi. For test 4-148 (cone index of 62 and slope of 15%) on Iwo Jima at 10 psi, the truck was operated on a 5% tilt, which may have caused the immobilization.

112. The family of curves for the wet and inundated sands, fig. 4 of plate 7, indicates that there is little difference in vehicle performance at 10-, 15-, and 20-psi tire pressures below a cone index of 30. The family of curves for dry and moist sands, fig. 7 of plate δ , indicates a different pattern. The vehicle performance improves more between 10 and 15 psi than between 15 and 20 psi, but even at 10 psi the M37 cannot climb as steep a slope on any given strength of dry-to-moist sand as it can at 20 psi on wet sand.

113. <u>2-1/2-ton, 6x6, M211 with 9.00x20 8 FR tires.</u> The following tabulation gives the number of tests of this vehicle for which data were taken from table 5 and the 13th Supplement and plotted in plate 9 according to tire pressure and sand moisture.

	No. of Tests	No. of Tests			
	From 13th Sup-	From Table 5	Plotted		
Tire	plement Plotted	llet-to-	Dry-to-		
Pressure, psi	Dry-to-moist Sand	inundated Sand	moist Sand		
45	0	14	24		
30	4.	0	11		
50	3	0	27		
15	4	0	5		
10	7	11	24		
Total	16	15	91		

Results of nine tests on dry-to-moist sund shown in table 5 were not plotted in plate 9. Four of these tests at 50-psi and two at 32-psi tire pressure were not plotted because of an insufficient number of tests at the respective tire prevsures; three tests, two at 45 psi and one at 10 psi, were run on negative slopes and therefore were not plotted.

114. Fifteen tes: swere run on wet-to-immdated sands at two vehicle weights, 13,120 and 18,120 lb, and two tire pressures, 45 and 10 psi.

Eleven of the fifteen tests are at 10 psi, and an approximate separation curve between immobilizations and nonimmobilizations is shown for these points (fig. 5, plate 9). The curve shows the M211 to be capable of climbing two to three times steeper slopes at cone indexes of 20 to 60 in wet sand than on dry-to-moist sand. Data on wet-to-inundated sands are insufficient for establishing curves for other time pressures.

115. One hundred and nine tests run with the M211 at vehicle weights of 13,120 and 18,120 lb on dry-to-moist sands are plotted in plate 9. All tests at the same tire pressure are plotted together since variation in weight apparently did not affect performance. Separation curves were developed. Of the fix tests that indicate immobilizations where they should not have occurred, five were run in the Yuma dune area and were reported in the 13th Supplement. The other, test 5-53 (cone index of 38 and slope zero), shown in fig. 3 of plate 9, was an immobilization on the berm crest of Makua Beach, Oahu. In this test, the vehicle was operating on a $\frac{14}{5}$ tilt, which no doubt hindered its forward progress.

116. <u>2-1/2-ton unnumbered truck with six 8.25x20 tires.</u> Four tests were conducted with this vehicle on two Kwajalein beaches. These tests are listed in table 5, items 112 through 115, but as stated earlier no plots are shown because results from such a limited number of tests are inconclusive. A comparison of results of these tests with results of tests of the 2-1/2-ton M211 at 45 psi and the M135 at 40 psi shows that these test results are not out of place.

117. 2-1/2-ton truck with 11.00x20 12 PR tires. Various models of 2-1/2-ton trucks with 11.00x20 tires have been tested during the sand trafficability program. Supplement 13 reports tests on three models: 1134, M47, and M135. The M135 was again tested during this test program (at Yuma). The M215 2-1/2-ton truck was tested on the Oahu Island beaches and, as mentioned in paragraph 55, although it is normally equipped with dual tandem 9.00x20 tires, for this test program it was equipped with 11.00x20 tires.

118. The tabulation on the following page lists the number of tests from table 6 and the 13th Supplement that are plotted in plate 10. Three tests, one at 50 psi and two at 18-1/2 psi, were not plotted. The three tests on vet-to-inundated sands (tests 6-17, -36, -55) were plotted, but no

separation curve could be constructed for them. Tests 6-17 and 6-36 at 20 psi were nonimmobilizations on Crescent foreshore; test 6-55 at 10 psi was an immobilization due to liquefaction of the sand when hit by surf.

	No. of Tests From 13th Sup-	No. of Tests From Table 6 Plotted			
Tire <u>Pressure, psi</u>	plement Plotted Dry-to-moist Sand	Nct-io- inundated Sand	Dry-to- moist Sand		
40	1		14		
30 20	26	2	44 C4		
15 ·	1 6 13	1	45 43		
10		-			
Total	7 0	3	210		

119. A total of 213 tests were conducted in the current program on dry-to-moist sand at vehicle weights of 12,450, 14,950-15,000, 17,320-17,450, and 19,820-20,500 lb. All tests are plotted together, however, since a variation in weights apparently did not affect vehicle performance. The plots also include 70 tests from the 13th Supplement.

120. Twenty-nine of the total number of 280 tests on dry-to-moist sand do not plot properly. Eight of these tests are immobilizations where the vehicle should have traveled, and three of these eight tests are from the 13th Supplement. The five remaining immobilizations that do not plot properly occurred during the 1957 test program at Yuma; one test can be seen in fig. 2, plate 10; one in fig. 3; one in fig. 4; and two in fig. 5. The remaining twenty-one outliers are nonimmobilizations that plot above and to the left of the separation curve, thus indicating that the curves are somewhat conservative. Test records do not reveal any reasons for these tests being outliers.

121. <u>5-ton. 6x6. Mal with 14.00x20 12 PR tires.</u> Vehicle-performance plots for the 5-ton Mal are shown in plate 11. Figs. 1-4 show plots of come index vs per cent slope at four tire pressures (30, 20, 15, and 10 psi), and the family of tire-pressure curves is shown in fig. 5. This vehicle was tested only at the Yumn dume area on dry-to-moist sand.

122. The tabulation on the following page lists the number of tests of the MAI at each tire pressure given in table 7 and plotted in plate 11.

Tire <u>Pressure, psi</u>	No. of Tests From Table 7 Plotted, Dry-to-moist Sand
30	1,1,
20	49
15	• 46
10	28
Total	167

123. The tests were run at four vehicle weights, 18,115, 24,275, 28,175, and 32,380 lb, but all are plotted together as the variations in weight did not affect vehicle performance. Twelve tests do not plot on the proper side of the separation curve or near enough to it to be considered borderline tests, and two of these tests (in figs. 1 and 2, plate 11) are immobilizations where the vehicle should have traveled. Test records do not reveal any reasons for these tests being outliers.

124. Suitable test areas with low cone indexes and flatter slopes were not found in the sand dune area; therefore, the separation lines for the low slopes are merely estimated and shown as dashed lines in the various plots in plate 11.

Towing Tests

125. The toying tests with self-propelled vehicles (five wheeled and three tracked) were conducted principally on harrowed sand lanes in the Yuma Test Station area, with a few conducted on natural sand in the Yuma dune area. Summary data and test results for all toying tests are presented in table δ .

126. The tests were conducted to determine the relation between toying ability and varying weights and three pressures of individual vehicles, and also to compare toying abilities of vehicles on harrowed sand and undisturbed sand. However, changes in the test program precluded conclusive testing on undisturbed sand; therefore, this analysis deals only with the hurrowed-cand tests, although into irom a few tests on undisturbed sand are included in table $\hat{\sigma}_{\bullet}$

127. Analysis of toxing-test data is presented by vehicle types: wheeled vehicles and tracked vehicles. Under each vehicle type the analysis consists of (1) a comparison of maximum drawbar pull with vehicle characteristics, (2) drawbar pull vs slip, and (3) a comparison of computed maximum drawbar pulls vs actual drawbar pulls measured on the test slopes. *Mathematical vehicles*

128. <u>Maximum drawbar pull vs tire pressure and test weights.</u> Twenty-eight maximum-drawbar-pull tests were run on level harrowed sand at the Yuma Test Station with five vehicles at four different tire pressures for each vehicle. The 2-1/2-ton M135 was tested with three loads; all others were tested with their respective recommended cross-country payloads. These tests and average maximum drawbar pull-tire pressure curves for each vehicle are shown in figs. 1-5, plate 12.

129. The maximum drawbar pull of a given vehicle increased with a reduction in tire pressure. The maximum drawbar pulls for all vehicles tested at 10-psi tire pressure ranged from 22.2% of test weight for the 5-ton M5¹ at 30,635 lb ur to 36.0% for the 2-1/2-ton M135 at 12,440 lb. The 3/4-ton M37 test (8-14) was not considered since examination of fig. 2, plate 12, shows this test is probably in error. At 30-psi tire pressure the maximum drawbar pulls ranged from 9.4% for the 1/4-ton M36A1 at 2975 lb to 16.1% for the 2-1/2-ton M135 at 12,450 lb.

130. Fig. 3, plate 12, shows the effect of varying loads on the performance of the 2-1/2-ton M135 truck. As the load was increased in approximately 5000-1b increments, the maximum irawbar pull decreased about 2.5% at all tire pressures. The maximum percentage of pull developed was 36.0 at 10 psi and test weight of 12,450 lb (truck empty).

131. A comparison of the towing capabilities of vehicles of similar size but equipped with different tires can be made by examining the data for the two 5-ton trucks (both tested with a 10,000-1b payload) in figs. 4 and 5, plate 12. The 5-ton M41 with 14.00x20 tires (single) had about 5/p more drawbar ability at all tire pressures than the 5-ton M54 with 11.00x20 tires (dual).

132. <u>Drawber pull vs wheel slip.</u> These tests were run on the 2-1/2ton M135 at three loads and four tire pressures to determine the effect of warying loads on its drawbar pull-slip characteristics. Results of tests with the H135 are shown in figs. 1-3, plate 13.

133. Maximum drawbar pull occurred at about 2% slip for all loads

tested at 10-psl tire pressure; as tire pressure was increased, maximum drawbar pull occurred at a lower percentage of wheel slip for all loads. The rate of decrease in maximum drawbar pull in regard to increased tire pressure was uniform, and at 30-psi tire pressure maximum drawbar pull occurred at about 15% wheel slip for all loads.

134. <u>Comparison of computed maximum drawbar pull with actual drawbar</u> <u>pull measured in tests on harrowed sand slopes.</u> Maximum-drawbar-pull data shown in table 8 for the five wheeled vehicles were used to determine the correlation between computed and actual maximum drawbar pulls on slopes of harrowed sand. The computed drawbar pulls on slopes were developed from measured drawbar pulls on level sand by the formula:

$$P^{\dagger} = P \cos \psi - M \sin \psi$$

where

P' = maximum drawbar pull on slope, computed
P = maximum drawbar pull on level, measured
M = gross weight of vehicle, lb
Ø = angle of the slope, deg

135. Sixty determinations of maximum drawbar pull were made on harrowed sand, 28 on level sand, and 32 on slopes. The following table shows the measured and computed results and the difference between them. A comparison of computed and actual tes results is shown graphically by the round symbols in plate 14.

	lieat	s Max						
(1) 1 mm	Draubs	r Pull	l/eas	i Max I	r aubar	Computed		
Pressure psi		Item No. Table 8	Slope	<u>_1</u>	Item No. Table 8	Pull on Clopes, 1b	Differ 1b	ence
		<u>1/4-to</u>	n 1:38A]	Truch	- 2.975 1	<u>b</u>		
15	550	3	10	200	6	250	+50	25.0
		3/4-4	on 1137	Truck	- 7.005 16	•		
10	1400	14	10	1000	15	751	-316	24.9
			(00	ntime	d)			

Computed - Heasured x 100.

