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AFWAL-TR-83-4033 VOLUME II

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# ICAM MANUFACTURING COST/DESIGN GUIDE

FINAL TECHNICAL REPORT AIRFRAMES USER'S MANUAL—VOLUME 2



# PERIOD OF PERFORMANCE 1 OCTOBER 1979-31 OCTOBER 1982 JANUARY 1983

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Computer Aided Manufacturing Fuselage Panels Extrusions
Manufacturing Cost Sheet Metal Parts Castings
Cost Drivers Assemblies Forgings
Design-to-Cost Mechanical Fastening Test, Inspection
Airframe Design Advanced Composites & Evaluation

# 20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

The "Manufacturing Cost/Design Guide" (MC/DG) enables airframe and electronic designers to achieve lowest cost by conducting trade-offs between manufacturing cost and other design factors. When fully developed, the MC/DG will, for example, permit airframe designers, at all levels of the design process, to quickly perform cost-trade comparisons of manufacturing processes and structural performance/cost trade-offs on airframe components and subassemblies in metallic and composite materials.

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#### 20, (Continued)

The first program, reported in AFML-TR-76-227, developed a model of the MC/DG, the contents, cost drivers, data requirements and designer-oriented formats for conventional and some emerging manufacturing technologies, and also an implementation plan.

The second program (Contract No. F33615-77-C-5027) consisted of four phases in which manufacturing man-hour data and designer-oriented formats were developed for "Sheet-Metal Aerospace Discrete Parts", "First-Level Mechanically Fastened Assemblies", and "Advanced Composite Fabrication". Further, structural performance/manufacturing cost trade-studies were conducted by designers in industry to demonstrate utilization of the manufacturing man-hour data developed in this program.

The data developed by the five participating aerospace companies were normalized by Battelle's Columbus Laboratories and the data plotted in designer-oriented formats. Data have been developed for base parts and discrete parts. The base part is a structural element in its simplest form and when modified with designer-influenced cost elements (DICE) such as joggles, cutouts, and heat treatment, a discrete part ready for assembly is obtained. Typical DICE analyzed for mechanically fastened assemblies are accessibility, material types, part and fastener counts, and sealing requirements. For composites, typical DICE are orientation and number of plies, overlaps, fiber mix, cutouts, and quality requirements.

The data are presented in the series of formats showing cost-driver effects (CDE) and cost-estimating data (CED) and have been evaluated in trade-offs on various fuselage panels designed in titanium, aluminum, and graphite/epoxy.

The third program (Contract No. F33615-79-C-5102) required the development of MC/DG sections on castings, forgings, extrusions, and test, inspection and evaluation (TI&E). Furthermore, as castings, forgings, and extrusions are normally machined prior to assembly in aerospace structures, data and formats were developed for the machining of typical discrete parts manufactured utilizing these methods. TI&E was included in the MC/DG as, in the case of certain materials such as graphite/epoxy and manufacturing methods such as castings, this can be a cost-driver that needs to be included in trade-off studies comparing various manufacturing methods.

The third program also required the development of an MC/DG for electronics fabrication, assembly, and TI&E. A series of typical discrete parts such as transistors, capacitors, diodes, and hybrids were analyzed and also, typical assemblies such as printed wiring boards. Hand, semiautomatic and automatic soldering and insertion processes were also analyzed. Furthermore, the manufacturing cost to meet typical reliability requirements in electronics is also presented to the designer for the selected discrete parts.

## 20. (Continued)

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This project is reported in a six-volume Final Technical Report as follows:

# VOLUME I. User's Manual - Airframes Volume 1 Contains:

- Utilization Procedures
- Trade-Off Study Examples
- MC/DG Sections for:

- Sheet Metal
- Mechanically Fastened Assembly
- Composites

# VOLUME II. User's Manual - Airframes Volume 2 Contains:

- MC/DG Sections for:
  - Extrusions
  - Castings
  - Forgings

# VOLUME III. User's Manual - Airframes Volume 3

#### Contains:

- MC/DG Test, Inspection & Evaluation Section for:
  - Sheet Metal
  - Mechanically Fastened Assemblies
  - Castings
  - Forgings
  - Machining
  - Composites

# VOLUME IV. User's Manual - Electronics Volume 1 Contains:

- Design Process Descriptions
- Conceptual Design Section for:
  - New Technology Part Count
  - Number of Assemblies Part Selection
  - Common Functions -- Reliability
  - Digital Design
    - ign -- Package
  - Built-in Test
  - Detail Design Section for:
    - Mechanization
- Insertion Process\_

- Processes

- Soldering Process: For

# VOLUME V. Project Summary

VOLUME VI. Technology Transfer Summary and Report Contents

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#### **FOREWORD**

This Manufacturing Cost/Design Guide document covers the work performed under Air Force Centract F33615-79-C-5102 from 1 October 1979 through 1 October 1982. The contract is sponsored by the Computer Integrated Manufacturing Branch, Manufacturing Technology Division, Materials Laboratory, Air Force Wright Aeronautical Laboratories. The ICAM Project Manager is Capt. Richard R. Preston. In previous phases, the following Air Force personnel directed the program; Mr. John R. Williamson, Capt. Dan L. Shunk, and Capt. Steven R. LeClair.

