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VELOCITY REDUCTION METHOD TO REDUCE THE

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FLOW-INDUCED NOISE OF TOWED SENSOR SYSTEMS

5

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STATEMENT OF GOVERNMENT INTEREST

7

The invention described herein may be manufactured and  
8 used by or for the Government of the United States of America  
9 for governmental purposes without the payment of any royalties  
10 thereon or therefor.

11

12

BACKGROUND OF THE INVENTION

13

(1) Field of the Invention

14

This invention generally relates to a velocity reduction  
15 method for reducing the flow-induced noise of towed sensor  
16 systems. More particularly, the invention relates to a method  
17 for reducing the tow velocity of a hydrophone system while  
18 keeping the tow vessel speed constant and therefore reducing  
19 the flow-induced noise received by the hydrophones without  
20 affecting ship trajectory or operation. By reducing the flow-  
21 induced noise, higher quality data can be obtained.

22

(2) Description of the Prior Art

23

Arrays of pressure sensors are used in both commercial  
24 and military systems for the reception of sound waves in  
25 water, air, or other fluids. The array is a multi-sensor  
26 system which allows for the simultaneous acquisition of  
27 signals from spatially separated locations. Commercial towed  
28 systems use hydrophone arrays to locate oil deposits beneath

1 the ocean floor. Military systems use pressure sensor arrays  
2 to locate and classify acoustic targets (e.g., a ship or  
3 submarine in water or a tank in air). A fundamental  
4 limitation of towed systems of pressure sensors is the flow-  
5 induced noise. This non-acoustic noise is generated by  
6 pressure fluctuations at the solid/fluid interface of the  
7 structure containing the sensors. Some part of the noise is  
8 transmitted through the structure and received by the pressure  
9 sensors. The resulting unwanted noise is termed, "self-noise"  
10 because it is the resulting noise of the system in the absence  
11 of any acoustic signals. The flow-induced noise is directly  
12 related to the speed of the array system relative to the  
13 surrounding fluid. Turbulence scaling has shown that the  
14 magnitude of the direct flow noise is proportional to the  
15 velocity cubed ( $U_0^3$ ) when a fully developed turbulent boundary  
16 layer is present.

17 By reducing or eliminating the self-noise induced by the  
18 flow of fluid relative to the pressure sensors, performance of  
19 the pressure sensors (e.g., detection range or signal-to-noise  
20 ratio) can be maximized. The following patents, for example,  
21 disclose various attempts at noise control in arrays:

1 U.S. Patent No. 2,729,300 to Paslay et al;  
2 U.S. Patent No. 3,281,767 to Cryar;  
3 U.S. Patent No. 3,286,225 to Huckabay et al;  
4 U.S. Patent No. 4,314,363 to Thigpen et al;  
5 U.S. Patent No. 4,566,083 to Thigpen;  
6 U.S. Patent No. 4,570,245 to Thigpen;  
7 U.S. Patent No. 4,581,723 to Savit;  
8 U.S. Patent No. 5,113,376 to Bjerkoy; and  
9 U.S. Patent No. 5,345,522 to Vali et al.

10 Specifically, Paslay et al. disclose a water borne means  
11 for making seismic surveys of underwater deposits of oil by  
12 seismic signals received by a plurality of detecting devices  
13 disposed within an elongated flexible streamer. The streamer  
14 is slightly positively buoyant when immersed in the water and  
15 is provided with a plurality of weights suspended therefrom at  
16 intervals and adapted to cause the streamer assembly to be  
17 neutrally buoyant when towed through the water at a high rate  
18 of speed by a moving vessel whereby the streamer slowly sinks  
19 through the water at the points of connection with the weights  
20 as the forward end of the streamer is momentarily brought to  
21 rest during the towing operation and the sections of the  
22 streamer intermediate the weights slowly rise within the  
23 water. An arrangement is thus provided in which only the  
24 forward end of the streamer is momentarily brought to rest,  
25 the remainder of the streamer continuing forward movement as a  
26 shot is fired and the entire length of the streamer is  
27 maintained in tension during the reception of the seismic  
28 signals whereby fortuitous noises of spurious character caused

1 by a release of the towing strain within the streamer and  
2 extraneous noise signals from the lead-in connecting the  
3 streamer and the vessel are prevented from being picked up by  
4 the detecting devices. Accordingly, the patent to Paslay et  
5 al. describes a system in which the array is designed to stop  
6 and physically touch the ocean floor. The weighted streamer  
7 is used to sink the array when its motion is minimized, thus  
8 the array is not maintained at a constant depth.

