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3 SONAR SYSTEM PERFORMANCE METHOD

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5 STATEMENT OF THE GOVERNMENT INTEREST

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7 The invention described herein may be manufactured and used
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9 Governmental purposes without the payment of any royalties
10 thereon or therefore.

11
12 BACKGROUND OF THE INVENTION

13
14 (1) Field of the Invention

15 The present invention relates generally to acoustic sonar
16 systems and, more specifically, to methods for evaluating,
17 comparing, and selecting sonar system configurations and sonar
18 sensors.

19 (2) Description of the Prior Art

20 Variable depth sonar arrays are routinely tested at a
21 variety of depths to determine their system performance. Sonar
22 performance may vary greatly with depth because of changes in
23 factors that affect the sensors such as temperature and depth.
24 Typically, near the surface, temperature is the primary
25 consideration. As the depth increases, then pressure has a

1 greater influence on performance as temperature becomes more
2 uniform. At intermediate depths, ducts form which can trap
3 transmitted acoustic waves and allow them to propagate for large
4 distances. Moreover, if the transmitting and receiving sensors
5 in a sonar system are at widely varying depths, then acoustic
6 boundaries caused by pressure and temperature may interfere with
7 sound wave reception. An acoustic sonar system may also vary
8 with respect to the organization or sensors within the array.

9 More specifically, sensor and system performance is
10 determined by performing a variety of tests at various ranges and
11 depths. The purpose of the tests is to determine the maximum
12 range of reception for a given depth. Often the maximum range
13 values are averaged together to provide a value which represents
14 the combined sensor performance. This may lead to an incorrect
15 evaluation because the sensor may have an exceptionally large
16 range value within a duct which will overshadow lesser values at
17 other depths.

18 As an example for evaluating a sonar system in a surface
19 layer environment, a sonar system that maintains both
20 transmitting and receiving sensor arrays in the surface layer may
21 normally achieve a relatively large detection range for a target
22 that also appears in the surface layer but may produce
23 comparatively small detection ranges for targets that are
24 situated below the surface duct. When the result of all target
25 depths are combined in a simple average or referenced to a

1 statistical measurement such as standard deviations, the outcome
2 may be skewed by the shallow event. Standard deviations give a
3 value indicating the closeness of the data to the average and so
4 standard deviation is meaningless without a reference to the
5 average value. Accordingly, whenever standard deviation is
6 provided, the average is provided.

7 Use of standard deviation techniques also results in
8 difficulty of comparison. For instance, one system may average
9 fifteen kiloyards (fifteen thousand yards) with a standard
10 deviation of three kiloyards. The next system may average
11 sixteen and one-half kiloyards with a standard deviation of four
12 kiloyards. With this type of comparison, there is no clear
13 answer as to which is the better system. Moreover, these results
14 are difficult to plot due to extra dimensions as compared with a
15 single performance rating.

16 The result is that prior art methods for comparing sonar
17 sensors and sonar sensor systems may lead to an unrealistic or
18 inaccurate appraisal of the system's detection capability against
19 targets at all water depths and may cause selection of a less
20 desirable sonar system.

21 Prior art patents that relate to this topic include the
22 following:

23 U. S. Patent No. 5,734,591, issued Mar. 31, 1998, to John C.
24 Yundt, (hereinafter, Yundt '591) discloses a method for analyzing
25 biochemical samples or human bodily fluids which operates over at

1 least two ranges. The method of Yundt '591 comprises obtaining a
2 first set of test results relating to the biochemical samples
3 from the testing device over at least two ranges, and calculating
4 from the first set of test results an individual range mean for
5 each of the at least two ranges. The method also includes
6 obtaining a second set of test results relating to the
7 biochemical samples from a group of testing devices that operate
8 over the at least two ranges, calculating from the second set of
9 test results a group range mean and a group range standard
10 deviation for each of the at least two ranges, and calculating
11 standard deviation indexes for the testing device from the
12 individual range means, the group range means and group range
13 standard deviations. The method further comprises forming
14 generally parallel spaced apart data range axes, each relating to
15 a range of operation of the testing device, to facilitate
16 analysis of the performance of the testing device over each range
17 of operation, wherein the respective positions of the data range
18 axes in relation to one another are scaled based on the values of
19 the operating ranges, and then plotting all of the standard
20 deviation indexes in relation to the data range axes in such a
21 way that analysis of the performance of the testing device over
22 the at least two operating ranges is provided in a single graphic
23 display.

24 U. S. Patent No. 5,541,854, issued Jul. 30, 1996 to John C.
25 Yundt, discloses a method and graph for analyzing the performance

1 of a testing device that operates over at least two ranges
2 related to the above U.S. Patent No.5, 734,591, to the same
3 inventor.

