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3 HORIZONTAL PLASMA ANTENNA USING PLASMA DRIFT CURRENTS

5 STATEMENT OF GOVERNMENT INTEREST

6 The invention described herein may be manufactured and used  
7 by or for the Government of the United States of America for  
8 governmental purposes without the payment of any royalties  
9 thereon or therefor.

11 BACKGROUND OF THE INVENTION

12 (1) Field of the Invention

13 The present invention relates generally to communications  
14 antennas, and more particularly to plasma antennas adaptable for  
15 use in any of a wide range of frequencies.

16 (2) Description of the Prior Art

17 A specific antenna typically is designed to operate over a  
18 narrow band of frequencies. However, the underlying antenna  
19 configuration or design may be adapted or scaled for widely  
20 divergent frequencies. For example, a simple dipole antenna  
21 design may be scaled to operate at frequencies from the 3-4 MHz  
22 band up to the 100 MHz band and beyond.

23 At lower frequencies the options for antennas become fewer  
24 because the wavelengths become very long. Yet there is a  
25 significant interest in providing antennas for such lower  
26 frequencies including the Extremely Low Frequency (ELF) band,

1 that is less than 3 kHz, the Very Low Frequency (VLF) band  
2 including signals from 20 kHz to 60 kHz and the Low Frequency  
3 (LF) band with frequencies in the 90 to 100 kHz band. However,  
4 conventional half-wave and quarter-wave antenna designs are  
5 difficult to implement because at 100 Hz, for example, a quarter-  
6 wave length is of the order of 750 km.

7         Notwithstanding these difficulties, antennas for such  
8 frequencies are important because they are useful in specific  
9 applications, such as effective communications with a submerged  
10 submarine. For such applications, conventional ELF antennas  
11 comprise extremely long, horizontal wires extended over large  
12 land areas. Such antennas are expensive to construct and  
13 practically impossible to relocate at will. An alternative  
14 experimental Vertical Electric Dipole (VEP) antenna uses a  
15 balloon to raise one end of a wire into the atmosphere to a  
16 height of up to 12 km or more. Such an antenna can be relocated.  
17 To be truly effective the antenna should extend along a straight  
18 line. Winds, however, can deflect both the balloon and wire to  
19 produce a catenary form that degrades antenna performance. Other  
20 efforts have been directed to the development of a corona mode  
21 antenna. This antenna utilizes the corona discharges of a long  
22 wire to radiate ELF signals.

23         Still other current communication methods for such submarine  
24 and other underwater environments include the use of mast mounted  
25 antennas, towed buoys and towed submersed arrays. While each of  
26 these methods has merits, each presents problems for use in an

1 underwater environment. The mast of current underwater vehicles  
2 performs numerous sensing and optical functions. Mast mounted  
3 antenna systems occupy valuable space on the mast which could be  
4 used for other purposes. For both towed buoys and towed  
5 submersed arrays, speed must be decreased to operate the  
6 equipment. Consequently, as a practical matter, the use of such  
7 antennas for ELF or other low frequency communications is not  
8 possible because they require too much space.

9         Conventional plasma antennas are of interest for  
10 communications with underwater vessels since the frequency,  
11 pattern and magnitude of the radiated signals are proportional to  
12 the rate at which the ions and electrons are displaced. The  
13 displacement and hence the radiated signal can be controlled by a  
14 number of factors including plasma density, tube geometry, gas  
15 type, current distribution, applied magnetic field and applied  
16 current. This allows the antenna to be physically small, in  
17 comparison with traditional antennas. Studies have been  
18 performed for characterizing electromagnetic wave propagation in  
19 plasmas. Therefore, the basic concepts, albeit for significantly  
20 different applications, have been investigated.

21         With respect to plasma antennas, U. S. Patent No. 1,309,031  
22 to Hettinger discloses an aerial conductor for wireless signaling  
23 and other purposes. The antenna produces, by various means, a  
24 volume of ionized atmosphere along a long beam axis to render the  
25 surrounding atmosphere more conductive than the more remote  
26 portions of the atmosphere. A signal generating circuit produces

1 an output through a discharge or equivalent process that is  
2 distributed over the conductor that the ionized beam defines and  
3 that radiates therefrom.

