Serial Number

Filing Date

Inventor

<u>7 July 1997</u>

896,527

Neil A. Jackson John T. Williamson Francis J. Frantz Patrick B. Ryll Hyman A. Greenbaum

## <u>NOTICE</u>

The above identified patent application is available for licensing. Requests for information should be addressed to:

OFFICE OF NAVAL RESEARCH DEPARTMENT OF THE NAVY CODE OOCC ARLINGTON VA 22217-5660

Approved for public released Distribution Unbinited

DIIC QUALERY INSPRETAD 4

1	Navy Case No. 77284
2	
3	FUSING CONTACT DATA FOR BEST-ESTIMATE SOLUTION
4	
5	STATEMENT OF GOVERNMENT INTEREST
6	The invention described herein may be manufactured and used
7	by or for the Government of the United States of America for
8	Governmental purposes without the payment of any royalties
9	thereon or therefor.
10	
11	CROSS-REFERENCE TO RELATED PATENT APPLICATIONS
12	This patent application is co-pending with one related
13	patent application entitled "CONTACT DATA CORRELATION WITH
14	REASSESSMENT" (Navy Case No. 77283) by the same inventors as this
15	patent application.
16	
17	BACKGROUND OF THE INVENTION
18	(1) Field of the Invention
19	The present invention relates generally to data fusion, and
20	more particularly to a method of fusing multiple contact data
21	sets for the same contact in order to provide the best-estimate
22	solution identifying the contact's geometric solution, physical
23	attributes, etc.
24	(2) Description of the Prior Art
25	A variety of multiple-contact tracking assessment or
26	correlation schemes are known in the art. For example, in U.S.

•

Patent No. 5,107,271, contact position data is initially 1 processed through a coarse filter. All unrejected data is then 2 passed on to a more stringent nearest-neighbor filter for 3 correlation to a stored contact track. In U.S. Patent No. 4 5,355,325, a measurement tree of nodes allows for the correlation 5 between tracks and objects in a multi-contact tracking system. 6 Three-dimensional volume measurements of the objects are 7 correlated to one or more tracks by projecting a contact 8 measurement into three two-dimensional planes. In U.S. Patent 9 No. 5,392,225, contact data from multiple sensors are correlated 10 to provide a more accurate estimate of contact position. 11 However, without effective fusion of data from multiple types of 12 sensors, a tactical situation "picture" can present conflicting 13 information. 14

15

16

### SUMMARY OF THE INVENTION

Accordingly, it is an object of the present invention to provide a method for fusing contact data from a plurality of sources in order to provide the best-estimate contact solution. Other objects and advantages of the present invention will become more obvious hereinafter in the specification and drawings.

In accordance with the present invention, a method of data fusion is provided to determine a best-estimate solution to a moving contact using a plurality of trackers. Bearing-to-contact data and range-to-contact data is provided from each tracker. An

averaging function is applied to the bearing-to-contact data to 1 determine weighted-average bearing data having a standard 2 deviation associated with each tracker. The same averaging 3 function is also applied to the range-to-contact data to 4 determine weighted-average range data associated with each 5 A computed solution to the moving contact is generated tracker. 6 using the weighted-average range data and the weighted average 7 bearing data from the one tracker having the lowest standard 8 deviation. The computed solution includes heading and speed of 9 the moving contact. A plurality of independently generated 10 solutions to the moving contact are also provided. A root mean 11 square (RMS) error in terms of bearing is then determined for the 12 computed solution and the independently generated solutions using 13 bearing-to-contact data from the one tracker having the lowest 14 standard deviation. One of the computed solution or the 15 independently generated solutions that produces the lowest RMS 16 error is considered to be the best-estimate solution. 17

- 18
- 19

#### BRIEF DESCRIPTION OF THE DRAWINGS

Other objects, features and advantages of the present invention will become apparent upon reference to the following description of the preferred embodiments and to the drawings, wherein corresponding reference characters indicate corresponding parts throughout the several views of the drawings and wherein:

FIG. 1 is a top-level block diagram of the input data processing blocks of an underwater multiple-contact tracking system utilizing the data correlation/reassessment and data fusion modules according to the present invention;

5 FIG. 2 is a functional block diagram of the data correlation 6 module; and

FIG. 3 is a functional block diagram of the data fusion
module.

