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SONAR DISPLAY SYSTEM AND METHOD

TO ALL WHOM IT MAY CONCERN:

BE IT KNOWN THAT (1) G. CLIFFORD CARTER and (2) WILLAM A. STRUZINSKI, citizens of the United States of America, employees of the United States Government, resident of (1) Waterford, County of New London, State of Connecticut, and (2) New London, County of New London, State of Connecticut, have invented certain new and useful improvements entitled as set forth above of which the following is a specification.

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1 Attorney Docket No. 79915

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SONAR DISPLAY SYSTEM AND METHOD

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STATEMENT OF THE GOVERNMENT INTEREST

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The invention described herein may be manufactured and used
7 by or for the Government of the United States of America for
8 Governmental purposes without the payment of any royalties
9 thereon or therefore.

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CROSS REFERENCE TO RELATED PATENT APPLICATIONS

12

Not applicable.

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14

BACKGROUND OF THE INVENTION

15 (1) Field of the Invention

16 The present invention relates generally to sonar displays
17 and, more particularly, to a system and method suitable for
18 displaying the outputs of multiple broadband processors with
19 different detection algorithms whereby each multiple broadband
20 processor operates on N-channels of sonar data from a towed
21 array.

1 (2) Description of the Prior Art

2 It is well known that submarines and other vessels may
3 utilize different types of towed arrays of sonar sensors for
4 receiving sonar data. The towed array may typically have some
5 number, N , of channels wherein the number of channels is
6 typically related to the number of sonar detectors in the array.
7 For instance, there may be one channel output for each acoustic
8 sensor input to provide for conservation of energy with respect
9 to each sensor. Each channel output may typically be considered
10 as a beam "pointed to" a particular listening direction. With
11 fewer beam outputs, information is lost. With more beams, the
12 outputs are merely interpolated values of the input set. So if,
13 for example, there are $N=10$ sensor inputs, then there may be
14 $N=10$ independent beam outputs steered in $N=10$ different
15 directions.

16 The information is processed to determine various
17 attributes of targets. For instance, bearing is a measure (as a
18 function of time) of the angle to the target (or acoustic
19 source) relative to true North or relative to the direction of
20 the ship's heading. Bearing rate is the rate of change of the
21 bearing with respect to time. High bearing rate contacts are
22 close to the array and tend to be relatively easy to spot. With
23 respect to relative bearings, low bearing rate contacts tend to

1 fall into one of three categories: opening away, running on
2 parallel velocity, or on a collision course.

3 For processing the data received by the particular type of
4 towed sonar array, different types of broadband detection
5 processing schemes may be used. Each type of broadband
6 detection processing scheme will typically have different
7 advantages and disadvantages depending on the particular type of
8 scenario of use. However, in the past, the output of each
9 broadband detection processing scheme has required a separate
10 display format. Due to the difficulty of viewing two different
11 displays concurrently or one at a time, it would be desirable to
12 provide a single display, such as a single bearing versus time
13 history display, whereby the relative advantages of each type of
14 detection scheme are built into a single display format.

15 Patents that show attempts to solve the above and other
16 related problems are as follows:

17 U.S. Patent Application No. 5,481,505, issued January 2,
18 1996, to Donald et al., discloses a method and apparatus for
19 detecting, processing and tracking sonar signals to provide
20 bearing, range and depth information that locates an object in
21 three-dimensional underwater space. An inverse beamformer
22 utilizes signals from a towed horizontal array of hydrophones to
23 estimate a bearing to a possible object. A matched field
24 processor receives measured covariance matrix data based upon

1 signals from the hydrophones and signals from a propagation
2 model. An eight nearest neighbor peak picker provides plane
3 wave peaks in response to output beam levels from the matched
4 processor. A five-dimensional M of N tracker identifies peaks
5 within the specified limit of frequency, bearing change over
6 time, range and depth to specify an object as a target and to
7 display its relative range and depth with respect to the array
8 of hydrophones.