4 U. S. Patent No. 3,404,403 to Vellase et al. uses a high  
5 power laser for producing the laser beam. Controls repeatedly  
6 pulse and focus the laser at different points thereby to ionize a  
7 column of air. Like the Hettinger patent, a signal is coupled  
8 onto the ionized beam.

9 U. S. Patent No. 3,719,829 to Vaill discloses an antenna  
10 constructed with a laser source that establishes an ionized  
11 column. Improved ionization is provided by means of an auxiliary  
12 source that produces a high voltage field to increase the initial  
13 ionization to a high level to form a more highly conductive path  
14 over which useful amounts of electrical energy can be conducted  
15 for the transmission of intelligence or power. In the Hettinger,  
16 Vellase et al. and Vaill patents, the ionized columns merely form  
17 vertical conductive paths for a signal being transmitted onto the  
18 path for radiation from that path.

19 U. S. Patent No. 3,914,766 to Moore discloses a pulsating  
20 plasma antenna, which has a cylindrical plasma column and a pair  
21 of field exciter members parallel to the column. The location  
22 and shape of the exciters, combined with the cylindrical  
23 configuration and natural resonant frequency of the plasma  
24 column, enhance the natural resonant frequency of the plasma  
25 column, enhance the energy transfer and stabilize the motion of

1 the plasma so as to prevent unwanted oscillations and unwanted  
2 plasma waves from destroying the plasma confinement.

3 U. S. Patent No. 5,450,223 to Wagner et al. discloses an  
4 optical demultiplexer for optical/RF signals. The optical  
5 demultiplexer includes an electro-optic modulator that modulates  
6 a beam of light in response to a frequency multiplexed radio-  
7 frequency information signal.

8 U. S. Patent No. 5,594,456 to Norris et al. discloses an  
9 antenna device for transmitting a short pulse duration signal of  
10 predetermined radio frequency. The antenna device includes a gas  
11 filled tube, a voltage source for developing an electrically  
12 conductive path along a length of the tube which corresponds to a  
13 resonant wavelength multiple of the predetermined radio frequency  
14 and a signal transmission source coupled to the tube which  
15 supplies the radio frequency signal. The antenna transmits the  
16 short pulse duration signal in a manner that eliminates a  
17 trailing antenna resonance signal. However, as with the Moore  
18 antenna, the band of frequencies at which the antenna operates is  
19 limited since the tube length is a function of the radiated  
20 signal.

21 A number of other references disclose various components for  
22 the production of ion beams and ion plasma. For example, U. S.  
23 Patent No. 5,017,835 to Oeschner discloses a high-frequency ion  
24 source for production of an ion beam. The source comprises a  
25 tubular vessel shaped to match the desired shape of the beam and  
26 designed to accommodate an ionizable gas. A coil surrounds the

1 vessel and is coupled to a high-frequency generator through a  
2 resonant circuit. A Helmholtz coil pair matched to the shape of  
3 the vessel generates a magnetic field directed normally to the  
4 axis of the coil surrounding the vessel.

5 U. S. Patent No. 5,225,740 to Ohkawa discloses a method and  
6 apparatus for producing a high density plasma. The plasma is  
7 produced in a long cylindrical cavity by the excitation of a  
8 high-frequency whistler wave within the cavity. This cavity and  
9 the plasma are imbedded in a high magnetic field with magnetic  
10 lines of force passing axially or longitudinally through the  
11 cavity. Electromagnetic energy is then coupled axially into the  
12 cylindrical cavity using a resonant cavity. In one embodiment  
13 electromagnetic energy is coupled radially into the cylindrical  
14 cavity using a slow wave structure.

15 U. S. Patent No. 5,648,701 to Hooke et al. discloses  
16 electrode designs for high pressure magnetically assisted  
17 inductively coupled plasmas. The plasma is formed in a vessel at  
18 a pressure of at least 100 mtorr. An antenna with a  
19 substantially planar face is positioned adjacent a portion of the  
20 vessel for applying an electromagnetic field to the plasma gas  
21 thereby to generate and maintain a plasma. Another magnetic  
22 field is also applied with a component in a direction  
23 substantially perpendicular to the planar face of the antenna.