Tire	M Dra on I	leas Max Winr Pull evel Sand Item No.	liea Pu Slope	s Max D 11 on S	rawbar lopes Item No.	Computed Max Dravbar Pull on	Differ	ence			
psi	lb_	Table 8	<i>\$</i>	<u>lb</u>	Table 8	Slopes, 1b	16	5			
		<u>2-1/2-t</u>	on M13	5 truck	- 12,450	<u>1b</u>					
15	3400	, r (10	2000	52	2144	+144	5.7			
10	14500	47	10	3200	53	3240	+40	1.2			
10	4500	47	12	2900	54	3040	-+240	- 4. <u>R</u>			
10	4500	47	15	2400	55	2600	- 200	8.3			
2-1/2-ton M135 Truck - 17,330 1b											
20	3200	66	10	1300	73	1460	+160	12.3			
15	4300	67	10	2000	74	2555	+550	27.7			
15	4300	67	14	2000	75	1855	-145	7.2			
10	5200	7 2	10	3800	76	3450	-350	9.2			
10	5200	72	13	2800	77	2923	+123	4.4			
		<u>2-1/2-t</u>	on M13	5 Truck	- 22,705	<u>1b</u>					
50	4500	87	10	2000	102	1940	-60	3.0			
15	5000	90	10	3000	103	2730	-270	2.0			
15	5000	ŝõ	12	2000	104	2260	+260	13.0			
15	5000	90	15	1600	105	1580	-20	1.3			
10	6000	100	12	3300	10 6	3260	-40	1.2			
10	6000	100	15	200	107	2570	-30	1.2			
10	6000	100	10	3800	108	3720	-20	2.1			
		5 -t a	on M+1	Truck -	28,175 1	2					
30	3400	109	8	1200	113	1146	- 54	4.5			
30	3400	109	10	600	114	576	-24	4.0			
20	5400	110	8	2700	115	3140	+440	15.6			
20	5400	110	10	2500	116	2580	+80	3.2			
15	6500	111	10	1000	117	4225	+225	5.6			
15	6500	111	15	2000	118	2260	+2ÚU	13.0			
15	6500	111	15	2200	- 119	2247	+47	2.1			
10	9000	112	10	5000	120	6000	+1000	20.6			
10	9000	112	13	4200	121	5300	+1100	26.2			
10	9000	112	15	4000	122	47+0	+740	13.5			
. 10	9000	112	20	2800	123	3459	+659	23.5			
		<u>5-to</u>	n 154	Truck -	30.635 1						
15	56 0 0	126	10	2000	128	2310	+310	15.5			
10	6800	127	8	3000	129	3097	+97	3.2			
10	6800	127	12	3000	130	3143	+143	4.3			

Avg (regardless of sign)

61

10.0

136. From an examination of the preceding table it can be seen that the computed drawbar pulls are usually slightly higher than those actually obtained in the tests. This is probably explained by the fact that even though the sand was essentially in the same condition for both slopes and level lanes, the rear wheels sank deeper than the front ones on slopes, thus increasing the actual slope that the test vehicle was attempting to climb.

137. The average percentage of absolute deviation between computed and actual toot results was 10.0. Considering sign, the computed pulls were an average of 5.7% higher than measured pulls. The large percentage deviations for the lightweight 1/4-ton and 3/4-ton trucks are probably attributable to the small magnitudes of the pulls and the relative inaccuracy of the dynamometer in the low range.

Tracked vehicles

138. <u>Maximum drawbar pull vs vehicle test weight</u>. Nine maximumdrawbar-pull tests were run on level harrowed sand with three vehicles: M29C weasel at 5970 lb and 6970 lb; 18-ton M4A2 hi-speed tractor at 36,910 lb; and 38-ton M6 hi-speed tractor at 76,000 lb. Data for these tests are presented in table 8, and average drawbar pull for each vehicle is shown graphically in plate 15.

139. In these tests the tracked vehicles had a maximum drawbar-pull ability ranging from 50 to 65% of their test weight. (The highest drawbar-pull ability of wheeled vehicles was around 35% when operating at 10-psi tire pressure.) The wetwel, the lightest of the vehicles (5970 and 6970 lb) and the one with the lowest contact pressure (1.9 and 2.2 psi), developed the highest drawbar-pull ability (62-65%) of the three tracked vehicles tested. The 36, the heaviest vehicle and the one with the highest contact pressure (76,000 lb and 9.8 psi, respectively), developed the lowest drawbar-pull ability (50%). Tests are needed on a wider range of vehicles and sand conditions in order to clarify the relations between the maximum drawbar pull of tracked vehicles and the sand on which they operate.

140. <u>Dravbar pull vs track slip.</u> Tests were run on the M290 weasel to show the relations of drawbar pull, track slip, and vehicle weight. Table 3 lists tests on this vehicle for three sand conditions: before harrowing (tests 131-137), after one pass of the harrow (tests 138-148),

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and after completion of harrowing (tests 149-155, and 161-176). One pass of the harrow did not leave the test lane uniform enough in strength for reliable testing. Data from items 149 through 155 and 168 through 176 are shown in fig. 4 of plate 13, in which drawbar pull is correlated with track slip and changes in vehicle weight. This plot indicates no change in track slip for the maximum drawbar pull when the vehicle weight is increased 1000 lb, i.e., the track slip at maximum drawbar pull for both weights is 37%. But for the same drawbar pulls below the maximum, track slip is greater for the lesser weight.

141. <u>Comparison of computed and measured maximum drawbar pulls on</u> <u>harrowed sand slopes.</u> Computed maximum drawbar pulls on slopes were developed from applicable measured maximum drawbar pulls on level sand by means of the formula given in paragraph 134. Nine measurements of maximum dravbar pull on slopes were made. A comparison of computed and actual test results is shown graphically by the square symbols in plate 14. The following table lists actual test results, computed maximum drawbar pulls, and the differences between the two.

Meas M Pull on	ax Drawbar Level Sand	Mea Pu	s Max) 11 on :	Dravbar Slope	Computed Mox Drugbar		
<u>_1t</u>	Item No. Table 8	Slope	<u>1b</u>	Item No. Table 8	Pull on <u>Slopes, 1b</u>	Differ 1b	ence 5#
	1/4-ton M290	Weasel,	5,970	1b, Contac	t Pressure = 1.	9 psi	
3,250 3,250	146 146	20 15	2,000 2,300	. 156 15 7	2,010 2,375	+20 +25	1.0 1.1
	1/4-ton M290	Measel,	6,970	1b, Contact	t Pressure = 2.	2 psi	
4,400 4,400	165 165	15 15	2,600 3,000	177 178	3,320 3,320	+720 +320	27•7 4•6
<u>18-t</u>	on M4A2 Hi-spe	eed Trac	tor, 3(5,910 1b, Ca	ontact Pressure	= 6.1	bci
20,000 20,000 20,000	179 179 179	8 12.5 15	15,000 15,000 12,000	180 181 182	16,960 15,262 14,300	+1960 +262 +2300	13.1 1.7 19.2
38-	ton 16 Hi-spec	ed Tract	or, 76,	000 1b. Cor	ntact Pressure	= 9.8 p	<u>s1</u>
38,000 38,000	188 188	8 12 . 5	29 ,00 0 2 8,000	189 190	31,829 28,267	+2829 +287	9.6 1.0
			٨	vg (regard)	less of sign)		0.0

<u>Computed - Measured</u> x 100.

142. The average deviation (expressed as a percentage difference between computed and measured drawbar pull) is 8.8% for all vehicles tested, and for all tests the computed drawbar pulls are higher than those actually measured. In examining the summary of test data in table 8 it may be noted that cone index for tests of the two hi-speed tractors on level sand (items 179 and 188) was much higher than the cone indexes on slopes. Had the cone indexes on slopes been the same as on level ground the maximum drawbar pulls developed might have been closer to computed results.

Towed-vehicle Tests

143. The towed-vehicle test program included tests on two- and fourwheeled trailers. One hundred and sixty-eight tests were run with five trailers (three two-wheeled and two four-wheeled), at loads varying from empty to 1-1/2 times their payload capacities, and at four tire pressures. A summary of the test conditions and results is presented in table 9.

144. Tests were conducted on asphalt pavement, undisturbed sand, and disturbed sand. The analysis of data was made only for tests conducted on sand, since towing-force requirements of all vehicles on asphalt were in the range or only 1.0 to 2.0%. The towing force on asphalt is a measure of the internal mechanical friction of the vehicle wheels plus the external frictional rolling resistance of the wheels on a hard, essentially unyielding, surface. In this report the forces (which were small) required to overcome the internal resistance are included in the gross towing force required on sand.

145. The results of tests on undisturbed sand, made by towing the test vehicle with a long cable as described in paragraph 77, are shown in plate 16 as open symbols. Results of tests on disturbed sand, made with the test vehicle towed at close hitch behind the towing vehicle, are shown in plate 16 as closed symbols.

146. A good correlation exists between the towing force req ired, cone index before traffic, and tire pressures for all vehicles. Apparently, disturbance of the sand by the towing vehicles had little or no measurable effect on the towing force required for the treilers since, for the range of come indexes tested, rut depths were shallow and little or no

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change in strength occurred after passage of the test vehicle.

147. A family of tire-pressure curves for towing force required vs cone index (before traffic) is shown in fig. 8, plate 16. The curves (if extrapolated) tend to converge at cone indexes above 200 and towing forces below 2%, and "fan out" uniformly to a cone index of 75 (which is near the lowest cone indexes measured) where the towing force required ranges from 10% at 10-psi tire pressure to 23% at 60-psi pressure. The average deviation (in per cent towing force required) of individual tests from the avereage line for each tire pressure is approximately 1.0%.

148. In summary, it appears that towing force required (per cent of test weight) is a function of sand strength and tire pressure for the range of vehicle weights tested (empty to 1-1/2 times payload capacity). The effect of number of wheels (two or four), tire arrangement (single or dual), and number of axles (one or two) on towing force is small when considered independently of the effects of test weight, tire pressures, and sand strength. Tests are needed of additional vehicles on lower-strength sands and on sands different from those at Camp Lejeune in order to determine more fully the relations between vehicle characteristics and towingforce requirements over a wide range of sand conditions.

Notes and Observations

149. During the course of the approximately 900 single selfpropelled vehicle tests on beach and desert areas, a few observations were made of several immeasurable factors that nevertheless influence vehicle mobility. These observations are discussed in the following paragraphs. Liquefaction and erosion

150. Several wheeled-vehicle immobilizations occurred on inundated beach sands when slopes were about 14% and the beach face was inundated by wave action. It is telieved that along with the slope factor, liquefaction and erosion of sand from around the wheels by the surf contributed to the ismobilizations. On several occasions when inwobilizations did not occur, it was observed that the top 2 to $\frac{1}{4}$ in. of sand in the ruts was liquefied. Hed the proper combination of loading and drainage occurred simultaneously, sand beneath the wheels might have liquefied to a depth that would have caused ismobilization.

151. Observations of vehicles operating in the surf also revealed that if a vehicle was stalled or purposely stopped for a few minutes, erosion of sand from around the wheels by wave action usually resulted in an immobilization.

152. Immobilizations did not occur on inundated sands as long as the water was not moving over or through the sand, as in lagoon areas of clean sand protected from the open sea or areas where water was trapped during periods of low tides.

Borderline conditions

153. When a vehicle is immobilized in sand it is usually because of traction failure. Traction failure is the inability of the sand surface to resist the horizontal dynamic stresses applied to it by a powered wheel or track. Thus, the thrust necessary to propel the vehicle cannot be developed. Close observation revealed that a vehicle operating on a slopestrength combination borderline between immobilizations and nonimmobilizations will leave slight shear planes in its ruts. These conditions were retested by repeating the operation parallel to the old ruts, but on the rerun the vehicle as allowed to come to a complete stop in the area under question and start again. In nearly every case the vehicle could not complete passage through the area. This was done to check the assumption that the reason a vehicle usually negotiated a borderline condition was that the momentum it developed in making its approach to the test area carried it through. In tests in which the vehicle did not leave these slight shear planes, it had no trouble in moving from a stopped position. For tests run on sand where the slope-strength combinations were much below the borderline conditions, immobilizations occurred almost simultaneously with the beginning of traction failure.

Effects of vehicle characteristics

15^h. <u>Tire pressure</u>. Tire pressure is the single vehicle characteristic that has the most influence on the performance of a given vehicle in sand. Careful adjustment of tire pressures is essential in conducting accurate tests or obtaining the expected performance from a vehicle. It was found that in order to achieve the accuracy desired, low tire pressures had to be measured with a pressure gage more accurate than the usual "stick gages." Nost stick gages register only as low as 10 psi and have been.
found in some cases to be as much as 3 psi off at low pressures.

155. Careful and constant regulating of tire pressures during testing was essential because of the tire-pressure changes that resulted from changes in tire temperature. At least four conditions were enconstered that caused tire temperatures and hence tire pressures to vary during testing: (1) changes in ambient air temperature during testing; (2) operation of the tires in wet and inundated sand after the tire pressure had been adjusted on warm dry sand; (3) starting tests on sand after the vehicle had been operating on a hard surface at high speeds; and (4) permitting wheels to slip for an extended period of time.