9

10

#### DESCRIPTION OF THE PREFERRED EMBODIMENT(S)

Referring now to the drawings, and more particularly to FIG. 11 1, a top level block diagram of the input data processing blocks 12 of an underwater multi-contact tracking system is shown and is 13 referenced generally by the numeral 10. However, while the 14 present invention will be described relative to underwater 15 tracking, it is to be understood that the novel features of the 16 invention are applicable to any multi-event scenario where 17 18 multiple systems provide independently measured/generated uncorrelated data concerning the event. 19

Input data processing blocks provide data or contact solutions (e.g., bearing and/or range-to-contact) on various contacts (not shown) being tracked. For example, an active emissions (AE) system 12 senses and interprets various emissions (e.g., noise) from each contact being tracked. One such AE system utilized by the U.S. Navy is the AN/WLY-1 system. If possible, AE system 12 assigns an AE contact number to the

emissions and outputs both the AE data and assigned contact 1 number to a data correlation and reassessment (DCAR) module 14 2 for storage in memory 18. Input data processing also includes a 3 sonar system 16 that collects and interprets various sonar data 4 on the contacts being tracked. Similar to AE system 12, sonar 5 system 16 assigns a contact number to the sonar sensor data and 6 outputs both to DCAR module 14 for storage in memory 18. 7 Examples of sonar systems include the U.S. Navy's AN/BQQ-5, 8

9

AN/BQQ-6, AN/BSY-1 and AN/BSY-2 systems. Additional systems 10 11 could be used to provide even more data (correlated and uncorrelated) on the contacts being tracked. If AE system 12 or 12 sonar system 16 are unable to assign a contact number to the 13 data, DCAR module 14 operates to identify which contact the 14 uncorrelated data is most likely to be associated with as will be 15 explained in detail below. As part of the correlation process, 16 DCAR module 14 performs novel reassessment processing to correct 17 18 for correlation errors and take advantage of contact updates brought about by the various contact-data collection systems. 19 Each contact having data assigned thereto is referred to 20 hereinafter as a reference contact having a contact identity and 21 data associated therewith stored in memory 18. 22

In addition to undergoing correlation and reassessment processing performed by DCAR module 14, each reference contact is also processed periodically (e.g., once per second) by a data fusion module 20 which, as will be described further below,

performs a variety of tasks. In general, the goal of these tasks 1 is to merge or fuse data from the multiple sensor data sets for 2 each reference contact in order to establish a fused reference 3 contact file stored in memory 18 for use by DCAR module 14 and by 4 other tactical situation processing tasks 22. The complex 5 process of data fusion takes into account sensor system 6 capabilities from a signal excess and parameter coverage 7 perspective. Based on sensor capability and signal excess, a 8 parameter tolerance is derived and used in a parameter 9 reconciliation process. A parameter smoothing process is applied 10 to mitigate bad data and large deviations in order to prevent 11 same from causing a ripple error effect through the processing 12 chain. 13

Data correlation at DCAR module 14 is performed each time 14 new (uncorrelated) data is received in order to decide with which 15 reference contact the data is associated with or if a new 16 The correlation process in reference contact should be created. 17 the present invention is, broadly speaking, a three-part process. 18 First, point-to-track correlation examines each new sensor data 19 block ("point") to see whether it is associated with one of the 20 existing reference contacts ("track") stored in memory 18 or 21 22 whether a new reference contact should be created. Next, a first reassessment procedure, referred to herein as track-to-track 23 decorrelation, is performed in which the updated reference 24 contact is examined to see whether the sensor data blocks 25 identified therewith should be separated into different reference 26

contact designations. Finally, a second reassessment procedure,
 referred to herein as track-to-track correlation, is performed to
 determine whether any two of the reference contacts are actually
 the same reference contact.

