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PROCESS FOR CONTINUOUS FOAM EXTRUSION OF THERMOPLASTIC POLYMERS  
VIA SYNTACTIC AND CHEMICAL FOAMING AGENTS

TO ALL WHOM IT MAY CONCERN:

BE IT KNOWN THAT (1) DONALD V. BEAUREGARD, employee of the United States Government of America and citizen of United States of America (2) NICK R. SCHOTT, (3) STEPHEN A. ORROTH, (4) LAWRENCE J. TRAINER, (5) JUDITH A.H. JONES AND (6) ROBERT J. REEDER, citizens of the United States of America, residents of (1) Jamestown, County of Newport, State of Rhode Island, (2) Westford, County of Middlesex, Commonwealth of Massachusetts (3) Windham, County of Rockingham, State of New Hampshire, (4) Miami Lakes, County of Dade, State of Florida, (5) Amherst, County of Hillsborough, State of New Hampshire, and (6) Waltham, County of Middlesex, Commonwealth of Massachusetts, have invented certain new and useful improvements entitled as set forth above of which the following is a specification:

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PATENT TRADEMARK OFFICE

2  
3 PROCESS FOR CONTINUOUS FOAM EXTRUSION OF THERMOPLASTIC POLYMERS  
4 VIA SYNTACTIC AND CHEMICAL FOAMING AGENTS

5  
6 STATEMENT OF GOVERNMENT INTEREST

7 The invention described herein may be manufactured and used  
8 by or for the Government of the United States of America for  
9 governmental purposes without the payment of any royalties  
10 thereon or therefor.

11  
12 CROSS REFERENCE TO OTHER PATENT APPLICATIONS

13 Not applicable.

14  
15 BACKGROUND OF THE INVENTION

16 (1) Field of the Invention

17 The present invention relates to plastic compositions and  
18 processes for producing plastic compositions and more  
19 particularly to foam extruded thermoplastic compositions for use  
20 as insulators in electrical conductors, cables and conductors and  
21 to processes for producing the same.

22 (2) Description of the Prior Art

23 Many naval submarines use a foam jacketed antenna cable made  
24 out of a polyethylene which is chemically foamed during a single  
25 screw extrusion operation. The material has proven to have

1 excellent electrical properties, marginal low density and at high  
2 hydrostatic pressure shows compression set. Efforts have been  
3 made to find improved polymers and blowing agents to obtain an  
4 extrudate with improved properties for use on submarines and for  
5 other uses.

6 The prior art discloses a number of processes relative to  
7 use of syntactic and chemical blowing agents in continuous foam  
8 extrusion.

9 U.S. Patent No. 4,837,251 to Okey et al., for example,  
10 discloses a composition for a pressure-molded core of a composite  
11 structure, including a thermal plastic resin. The composition  
12 also includes a component to reduce the coefficient of thermal  
13 expansion, a lightweight high compressive strength filler and a  
14 blowing agent. The thermoplastic resin may be  
15 polyetheretherketone, the component may be carbon fibers and the  
16 filler may be hollow glass microspheres.

17 U.S. Patent No. 5,120,769 to Dyksterhouse et al. discloses  
18 compositions, which are suitable for the preparation of  
19 thermoplastic syntactic foam intermediate and final products.  
20 These compositions comprise a slurry or putty containing  
21 thermoplastic particles, microballoons and a non-solvent,  
22 optionally in the presence of suitable thickeners, binders and  
23 surfactants. In a preferred embodiment, the composition contains  
24 particles of an engineering thermoplastic having a mean particle  
25 size less than about 100  $\mu\text{m}$ , microballoons, water as the non-

1 solvent and a thickener/binder which is a lightly crosslinked  
2 polyacrylic acid.