156. Tire pressure also apparently has an effect on the peculiar action of vehicle "jerking" when traction failure occurs. For the 2-1/2ton and 5-ton trucks, the "jerking" action was violent at higher tire pressures and much more gentle at the lower tire pressures of 10 and 15 psi.

157. <u>Tire condition.</u> All military vehicles tested were equipped with the standard nondirectional cross-country tire; however, the physical condition of these tires varied considerably as some were new, some recapped, and some had little or no tread. Although it is generally thought that tire condition has some effect on vehicle performance, the observations made during this test program do not appear to bear this out. This is indicated by the fact that although the same tires or vehicles were not used for the complete test program, the performance of a given type of vehicle and size of tire was consistent.

158. The theory that tire conditions (within the range of tire conditions tested) have little effect on vehicle performance in coarse-grained soils is also supported by measurements of the contact area of the tires on the 3/4-ton M37 tested at Yuma. This vehicle was equipped on one side with two newly recapped tires and on the other side with two old, well-worn tires; however, the contact areas for these tires were practically the same at a given tire pressure, with neither set consistently greater or smaller than the other. Some difference in the shape of the tire print was apparent, however; worn tires generally produce a more rectangular pattern than new or newly recapped tires.

159. <u>Rut configuration</u>. Ruts made by the 2-1/2-ton and 5-ton trucks operating at low tire pressures (10 and 15 psi) on the soft harrowed sand

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contained a slight bulge (convex upward) along the center of the rut surface. This bulge was approximately 1/4 to 1/2 in. in height with respect to the depth along the sides of the rut wall. Puts made in tests in the undisturbed sand areas at low tire pressures showed an indication of this bulge but it was not nearly so pronounced as in the harrowed sand. The higher strength of the undisturbed sand yielded less to rutting and hence less bulging occurred in the center of the rut. This configuration, although slight, may be a clue to the confining effect of the side walls of the tire on the sand beneath the tire, and may be the cause of the improvement in vehicle performance in sand when tire pressures are reduced.

160. <u>Transmission type.</u> Vehicles with both automatic and manual transmissions were used throughout the test program. No conclusive observations were made as to the advantage of one over the other from the standpoint of vehicle performance. It is recognized, however, that the automatic transmission does eliminate the "driver effect" more than the mechanical transmission by partially assisting in a smooth movement from a stopped position on slopes. It may be possible that for a few tests near the borderline conditions of cone index-slope as described in paragraph 153, the positive connection of the mechanical transmission may have caused the tires to shear the sand surface initially and to start a process of shearing that eventually led to immobilizations, whereas an automatictransmission type vehicle might not have become immobilized. Sand strength

161. The use of the cone penetrometer and other instruments for measuring the existing strength of the 0- to 6-in. layer of soil was discussed in the 13th Supplement of the "Trafficability of Soils" series. The following paragraphs discuss the relations of sand strength (as measured by the cone penetrometer) and other sand characteristics.

162. <u>Variations of strength with depth.</u> The standard test procedure for all vehicle tests included the collection of cone index data to a depth of 15 in. or greater whenever possible. The best correlation between cone index and vehicle performance was obtained by considering average beforetraffic cone index for the 0- to 6-in. depth; measurements taken at the surface, 3-in., and 6-in. depths are used in determining the average value. Except for a few cases, the strength of a sand consistently increased with

depth. It was found essential that the cone index be read at exactly the correct depth. The increase in strength with depth is usually of sufficient magnitude that, unless the cone index measurements are made with considerable care, the results can be very erroneous. The following table shows an example of what would happen if measurements were made 1 in. below the prescribed depths. For this example it was assumed that the data shown in table 6 for item 40 were correctly taken. Cone index was plotted against depth, and a curve was drawn. Readings were then taken at depths 1 in. lower than those prescribed, and the two were compared.

	Dept in.	th Cone Index	Depthin.	Cone Index
	0	2	1	9
	3	38	4	62
	6	128	7	160
	9	240	10	284
Avg O- to	6-in. layer	56		77

163. An exemination of test 40 (cone index 56, slope 15%, fig. 4 of plate 10) reveals what would happen to this test were it plotted at a cone index of 77 rather than at 56. The test was an immobilization that would plot on the wrong side of the line of separation if plotted at a cone index of 77. The fact that large differences in average readings can be introduced by reading cone index values at improper depths may well explain why some of the tests plot near or on the wrong side of the line of separation.

164. <u>Variations of strength with moisture.</u> As shown by plots of vehicle slope-climbing ability vs cone index, a given vehicle at a given tire pressure can operate more easily on a wet sand than on a dry or moist sand of equal cone index. This precludes any correlation that might be attempted between strength (as measured by the cone penetrometer) and vehicle performance without considering moisture condition of the sand. However, use of the cone index as a measure of expected vehicle performance in actual operation would give the lower limit of performance expected and, as moisture content increases, the performance of the vehicle would increase accordingly until a mear-saturated state is reached and then the vehicle performance is less predictable. Any refinament that includes moisture condition will improve the over-all accuracy of measuring sand trafficability.

PART IV: CONCLUSIONS AND RECOMMENDATIONS

Conclusions

165. The following conclusions are based on analysis of the data collected in the three test programs reported herein. The basic guide for these test programs was the findings reported in the 13th Supplement of the "Trafficability of Soils" series; therefore, these conclusions are also applicable for all coarse-grained soil tests conducted to date.

Single self-propelled wheeled vehicles

- a. Vehicle performance expressed in cone index-slope climbing ability terms is influenced by the moisture condition of the sand. Wet-to-inundated sands are more trafficable than dry-to-moist sands. Inundated sands, however, are apt to be in a quick condition if the water is in motion over and through the sand. Quick condition sands are not able to support traffic.
- b. The performance of self-propelled vehicles on dry-to-moist sands, as defined by the cone index-slope climbing curves, is the same regardless of sand source (quartz, volcanic, or coral) or location (beach or desert).
- c. Payload variations from empty to 1-1/2 times the rated load had no major effect on the slope-climbing ability of the self-propelled vehicles tested.

Towing tests with self-propelled vehicles

- a. The maximum drawbar pull for wheeled vehicles on level harrowed sand ranges between 20 and 40% of their gross weight; trached vehicles are capable of maximum drawbar pulls of as much as 50 to 60% of their test weight.
- b. Load increase on the 2-1/2-ton M135 from empty to 10,000 lb decreased the maximum toring-force ability by 2.5% of the test weight at all tire pressures tested. For a given tracked vehicle (1/4-ton M29C), an increase in test weight of 1000 lt reduces the maximum toring-force ability by 3.5% of the test weight.
- c. The single-tandem 5-ton 141 has a 5% higher drawbar-pull ability than the dual-tendem 5-ton M54.
- <u>a</u>. For wheeled vehicles, maximum drawbar pull occurs at about 25% wheel slip for all loads at 10-pri tire pressure. At 30-psi tire pressure, saximum drawbar pull occurs at approximately 15% wheel slip. For tracked vehicles, track

slip is 37% at maximum drawbar pull for the 1/4-ton M29C at two test weights. At lower drawbar pulls, the percentage of track slip is less for the lighter load.

e. Towing-force ability on harrowed sand slopes can be computed from test results on level harrowed sand, with an average difference of about 10% between actual and computed results.

Towed-vehicle tests

- a. Toving-force requirements for wheeled trailers can be correlated with cone index and tire pressure.
- b. For the tire pressures tested, sand disturbance by the towing vehicle has little effect on towing-force requirements when the towed and towing vehicles are operated at the same tire pressures.

Recommendations

- 166. It is recommended that:
 - a. A rapid method be developed for confident recognition of the three moisture conditions of sand that are important from the trafficability standpoint--dry to moist, wet to inundated, and quick condition.
 - b. Additional single self-propelled vehicle tests be made, with emphasis on wheeled vehicles of more than 5-ton capacity.
 - <u>c</u>. Detailed studies of the effect of wheel load, tire pressure, and other vehicle characteristics on performance of vehicles in sand be continued.
 - d. . Toving tests on undisturbed sand with a range of military vehicles be conducted.
 - e. Additional towed-vehicle tests, including tests with tractor-trailer combinations, be conducted.
 - <u>f</u>. Nork be conducted on procedures to derive means of evaluating performance of vehicles not tested.
 - g. Vehicle tests on gravel teaches be conducted.
 - h. Cork on estimating the trafficability of untested beaches be continued.

			as a		Banda			Uniformity	Median Disectores	Effective Disasteres	Specific		Inified Soil Classification
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		M ahuan Mahuan	Coral	0	7	53	0	1.7	0.500	6.0	2.74	6	
		Creacent	Cornil	0	า	8	0	1.58	6	0.10		5 8	
		Busher	Corel	0	\$	51	0	1.58	0.41	92.0		5	Mudding to fine seed
		Point My 1	Coral	Ś	67	2	0	1.46	0.57				Madine voite see
		Point Day 2	Corel	m	6	2	0	1.63	0.58	9.0		5	
		3	Corni	0	73	21	0	1.41	0.50	0.37		- 6 5	
			Coml	0	R	0	0	9	0.06	0.50		46	
	Bom11, T. I.		Volcenic	0	76	24	0	1.04	0.56	0.12		6	Pine to medium and
0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0	ماماهرهما	-4	Conl	0	9	16	0	2.27	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	0.11		55	
1 0 Cont 0		~	Coral	10	ጽ	3	0	69.4	0.51	1.0	01.0	6	Fire to making and
Tate Cont Cont 1 Cont Cont Cont 1 Cont Cont Cont Cont 1 Cont Cont Cont Cont 1 Cont Cont Cont Cont Cont 1 Cont Cont Cont Cont Cont Cont 1 Cont		9	Conl	0	R	\$	~	1.26	0.26			5	
Matter Cont O.2 Matter Cont 0.2 Matter Cont <td< td=""><th></th><th>-</th><td>Const</td><td>0</td><td>13</td><td>5</td><td>0</td><td>2</td><td>0.00</td><td>8.0</td><td></td><td>5 8</td><td></td></td<>		-	Const	0	13	5	0	2	0.00	8.0		5 8	
Continue Continue <td< td=""><th></th><th>Nimite</th><td>Cont</td><td>0</td><td></td><td>16</td><td>. 0</td><td>1</td><td>8</td><td></td><td></td><td></td><td></td></td<>		Nimite	Cont	0		16	. 0	1	8				
Martin Cont 23 Martin Cont 24 Martin Cont <t< td=""><th></th><th>Jones</th><td>Corel</td><td></td><td>`£</td><td></td><td>00</td><td></td><td>5.75</td><td></td><td>0 1</td><td></td><td></td></t<>		Jones	Corel		`£		00		5.75		0 1		
Main Cont 0.0 2.15 0.0 0.0 Main Cont 0.0 2.17 0.0 0.0 0.0 0.0 Main Values Cont 0.0 2.17 0.0		Pres.	Coml	I	2	4	• c				•	7 8	
Nicroto Viscanic Output Output <th></th> <th>821</th> <td>Cont</td> <td>· 0</td> <td>38</td> <td>2 5</td> <td>) (</td> <td></td> <td></td> <td></td> <td>•</td> <td>2</td> <td>Medium to fine sand</td>		821	Cont	· 0	38	2 5) (•	2	Medium to fine sand
Numera, P. I. Numera Cont O P Numera Nume		This for the	Valcanic	o c	2	202	• c				8		time to sectual and
Minimute Minimute <td< td=""><th></th><th></th><td></td><td>> c</td><td>28</td><td>28</td><td>vc</td><td></td><td></td><td>0.10</td><td>•</td><td>45</td><td>Medium to fine sand, some silt</td></td<>				> c	28	28	vc			0.10	•	45	Medium to fine sand, some silt
Mile Constraint	Lacros P. 1.) ^	2	83	5 0			11.0	•	5	Nedline to fine and
Notanic 0 2 0 2 7 0 2 7 0 2 7 0 2 7 0 2 7 0 2 7 0 2 7 0 0 2 7 0 0 2 7 0 0 2 7 0 0 2 7 0 0 2 7 0 2 7 0 2 7 0 0 2 7 0 0 2 7 0 0 2 7 0 0 2 7 0 0 2 7 0 0 2 7 0 0 2 7 0 2 7 0 2 7 1 </td <th></th> <th></th> <td></td> <td>nd</td> <td>23</td> <td>2</td> <td>5</td> <td>2.51</td> <td>74°0</td> <td>0.21</td> <td>•</td> <td>6</td> <td>Fine to medium sand</td>				nd	23	2	5	2.51	74°0	0.21	•	6	Fine to medium sand
Volume70.000 3° <th< td=""><th></th><th></th><td></td><td>> <</td><td>83</td><td>;</td><td>5</td><td>2.27</td><td></td><td>ັ ດ</td><td>:</td><td>e.</td><td>Fine to widtum and</td></th<>				> <	83	;	5	2.27		ັ ດ	:	e.	Fine to widtum and
Nut that on that ion volume (0,1) 0.49 2.72 3P Module and (10,1) Nut that on that ion Counts 0 2.40 0.91 0.49 2.77 3P Module and (10,1) Nut that on that is Counts 0 2.40 0.21 7 1 2.75 0.28 Module to fine and (10,2) Node and (10,1) Num that Counts 0 21 7 1 2.75 0.28 Node and (10,1) Node and (10,1) Num that Counts 0 1 2.75 0.28 0.00 3P_2M Module to fine and, cons all the (10,1) Num that Counts 0 0 1 3.50 0.28 0.00 3P_2M Module to fine and, cons all the (10,1) Num that Counts 2.75 0.28 0.28 0.26 3P_3 Node and (10,1) No Outs 0 0 1 0.26 0.21 0.26 2.68 3P_3 No				21	88	£ ,1	3	84.	0.48	8.0	2.71	d .0	Fine to medium sand
Van Toat Site Van Toat Site Nat tabie			Actemite	~	8	-	0	2.40	16.0	0.49	2.72	32	Medium send
Nut station Quarta 0 21 75 4 2.75 0.26 0.12 SPL:3K Median to fine and, complete Name area 19 74 1 3.50 0.03 SPL:3K Median to fine and, complete SPL:3K Median to fine and, complete SPL:3K Median to fine and, complete							기	m Test Site					-
Num erse (unerts 0 19 71 7 3.50 0.23 0.06 37.31 Notice 100 111 Comp Labour Test Site Comp Labour Test Site 0.23 0.06 37.31 Notice 100 100 111 Comp Labour Test Site 0.23 0.26 0.23 0.26 37.31 Notice 101 100 111 Contract 0 100 0 0.25 0.26 0.23 0.06 37.31 Notice 111	het station	: : : : : : : : : : : : : : : : : : : :	Quer's	0	21	ĸ	.4	2.7	0-20	c1 - 0	1 7 1	45	
Chalce Quarts 0 0 100 0 0.76 0.21 0.23 2.63 37 Fine mant		:	functe	0	61	1	•	2.5	0 . 23	8000	• •	56	Medium to fine sand, some silt Medium to fine sand, some silt
Casica Quarta 0 0 100 6 0.76 0.21 0.75 2.63 37 Fine and								•					
Omelow Quarts 0 0 100 0 0.76 0.21 0.25 2.63 3P Fine mant								Pur Test 5	3				
		Omelan		0	0	001	J	0.76	12-0	2 ,2	6	40	
											3	5	