9 U.S. 5,251,185, issued October 5, 1993, to P. M.
10 Baggenstoss, discloses an improved sonar signal processor and
11 display combining the use of both coherent and incoherent signal
12 processors. In addition to a conventionally used matched filter
13 detection processor, an incoherent signal processor comprising a
14 cross-range energy filter and a down-range energy filter is
15 used. The cross-range energy filter detects objects
16 characterized by a narrow bearing response; whereas the down-
17 range energy filter detects objects characterized by a narrow
18 range response. The detection events resulting from the
19 incoherent signal processor are displayed in a subdued color to
20 prevent distraction from the primary display events and to
21 reduce the false alarm rate by allowing the sonar operator to
22 view events in the context of natural boundaries.

23 U.S. Patent No. 5,216,640, issued June 1, 1993, to Donald
24 et al., discloses an apparatus and method for detecting,

1 processing, and tracking sonar signals. Plane wave energy from
2 the sonar signal source is measured at multiple points using an
3 array of plane wave energy receptors. These measurements are
4 processed using an inverse beamformer to generate output beam
5 levels. These output beam levels are then processed using the
6 spectrum normalizer to yield spatially and spectrally normalized
7 output beam levels. The normalized beam levels are then
8 processed using an eight nearest-neighbor peak-picker to provide
9 plane wave peaks. Finally, the plane wave peaks are processed
10 by a three-dimensioned M of N tracker to identify peaks within a
11 specified limit of frequency and angle change over time. The
12 identified peaks may be displaced or recorded for further
13 analysis.

14 U.S. Patent No. 5,058,081, issued October 15, 1991, to
15 Gulli et al., discloses a method of formation of channels for a
16 sonar after being sampled at a frequency $T=1/4f_0$ (where f_0 is the
17 receiving center frequency of the sonar) the signals from the
18 hydrophones of the sonar and having translated them to baseband,
19 the signals thus translated are subsampled with a period $T_{SE} = kT$
20 (wherein k is an integer) substantially equal to $1.25 B$, where B
21 is the reception bandwidth of the sonar. A first set of signals
22 is subsampled at identical times to form a frontal sector. Two
23 further sets of signals are subsampled with delays between the
24 signals from two adjacent hydrophones equal to T , which

1 determines two side sectors adjacent to the frontal sector. The
2 subsampled signals are then transmitted serially by the towing
3 cable of the sonar device towed array and are processed in FFT
4 circuits which allow to form in each sector a set of channels
5 covering the sector. This allows to considerably reduce the
6 data transmission rate between the towed portion of the sonar
7 and the portion located in the towing ship.

8 U.S. Patent No. 4,935,748, issued June 19, 1990, to Schmidt
9 et al., discloses a blast recorder and method for monitoring and
10 processing vibrations from blasts, and for displaying the
11 results in a nearly real time basis and in a manner which is
12 easily interpreted by a relatively unskilled field worker and
13 corresponds to a form which closely correspond to the real
14 damage causing aspect of the blast than heretofore. The
15 invention operates by receiving seismic energy signals from a
16 blast sensor, processing the energy signals to obtain velocity
17 signals relating to said blast, filtering either the energy
18 signals prior to, or the velocity signals following said
19 processing step, into high and low frequency bands, to obtain
20 high and low band velocity signals, integrating over the period
21 of the blast the high and low band velocity signals to obtain
22 high and low band displacement signals, determining the peak
23 velocity signal in each band, over the period of the blast, and
24 displaying one or all of the peak of the velocity signal

determined in the high frequency band, the peak of the velocity signal determined in the low frequency band, and the displacement signal related to the low frequency band.

