

Serial No. 721,846
Filing Date 30 September 1996
Inventor John A. Moon
Lynda E. Busse
Jasbinder S. Sanghera
Ishawar D. Aggarwal

NOTICE

The above identified patent application is available for licensing. Requests for information should be addressed to:

UNCLASSIFIED INFORMATION
Approved for public release;
Distribution Unlimited

OFFICE OF NAVAL RESEARCH
DEPARTMENT OF THE NAVY
CODE OCCC3
ARLINGTON VA 22217-5660

19970205 054

DTIC QUALITY INSPECTED 3

Serial No.
Inventors: John A. Moon et al.

PATENT APPLICATION
Navy Case No. 77,161

1 Solids, Vol. 59-60, Part II, pp 925-928, (1983). Photoinduced
2 birefringence and dichroism are discussed at greater length in
3 "Photoinduced Optical Anisotropy in Chalcogenide Vitreous
4 Semiconducting Films", V. G. Zhdanov et al., Physica Status
5 Solidi (a), Vol.52, No. 1, pp 621-626, (March 1979) and in
6 "Anisotropy of Photoinduced Light-Scattering in Glassy As_2S_3 ", V.
7 Lyubin et al., Journal of Non-Crystalline Solids, Vols. 164-166,
8 pp 1165-1168, North-Holland (1993).

9 Although a unified theoretical microscopic description of
10 these effects is not complete, it is believed that photodarkening
11 is produced as carriers break As-S bonds when they recombine,
12 causing an increase in As-As and S-S bonding, which in turn
13 causes a lowering of the band-gap energy by as much as 0.05 eV at
14 room temperature. (See "The Origin of Photo-Induced Optical
15 Anisotropies in Chalcogenide Glasses", H. Fritzsche, Journal of
16 Non-Crystalline Solids, Vols. 164-166, pp. 1169-1172, North-
17 Holland, 1993.) Since only a finite number of As-S bonds have a
18 local environment which allows this process to happen, the effect
19 saturates with total illumination energy. Regardless of the
20 model, however, these effects are experimentally well
21 characterized: the total refractive index change at 600 nm is
22 about 0.01. (See "Photodarkening Profiles and Kinetics in
23 Chalcogenide Glasses", S. Ducharme et al., Physical Review B,
24 Vol. 41, No.17, pp. 12 250 - 12 259, 15 June 1990.) A simple

Serial No.
Inventors: John A. Moon et al.

PATENT APPLICATION
Navy Case No. 77,161

1 Kramers-Kronig analysis predicts that this index change will
2 decrease linearly with photon energy in the transparent region of
3 the glass, thus allowing large amplitudes ($\Delta n \sim 10^{-3}$) to be
4 induced in the infrared.

5 The technique of side writing fiber Bragg gratings in
6 germanium-doped silica fibers is well established and was first
7 described by Meltz, et al. ("Formation of Bragg Gratings in
8 Optical Fibers By A Transverse Holographic Method", Optics
9 Letters, Vol. 14, No. 15, pp 823-825, Aug. 1989.) Two "writing"
10 beams are crossed at some angle θ , with the intersection point
11 coinciding with the core of the silica fiber. The crossed beams
12 form an intensity grating along the axis of the fiber with period
13 $\Lambda = \lambda_w / (2\sin\theta)$, where λ_w is the wavelength and θ is the half-
14 angle between the writing beams, respectively. The writing beams
15 change an absorption line due to the germanium doping of the
16 core, causing a change Δn in the index of refraction n at lower
17 photon energies. The index change amplitude is around $\Delta n \sim 10^{-5}$ -
18 10^{-6} for silica glass. This grating forms a Bragg reflector at
19 the vacuum wavelength λ_B for light launched down the core of the
20 fiber at $\lambda_B = 2n\Lambda$. The "photonic band gap" energy, Δv_B , which
21 corresponds to the full-width of the reflectance between the
22 first two zeros of the reflectivity, is $\Delta v_B/v_B = \Delta n/n$ where v_B
23 $= c/\lambda_B$ and c is the speed of light. See "Propagation Through
24 Nonuniform Grating Structures", J. E. Sipe et al., J. Opt. Soc.

Serial No.
Inventors: John A. Moon et al.