Physical Properties of Sand from the O- to 6-in. Depth at Test Sites

Table 1

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Contre and -per east by might of ample retained on No. 10 U. S. Standard alon (2.00 ms) but passing No. 4 alone holds and -per east by might of ample retained on No. 40 U. S. Standard alon (0.40 ms) but passing No. 10 alone Plan passi-per east by weight of ample related on No. 200 U. S. Standard alone (0.40 ms) but passing No. 10 alone are bet writed on No. 200 U. S. Standard alone (0.40 ms) but passing No. 10 alone are bet writed on No. 200 U. S. Standard alone (0.40 ms) but passing No. 10 alone are bet writed on No. 200 U. S. Standard alone (0.40 ms) but passing No. 10 alone are bet writed on No. 200 U. S. Standard alone (0.40 ms) but passing No. 10 alone are bet writed on No. 200 U. S. Standard alone (0.40 ms) but passing No. 10 alone

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								Tire Desc	rigtion	-	-	
Vehicle	Empty Weight 1b	Approx Load 1b	Test Weight <u>lb</u>	Vidth in.	Rim Diam <u>in</u> .	Ply Anting	No. of <u>Tires</u>	Tire Pressure 	Total Contact Area eq in.*	Average Contact Pressure paies	Average Print	Tire in.† Vidth
				Pacific	Islan	ds Test	Program					
			8	elf-prop	elled	Whee Led	Vehicle	<u>stt</u>				
1/4-ton M38A1 4x4 truck	2,625	500	3,125	7.00	16	6	4	30 20 15	100.4 133.8 164.4 -	31.1 23.4 . 19.0	6.5 7.4 8.4	5.0 5.3 5.4
3/4+ton N37 4x4 truck	5,917	1,500	7,417	9.00	16	8	à	10 30 20 15	188.6 224.4 297.8	16.6 33.0 26.9	8.6 8.7 10.8	5.6
2-1/2-ton M211 byb truck	13,120	5,000	18,120	9.09	20	8	10	10 30 .*0	341.7 401.3 454.9 508.7	21.7 45.2 39.8	11.9 8.4 9.0	7.6 9.60 9.90
2-1/2-ton M215 Ox6 truck	14,820	2,500	17,320	11.00	20	12	6	10 30 20	591.5 399.0 449.6 502.2	30.6 43.4 38.5 34.5	10.9 11.2 11.9	10.20 10.20 7.1 7.3 7.4
		5,000	19,820	11.00	50	12	5	10 30 20 15	569.6 426.1 492.2 530.5	30.4 46.5 40.3 37.4	14.4 11.8 13.0 13.4	7.5 7.0 7.4 7.5
2-1/2-ton un- numbered 5x6 truck	11,0 Ø est	4,600	15,800	8.25	20		6	19 50	eJ1.5	12.6	14.5	7.6
				Y	ma Ter	st Prog		•				
			8	lf-prop	lied 1	theeled	Vehicle					
1/4-ton N38A1 4x4 truck	2,475	500	2,975	7.00	16	6	4	30 20 15	98.6 121.7 141.3	30.2 24.4 21.1	6.7 7.5 8.2	4.4 4.7 4.8
3/6-ton M37 4x4 truck	5,645	0	5,645	9.00	16	8	•	10 30 20 15	167.5 178.7 217.4 247.3	17.8 31.6 26.0 22.8	9.2 7.8 8.6 9.1	5.0 6.7 7.2 7.5
		75 0	6 ,215	9.00	16	8	4	10 30 20 15	290.9 197.7 236.2 262.5	19.4 31.7 26.6 23.9	10.2 8.0 8.8 9.4	7.6 7.1 7.3 7.5
		1,500	7,085	9.00	16	8	4	10 30 20 1	306.0 223.1 265.7 301.0	20.5 31.8 26.7 23.5	10.7 9.0 9.9 10.7	7.6 7.2 7.5
		2,300	7,805).00	16	8	4	10 30 20 15	338.8 261.2 281.1 317.4	20.9 32.4 27.8 24.6	11.6 9.0 10.2 10.7	7.6 7.6 7.6
2-1/2-ton M135 6a6 truca§	12,450	0	11.,450	11.00	20	12	6	10 30 20 15	363.6 324.9 372.8 436.9	21.5 38.3 33.4 28.5	12.2 9.9 10.7 11.0	7.7 6.3 6.6 6.9
		5,000	17,330	11.99	20	15	6	10 30 20 15	499.8 415.4 494.0 566.1	26.9 61.3 35.1 30.6	12.9 11.7 12.8 13.9	7.1 6.8 7.2 7.5
		10,000	22,105	11.00	20	12	6	10 30 20 15	637.7 950.0 638.3 710.4	27.2 41.3 35.6 32.0	15.1 13.6 14.9 15.9	7.8 7.5 7.7 8.0
					(Cunt	(bund		10	an 240	₹ ₹ • * `	↓ 7 ● ⁷ ?	7.4

Table 2 Vehicle Date

Determined from tire prints on a hard surible.
Computed by dividing test wright by total contact area, among these soled.
Average of greatest length and tidle of each tire.
Buply wrights from data plate on each vehicle; tire prints and for one side of vehicle only.
Dual tires are empidered as one for determining visit.
Webicles wright a platform seales and tire prints ande for all tires.
Total context area, everage restort presents, and everage tire print set determined for 15,000- and 20,500-15 test wright:

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								Tire Dest	ristics			
Vehicle	Nepty Velght 1b	Approx Lond 1b	Test Veight <u>lb</u>	Vidth in.	Rim Diam <u>in</u> .	Ply Nating	No. of Tires	Tire Pressure psi	Total Contact Area ag in.	Average Contact Pressure 	Average Print Length	Tire in. Width
			التوجيعات البدي	Yunn Te	st Pro	Co	stinued)				
			Self-pi		ites)	ed Vebic	ies (Qu	stinued)				
5-ton Hel 6x6 truck	18,115	0	18,115	14.00	20	12	6	30 20 15	568.0 684.6 788.8	31.3 26.5 23.0	11.9 13.3 14.6	8.9 9.4 9.5 9.0
		5,000	24,275	14.00	20	12	6	30 20 15	689.6 852.5 970.3	35.2 28.5 25.0	13.3 15.6 16.9	9.4 9.9 10.2
		10,000	26,175	14.00	20	1.2	6	30 20 15	795.7 955.3 1052.4 1139.2	35.4 29.5 26.5 21.8	14.8 16.5 17.8 29.5	10.0 10.3 10.7 11.1
		15,000	32,380	14.00	20	12	6	30 20 15 10	5'9.9 1078.3 1211.1 1480.2	35.6 30.0 26.7 21.9	16.0 18.2 19.8 22.6	10.4 10.6 10.9 11.3
5-ton M54 6ar6 truck	20,635	10,000	30,635	11.00	20	12	10	30 20 15 10	773.4 1004.6 1128.4 1307.6	39.6 30.5 27.2 23.4	12.8 15.1 16.7 18.2	12.00 12.90 13.10 13.70

Table 2 (Continued)

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Self-propelled Tracked Vehiclests

	Test Weight 1b	One 1 Length	Vidth	Both Trucks Total Contact Area sq in.	Average Contact Pressure psi
1/4-ton MP9C weasel	5,970 6,970	78 78	20 20	3,120 3,120	1.9 2.2
speed tractor	36,910	126	24	6,048	6.1
tractor	76,000	176	22	7,754	9.8

				Carry	10.301	the Test	Program					
			2	11-2102	-11-1	Whee led	Vehicle	<u>eii</u>				
1/4-ton M36A1 484 truck	2,775	200	2,975	7.00	16	6	i.	3 0 20	98. 6 121 .7	30.2 24.4	6.7 7.5	4.4 4.7
-								15 10	141.3 167.5	21.1 17.8	8.2 9.2	4.8
3/betan 1137 bab truck	6 ,06 7	0	6,067	9.00	16	8	*	30 20	178.7 217.4	31.6 26.0	7.8 8.6	6.7 7.2
/				•				15 10	247.3 290.9	22.8 19.4	9.1 10.2	7.5
2•1/2-ton M115 685 truck	12,450	5,000	17,450	11.00	20	12	6	30 20	419.4	41+3 35+1	11.7	6.8
								15	500+1 637+7	30.6 27.2	13.9	7.5

("cetimust)

9 Sul tires are excidented as one for determining width.
90 Subicions weight an platform scales.
95 Subicions weight area, average contact pressure, and average tire print length and width are assumed to be sume as Tums, Aris., deta.