The organization of the program is comprised of a coalition of seven participating companies with Battelle's Columbus Laboratories (BCL) as the prime contractor. Mr. Bryan R. Noton is the BCL Program Manager. The other participating companies of the coalition are listed below:

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Approved by:

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BRYAM R. NOTON, MC/DG Program Manager

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# 4.4 Extrusion Section

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This section contains format selection aids, identification of the types of parts analyzed for data to determine the manufacturing man-hour data, examples of how the data are utilized in airframe design and a set of formats. These formats include cost-driver effects (CDE), cost-estimating data (CED), and designer-influenced cost elements (DICE).

#### 4.4.1 Format Selection Aids

Format selection aids are presented to provide the user with a building-block approach to determine manufacturing cost data for alternative designs or processes. The designer can review the format selection trees and identify those areas that have an impact on his design. The formats provide cost-driver effects (CDE) for qualitative guidance to lowest cost and cost-estimating data (CED) in man-hours for conducting trade studies.

Selection aids are provided in the MC/DG Section for Extrusions for the following categories of formats:

- (a) Cost-driver effect of material extrusion and fabrication cost for curved parts in aluminum, titanium, and steel (CDE-EXTN-I to VI).
- (b) Determination of material cost and related factors (CED-EXTN-1 to 7) in aluminum, titanium, and steel.
- (c) Cost-estimating data for straight and contoured extrusions in aluminum, titanium, and steel (CED-EXTN-8 to 15), and also, designer-influenced cost elements (DICE-EXTN-1 to 5). DICE considered for extrusions are joggles, flanged holes, heat treatment and trim.

The designer first reviews CDE formats for guidance to the lowest cost. The selection aids indicate the scope of these formats. The designer then utilizes the CED formats.

A Cost Worksheet for Extrusions is included for use at the discretion of the designer to determine costs of the discrete part cost and/or the total program cost.

# FORMAT SELECTION AID

EXTRUDED AEROSPACE DISCRETE PARTS COST-DRIVER EFFECTS

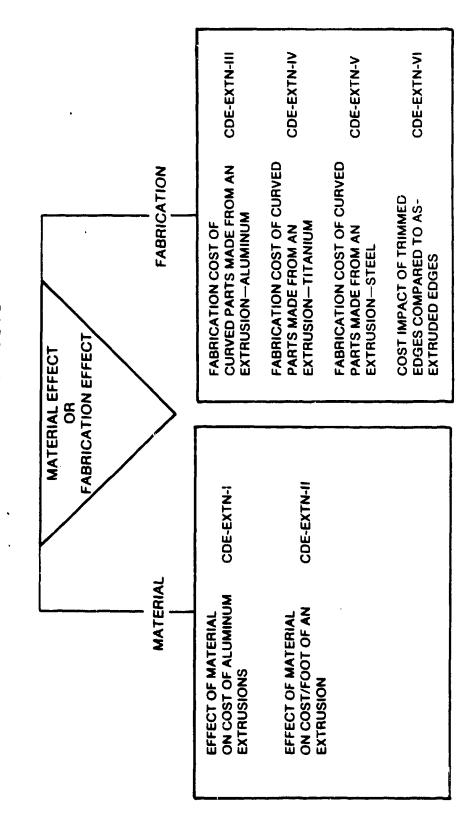
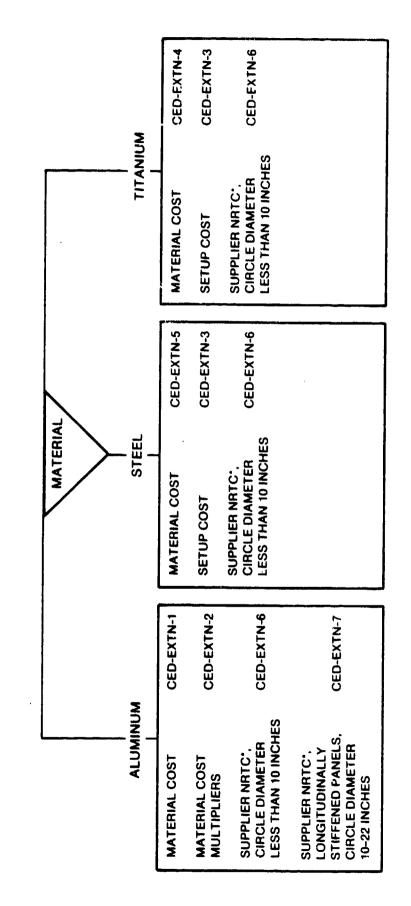


FIGURE 4.4-1

.