PATENT APPLICATION
Navy Case No. 77,161

1 Am. A., Vol. 11, No. 4, pp.1307-1320 (April 1994).

2 It has been previously demonstrated by Shiramine et al.
3 ("Photoinduced Bragg Reflector In As_2S_3 Glass", Appl. Phys.
4 Lett., Vol. 64 (14), pp 1771-1773, 4 April 1994) that Hill
5 gratings may be written in As_2S_3 glass flakes. Hill gratings
6 are formed from absorption of the peaks of the standing wave
7 produced by multiple reflections from parallel end-surfaces.
8 (See "Photosensitivity In Optical Fiber Waveguides: Application
9 To Reflection Filter Fabrication", K. C. Hill et al., Appl.
10 Phys. Lett., Vol. 32 (10), pp. 647-649, 15 May 1978.) The
11 period of the standing wave sets the Bragg reflection condition,
12 which gives a reflection maximum at the wavelength of the writing
13 beam. Since the energy of the writing beam needs to be near the
14 Tauc gap in order to photoinduce carriers, Hill gratings will not
15 be useful at infrared wavelengths which are not significantly
16 absorbed in the material.

17
18 Summary of the Invention

19 It is therefore an object of the invention to provide
20 variable-bandwidth, high reflectance fiber Bragg gratings for
21 mid-infrared integrated optics applications.

22 Another object of the invention is to write reflective Bragg
23 gratings into infrared transmitting fibers.

24 Another object of the invention is to side write fiber Bragg

Serial No.
Inventors: John A. Moon et al.

PATENT APPLICATION
Navy Case No. 77,161

1 gratings into infrared transmitting fibers.

2 Another object of the invention is to provide fiber Bragg
3 gratings in chalcogenide or chalcohalid-based infrared optical
4 fibers at one or more wavelengths between 1.5 and 15 microns in
5 the infrared.

6 A further object of the invention is to side write highly-
7 reflective, fiber Bragg gratings into sulfide-based chalcogenide
8 infrared optical fibers.

9 A further object of the invention is to provide fiber Bragg
10 gratings in infrared transmitting sulfide-based fibers.

11 These and other objects of this invention are achieved by
12 forming reflective fiber Bragg gratings in the interior of an
13 infrared transmitting glass fiber, such as a chalcogenide or
14 chalcohalid-based infrared optical fiber, by side illuminating
15 the fiber with two same-wavelength, laser writing beams which
16 intersect at some angle in the fiber to form an intensity grating
17 by way of interference along the length of the fiber, maintaining
18 the infrared transmitting glass fiber at the intersection of the
19 two writing beams to produce a reflective Bragg grating in the
20 core and cladding of the glaa fiber, and repeating this operation
21 for each reflective fiber Bragg grating that is desired.

1 gratings into both core only multimode sulfide fiber ($\text{As}_{40}\text{S}_{55}\text{Se}_5$,
2 300- μm diameter) and a core-clad multimode sulfide fiber
3 ($\text{As}_{40}\text{S}_{55}\text{Se}_5$, 200 μm core diameter, $\text{As}_{40}\text{S}_{60}$ 300 μm clad diameter).
4 Thus, it should be understood that the fibers in which gratings
5 can be written in this invention can be core only (a single
6 composition of glass) or core-clad (two concentric compositions
7 of glass, where the core index is higher than the cladding
8 index.)
9

10 Referring now to the drawings, Fig. 1 illustrates a
11 simplified schematic diagram of a reflective fiber Bragg grating
12 side-written into a sulfide-based chalcogenide infrared optical
13 fiber and further indicates a method for side-writing the grating
14 into the sulfide-based chalcogenide infrared optical fiber.

15 As shown in Fig. 1, two exemplary laser beams at the same
16 writing wavelength are used as input "writing" beams 11 and 13.
17 These two writing beams 11 and 13 are crossed at some angle θ , in
18 space.

19 A chalcogenide- or chalcohalid- based glass (Fig. 2)
20 infrared transmitting optical fiber, such as a sulfide-based
21 fiber 15 having a core 17 and a cladding 19, is placed at the
22 intersection point where the two writing beams 11 and 13 cross in
23 space such that where the beams 11 and 13 cross coincides with
24 the fiber 15 itself - the fiber core 17 and cladding 19. The

Serial No.
Inventors: John A. Moon et al.