In FIG. 2, a functional block diagram of DCAR module 14 is 5 Incoming sonar data and AE data is received by a depicted. 6 tracker manager 140 which maintains a history of such data. As 7 mentioned above, if either type of data is already identified by 8 a contact number that exists in the set of reference contacts, 9 then the incoming data is correlated with the corresponding 10 reference contact. However, if the incoming data block is not 11 identified with a contact number (i.e., the data is 12 uncorrelated), tracker manager 140 performs point-to-track 13 correlation in the following manner. Tracker manager 140 first 14 supplies the uncorrelated data to a bearing screen test processor 15 141 to reduce the number of reference contacts against which the 16 incoming (uncorrelated) data must be evaluated for possible 17 association. A test on bearing is used because both AE data and 18 sonar data will include at least bearing-to-contact information. 19 One such bearing screen test that can be used in the present 20 invention will now be described by way of example. Let  $B_1 =$ 21 tracker bearing, 22

23

 $\sigma_1$  = standard deviation of tracker bearing,

 $B_2$  = reference contact bearing (time corrected to the tracker bearing time), and

26

 $\sigma_2$  = standard deviation of reference contact bearing.

1	Further, let
2	$s_1 = B_1 - 3\sigma_1,$
3	$s_u = B_1 + 3\sigma_1,$
4	$T_1 = B_2 - 3\sigma_2, \text{ and}$
5	$T_u = B_2 + 3\sigma_2,$
6	be the 3-sigma lower and upper bounds on $B_1$ and $B_2$ defining the
7	threshold criteria for the bearing screen test.
8	Applying the above in an example where the tracker and
9	reference contact bearing source are colocated (i.e., the sensors
10	are the same or colocated), the bearing screen test is as
11	follows:
12	If $ s_1 - s_u  > 180^\circ$ , then convert $s_1$ , $s_u$ , $T_1$ , $T_u$ to be
13	between -180° and + 180°.
14	And, if $[S_1 \leq T_1 \leq S_u]$ , or
15	$[S_1 \leq T_u \leq S_u]$ , or
16	$[T_1 < S_1 \text{ and } T_u > S_u \text{ and }  T_1 - T_u  < 180°],$
17	then the reference contact passes the bearing screen test.
18	For the situation where the tracker and reference contact
19	bearing source are not colocated, the angle $ heta$ between tracker
20	sensor position and reference contact bearing sensor position
21	must be accounted for where
22	$\theta = \arctan\left(\frac{x_{track} - x_{con}}{y_{track} - y_{con}}\right)$

.

.

and where  $(x_{track}, y_{track})$  is the tracker's position, and  $(x_{con}, y_{con})$  is the time-corrected reference contact bearing source position.

1	Then, let
2	$s_1' = s_1 - \theta$ ,
3	$s_{u'} = s_{u} - \theta$ ,
4	$T_1' = T_1 - \theta$ , and
5	$T_{u'} = T_{u} - \theta$ .
6	The bearing screen test is passed when:
7	1) $S_{1}' \leq 180^{\circ} < S_{u}'$ , and $ S_{1}' - S_{u}'  < 180^{\circ}$ , or
8	2) $T_1" \le 0^\circ \le T_u"$ and $ T_1" - T_u"  < 180^\circ$
9	where $T_1'' = T_1' \mod (-180^\circ \ to \ 180^\circ)$ and
10	$T_u'' = T_u' \mod (-180^\circ \text{ to } 180^\circ), \text{ or }$
11	3) $S_u' < 180^\circ$ and $T_1' < S_u'$ , or
12	4) $S_1' > 180^\circ$ and $T_{11}' > S_1'$ .

Each reference contact having a bearing that is within the (3-sigma) threshold criteria is used in the next step of the point-to-track correlation. Each comparison falling outside the threshold criteria causes the associated reference contact to be dropped from further point-to-track correlation processing.

Reference contacts passing the bearing screen test are 18 evaluated in a more exhaustive manner by a likelihood-of-match 19 processor 142 that applies a total correlation algorithm to each 20 21 such reference contact. Likelihood-of-match processor 142 22 computes a score based upon a comparison of the incoming (uncorrelated) data block and the data identified with each 23 24 reference contact passing the bearing screen test performed by The incoming data is then correlated to the 25 processor 141. reference contact that achieves the highest score. A contact 26

1 m

2

manager 143 updates the reference contact (using the incoming data) and stores the updated reference contact in memory 18.

