

Serial Number 09/718,759
Filing Date 24 November 2000
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3 A METHOD FOR REDUCING STRUM IN TOW CABLES

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5 STATEMENT OF GOVERNMENT INTEREST

6 The invention described herein may be manufactured and used
7 by or for the Government of the United States of America for
8 governmental purposes without the payment of any royalties
9 thereon or therefor.

10
11 BACKGROUND OF THE INVENTION

12 (1) Field of the Invention

13 The present invention relates to towing devices and
14 more particularly tow cables with vibration damping means.

15 (2) Brief Description of the Prior Art

16 For towed components such as arrays or streamers, strum
17 (vortex-induced vibration) is a persistent problem. Such
18 vibration is transmitted into the towed array or streamer,
19 causing damage to internal components.

20 The prior art includes a number of patents addressed to the
21 management of such forces in cables.

22 U.S. Patent No. 5,214,244 to Cummings et al., for example,
23 discloses an underwater cable having a flexible, elongated core

1 surrounded by a flexible, elongated jacket. A distributed jacket
2 includes a helically displaced phase shifter to decouple the
3 cable from strumming produced by shedding of von Karman vortex
4 streets from the cable.

5 U.S. Patent No. 5,601,046 to Berglund discloses a variable-
6 gap, distributed-capacitance sensor that provides an output
7 signal that is a function of its instantaneous elongation. The
8 sensor is integrally associated with a seismic isolator section
9 for measuring the instantaneous stretch thereof.

11 SUMMARY OF THE INVENTION

12 It is an object of the present invention to provide a still
13 better method for reducing strum in tow cables.

14 The present invention is a method for reducing strum in a
15 tow cable extending from a marine vessel. Such cables have an
16 adjustable length. The length of the cable is adjusted so that
17 the number of longitudinal waves is an integral number.

19 BRIEF DESCRIPTION OF THE DRAWINGS

20 Other objects, features and advantages of the present
21 invention will become apparent upon reference to the following
22 description of the preferred embodiments and to the drawing,

1 wherein corresponding reference characters indicate corresponding
2 parts in the drawing and wherein:

3 FIG. 1 is a schematic illustration of a tow cable showing
4 transverse waves as may be generated by means of the method of the
5 present invention;

6 FIG. 2a is a schematic illustration of a tow cable showing
7 longitudinal waves as may be generated by means of the method of
8 the present invention;

9 FIG. 2b is a graph of amplitude of the longitudinal wave
10 corresponding to the position in FIG. 2a; and

11 FIG. 3 is a schematic illustration of a ship and tow line
12 illustrating the method of the present invention.

13
14 DESCRIPTION OF THE PREFERRED EMBODIMENT

15 There are generally two types of waves in the tow cable:
16 transverse waves and longitudinal waves. The transverse waves
17 tend to have very short wavelengths since their propagation speed
18 is approximately

19
$$C_t = \sqrt{Tg/W},$$

20 where T is the tension, W is the weight per unit length, and g
21 $= 9.81 \text{ m/s}^2$. In many applications, the tow cable is often very

1 long (a mile or more) to reduce the noise radiated from the tow
2 ship so that there are typically on the order of hundreds to
3 thousands of transverse wavelengths in a tow cable. Because of
4 this large number of wavelengths, there is a tremendous amount of
5 damping on any individual wave as it travels from one end of the
6 cable to the other. This damping prevents the establishment of
7 standing waves (except in localized regions near reflective
8 boundaries) because each wave will be almost completely
9 attenuated by the time it is reflected back to its original
10 location. Therefore, tuning the tow cable on the basis of
11 transverse waves is all but impossible.

12 Longitudinal waves, on the other hand, have wavelengths that
13 are much longer by virtue of a propagation speed governed by

14
$$Cl = \sqrt{E/\rho}$$

15 where E is the cable Young's modulus and ρ is the cable density.
16 For longitudinal waves, there are only on the order of 1 to 10
17 wavelengths contained by a typical tow cable. Because of this
18 fact, standing waves over the length of the cable should be
19 easily established, and therefore, tuning should be easily
20 achieved.