24 Notwithstanding the disclosures in the foregoing references,  
25 applications for ELF frequencies still use conventional land-  
26 based antennas, commonly called Horizontal Electric Dipole (HED)

1 antennas. There remains a requirement for an antenna that can be  
2 mast mounted or otherwise use significantly less space than the  
3 existing conventional land-based antennas for enabling the  
4 transmission of signals at various frequencies, included ELF and  
5 other low-frequency signals, for transmission in an underwater  
6 environment.

7

8

#### SUMMARY OF THE INVENTION

9 Accordingly it is an object of the present invention to  
10 provide an antenna capable of operation with ELF signals.

11 Another object of this invention is to provide an antenna  
12 that is capable of transmitting signals in different frequency  
13 ranges including the ELF range.

14 Still another object of this invention is to provide an ELF  
15 antenna that is transportable.

16 Yet another object of this invention is to provide an ELF  
17 antenna that can be mounted in a restricted volume.

18 In accordance with this invention, an antenna is formed by  
19 generating a plasma column extending along a horizontal axis in a  
20 gravity field. A magnetic field in a horizontal plane is  
21 directed perpendicularly to the horizontal axis. A modulating  
22 signal controls the magnetic field so that variations in the  
23 field produce a drift current in the plasma. The drift current  
24 varies in accordance with the modulating signal and radiates an  
25 electromagnetic field that is at the frequency of and varies in  
26 accordance with the modulating signal.





1 an output aperture 14 along a horizontal axis 15 through a  
2 coaxial tube 16.

3 When the laser 12 is active, the laser beam interacts with a  
4 medium in the tube 16, normally the atmosphere, to form an  
5 ionized gas column in the tube 16. The plasma comprises ions and  
6 electrons as known in the art. A basic criterion for providing  
7 such an antenna system 10 is that the plasma in the tube 16 have  
8 an electron density of at least  $10^{12}$  electrons per cubic  
9 centimeter.

10 For this application any ionizing mechanism including rf or  
11 electric discharge mechanisms can be substituted for the laser  
12 12. If the tube 16 is closed, the other gases, such as the inert  
13 gases, can fill the tube 16 as the ionizable medium. Whatever the  
14 combination, it is only critical that the ionizing mechanism can  
15 achieve the above-mentioned criterion.

16 Although it may possible to provide that level of ionization  
17 by constantly ionizing the atmosphere, continuous wave ionizers  
18 constantly ionizing the column are prohibitively expensive.  
19 Pulse mode lasers offer a better option as ionizers. In FIGS. 1  
20 and 2 the laser 11 may comprise a CO<sub>2</sub>, Nd:YAG or other laser.  
21 Typically these lasers operate in a pulse mode with a pulse  
22 repetition frequency that is much higher than ELF. For example,  
23 a CO<sub>2</sub> laser may operate with a pulse repetition frequency (PRF)  
24 in the megahertz range; one such CO<sub>2</sub> laser operates at about 67  
25 MHz with a 33% duty cycle.

1           As the laser power supply 12 generates continuous pulses,  
2 the laser beam ionizes the medium in the tube 16 to form the ion  
3 plasma. More specifically, FIG. 3 depicts this action by showing  
4 a pulse train 20 at some pulse repetition frequency with the  
5 pulse train shifting between an ON level 21 and OFF level 22.  
6 The OFF time 22, between successive pulses in the pulse train 20  
7 is selected to limit the amount of relaxation between successive  
8 pulses. For example, the interval is chosen to limit the  
9 relaxation to about 10% of the maximum ionization. A graph 23 in  
10 FIG. 3 shows the effect on the level of ionization of repetitive  
11 pulses having an OFF time corresponding to above criterion.  
12 Although there is a minor variation in the ionization level in  
13 the column during successive pulses, that variation is less than  
14 about 10% of the maximum ionization. Therefore, the variation is  
15 insignificant with respect to the operation of this invention.  
16 What is important is that the plasma in the tube 16 of FIG. 1  
17 continue to meet the concentration criteria for the duration of  
18 any transmission.

