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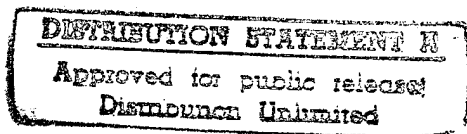
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DTIC QUALITY INSPECTED 1

1 Navy Case No. 76312

2
3 ULTRA-BROADBAND HYDROPHONE

4
5 STATEMENT OF GOVERNMENT INTEREST

6 The invention described herein may be manufactured and used
7 by or for the Government of the United States of America for
8 governmental purposes without the payment of any royalties
9 thereon or therefor.

10
11 BACKGROUND OF THE INVENTION

12 (1) Field of the Invention

13 The present invention relates to an extremely broadband
14 acoustic hydrophone device.

15 (2) Description of Prior Art

16 Classical acoustic hydrophones for ship sonar use
17 relatively large mass piezoelectric materials for the conversion
18 to electrical energy. This piezoelectric mass has mechanical
19 resonances and acoustic impedances that alter its responses to
20 acoustic waves. The classic hydrophones operate in bandwidths
21 less than two decades of frequencies. The ultra-broadband
22 hydrophone does not suffer from either of these anomalies or a
23 thermal noise limit except for its electronic circuits.

1 SUMMARY OF THE INVENTION

2 Accordingly, it is a principal object of the present
3 invention to provide a hydrophone which operates over a broad
4 band of frequencies.

5 It is a further object of the present invention to provide a
6 hydrophone as above which lends itself to a wide variety of
7 configurations.

8 It is still a further object of the present invention to
9 provide a hydrophone as above which has increased sensitivity.

10 The foregoing objects are attained by the ultra-broadband
11 hydrophone of the present invention which has a first means for
12 sensing an acoustic wave having changes (increases and decreases)
13 in pressure relative to the ambient pressure. The acoustic wave
14 pressure sensing means comprises magnetic means for causing a
15 magnetic field to move synchronously. Preferably, the magnetic
16 means is a flexible diaphragm having magnetic particles, which
17 particles when contacted by the pressure of an acoustic wave
18 cause changes in the ambient magnetic field. The hydrophone
19 further has second means for sensing flux changes in the ambient
20 magnetic field and for generating an electrical signal
21 representative of the ambient magnetic field. Preferably, the
22 flux change sensing means comprises a flux-gate magnetometer.

23 The hydrophone of the present invention further has means
24 for generating an output signal. The output signal generating
25 means includes means for demodulating the electrical signal

1 representative of the ambient magnetic field and a low pass
2 filter for smoothing out the demodulated electrical signal.

3 In a preferred embodiment of the present invention, the
4 hydrophone further comprises means for generating a differential
5 magnetic field for nulling the magnetic field at the flux change
6 sensing means. It has been found that providing a differential
7 magnetic field causes an increase in the sensitivity of the
8 hydrophone by operating the flux change sensing means in its most
9 linear point.

10 Other details of the present invention, as well as other
11 objects and advantages attendant thereto, are set forth in the
12 following detailed description and the accompanying drawings
13 wherein like reference numerals depict like elements.

14 BRIEF DESCRIPTION OF THE DRAWINGS

15
16 FIG. 1 is a schematic representation of a first embodiment
17 of a hydrophone in accordance with the present invention;

18 FIG. 2 illustrates a flux-gate magnetometer used in the
19 hydrophone of the present invention;

20 FIG. 3 illustrates the manner in which acoustic wave
21 pressure is transformed into an electrical signal; and

22 FIG. 4 is a schematic representation of a second embodiment
23 of a hydrophone in accordance with the present invention.

1 DESCRIPTION OF THE PREFERRED EMBODIMENT

2 Referring now to FIG. 1, an ultra-broadband hydrophone 8 in
3 accordance with the present invention has two major electronic
4 components and one mechanical component. The first electronic
5 component comprises a flux-gate magnetometer 14, while the second
6 electronic component comprises a circuit having a synchronous
7 demodulator 24 and a low pass filter 26. The mechanical
8 component comprises a magnetic diaphragm 12.