1 The amplitude of vibration at a towed streamer, array, or
2 any other component is usually dominated by the longitudinal
3 vibration component, which can be generated along the tow cable
4 in two ways. The first way involves cable curvature: on any
5 point on the cable, curvature causes some of the transverse
6 component of motion to be converted into the longitudinal
7 component and vice versa. The second way occurs due to the fact
8 that the transverse component creates a localized region of
9 curvature in the cable, which shortens the cable. This
10 shortening, which generates longitudinal waves, occurs twice for
11 each transverse wave cycle. Therefore, the frequency of the
12 longitudinal wave is double that of the transverse wave. Note
13 that the second wave of generating longitudinal waves usually
14 leads to much greater amplitudes than the first. This fact is
15 especially true for "critical angle tow" in which there is
16 essentially no curvature since virtually the entire tow cable is
17 at its critical angle (the angle that the weight and drag
18 balance).

19 The boundary conditions seen by the cable longitudinal waves
20 are the winch (which can be modeled as a rigid boundary) and the
21 towed component on the other end (which can be modeled as a free
22 boundary). At the free boundary, the displacement is maximized
23 while the tension approaches zero. If there are approximately an

1 integral number of longitudinal wavelengths contained in the
2 cable, the vibration at the aft end will be minimized. If, on
3 the other hand, there are approximately an odd integral number of
4 half wavelengths contained in the cable, the longitudinal
5 vibration at the aft end will be maximized.

6 Referring to FIG. 1, the generation of transverse waves
7 according to this invention is illustrated in which a tow cable is
8 shown at 10. There is also shown the direction of tow 12 and a
9 transverse wave 14. The maximum positive and negative amplitudes
10 of the transverse wave are shown at 16 and 18, and another maximum
11 positive amplitude is shown at 20. Directions of propagation are
12 respectively at 22 and 24 in opposite directions coaxial with tow
13 cable 10.

14 Referring to FIG. 2a, there is shown a tow cable 26 and the
15 direction of tow 28. Compressed region 30 is shown in which the
16 strain is negative. A stretch region 32 is also shown where the
17 strain is positive. Referring to FIG. 2b, a graph of amplitude of
18 the longitudinal wave against position is shown. The longitudinal
19 wave 34 has a maximum positive amplitude 36, a maximum negative
20 amplitude 38 and another maximum amplitude 40. Directions of
21 propagation are coaxial with the cable at opposite directions 42
22 and 44.

1 Referring to FIG. 3, a ship 46 is shown as well as a body of
2 water 48 and atmosphere 50. Mounted on the deck of the ship 46
3 there is a winch 52. Tow cable 34 extends from winch 52 from a
4 rigid boundary 56 and its proximate end to a free boundary 58 at
5 its distal end. Beyond the free boundary 58 there is a tow
6 component 60 and an accelerometer 62. The accelerometer 62 is in
7 communication with a display 64, which is in communication with a
8 processor 66 which controls the operation of the winch 52 to let
9 out or take in additional tow cable 34.

10 A display at the stop shows acceleration levels. The cable
11 length can be changed at the winch in predetermined amounts
12 (e.g., 100 feet). A history of acceleration levels at each
13 length is built up until the optimal length is obtained which
14 minimizes the acceleration seen by the towed component. The
15 entire process can easily be automated with a personal computer
16 (PC) or some other processor that contains an algorithm that
17 stores the history of acceleration levels vs. cable length and
18 controls the winch to change the cable length until the optimal
19 length is reached.

20 It will be appreciated that a method has been provided which
21 effectively reduces strum in tow cables.

22 While the present invention has been described in connection
23 with the preferred embodiments of the various figures, it is to

1 be understood that other similar embodiments may be used or
2 modifications and additions may be made to the described
3 embodiment for performing the same function of the present
4 invention without deviating therefrom. Therefore, the present
5 invention should not be limited to any single embodiment, but
6 rather construed in breadth and scope,

7

1 Attorney Docket No. 79243

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3 A METHOD FOR REDUCING STRUM IN TOW CABLES

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5 ABSTRACT OF THE DISCLOSURE

6 A method for reducing strum in tow cables. Such tow cables
7 typically extend from a marine vessel and have their lengths
8 controlled by a winch on the deck of the ship and have a tow
9 component at their distal end. The length of the cable is
10 adjusted so that the number of longitudinal waves is an integral
11 number of the number of transverse waves is an odd integral
12 number.

