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NOTICE

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DTIC QUALITY INSPECTED 4

1	Navy Case No. 77347
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3	MULTI-LAYER TILED ARRAY
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5	STATEMENT OF GOVERNMENT INTEREST
6	The invention described herein may be manufactured and used
7	by or for the Government of the United States of America for
8	governmental purposes without the payment of any royalties
9	thereon or therefor.
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11	BACKGROUND OF THE INVENTION
12	(1) Field of the Invention
13	The present invention relates to planar sonar arrays. More
14	particularly, the invention relates to the arrangement of
15	transducer elements in planar sonar arrays.
16	(2) Description of the Prior Art
17	Conventional planar sonar array designs typically comprise
18	ceramic or polyvinylidene fluoride (PVDF) transducer elements
19	arranged in a single plane according to a required inter-element
20	spacing. The inter-element spacing is based on the half
21	wavelength dimension of acoustic signals at the desired operating
22	frequency. There are several disadvantages associated with this
23	conventional array design. First, the inter-element spacing
24	places an upper bound on the center to center distance between
25	adjacent elements. If this upper bound is violated, beamformed
26	acoustic energy will be allowed to fold back spatially, resulting

in false indications of received energy. This is analogous to
 frequency domain aliasing where the Nyquist criteria has been
 violated, but in the case of a beamformer or spatial filter, the
 independent variable is bearing instead of frequency.

Furthermore, because the inter-element spacing constrains 5 6 the maximum separation distance between elements, there is a corresponding upper bound on element size. That is, as the 7 inter-element spacing is decreased, the area available for the 8 element face decreases as a function of the square of the linear 9 dimension of the element's side. Element signal-to-noise ratio 10 is proportional to the volume of an element and decreases as the 11 elements get smaller. Furthermore, since the PVDF transducer 12 elements used in conventional array construction are essentially 13 flat plate capacitors, the capacitance of any element is directly 14 proportional to the electrode area of the element. As the area 15 available for the element electrode decreases, the capacitance is 16 lowered, thereby increasing electronic noise floor levels. 17 Elevated noise floor levels can mask acoustic signals of 18 interest. Furthermore, the effects of the increased noise floor 19 levels can be exacerbated by the fact that at certain operating 20 frequencies, the deep ocean ambient sound pressure level has a 21 notch making it the quietest region in the usable spectrum. 22 It is at these frequencies that problems resulting from the limited 23 24 capacitance of the elements are most noticeable.

In addition to the sensitivity and detection problems,
elevated noise floor levels complicate the fabrication of

1 conventional arrays. To keep the electronic noise floor level as
2 low as possible, the capacitive loading of the elements must be
3 kept at a minimum. The capacitive loading at the elements is
4 kept at a minimum by keeping the lead lengths of any signal
5 conditioners (preamplifiers) as short as possible. However, this
6 requirement complicates fabrication and provides little space to
7 connect the preamplifiers.

8 Two alternatives have been considered to increase the 9 capacitance in a flat plate capacitor without increasing the area of the electrodes. One approach is to decrease the spacing 10 11 between the two electrodes of the capacitor. The second approach is to increase the dielectric constant of the material between 12 the electrodes. However, neither of these approaches has proven 13 14 feasible for use in elements within a sonar array. The first approach decreased the element sensitivity greatly and 15 alternative dielectric materials considered in the second 16 approach either decreased the element sensitivity or increased 17 18 the thermal noise of the array.

Thus, what is needed is a planar array with an arrangement for the individual elements that increases the capacitance of the elements by increasing their surface area while maintaining the inter-element spacing required to avoid spatial aliasing in the received signals.

SUMMARY OF THE INVENTION

Accordingly, it is a general purpose and object of the present invention to provide a sonar array that maximizes the capacitance of the array elements while maintaining the required inter-element spacing.

6 Another object of the present invention is to increase the 7 distance between the array element preamplifiers and the 8 elements.

9 A further object of the present invention is to reduce the 10 electronic noise floor levels of the array element and 11 preamplifier combinations.

12 These and other objects made apparent hereinafter are accomplished with the present invention by providing a multi-13 14 layer tiled arrangement for the individual elements that 15 increases the capacitance of the elements by increasing their surface area while maintaining a required inter-element spacing. 16 17 The array comprises an outer array and an inner array of 18 transducer elements which convert an acoustic pressure to an 19 electrical response. The transducer elements of the outer array 20 are positioned so as to form a grid of isolation spaces 21 separating each one of the transducer elements. Similarly, the 22 inner array also has transducer elements arranged in a two 23 dimensional matrix with a grid of isolation spaces separating 24 each one of the transducer elements. When an acoustic signal 25 reaches the array, a portion of the signal strikes the transducer 26 elements of the outer array and a portion of the signal

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propagates through the outer array and strikes the transducer elements of the inner array. The electrical response generated by the transducer elements are conditioned by preamplifiers that are coupled to a beamformer. The beamformer combines and postprocesses the conditioned signals from the elements of the outer and inner arrays as signals from a single array of transducers.