4 U. S. Patent No. 5,828,567, issued Oct. 27, 1998, to Eryurek
5 et al., discloses a transmitter in a process control system
6 including a resistance sensor sensing a process variable and
7 providing a sensor output. Sensor monitoring circuitry coupled
8 to the sensor provides a secondary signal related to the sensor.
9 Analog-to-digital conversion circuitry coupled to the sensor
10 output and the sensor monitoring circuitry provides a digitized
11 sensor output and a digitized secondary signal. Output circuitry
12 coupled to a process control loop transmits a residual life
13 estimate related to residual life of the sensor. A memory stores
14 a set of expected results related to the secondary signal and to
15 the sensor. Diagnostic circuitry provides the residual life
16 estimate as a function of the expected results stored in a
17 memory, the digitized sensor output and the digitized secondary
18 signal.

19 U. S. Patent No. 4,675,147, issued Jun. 23, 1987, to
20 Schaefer et al, discloses the real time actual and reference
21 values of parameters pertinent to the key safety concerns of a
22 pressurized water reactor nuclear power plant which are used to
23 generate an integrated graphic display representative of the
24 plant safety status. This display is in the form of a polygon
25 with the distances of the vertices from a common origin

1 determined by the actual value of the selected parameters
2 normalized such that the polygon is regular whenever the actual
3 value of each parameter equals its reference value despite
4 changes in the reference value with operating conditions, and is
5 an irregular polygon which visually indicates deviations from
6 normal otherwise. The values of parameters represented in analog
7 form are dynamically scaled between the reference value and high
8 and low limits which are displayed as tic marks at fixed
9 distances along spokes radiating from the common origin and
10 passing through the vertices. Multiple, related binary signals
11 are displayed on a single spoke by drawing the associated vertice
12 at the reference value when none of the represented conditions
13 exist and at the high limit when any such condition is detected.
14 A regular polygon fixed at the reference values aids the operator
15 in detecting small deviations from normal and in gauging the
16 magnitude of the deviation. One set of parameters is selected
17 for generating the display when the plant is at power and a
18 second set reflecting wide range readings is used the remainder
19 of the time such as following a reactor trip. If the quality of
20 the status, reference or limit signals associated with a
21 particular vertex is "bad", the sides of the polygon emanating
22 from that vertex are not drawn to appraise the operator of this
23 condition.

24 In summary, while the prior art shows various methods for
25 making comparisons, the above disclosed prior art does not show a

1 suitable method for comparing sonar sensors or sonar sensor
2 systems. Consequently, there remains a need for a system that
3 provides a single performance rating that accounts for both the
4 average and deviation from the average for performance at
5 different target depths which may be plotted for different
6 sender/receiver depth configurations. Those skilled in the art
7 will appreciate the present invention that addresses the above
8 and other problems.

10 SUMMARY OF THE INVENTION

11 Accordingly, it is an object of the present invention to
12 provide an improved method for comparing acoustic sensors and
13 acoustic sensor systems.

14 It is yet another object of the present invention to provide
15 a method of comparison of acoustic sensors and acoustic systems
16 that provides a single performance rating that takes into effect
17 the depth sensitive nature of performance of the acoustic sensors
18 and acoustic sensor systems.

19 These and other objects, features, and advantages of the
20 present invention will become apparent from the drawings, the
21 descriptions given herein, and the appended claims.

22 A method is provided for evaluating and/or selecting a sonar
23 system wherein the sonar system comprises at least one sender and
24 at least one receiver. The method includes such steps as
25 positioning the sender and the receiver at a plurality of sensor

1 depths wherein tests are performed for each of the plurality of
2 sensor depths. For instance in one test, the sender may be
3 located at a one hundred foot depth and the receiver at a three
4 hundred foot depth. In a subsequent test, both the sender and
5 receiver may be at a two hundred foot depth. Different sonar
6 system configurations which may comprise only one sender/receiver
7 or may comprise sensor arrays or different sonar systems can be
8 evaluated as discussed below.

9 For each of the plurality of sensor depths or sonar system
10 configurations, a target may be positioned at a plurality of
11 target depths. For each of the plurality of target depths, a
12 detection range is determined for the sonar system, e.g., twenty
13 kiloyards at one target depth, eighteen kiloyards at another
14 target depth, and so on. An average detection range is
15 determined.

16 Moreover, a scaling factor related to a ratio of the dynamic
17 range to the maximum range is produced. A dynamic range
18 sensitivity weighting term is selected. The value of the dynamic
19 range sensitivity weighting is typically but not necessarily
20 selected to be between zero and one. Preferably, the range
21 weighting term is selected to be no greater than the smallest
22 value of the inverse of the scaling factor.