19           FIG. 1 also depicts a signal processor or source 24 that  
20 produces an output signal containing information to be  
21 transmitted. The signal processor drives a Helmholtz coil set  
22 25, shown in FIGS. 1 and 2, to generate a uniform magnetic field.  
23 In this particular embodiment, the magnetic field is horizontal  
24 and is perpendicular to the axis 15. In FIGS. 1 and 2 an arrow  
25  $\bar{B}$  32 that lies horizontally in the end view of FIG. 2 represents

1 this field. The two heads on the arrow 32 are included to  
2 demonstrate that the Helmholtz coil set 25 can produce a field  
3 across the tube in either direction. That is, in the orientation  
4 of FIG 2, the magnetic field can have a north-to-south direction  
5 from right to left or from left to right.

6 FIG. 2 also depicts a gravity vector  $\bar{g}$  35. This represents  
7 normal gravity that will act upon the plasma in any application  
8 when the plasma axis is horizontal; i.e., parallel to a tangent  
9 to the earth's surface.

10 With this configuration, a charged particle in the plasma  
11 subjected to a gravity field and a horizontal magnetic field at  
12 right angles to the axis will generate a drift current,  
13 represented mathematically as  $\bar{v}_{DG}^{\alpha}$ . As known, this relationship  
14 is given by:

$$\bar{v}_{DG}^{\alpha} = \frac{m_{\alpha}}{q_{\alpha}} \frac{\bar{g} \times \bar{B}}{q_{\alpha} B^2} c \quad ( 1 )$$

15  
16 where  $m_{\alpha}$  and  $q_{\alpha}$  represent the mass and charge on a charged  
17 particle, such as an ion  $i$ , or electron  $e$ , and  $B$  represents the  
18 magnitude of the magnetic field vector  $\bar{B}$ .

19 The contribution of an ion as a charge carrier in the  
20 gravity and magnetic fields can be specified by:

$$\bar{v}_{DG}^i = \frac{m_i}{q_i} \frac{\bar{g} \times \bar{B}}{q_i B^2} c \quad ( 2 )$$

1

2 Equation (1) also describes the contribution of electrons by  
3 setting  $q = e$ .

4 Still referring to Equation (2), for an alternating field at  
5 a frequency  $\omega$  and where the operator  $R_e$  defines the real  
6 component, the field is given by:

$$\bar{B} = R_e \hat{B} e^{j\omega t} \quad ( 3 )$$

7 Substituting Equation (3) in Equation (2) yields:

$$\bar{v}_{DG}^i = \frac{m_i}{q_i} \frac{R_e \hat{B} e^{j\omega t}}{B^2} c \quad ( 4 )$$

8

9 that indicates the impact of ions on the drift current by  
10 introducing an alternating magnetic field. Solving this equation  
11 yields:

$$\bar{v}_{DG}^i = R_e \left[ \frac{m_i}{q_i} \frac{\bar{g} \times \hat{B}}{B^2} \right] e^{j\omega t} \quad ( 5 )$$

12

13 in which the mass and charge and the peak values of gravity and  
14 magnetic field are considered collectively as a constant. Thus,

1 the magnetic field through the plasma column is the real  
2 component of a constant field times  $e^{j\omega t}$ , the frequency operator.

3 FIG. 4 depicts a portion of the plasma system in which the  
4 magnetic field is directed to enter the paper as represented by  
5 circles 33 with crosses. This represents a north-to-south field  
6 from left to right in FIG. 2. The impact is shown on ions 30  
7 that are moving to the right and electrons 31 that are moving to  
8 the left. According to Equation (5) the velocity is determined  
9 by the magnitude of the magnetic field. When the field reverses  
10 and the field is directed out of the paper, (i.e., a north-to-  
11 south field extending from right to left in FIG. 2), the  
12 direction of travel of the ions 30 and electrons 31 reverse as  
13 shown in FIG. 5 where circles 34 containing central dots denote  
14 the field reversal with respect to the field direction in FIG. 4.