PATENT APPLICATION
Navy Case No. 77,161

1 crossed beams 11 and 13 form an interference pattern or intensity
2 grating 21 along the axis of the fiber 15 itself with period $\Lambda =$
3 $\lambda_w / (2\sin\theta)$, where λ_w is the writing wavelength and θ is the
4 half-angle between the writing beams 11 and 13. The writing
5 wavelength λ_w is in the range of 0.5 μm to 1.5 μm . This
6 wavelength is chosen to have an absorption length in the
7 particular glass composition of the fiber 15 such that it is
8 weakly absorbed in the glass. Weakly absorbed is defined as an
9 absorption of between 0.1 and 10 cm^{-1} . For example, this would
10 correspond to a wavelength in the range of 0.5 μm - 0.8 μm in the
11 $\text{As}_{40}\text{S}_{60}$ glass composition, and a wavelength range of 0.8 μm -
12 1.4 μm in the $\text{Ge}_{33}\text{As}_{12}\text{Se}_{55}$ composition.

13 When the two crossed beams 11 and 13 are left on the fiber
14 15 for a predetermined length of time, such as an exemplary three
15 or four minutes, the interference pattern 21 in the fiber 15
16 produces an index change in the glass, causing a change Δn in the
17 index of refraction n at lower photon energies. The range of Δn
18 induced by the crossed beams 11 and 13 at λ_w is between 0 and
19 0.2. It should be noted at this time that the typical range of
20 writing fluences at λ_w is between 0.1 and 100 W/cm^2 , and will be
21 incident from 0 -1000 minutes. Any writing fluence/temporal
22 duration of writing sufficient to write a Δn consistent with the
23 above specified 0 to 0.2 range of an Δn induced by the crossed
24 beams 11 and 13 at λ_w is intended to be covered by the claimed

1 invention.

2 The grating produced by the two writing beams 11 and 13
3 forms a Bragg reflector at the vacuum wavelength λ_B for light
4 launched down the core of the fiber at $\lambda_B = 2n\Lambda$. The "photonic
5 band gap" energy, Δv_B , which corresponds to the full-width of the
6 reflectance between the first two zeros of the reflectivity, is
7 $\Delta v_B/v_B = \Delta n/n$ where $v_B = c/\lambda_B$ and c is the speed of light.

8 So the change in the index of refraction will go higher and
9 lower periodically in space along the length of the fiber 15,
10 essentially producing a multi-stack mirror (not shown). The
11 wavelength at which the mirror reflects depends on the period of
12 that grating which can be changed by changing the angle θ_i
13 between the beams 11 and 13. (To be discussed in regard to
14 Fig. 3.)

15 When it is desired to determine the wavelength at which
16 reflecting occurs, an infrared beam can be injected into the core
17 of the fiber 15 and the writing wavelength of the beams 11 and
18 13 can be changed until a wavelength is reflected from the fiber
19 15. That reflected wavelength is called the Bragg wavelength or
20 the Bragg reflection wavelength λ_B . The Bragg reflection
21 wavelength λ_B is in the infrared region from 1.5 μm - 15 μm . The
22 necessary writing angles and wavelengths to achieve a desired
23 Bragg reflection wavelength are shown and discussed in relation
24 to Fig. 3.

Serial No.
Inventors: John A. Moon et al.

PATENT APPLICATION
Navy Case No. 77,161

1 The mechanism for writing a photo-induced index change is
2 based on rearranging the local bonding structure of the intrinsic
3 atoms of the chalcogenide-based or chalcohalid-based glass used
4 in the infrared optical fibers. No dopants are used or required
5 for the photoinduced index change.

6
7 The fiber materials covered by this application are all
8 chalcogenide and chalcohalid glasses where an index change can be
9 photoinduced with a writing wavelength λ_w using the mechanism
10 described in the previous paragraph. Components of exemplary
11 fiber material glass compositions of chalcogenide-based infrared
12 optical fibers are shown in Fig. 2A, while components of
13 exemplary fiber glass compositions of chalcohalid-based infrared
14 optical fibers are shown in Fig. 2B.

15
16 As indicated in Fig. 2A, the chalcogenide glass compositions
17 include any glass composed of at least one of the cations sulfur
18 (S), selenium (Se) and tellurium (Te) and at least one suitable
19 anion, including but not limited to barium (Ba), germanium (Ge),
20 indium (In), arsenic (As), gallium (Ga), or lanthanum (La) in
21 binary, ternary, quaternary, etc. mixtures. Example chalcogenide
22 glass compositions include $As_{40}S_{60}$, $As_{40}S_{55}Se^5$, and $Ge_{33}As_{12}Se_{55}$.