9 The operation of the ultra-broadband hydrophone of the
10 present invention can be seen from FIGS. 1 through 3. Sound wave
11 pressures 10, when changing about the ambient pressure, produce
12 vibrations in the magnetized diaphragm 12 which causes the
13 diaphragm to flex. This in turn causes the ambient magnetic
14 field about the diaphragm to move synchronously to the altered
15 position 12a shown in dotted lines in FIG. 3. Slight increases
16 and decreases in the flux H of the ambient magnetic field produce
17 a change in an AC signal 16 generated by the flux-gate
18 magnetometer 14. Thereafter, the AC signal 16 is demodulated
19 synchronously by demodulator 24 and filtered by filter 26 to
20 convert the fluctuating input acoustic wave pressure to an
21 electric output signal 38.

22 The flux-gate magnetometer 14 used in the hydrophone of the
23 present invention may be similar to that shown in the article
24 "The Flux-Gate Magnetometer: A Very Sensitive ELF Magnetic
25 Detector" by Peter Vizmuller, RF Design, Vol. 17, No. 1, January
26 1994, pp. 27-29 and 32. Such a magnetometer has a sensitivity

1 vying a superconducting SQUID and can be made into an extremely
2 small package. Additionally, it is a sensing device that is many
3 magnitudes more economical than a superconducting SQUID. The
4 magnetometer 14 is also a sensor that has the sensitivity to
5 measure changes in the earth's magnetic flux.

6 As shown in FIG. 2, the flux-gate magnetometer 14 used in
7 the hydrophone of the present invention is a device composed of
8 two orthogonal magnetic windings 20 and 22 wound on two ferrite
9 cores 18 and 19. The output signal 16 of the magnetometer is an
10 AC signal that has an amplitude and phase relative to the
11 strength and direction of the ambient magnetic field. The output
12 signal 16 is obtained through repetitive saturations of the
13 ferrite cores 18 and 19 driven by a high frequency bias current
14 40 passed through the winding 22. The current 40 may be produced
15 by any suitable current source (not shown) known in the art.
16 Changes in these saturations are sensed by the sensing winding 20
17 which is orthogonal to winding 22 to null any magnetic field
18 created by the bias current. The sensing winding 20 produces no
19 output signal when there is no external magnetic field. In an
20 applied magnetic field 36 that is perpendicular to the sensing
21 winding 20 and orthogonal to winding 22, the vector of the
22 magnetic flux H passes through the two ferrite cores 18 and 19
23 and the sensing winding 20. When the ferrite cores 18 and 19 are
24 saturated by the bias current 40, the flux of the magnetic field
25 36 is blocked from passing through the ferrite cores 18 and 19
26 and the sensing winding 20. Thus the sensing winding 20 induces

1 the presenting and absenting of the applied magnetic field 36 to
2 produce the AC output signal 16, which signal has an amplitude
3 and phase relative to the magnetic field's strength and
4 direction. The applied magnetic field 36 is sampled twice per
5 cycle of the high frequency bias current to produce an output
6 frequency that is twice the frequency of the bias current.

7 As previously discussed, the second electric component
8 comprises a synchronous demodulator 24 and a low pass filter 26.
9 Preferably, the filter 26 has a cutoff frequency below the bias
10 frequency. If one assumes that there is a continuous positive
11 pressure 10 on the magnetic diaphragm 12, as shown in FIG. 3,
12 that produces a steady AC output signal 16 from the flux-gate
13 magnetometer 14, the demodulation of the AC output signal 16 is
14 synchronous to its own output frequency. The low pass filter 26
15 smoothes the demodulated signal to a plus or minus DC signal as a
16 function of the magnitude and direction of the ambient magnetic
17 field. Therefore, a steady pressure produces a steady DC output
18 signal 38 and a fluctuating pressure will cause a fluctuating
19 output electrical signal 38. It can be seen from the foregoing
20 that an acoustic input will be reproduced in frequency and
21 magnitude in the filtered output.

22 The magnetized diaphragm 12 is a passive mechanical
23 component that is a highly flexible light diaphragm impregnated
24 with fine grain magnetic particles. The diaphragm may be formed
25 from any suitable rubber-like flexible material known in the art.
26 Similarly, the magnetic particles may be any magnetic particles

1 known in the art such as iron, nickel, rare earth and cobalt
2 particles. Preferably, the magnetic particles are aligned
3 magnetically in the same direction as the response axis of the
4 flux-gate magnetometer 14. The diaphragm 12 and the magnetometer
5 may be encased in any suitable structure 11 as shown in FIG. 1.