15 From a practical standpoint the contribution to the drift  
16 current of the ions is significantly greater than that of the  
17 electrons. However, the final drift current is the sum of the  
18 ion and electron drift currents and is given by:

$$\bar{v}_{DG} = \bar{v}_{DG}^i + \bar{v}_{DG}^e \quad (6)$$

19  
20 Thus, as the magnetic field changes direction at a given  
21 frequency,  $\omega$ , the current oscillates at the same frequency. It  
22 produces a large dipole moment since it is primarily ion current  
23 oscillating at the plasma frequency which is set equal to this  
24 frequency. Currents in such a horizontal plasma antenna would be

1 greater than those in a conventional antenna, such as a  
2 horizontal electric dipole (HED) antenna, particularly for ELF  
3 applications.

4 As previously indicated, conventional ELF antennas have a  
5 length  $L_A$  that is quite long. In accordance with conventional  
6 antenna analysis, two antennas provide equal radiation if they  
7 have an equal  $I*L$  product where  $I$  is the current in the antenna  
8 and  $L$  is the length of the antenna. Assuming the conventional  
9 antenna has a length  $L_A$ , the length  $L_P$  of the plasma antenna will  
10 be:

$$L_P = \frac{I_A}{I_P} L_A \quad ( 7 )$$

11 where  $I_A$  and  $I_P$  represent the currents in the conventional and  
12 plasma antennas. Thus, if the plasma generates a current  $I_P$  that  
13 has a greater magnitude than the current  $I_A$  of a conventional  
14 antenna, the length  $L_P$  of the plasma antenna can be decreased by  
15 a corresponding amount. It is expected that the ratio  $I_A/I_P$  will  
16 be in a range of about 2 to 5, and may be higher.

17 For applications in which the plasma column 16 in FIGS. 1  
18 and 2 reaches well into the atmosphere a combination of increased  
19 current and length may provide even greater field strengths and  
20 dipole moments than presently available in ELF applications.  
21 That is, if  $I_P > I_A$ , it is possible to construct an antenna with  
22 a length that is less than the length of a conventional HED  
23 antenna. Alternatively if the lengths are the same, the  
24 horizontal plasma antenna will develop a higher electric dipole

1 moment. At high frequencies the antenna can be more flexible  
2 than conventional solid metal antennas. Basically the length can  
3 be considerably shorter than a conventional antenna for a  
4 corresponding frequency. Moreover, the resonant frequency of the  
5 plasma is not dependent on the length of the antenna.

6 As the only hardware associated with the antenna includes  
7 the plasma generating mechanism, signal source and Helmholtz  
8 coils, this construction provides a compact, transportable  
9 antenna structure even for ELF applications. Moreover, this  
10 invention enables the construction of an antenna that is  
11 significantly shorter than a conventional antenna for the same  
12 frequency which provides corresponding electromagnetic radiation.

13 This invention has been described in terms of specific  
14 implementations. As described lasers or other ionizing  
15 mechanisms can be used to provide the plasma. Helmholtz coils  
16 are known for providing a uniform magnetic field; other magnetic  
17 field generators could be substituted. Therefore, it is the  
18 intent to cover all such variations and  
19 modifications as come within the true spirit and scope of this  
20 invention.



2  
3 HORIZONTAL PLASMA ANTENNA USING PLASMA DRIFT CURRENTS

4  
5 ABSTRACT OF THE DISCLOSURE

6 A horizontal plasma antenna is provided. An ionizer  
7 generates an ionizing beam through a horizontal tube to form a  
8 bounded plasma column extending along a horizontal axis in a  
9 gravity field. An amplitude or frequency modulating signal is  
10 applied to Helmholtz coils to control a horizontal magnetic field  
11 that is perpendicular to the horizontal axis. The resulting  
12 changes in the magnetic field produce a drift current in the  
13 plasma that, in turn, radiates an amplitude or phase modulated  
14 electromagnetic field from the plasma column.