									ire Des	cription				nia in Alfred
Vehicle	Mapty Weight 1b	Approx Lond	Test Weight	Width	Rin Diam in.	Ply Ant- 186	No. of Tires	Tire Pres- sure psi	Total Con- tact Area sq in.	Aver- egs Con- tact Pres- sure psi	Average Print, Length	Tire in. Width	Distri of Weig Tongue	bution st, 1b Wheels
				Cum	Lajev	ine Tee	t Prog	ma (Cue	(beunite					
					Tow	d the	led Vel	iclest)					
1/4-ton M100 cargo trailer	569	0	565	7.00	16	6	2	25 20 15	- 29.9 31.4 37.7	16.5¶ 15.7¶ 13.1¶	4.4 4.7 5.0	4.4 4.6 4.7	75	بلونا .
		250	782	? 7.0 0	ń	6	2	10 25 20 15	41.2 31.0 33.0 38.6	12.04 22.04 21.44 18.34	5.2 4.8 4.8 5.1	4.7 4.2 4.3 4.8	75	707
		500	1,127	7.00	16	6	2	10 25 20 15	43.7 43.7 47.1 54.5	15.04 23.54 21.84 18.84	5.0 5.7 5.9 6.0	5.0 5.0 5.0	101	1,026
		750	1,211	7.00	1€	6	5	.0 45 20 15	51.5 47.0 51.2 55.7	16.74 23.84 21.84 20.04	7.0 6.0 6.6 6.6	5.2 5.1 5.2	ملوي	1,117
3/4-ton MO1 oargo trailer	1,339	750	2 ,08 9	9.00	16	8	2	*) 30 20	58.3 71.3 81.6	33.49 27.39 23.99	6.5 1.7 7.0 8.6	5.8 6.4 6.6	140	1,949
		1,500	2,960	9.00	16	8	5	45 30 20	75.7 96.3 113.9	36.74 28.04 24.44	7.0 8.0 8.8	6.8 7.2 7.5 7.6	183	2,777
		2 ,25 0	3,679	9.01	16	8	2	45 30 20	90.5 104.6 132.3	38.44 33.24 26.24	7.6 8.2 9.8	7.e 7.5 7.7	207	3,472
1-1/2-ton 1961-05 cargo trailer	2,450	1,500	4,110	9.00	20	8	2	45 30 20	100.5 121.6 144.7 196.0	37.49 30.99 26.09	9.9 9.9 11.5	7.0 7.1 7.4 7.6	352	: ,758
		3,000	5,648	9.00	20	8	2	45 30 20	120.9 140.5 188.6 269.7	43.94 37.84 28.14	10.1 10.6 13.4 17.0	7.4 7.5 7.7 8.0	340	5,308
		4,500	7 , 68 2	9.00	20	8	2	45 30 20 15	145.4 177.5 224.4 262.8	49.44 40.44 32.04 27.54	11.0 12.6 15.0 17.1	7.5 7.7 7.9 8.0	201	7,179
6-ton oargo trailer	10,960	0	10,960	(10.00 (11.00	20 20	10 12	*)***	45 30 15	307.5 358.3	35.6 30.6 23.7	7.6 8.2 9.3	6.1 6.6 7.2		
		6,000	17,150	(10.00 (11.00	50 50	12 10		60 45 30 15	377-2 433-3 498-1 660-5	45.5 39.6 34.4 25.0	6.4 9.0 9.8	6.8 7.1 7.4 7.5		
		12,000	25,520	(10.00 (11.00	20 20	10 12	*}**	50 45 30	490.4 533.8 638.0 799.6	\$2.0 \$7.8 \$0.0	9.8 10.6 11.6	7.3 7.5 7.5		
37.5-101 generator tradier	7,153	0	7,155	7.00	20	8	•	60 65 30	128.5 146.2 175.4 243.8	55.7 62.9 60.8 29.3	8.2 6.8 9.8 12.4	4.9 5.0 5.1 5.0		

Table 2 (Continued)

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Vehicles unight a pistfut same and tise prints and for all tires.
 Computed from unight an about instead of total test unight.
 20.100000 tires as from about and 22.00000 tires as rear about.

Short 3 of 3 shorts

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Summery of Data and Test New Ats, Single Self-propelled Vehicle Tests

1/4-ton "." And with Truck (Four 7-00x16 Tires)

	ž ži	42	a i E e	ר א ^ר און			• 1	S.			e N	1 1	9 ej 2 3	3 4	3 i 1 1		hearts
						Vehi	le ter		Let L	te Teet	Property of	Lost 50	4				
	25	25			8	,	~	2	3	8	3	a l	8	*	5	2 0 0	Send dry to 2 in., wist below
	9.9 •	R S		0 c	89	9 2	N (1	R#	R 2	512		9 1 00	R 7	88	۶Ę	ю -œ	Blight Jerling motion Dry memil, maxy travel
	5P	9.P		00	3 2		1 04	5	8	15	2	5	: %	2	18	-	Dry ward, slight Jerking motion
	2	F			.8	2	04 (81	¥:	81	8	utti i	81	21	2	3°	Holer and
	R (R (•	<u>ا</u> ر ا		~ ~	62	82	6 7	9 10	-0	29	178	11	¢	Ments animiter
		2E	-	~~	38	ļ	4 5	2	32		530		1.9	-		.	Sand dry to 1-1/2 in., molet below
	2	4		•	8	2	5	4	on n	8	3	106	53	137	8	~	fand dry to 1-1/2 in., moist below
	2 1 27	\$1		<u>د</u>	R 8	2	. 🕈 🕻	2 2		8	1	8	5	6 67	<u>,</u>	.æ 0	Send dry to 1 in., may travel
	61	et		•	88		N 0	25	38	ខ្មរ	<u>.</u>		81	5 2	58	9 5	Band Gry to 4 In., wheeld spinning Band Are to 1 (n., slight spinning
	: s	:\$: 01	R 8	2 .	• ••	28	12	19	191	18	12	18	58	- 90	the spining
	19	61		-	8	2		8	P.	2	n N	4	. #`	III	R	7	Bend try to 3 in., alight spimint
	נע 12	R .(0	ន្ត		cy (81	R	8 Ş	81	83	8:	i i	3	3,	Moist and, wheels spinsing
	8 F	81	_	0 0	R =		N 0	R	р з	9 9	5			£.	50	e e	
		٥Ķ	-	20	ំង	2	4 A4	38	2 ye	8 F		1	9¥	2	116	* *	find the to 2-1/2 (p., then a purification
	R	R		8	1	2	~	8	3	9	216	8	\$	151	18	••	Bany trevel
	2	2		<u>د</u>	15	2	~	\$.	8	r:	N	ŧ	.	Ę	511	~	Bug trem.
	5	5		a: 4	5	2,	~	Ş	8.	3	える	13	31	5	31	æ .	See 417 to 1-1/2 in.
		EF		e ~	<u>.</u>	2 4	04 O	8 9	2	<u>849</u>	210		Ra	85	<u>5</u> 5	e	Berd Gry U: 4 In.
	5	5			12	u e	~	18	8	F	8	8	12	F	8	4	Band day to 2 in., violant Jerting
						;		4	i			-	1	7		`	wition
	8 j	96			21	24	~ ~	83	22	5	[0]	5	\$:	ĸş	28	•	Bend dry to 2 in., acte wheel spiming
	3 2 2 2 2 2 2	.		~~	22	2 5	4 64	i 1.	58	Į F	5	35	:5	P	12	n ac	Multit and, considerable effort
	5	F		0	1	Te.	c,	2	2	S .	Ľ		2	63	7	a.	Noist send, Jerting Botion
				c .	GI :	.	~ (8	87	S 2	2	ł	51	551	10	- ب	tent ary to 2-1/2 in.
		26		-	19	a .a	w r w	C af	1 .5	8 <u>9</u>	Į Z	1 8	× 8	ŝě	t R	<u>.</u>	
	2	-		~	10		~	2	\$	67	E)	r	3	61	2	5	tend dry to h In., Jerking motion
		**		• •	çç	ē,	ou o	2	8.8	3	8		21	35	¢2	1 71 - 4	tend dry to this, Jerning totion
		15			- 196 21 - 1942 - 1 194 - 1949 - 1949		<u>.</u>		2.94	4 P	2 F.	8	. R	35	5	** * ***	Mulat and, Jerting motion
	3	3		Y	-	2		- 94	3	5	3	8	2	8	3	•	Rolet and, slight betting totion
	2	ب الج			4	.	~	# .;			×.	Ŕ		Ē		•	They trans
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· See "Deer Terre" when "Definitions" in terr.

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Table 7 Summary of Data and Test Meauits, Single Self-propeiled Vebicle 7- ats 2-ton MAL, Sub Truck (Six 14.00x20 fires)

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7	7 % 705	15	्र मुख्य	Te s Te c	5	- 24 51	101	214 141	.,∕ 0 • 210	300+	19 12	213 151	10£	******	*****	BARG GPy on surface,
51	267	11	₩ >	Ter	5	96	134	200	266	300+	65	200	112	******		motat below
`>* \$\$	- 205 3974	9.5 3	942) ₩3	No. Yes)		144. 86.	172	1/8	216	71	1779	115 8*.	10	3-1/4	
1	240	9	¥.)	80	*،	66	1 30	184	268	y00+	67	201	135	15	8	
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·	्म 	23.5	20	144 100	7	72	126	172	204	300 4	6	19	132	161/7	2	
* 3	423	22	20	Tes	5	6	1.36	Mo	27,2	270	15	199	131	*****	*****	
6 4. 6.8.	*01 208	n.5	20 6 3	Se Se	5	66 Ar	162	222	212	20 militaria 14 Militaria	い	219 20-5	159	19	1-1/2	
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51	277	17	20	74.	5	L)		125))a)	140	16	no	71	*****	*** * 1 *	
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79	796	13.5	20		\$	ħ	12	28	70%	4 2 4	ħ		151	13-1/2	1-1/2	
7) 79	200 111	19 29	20 14	Ten Ten	2		116 116	145 1146		127	¥5 45	103 103	72	10=1/7 ****	3	Sind wet to
73	4)	A .,	15	900	5	,	JIG.	in	1%	154	5	196	110	*** ***	*****	1 14.,
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87 8 6	264	23 23	10 10	106 No	10	126	176	232	200		105	232	70 167	18	1-1/2	
89 90	263 279	22.5 20	10 10	No No	10 10	54 206	85 152	122 143	150 168	210 1 86	49. 89	119 156	3% 117	23 	4- <u>1</u> /4 *****	
91 02	243	16	30 30	Tee Yee	5	107	160 72	212 	264 79	292 74	91 16	212	150		*****	find wet to 1 in
<u> </u>	236	12.5	30	Yee.	Ś	Ä	112	1/55	236	264	60	179	121	19-1/2	3-1/2	moist below
5	244	10.5	30	No.	10	100	143	196	250	266	6	200	142	•••	*****	
90 71	242 241	10 10	0ز 50	Yee No	5	86 85	100	208 198	230	2782 26.4	76	189	143 131	20-1/2	4-3/4	
98 99	239 238	9 7	30 30	Yes No	5	53 71	79 96	113 160	154 246	206 296	45 57	1.) 167	61 116	20-1/2	••••• 5	
100	249	22	20 [#]	Yes	ş	64 86	121 120	178	226 208	968 260	63 70	176 164	119	:Hat /2	2	
102	251	20.5	20	Yes	Ś	75	82	n	61	58	54	n	59	*****	• • • • •	
103 104	¥73 252	a) 19	20	1ee No	10 2	233 233	182	274	588	***	178	241	175	16	1-1/4	
105 106	247 246	19 18	20 20	Tes Yes	5 5	38 30	30 35	32 41	3" 47	39 14	24	92 41	26 12	******	••••	
107	255	15.5	20 20	Yes No	5	67 97	90 122	133	166 234	176 276	5Å 71	130	32 :27	18-1/2	2-1/2	
109	245	14	20	iic Iic	10	119	175	248	296	200+	102	240	170	16-1/2	1-1/2	
111	254	43 14•5	20	No	5		134	171	212	248	77	172	123	22-1/2	5-1/4	
112 133	252 258	27 25	15 15	Tes Tes	10	01 77	57 120	59 180	57 216	228	41 69	115	:21		••••	
114 115	261 263	25 23.5	15 15	340 180	10 10	120 116	172	28 4 220	300+ 252	29R	: 77 99	259 215	181 154	1 8- 1/2 18	(1-1/2	
115	260	23	15	No No	10 10	82	130	16 4 220	212 260	952 205	74	169 218	120 157	19	2-1/2 2	
118	264	20.5	15	Yes	10	50	68 A6	88	158	188		105	75		••••	
120	459	19	15	No.	10	- 2 5	140	188	252	296	82	193	437	19	2-1/2	
121 1 22	265 265	19	15 15	No Yes	10 10	64 72	- 5 5	58 225	16 8	81 204	50 59	60 129	55 94	19 *****	2-1/2 	
123 124	267 268	18 18	15 15	Yes Ng	10 10	- 64 120	80 164	2¥6	122 277	146 208	91 98	99 XK	74 161	24	•••••	
25	271	29 21	10 10	No.	ेंडू इ.	58 61	100	152	256 57	30 0+ 63	54 63	169 58	11- 68	21	e•143	
127	212	27	15	Yes	5	39	65	100	134	152	y ,	100		*****	*****	
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130 131	27.5	22 72	10 10	Yes Ng	10 5	66 73	5% 112	82 156	. 20 226	268 268	37 63	89 165	44 125	25	4-:/2	
1,52	270	20	• -	3 0	10	90	8 7,	82	196	158	62	101	81	*****	*****	
						Webici#	Test Me	ight 32	300 15	Approx	impte L	and 15,0	00 16			
1:55 1:44	207 207	14 11	0; 10	Yes Yes	5	45 6a	101 120	186 157	244 20 :	276 283	50 63	177 169	115 119	******	•••••	Sand wet to
1.5	205	12.5	19 10 10	Y*s	3	49	92 158	146	204	264	49 70	147	39 162	•••••	*****	woist bears
1.7	222	* * * -		第9 第0	Ś	59	120	204	209	2(4	- 64	175	119	*****	****	
1.0	24	10	0: (ز	No Yes	> 5	80 80	109	112	285	240 240	- 65	190 175	123	******	*****	
.40 :-1	کل کے ا	, B	्रम् १३	No No	5	101 73	176 131	264 185	300+ 284		ijih Tie	247 202	144) 231	***	*****	
	21	8 7	90 40		5	101 78	164	224 267	28)A 277	300+ 100+	78	22'- 27's	156 160	******	*** *	
1944 1944	208	55	50 50	No.	5	2	128	206	248	254	75	195			••••	
147 147	221	2°)	90 24)	No.	8	133	172	229	500+	1 (* ***	104	234	1.0	*****		
147 148	224 214	17 18	21 21	No Yes	5	196 74	105	216 124	255 172	:0 0+ 274	91 42	222 1;5	19 II	******	*****	
149	22:	17 14	2 0 20	% . Yes	5	108 	192	212 216	21 2 220	(00) ()	86 54	212 101	150 119	****** ******	• • • • • •	
.51	215	.5	20	1 0	5	104	140	200	275 °	900+ 268	ð: a	205 205	145	*****	*****	
• 74 • 75	ees ZZZ	47 24	20	74+ 74+	5	<u>بو</u>	<u>.</u>	474 (1)	<i>6</i> 9	A contraction	62	71	,	*****	*****	
154 155	219 215	14 12	20 20	R o 744	5	900 36	(A)	170 9	125	152	73 3/2	479 96	11# *≸,	******	•••••	
19 ² 197	5»4 21	19 26.5	20 15	No Tea	5	60 84	115 119	215 701	292- 36		61 67	201 108	1 (1 79		*****	
150	2 50 9 11	24 21	25	10.	5	90 11-	48 1.87	14	54 2008	96 225	29	54 918	9) 146	****** 20)	2.1/2	
• <i>17</i> 140	* 27 231	21	47	Tes	3	• 7' 10	₩,	12	53	57	ý	50	Ž	*****		
101 102	272 272	18.5	13		7	5	10	100	K	2	94 43	95 105	• **	******	*****	
14) 164	827) 222	译 译	15 15	9 9 3 9	5 7	51	弊	105 95	1 yr 1%	146 884	49 54	10 8 110		******	***** ***-*	
1665 1666	2 2 56 2711	14 14.4	15 14		5	() 8	27	117 889	114 300-	179	%	りの	50 150	19-1/1	***** 2	<u>ية.</u>
167	**	13	iś		5	丙	13	117	55	70		115		•*****	*****	*