The total correlation (TCOR) computation used by processor 3 142 utilizes both geometric data (i.e., bearing, bearing rate, 4 range, range rate, and depression/elevation angle) and 5 classification data maintained in an intelligence data base 144. 6 Such TCOR computations are in use by the U.S. Navy in a variety 7 of applications and are therefore well understood in the art. In 8 the present invention, for each type of data existing for both 9 the incoming data block and the reference contact being compared, 10 TCOR computes a score. A positive score favors correlation of 11 the incoming data block with the reference contact to which it is 12 being compared, while a negative score favors non-correlation. 13 For each type of data, there is a maximum allowed score and a 14 threshold for which the maximum score is applied. For example, a 15 maximum score of 10 could be given if the incoming data bearing 16 and reference contact bearing are within a small deviation (e.g., 17 a 1/4 sigma threshold) after adjustment for sensor position and 18 Other deviation thresholds are used to determine non-19 time. 20 correlation or neutral correlation scores. Each type of geometric data has its own thresholds and minimum/maximum scores. 21 The present invention can also include classification data 22 comparisons (according to comparison methods known in the art) 23 that are based on spectral consistency and classification types. 24 These values can be 25

adjusted based on available data in order to optimize performance
 of the TCOR computation.

The TCOR computation is based on a comparison of several 3 parameters (depending on availability for both the incoming data 4 block and the reference contact) and can include bearing, bearing 5 rate, range, range rate, depression/elevation angle, passive 6 narrow band (PNB) tonals, emitted frequency correspondence to 7 radiated frequencies, and classification. For the given incoming 8 data block and reference contact the TCOR computation resembles 9 that used in other Navy applications. Briefly, 10

TCOR = 70 + GCOR + SCOR + ACOR + CCOR(1)

12 where GCOR is the geometric correlation coefficient, SCOR is the 13 signature correlation coefficient, ACOR is the AE correlation 14 coefficient, and CCOR is the classification correlation 15 coefficient. The constant "70" is an arbitrary number selected 16 as a threshold level passing score.

If the incoming data block indicates a new track (i.e., is 17 not currently correlated with a reference contact), it will be 18 correlated with the reference contact which yields the highest 19 TCOR value provided TCOR  $\geq$  70. Otherwise, a new reference 20 21 contact will be created. If the incoming data block is already associated with a reference contact by means of an assigned 22 contact number from either AE system 12 or sonar system 16, it 23 can again be correlated with that reference contact. However, 24 the threshold level passing score is slightly reduced, e.g., to 25

60, to prevent unwanted decorrelation when contact numbers have
 already been assigned.

Determination of GCOR will be explained below by way of 3 example with respect to bearing data. A similar determination 4 can be made using range data. The reference contact bearing is 5 time-corrected using the reference contact bearing rate and 6 acceleration (if it is available). Otherwise, the bearing will 7 be used as is but the bearing standard deviation will be 8 increased (e.g., at a rate of 10°/minute up to a maximum of 10°) 9 to the time of the tracker bearing. More specifically, 10 let B = reference contact bearing (tracker time) 11 = reference contact bearing (previous time) + ( $\Delta T \times B_{RATE}$ ) 12  $\Delta T$  = tracker time - contact recorded time, and where 13  $B_{RATE}$  = reference contact bearing rate. 14 Note that if the reference contact bearing is from a towed array, 15 the tracker bearing is from a hull array, and the reference 16 contact has a range associated with it, then the towed array 17 reference contact bearing must be parallax corrected as is known 18 in the art. 19

20 To perform the bearing comparison, the scoring function 21 given below will be used,

22 
$$L(B) = 18.12 - 7.391 (\ln(\sigma_{bres}) + bres^2/2\sigma_{bres}^2)$$
 (2)

23 where bres = bearing residual
24 = reference contact bearing - tracker bearing, and

$$\sigma_{bres} = \sqrt{\sigma_{btracker}^2 + \sigma_{bref}^2}$$
wherein  

$$\sigma_{Bref} = \text{standard deviation of reference contact bearing, and}$$

$$\sigma_{Btracker} = \text{standard deviation of tracker bearing.}$$
In addition, L(B) is clipped so as not to exceed -10 or +10. This  
is done to prevent an error from having an unrealistic effect on  
the scoring function and to prevent one term (e.g., GCOR, SCOR,  
etc.) from skewing the overall TCOR score. If a bearing  
comparison cannot be performed L(B) = 0.  
The above scoring function in equation (2) is derived from  
the likelihood function (ie., the population density function of

12 the residual)

