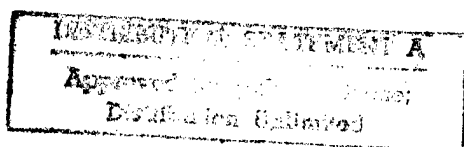


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NOTICE

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2  
3 BEAM PATTERN SHAPING FOR TRANSMITTER ARRAY

4  
5 STATEMENT OF GOVERNMENT INTEREST

6 The invention described herein may be manufactured and  
7 used by or for the Government of the United States of America  
8 for Governmental purposes without the payment of any royalties  
9 thereon or therefor.

10  
11 BACKGROUND OF THE INVENTION

12 (1) Field of the Invention

13 The present invention relates generally to controlling  
14 transmitters such as sonar transmitters, and more particularly  
15 to a method and system for controlling the output of an array  
16 of transmitters in order to achieve a desired beam pattern.

17 (2) Description of the Prior Art

18 In sonar applications using an array of transmitters, it  
19 is desirable for each transmitter to be transmitting the same  
20 power at any given time in order to produce a beam pattern that  
21 maximizes the transmitted energy for a given power constraint.  
22 To provide a background to beamforming, the following briefly  
23 describes a typical situation that requires beamforming and a  
24 number of approaches that can be used.

25 Consider a plurality of transducers where each transducer  
26 transmits a signal that can be adjusted in amplitude and

1 delayed in time. Together, the transmitted signals add  
2 constructively in certain directions and destructively in other  
3 directions. This variation in the gain profile provides a beam  
4 pattern. A typical beam pattern has a main lobe in the main  
5 axis and a number of side lobes in the off-axis directions. It  
6 is desirable in some applications to change the width of the  
7 main lobe and/or reduce the level of the side lobes. These  
8 types of adjustments are known as beam shaping.

9 One approach to beam shaping is to change the spacing  
10 between the transmitters. However, this approach involves a  
11 mechanical change to achieve a new beam pattern and is  
12 therefore not suitable for adaptive situations. Alternatively,  
13 one can electronically alter the beam pattern by changing the  
14 amplitude (i.e., amplitude shading) or the time delays (e.g.,  
15 phase shading for a narrowband signal) associated with the  
16 transmitted signals.

17 In amplitude shading, the amplitudes of the transmitted  
18 signals are weighted to achieve a certain beam shape. For  
19 example, the amplitude can be tapered to achieve a wider main  
20 lobe and lower side lobe levels using well-known weighting  
21 functions such as the Binomial, Taylor or Dolph-Chebyshev  
22 weighting functions. However, this type of amplitude shading  
23 is generally only effective for a uniformly-spaced linear array  
24 of transmitters, and is therefore not appropriate for use with  
25 non-uniform or arbitrary array of transmitters. Also,  
26 extensions of these approaches to a two-dimensional array are

1 not a direct process. Moreover, the tapering of the amplitudes  
2 usually causes a loss in the transmitted energy as attenuations  
3 are applied to the transmitters.

4 To maintain a high transmit level and to form beams at the  
5 same time, time-delay beamforming or phase shading for a  
6 narrowband signal can be used where the relative delays of the  
7 transmitted signals are used to form beams. This approach,  
8 however, lacks a direct analytic solution that relates the  
9 desired beam pattern to the time delays.

#### 10 11 SUMMARY OF THE INVENTION

12 Accordingly, it is an object of the present invention to  
13 provide a method of shaping a beam pattern of an array of  
14 transmitters.

15 Another object of the present invention is to provide a  
16 method of generating transmitter phase coefficients to  
17 optimally shape the transmit beam pattern.

18 Other objects and advantages of the present invention will  
19 become more obvious hereinafter in the specification and  
20 drawings.

21 In accordance with the present invention, a method is  
22 provided to shape a transmit beam pattern of an array of  
23 transmitters based on an optimal beam pattern intensity. An  
24 initial time delay/phase coefficient is set for each  
25 transmitter such that a set of baseline time delays/phase  
26 coefficients is defined. A plurality of beam pattern

1 intensities is iteratively generated using the set of baseline  
2 time delays/phase coefficients and a plurality of sets of  
3 adjusted time delays/phase coefficients. Each one of the sets  
4 of adjusted time delays/phase coefficients differs from the set  
5 of baseline time delays/phase coefficients by only one time  
6 delay/phase coefficient. Thus, each beam pattern intensity has  
7 a unique set of time delays/phase coefficients associated  
8 therewith. Each beam pattern intensity is compared with an  
9 optimal beam pattern intensity to determine which set of unique  
10 time delays/phase coefficients minimizes a difference between  
11 the optimal beam pattern intensity and the corresponding one of  
12 the plurality of beam pattern intensities. The set of unique  
13 time delays/phase coefficients that minimizes the difference  
14 replaces the set of baseline time delays/phase coefficients to  
15 become the new set of baseline time delays/phase. The above  
16 steps of iterative generation, comparing and replacing are  
17 repeated until the difference can no longer be reduced with the  
18 existing set of baseline coefficients used to control the  
19 transmitters.  
20