23
24 As indicated in Fig. 2B, the chalcohalide glass compositions

1 include any glass composed of at least one of each of the
2 aforementioned cations and anions, plus at least one of the
3 halides (but less than a total of 50 weight percent) of chlorine
4 (Cl), fluorine (F), bromine (Br) and iodine (I).

5 It is intended that all compositions of the chalcogenide and
6 chalcohalide glasses that form a stable glass and exhibit
7 photoinduced index changes are included in the claimed invention.

8
9 Referring now to Fig. 3, Fig. 3 illustrates the Bragg
10 reflection wavelength λ_B verses the writing angle θ_w for three
11 typical writing wavelengths λ_w . The angle of θ_w on the X-axis of
12 Fig. 3 corresponds to the angle θ_i between the writing beams 11
13 and 13 that are incident upon the fiber 15 in Fig. 1. Fig. 3
14 indicates that upon choosing a given θ_w angle along the X-axis for
15 one of the three typical writing wavelengths shown in Fig. 3, an
16 associated Bragg reflection wavelength will be indicated on the
17 Y-axis. For example, if a writing wavelength of about 532 nm,
18 which corresponds to a frequency doubled Nd:YAG laser, were
19 selected and an θ_w angle of 30° were chosen, Fig. 3 would
20 indicate that a Bragg reflection wavelength of about 2.4 microns
21 would result. So as indicated in the curve of Fig. 3, as the θ_w
22 angle gets smaller as the left-hand side of the curve is
23 approached down to 0° , the Bragg wavelength increases to longer
24 and longer wavelengths λ_B . Thus, if it were desired to write a

1 Bragg grating at, for example, 10 microns, it can be seen that
2 the 10 on the Y-axis would correspond to a θ_w angle of about 10° .
3 So if 10° were put on the angle shown in Fig. 3, Fig. 3 would
4 correspond to Fig. 1.

5 Three different curves are shown in Fig. 3. The three
6 different curves correspond to three different writing
7 wavelengths which would be crossed in Fig. 1. Pairs of beams
8 would be derived from the same laser. The lowest curve 23
9 corresponds to a wavelength of 532 nm from an exemplary frequency
10 doubled Nd:YAG. The center curve 25 corresponds to a 632 nm
11 wavelength from a helium-neon laser. And the upper curve 27
12 corresponds to a $1,064 \mu\text{m}$ wavelength from a Nd:YAG laser. From
13 Fig. 3, it can be readily seen that the angle necessary to write
14 a given reflectivity gets wider with longer wavelengths. A
15 different writing wavelength may be required to write in infrared
16 fibers having different compositions in order to make sure that
17 the radiation from a laser is completely absorbed in the glass of
18 the infrared transmitting fiber.

19
20 Referring now to Fig. 4, a schematic diagram of an
21 experiment which demonstrated the side-writing of a fiber Bragg
22 grating in an arsenic sulfide-based chalcogenide infrared optical
23 fiber is shown. As shown in Fig. 4, a krypton ion laser 31
24 transmits a 40 mW CW beam at a wavelength $\lambda = 6471 \text{ nm}$ (or 0.6471

Serial No.
Inventors: John A. Moon et al.

PATENT APPLICATION
Navy Case No. 77,161

1 μm). The transmitted beam is sequentially reflected by two
2 mirrors 33 and 35 so that the beam can be focused down to a small
3 point by a lens 37.

4 The focused beam from the lens 37 is passed through a
5 spatial filter 39 which basically is just a pinhole (not shown)
6 in a piece of metal to clean up the beam. Any irregularities in
7 the shape of the beam or distortions caused by, for example, dust
8 will not focus to a nice fine point of light that will readily
9 pass through the pinhole in the spatial filter 39 but will be
10 blocked by the spatial filter 39. The only light that comes
11 through the pinhole in the spatial filter 39 is basically a
12 perfect beam which starts to diverge as it exits the pinhole. The
13 diverging beam that is exiting the pinhole in the spatial filter
14 39 is collimated by a lens 41. The lenses 37 and 41 and the
15 spatial filter 39 operate together to make the beam at the output
16 of the lens 41 round and clean-shaped.