13 
$$P(bres) = \frac{1}{\sqrt{2\pi}\sigma_{bres}} \exp\left(-bres^2/2\sigma_{bres}^2\right)$$
(3)

14 and the log likelihood function

15 
$$\ln(p) = -\ln(\sqrt{2\pi}) - \ln(\sigma_{bres}) - bres^2/2\sigma_{bres}^2$$
(4)

A linear combination L(B) of ln(p) is then found which satisfies
acceptable boundary conditions, e.g.,

18 for  $\sigma_{bres} = 3^{\circ}$  and  $bres = 0^{\circ}$ , L(B) = 10; and 19 for  $\sigma_{bres} = 3^{\circ}$  and  $bres = 1.645\sigma_{bres}$ , L(B) = 0, thereby yielding 20 equation (2). Similar scoring functions  $L(B_{RATE})$ , L(R),  $L(R_{RATE})$ 21 and L(D/E) are used for bearing rate, range, range rate

and depression/elevation angle, respectively. The value of GCOR
 is then determined from the sum of all the above scoring
 functions.

Determination of SCOR is based on the PNB tonals associated 4 with the reference contact and incoming data block. The PNB 5 tonals originate either from the same sensors/band or from 6 sensors with overlapping bands with the tonals in the overlap 7 being compared to determine SCOR. The scoring function, L(PNB), 8 also has a permissible range, e.g., between -7 and +10. То 9 perform this scoring, the fraction of correctly matched and 10 unmatched tonals is determined. 11

12 Let N = number of matched overlapping tonal bands,

13 M = number of tonal bands left unmatched

14 = (number in tracker - N) + (number in reference - N).
15 Then the scoring function is given by:

16 
$$SCOR = L(PNB) = 10 \times \left(\frac{N - \max(O, M - N_E)}{\max(N + M, DMIN)}\right)$$
(5)

17 where DMIN = minimum allowable denominator which is used to keep 18 scores lower with fewer lines, and  $N_E$  = number of extraneous 19 (unmatched) lines to discount before affecting scoring.

Determination of ACOR is based on a comparison of the PNB tonals of either the incoming data block or reference contact with tonals maintained in intelligence data base 144. ACOR is then given a value of, for example, 0 for no matches, +3 for 1 tonal match, and +6 for 2 or more tonal matches.

CCOR is obtained from a comparison of the reference contact 1 classification with the incoming data block classification. If 2 the reference contact of the incoming data block contains 3 multiple classifications, each classification of the reference 4 contact is compared with each classification from the incoming 5 The comparison which results in the highest value is data block. 6 then utilized to obtain CCOR. If the reference contact 7 classification is from the same sonar tracker as the incoming 8 data block processed, CCOR = 0. If the reference contact 9 classification is from a different sonar tracker than the one 10 being processed, the CCOR value is assigned is accordance with a 11 predetermined correlation score between the values of -10 and 12 +10. 13

Upon update of a reference contact with the data from the 14 incoming data block, contact manager 143 applies a track-to-track 15 decorrelation in order to reassess the newly updated reference 16 This is a form of error checking to verify whether two contact. 17 just-correlated contact "tracks" should remain correlated. 18 (If only one data block or stream is associated with the reference 19 contact, e.g., as is the case with a newly created reference 20 contact, track-to-track decorrelation is not performed.) 21

Track-to-track decorrelation is performed in the following manner. The incoming data used to update a reference contact is compared with each of the other data blocks already associated with that reference contact. Each such comparison begins with a check of the classification of the incoming data used to update

the reference contact and each of the other data blocks already 1 associated with the reference contact. If there is an 2 incompatibility between the classification of the incoming data 3 block used to update the reference contact and that of one of the 4 other data blocks already associated with the reference contact, 5 the two data blocks are decorrelated into two reference contacts 6 by contact manager 143. If the classifications agree, contact 7 manager 143 submits the same two data blocks to bearing screen 8 test processor 141 (which operates as described above). If the 9 bearing screen test is failed, i.e., the threshold tolerance is 10 exceeded, contact manager 143 decorrelates the two data blocks 11 into two reference contacts. Finally, if range and range rate 12 are available in each of the two data blocks, a range screen test 13 is applied by range screen test processor 145. The range screen 14 test algorithm used in the present invention is the same as the 15 above-described bearing screen test except that the range data 16 and their standard deviations are used in place of the bearing 17 data/standard deviations. If the range screen test is failed, 18 contact manager 143 decorrelates the two data blocks into two 19 reference contacts. 20