9 The patent to Cryar discloses a method and apparatus for  
10 continuous marine seismic surveying, in which a seismic  
11 impulse source is transported along the surface of a marine  
12 body and produces seismic impulses at intervals, the  
13 reflections of which from the marine bottom and sub-bottom  
14 strata are detected and recorded to produce a profile of the  
15 subsurface conditions. Accordingly, Cryar describes the  
16 simultaneous deployment and retrieval of two hydrophones or  
17 groups of hydrophones (an array) such that one is "always at a  
18 condition of minimum movement in the water." However, there  
19 is no consideration or understanding in Cryar of the effect  
20 that the negatively buoyant tow cable therein will have on the  
21 system, and two separate arrays must be used.

22 Huckabay et al. disclose a continuous marine seismic  
23 surveying system whose intent is to improve the signal-to-  
24 noise ratio in continuous marine seismic surveying by  
25 periodically stopping or slowing the motion of the towed  
26 detector member, so that during a portion of the survey  
27 operating cycle the hydrophone array can be dead in the water.  
28 During this portion of the cycle, the requisite function of

1 transducing the returned pressure waves can take place with  
2 little or no noise interference generated in the hydrophones.  
3 The system has the capability of conducting a continuous  
4 survey of an area from a craft moving at a substantially  
5 constant speed. Although Huckabay et al. describe the basic  
6 concept of "stopping or slowing" the motion of the towed array  
7 to improve a signal-to-noise ratio, only the use of a  
8 neutrally buoyant array or "streamer" is described.  
9 Accordingly, Huckabay et al. fail to recognize or address the  
10 effect of a non-neutrally buoyant tow cable on the array  
11 shape.

12 Thigpen et al. disclose a marine seismic cable handler  
13 which is a hydraulically-powered yo-yo reel for handling a  
14 marine seismic cable in shallow water. At the beginning of a  
15 recording episode, a partially reeled-in seismic cable is  
16 released to drift to a standstill behind a ship. Data are  
17 recorded. The cable is then accelerated to match the ship's  
18 velocity. Following the initial acceleration, the cable is  
19 super-accelerated as it is partially reeled in. A  
20 microprocessor adjusts a dwell time between recording episodes  
21 to compensate for small variations in the ship's velocity. It  
22 is acknowledged that the patent to Thigpen et al. describes  
23 the basic concept of deploying the tow cable to decelerate the  
24 array to a standstill and mentions the need for maintaining a  
25 constant array depth; but proposes achieving these results via  
26 chains or buoys and does not describe a system using a  
27 neutrally buoyant tow cable.

1           Thigpen '083 discloses a seismic timing control system  
2 for optimizing the acoustic signal-to-noise ratios during a  
3 useful maximal-length recording cycle within the time frame of  
4 a minimal-length recording episode. To implement the method,  
5 during an intermittent-tow seismic operation, the noise level  
6 due to cable manipulation during an entire recording episode  
7 is monitored. A quiet-window of a desired length is  
8 established by adjusting the length of the interval during  
9 which the seismic cable is at rest. The initiation of a  
10 recording cycle is adjusted relative to the quiet window to  
11 take maximum advantage of the quiet period. Although Thigpen  
12 '083 describes the basic concept of deploying the tow cable to  
13 decelerate the array to a standstill and mentions the need for  
14 maintaining a constant array depth, these results are again  
15 obtained by provided chains or buoys to the array. Thigpen  
16 '083 does not describe a system using a neutrally buoyant tow  
17 cable.

18           Thigpen '245 discloses a constant tensioner for a seismic  
19 marine cable or towed seismic cable, wherein the instantaneous  
20 towing force and the instantaneous cable displacement relative  
21 to a fixed shipboard reference are continuously measured and  
22 sampled. A microprocessor associated with a servo controlled  
23 capstan device uses those measurements to pay out cable or to  
24 retrieve cable in response to an increase or decrease in the  
25 instantaneous towing force. The microprocessor also tries to  
26 minimize the average cable displacement. Accordingly, Thigpen  
27 '245 describes a system to maintain constant tow cable tension  
28 via deployment and retrieval of the tow cable. This system is

1 only for small displacement and not the gross motions needed  
2 to effect flow-induced noise reduction.

3       The patent to Savit discloses a method for maintaining a  
4 substantially constant tension on a towed seismic cable,  
5 wherein the instantaneous towing force and the instantaneous  
6 cable displacement relative to a fixed shipboard reference are  
7 continuously measured and sampled. A microprocessor  
8 associated with a servo controlled capstan device uses those  
9 measurements to pay out cable or to retrieve cable in response  
10 to an increase or decrease in the instantaneous towing force.  
11 The microprocessor also tries to minimize the average cable  
12 displacement. As with Thigpen '245, Savit is primarily  
13 describing a system to maintain constant tow cable tension via  
14 deployment and retrieval of the tow cable and is thus only for  
15 small displacement.