17 The collimated beam from the lens 41 is reflected by a
18 mirror 43 to a beamsplitter 45 in the part of the experiment that
19 actually writes the grating. The beam splitter 45 reflects half
20 of the power or 20 mW to another mirror 47 which, in turn,
21 reflects the light to a cylindrical lens 49. The beam splitter 45
22 passes the other half of the power or 20 mW therethrough to the
23 cylindrical lens 49. Thus, essentially two parallel 20 mW light
24 beams are applied to the cylindrical lens 49. The cylindrical

Serial No.
Inventors: John A. Moon et al.

PATENT APPLICATION
Navy Case No. 77,161

1 lens 49 recollimates the two beams and begins to focus each of
2 them in only one direction down to a relatively long and thin
3 line.

4 As the beams are focusing, they are redirected toward each
5 other by flat mirrors 51 and 53 to cross at an angle θ . So the
6 beams look like lines at the point where they cross in space at
7 the focus. It is at that point in space where an arsenic sulfide
8 fiber 55 is placed so that the two beams cross at an angle θ
9 along the core of the arsenic sulfide fiber 55 so that a Bragg
10 grating can be written into into the fiber 55.

11 The arsenic sulfide fiber transmits most of the $0.6471 \mu\text{m}$
12 light which is incident on the side of the fiber 55. This light
13 emerges as from a very strong cylindrical lens in two opposing
14 "arc" shaped patterns. Each beam also has a visible reflection
15 from the surface of the fiber. To get the alignment correct,
16 these directions of the "arc" shaped reflections off the fiber
17 are matched with the complementary input beam to assure that the
18 beams overlap in the fiber core.

19 It was determined that about 3 minutes of illumination with
20 20 mW in each writing beam (for a 3mm long grating) was
21 sufficient to saturate the amplitude of the photoinduced index
22 change. The fact that a large amplitude Bragg grating was written
23 in the fiber was verified by blocking one of the writing beams
24 after the beams were incident for several minutes. As one beam is

Serial No.
Inventors: John A. Moon et al.

PATENT APPLICATION
Navy Case No. 77,161

1 blocked, a large portion of the other beam is diffracted into the
2 blocked-beam's direction which was clearly visible to the naked
3 eye with normal room lighting present.

4
5 Advantages and New Features of the Invention

6 There are two new features of the invention. The first key
7 new feature is that λ_g is now in the IR region of 1.5 - 15 μm .
8 The second new key feature is that the mechanism of making Δn
9 does not depend on any dopant(s) to be present in the glass
10 material. Also, when light is sent down the core of a single-
11 mode sulfide fiber, it will be reflected by this Bragg grating.
12 Unlike silica fiber Bragg gratings, however, the index-change
13 amplitude of these gratings is larger by two orders of magnitude,
14 allowing the possibility of constructing highly reflective, wide
15 band structures.

16 Also, since the writing wavelength is around 650 nm, the
17 writing could be done in principle with commercially available
18 pulsed laser diodes, eliminating the need for an expensive and
19 unwieldy excimer or krypton laser.

20
21 Alternatives

22 The writing process depends only on the total number of
23 photoinduced carriers which subsequently recombine in the
24 illuminated area. This suggests that the fibers may be written

Serial No.
Inventors: John A. Moon et al.

PATENT APPLICATION
Navy Case No. 77,161

1 with short pulses which inject the same total number of carriers.
2 This will allow very fast writing of a single grating, similar to
3 the process already in use with silica fibers. See "Fiber Bragg
4 Reflectors Prepared By A Single Excimer Pulse", C. G. Askins et
5 al., Optics Letters, Vol. 17, No. 11, pp. 833-835, (June 1,
6 1992).

7 In addition, fiber Bragg gratings can be written via the
8 same method and using the same physical process in other fiber
9 compositions. This photodarkening effect occurs in any
10 chalcogenide or chalcohalide based fibers, including fiber
11 compositions containing the chalcogens sulfur, tellurium, and
12 selenium, and mixtures of the aforementioned chalcogens with
13 halides such as fluorine and chlorine.

14 Fiber Bragg gratings can also be written in chalcogenide
15 fibers which are doped with rare-earths such as erbium and
16 praesodymium, which will allow mirror integration in laser and
17 laser amplifier devices based on these materials.

18
19 Therefore, what has been described in a preferred embodiment
20 of the invention is a method, and the resultant device, for
21 forming at least one reflective fiber Bragg grating in the
22 interior of an infrared transmitting glass fiber, such as a
23 chalcogenide or chalcohalid-based infrared optical fiber, by side
24 illuminating the fiber with two same-wavelength, laser writing

Serial No.
Inventors: John A. Moon et al.