3 U.S. Patent No. 5,122,316 to Saatchi et al. discloses a  
4 process using high temperature thermoplastic polymers in the in-  
5 situ fabrication in the formation of foamed composite sandwich or  
6 foam articles often resulting in weak unsound products, which may  
7 be avoided by utilizing a high temperature thermoplastic in  
8 powder form, a blowing agent having a high decomposition  
9 temperature, and, if desired, reinforcers and/or fillers, mixing  
10 the thermoplastic, blowing agent and reinforcer and fillers,  
11 placing the mixture in a mold and if forming a composite  
12 structure, in abutment with at least one skin and applying  
13 sufficient heat and/or pressure to the mold and its contents to  
14 melt the thermoplastic and generate gas within said mixture by  
15 decomposition of the blowing agent. Also, an activator may be  
16 included with the blowing agent, which promotes the production of  
17 gas. The thermoplastic should be free from any material, which  
18 will react with the blowing agent or the activator at  
19 temperatures below the melting point of the thermoplastic.

20 U.S. Patent No. 5,174,932 to Saatchi discloses a process  
21 using high temperature thermoplastic polymers in the in-situ  
22 fabrication in the formation of foamed composite sandwich or foam  
23 articles often resulting in weak unsound products, which may be  
24 avoided by utilizing a high temperature thermoplastic in powder  
25 form, a blowing agent having a high decomposition temperature,

---

1 and, if desired, reinforcers and/or fillers, admixing the  
2 thermoplastic, blowing agent and reinforcer and fillers, placing  
3 the mixture in a mold and, if forming a composite structure, in  
4 abutment with at least one skin, compacting the contents of the  
5 mold, and applying sufficient heat and/or pressure to the mold  
6 and its contents to melt the thermoplastic and generate gas  
7 within said mixture by decomposition of the blowing agent. Also,  
8 an activator may be included with the blowing agent, which  
9 promotes the production of gas. It is disclosed that the  
10 thermoplastic should be free from any material, which will react  
11 with the blowing agent or the activator at temperatures below the  
12 melting point of the thermoplastic. Articles made by the process  
13 are also disclosed.

14 U.S. Patent No. 5,401,785 to Kumagai et al. discloses a  
15 process of obtaining foamed polyurethanes substantially free from  
16 non-uniform density distribution by dispersing an inert gas with  
17 mechanical stirring into a foamed polyurethane-forming  
18 composition containing substantially no blowing agent and  
19 comprising (1) an organic polyisocyanate component, (2) a polyol  
20 component comprising a high molecular weight polyol (A1) and a  
21 low molecular weight polyol (A2), (3) a dehydrating agent (B) and  
22 optionally organic microballoons, and curing the resulting  
23 composition containing therein the inert gas substantially  
24 homogeneously distributed. It is disclosed that foamed

1 polyurethanes thus obtained are lightweight and of reduced  
2 warpage after processing and are suitable for model materials.

3 U.S. Patent No. 5,691,390 to Harrison et al. discloses a  
4 low-density, porous material prepared by mixing together  
5 microballoons and an oligomeric precursor to a polyesterimide  
6 polymer. The oligomeric precursor has an initial viscosity  
7 sufficiently low that it can flow and wet the microballoons when  
8 first heated to a polymerization processing temperature, and  
9 thereafter polymerize. It is disclosed that fibers may be  
10 controllably incorporated into the material during processing to  
11 impart specific properties, and air may be controllably  
12 incorporated into the material during processing to further  
13 decrease its density.

14 U.S. Patent No. 5,783,272 to Wong discloses a thin, tacky,  
15 non-pourable in-situ expandable thermoplastic particles and  
16 thermosettable matrix resin that contains an essentially uniform  
17 density and thickness across the breadth of the film. The in-  
18 situ expandable mass is not pourable yet can be easily dispensed  
19 in a uniform manner within a mold and thereafter expanded to the  
20 dimensions of the mold. Composites and reinforced compositions,  
21 as well as methods of molding are disclosed.