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Summery of Data and Test Monits, Towing Tests Time Test Program

Ites	Test Area	Test.	81.0pm	Tire Pressure pai	Druthar Pull	811p	Bruchar Full \$ of Test Weight	Come Index O- to 5-in. Depth before Traffic	Dem riss
		، <u>ل</u> اتنگ				heoled We	hicles		
	-			1/6.40	- 1/2/24 3	huh Teuch	Bast Mature *	075 ib	
		L					<u> </u>	11	Martin anna
2	Tump Test Station	40	0	20 20	4500	****	15.2	14	MCTA. BOUG
3		49 80	ũ	15	5504		18.5 26.6	14	
5		52A	10	15		****	****	24	Moist sand, could not pull
-		6.78	10	18	2008		6.7	26	enough to register
7	Distor area	944 	1	10	8000	****	26.9	89	Dry mand on surface, noic below
8		ji j	1.5	19	8000 700#		26.9	102	
10		9 - 0	2	10	700		23.5	1.8	
-				3/4-2	on Nº7, 4	the Truck	Test Weight 7.	085 <u>18</u>	
11	Yumm Test Station	54 55	0	34. 20	8000	••••	11.3	19 19	Hoist sand
13		- 56	ò	15	1,600		22.6	.9	
14		57	9 10	10	1,4000	••••	19.7	19	
10	Dane area	- și b	1	15	1,993		25.8	120	Dry and on surface, moist balow
17	ŵ	91A 88	4 6.5	15	1,4000		19.8	¥2 106	
19		90A	6.5	15	1,200		16.9	11 9 4	
20		89 90	10	15	1,000	****	14.1 15.5	. 12	
22		9.4	õ	15	1,9000	****	26.8	112	
23		A CAN	2.5	10	1,8000	· • • • •	25.4	10 5 96	
25		35	5	10	1,0000		14.1	78	
				2-1/2-2	on 1135, 0	into Truck	Tost Weight 1	2,090 .t	
1	Yumn Test Station	424	2	ديو 10	2,0000 1,800	14.5	15.1	29 24	No1#1 wand
26		420	3	10	1,900	8.5	14.5	29	
29		420	0	20	1,200	9.9 1.0	9.6	29	
ليو. الدر		434	õ	20	1,600	4.0	12.9	1	
32		430 430	2	20	2,700	11.5	20.1	1646. 1444	
3.2 346		- 54	ŏ	20	2,000	8.5	16.1	44	
35		438	0	20 20	2 ,50 0	28.5	20.1	in in In in	
37		-	č	1,	1,200	1.5	9.6	19	
36 30		145 140	<u>່</u>	15	2,100	5.0 7.0	6.9 3	19	
÷5		44D	ő	45	2,300	13.5	27.3	14	
41 42	,	44 5 647	2	15	3,400	19.5	22.5	19	
43		454	0	10	2, 100	5.5	18.5	26	
4444 3455		49 8	2	10	1,000		8.0 24.7	20 20	
46		450	0	2.5	4,100	16.5	32.9	2	
47		45 8 45 8	0	10	4,100	23.0 40.0	35.0 12.9	20	
49		31	12	*0	0	****	****	31	
50 51		3984. 1/38	10	در 20	0			25	
52		39	10	15	2,000		10.0	2	
55 54		40 41a	10	10	3,200		25.7 23.3	25 31	
55		413	15	10	2,400*	****	19.2	51	
-	Marine Marine Marine and	~~~		2-1/2-4	on M235, 6	ant Truck	Test Height 17	1.330 36	Martine and
57	TAND TABE NOT TOP	570	0	30	1,600	42.5	5.5	22	
50 59		21C 21C	0	30 30	5,000	23.0 11.5	5.7 2.4.5	29 29	
60		244	.) A	20	1,000	1.0	5.8	*	
62		240	0	20	2,300	45.0	13-3	24	
63 63		24	0	20	2,200	99. 0	18.7	25	
65		24.	5	20	2,600	9.0	19.0	2	
5 <u>6</u> . 61		2%6 254	0	20 15	3,300	10.5	入型 (5) (株) 各	A 19	3
6		259	Ō	15	3,700	\$7.5	22.1	19	
99 1 0			0	17	1.20	8.0 53.5	19.0 21.9	78	
11		20	0	19	3,500	N.9	40.2	19	
73		1	19	10 10	1,300	27447 27447	7.5	1)	
						(Cast in	(Jan		

· iprime tealter pull.

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Bussery of Data and Test Beaults, Towing Tests Tune Test Program

Iten Bo.	Test Area	Test. Bo,	Bloge	Tire Pressure 	Puli Ib	110 110	Druchar Pull \$ of Test Weight	Come Isdex O- to 6-in. Depth before Truffic	
	-			• /• •		hegied Ve	hicles		
				14460	a Mydal,	ALA TINCA	THAT WILLIAG	1913 10	
1	Yum Test Station	47	о 0	30 20	280*	****	9.4 15.2	14 14	941 C. 6604
3		14.54 2.0	ů,	15	550		18.5	14	
4 5		52A	0 10	10		****	40 40 ****	25	Noist sand, could not pull
			10	1.6	0008		6 1	24	enough to register
7	Dune area	944 1944	1	70	800#	****	26.9	89	Dry sand on surface, noic below
8		943	1.5	10	800#	****	26.9	102	
10		9 - 0	2	10	700		23.5	1.8	
•	•			3/4-2	an: 1137, 44	the truck,	Test Weight 7	<u>985 16</u>	
11	Tumm Test Station	54	0	<u>ن</u> ار.	8000		11.3	19	Noist sand
12		- 55	0	15	1,600	****	22.6	19	
14		57	0	10	1,4000		19.7	19	
10	Dape area	23 913	1	15	1,000		26.8	120	Dry mand on surface, moist below
17	*	91A 88	4. 4. г.	15	1,400	****	19.8		
19		90A	6.5	15	1,200	****	15.9	<u>113</u> 0	
20		89	10	15	1,000	****	14,1	.12	
22		948 943	20	10	1,900#		26.8	312	
23		≪PA GDA	2	15	1,8000		25.4	10 8 86	
25		940 95	5	10	1,000		14.1	78	-
				2-1/2-	ob 1135, (646 Truck	Toot Weight	2,450 .b	
đi M	Tunn Test Station	42A	3	355 40	2,000 0	14.5	16.1	29 24	Notet sand
26		420	a l	30	1,900	5.5	14.5	29	
29		420	2	<u>30</u> 10	1,200	3.0 1.0	9.6	29 29	
بر نز		434	ó	io.	1,600	4.0	12.9	44	
¥2		430 11 12	2 9	20 20	2,700	16.5	21.7	1.44 1.44	
33 34		Ф	õ	20	2,000	8.5	16.1		
35 16		- 入 理:	о 0	20 20	2,500) 21 M Yo	28.5 28.0	29.1	i de la	
31			Š.	1,	1,200	1.5	9.6	19	
30		443)	1>	2,100	5.0	6.9	19	
,)≇ ⊷)		44D	ő	45	2,700	13.5	21.3	19	
41 13		يغيد جيديد	י ר	15	3,4000 2 800	19.5	22.5	19 10	
44 6 g		*54	5	16	2, 300	5.5	18.5	*	
444) 2.12		4 58 460	2	10	1,000	0	6.0 24.7	26 26	
5		50	ó	1.5	4,100	16.5	32.9	a de la companya de l	
47 R		45 2	9	1)	4,500 [®]	23.0	36.0 12.0	26. 24.	
₩9		37	:2	40		****	<u>3</u>	31	
50 1		ja	10	<u>ر</u>	9			25 26	
21 52		90 9 39	10	15	2,000	****	16.0.	47 21	
55		40 518	10	10	3,2000	****	25.7	25	
55		11	12	10	2,500	****	43.3 19.2	34 31	
				2-1/2-4	op 10.35, (truck	Tres Wester 1	4. 91.10	
% 57	Type Test Station	A(S	а 9	99 30	2,2000 1,600	15.0 41.5	12.7 9.2	29 29	Noist seri
%		2,0	0	30	1,500	2).0	A.7	29	
77 60		يو » 44	eu نړ	シ 約	1,000	44+7 3-0	5.0	67 25	
61		24	0	20	2, 100	10.5	14.4	24 	
63 63		24	0	#0 20	2,200	•7.0 39.0	*2+3 12:7	*	
<u>Ģ</u>		24	0		1,000	12.0	17.3	25	
74		244	0	(4) (約)	3,8000	10.5	10.5	A	1
(t)		274	0	15	4, 200	21.0	8	19	•
4		276 276	9	47	5, 190 5, 39 0	8.0	49.9	19	
10		×4	9	10	3,800	2.2	\$1.9 \$5 a	19 ta	
14 12		×.	ō	10	3, 740 5 , 200	M. 0	30.0	19	
73		19	19	**	7*)(100		7.3	13	
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					Te	nte g (ci	997 9999)		
Ites No.	Test Ana	10.1	51.0pe	TIN Pressure 	Draider Null	Bilip	Dreider Pill § of Test Weight	Crime Index O- to 6-in, Depth before Traffic	Reports
					theo los	Yahicles	(Continued)		
			2-1	/2-4 m 1035	, Gul Tru	the Test	W . M 17, 30 1	b (Continued)	
* 1	Test Station	19	- 10	15	2,000*		11.5	13	Noist sand
, #3	(Tontinued)	21	14	15	3,800*	****	د. 11 19	13	
71 78	Dune sree	22 10 1	13	10 15	2,800*	****	16.2 11.5	14	Dry and on surface, addst below
74		184	ý.	10	2,400	****	13.8	Ĵ.	
				2-1/2-1	on ML35.	ień Truci	, Test Wright 2	22,105 16	
80	Yuma Test Station	273	o	<u>)</u> (2,000	10.5	8,8	A)	Hoist sand
62 62		27C	0	90 90	2,500	17.5	11.3	20	
8- 8-		27⊅ 27€	ф Ф	90 ()	2,200	36.0 ₩6.0	9. t 8.8	20	
85		284	ò	20		9.0	13.4	<u>.</u>	
500 501		59C	2	20	4,200	20.5	10.1	€ 4 ≥ de	
38 80		280 280	9	20 20	2,000	5.5	8.8	₹ 3 6 <i>4</i> 44	
- yo		234	õ	15	5,000	25.0	32.9	90 10	
91 20		29 0 290	4 3	# 15	4,000	54.0 40.0	17.6 19.8	्र स्ट्र	
94		290	ō	15	2, *00	5.	15.1	:0	
_#* }*>		298 298	c	15	5, ruu 4,600	0.0 14.5	19+5 -40+3	د. د ب	
₩ 27		290	A	15	4 ,800	17.5	21.1	40 2	
· #9		3008	2	12	900	с. С. с.	16.7	÷1	
100		300 300	0 2	10 17	4,700 6,000	9.0 25.5	20.7 25.4	-1	
101		30 2	2	10	5,000	59.0	22.0	-1 -1	
1.14		يمو و و	10	15	2,000# 1,000#	****	11.2	25	
104		:	12	15	2,000	••••	8.8 7.0		
1.32		354	12	ić.	1,300		24.5	2	
7-2% 7-2%		:⊃# 36	16	1.J	:,800		14+2		
				>-ton	141, 6 06 1	ruck, Te	et Weight 28,17	5 16	
109	Yum Test Station	59	>	Ot	3,4000		:2.1	14	Notst sand
10 111		40 61	5 3	20 15	5,400*	****	19.2 24.1	14	
114		52	- j	10	3,000		1	1	
114		95 8	.7 .7	10 10	1,200		8•5 2•5	29 29	
115		- #A 	8	برج 20	2,790 0 2.5000	****	9.0	- 29 29	
127		95	15	15	4,0004		14.2	22	
11^{-1}		97 98	15 15	15	2,000	****	7.8	2 t	
		1.77 1/514	15 13	4 - 1 -	5,000 5,000	••••	17.8 11.0	22 24	
12		1018	15	ŭ	000		1999 1997	2,	
1.e	_	172	20	13 1	2,000#		9+9 	42	
7 *		s #	~	<u>y-tor</u>	<u> </u>	TU 1. TO		2.40	Martin and
125	ian tear 1492 108	136	9	99 20	5, 300A	****	12.1	* *	en el 1876 e 1985 also
125		1.37 1.36	о Э	15 10	5.400* 6.800*	****	18.1	<u>د</u> د	
		12	10	15	2,000	****	5	÷ +	
129		111 110	·2	4 # 349	- 190 1	****	/*2 (** 9	 72	
					-	<u></u> -			
	-				Tr.			· · · ·	Net - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -
	14 M4 MA	ن ۇ رىد.	Æ	1	3 200		<u> </u>	2 A T	Mit familie and a
a., 1•● 1. g2●●	<u> and 1905</u> 2005	4 28	1≇ 15	**	x,790 2,000	\$14 ² 4347	tti e∰ Na rets	49'* 19.*	रस्य-∔ सम्बद्धः आत्मुव्य द्वर्थदे
2 : - - 10		流	2 3	**	2,800 2,400	11.) 12.5	λαβος του 1	13™• 137•	
4 55 **		a	ур , , , , ,	**		444, ()	A.	● 31 ♥ 51	
¥2.## 		a) M	. я Г	**	7 ,90 0 3, 400	17,4 % ,44	₩.7 57.0	157+ 157+	
1. 20 1		14	# 2.# #**	**	2,230	14.0 25		, ∦ ™ * 	
x 1777 23459		×	* ****	**	2,270	**** 	· · · ·		
29.1 2924		'净 '津	یتو. چ بطن	**	e 30. 3 306	14.5 14.5	₩ \$91.3	an an Frantsa Frantsa	
 1		4		**	. ×4.	26. 5	5. 5. 5.	- 12 Ma 12 Jun	
7 Marca A		76	¥.	**	1#***# # *	****	2842 	<u>≜</u> .⊄	

