

Serial Number 09/922,309
Filing Date 30 July 2001
Inventor Thomas S. Ramotowski

NOTICE

The above identified patent application is available for licensing. Requests for information should be addressed to:

OFFICE OF NAVAL RESEARCH
DEPARTMENT OF THE NAVY
CODE 00CC
ARLINGTON VA 22217-5660

DISTRIBUTION STATEMENT A
Approved for Public Release
Distribution Unlimited

20020215 105

1 Attorney Docket No. 82628

2

3 METHOD FOR INCREASING FRACTURE TOUGHNESS AND
4 REDUCING BRITTLINESS OF FERROELECTRIC POLYMER

5

6 STATEMENT OF GOVERNMENT INTEREST

7 The invention described herein may be manufactured and
8 used by or for the Government of the United States of America
9 for Governmental purposes without the payment of any royalties
10 thereon or therefor.

11

12 CROSS-REFERENCE TO RELATED PATENT APPLICATIONS

13 This patent application is co-pending with one related
14 patent application entitled "METHOD FOR INCREASING FRACTURE
15 TOUGHNESS AND REDUCING BRITTLINESS OF SEMI-CRYSTALLINE POLYMER"
16 (Attorney Docket No. 82468), by the same inventor as this
17 patent application and filed on even date.

18

19 BACKGROUND OF THE INVENTION

20 (1) Field of the Invention

21 The present invention relates generally to the manufacture
22 of annealed ferroelectric copolymer materials, and more
23 particularly to a method for increasing fracture toughness and
24 reducing brittleness of a semi-crystalline ferroelectric

1 polymer material such as poly(vinylidene fluoride-
2 trifluoroethylene) or p(VDF-TrFE).

3 (2) Description of the Prior Art

4 Many semi-crystalline polymers become brittle when formed
5 into thin sheets. In terms of a quantitative measure, these
6 materials have a low fracture toughness which is measured as
7 energy per unit volume in Joules/meter³ (J/m³). Brittleness is
8 caused by a high percentage of crystallinity and/or an
9 increased average size of the polymer crystallites brought
10 about by the manufacturing process. As a result of the
11 material's brittleness, damage during normal handling thereof
12 is prevalent thereby increasing the cost of using semi-
13 crystalline polymers in various products.

14 In some applications, crystallinity percentages in excess
15 of 80% are desired or required in order for the semi-
16 crystalline material to perform properly. For example, the use
17 of ferroelectric p(VDF-TrFE) has been problematic because it is
18 necessary to anneal the material to a very high level of
19 crystallinity in order to maximize the material's piezoelectric
20 properties. However, while the annealing step greatly
21 increases the material's crystallinity in preparation for a
22 ferroelectric poling operation, this processing step also makes
23 the treated material so brittle that it often cracks during
24 routine handling thereof.

1 SUMMARY OF THE INVENTION

2 Accordingly, it is an object of the present invention is
3 to provide a method for increasing a semi-crystalline
4 ferroelectric material's fracture toughness to thereby reduce
5 its brittleness without substantially damaging the material's
6 ferroelectric properties.

7 Another object of the present invention is to provide a
8 method to increase the fracture toughness of an annealed
9 ferroelectric polymer material while substantially maintaining
10 the material's ferroelectric properties.

11 A still further object of the present invention is to
12 provide for increased use of ferroelectric p(VDF-TrFE) in
13 applications where the material's brittleness previously
14 prevented such use.

15 Still another object of the present invention is to reduce
16 the brittleness of ferroelectric p(VDF-TrFE) while retaining
17 its ferroelectric properties.

18 Other objects and advantages of the present invention will
19 become more obvious hereinafter in the specification and
20 drawings.

21 In accordance with the present invention, a method is
22 provided that increases fracture toughness and reduces
23 brittleness of a semi-crystalline ferroelectric polymer
24 material while substantially maintaining ferroelectric
25 properties of the material. A semi-crystalline ferroelectric

1 polymer material such as poly(vinylidene fluoride-
2 trifluoroethylene) is placed in an inert oxygen-free atmosphere.
3 The material is heated to a temperature that is greater than
4 the material's Curie transition temperature, but below its
5 melting temperature. The material is then irradiated with beta
6 particles to provide a desired level of fracture toughness that
7 substantially maintains ferroelectric properties of the
8 material. In the case of poly(vinylidene fluoride-
9 trifluoroethylene), the heating temperature is approximately
10 between 100-120°C, the beta particles have an energy level of
11 approximately 2.5 mega electron volts (MeV), and the radiation
12 dose does not exceed approximately 50 megarads (Mrads).