22 U.S. Patent No. 5,804,762 to Jones et al. discloses an  
23 electromagnetic interference (EMI) shielding gasket for mounting  
24 on a substrate having a surface. The gasket is formed of a  
25 resilient, elongated core member extending along a central

1 longitudinal axis and having an outer circumferential surface  
2 defining a cross sectional profile, and an electrically-  
3 conductive outer member having an inner and an outer surface and  
4 extending from a first distal end to a sheathing portion. The  
5 sheathing portion of the outer member covers a portion of the  
6 circumferential surface of the core member and extends from a  
7 first proximal end to a second proximal end. The first distal  
8 end of the outer member and the first proximal end of the  
9 sheathing portion thereof define a first inner shear surface  
10 therebetween, which is attachable to the substrate. The  
11 uncovered portion of the circumferential surface of the core  
12 member defines an interface surface for disposition on the  
13 surface of the substrate.

14 U.S. Patent No. 6,074,475 to Harrision et al. discloses low-  
15 density, syntactic foam, which is prepared by mixing together a  
16 plurality of microballoons and a finely divided solid  
17 thermosetting resin. Fibers are also preferably incorporated  
18 into the material during processing to impart specific  
19 properties. The mixture is heated to allow the thermosetting  
20 resin to flow and wet the microballoons in the mixture. The  
21 mixture is then cured to set and cross-link the thermosetting  
22 resin to form the syntactic foam of the invention. It is also  
23 disclosed that the syntactic foam material has highly uniform  
24 properties and can be used in aerospace applications.



1 U.S. Patent No. 6,075,205 to Zhang discloses an EMI  
2 shielding and environmental sealing gasket for interposition  
3 between a first substrate and an oppositely disposed second  
4 substrate. The gasket is formed of a resilient, tubular body  
5 having a generally continuous interior and exterior surface  
6 defining a wall thickness of the gasket therebetween, and  
7 including base, arcuate and lateral members. The base member  
8 extends intermediate a first and a second edge and has an inner  
9 and outer for contact with the second substrate. The arcuate  
10 member, which has an inner surface spaced apart radially from the  
11 inner surface of the base member and an outer surface for contact  
12 with the first substrate, extends intermediate a first proximal  
13 end disposed radially inwardly of the first edge of the base  
14 member, and a second proximal end disposed radially inwardly of  
15 the second edge of the base member. A first lateral member  
16 extends from the first edge of the base member to the first  
17 proximal end of the arcuate member, with a second lateral member  
18 extending from the second edge of the base member to the second  
19 proximal end of the arcuate member. Each of the lateral members  
20 has an outer surface and an inner surface, which defines an acute  
21 angle with the inner surface of the base member. It is disclosed  
22 that the gasket so constructed is deflectable under a  
23 predetermined compressive force between the first and second  
24 substrates into a collapsed orientation characterized in that

1 substantially continuous contact is maintained between the outer  
2 surface of the base member and the second substrate.

3 A need still exists for an improved process for producing a  
4 buoyant electrical insulative material with good mechanical  
5 cushioning properties.

6

7

#### SUMMARY OF THE INVENTION

8

9 It is an object of the present invention to provide a  
10 process to continuously extrude a low density closed cell foam  
11 using thermoplastic polymers and syntactic polymeric  
12 microballoons, which will physically expand during processing, in  
13 combination with chemical blowing agents.

14

15 It is a further object of the present invention to provide a  
16 closed cell foam extrudate with a density below  $0.5 \text{ g/cm}^3$ , low  
17 moisture absorption, good low temperature flexibility, good skin  
18 surface, controlled foaming, good compressive strength, low  
19 compression set and good electrical and mechanical properties as  
20 defined for the application of a submarine antenna cable jacket.

21

22 The present invention is a process for producing a foam  
23 electrical insulative material. As a first step, a composition  
24 is provided, which is a thermoplastic polymer resin selected from  
25 the group consisting of a polyethylene octene, a polyethylene  
hexene, a polyethylene heptene, a polyethylene nonene and a  
polyethylene decene; a filler selected from the group consisting  
of expandable polymer microballoons and glass or other rigid

1 microspheres; and a blowing agent comprising a physical blowing  
2 agent and a chemical blowing agent, wherein the chemical blowing  
3 agent is selected from one or more of the group consisting of an  
4 exothermic blowing agent and an endothermic blowing agent. This  
5 composition is then continuously foam extruded.