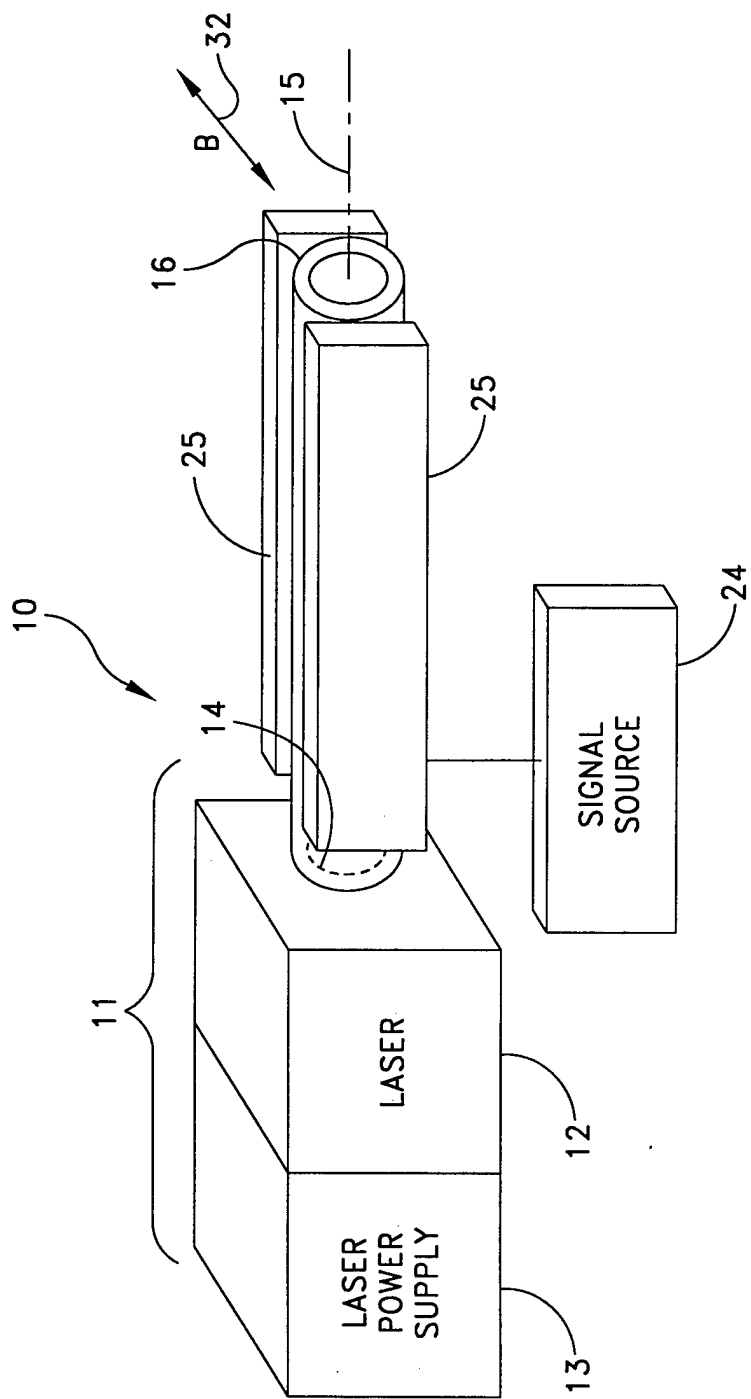


FIG. 1

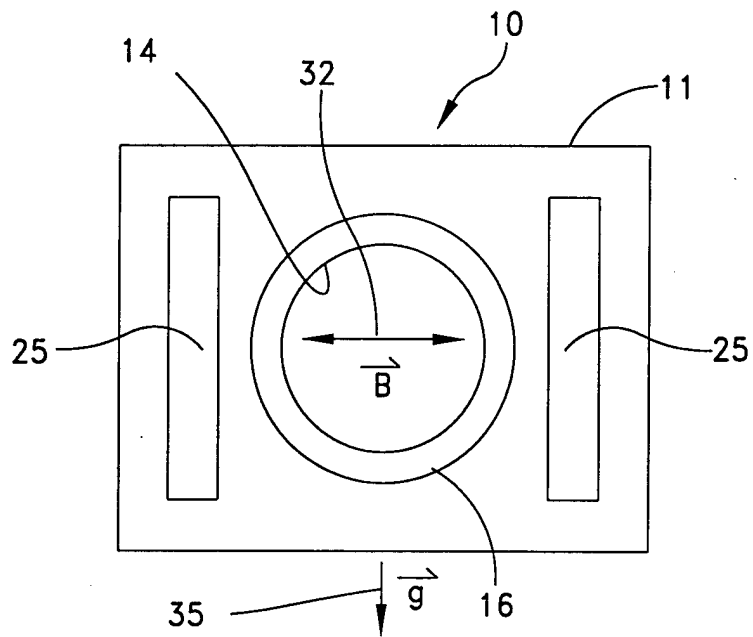


FIG. 2

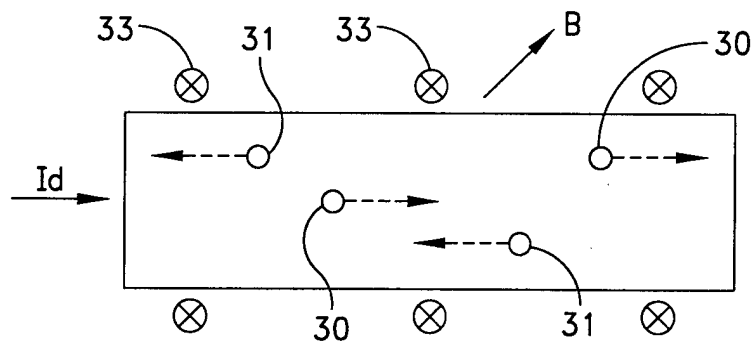