U.S. Patent No. 3,713,087, issued January 23, 1973, to Bauer et al., discloses an acoustical detection apparatus for determining the direction of origin of sounds. A first acoustic receiving system having a relatively high uniform sensitivity in a predetermined plane and a relatively low sensitivity in and about the direction perpendicular to the plane is provided. A second acoustic receiving system having a spherical sensitivity pattern is also provided. The sensitivity of the second system is set substantially equal to the sensitivity of the first system in the predetermined plane. Means are provided for comparing the outputs of the first and second systems, the ratio of these outputs indicating the direction from which received sounds are arriving. In a preferred embodiment, of the invention, the first acoustic receiving system has a donut-shaped reception characteristic.

The above cited prior art which does not show a suitable means for combining the results of multiple broadband detection processing schemes to thereby produce a single display wherein the advantages of each type of broadband detection scheme are incorporated without the need for viewing multiple displays concurrently or consecutively. Those skilled in the art will

1 appreciate the present invention that addresses the above and
2 other problems.

4 SUMMARY OF THE INVENTION

5 Accordingly, it is an object of the present invention to
6 provide an improved sonar system and method.

7 It is another object of the present invention to provide a
8 system with one or more processes for combining the outputs from
9 multiple broadband detection schemes.

10 It is yet another object of the present invention to
11 provide a sonar operator with a single bearing versus time
12 history display which is based on the outputs of two passive
13 broadband detectors.

14 An advantage of a system in accord with the present
15 invention is that it is less likely to miss an acoustic contact.

16 A feature of the present invention, in one embodiment, is
17 the use of at least two detectors operating on data supplied
18 through each sonar data channel to effectively split the data
19 path whereby the data is processed in several ways
20 simultaneously and subsequently recombined into one data path.

21 These and other objects, features, and advantages of the
22 present invention will become apparent from the drawings, the
23 descriptions given herein, and the appended claims. It will be
24 understood that above listed objects and advantages of the

1 invention are intended only as an aid in understanding aspects
2 of the invention, are not intended to limit the invention in any
3 way, and do not form a comprehensive list of objects, features,
4 and advantages.

5 In accordance with the present invention, a system for
6 displaying sonar data is provided which can comprise elements
7 such as a sonar array with a plurality of sonar sensors and a
8 plurality of data channels. The plurality of data channels can
9 be split to form a plurality of first detector channels and a
10 plurality of second detector channels. A plurality of
11 comparators may be utilized for selecting an output from each of
12 the first detector channels and each of the second detectors. A
13 display can be provided for displaying a comparator output for
14 each of the plurality of comparators. The plurality of
15 comparators can in one embodiment each utilize a binary OR
16 operation selecting from the first detector channel and the
17 second detector channels. The OR operation can be of the type
18 which selects a maximum value from each of the first detector
19 channels as compared with each of the second detector channels
20 when the outputs of the detector channels are not strictly
21 binary.

22 The system can further comprise a plurality of first
23 normalizers for the plurality of first detector channels, and a
24 plurality of second normalizers for the plurality of second

1 detector channels. The comparators can be used select a maximum
2 output from the first normalizers as compared to the second
3 normalizers. Preferably, the first detector channels and the
4 second detector channels utilize different types of broadband
5 detection schemes. In a preferred embodiment, each of the first
6 detector channels utilizes a Smooth Coherence Transform (SCOT)
7 processor and each of the second detector channels utilize a
8 Sub-band Peak Energy Detection (SPED) processor. In one
9 embodiment, the display is a bearing versus time history
10 display.

11 A method is also provided for displaying the sonar data
12 which may comprise one or more of the following steps such as
13 processing sonar data through a plurality of data channels,
14 splitting each of the plurality of data channels for processing
15 by at least two different detection processors, recombining each
16 of the split data channels to form a plurality of recombined
17 data channels, and utilizing data from each of the plurality of
18 recombined data channels for a display. The processing may
19 comprise simultaneously utilizing a first detector and a second
20 detector. The step of recombining may further comprise
21 executing a binary OR operation on an output related to the
22 first detector and the second detector to produce a plurality of
23 OR outputs. Other steps may include displaying the plurality of
24 OR outputs on the display and/or scaling the outputs of the

1 first detector and the second detector prior to the step of
2 executing the OR operation.