#### 7 BRIEF DESCRIPTION OF THE DRAWINGS

8 Other objects, features and advantages of the present  
9 invention will become apparent upon reference to the following  
10 description of the preferred embodiments and to the drawings,  
11 wherein corresponding reference characters indicate corresponding  
12 parts in the drawings and wherein:

13 FIG. 1 is a schematic drawing on the apparatus by means of  
14 which a preferred embodiment is the method of the present  
15 invention may be carried out.

#### 17 DESCRIPTION OF THE PREFERRED EMBODIMENT

18 It has been found that the combination of metallocene  
19 catalyzed polyolefins, expandable acrylic based microballoons  
20 with a physical blowing agent and exothermic or endothermic  
21 chemical blowing agent (CBA) or a combination of exothermic and  
22 endothermic CBAs produced the desired density reduction during  
23 extrusion as the melt exited the die. Preferably the process is  
24 a single step, continuous extrusion foaming process that may be  
25 performed with or without a breaker plate.

1 The preferred polymeric resin used in the invention is  
2 polyethylene 1-octene. Typical commercial grades of this polymer  
3 are ENGAGE 8100, which is commercially available from Dupont-Dow  
4 or AFFINITY EG8100, which is commercially available from Dow  
5 Chemical. EXPANCEL 092-120, which is commercially available from  
6 AKZO NOBEL may be used as the acrylic expandable syntactic foaming  
7 agent. Alternatively, the resin may be any polyethylene octene,  
8 polyethylene hexene, polyethylene heptene, polyethylene nonene and  
9 polyethylene decene. Preferably the resin will have a density of  
10 from about  $.75 \text{ g/cm}^3$  to about  $1.5 \text{ g/cm}^3$ . Alternatively, rigid  
11 hollow microspheres may be used, which may be glass microspheres  
12 that are commercially available from 3M under the trade  
13 name/product number Scotchlite S60. Other suitable rigid  
14 microspheres are none. The endothermic chemical foaming agent  
15 used was SAFOAM FP, which is commercially available from Reedy  
16 International and the exothermic chemical foaming agent used was  
17 CELOGEN AZ (azodicarbonamide), which is commercially available  
18 from Unroyal Chemical Division. These foaming agents are typical  
19 of their classification and other commercially available chemical  
20 foaming agents could be used in their place. A typical  
21 formulation is presented in Table 1.

Table 1: Typical Formulation

Component	Percentage Loading
Polyethylene 1-octene	88-97%
Expandable Acrylic Microballoon	3-10%
Exothermic CBA	0-1%
Endothermic CBA	0-1%

Referring to FIG. 1, the apparatus by means of which the method of the present invention may be practiced includes a gravity fed hopper 10 into which the resin, filler and blowing agent are initially added. The mixture is then metered into an extruder 12, which is made up of a barrel 14 with a single screw 16. The extruder 12 also has a breaker plate 18 and then a die 20 at its terminal end. A hot extrudate 22 leaves the die 20 into a reservoir 24 having copper heating coils 26, which are contained in water bath 28. Cooled extrudate 30 leaves the water bath 28 and enters roller apparatus 32. Roller apparatus 32 includes an upper section 34, which is comprised of roll 36 and roll 38 and continuous belt 40. The roller apparatus 32 also includes a lower section 42. Lower section 42 includes a roll 44 and a roll 46 and a continuous belt 48. The upper section 34 is superimposed in spaced relation over the lower section 42. The cooled extrudate 30 passes between upper section 34 and lower section 42 of the roller apparatus 32 and emerges a completed rolled extrudate 50. Both the resin and the blowing agents are preblended to be fed by gravity in the hopper 10 via single screw extrusion. The