the study of solar pail.
 Peets ()) = 3.3" -modured on text (and before hardwring.
 Peets ()) = 3.4" successful on text (and offer and proceed the target.

See 2 of 1 dants

						14	ble 6 (Co	stimuet)			
Nes Re-	Trat A	111	Test <u>Ro.</u>	Alope	Tire Pressure 	Druider Pull 13	80001 0110	Dreifer Nali § of Thet Bright	Cons Index C- to 5-in. Depth before Traffic		Americ
						True	Yehleles	(Continued)			
		-		and and the summary set of the	1/6-ton :4	SC Yourel	ters in	10t 5,97. 10 (Continued)		
346 0	Time Text (-	٥		1.000	25.0	50.1	11	Motet and	
14/14	Continued)	51 51	0		1.2500	55.0	54.4	14	1999 B 2 8 8 8 8 8 8 8 9 8 9 8 9 8 9 8 9 8 9 8	
1674	(,	ŝ	ō		3.2500	62.0	54.4	14		-
1484			- <u>é</u>	õ	**	3.250	79.0	54.4	14		
149			- G	ō	**	3,600	40.0	ΰύ. 3	5		
150			6	9		3,600	50.0	60. 3	5		
151			÷C	0		1,300	5.0	21.8	÷,		
15-			60	0	**	3,490	24.0	57.0	£.		
153			62	0	**	700	2.0	11.7	5.		-
154			67	0		3,500	26.0	58.6	5		
155			40	0	**	3,700	57.0	62.0	5		
136			3	20	**	≨,000 ≠	****	33.5	4		
15"			* 4	15	**	2,3000		38.5	i cui		
150	Dupit area		<i>,</i> 87	8		2,800	****	46.9	54	Dry said on	surface, moist below
159			309	10		2,300	****	30.5			
160			y 10	14	**	2,600		43.6	90		
					1/4-4 or #2	90 Wessel	Tost We	144 6,970 15			
1F1	Tumm Test	Astion	7 A	J	**	1,600	7.5	23.9	ý	Noist sand	
M				0	**	1,500	5.0	21.5	9		
16?			7C	9		2,400	10.0	بالبيادر	1 J		
164			TD	0	**	3,800	¥7.0	54.5	9		
165			71	Ģ	**	-,400 -	40.2	53.1	÷.		
16.			77	A		4,4000	0.6ر	61.1	9		
167			70	9	**	2,600	10.0	37.3	9		
1/2			ČA.	0		1,500	5.0	23.0	10		
19			1 1	3	**	3,600	12.0	52.0	4 -		
172			ac .	0	**	1,500	3.0	21.5	*		
117		•		9		3,000	9.0	4 (U . A A	1-		
172			e y Om	9 A		3,400) 	10.0	40,6	1.1 1		
113			047 8-0	9		4,000	21.9	60.2	15		
174			- 112 Ann	1		4,230 5 (2004	27949 1111	74.3	1		
117				~ ~	· ·	4,999	12.0	51 £	** *A		
1.15			101 10			2,000	+	7 1 1	44 261		
∔ [] 178			11	47		2,000 0	****	24+2 44.0			
• • •			*1	•/	16				7799 		
					10-LOD HA		a incu	r int wight	2-19-2-16		7
179	Yuma Twat	station	374	Q a	**	20,000		24.4	h (pry and to	1/11/1/ BG185 7#1/W
100			514	.0	**	15,000		440.2 g (₂ 3. es - 1	4년 17		
181			3708	12.5	**	17,000		And interesting to a	4.4C		
102			SPC	15	**	14,000	****	34.13	3 6 73		
103	have ever		9000 . Sar		**	11,100		c 9 4 7 		ury aans an	EATIMAT, MOLEV DELOW
104			- 5000 1-200	4.4 	**	S WWW		-7 7+ 4 ≂33 19	£ 1		
103			99 96 - 144	17	-•	G, JAN		624 + F., 1946 - 17	مر ہ +		
187			2/27) aB1	15		7,500		20.1	4 1 1 1		
401			Jre }	. .	18.4 - #		1 Tmator	To at intant	** '6.000 at		
. B ár				0	2073 BA		- 178-03	A	n an	frank ward be	بينظ هموري وفار
1/905	Tump Test i	stizz	:70	7) A		50,000 	****	57.0	14 j.	hell anna re	1 15., 50185 €°2 #
104			57 (A) 27 M	19 6	**	-79,30.₩ 28.300€	****	312 + 1 4/3 - Å	19 19		
4 7 4			31 	** * *	**			€× 1 ¥	**		

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• Susan devide pull. • Suda 13-16 modeted in fest inte after un juss s'

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Table 9 Busery of Data and Test Proults, Town-rubicle Tests Onslow Beach, Camp Lejeume

		•		Towing		Come	Inde x	Rat	Noisture	
iena.	Type of Test Sufface)	Test.	Tire Pressure Del	Force Reguland lb	as \$ of Test		Arter	Daryeth One Paus 10.	Content 0- to 6+in. Depth	Sand Condition
				1/1ton M100	Trailer, Test W	eight 569 :	<u></u>			
		0	36	1.3	÷ 1					
	Asphalt pavement	10	20	12	2.1					
	Asphalt pavement	11	15	15	2.6					
	Asphalt pavement	12	10	18	3.2		•••			
	Disturbed sand	5	25	30	5.3	156	155	1/2		Wet
) ,	histures mand	7	20	30	2.5	155	455	0		Net. Net
3	Disturbed sand	ė	10	30	5.3	153	153	ŏ		Wet
	Undisturbed sand	ĩ	25	2	3.9	176	174	ō		Wet.
	Undisturbed sand	2	20	22	5.9	173	174	0		Wet
	Undisturbed sumd Undisturbed sumd	3	15	20 18	3.5 3.2	174	174	о 0		Vet Vet
				1/4-ton 1100	Trailer, Test W	eight 782	b			
	Asphalt pavement	63	25	Ř L	2.7	•••	** *			
	Asphalt pavement	65	20		2.2	•••	•••			
	Asphalt pavement	65	10	17	2.2					
	Disturbed sand	18	25	51	6.5	152	152	1/16	4 . 1	Vet
	Disturbed sand	19	20	38	4.9	156	154	1/16	6.0	Wet
	Disturbed sand	20	15	38	4.9	155	155	1/16	4.0	det.
	Undisturbed and	13	25	53	5.8	151	151	1.78	4 .0	Wet.
	Undisturbed sand	14	20	60	7.6	147	147	1/8	4.0	Wet.
	Undisturbed and	16	15	47	6.0	1+8	148	1/8	4.0	We t
	Undisturbed sand	17	10	50	6.4	123	124	1/8	4.~	We .
			1	A-ton 100	Drailer, Dest We	1011 1.127	<u>1</u>			
	Asphalt payment	59 60	25	22	2.0	•••	***	*****		
	Asphalt pavement	61	15	22	2.0		•••			
	Asphalt pavement	62	10	25	5.2					
	Disturbed sand	43	25	65	5.8	149	192	1	11.1	Wert.
	Disturbed cand	44 1.5	20	20	5.0	110	114	1	11.1	Wet
	Disturbed and	46	10	30	1.6	149	153	3/0		uner. Mast
	Undisturbed sand	39	25	75	6.7	151	156	1/4	11.1	We*
	Undisturbed mad	10	20	87	7.7	151	152	1/4	11.1	Wet
	Undisturbed and Undisturbed and	41 42	15 10	82 60	7.3 5.3	149 150	151 151	:/* 1/*	11.1 11.1	Wet.
			1	/4-tas 10:00 1	miler, Test We	1.04 1,211	10	- ,		
	Asphalt pavement	55	25	23	1.9		•••			
	Aspent process	50	20	23	1.9	***	• • •			
	Asphalt myseset	58	10	63	3.6	***	•••			
	Disturbed sead	17	25	72	5.9	153	152	3/4	6.2	Wet '
	pisturbed mand	-	20	72	5.9	146	146	1	6.2	Ve t
	Disturbed and	*9	15	50	5.0	150	150	3/4	5.2	Mert.
	that sturbed sand	51	25	118	4.7	150	171	3/0	5.2	NOT.
	Undisturbed end	52	20	72	7.6	146	1-0	1/2	6.2	Mart.
	Updisturbed sand	53	15	75	6.2	151	154	1/4	6.2	West.
	Undisturbud and	54	10	63	5.2	196	157	1/4	6.2	Wet.
			3	Varian MUL 1	miler, Test We	100 2,009	15			
	August pavelet	132	97 30	27	4+3 1-4	***	•••	******		
	Asphalt pevenest	134	20	32	1.5	***		*****		
	Asphalt pavement	135	10	35	1.7	***	+			
	Disturbed met	91	45	196	9.4	153	154	1-1/2	6.1	Wet.
	Distantion and	9 2	30	149	7.2	153	354	1-1/2	6.1	Wet.
		95 ch	10	+ AM	- B	473	177	↓−↓/ ● 1	5.1 Æ 1	
	that sturbed such	5	45	150	7.2	167	160	• 1/B	11.1	tint.
	these body to be	×	yŐ	121	¢.0	166	167	1/8	13.3	Wet
١						-		· -		