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BRIEF DESCRIPTION OF THE DRAWINGS

9 A more complete understanding of the invention and many of 10 the attendant advantages thereto will be readily appreciated as 11 the same becomes better understood by reference to the following 12 detailed description when considered in conjunction with the 13 accompanying drawings wherein like reference numerals and symbols 14 designate identical or corresponding parts throughout the several 15 views and wherein:

16 FIG. 1 is a block diagram of a multi-layer tiled array; 17 FIG. 2 is a diagram showing an arrangement of transducer 18 elements for a section of a multi-layer tiled array; and

19 FIG. 3 shows a cross-sectional view of a multi-layer tiled 20 array.

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DESCRIPTION OF THE PREFERRED EMBODIMENT

Referring to the drawings, there is shown in FIG. 1 a block diagram of a multi-layer tiled array 10 in accordance with the present invention. Array 10 comprises an outer array 12a of transducer elements 14a and an inner array 12b of transducer

elements 14b. Each of the elements 14a and 14b within arrays 12a 1 and 12b, respectively, are electrically independent; thus, each 2 of the elements 14a and 14b are shown separated from their 3 neighboring elements by a space 28. Each of the elements 14a and 4 14b convert acoustic signals incident upon the element to an 5 electrical response such as a change in voltage, a change in 6 current or the like. Transducer elements 14a and 14b can 7 comprise any conventional acoustically transparent material such 8 as polyvinylidene fluoride (PVDF) or the like. The electrical 9 signals generated by transducer elements 14a and 14b are 10 conditioned by preamplifiers 16 and coupled to beamformer 18. 11 Such coupling of preamplifiers 16 to an array 10 is well-known in 12 the art. Using well known techniques, beamformer 18 processes 13 the conditioned signals from preamplifiers 16 to generate an 14 output signal 20. Such techniques can include beamforming, match 15 filter, or the like. 16

Processing only the signals from elements 14a of array 12a, 17 results in a conventional array having an inter-element spacing 18 22 measured from element center to element center. However, 19 processing the signals from elements 14a and 14b as a single 20 array creates a multi-layer array having a reduced inter-element 21 22 spacing 22' measured between an element 14a of array 12a and a 23 neighboring element 14b of array 12b without reducing the size of 24 the elements.

In operation, a sound source 24 which in the present
instance may represent either an active source or an echo from a

source located elsewhere, generates acoustic signals 26 which 1 propagate through the water to array 10. When signal 26 reaches 2 array 10 it strikes the transducer elements 14a of outer array 3 12a and propagates through transducer elements 14a and spaces 28 4 to strike transducer elements 14b of inner array 12b. 5 The electrical response generated by transducer elements 14a and 14b 6 of outer array 12a and inner array 12b, respectively, are 7 conditioned by preamplifiers 16 that are coupled to beamformer 8 The signals generated by elements 14a and 14b of arrays 12a 9 18. and 12b are processed as a single array by beamformer 18 to 10 11 produce output signal 20.

12 Referring now to FIG. 2, there is shown a diagram 13 illustrating an arrangement of transducer elements for a section of a multi-layer tiled array 10. A section of array 10 14 comprising outer array 12a represented by the solid lines and 15 inner array 12b represented by the dashed lines is shown. 16 Outer 17 array 12a and inner array 12b each comprise a plurality of electrically independent transducer elements 14a and 14b, 18 respectively, arranged in a two-dimensional matrix. 19 The elements 14a of outer array 12a are arranged such that each 20 21 element 14a is separated from its neighboring elements within array 12a by a distance of " W_1 "; thereby forming a grid of 22 isolation spaces 28 of width " W_1 " separating each of the elements 23 24 Similarly, elements 14b of inner array 12b are arranged so 14a. as to form a grid of isolation spaces 30 of width "W₂" separating 25 each of the elements 14b. Widths "W1" and "W2" are negligible in 26

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size in comparison to the size of transducer elements 14a and
 14b.

3 Transducer elements 14b of inner array 12b are positioned 4 such that the center of each transducer element 14b is aligned 5 with an isolation space 28 of outer array 12a. Preferably, 6 elements 14b are positioned such that the center of each element 7 14b in array 12b is substantially aligned with the intersection 8 of two of the isolation spaces 28 of outer array 12a thereby 9 maximizing the inter-element spacing 22'.

Preferably, both arrays 12a and 12b are oriented at angle α 10 of approximately 45 degrees relative to the horizontal to 11 maintain the conventional azimuthal and elevation angle 12 13 orientation for the inter-element spacing 22'. Because of the 14 square shape of the individual physical elements 14a and 14b and the 45 degree orientation, Bartlett shading is imposed on the 15 individual elements. The elements may take other shapes such as 16 rectangular, circular, or the like; however, the square shape 17 will maximize the element capacitance. Optionally, conventional 18 shading techniques, such as Hamming or the like, can be employed 19 either electronically or computationally to the entire array in 20 21 addition to any shading technique imposed during fabrication 22 resulting from the shape of the elements.