1 extruder 12 has a water jacket around the feed throat and the  
2 barrel 14 is divided into several zones to heat the polymer as it  
3 progresses to the die 20. The temperature of the melt is  
4 increased so that the resin melted is plasticated and the  
5 chemical blowing agent is decomposed as the melt travels to the  
6 die 20. As the melt temperature increases the physical blowing  
7 agent also causes an expansion of the acrylic microballoons  
8 (syntactic foam portion). Conditions in the extruder 12 are  
9 regulated, i.e., melt temperature, pressure, shear rate,  
10 residence time so as to produce a low-density foam as the melt  
11 exits the die 20. Typical processing conditions are shown in  
12 Table 2. These processing conditions are presented for an  
13 extruder 12 with three heating zones, one gate-heating zone and  
14 two die heating zones. The invention is not limited to this many  
15 heating zones and the foaming process may be performed on  
16 extruders with a different number of barrel, gate and die heating  
17 zones. Head pressure developed is largely dependent on screw  
18 speed, melt viscosity, die design and the use of breaker plate.  
19 Due to the wide variation in variables that effect head pressure,  
20 a very wide range of possible head pressures is presented in  
21 Table 2.

1 Table 2: Typical Processing Conditions

2

Processing Parameter	Setting
Barrel Zone 1	150°C - 170°C
Barrel Zone 1	165°C - 185°C
Barrel Zone 1	165°C - 185°C
Gate Zone	165°C - 185°C
Die Zone 1	180°C - 200°C
Die Zone 2	180°C - 200°C
Screw Speed	10-50 RPM
Head Pressure	2-14 MPa

3

4 (the screw speed and screw design). The shear rate and residence  
 5 time in the extruder 12 depend upon the invention using both a  
 6 24:1 and 30:1 L/D extruders 12. The screws 16 used possessed  
 7 compression ratios of 2.5-3:1. All screws 16 were single stage  
 8 screws with approximately one-third of the screw 16 comprising the  
 9 feed section, one-third of the screw 16 comprising the transition  
 10 and one-third of the screw 16 comprising the metering section of  
 11 the screw. Screws 16 with a Maddock mixing section and screws 16  
 12 with a Pulsar mixing section were used in the development of the  
 13 invention. The die design was adjusted so that melt fracture was  
 14 minimal. This is done via correct design of the die land. Since  
 15 the viscosity of the melt decreases with increased temperature,  
 16 the melt temperature has to stay below a certain limit.

17 The melt extrudate 22 is passed through a water bath 28,  
 18 which has copper tubes 26 to heat the water to an elevated  
 19 temperature. A set of foamed rubber pull rolls 32 continuously  
 20 pulled the extrudate 22 through the bath 28. The haul off speed

1 in combination with the extruder screw speed and process  
2 conditions (melt temperatures, viscosity, melt pressure)  
3 determines the outside diameter, extrudate foam density and  
4 surface roughness. (Typically an optimum condition where low  
5 density and good skin quality are obtained can be found.)  
6

7 Example 1: Acrylic Microballoons

8 95.4g of polyethylene 1-octene resin commercially  
9 obtained from Dow Chemical (supplier) under the trade  
10 name/product number Affinity EG 8100 is mixed with 4.6g of  
11 expandable acrylic microballoons commercially obtained from Akzo-  
12 Nobel (supplier) under the trade name/product number Expancel 092  
13 MB 120 in the gravimetric hopper 10 of a single screw extruder  
14 12. The acrylic balloons contain a hydrocarbon gas (a physical  
15 blowing agent). The mixture is then processed in the extruder  
16 under the following temperature conditions: 250°F, 280°F, 300°F  
17 and 320°F in the four barrel zones, 320°F in the die zones.  
18 Screw speed of 20 rpm. The resulting exudate 50 should have a  
19 density of lower than 0.5g/cc and pressure conditions.  
20

21 Example 2: Acrylic Microballoons with an Exothermic CBA

22 96.4g of polyethylene 1-octene resin commercially obtained  
23 from Dow Chemical (supplier) under the trade name/product number  
24 Affinity EG 8100 is mixed with 3.1g of expandable acrylic  
25 microballoons in a masterbatch commercially obtained from Akzo-



1 Nobel (supplier) under the trade name/product number Expancel 092  
2 MB 120 in the gravimetric hopper 10 of a single screw extruder  
3 12. Also included in the mixture is 0.5g of Azodicarbonate  
4 commercially obtained from Uniroyal Chemical Co. (supplier) under  
5 trade name/product number Celogen AZ. The mixture is then  
6 processed in the extruder 12 under the following temperature:  
7 250°F, 280°F, 300°F and 320°F in the four barrel zones, 250°F in  
8 the die zones. Screw speed of 20 rpm. The resulting exudate 50  
9 should have a density of lower than 0.5g/cc.