16       The patent to Bjerkoy discloses a method for conducting  
17 seismic surveys in waters covered with ice. Seismic impulses  
18 are actuated under water and reflected signals are detected by  
19 a streamer cable towed behind a vessel in order to avoid the  
20 source of noise located outside of the seismic system due to  
21 the ice-breaking operation of the vessel. The vessel is  
22 stopped during active survey and the streamer cable is hauled  
23 in with a speed corresponding to the desired propulsion speed  
24 of the cable during detection. After detection, the vessel  
25 again resumes ordinary operational speed and the streamer is  
26 paid out with a speed which maintains the desired advancing  
27 speed of the system. Bjerkoy is therefore confined to the



1 retrieval of an array when the tow vessel is not moving. This  
2 method cannot be used for a continuously moving vessel.

3 Vali et al. disclose a reduced noise fiber optic towed  
4 array and method of using the same wherein the fiber sensors  
5 are connected in parallel, and the optical fiber cable is paid  
6 out from the towing ship at a velocity about equal to but  
7 opposite to the velocity of the towing ship. Turbulence and  
8 acceleration noise is reduced due to the manner in which the  
9 fiber cable is paid out, and crosstalk between sensors is  
10 eliminated. Although Vali et al. describe the basic concept  
11 of paying out the tow cable to reduce the array velocity to  
12 zero, a negatively buoyant tow cable as used therein will  
13 cause the front end of the array to sink dramatically when the  
14 speed of the array is reduced to zero or near-zero.

15

16

#### SUMMARY OF THE INVENTION

17 Therefore it is an object of this invention to provide a  
18 system and apparatus for reducing flow-induced noise of towed  
19 sensor systems.

20 Another object of this invention is to provide a system  
21 and apparatus for reducing flow-induced noise of towed sensor  
22 systems in which a relative velocity is reduced between a  
23 towed array and the surrounding water.

24 Still another object of this invention is to provide a  
25 system and apparatus for reducing flow-induced noise of towed  
26 sensor systems in which a relative velocity is reduced between  
27 a towed array and the surrounding water by providing a  
28 neutrally buoyant towed sensor system.

1           A still further object of the invention is to provide a  
2 system and apparatus for reducing flow-induced noise of towed  
3 sensor systems in which a relative velocity is reduced between  
4 the towed array and the surrounding water by providing a  
5 neutrally buoyant tow cable.

6           Yet another object of this invention is to provide a  
7 system and apparatus for reducing flow-induced noise of towed  
8 sensor systems which is simple to manufacture and easy to use.

9           In accordance with one aspect of this invention, there is  
10 provided a system for reducing flow-induced noise in an  
11 underwater towed system. The system includes at least one  
12 neutrally buoyant towed array, a tow platform for defining a  
13 towed direction of the at least one towed array, a neutrally  
14 buoyant tow cable connected to the at least one towed array  
15 and the tow platform, and a deploy and retrieve apparatus for  
16 deploying and retrieving the tow cable. The deploy and  
17 retrieve apparatus is connected to both the tow cable and the  
18 tow platform. Deployment of the tow cable from the deploy and  
19 retrieve apparatus correspondingly deploys the at least one  
20 towed array, and retrieval of the tow cable with the deploy  
21 and retrieve apparatus correspondingly retrieves the at least  
22 one towed array.

23

24                           BRIEF DESCRIPTION OF THE DRAWINGS

25           The appended claims particularly point out and distinctly  
26 claim the subject matter of this invention. The various  
27 objects, advantages and novel features of this invention will  
28 be more fully apparent from a reading of the following

1 detailed description in conjunction with the accompanying  
2 drawings in which like reference numerals refer to like parts,  
3 and in which:

4 FIG. 1 is a schematic view of a proposed system according  
5 to a first preferred embodiment of the present invention;

6 FIG. 2 is a schematic view of a proposed system according  
7 to a second preferred embodiment of the present invention;

8 FIG. 3 is a graph illustrating an estimated change in  
9 wall pressure spectral level with a change in tow speed  
10 according to the present invention;

11 FIG. 4 is a graph illustrating a tow cable deployment  
12 rate according to the present invention; and

13 FIG. 5 is a graph illustrating data acquisition time as a  
14 function of relative tow speed.

15

16 DESCRIPTION OF THE PREFERRED EMBODIMENT

17 In general, the present invention is directed to a system  
18 for reducing a tow velocity of a hydrophone system while  
19 keeping a tow vessel speed constant and therefore reducing  
20 flow-induced noise received by the hydrophone system without  
21 affecting either a trajectory or operation of a ship. By  
22 reducing the flow-induced noise received by the hydrophone  
23 system, higher quality data can be obtained.

24 Referring first to FIG. 1, a schematic of a first  
25 proposed system according to the present invention, the  
26 structure for achieving the system is relatively simple and  
27 includes a towed system 10 such as a hydrophone system, a tow  
28 platform 12 which determines the direction (indicated by arrow

1 12a) of the towed system 10, a tow cable deploy and retrieve  
2 system 14 mounted to the tow platform 12, and a tow cable 16  
3 operatively connected to the tow cable deploy/retrieve system  
4 14 and the towed system 10. It should be understood that  
5 generally the environment in question is an underwater  
6 environment and that the towed system 10 illustrated herein is  
7 therefore in an underwater environment and the tow platform 12  
8 is generally situated on the surface of the water.