FIG. 4

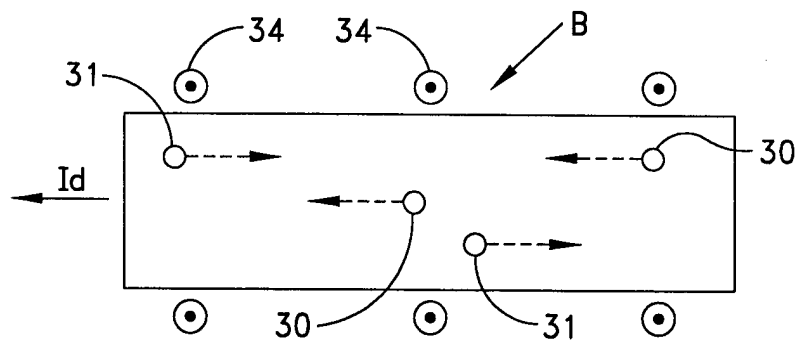


FIG. 5

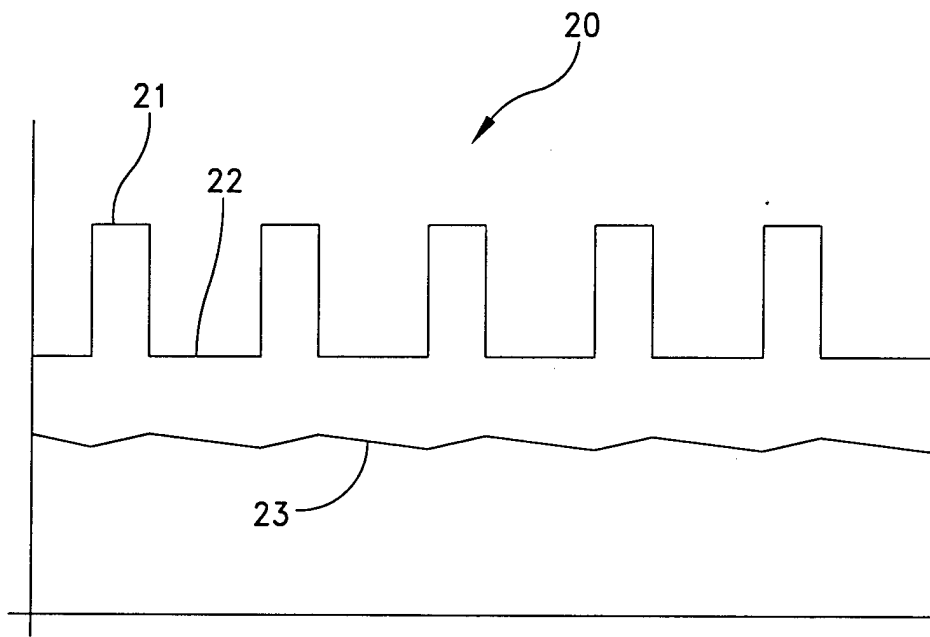


FIG. 3