PATENT APPLICATION
Navy Case No. 77,161

1 beams which intersect at some angle in the fiber to form an
2 intensity grating by way of interference along the length of the
3 fiber, maintaining the infrared transmitting glass fiber at the
4 intersection of the two writing beams to produce a reflective
5 Bragg grating in the core and cladding of the glass fiber, and
6 repeating this operation for each reflective fiber Bragg grating
7 that is desired.

8 It should therefore readily be understood that many
9 modifications and variations of the present invention are
10 possible within the purview of the invention. It is
11 therefore to be understood that

12 the invention may be practiced otherwise than as
13 specifically described.

Serial No.
Inventors: John A. Moon et al.

PATENT APPLICATION
Navy Case No. 77,161

ABSTRACT

1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20

A reflective Bragg grating in the interior of an infrared transmitting glass fiber, and a method for fabricating such reflective Bragg grating in the interior of the infrared transmitting glass fiber is disclosed. The method comprises the steps of: producing first and second writing beams at the same wavelength; orienting the first and second writing beams in parallel with respect to each other; crossing the first and second writing beams at a preselected angle with respect to each other to form an interference pattern at the intersection of the first and second writing beams; positioning the infrared transmitting glass fiber at the intersection of the first and second writing beams so that the interference pattern occurs along a portion of the length of the infrared transmitting glass fiber; and maintaining the infrared transmitting glass fiber at the intersection of the first and second writing beams for a time sufficient to produce a Bragg grating in the core and cladding of the infrared transmitting glass fiber.