3 In one particular embodiment of the invention, a SCOT OR
4 SPED (SOS) method is provided for displaying sonar data which
5 may comprise one or more steps such as providing N channels of
6 sonar data, detecting each of the N channels of sonar data with
7 a plurality of SPED detectors, detecting each of the N channels
8 of sonar data with a plurality of SCOT detectors, and producing
9 channels of data for display by performing a binary OR operation
10 between a SPED output for each respective SPED detector and a
11 SCOT output for each respective SCOT detector for each of the N
12 channels of sonar data. Other steps may include scaling and
13 aligning each SPED detector output and each SCOT detector output
14 prior to the step of performing the OR operation. The OR
15 operation may comprise selecting a maximum of the SPED output as
16 compared to the SCOT output. Other steps may include displaying
17 the N channels of data for display in a bearing versus time
18 history display format. Additional or alternative steps may
19 include producing the N-channels of sonar data with a beamformer
20 and applying data from a towed array with a plurality of sonar
21 sensors to the beamformer.

BRIEF DESCRIPTION OF THE DRAWING

A more complete understanding of the invention and many of the attendant advantages thereto will be readily appreciated as the same becomes better understood by reference to the following detailed description when considered in conjunction with the accompanying drawing wherein corresponding reference characters indicate corresponding parts and wherein the FIG. is a block diagram of a sonar processor system that may be used for processing sonar data to provide a sonar display in accord with the present invention.

DESCRIPTION OF THE PREFERRED EMBODIMENT

Presently, two types of passive broadband detection processing schemes are frequently favored for concurrent use in analyzing data from towed sonar arrays. One group of prior art detection processing techniques is referred to as Generalized Cross Correlation (GCC) methods. One type of GCC broadband detection processing is the Smoothed Coherence Transform (SCOT) cross correlation method; however, other types also exist in the prior art. Another group of prior art detection processing techniques are energy detection methods having frequency and time normalizations for display. These methods include the Sub-band Peak Energy Detection (SPED) method and the Sub-band Extrema Energy Detection (SEED) method. These two types of

1 processing, as may presently be used with the invention, are
2 discussed hereinafter in some detail for reference although
3 other types of detectors such as, for instance, other types of
4 broadband detection processing schemes, could also be used.
5 Therefore, the present invention is not limited to use of SCOT
6 processing and SPED processing.

7 Referring now to the FIG., where sonar system 10 in accord
8 with the present invention is shown in a block diagram schematic
9 for receiving signals received typically by reflection from
10 objects in response to a transmitted sonar signal. The received
11 signals are used to provide events or pings for display with
12 such events corresponding to detected objects and providing data
13 related to a range and a bearing of the detected object. Sonar
14 system 10 includes sonar transducer array 12 for receiving the
15 sonar signals. The present invention may be used with different
16 types of sonar transducer arrays which can be towed by vessels
17 such as a submarines and ships. Transducer array 12 is coupled
18 via signal line 14 to beamformer 14. Beamformer 14 provides a
19 plurality of outputs such as outputs 18, 20, and N. Beamformer
20 14 is a well known specialized electronic system that delays or
21 adds the signals from individual hydrophone and provides these
22 converted signals as outputs, such as outputs 18, 20, and N,
23 that are electronically steered to a particular "look"
24 direction. Outputs 18, 20, and N comprise streams of digital

1 data taken at an initial sampling rate. Each output may
2 typically correspond to a beam or lobe characterized by a
3 predetermined interval of ranges and a given bearing.