6 The hydrophone of the present invention can sense acoustic
7 energy from a lower frequency of zero Hertz to an upper frequency
8 limit where the hydrophone's magnetic diaphragm 12 is no longer
9 capable of being moved by the acoustic energy. It has been found
10 that the physical and electrical laws of this device allow a
11 transducer operating frequency range from DC to above 100 Khz.

12 A preferred embodiment of the ultra-broadband hydrophone of
13 the present invention is shown in FIG. 4. This embodiment
14 includes a sub-Hertz differential magnetic field winding 28, a
15 sub-Hertz low pass filter 32 and a differential field driver 30.
16 The differential magnetic field 28a produced by the winding 28 is
17 used to null the flux H of the magnetic field 12a at the flux-
18 gate magnetometer 14. This action increases the sensitivity of
19 the hydrophone 8 by operating the flux-gate magnetometer 14 in
20 its most linear point. This action also compensates for the
21 earth's magnetic field and for local steady or slow changing
22 stray magnetic fields. In operation, the sub-Hertz low pass
23 filter 32 senses the average voltage of the hydrophone's
24 electrical output signal 38 and inputs the average voltage to the
25 differential field driver 30. Through a negative feedback mode,
26 the differential field driver 30 controls the direction and level

1 of the differential magnetic field 28a to null the average
2 magnetic field 12a at the flux-gate magnetometer 14.

3 The ultra-broadband hydrophone of the present invention may
4 be constructed in a variety of different configurations. For
5 example, it can be constructed as a cylindrical hydrophone, a
6 thin plate array of hydrophones, a conformal array of
7 hydrophones, a thin array of hydrophones, and a very small
8 hydrophone. If desired, the ultra-broadband hydrophone can be
9 constructed with a rigid fixed magnet behind the flux-gate
10 magnetometer to null the magnetic field at the flux-gate
11 magnetometer. The removal of the magnetic bias at the flux-gate
12 magnetometer from the diaphragm's field will increase the
13 hydrophone's sensitivity by moving the flux-gate magnetometer's
14 operation toward the most linear part of the saturation curve.

15 The effect of motion and the earth's magnetic field can be
16 decoupled from the output of the ultra-broadband hydrophone
17 causing a very slight frequency increase at the zero Hertz
18 response point.

19 The ultra-broadband hydrophone of the present invention can
20 be used in air as a microphone.

21 There are numerous advantages attendant to the hydrophone of
22 the present invention. For example, it has an increased
23 operating bandwidth. It also has an increased operating
24 sensitivity. Still further, it can be scaled in size. Yet
25 another advantage is that it has no thermal noise limit except
26 for the electronics that can be optimized for a minimum effect.

1 It is apparent that there has been provided in accordance
2 with this invention an ultra-broadband hydrophone which fully
3 satisfies the objects, means and advantages set forth
4 hereinbefore. While the invention has been described in
5 combination with specific embodiments thereof, it is evident that
6 many alternatives, modifications, and variations will be apparent
7 to those skilled in the art in light of the foregoing
8 description. Accordingly, it is intended to embrace all such
9 alternatives, modifications, and variations,

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1 Navy Case No. 76312

2
3 ULTRA-BROADBAND HYDROPHONE

4
5 ABSTRACT OF THE DISCLOSURE

6 The present invention relates to an ultra-broadband
7 hydrophone which has two major electronic components and one
8 mechanical component. The first electronic component comprises a
9 flux-gate magnetometer for sensing changes in an ambient magnetic
10 field and for creating an electrical signal representative of the
11 ambient magnetic field. The second electronic component
12 comprises an electrical circuit for demodulating the electrical
13 signal and a low pass filter for smoothing the demodulated
14 signal. The mechanical component is a magnetic diaphragm for
15 receiving acoustic pressure waves and for causing changes in the
16 ambient magnetic field in response to the received acoustic
17 pressure waves. In a preferred embodiment, the hydrophone of the
18 present invention also includes a sub-Hertz differential magnetic
19 field winding for generating a differential magnetic field which
20 nulls the ambient magnetic field about the flux-gate
21 magnetometer.