1/2

FIG. 1

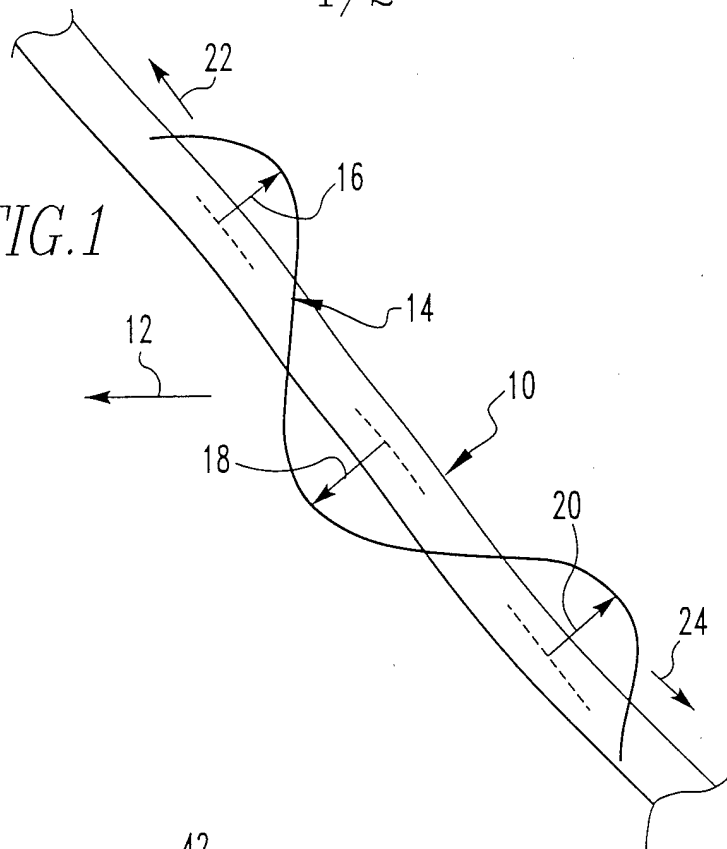


FIG. 2b

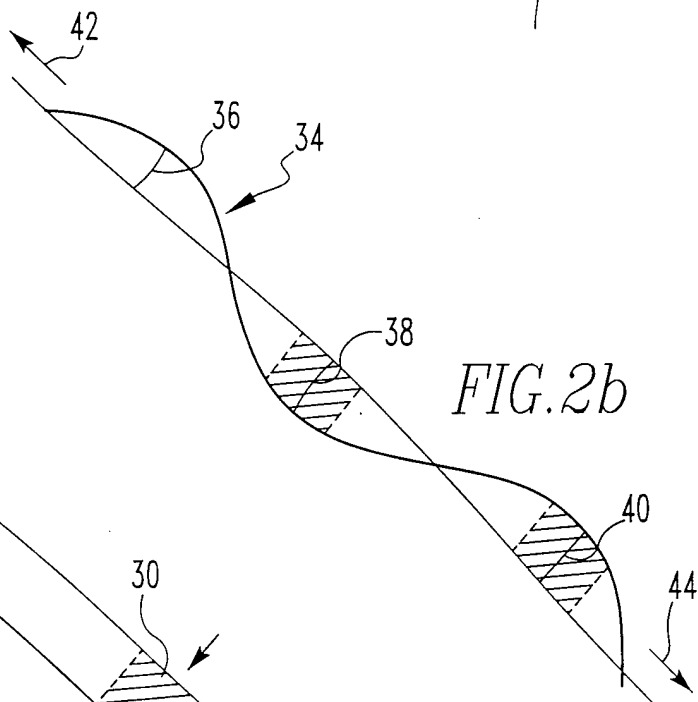
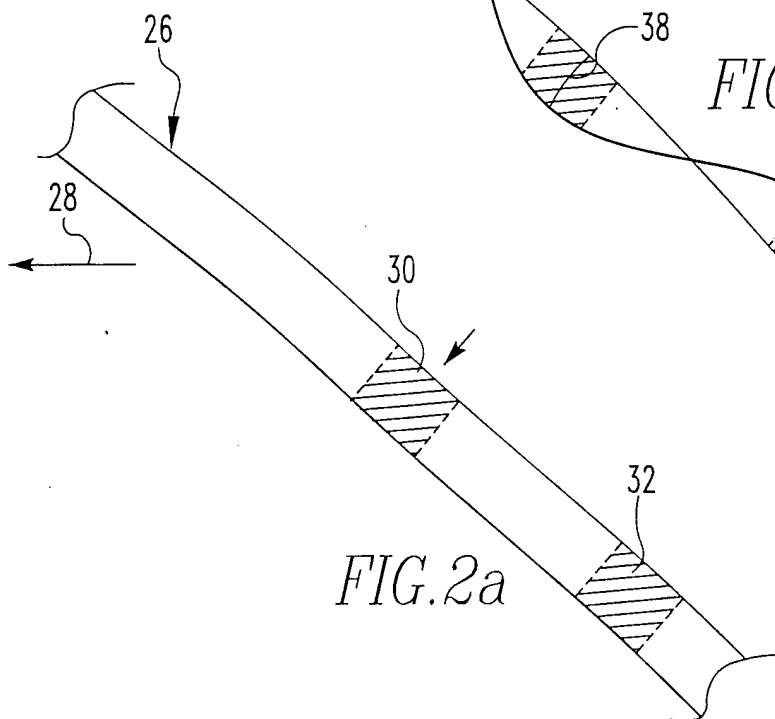