#### 21 BRIEF DESCRIPTION OF THE DRAWINGS

22 Other objects, features and advantages of the present  
23 invention will become apparent upon reference to the following  
24 description of the preferred embodiments and to the drawings,  
25 wherein corresponding reference characters indicate

1 corresponding parts throughout the several views of the  
2 drawings and wherein:

3 The sole figure is a schematic of a transmitter system  
4 used to carry out the method of the present invention.  
5

6 DESCRIPTION OF THE PREFERRED EMBODIMENT(S)

7 Referring now to the sole figure, a schematic view of a  
8 transmitter system used to carry out the method of the present  
9 invention is shown and referenced generally by numeral 10.  
10 System 10 includes an array 12 of transmitters 12-1, 12-2, ...,  
11 12-N, the outputs of which are controlled in terms of when  
12 transmission begins. Such control is provided by a  
13 corresponding array 14 of time delays/phase coefficients 14-1,  
14 14-2, ..., 14-N coupled to transmitters 12-1, 12-2, ..., 12-N,  
15 respectively. For purpose of illustration, it will be assumed  
16 that each transmitter in array 12 is a narrow-band sonar  
17 transmitter that generates a simple sine wave. As such,  
18 relative phase changes between each of transmitters 12-1, 12-2,  
19 ..., 12-N, is indicative of a time delay therebetween.  
20 However, it is to be understood that each transmitter in array  
21 12 could also be capable of wide-band transmission in which  
22 case time delays between transmissions is the relevant quantity  
23 to control. Control of time delays/phase coefficients 14-1,  
24 14-2, ..., 14-N is dictated by processor 16 which operates in  
25 accordance with the present invention to shape the beam pattern  
26 generated by array 12.

1           The method of the present invention will be described as  
2 it relates to the setting of phase coefficients 14-1, 14-2,  
3 ..., 14-N for narrow-band transmitters 12-1, 12-2, ..., 12-N,  
4 respectively. The present invention searches for a suitable  
5 set of phase coefficients using a novel search methodology in  
6 order to shape the transmission beam pattern at some far field  
7 100. Far field 100 is representative of a plane or any other  
8 spatial shape that can be divided into discrete points and be  
9 indexed by a set of coordinates. For example, if far field 100  
10 is a two-dimensional plane at which measurements are to be  
11 taken, far field 100 can be indexed by a pair of numbers (x,y)  
12 which could correspond to azimuth and elevation, respectively.  
13 At each coordinate (x,y) of far field 100, the desired beam  
14 intensity is provided so that a desired beam pattern intensity  
15 B(x,y) is given for all of far field 100.

16           Let b(x,y) designate the beam pattern intensity that is  
17 generated at far field 100 by the transmitters 12-1, 12-2, ...,  
18 12-N. The goal of the present invention is to control time  
19 delays/phase coefficients 14-1, 14-2, ..., 14-N so that the  
20 generated intensities b(x,y) equal or closely approximate the  
21 desired intensity B(x,y). To measure how close the generated  
22 beam intensity b(x,y) is to the desired beam intensity B(x,y),  
23 a beam error quantity or BE is defined as

$$24 \quad BE = \sum_x \sum_y |B(x,y) - b(x,y)|^2 \quad (1)$$

1 Thus, beam error BE is a non-negative quantity that approaches  
2 zero as the generated intensities  $b(x,y)$  approach the desired  
3 intensity  $B(x,y)$ .

4 The present invention reduces beam error BE by adjusting  
5 time delays/phase coefficients 14-1, 14-2, ..., 14-N. In terms  
6 of the illustrative example (i.e., narrow-band transmitters 12-  
7 1, 12-2, ..., 12-N), the remainder of the description will  
8 refer only to phase coefficients. While there are many ways to  
9 adjust phase coefficients 14-1, 14-2, ..., 14-N, the present  
10 invention does so in a way that is adaptive and in a way that  
11 minimizes degradation in the beam pattern during such  
12 adjustment of the phase coefficients. More specifically, the  
13 present invention adjusts phase coefficients 14-1, 14-2, ...,  
14 14-N, only one at a time in an iterative fashion. Each  
15 adjustment changes one phase coefficient by a change value  $\rho$ .

16 The process starts by setting all phase coefficients 14-1,  
17 14-2, ..., 14-N to a known value to thereby define an initial  
18 baseline set of phase coefficients. One of the transmitters is  
19 designated as the reference transmitter having a fixed phase  
20 coefficient. Thus, there are N-1 degrees of freedom to adjust  
21 the phase coefficients. The remaining phase coefficients are  
22 considered relative to the reference transmitter. That is,  
23 only the difference in the phase coefficients need be  
24 considered. In general, the initial setting of the baseline  
25 set of phase coefficients can be arbitrary. Since the beam  
26 pattern without shading tends to be used as a reference beam,



1 one can start with an initial set of baseline phase  
2 coefficients in which, for example, all phase coefficients are  
3 set to the same value, e.g., zero. The beam error BE is then  
4 calculated at processor 16 and saved.