10

11 Example 3: Acrylic Microballoons with an Endothermic CBA

12 96.4g of polyethylene 1-octene resin commercially obtained  
13 from Dow Chemical (supplier) under the trade name/product number  
14 Affinity EG 8100 is mixed with 3.1g of expandable acrylic  
15 microballoons in a masterbatch commercially obtained from Akzo-  
16 Nobel (supplier) under the trade name/product number Expancel 092  
17 MB 120 in the gravimetric hopper 10 of a single screw extruder  
18 12. The acrylic microballoons contain a hydrocarbon gas (a  
19 physical blowing agent). Also included in the mixture is 0.75g  
20 of Safoam FP commercially obtained from Reedy International  
21 (supplier). The mixture is then processed in the extruder 12  
22 under the following temperature conditions: 250°F, 280°F, 300°F  
23 and 320°F in the four barrel zones, 300°F in the die zones.  
24 Screw speed of 20 rpm. The resulting exudate 50 should have a  
25 density of lower than 0.5g/cc.

1 Example 4: Acrylic Microballoons with an Endothermic CBA

2 96.4g of polyethylene 1-octene resin commercially obtained  
3 from Dow Chemical (supplier) under the trade name/product number  
4 Affinity EG 8100 is mixed with 3.1g of expandable acrylic  
5 microballoons in a masterbatch commercially obtained from Akzo-  
6 Nobel (supplier) under the trade name/product number Expancel 092  
7 MB 120 in the gravimetric hopper 10 of a single screw extruder  
8 12. The acrylic microballoons contain a hydrocarbon gas (a  
9 physical blowing agent). Also included in the mixture is 0.5g of  
10 Azodicarbonamide commercially obtained from Uniroyal Chemical Co.  
11 (supplier) under the trade name/product number Celogen AZ znd  
12 0.75g of Safoam FP commercially obtained from Reedy International  
13 (supplier). The mixture is then processed in the extruder 12  
14 under the following temperature conditions: 250°F, 280°F, 300°F  
15 and 320°F in the four barrel zones, 250°F in the die zones.  
16 Screw speed of 20 rpm. The resulting exudate 50 should have a  
17 density of lower than 0.5g/cc.

18 Example 5: Acrylic Microballoons in A pre-compounded foam  
19 grade of LDPE 96.15g of DFD 4960, a pre-compounded foaming grade  
20 of LDPE, commercially obtained from Union Carbide (supplier) is  
21 mixed with 3.1g of expandable acrylic microballoons in a  
22 masterbatch commercially obtained from Akzo-Nobel (supplier)  
23 under the trade name/product number Expancel 092 MB 120 in the  
24 gravimetric hopper 10 of a single screw extruder 12. The acrylic  
25 microballoons contain a hydrocarbon gas (a physical blowing

1 agent). The mixture is then processed in the extruder 12 under  
2 the following temperature conditions: 200°F, 250°F, 260°F and  
3 275°F in the four barrel zones, 250°F in the die zones. Screw  
4 speed of 20 rpm. The resulting exudate 50 should have a density  
5 of lower than 0.5g/cc.

6 For the purposes of this disclosure, the term "foam  
7 extruding" refers to any extrusion process in which inert gases  
8 in the materials being processed are allowed to expand to form a  
9 cellular polymeric material after the material being processed is  
10 discharged from a pressurized extruder.

11 For the purposes of this disclosure, a "physical blowing  
12 agent" is any material used in a foam extrusion process which  
13 produces an inert gas as a result of a physical change of state  
14 in that material to form a cellular polymeric material. A non-  
15 limiting example of the same would include low boiling point  
16 liquid organic materials such as isopentene.