9 The towed system 10 is described herein as a hydrophone  
10 array, however, the application is suitable to any underwater  
11 towed system which is affected by flow turbulence and the  
12 noise generated therefrom. The tow platform 12 may be a  
13 barge, ship, or any other suitable surface vessel. Further,  
14 the tow cable deploy and retrieve apparatus 14 may be a pulley  
15 member or any other similar structure that is intended to reel  
16 in and reel out a length of cable 16. It will further be  
17 appreciated that the environment may be an air environment  
18 with the tow platform 12 being an airborne vehicle, or the tow  
19 platform 12 may be a submarine rather than a surface vessel.

20 The primary source of unwanted noise in towed hydrophone  
21 systems 10 is the noise induced by the turbulent flow of fluid  
22 (e.g., water or air) over the structure containing the  
23 hydrophones. Although not specifically shown due to the  
24 variety of options available, the hydrophone system 10 may be  
25 in a cylindrical shell, a flat plate, or other comparable  
26 housing. By reducing a relative velocity between the  
27 hydrophone system 10 and the surrounding water, a magnitude of  
28 the fluctuating noise induced by the turbulent boundary layer

1 will be decreased. The turbulent boundary layer is defined as  
2 the layer of fluid which passes over the surface of the  
3 hydrophone system housing 10. The direct pressure flow noise  
4 scales as a function of velocity cubed, so significant  
5 reductions in flow noise are possible with modest decreases in  
6 tow speed. The method allows for the reduction in a velocity  
7 of the hydrophone array while maintaining a constant velocity  
8 of the tow platform 12 (also referred to as the tow point,  
9 e.g., a ship or tow body).

10 A fundamental way to decrease the flow-noise of a towed  
11 system 10 is to decrease the tow speed. Because it is not  
12 desirable to decrease the speed of the tow platform 12, the  
13 speed of the towed system 10 must be decreased independently.

14 This can be accomplished by increasing a deployment length of  
15 the tow cable 16 at a velocity corresponding to the desired  
16 decrease in relative velocity of the towed system 10. For  
17 example, if the tow platform 12 is traveling at a speed of 10  
18 knots and the desired absolute speed of the towed system 10 of  
19 hydrophones is 4 knots, then the relative velocity between the  
20 tow platform 12 and the towed system 10 must be 6 knots. The  
21 tow cable 16 must then be deployed at a speed of 10.1 feet per  
22 second relative to the tow platform 12. In FIG. 1, rotation  
23 of deploy/retrieve system 14 in the direction indicated by  
24 arrow 14a, provides a relative motion of towed system 10 with  
25 aspect to tow platform 12 as indicated by 10a.

26 Both the tow cable 16 and the towed system 10 are formed  
27 so as to be neutrally buoyant, thereby preventing the  
28 hydrophone system 10 from sinking as the tow cable 16 is

1 deployed. This feature of providing both a neutrally buoyant  
2 tow cable 16 and neutrally buoyant towed system has not  
3 previously been proposed in the art. Instead, it was thought  
4 that the neutrally buoyant towed system 10 and the speed at  
5 which the system was towed would compensate for non-neutrally  
6 buoyant tow cables.

7 Further, any electrical connections to the hydrophone  
8 system 10 may be maintained via a slip-ring conductor (not  
9 shown) within the deploy/retrieve system 14. The data  
10 connection could also be maintained through a slip-ring or  
11 with a wireless short-range transmit/receive unit (not shown).

12 In FIG. 1, the towed system 10 is deployed from the tow  
13 platform 12 until the available tow cable 16 length is  
14 reached. Then, the array 10 is retrieved so that another  
15 deployment cycle may begin. It should be understood that  
16 multiple systems may be implemented so that one system is  
17 always being deployed.

18 FIG. 2 illustrates another possible system where there  
19 are actually two hydrophone systems 20, 30 connected in a  
20 looped and neutrally buoyant tow cable 22. More specifically,  
21 the tow cable 22 is looped around a remote tow cable  
22 deploy/retrieve structure 24 and the tow cable 22 is a  
23 continuous loop. The reeling structure 24 is intentionally  
24 provided to be remote from the tow platform 12, the reeling  
25 structure 24 having the tow cable 22 looped therearound. With  
26 the reeling structure 24 being positioned remote from the tow  
27 platform 12, a separate attachment line 26 is provided between  
28 the tow platform 12 and the reeling structure 24. Although

1 not specifically shown, it is also contemplated that the  
2 reeling structure 24 may be mounted to the tow platform 12 as  
3 in the embodiment of FIG. 1. If the reeling structure 24 is  
4 in fact remote from the tow platform 12, the reeling structure  
5 24 will be underwater during operation. While one system 20  
6 is being deployed to reduce the absolute speed of deployment  
7 (indicated by arrow 20a) of that system and thus the self-  
8 noise, the other system 30 is being retrieved as indicated by  
9 arrow 30a. All remaining structure is similar to that shown  
10 in FIG. 1 and will not be repeated herein for the sake of  
11 brevity.