Following any track-to-track decorrelation processing, contact manager 143 performs track-to-track correlation as another level of error checking. Track-to-track correlation is used to determine if an updated (or newly created) reference contact is actually one of the other existing reference contacts. As a first step, contact manager 143 submits the updated (or

newly created) reference contact and each of the existing 1 reference contacts to bearing screen test processor 141 (which 2 operates as described above). If one or more of the existing 3 reference contacts is within the given bearing threshold, a 4 second track-to-track correlation step is performed. In the 5 second step, likelihood-of-match processor 142 computes total 6 correlation scores (using the above-described TCOR algorithm) 7 between the updated (or newly created) reference contact and 8 those of the existing reference contacts passing the most recent 9 bearing screen test application. Contact manager 143 then uses 10 the updated (or newly created) reference contact to update the 11 existing reference contact that i) passes this most recent 12 bearing screen test application, ii) achieves a TCOR threshold 13 value (e.g., a value of 70 in the illustrated example), and iii) 14 achieves the highest TCOR score. If the TCOR threshold is not 15 met by any of the existing reference contacts passing this most 16 recent bearing screen test application, no further update takes 17 18 place.

19 Referring again to FIG. 1, each reference contact maintained 20 by contact manager 143 in memory 18 is processed periodically by 21 data fusion module 20 which is depicted as a functional block 22 diagram in FIG. 3. The goal of data fusion module 20 is to 23 generate the best quality data possible for each reference 24 contact. The data fusion process consists of several functional 25 blocks to include a bearing fusion block 201, a range fusion

block 202, a compute trajectory block 203, a select solution
 block 204 and a data fusion manager block 205.

Bearing fusion block 201 periodically receives bearing data 3 associated with a reference contact from contact manager 143. 4 The bearing data originates from a plurality of independently 5 operating trackers (e.g., sensor systems such as AE system 12 and 6 sonar system 16). Bearing fusion block 201 applies a linear or 7 quadratic weighted least squares fit to each tracker's bearing 8 data over a given time span (e.g., up to 30 bearings over a two-9 minute time span). While the linear fit function is useful for 10 short range or high (bearing) noise applications, the quadratic 11 fit function is a more general solution. A weighted least 12 squares fit technique was selected over an unweighted technique 13 so that better bearing data would be used and aberration bearing 14 data would be filtered out. Accordingly, the following 15 description will focus on a quadratic weighted least squares fit 16 technique. 17

18 The quadratic weighted least squares fit is performed as 19 follows. Let  $b_i = i$ -th bearing,

 $t_i = time of i-th bearing, and$ 

21  $W_i$  = weight of i-th bearing.

22 Then, the coefficients A, B, C of the quadratic equation

23  $b(t) = At^2 + Bt + C$ 

24 are found which minimize the sum

25 
$$\Sigma w_i (b_i - b(t_i))^2$$

where b(t) represents the fitted bearing at time t. The equation

for b(t) is used to estimate a weighted-average bearing at the 1 current time, as well as the bearing rate and bearing 2 acceleration, and the standard deviations of the bearing and 3 This estimation is performed for each tracker bearing rate. 4 which has been assigned to a reference contact. The tracker 5 providing the lowest standard deviation of the bearing data is 6 considered to be the best tracker. The best tracker is thus 7 selected to provide the bearing parameters for each reference 8 contact used by compute trajectory block 203 in further 9 Since the bearing data sets are evaluated processing. 10 periodically by bearing fusion block 201, the "best tracker" 11 selection is a dynamic process that adapts to changing 12 conditions. 13

Range fusion block 202 receives range data for each 14 reference contact from contact manager 143 and processes the data 15 in parallel with bearing fusion block 201. Range fusion block 16 202 performs a quadratic weighted least squares fit to the range 17 data using an algorithm similar to that used by bearing fusion 18 block 201. For example, up to 30 ranges (over a maximum of two 19 20 minutes) could be processed at a time. However, there is no restriction that the ranges be associated with a single tracker. 21 A weighted-average range, range rate, range acceleration, 22 standard deviation of range, and standard deviation of range rate 23 These computed parameters are then provided to 24 are computed. compute trajectory block 203 for further processing. 25

Compute trajectory block 203 utilizes the range and range rate provided by range fusion block 202 and the bearing and bearing rate provided by the tracker selected at bearing fusion block 201 to generate a solution for the reference contact. The solution computed includes the course (heading) and speed of the reference contact. This solution is then sent to select solution block 204.