23 For each of the plurality of sensor depths, a performance
24 rating is produced from the average detection range, the dynamic
25 range, the maximum detection range, the minimum detection range,

1 and the dynamic range sensitivity weighting term. More
2 specifically, the minimum detection range may be subtracted with
3 respect to the average detection range to provide a first factor.
4 The dynamic range sensitivity weighting term may be multiplied
5 with respect to the first factor to obtain a second factor. The
6 scaling factor may be multiplied with respect to the second
7 factor to obtain a dynamic range factor. Then the dynamic range
8 factor may be subtracted with respect to the average detection
9 range to provide a performance rating.

10 As noted above, the performance rating is preferably
11 determined with respect to each of the plurality of sensor
12 depths. In one preferred embodiment, the performance rating may
13 be plotted for each of the plurality of sensor depths.

14 With respect to comparison and selecting purposes, it is
15 desirable to utilize a constant value for the range weighting
16 term for each of the plurality of sensor depths and/or for each
17 sonar system or sonar system components to be tested.

18 19 BRIEF DESCRIPTION OF THE DRAWINGS

20 A more complete understanding of the invention and many of
21 the attendant advantages thereto will be readily appreciated as
22 the same becomes better understood by reference to the following
23 detailed description when considered in conjunction with the
24 accompanying drawings wherein corresponding reference characters

1 indicate corresponding parts throughout the several views of the
2 drawings and wherein:

3 FIG. 1 is a diagram showing a typical test set up for
4 gathering data used in calculating the subject performance
5 rating; and

6 FIG. 2 is a graph showing a performance rating in accord
7 with the present invention plotted to illustrate the performance
8 of a source and a receiver positioned at different depths.

9
10 BRIEF DESCRIPTION OF THE PREFERRED EMBODIMENTS

11 Referring now to the drawings, in FIG. 1 there is shown the
12 test setup for developing the performance measure of the current
13 invention. An acoustic transmitter 10 is positioned at a
14 transmitter depth 12 below the surface 14 of a body of water. An
15 acoustic receiver 16 is positioned at a receiver depth 18 below
16 the surface 14. A target 20 is also located below the surface 14
17 at a range 22 away from the receiver 16. During testing,
18 transmitter 10 is positioned at transmitter depth 12 where it
19 transmits an acoustic signal which bounces off of target 20 and
20 is received at receiver 16. Data is collected concerning
21 reception at range 22, transmitter depth 12, and receiver depth
22 18. This process is repeated for various transmitter and
23 receiver depths.

24 Referring now to FIG. 2 there is shown one use of the system
25 of the present invention for a simplified visual display. The

1 performance rating, as discussed in detail subsequently, is
2 plotted for various depths of the source and receiver and may
3 typically be a value in terms of thousands of yards (kiloyards).
4 At respective source and receiver depths that may be selected
5 from the plot of FIG. 2, a plurality of tests have been made
6 wherein the target depth varied and the respective target ranges
7 were determined whereupon a performance rating was made as
8 discussed hereinafter. Different cross hatching types in FIG. 2
9 relate to different performance ratings. For instance, at point
10 100, the source depth is 150 ft. and the receiver depth is 100
11 ft. and the performance rating is in the range of 26-28
12 kiloyards. The performance rating is based on both the magnitude
13 and uniformity of detection ranges achieved for targets at a
14 variety of water depths. At point 110, the source depth is about
15 220 ft. and the receiver depth about 125 ft. and the performance
16 rating is 28-30 kiloyards. Taking another point 120, the source
17 depth is 100 ft. and the receiver depth is 200 ft. and the
18 performance rating is 26-28 kiloyards. The various layers of the
19 performance ratings as plotted may be in color or otherwise
20 distinguished. Different source/receiver pairs or the same pair
21 at different positions may be evaluated and compared in this
22 manner.

23 The performance rating of the present invention evaluates
24 the overall performance of a sonar system by using both the
25 magnitude and the consistency of detection performance achieved

1 for targets within a predetermined range of water depths. The
2 performance rating of the present invention is based on depth
3 sensitive system performance and may preferably utilize a user
4 adjusted dynamic range weighting function for appropriate
5 weighting of the outcome of depth averaged detection ranges.