12 Turbulence research has shown that the pressure flow  
13 noise on the outside of a towed structure, such as a flat  
14 plate or a cylinder in axial flow, scales with the "free  
15 stream velocity" raised to the third power. In this case, the  
16 "free stream velocity" is the speed of the towed system 10  
17 relative to the surrounding fluid. A typical scaling of the  
18 wall pressure frequency spectrum is

$$20 \quad \Phi(\omega) = F\left(\frac{\omega\delta^*}{U_0}\right) \rho^2 \delta^* U_0^3 \quad (1)$$

21  
22 where F is a universal function of the non-dimensional  
23 frequency  $\omega\delta^*/U_0$ . Here  $\Phi(\omega)$  is the frequency power spectrum of  
24 the pressure fluctuation of the outside of the structure  
25 containing the hydrophones,  $\rho$  is the surrounding fluid  
26 density,  $\delta^*$  is the boundary layer displacement thickness, and  
27  $U_0$  is the free stream velocity. The function F is relatively

1 constant at low values of non-dimensional frequency (e.g.  
 2  $\omega\delta^* / U_0 < 0.1$ ). Therefore, the reduction in wall pressure  
 3 power spectrum can be estimated with a reduction in free  
 4 stream  
 5 velocity by using equation (1) and holding F constant. For  
 6 example, the ratio of the power spectra from speed 1 and 2  
 7 are,

$$8 \quad \frac{\Phi_2(\omega)}{\Phi_1(\omega)} = \frac{\left[ F\left(\frac{\omega\delta^*}{U_0}\right) \rho^2 \delta^* U_0^3 \right]_{\text{speed 2}}}{\left[ F\left(\frac{\omega\delta^*}{U_0}\right) \rho^2 \delta^* U_0^3 \right]_{\text{speed 1}}} \approx \frac{U_0^3|_{\text{speed 2}}}{U_0^3|_{\text{speed 1}}} = \left(\frac{U_2}{U_1}\right)^3 \quad (2)$$

9  
 10 where the right part of the equation (2) holds if the boundary  
 11 layer displacement thickness and the function F do not change  
 12 significantly. The power spectrum change, R, in decibels (dB)  
 13 is then approximated as,

$$14 \quad R \approx 10 \log_{10} \left[ \left(\frac{U_2}{U_1}\right)^3 \right] = 30 \log_{10} \left(\frac{U_2}{U_1}\right). \quad (3)$$

15  
 16 For a tow platform speed,  $U_1$  of 15 knots, the change in wall  
 17 pressure power spectrum (from the turbulent boundary layer) is  
 18 shown in FIG. 3 as a function of the difference in speed  
 19 between the towed system 10 and the tow platform 12,  $U_2 - U_1$ .  
 20 Negative decibel values indicate a reduction while positive  
 21 values indicate an increase in power spectrum level. For  
 22 example, a spectral noise reduction on the order of 14 dB is  
 23 possible if the towed system velocity is decreased by 10 knots  
 24 from 15 knots to an absolute speed of 5 knots.



1 The relative velocity between the towed system 10 and the tow  
2 platform 12 dictates that the tow cable 16 length must  
3 dynamically change as a function of time. For a steady state  
4 situation, the required deployment rate of the tow cable 16 is  
5 equal to the same relative velocity of the towed system 10.

6 FIG. 4 shows the cable deployment rate as a function of  
7 relative velocity. The available tow cable 16 length will  
8 dictate the time available for data acquisition unless a  
9 circular system, such as that shown in FIG. 2, is used.

10 FIG. 5 shows the available data acquisition time for an  
11 available tow cable 16 length of 1500 feet. For example, if  
12 the towed system 10 speed is decreased by 5 knots, 3 minutes  
13 of time are available for data acquisition.

14 The primary advantage of the proposed systems is the  
15 reduction of flow-induced noise in a towed system via a  
16 reduction in the velocity of the towed system 10, 20, or 30  
17 independent of the speed of the tow platform 12. These noise  
18 reductions maximize the system performance by eliminating or  
19 significantly reducing the flow-induced noise for a particular  
20 acoustic environment. This type of feature for a towed system  
21 is not known to currently exist. Even if the flow-induced  
22 noise is eliminated, any system will still be limited to some  
23 extent by other factors such as ambient and electronic noise.