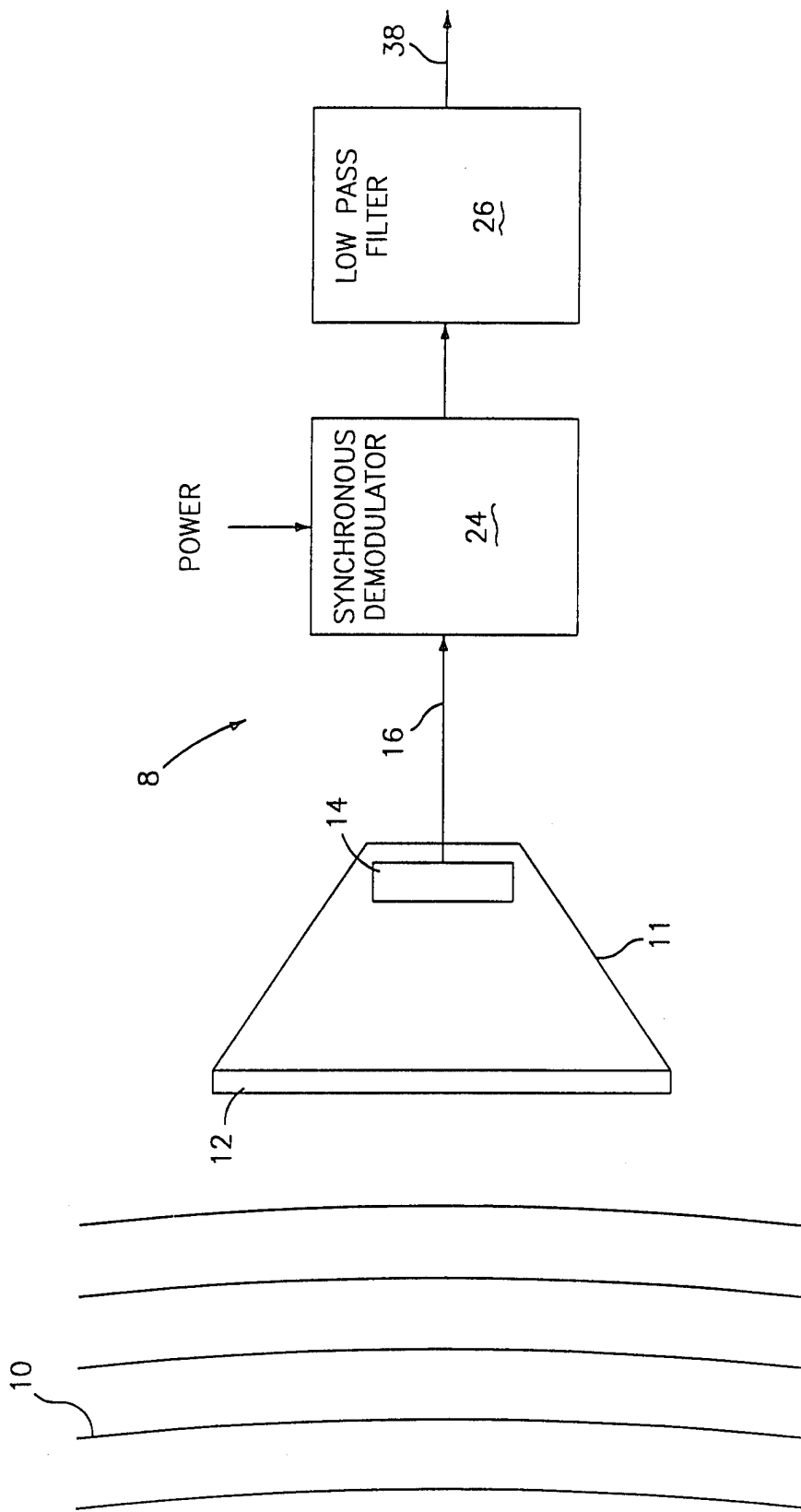
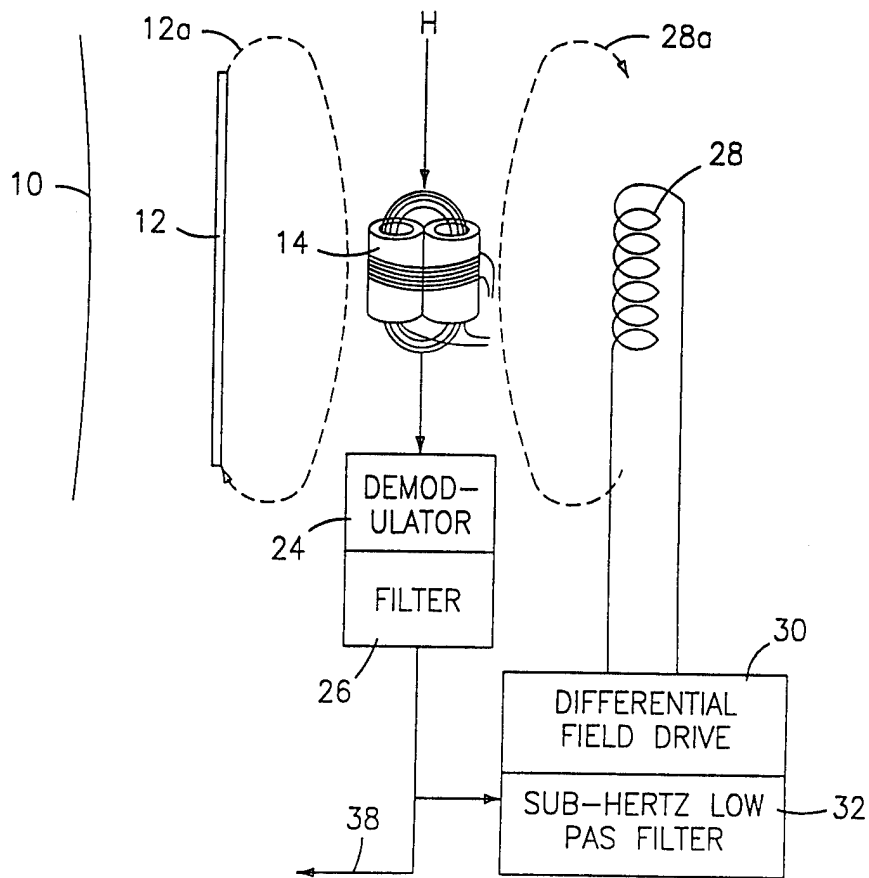