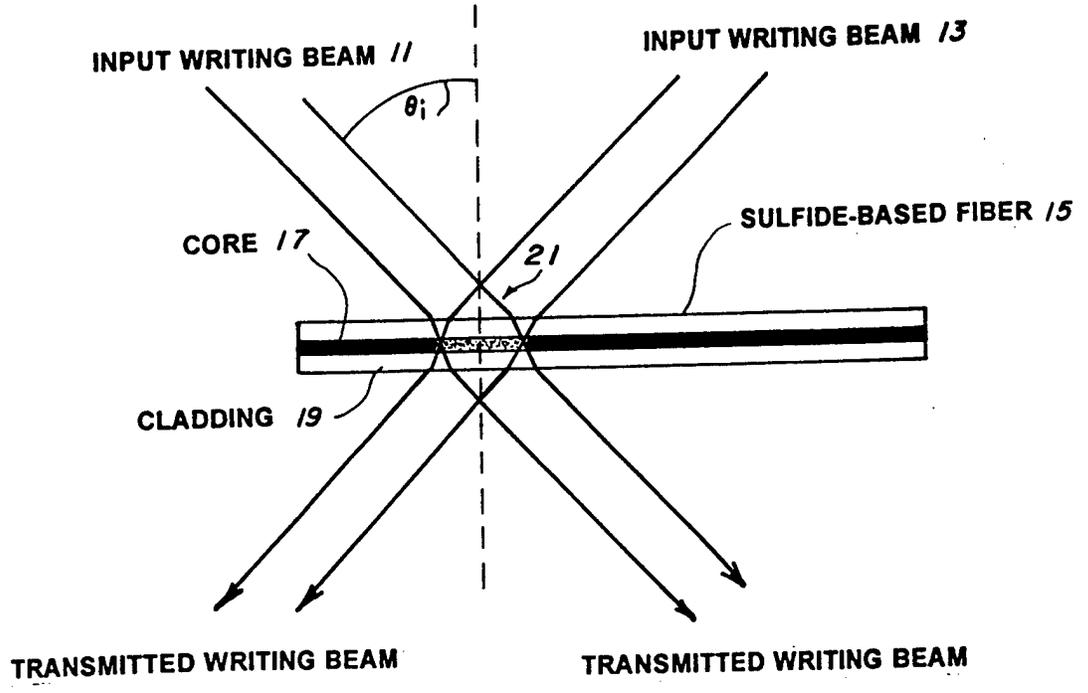


FIG. 1

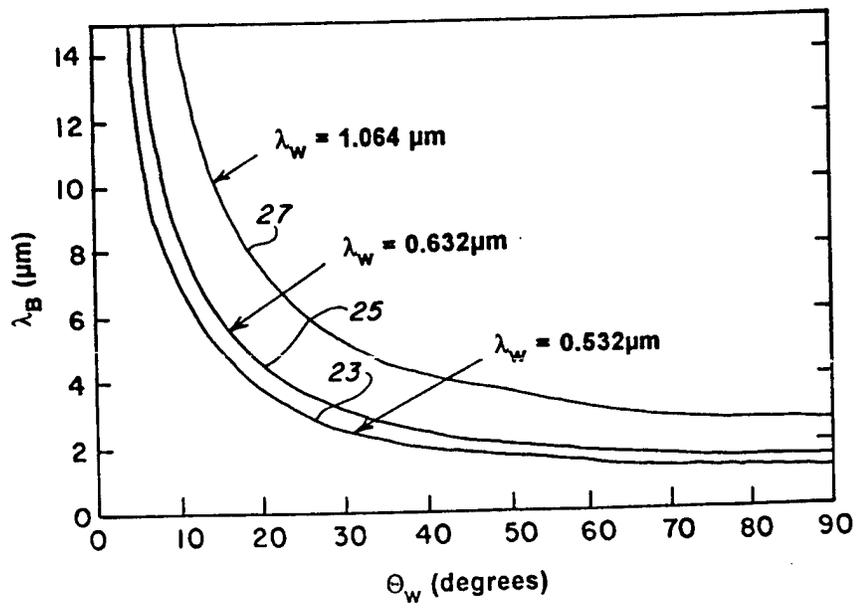


FIG. 3

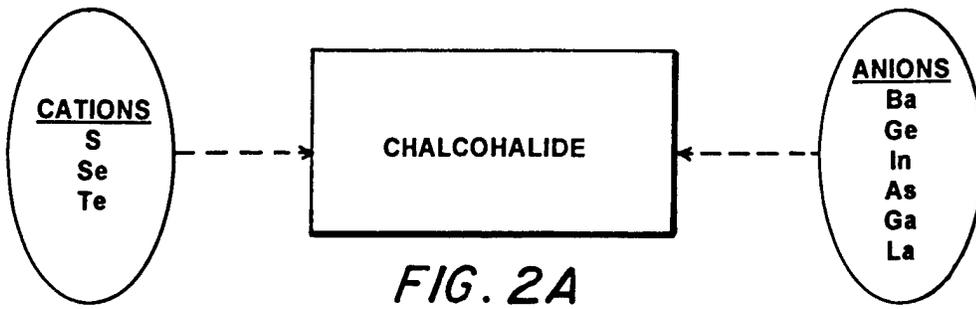