4 In a preferred embodiment of the present invention, each
5 output or channel, such as channel 18, is split as shown into
6 two paths, such as paths 22 and 24, respectively. The
7 particular inputs used by processors 26 and 28, discussed
8 hereinafter, can be time domain complex full beam data, time
9 domain complex half beam data or the like, if desired. Thus, in
10 the present invention, each channel is processed separately
11 utilizing two different processing schemes. In a preferred
12 embodiment, the combination of SCOT processing and SPED
13 processing is used for processing data from each channel as
14 indicated at 26 and 28. Thus, in the embodiment shown in the
15 FIG., each channel is processed at least twice in a parallel
16 fashion prior to a subsequent recombination as discussed
17 hereinafter. However, it will be understood that additional or
18 different broadband processing schemes can be used such that the
19 present invention can accommodate multiple parallel processing
20 schemes whereby the outputs are then further processed as
21 discussed hereinafter.

22 As indicated above, at least two detection algorithms are
23 normally required because the performance of each algorithm is
24 scenario dependent. For instance, SPED outperforms SCOT for

1 static and low bearing rate targets, but SCOT outperforms SPED
2 for high dynamic targets and two closely spaced targets in
3 bearing. "Low bearing rate" may considered to be a bearing rate
4 at most 6 degrees/minute or otherwise defined. "High bearing
5 rate" may be considered to be a bearing rate at least 12
6 degrees/minute unless otherwise defined. Two targets might be
7 considered closely spaced, as used herein, if they have a
8 bearing separation of no more than two beams. For instance,
9 suppose there are $M=10$ beams over 180 degrees then each beam
10 width is nominally 18 degrees. In this case it may be desirable
11 to resolve targets or acoustic contacts less than, say, for $M =$
12 10, $180/M = 18$ degrees.

13 The SCOT detection scheme and the SPED detection scheme
14 are each preferably displayed in the form of a bearing versus
15 time display. Since the SCOT detector and SPED detector react
16 differently in different scenarios, it is desirable to utilize
17 information from both types of detectors. Therefore, two
18 displays are required in the prior art, one for SCOT and one for
19 SPED. Previously, the sonar operator would need to view either
20 the SCOT display or the SPED display one at a time or both
21 concurrently to determine if targets of interest are present.

22 The particular embodiment of the SCOT processing preferably
23 used with the present invention provides for an input to the
24 SCOT processing which is time domain complex half beam data.

1 The SCOT processing consists, in a preferred embodiment, of
2 eight subfunctions: 1) Fast Fourier Transform (FFT) processing,
3 2) Power Spectrum Estimation, 3) Weight, 4) Cross Spectrum, 5)
4 Time Integration, 6) Complex Multiple, 7) Complex-to-Real
5 Inverse FFT, and 8) Display Cell Interpolation. A description
6 of each subfunction is given.

7 The FFT processing subfunction converts the complex half
8 beam data to the frequency domain. The FFT operation is
9 preferably performed four times for the shortest time update
10 interval, as discussed below.

11 The Power Spectrum Estimation subfunction consists of
12 four steps: 1) Hanning Windowing, 2) Square Law Detector, 3)
13 Sum-and-Dump Integration, and RC Integration. Each of these
14 steps will now be described. A Hanning window is applied to the
15 forward and aft FFT data blocks that were generated in the FFT
16 processing subfunction. The window used is a modified Hanning
17 window that is normalized in power and to compensate for the
18 complex-to-real inverse FFT. A square law detector is then
19 applied to the Hanning windowed FFT data and followed by a sum-
20 and-dump integrator. The square law detector takes the
21 magnitude squared of the data. The data is time averaged (sum-
22 and-dump integrator) to three time update intervals, IT2, IT3,
23 and IT4. These time update intervals are chosen based on the
24 frequencies or frequency range of interest. The RC Integration

1 step is performed only when the sum-and-dump integrated data
2 matures. A recursively smoothed average is calculated using the
3 RC integrator.