13

14 BRIEF DESCRIPTION OF THE DRAWINGS

15 Other objects, features and advantages of the present
16 invention will become apparent upon reference to the following
17 description of the preferred embodiments and to the drawings,
18 wherein corresponding reference characters indicate
19 corresponding parts throughout the several views of the
20 drawings and wherein:

21 FIG. 1 is a schematic view of an apparatus for carrying
22 out the method of increasing fracture toughness of a semi-
23 crystalline polymer material in accordance with the present
24 invention;

1 FIG. 2 is a graph of fracture toughness as a function of
2 radiation dosage for the semi-crystalline polymer
3 poly(vinylidene fluoride-trifluorethylene) after processing in
4 accordance with the present invention; and

5 FIG. 3 is a graph of fracture toughness as a function of
6 radiation dosage for the annealed ferroelectric polymer
7 poly(vinylidene fluoride-trifluorethylene) after processing in
8 accordance with the present invention.

9

10 DESCRIPTION OF THE PREFERRED EMBODIMENT(S)

11 Referring now to the drawings, and more particularly to
12 FIG. 1, a system for carrying the method of increasing fracture
13 toughness in accordance with the present invention is shown and
14 referenced generally by numeral 10. As is known in the art,
15 fracture toughness is a quantitative measurement indicative of
16 the energy required to crack/fracture a material. Thus,
17 increasing fracture toughness of a material reduces its
18 brittleness which, while not a measurable quantity, describes a
19 quality thereof.

20 System 10 includes a fixture or chamber 12 (e.g., a sealed
21 chamber, irradiation fixture, etc.) for holding a semi-
22 crystalline polymer material 14 to be processed in accordance
23 with the present invention. In order to assure that no
24 chemical reactions occur between material 14 and its
25 surrounding gaseous environment, an inert gas source 16

1 supplies chamber 12 with an inert gas environment, i.e., inert
2 with respect to material 14. Typically, a flow of inert gas is
3 passed continuously through chamber 12 as indicated by arrows
4 18. The gas is oxygen-free because many polymeric materials
5 can react with oxygen during irradiation thereof. Although not
6 an exhaustive list, some common inert gases suitable for use in
7 the present invention include nitrogen and argon.

8 A heater 20 is coupled to chamber 12 for raising the
9 temperature of material 14 during the processing thereof. A
10 radiation source 22 generates a beam of beta radiation that is
11 directed to/through chamber 12, i.e., material 14 is exposed to
12 high energy electrons. A radiation dosage monitor 24 is
13 coupled to/through chamber 12 for monitoring/measuring the
14 radiation dosage to which material 14 is exposed. System 10 so
15 constructed/configured can be made from a variety of
16 commercially-available components as would be understood by one
17 of ordinary skill in the art.

18 In operation of system 10 in accordance with the present
19 invention, material 14 is placed in chamber 12 and a flow 18 of
20 inert gas is provided to chamber 12 by inert gas source 16.
21 Flow 18 should be sufficient to purge chamber 12 of oxygen-
22 containing atmospheric gas so that only the inert gas is
23 contained in chamber 12. Heater 20 is activated to heat
24 material 14 to a temperature that, in general, is greater than
25 the Curie transition temperature of material 14, but below the

1 melting temperature of material 14. As is known in the art,
2 the Curie transition temperature is a known quantity for a
3 given material content. In the present invention, with
4 material 14 being heated under an inert gas purge, radiation
5 source 22 irradiates material 14 with beta particles of a
6 specified energy. Radiation dosage is simultaneously monitored
7 by a radiation monitor 24 which is representative of direct
8 monitoring systems or indirect monitoring systems such as those
9 capable of monitoring electron flux. In these conditions, it
10 was found that an increase in fracture toughness was associated
11 with the energy level of the radiation and the amount of
12 radiation to which material 14 is exposed. Thus, depending on
13 the type material 14 and the desired level of fracture
14 toughness, irradiation of material 14 continues until a
15 specified radiation dosage is achieved indicative of the
16 desired level of fracture toughness for a given energy level of
17 radiation.