10 R = range (known from range fusion);

11 R<sub>RATE</sub> = range rate (known from range fusion);

12 B = bearing (known from bearing fusion);

13 B<sub>RATE</sub> = bearing rate (known from bearing fusion);

14 V<sub>OSx</sub> = ownship east velocity (known from a ship system); and

15 V<sub>OSV</sub> = ownship north velocity (known from a ship system).

16 Then, the computed solution is given by:

18

20

=  $V_{OSx}$  +  $R_{RATE}sin(B)$  +  $RB_{RATE}cos(B)$ ;

19 V<sub>tv</sub> = contact north velocity

= 
$$V_{OSy}$$
 +  $R_{RATE}cos(B)$  -  $RB_{RATE}sin(B)$ ;

21 
$$C_t = contact course = arctan (V_{tx}/V_{ty});$$
 and

22 St = contact speed = 
$$\sqrt{V_{tx}^2 + V_{ty}^2}$$
.

23 Select solution block 204 selects one of several available
24 solutions for the reference contact. Each such available

solution is independently generated or made available from 1 2 several subsystems, e.g., the solution provided by compute trajectory block 203, a solution provided by active emissions 3 system 12, a solution provided by sonar system 16, etc. 4 More specifically, select solution block 204 uses the bearing data 5 from the best tracker (as determined by bearing fusion block 201) 6 to compute the root mean square (RMS) bearing error for each 7 available solution. The solution with the minimum RMS error over 8 a given time period is then selected as the contact solution for 9 that reference contact. The solution is provided to data fusion 10 11 manager 205.

12 Data fusion manager 205 builds the fused contact data files 13 containing the best current estimates of contact parameters. These files include both geometric solution data and attribute 14 data such as classification. Data fusion manager 205 uses 15 geometric data provided by bearing fusion block 201, range fusion 16 17 block 202, and select solution 204. Data fusion manager 205 also 18 receives or assigns confidences to classification data in order to reconcile any conflicts in classification. Thus, data fusion 19 20 manager 205 has access to intelligence database 144 to aid in the 21 reconciliation process. The fused data files for each reference 22 contact are stored in memory 18. The fused data files contain 23 all of the geometric and attribute data that is believed to best 24 represent the current tactical situation for use by DCAR module 14 and tactical situation processing tasks 22. 25

1 The advantages of the present invention are numerous. By 2 combining correlation with reassessment processing, correlation 3 errors can be reduced or minimized. Data fusion can be used to 4 pick the best solution from a variety of independent solution-5 generating sources to provide the clearest tactical "picture" 6 possible.

By way of illustrative example, the present invention has been described relative to a particular application thereof. However, it will be understood that many additional changes in the details, materials, steps and arrangement of parts, which have been herein described and illustrated in order to explain the nature of the invention, may be made by those skilled in the art within the principle and scope of the invention.

14

Navy Case No. 77284

1

2

3

4

5

# FUSING CONTACT DATA FOR BEST-ESTIMATE SOLUTION

## ABSTRACT OF THE DISCLOSURE

A method of data fusion determines a best-estimate solution 6 7 to a moving contact using a plurality of trackers that provide bearing-to-contact data and range-to-contact data. An averaging 8 function is applied to the bearing-to-contact data to determine 9 weighted-average bearing data associated with each tracker. 10 The same averaging function is also applied to the range-to-contact 11 data to determine weighted-average range data. A computed 12 13 solution to the moving contact is generated using the weightedaverage range data and the weighted average bearing data from the 14 15 one tracker having the lowest standard deviation. A root mean square (RMS) error in terms of bearing is then determined for the 16 computed solution and each of a plurality of independently 17 18 generated solutions using bearing-to-contact data from the one 19 tracker having the lowest standard deviation. One of the computed solution or the independently generated solutions that 20 21 produces the lowest RMS error is considered to be the best-22 estimate solution.



FIG. 1

• •



FIG. 2

. •



FIG. 3

. •