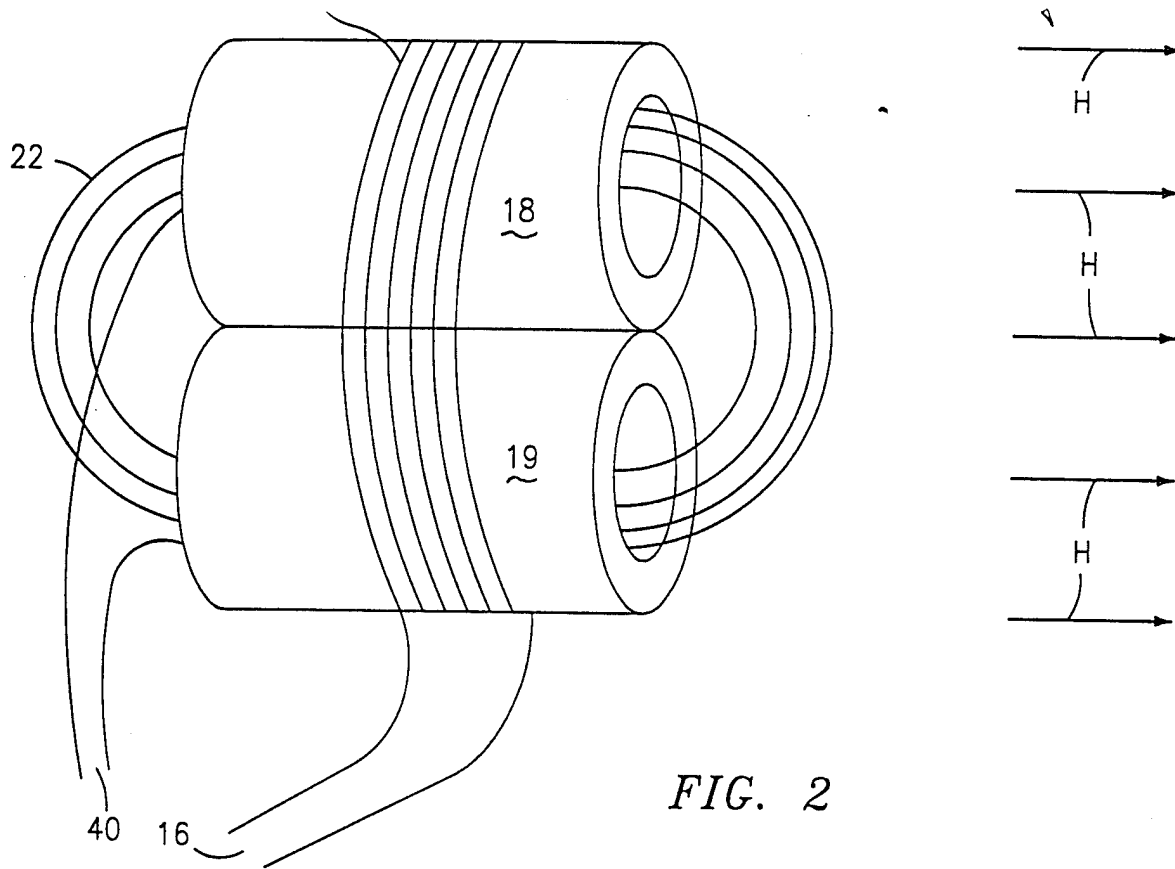