24 By the present invention, a system is achieved in which  
25 flow-induced noise from a towed array is substantially  
26 eliminated in a more efficient manner than previously achieved  
27 in the art.

1           This invention has been disclosed in terms of certain  
2   embodiments. It will be apparent that many modifications can  
3   be made to the disclosed apparatus without departing from the  
4   invention. Therefore, it is the intent  
5   to cover all such variations and modifications as come within  
6   the true spirit and scope of this invention.

VELOCITY REDUCTION METHOD TO REDUCE THE

FLOW-INDUCED NOISE OF TOWED SENSOR SYSTEMS

ABSTRACT OF THE DISCLOSURE

7 A system and method are disclosed for reducing flow-  
8 induced noise in an underwater towed system. The system  
9 includes at least one neutrally buoyant towed array, a tow  
10 platform for defining a towed direction of the at least one  
11 towed array, a neutrally buoyant tow cable connected to the at  
12 least one towed array and the tow platform, and a deploy and  
13 retrieve apparatus for deploying and retrieving the tow cable.  
14 The deploy and retrieve apparatus is connected to both the  
15 tow cable and the tow platform. Deployment of the tow cable  
16 from the deploy and retrieve apparatus correspondingly deploys  
17 the at least one towed array, and retrieval of the tow cable  
18 with the deploy and retrieve apparatus correspondingly  
19 retrieves the at least one towed array. The speed of  
20 deployment of the tow cable can be varied to decrease the  
21 velocity of the towed array relative to the surrounding water  
22 thus reducing flow-induced noise.