18 The above-described process was used successfully for the
19 semi-crystalline polymer poly(vinylidene-trifluoroethylene) (or
20 p(VDF-TrFE)) comprised of 50-85 weight percent vinylidene
21 fluoride (VDF) which, in its cast form, has a crystallinity of
22 40-50%. However, crystallinity of this material can be
23 increased to 80-90% or more using an annealing process.
24 Whether cast or annealed, p(VDF-TrFE) is generally formed into
25

1 thin sheets which are less brittle in the cast form, but highly
2 brittle in the annealed form.

3 To increase the fracture toughness of semi-crystalline
4 p(VDF-TrFE) without regard to retaining the material's
5 ferroelectric properties, the p(VDF-TrFE) material was placed
6 in an irradiation fixture under a nitrogen purge, and heated to
7 a temperature between approximately 100-120°C, i.e., greater
8 than room temperature but below the material's melting
9 temperature. The p(VDF-TrFE) was then irradiated with
10 approximately 1.2 mega electron volt (MeV) beta particles while
11 the radiation was monitored. A graph of the resulting fracture
12 toughness as a function of radiation dosage is illustrated in
13 FIG. 2 for a p(VDF-TrFE) polymer comprised of 65 weight percent
14 VDF that was heated to 100°C under a nitrogen purge.

15 As is evident from the graph in FIG. 2, significant
16 improvements in fracture toughness were realized. The greatest
17 increase in fracture toughness occurred when radiation dosage
18 was increased from approximately 60 to approximately 80
19 megarads (Mrads) for a radiation dosage of 1.2 MeV. Note that
20 this result is unexpected since, below the melting temperature,
21 beta particle radiation on its own would be expected to induce
22 polymer chain scissioning and perhaps some cross-linking, both
23 of which tend to reduce fracture toughness. It is therefore
24 believed that the present invention's combination of steps
25 increases fracture toughness by means of a reduction in the

1 average size of the crystallites in the material through the
2 generation of pendant group defects which interfere with
3 crystallinity.

4 It is apparent from the above description that the semi-
5 crystalline polymer p(VDF-TrFE) can undergo dramatic increases
6 in fracture toughness. However, p(VDF-TrFE) is also commonly
7 used in its ferroelectric state for the manufacture of
8 transducers and hydrophones. To achieve the ferroelectric
9 state, cast semi-crystalline p(VDF-TrFE) can be poled to align
10 its domains, or can first be annealed to increase crystallinity
11 and then poled as is well known in the art. The problem that
12 plagues cast or annealed ferroelectric p(VDF-TrFE) is its
13 brittleness. However, any increase in fracture
14 toughness/decrease in brittleness for this material usage must
15 be achieved while maintaining the material's ferroelectric
16 properties/domains. The patentee then inventively discovered
17 that the above-described process of increasing fracture
18 toughness caused a destruction of ferroelectric domains at
19 levels of fracture toughness that were less than 1 J/m^3 . That
20 is, the dramatic increases in fracture toughness evidenced in
21 FIG. 2 came at the expense of ferroelectric domain destruction
22 in the case of ferroelectric p(VDF-TrFE). Therefore, continued
23 irradiation is counterproductive for usages of the material in
24 which ferroelectric properties are desired. Such usages
25 include the construction of hydrophone sensing elements.

1 To overcome this problem, it is necessary to heat the
2 material to a temperature that is above its Curie transition
3 temperature, and select a suitable beta particle radiation
4 energy level and radiation dosage that achieves a desired level
5 of fracture toughness without destroying the material's
6 ferroelectric properties. In terms of cast or annealed
7 ferroelectric p(VDF-TrFE) comprised of 50-85 weight percent
8 VDF, it was found that an increased radiation energy level
9 could increase the material's fracture toughness without
10 destroying its ferroelectric properties. This is evidenced in
11 FIG. 3 for an annealed ferroelectric p(VDF-TrFE) having 65
12 weight percent VDF that is heated to 120°C under a nitrogen
13 purge prior to irradiation with 2.55 (MeV) beta particles. In
14 particular, it was found that at this radiation energy level,
15 ferroelectric properties which were initially present were
16 substantially maintained for radiation doses up to
17 approximately 50 Mrads. After this, increases in beta particle
18 energy levels destroyed ferroelectric properties. Note that
19 substantial fracture toughness (which also is a maximum value
20 of the limited number of data points in FIG. 3) was achieved
21 and ferroelectric properties maintained at a radiation dosage
22 of approximately 32.5 Mrads. As FIG. 3 shows, the fracture
23 toughness initially monotonically increased to the substantial
24 toughness value at a dosage of approximately 32.5 megarads, and
25 thereafter decreases, and is in fact a monotonically decreasing