Referring now to FIG. 3, there is shown a cross-sectional view of array 10 according to one embodiment of the present invention. In the embodiment shown in FIG. 3, transducer elements 14a of outer array 12a comprise a layer of PVDF film 32

1 with a top surface 34 and an opposing bottom surface 36 with a 2 plurality of electrically independent electrodes 38 disposed on each of the surfaces 34, 36. Each electrode 38 can be 3 individually placed on surfaces 34 and 36, or each electrode can 4 5 be formed by depositing a thin layer of conductive material such 6 as copper or the like on surfaces 34, 36 and etching away 7 material to form a grid of isolation spaces 28. Any conventional 8 technique such as spraying or the like can be used to deposit a 9 thin layer of conductive material. Alternatively, array 12a can comprise a single electrode disposed on surface 34 or 36 with a 10 plurality of individual electrodes disposed on the opposing 11 12 surface. However, in a preferred embodiment array 12a comprises 13 individual electrodes 38 disposed on each surface to reduce 14 coupling between adjacent elements. Similarly inner array **12b** 15 can comprise a layer of PVDF film 40 with a top surface 42 and an 16 opposing bottom surface 44 with a plurality of electrically 17 independent electrodes 46 disposed on each of surfaces 42,44.

18 A window 48 of acoustically transparent material such as 19 polyurethane or the like can be disposed to outer surface 50 of outer array 12a. The window 48 allows acoustic signals 26 to 20 21 propagate to elements 14a, 14b and keeps water away from array 22 10. A non-conductive adhesive 52 can be used to join inner array 23 12a to outer array 12b and to help prevent any misalignment of 24 elements 14a, 14b. A substrate 54 can be disposed to the lower 25 surface 56 of inner array 12b to support arrays 12a and 12b. 26 Additionally, substrate 54 can be comprised of materials to

dampen the acoustic signals propagating through the array thereby 1 reducing any reflection of the signals towards array 10. Leads 2 58 receive the electrical signals generated by transducer 3 elements 14a and 14b. The signals are then conditioned by 4 preamplifiers 16. Widths "W1" and "W2" are made large enough to 5 allow for the connection of leads 58 to transducer elements 14a 6 and 14b and small enough to obtain the maximum physical size of 7 transducer elements 14a and 14b. 8

9 In operation, signal 26 propagates through the water until 10 it reaches array 10. The material used to form transducer 11 elements 14a and 14b is acoustically transparent thereby allowing 12 signal 26 to propagate through transducer elements 14a to 13 transducer elements 14b.

The multi-layer tiled array of the present invention 14 provides a novel arrangement for the individual elements that 15 increases the capacitance of the elements by increasing their 16 surface area while maintaining the inter-element spacing required 17 to avoid spatial aliasing in the received signals. The array 18 provides significant advantages over prior art arrays. First. 19 the array increases the maximum allowable distance between array 20 elements. Second, it increases the capacitance of the elements 21 which can be utilized to obtain a lower electrical noise floor 22 level thereby improving the sonar system's performance in 23 detecting low level target signals. Furthermore the arrangement 24 eases the fabrication of the array by allowing the preamplifiers 25 to be located a greater distance from the array. 26

1 What has thus been described is a sonar sensor array that 2 provides a multi-layer tiled arrangement for the individual array 3 elements. The arrangement increases the capacitance of the array 4 elements while maintaining the required inter-element spacing.

5 It will be understood that various changes in the details, 6 materials, steps and arrangement of parts, which have been herein 7 described and illustrated in order to explain the nature of the 8 invention, may be made by those skilled in the art within the 9 principle and scope of the invention.

For example: a different material might be used for the construction of the array to attain better sensitivity or capacitance. Other shading could be implemented readily during fabrication of the inner and outer arrays or additional shading could also be applied after the sensor either electronically or computationally if further improved sidelobe performance of some other shading design is required.

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MULTI-LAYER TILED ARRAY ABSTRACT OF THE DISCLOSURE

A sonar sensor array having a multi-layer tiling arrangement 5 for the individual elements that increases surface area available 6 for each element while maintaining the inter-element spacing 7 required to avoid spatial aliasing when the received signals are 8 combined to form a sonar beam. The array comprises outer and 9 10 inner arrays of transducer elements for converting an acoustic signal to an electrical response. The transducer elements of the 11 outer array are positioned such than a grid of isolation spaces 12 separates each of the transducer elements. The transducer 13 14 elements of the inner array are also positioned such that a grid of isolation spaces separates each one of the transducer 15 elements. The electrical response generated by the transducer 16 elements of the inner and outer arrays are coupled to a 17 beamformer which processes the responses to produce an output 18 19 signal.



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