FIG. 1



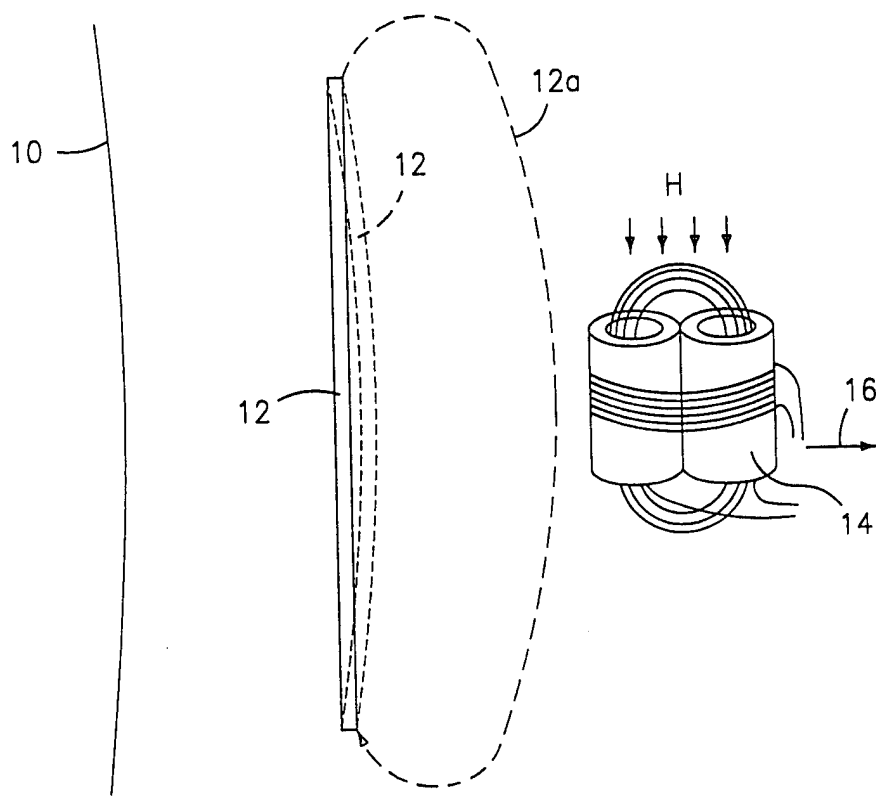


FIG. 3