4 The next subfunction performed after Power Spectrum
5 Estimation is Weight. This subfunction computes weights using
6 the power spectrum estimates and the low and full band filters.
7 The weights are computed for the IT2, IT3, and IT4 integration
8 times. The Cross Spectrum subfunction performs the conjugate
9 multiplication of the forward and aft half beam pairs. The Time
10 integration subfunction time averages the normalized cross
11 spectrum estimates to the IT2, IT3, and IT4 data rates. The
12 Complex Multiple subfunction applies the weights calculated in
13 the Weight subfunction to the cross spectrum data from the Cross
14 Spectrum subfunction. The next subfunction is Complex-to-Real
15 Inverse FFT, which converts the normalized complex cross
16 spectrum back to the lag domain for display cell interpolation
17 processing. The final subfunction is Display Cell
18 Interpolation. Time delays corresponding to each of the display
19 cells are computed based upon the speed and sound and phase
20 center displacement values. Then interpolation in beam space
21 and lag domain is performed. The output of the SCOT processing
22 26 is applied to scale and align element 30 as discussed
23 subsequently. The output may comprise some discrete number of
24 bearing cells, say for instance 401.

1 The particular embodiment of the SPED processing as used in
2 accord with the present invention preferably has inputs at 24
3 comprised of time domain full beam data. The SPED processing as
4 preferably used herein may consist of nine subfunctions: 1) Time
5 Domain Weighting such as Hanning (or Hamming, triangular, etc.),
6 2) Fast Fourier Transform (FFT) Processing, 3) Frequency Bin
7 Selection, 4) Magnitude Squared Detection, 5) Time Integration,
8 6) Noise Power Estimation, 7) Azimuthal Peak Detection and Fine
9 Bearing Calculation, 8) Peak Integration, and 9) Azimuthal
10 Smoothing. Describing each subfunction in more detail, a
11 Hanning window may be applied to the 50% (or variable depending
12 on processing power available and weighting/window selected)
13 overlapped complex time series beam data. FFTs are performed at
14 the IT2 data rate using the Hanning windowed data. A total of N
15 beams by some number of frequency bins (~1024) are produced. In
16 order to decrease the number of computations through the rest of
17 the processing, frequencies outside a selected frequency range
18 of interest are dropped from processing. The output of
19 Frequency Bin selection subfunction is N beams by some number of
20 bins (~720 IT2 FFT data). Each beam's frequency spectrum is
21 then magnitude-squared bin by bin for IT2 truncation frequency
22 spectra. The IT2 squared magnitude data are time averaged to
23 the IT3 ($IT3=4*IT2$) and IT4 ($IT4=3*IT3$) data rates. The
24 integrators are sum-and-dump integrators. The next subfunction

1 performed is Noise Power Estimation. This subfunction consists
2 of three steps: 1) Time Smoothing, 2) Tone Removal, and 3) Quiet
3 Beam Selection. The Time Smoothing step obtains a mean for each
4 beam and bin by computing a running average of the most recent
5 12 IT2 samples. If the current time cycle is IT4, the IT4 data
6 is used as the time average. The Tone Removal step obtains a
7 noise mean estimate for each beam by using the split two pass
8 mean normalizer algorithm. At each frequency, the second
9 quietest beam within a specified azimuthal sector is selected as
10 representative of the noise at the center of the sector. The
11 next subfunction performed after Noise Power Estimation is Peak
12 Detection and Fine Bearing Calculation. For each frequency bin,
13 if the amplitude is greater than the corresponding bin in each
14 of the adjacent beams, then that frequency bin is considered the
15 peak. The bearing is then computed for each peak using a
16 parabolic fit. The subfunction is performed for the IT2, IT3,
17 and IT4 data. The Peak Integration subfunction takes the IT2,
18 IT3, and IT4 data from the Peak Detection and fine Bearing
19 Calculation subfunction and integrates it across the frequency.
20 Prior to integration, the data are normalized by the squared of
21 the noise value from the second quietest beam. The last
22 subfunction is Azimuthal (i.e., bearing) Smoothing. This
23 subfunction is performed on the integrated data by sliding an
24 averaging window over the azimuthal cells. The output of the

1 SPED processing is estimated power as a function bearing for
2 some discrete number of bearing cells, say for instance 401, of
3 smoothed data. This process is repeated as time progresses.