6 A dynamic range factor, DR, is given by the following
7 equation:

$$8 \quad DR = \left(\left(\frac{SD}{NS} - SR \right) * W \right) * \left(\frac{MR - SR}{MR} \right) \quad (1)$$

9 where:

10 SD = Sum of the detection ranges at all target depths;

11 SR = Smallest detection range;

12 MR = Largest detection range;

13 NS = Number of detection range samples;

14 W = Dynamic range sensitivity weighting term. (0 = Low
15 Sen., 1 = High Sen.)

16
17 The right most term of the above equation is merely a
18 scaling factor. The performance rating is given as:

$$20 \quad \text{Performance Rating} = \frac{SD}{NS} - DR \quad (2)$$

21

22

1
2 For the results of FIG. 2, the performance rating and each
3 term refers to a source-receiver pair at a particular depth
4 configuration. In this case, the determination should be
5 performed for each source and receiver depth combination to be
6 modeled within the same specific environment. The highest
7 performance ratings for different types of source receiver pairs
8 or for a particular depth combination of a specific pair will be
9 based upon achieving the best combination of the magnitude of the
10 detection ranges and consistent performance across the depth
11 ranges.

12 As will be appreciated from review of the above equation
13 with respect to a particular source and receiver depth
14 combination, the performance rating is computed by first finding
15 the average (mean) for all modeled target depths. Subtracted
16 from this average detection range is a dynamic range weighting
17 function that is composed of the average detection range, the
18 minimum detection range, the maximum detection range, the dynamic
19 range, and a dynamic range sensitivity weighting term, "W". The
20 dynamic range sensitivity weighting term W is a user defined
21 value, which can be chosen to be as small as zero, rendering no
22 sensitivity to dynamic range (pure mean values). On the other
23 hand, the term W could be as large as one (and in some cases more
24 than one), which produces a very high sensitivity to dynamic
25 range in the performance results. For comparison of the same

1 source receiver pair at different depths, and for comparison of
2 different types of source receiver pairs, the same W is
3 preferably used.

4 In general, when the sum of the detection ranges is large,
5 the outcome of the performance rating will also be large.
6 However, if the individual magnitudes of detection range vary a
7 great deal with depth, then the dynamic range will grow to
8 significant proportions and the performance rating will be
9 reduced by a correspondingly large amount. If under a different
10 set of circumstances, the same total sum of detection ranges is
11 achieved but with relatively small variations in individual
12 system performance, then the dynamic range weighting function
13 will be small and a larger performance rating will ultimately
14 result. One other important consideration is that the outcome of
15 the performance rating is most reliable when the data being
16 analyzed contains a sufficient number of target-depth samples to
17 accurately reflect the particular system's performance
18 capabilities across the entire range of the target's potential
19 operating depths.

20 As stated hereinbefore, the smaller the value assigned to W
21 (low sensitivity), the more the performance rating will approach
22 the simple mean of the detection ranges. Conversely, the greater
23 the assigned value of W (high sensitivity), the more the
24 performance rating will tend towards the smallest detection range
25 in the target depth data set. In fact, if W is selected to be

1 greater than one, it is possible, when accompanied by large
2 dynamic range, to produce a performance rating that is actually
3 less than the smallest detection range that appears in the target
4 depth data set. Therefore, the user must exercise care when
5 specifying values of W that are greater than one to insure that
6 the performance rating is within the bounds of a reasonable set
7 of results for a particular data set. Generally, W should be no
8 greater than the smallest inverse scaling factor or $MR/(MR-SR)$
9 that appears in any of the data sets being evaluated or compared.
10 If W was greater than the smallest inverse scaling factor, then
11 the performance rating could be less than the smallest value in
12 the set. If the performance measurement was less than the
13 smallest value in the set, this may result in an inaccurate view
14 of the data. The same weighting value, W , should be used when
15 comparing different sonar systems to obtain a valid basis for
16 comparison.

17 In summary, tests related to target depth and detection
18 range are taken for each sonar system configuration. For
19 instance, if the sonar system comprises a single source and
20 receiver, then for each source depth and receiver depth to be
21 considered, target depth and detection range tests are performed.
22 Generally it is desirable to test at several different target
23 depths to produce more complete information from which an
24 evaluation or selection may be made. The dynamic range
25 weighting factor W is selected and preferably maintained as a

1 constant. The value of the performance rating can be plotted as
2 in FIG. 2 for each sonar system variation such as source depth.
3 versus receiver depth.