FIG. 2a



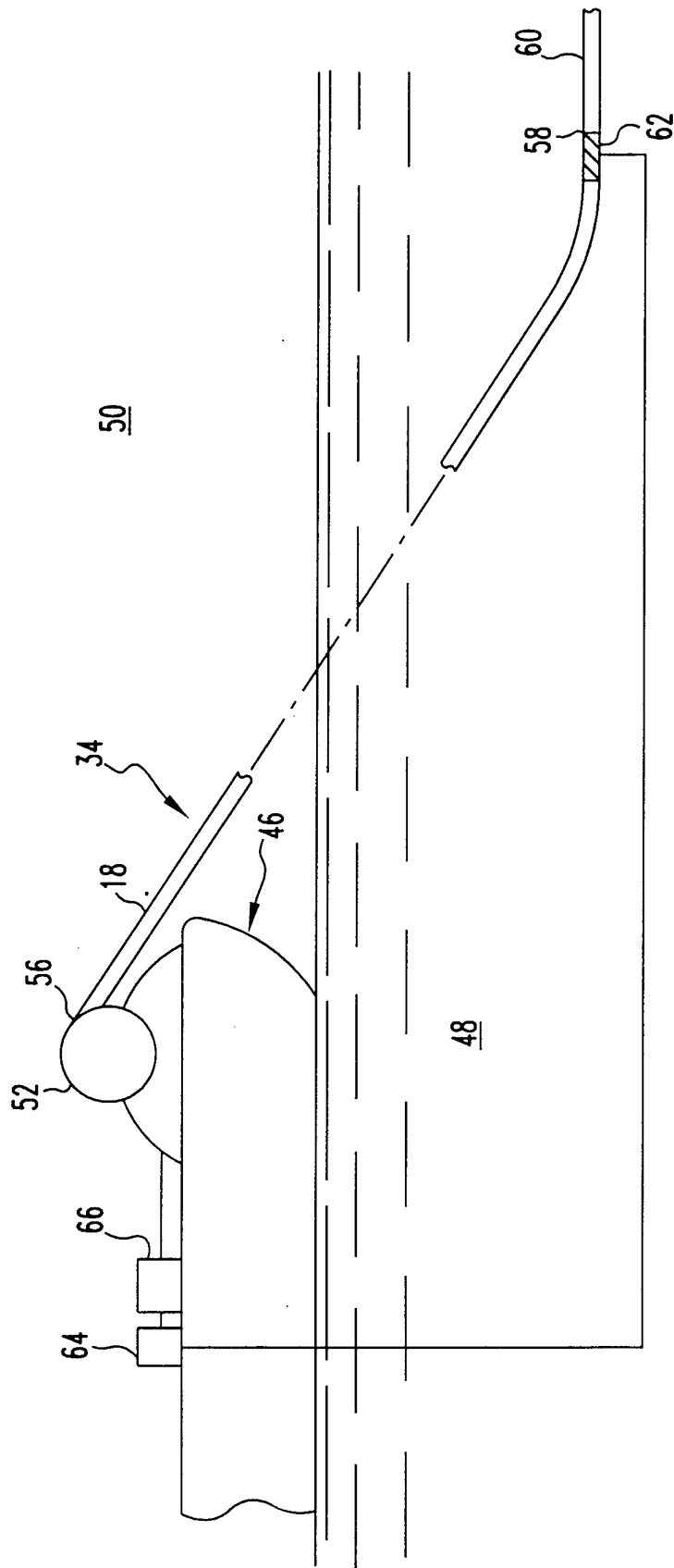


FIG. 3