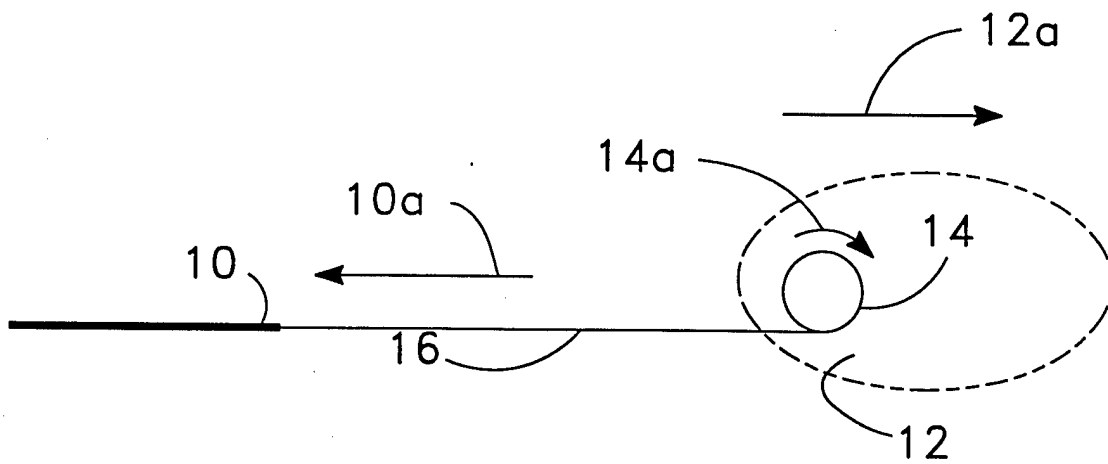


FIG. 1

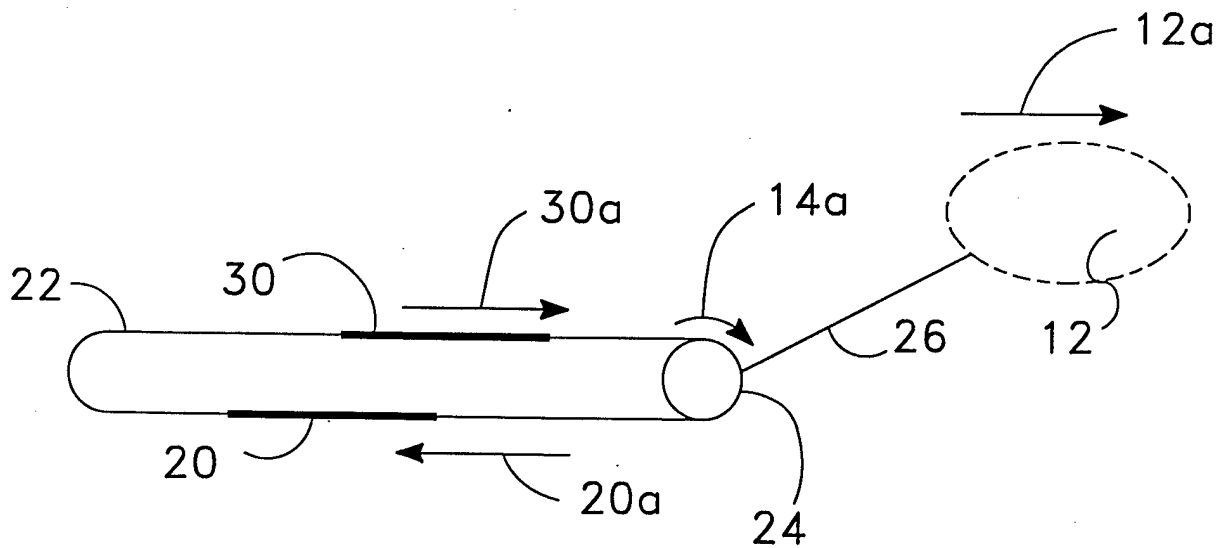


FIG. 2

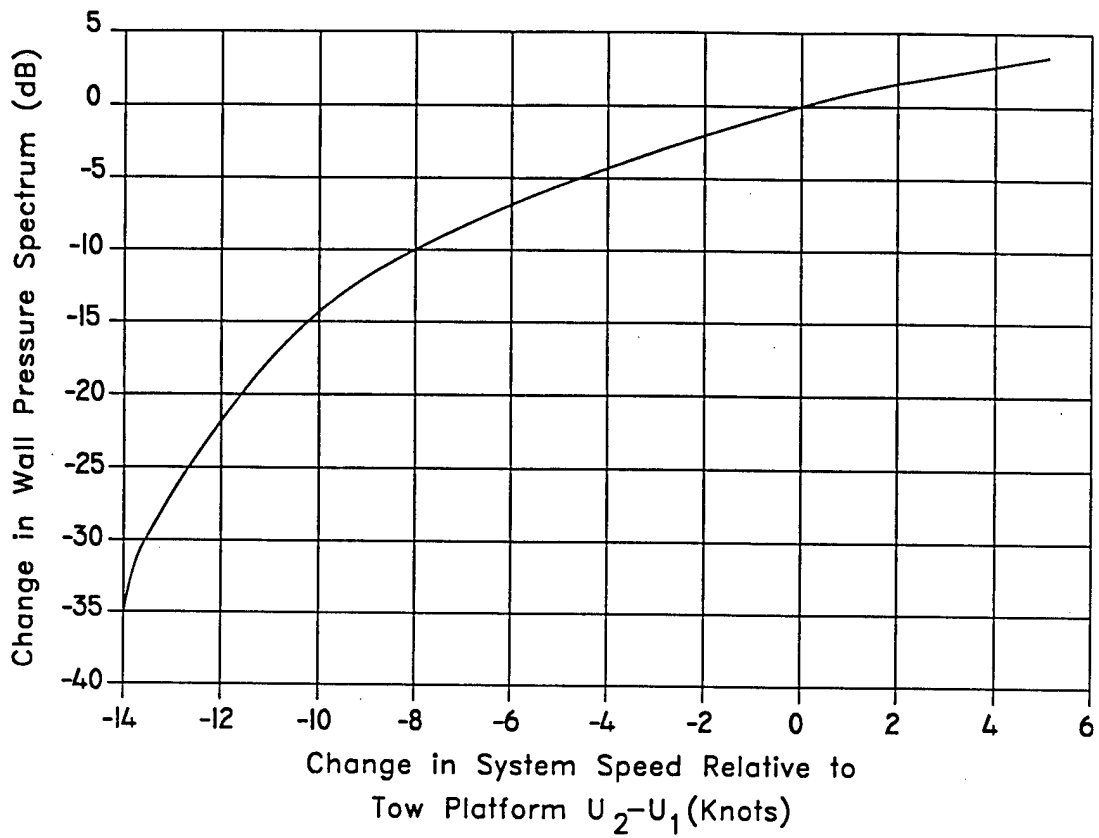