1 value at the aforesaid 50 megarads value of dosage. Also, note
2 that if only increased fracture toughness is of concern, this
3 example implies that fracture toughness can be increased by
4 utilizing beta particles having an energy level between
5 approximately 1.0-3.0 MeV.

6 The advantages of the present invention are numerous.
7 Cast or annealed ferroelectric p(VDF-TrFE) can have its
8 fracture toughness increased without loss of ferroelectric
9 properties. This will greatly reduce breakage of components
10 made from this material thereby making the assemblies including
11 same more reliable and cost-effective. While the mechanisms at
12 work in the present invention are not fully understood, it is
13 believed that the above-described methodology can be extended
14 to other semi-crystalline ferroelectric polymers. In general,
15 once a desired fracture toughness is identified, a particular
16 combination of heating, electron energy bombardment and
17 radiation dosage can be implemented in a repeatable
18 manufacturing process. With the heat and electron energy being
19 fixed for a given material, only radiation dosage need be
20 monitored as fracture toughness is a function thereof in the
21 present process.

22 It will be understood that many additional changes in the
23 details, materials, steps and arrangement of parts, which have
24 been herein described and illustrated in order to explain the
25 nature of the invention, may be made by those skilled in the

l art within the principle and scope of the invention, _____

1 Attorney Docket No. 82628

2

3 METHOD FOR INCREASING FRACTURE TOUGHNESS AND
4 REDUCING BRITTLINESS OF FERROELECTRIC POLYMER

5

6 ABSTRACT OF THE DISCLOSURE

7 A method is provided that increases fracture toughness and
8 reduces brittleness of a semi-crystalline ferroelectric polymer
9 material while substantially maintaining ferroelectric
10 properties of the material. The material is heated in an inert
11 oxygen-free atmosphere to a temperature above the material's
12 Curie transition but below its melting temperature. The
13 material is then irradiated with beta particles to provide a
14 desired level of fracture toughness that substantially
15 maintains ferroelectric properties of the material. In the
16 case of poly(vinylidene fluoride-trifluorethylene), the heating
17 temperature is just above the material's Curie transition
18 temperature, the beta particles have an energy level of
19 approximately 2.5 mega electron volts (MeV), and the radiation
20 dose should not exceed approximately 50 megarads (Mrads).