FIG. 2A

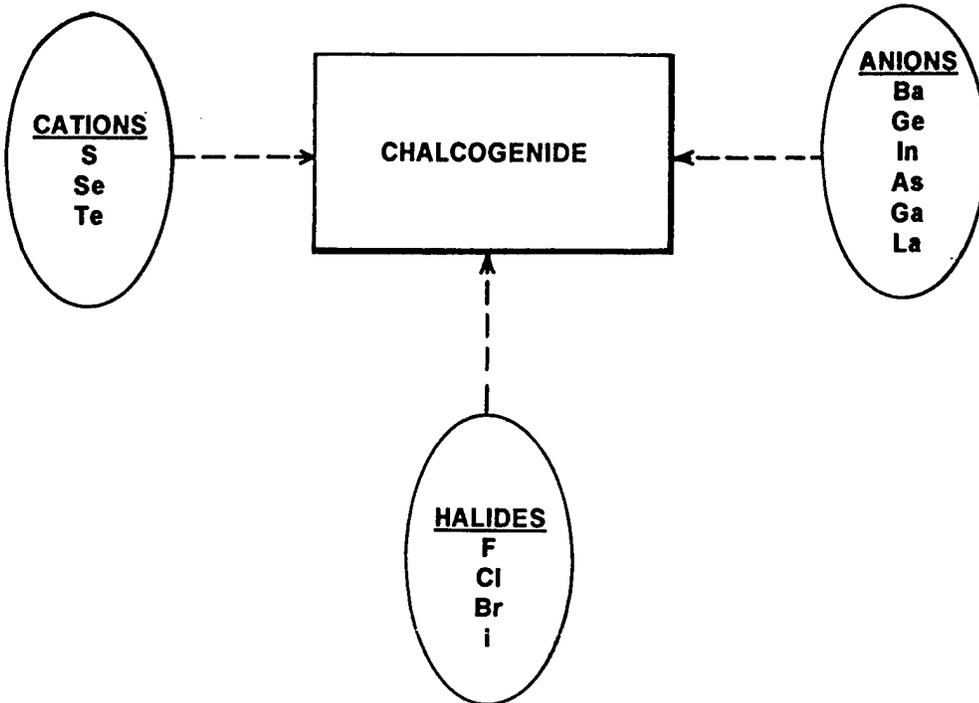


FIG. 2B

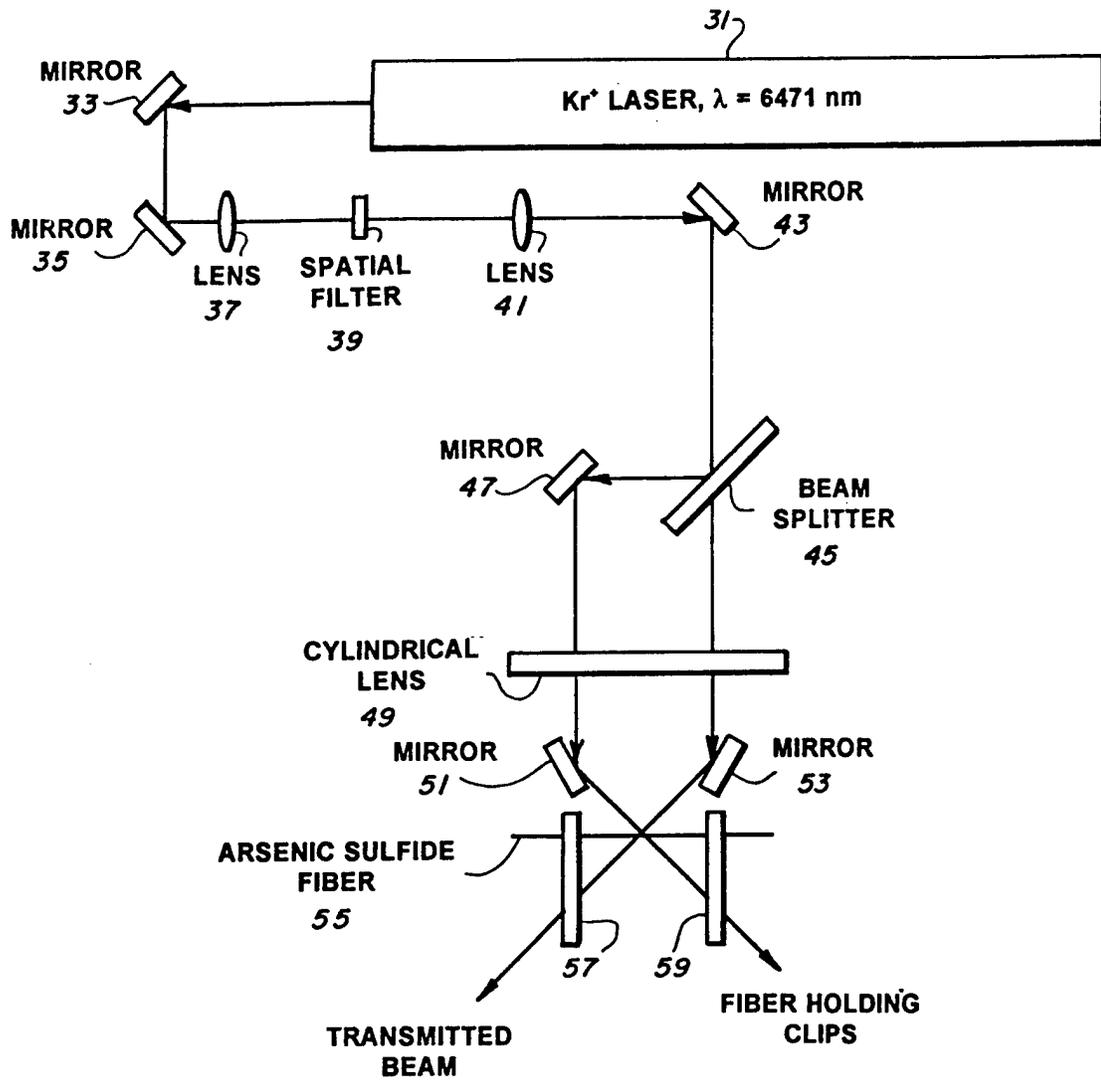


FIG. 4