5 Adjustments in the baseline set of phase coefficients are  
6 performed iteratively by increasing and then decreasing each  
7 phase coefficient  $14-1$ ,  $14-2$ , ...,  $14-N$  by change value  $\rho$ .  
8 Each resulting intensity  $b(x,y)$  generated by this change is  
9 then used to again calculate beam error BE. Thus, for  $N$   
10 coefficients, there are  $2(N-1)$  actual beam intensities  $b(x,y)$   
11 and  $2(N-1)$  beam errors BE for any given set of baseline phase  
12 coefficients. Once this is done, the set of phase coefficients  
13 producing the smallest beam error BE is selected to be the new  
14 set of baseline phase coefficients. The above process is then  
15 repeated. That is,  $2(N-1)$  adjustments are made to the new set  
16 of baseline phase coefficients in order to generate  $2(N-1)$   
17 actual beam intensities  $b(x,y)$  and  $2(N-1)$  beam errors BE. Once  
18 again, the set of phase coefficients producing the smallest  
19 beam error BE becomes the new set of baseline coefficients on  
20 which the next set of adjustments will be performed. The  
21 process continues until the current set of baseline  
22 coefficients produces the smallest beam error BE or until the  
23 difference in beam error BE does not change significantly.

24 The change value  $\rho$  can be selected or adjusted to suit a  
25 particular application. A large value of  $\rho$  allows the process  
26 of the present invention to move quickly to completion while a

1 smaller value of  $\rho$  allows the actual beam pattern intensities  
2  $b(x,y)$  to more closely approximate the desired beam pattern  
3 intensities  $B(x,y)$ . However, the trade-off for a smaller value  
4 of  $\rho$  is that a greater number of iterations are required to  
5 reach the ultimate solution.

6 The process of the present invention can be carried out  
7 empirically by making iterative measurements at far field 100.  
8 Alternatively, the process can be carried out analytically by  
9 making an assumption that the beam pattern is a summation of  
10 the individual transmitter response adjusted by the appropriate  
11 phase coefficients. For example, one can first take empirical  
12 measurements of the individual transmitter response and store  
13 this information in a database. This information can be used  
14 to determine an approximation to the actual beam intensity  
15  $b(x,y)$  by taking a summation of the individual transmitter  
16 response with an adjustment applied according to the  
17 corresponding phase coefficient. However, this is not as  
18 accurate as taking empirical measurements of the full beam  
19 pattern.

20 The advantages of the present invention are numerous. The  
21 process can be applied to any sonar or other transmitter array  
22 geometry. The adaptive approach can be adjusted to achieve a  
23 quick solution or a finely-tuned solution by merely adjusting  
24 the change value  $\rho$ . The approach can be extended to more  
25 complex transmissions in which case the time delays between  
26 commencement of transmission is adjusted adaptively (as opposed

1 to phase coefficient adjustment in the case of narrow-band  
2 transmissions). The process achieves an optimal set of time  
3 delays/phase coefficients relative to a desired beam pattern.  
4 The beam error near its minimum is smooth and locally convex  
5 (i.e., nearest neighbor time delays/phase coefficients are  
6 checked) which tends to make the ultimate solution robust. In  
7 this way, small time delay/phase perturbations will not lead to  
8 a large degradation in the actual beam pattern.

9 It will be understood that many additional changes in the  
10 details, materials, steps and arrangement of parts, which have  
11 been herein described and illustrated in order to explain the  
12 nature of the invention, may be made by those skilled in the  
13 art within the principle and scope of the invention,  
14

1                    BEAM PATTERN SHAPING FOR TRANSMITTER ARRAY

2  
3                    ABSTRACT OF THE DISCLOSURE

4  
5                    A method to shape a transmit beam pattern of a transmitter  
6 array. A baseline time delay/phase coefficient is set for each  
7 transmitter. A plurality of beam pattern intensities are  
8 iteratively generated using the set of baseline time  
9 delays/phase coefficients and a plurality of sets of adjusted  
10 time delays/phase coefficients. Each beam pattern intensity  
11 has a unique set of time delays/phase coefficients associated  
12 therewith. Each one of the sets of adjusted time delays/phase  
13 coefficients differs from the set of baseline time delays/phase  
14 coefficients by only one time delay/phase coefficient. Each  
15 beam pattern intensity is compared with the optimal beam  
16 pattern intensity to determine which one of the set of unique  
17 time delays/phase coefficients minimizes a difference between  
18 the optimal beam pattern intensity and a corresponding one of  
19 the plurality of beam pattern intensities. The set of baseline  
20 time delays/phase coefficients is then replaced with the one of  
21 the set of unique time delays/phase coefficients that minimizes  
22 the difference. The above steps of iterative generation,  
23 comparing and replacing are repeated until the difference can  
24 no longer be reduced.