17 For the purpose of this disclosure, a "chemical blowing  
18 agent" is any material used in a foam extrusion process, which  
19 produces an inert gas as a result of a chemical change in that  
20 material to form a cellular polymeric material. A non-limiting  
21 example of the same would includes azodicarbonamide.

22 For the purpose of this disclosure, an "expandable  
23 microballoon" refers to any hollow particle comprised of a  
24 polymeric or other flexible or expandable material. While such  
25 particles are often spherical in shape, particles of other

1 shapes, which may have these characteristics, are also intended  
2 to be encompassed within this definition.

3 For the purpose of this disclosure, a "rigid microsphere" is  
4 any hollow particle, which is comprised of a rigid exterior.  
5 While such particles are often glass and spherical in shape,  
6 hollow particles comprised of other rigid material and having  
7 other shapes are also intended to be encompassed within this  
8 definition.

9 It will be appreciated that a process for making a buoyant  
10 closed cell foam extrudate polymeric material having a density  
11 below  $0.5 \text{ g/cm}^3$ , low water absorption, low compression set, with  
12 excellent electrical insulating and cushioning properties has  
13 been described.

14 While the present invention has been described in connection  
15 with the preferred embodiments of the various figures, it is to  
16 be understood that other similar embodiments may be used or  
17 modifications and additions may be made to the described  
18 embodiment for performing the same function of the present  
19 invention without deviating therefrom. Therefore, the present  
20 invention should not be limited to any single embodiment, but  
21 rather construed in breadth and scope in accordance with the  
22 recitation of the appended claims.

2

3 PROCESS FOR CONTINUOUS FOAM EXTRUSION OF THERMOPLASTIC POLYMERS  
4 VIA SYNTACTIC AND CHEMICAL FOAMING AGENTS

5

6 ABSTRACT OF THE DISCLOSURE

7 A process for producing an electrical insulative material.  
8 First there is produced a composition including a thermoplastic  
9 polymer resin selected from the group consisting of a polyethylene  
10 octene, a polyethylene hexene, a polyethylene heptene, a  
11 polyethylene nonene and a polyethylene decene; a filler selected  
12 from the group consisting of expandable polymer microballoons and  
13 glass microspheres; and a blowing agent comprising a physical  
14 blowing agent and a chemical blowing agent. The chemical-blowing  
15 agent is selected from one or more of the group consisting of an  
16 exothermic blowing agent and an endothermic blowing agent. This  
17 composition is then continuously foam extruded.

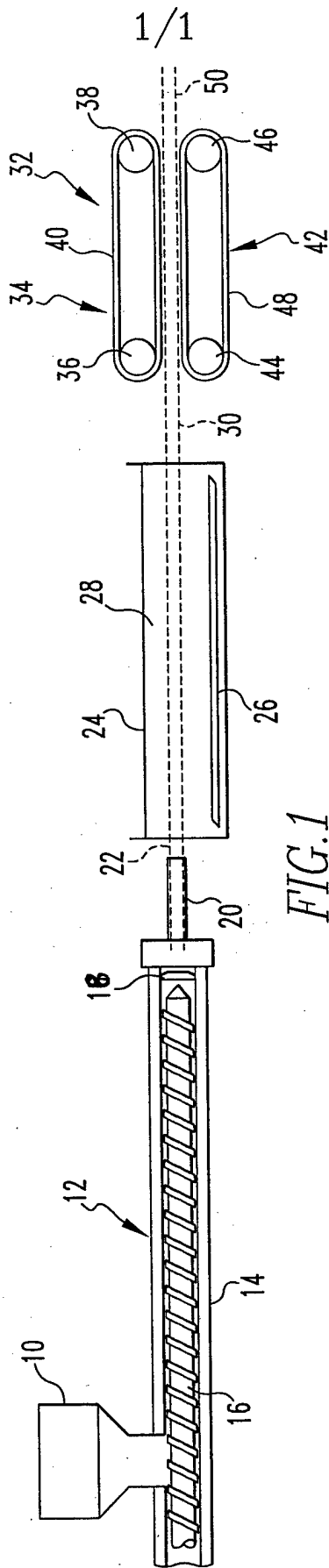


FIG. 1