FIG. 1

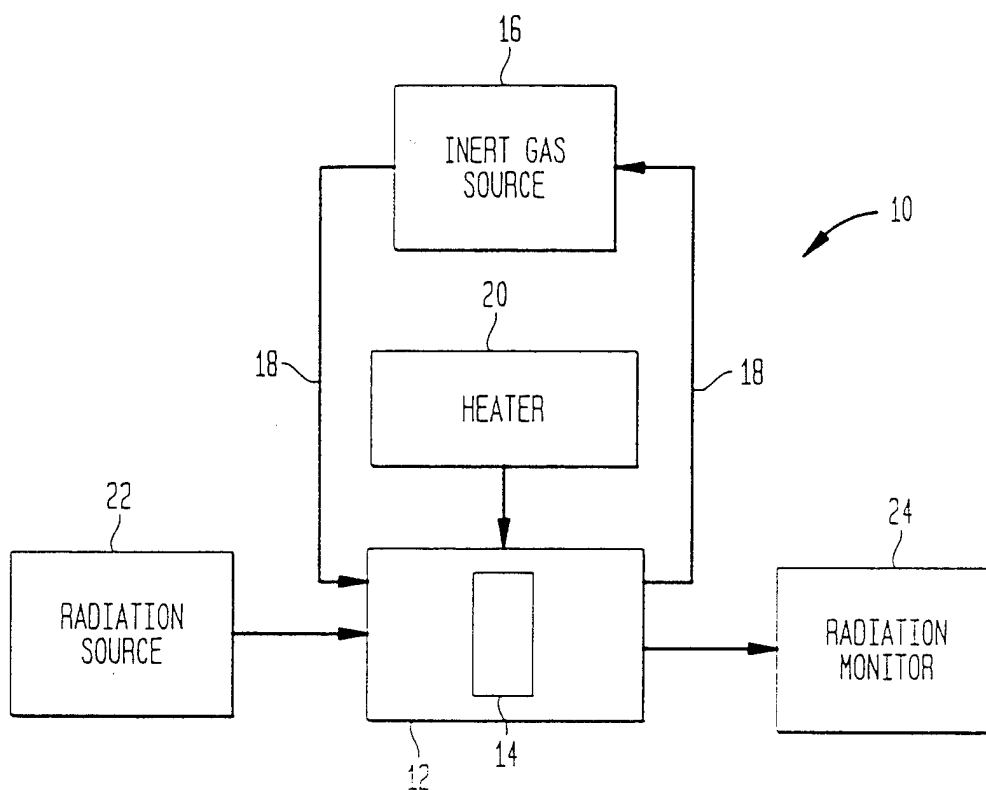


FIG. 2

FRACTURE TOUGHNESS v. RADIATION DOSE
65/35 p(VDF-TrFE) 100°C/1.2MeV

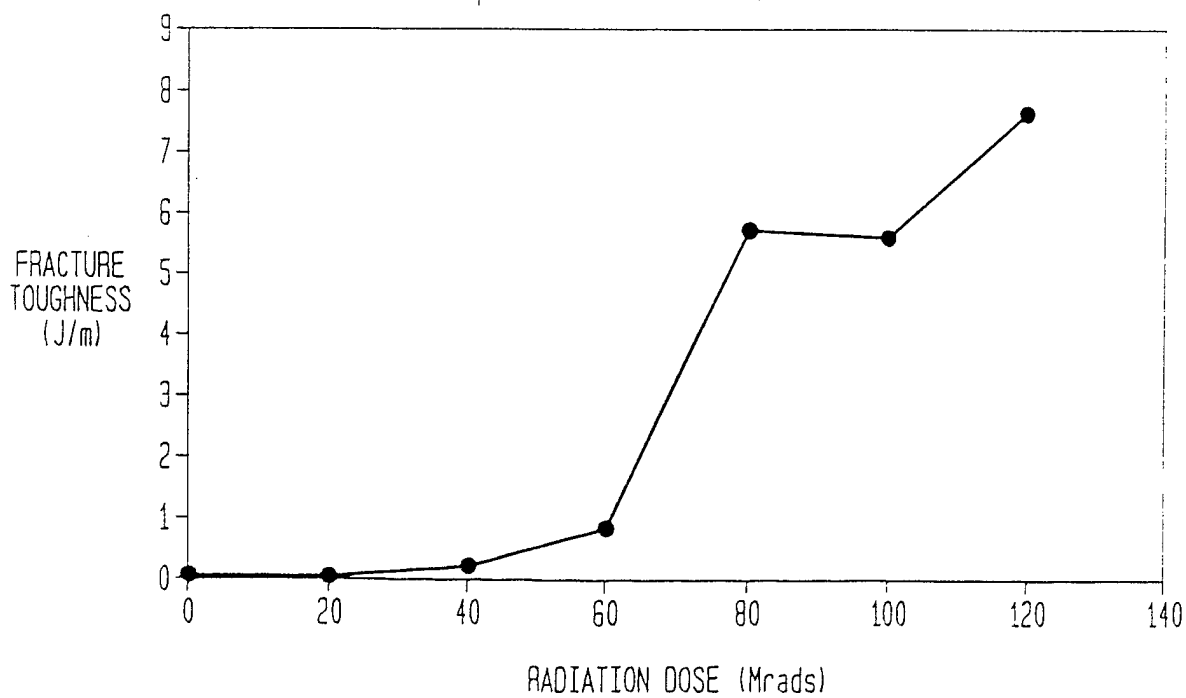


FIG. 3

FRACTURE TOUGHNESS v. RADIATION DOSE 65/35 p(VDF-TrFE)
120°C/2.55MeV