4 Output from SPED processing 30 is also applied to a scale
5 and align section such section 32. The outputs of the SCOT 32
6 (or other Generalized Cross Correlation, GCC, function) are a
7 function of delay and have a wide range of amplitudes. Unlike
8 the normalized cross correlation function which goes between
9 minus unity and plus unity, the GCC functions like the SCOT can
10 have larger extremes. On the other hand the SPED (and its
11 variant the SEED) can have different extremes. Also the SPED
12 (or SEED) are a function of bearing (which is related to delay
13 by a cosine trigonometric function). Scale and align 30
14 converts the SCOT processing output to the same abscissa as the
15 SPED. Then both outputs are delay or both outputs are bearing.
16 Scaling as indicated at 30 and 32, is an attempt to have a
17 common or consistent amplitude normalization. One possible
18 method for achieving this purpose, for example only, might be to
19 normalize each scan so that the maximum was unity and the
20 minimum was zero. However, it will be understood that there
21 are a variety of possible methods of normalizing, including
22 single pass and multi-pass sector space averagers.

23 Outputs 36 and 38 for Scale and Align elements 30 and 32
24 are applied to select element 34 which preferably performs a

1 comparing and selecting function. In select element 34, a
2 selection is made from outputs 36 and 38 to determine how data
3 from outputs 36 and 38 will be displayed. In a preferred
4 embodiment, the desired scaled and aligned output 36 of SCOT 26
5 and the scaled and aligned output 38 of SPED 28 are selected
6 through the process of being OR-ed together for each channel.
7 OR-ing, as used herein, is preferably the process of selecting
8 the maximum in select 34 for each of the channels. In this
9 example, the maximum will be the maximum of outputs 36 and 38
10 for each channel. The Boolean Algebra mathematical function
11 called "OR-ing," as presently used herein, can be designed to
12 capture a maximum of output one or output two (or other detector
13 outputs, if used). Thus, if either sub-system of the total
14 system makes a detection, the system will declare an object
15 present. In this way, one is guaranteed the best of performance
16 of either of the two sub-systems. A significant advantage of
17 such a system is that it is less likely to miss an acoustic
18 contact. While OR-ing is the presently preferred comparing or
19 selection means, other Boolean operators (NOR, NAND, AND) or
20 combinations of Boolean operators, as well as other types of
21 comparators and/or mathematical operators could also conceivably
22 be utilized. Scenario dependent feedback could also be supplied
23 to select element 34 or other means for controlling select
24 element 34 could be utilized.

1 Thus, each channel 18, 20, ...N, will now have an output and
2 be applied to section 40 for display. The display will be
3 produced in accord with principles previously used in displaying
4 data such as the SCOT or SPED. Therefore the presently
5 preferred output from select module 34 is SCOT or SPED which is
6 herein referred to as SOS. The SOS system, method, or algorithm
7 eliminates the need for two different displays to be viewed
8 either concurrently or consecutively by a sonar operator.
9 Therefore, sonar operator overload is reduced. Furthermore,
10 since the sonar operator needs to view only one display, the
11 time required to determine if targets of interest are present is
12 reduced.

13 It will be understood that many additional changes in the
14 details, materials, steps and arrangement of parts, which have
15 been herein described and illustrated in order to explain the
16 nature of the invention, may be made by those skilled in the art
17 within the principle and scope of the invention as expressed in
18 the appended claims.

1 Attorney Docket No. 79915

2 SONAR DISPLAY SYSTEM AND METHOD

3
4 ABSTRACT OF THE DISCLOSURE

5 A system and method for displaying sonar data are
6 disclosed. In a presently preferred embodiment, each of N
7 channels from a beamformer are separately processed utilizing a
8 pair of passive broadband detection processors such as SCOT
9 processors and SPED processors. The output of each SCOT
10 processor and each SPED processor are scaled, aligned, and then
11 compared. The maximum scaled and aligned output from each pair
12 of processors is selected for input to a bearing time history
13 display.