(Centimet)

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Table y (Continued)

iten;	Type of Test. Surface	Tost No.	Tire Pressurt Bei	Towing Paros Required	Towing Torce, as \$ of Test- bright	Come 0- to 6 Jefere Traffic	Index -is. Depth After Ote Pass	- Art Depth One Pass in.	Average Noisture Content D- to 6-in. Deeth	Sand Condition
<u> </u>				3/4-100 1001	Trailer, Test W	1 2,760	16			
6 1	tonkalt menungat	197	Lc	20	1.0					-
62	Asphalt pavement	124	10	32	1.1	***		******	_	
63	Asphalt pavement	125	20	50	1.4	* ***	***			
64	Asphult pavement	126	10	50	1.7	***	•••	*****		
95 	Disturbed sand	103	45	350 978	11.5	149 714	349) 167	2+;/4 1-3/8	4,2 4	W#1 Max
67	Disturbed and	105	20	220	7.4	145	167	1-1/4	4.2	Vet
68	Disturbed and	106	10	185	4. 2	14	147	3/4	4.2	Vet
69	mainturbed wind	- 39	45	219	7.1	160	161	0	1	Vet
1 0	Undisturbed rend	100	32	179	3.7 6.6	101 160	101	1/8	19.3	det. Cot
72	Undisturbed sand	105	12	+92 175	9.7	19,	194 194	1/4	₩7+3 2(1+)	Wet
				14-tor H101	Twiler, Test Ve	100 : (73	ib	-		
73	Asphalt parenent	119	45	32	0.6			*****		
74	Asphalt payers 7	120	352 	钙	1.9					
75 16	A sphait pavement	150	<u>وم</u> د م	44 15.	***		** *	* *****		
\overline{n}	Distarted sad	107	Le.	404	11.5	142	<u>)</u> 49.89	*	11.0	Wet
73	Disturbed mid	108	in a	352	9.6	126	115	1-1/2	41.0	Set.
79	Disturbed sand	109	<u>ಕೆ</u> ಗ್ರ ಸಿಗೆ	y i i	5.j	***	172 N#2 101	1	110	Wet
80) 80	Disturbed and Undisturbed and	114	10	217 312	8.5	151	4.5 Ma	1/2	1172	and the second s
82	Undisturbed sand	116	39	239	6.3	160	161	1/4	17.1	Wet.
83	Undisturbed wand	117	20	171	4.Ö	166	167	1/16	17.1	Vet
84	Undistyres and	118	10	150	4 • 1	171	172	./9	***	Wet.
_			3	-1/2-100 DCJ	6 Trailer, Test	Weight 4,1	10 16			
85 84	Asptalt pavement	264) 364	• 3 	65°	1.5	***	***			
	Assialt javement	146	1. Alexandre de la construcción de la const	52	1.5		***			
¥.	Asphalt pavement	147	12	12	2.5		• • • •	***** -		
8,	pt -t otherd word	1+0	45	488	11.7	124	135	1-1/2	*• 4	tie t
1974 143	14 et union and	143	39) 20	₩¥¥Z FLEUS	19.9	2£	4975 141	1•1/*	9.9	int.
74 %	Disturbed and	14 ?	15	350	*3*** ***		70	1-1/4	9.0	
11	undisturbed send	1%	45	510	1.4	1	100	ł	18.5	Wet
*	that sturbed sand	137	<u>1</u> 0	*20	11.2	· .	1 X6	1	18.6	Vet
ぞう 26	Undisturbed sand	4 SF 139	10	280	6,8	101	112	>/¤ ⊴/¥	18.6	Wet.
			1	-1/2-200 100.0	5 Tmiler, Test	Veight 5,6	<u>4; 8</u>			
<u>F</u>	Asphalt present	146	4¢,	ŕ,		•••		******		
945 - Dica 1	Asphalt payment	449 166		[+, 76	* •]			******		
ά.	Astial Davement	151	• ·	R	1.5	••	** *	******		
31	L. Larbed and	152	44 S.	1,0.7	18.,	* 3 5	9 -	4 4 2	2.6	Moist
96	Disturbed and			515	14.4	y Br	`3-∦ ⊜e	£	2.6	Moist
.23 ^£	Distinged with	1*# 1:1%	454 175	390 5/08	3 • 1 • 1	or Ja		1-1/4 1-1/4	2.C. 3.f.	9901 <i>8</i> 1. Minist
95. 195	Undisturbed sand	. 56	45	18	2400 2494 m	94 94	×.	···/-	5.412 5.44	Moist
зś	Undisturbed sami	-57	30	150	14.	8.	90	1- /4	3.4	Moist
07	Undisturted sand	158	26	4,592 6.00	11.5	1990 - 19900 - 19900 - 19900 - 19900 - 1990 - 1990 - 1990 - 1990 - 1990	1962 - 19	1 . A.	3. 4	
		477	10	1960/ 	19.4		# 4	:/*	5* *	1 0130
<u>^</u>	A	16.	£ #	-1/2-106 DC9	o Trailer, Test	er ty tot 7, 44	× <u>.</u>			
10	Assialt memorel	169	•7 K)	巍		***		*****		
11	Asphalt payment	170	20	55		***	***	*****		
12	Asphalt pavement	171	15		 ▲ ≠ #	***	***	******	* 2	
45 16	n statement sing *	1417 161	•7 *5	1.360	4/+2 14.2	90 14	1911 	4+3/4 2+1/2	2.6	Maist
15	Disturbed and	:42	ž.		 11.jy	ý.	F- I	i=3/4	ĩ.É	Motes
16	Disturbed sand	16)	15	•27)	12.*	Bj	36		2.6	Mar' et
17	Undisturbed sand	164	45	1,13	15.0	96 	92	1+1/2	2. 9 4 4	
19	and started and	166	74 第1	9772 1750	10.0	7' 109	14	*** <i>i *</i> \/ b	2.9	297183 19 2161
20	Undisturbet max	:67	15	• 615	9.6	129	12%	10	2.9	Mp1 et.

Teble 9 (Concluded)

Ites No.	Type of Test Sufface	Test No.	Tire Pressure sei	Toving Porce Juquired 1b	Towing Porce as \$ of Test Width	C- 10 5- Defare Traffic	Luter in. Depth After One Pase	Ret Depth One Pass in.	Abertage Hoistare Content 7- to 6-is. Desta	Sand Condition
			37	-5-101 Generat	or Trailer, Test	i vista 7.	153 15	Street and the	يويد جنار بالاست	
101	Armh - 18 marcamiash		40	67	· · ·					
100	Angles it an annat	217	¢.0	116	1.6			******		
121	Acabalt savaned	218		126	1.8	***		*****		
124	Archalt savant	219	15	201	2.8					
125	bisturbed wand	208	66	1.110	18.3	_ 116	431	******	9.6	Wet.
126	bisturing and	209	45	1.212	15.9	114	119	*****	9.6	Wet
121	Disturbed sand	210	jó	1,019	14.2	96	10)	*** * ***	3.6	Wet.
126	Disturbed samt	211	15	700	9.8	95	94	*****	9.6	Me %
129	Unit started sand	212	60	480	* 6.7	172	171	*****	81.7	Wet.
130	Undisturbed mad	213	45	380	5.3	174	1,6	******	21.7	Vet
131	Undisturbed mod	214	30	280	3.9	194	197	******	21.7	Mark.
112	Undisturbed and	215	15	2 6 0	۰, ۱	198	.200	*****	21.7	Wet
				6-400 Tra	Lor, fest wight	10,960 10				
113	Asphalt pavenest	196	60	190	0.9	***		* = = * * = =		
134	Asphalt pavement	197	45	200	0.9			******		
135	Asphalt pavement	178	30	130	1.4	***				
136	Asphalt pavement	199	15	200	1.6	***	•••	*****		
117	Disturbed same	204	60	1,090	9.9	162	162	1	14.5	Vet
135	Disturbed mand	205	45	690	6.3	176	173	1/2	14.5	Net.
11#	Disturbed send	206	30	450	4.1	174	2	3/8	14.5	Net.
140	Disturbed mand	201	15	320	8.9	104	1'r *	******	14.5	344
141	base bedrutethed	200	60	1,920	.7.5	112	114	1-1/4	1.0	M0187.
142	Undisturbed mand	531	45	لأسعام لا	14.6	104	112	1-1/8	1.0	Mp1 at
143	that sturbed sand	202	NO.	1,040	2.5	129	127	1/2	1.0	MD1 et
1 wite	Undisturbed mad	203	15	720	6.0	1.96	130	1/4	1.0	
				6-1.4 Tra	Ler, Test Weight	17,160 11				
145	As shalt an venest	192	60	220	1.1			*****	*	
116	Asphalt payment	193	45	220	1.3		***			•
147	Asphalt sevenat	194	jū j	230	1.3		***	* - **** *		
148	Asphalt savenest	195	15	540	2.0	***		*****		
149	Disturbed sand	1.64	50	1,600	9.3	169	159	1-3/8	5.5	Viet.
150	Disturbed stad	185	45	2,600	16.3	115	113	2	5.5	Wet.
151	DI "Rushed wand	186	30	2,200	12.8	102	94	£/ر +£	5.5	Vet
152	Disturbed and	1.87	15	1,900	11.1	đi,	65	1-1/2	5.5	Wet
153	Badistarbad and	2.88	66	2,500	14.5	1.00	179	1-1/2	6.7	246
154	Undistanturbud sand	189	45	2,000	11.7	121	112	1-1/2	6.7	Wet.
155	Undisturbed sand	190	NO.	1,600	9.3	127	120	1-1/4	2.7	And a
196	has befuititing	131	15	300	5.2	259	161	1-1/6	9. 7	
				6-ten Trai	ler, Test Velde	25,580 15				
157	Asphalt pavened	180	60	640	1.7	***	***			
155	Aspinit pavement	191	45	*50	1.0	***	*** *	******		
159	Argenals pareness	102	90	500	2.0		•••	******		
160	Aspinit prevenent	103	13	790	2.7	***			. -	
101	Disturbed sumi	172	60	8,20Qe	10.5+	2	***	1+5/0	- .7	
102	platurned and	173		N , M	10.0	चा	7 9	2=3/4	₩ •7	70 100
103	Distant and	174	90	3,000	14.I	. WI	97	x=1/0	₩ 41 b. 4	
70 0		12	12	87, 19 -42 5 2005	974 1		97 8 -		6	March 1976
197		4.199		2.24	534Å 10	<u></u>		7	6.0 6 A	Side 4
1000 1630			-7	7.2.2	17+4 17 12		*** **E	*****	6.4	and a
107		#799 1990				-		F	4.4	time t
1.000		ATV	*2		1740			*****		

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PLATE 6



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100 ¢ П ł 50 RESULTS) 1 45° LINE LA (TEST ٥ 1 10 **_** THOUSANDS OF 5 ₽ A PULL N 0 ۱ 0.5 -Ô 01 MARINAM DRAWBAR PULL IN THOUSANDS OF LB (COMPUTED) 01 50 LEGEND O WHEELED VEHICLES O TRACHED VEHICLES TEST RESULTS NOTE REFER TO TABLE & AND TOWING TEST SECTION IN VS COMPUTED MAXIMUM TEXT FOR SUPPLEMENTARY DRAWBAR PULLS DATA. WHEELED AND TRACKED

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