FIG. 3

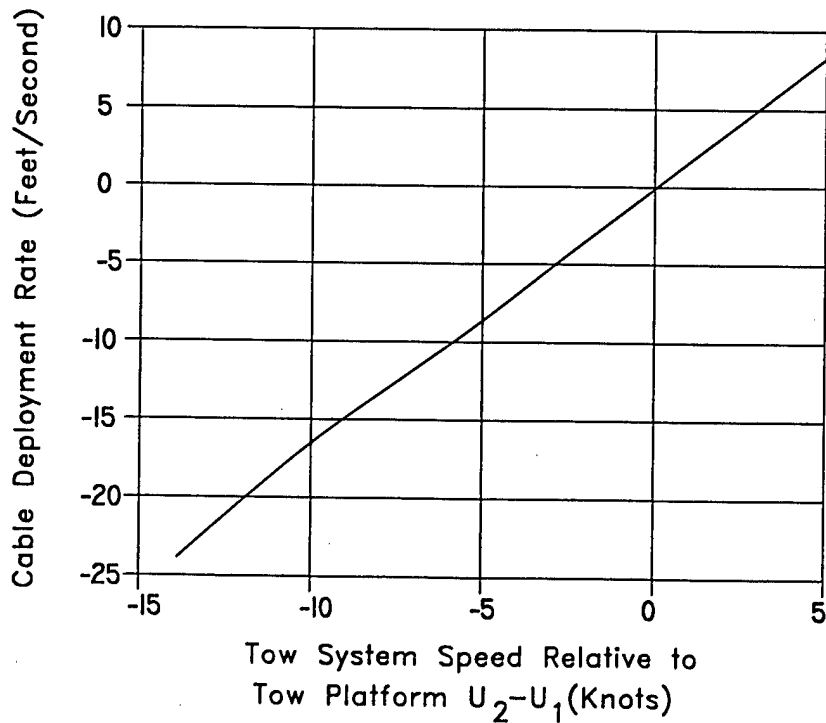


FIG. 4

Available Cable Deployment Length -1500 Feet

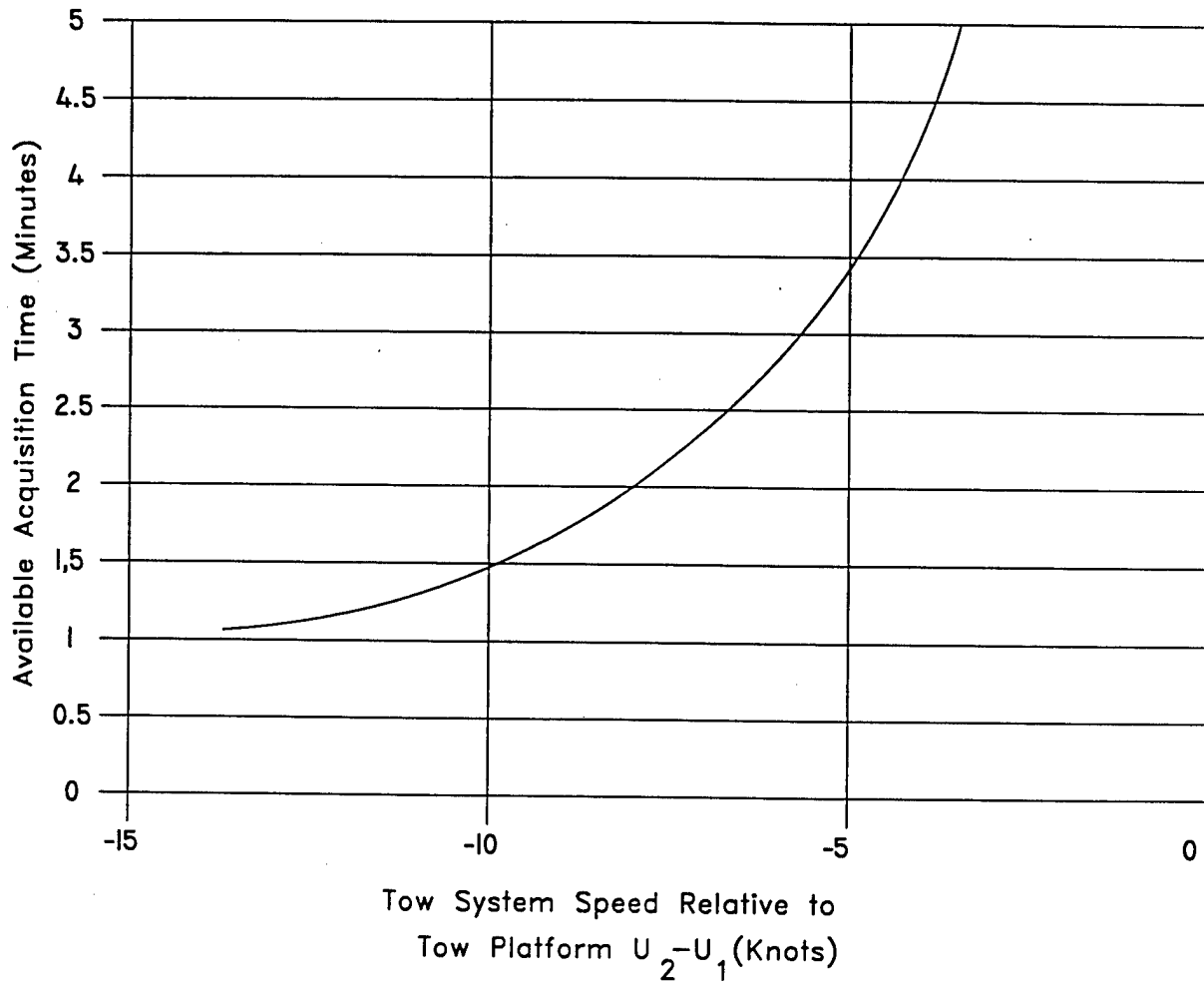


FIG.5