4 It will be understood that many additional changes in the
5 details, materials, steps and arrangement of parts, which have
6 been herein described and illustrated in order to explain the
7 nature of the invention, may be made by those skilled in the art
8 within the principle and scope of the invention. _____
9 _____

2
3 SONAR SYSTEM PERFORMANCE METHOD

4
5 ABSTRACT OF THE DISCLOSURE

6 A method is disclosed for evaluating and/or selecting sonar
7 systems and sonar sensors is provided that results in a
8 performance rating that represents both the magnitude and
9 consistency of detection of targets positioned at different
10 depths. In a preferred embodiment wherein a sonar system
11 includes at least one source and at least one receiver, the
12 performance rating related to target detection, is plotted for
13 each of a plurality of source and receiver depths. A dynamic
14 range sensitivity factor is selected that provides sensitivity in
15 the performance rating with respect to consistency of the
16 detection range at different depths. The dynamic range
17 sensitivity factor is preferably selected between zero and an
18 inverse of a scaling factor related to a maximum detection range
19 and a minimum detection range for a particular source and
20 receiver depth relationship.

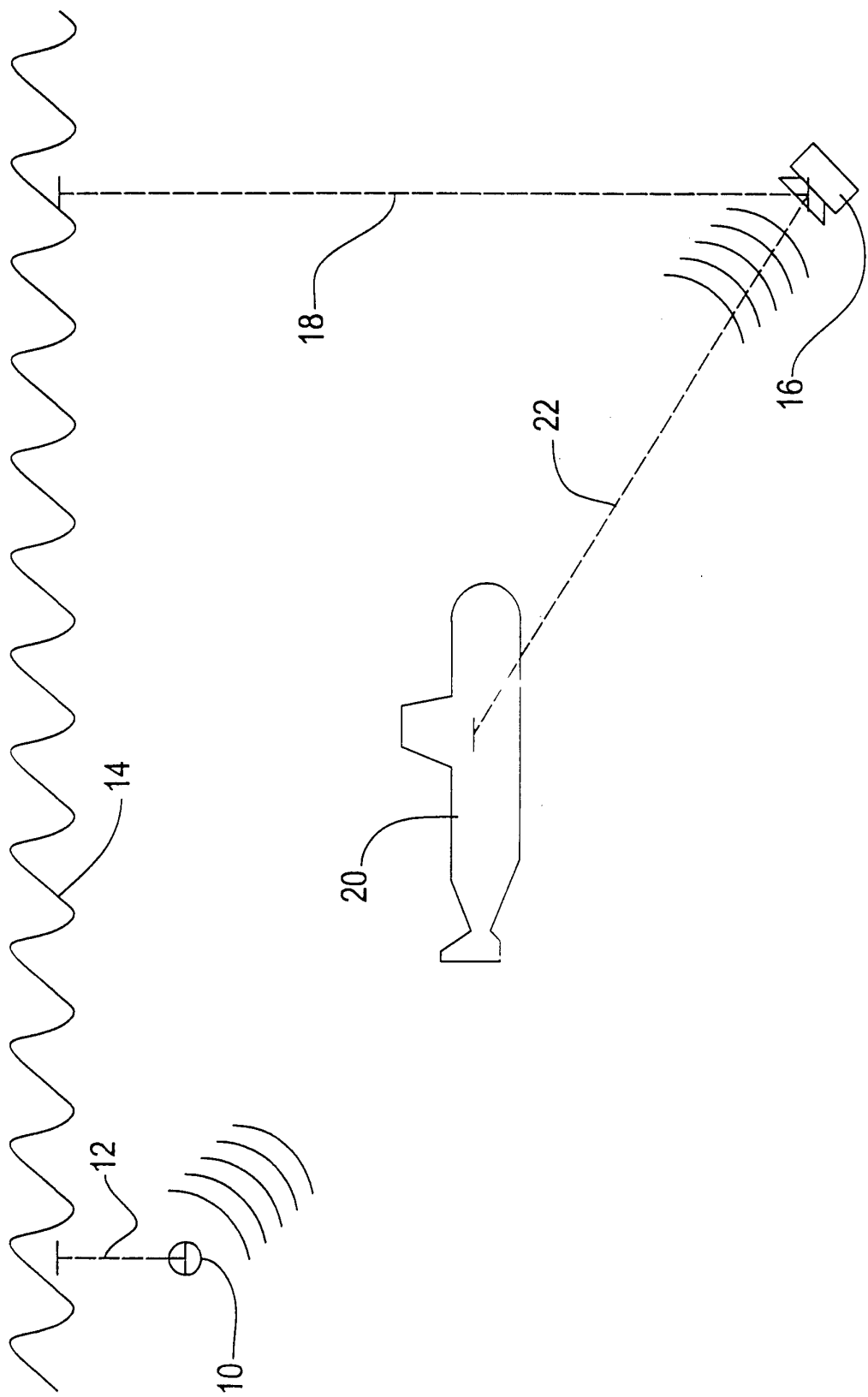


FIG. 1

FIG. 2