# FORMAT SELECTION AID

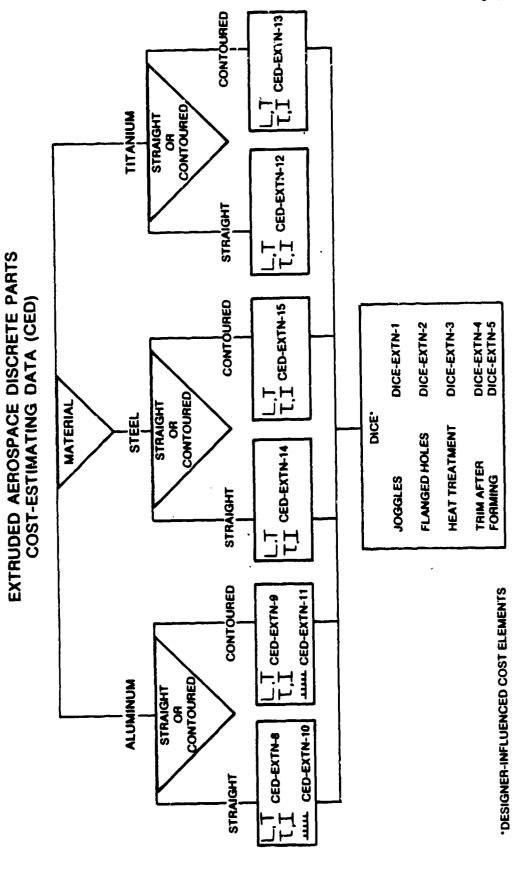
# EXTRUDED AEROSPACE DISCRETE PARTS MATERIAL COST



NONRECURRING TOOL COST

FIGURE 4.4-2

FIGURE 4.4-3



FORMAT SELECTION AID

4.4-4

# 4.4.2 Example of Utilization

This example demonstrates how the data generated are utilized on a specific design problem. The example shows how to identify applicable formats, how to extract data from the formats, and provides a discussion on how the data are used to determine the part cost in man-hours or dollars. The MC/DG cost worksheet can be used to record the cost data for easy reference and to determine the total program cost. The worksheet is included as Table 4.4-1.

#### 4.4.2.1 Material Cost for Aluminum Extrusions

#### Problem Statement

47

To determine the material cost for an aluminum extrusion:

- 1. Calculate the extrusion factor per example (page 4.4-7).
- 2. Using the extrusion factor from CED-EXTN-1 (Figure 4.4-5), determine the base price in 1983 dollars/pound.

NOTE: Use the 7075-T6511 curve for all extrusions except 6061 and wide ribbed shapes.

- 3. Select multiplier from Table CED-EXTN-2 (Figure 4.4-6).
- 4. Multiply the airplane design quantity by the number of parts per airplane (include both LH & RH) to arrive at the total number of parts. From CED-EXTN-3 (Figure 4.4-7), determine the extrusion supplier setup cost in 1982 dollars/part.
- 5. Calculate recurring material cost/part:
- 6. Determine the nonrecurring cost from CED-EXTN-6 (Figure 4.4-10) or CED-EXTN-7 (Figure 4.4-11).

# 4.4.2.2 Material Cost for Titanium/Steel Extrusions

### Problem Statement

Note that then calculating extrusion cross-sectional area and weight, all surfaces of titanium and steel extrusions must be machined. A machining allowance of 0.06 and 0.012 in. per surface should be made.

To determine the material cost of a titanium or steel part:

- 1. Calculate the extrusion weight (pounds/foot).
- 2. From CED-EXTN-4 (Figure 4.4-8) or CED-EXTN-5 (Figure 4.4-9), determine the price in dollars/pound for the appropriate material.

3. Calculate recurring material cost:

Material cost/part = [part length (ft) x weight (lb/ft) x cost (\$/lb) + setup cost] x inflation factor.

4. Determine nonrecurring cost from CED-EXTN-6 (Figure 4.4-10).

# 4.4.2.3 Cost of Aluminum Extrusion

# Problem Statement

Determine the cost of a Tee Section of dimensions 4" x 1.5" x 0.250".

• Weight: 1.28 lb/ft

• Extrusion Factor: 7

Part Length: 10 ft Material: 7075-T76511

Parts/Airplane: 2

Design Quantity: 200

CIRCUMSCRIBING CIRCLE

DIAMETER 3.06"

1.50"

1.50"

7YP.

FIGURE 4.4-4. EXTRUSION ANALYZED

# The extrusion factor must first be determined:

- (a) Calculate cross-sectional area perimeter (inches)

  Perimeter = (2 x 3.00 + 2 x 1.50) in

  = 9 in.
- (b) Calculate extrusion weight (pounds/foot)

  Cross-sectional area = 0.250 (3.00 + 1.50-0.25)in.2

  = 1.0625 in.2

Weight = area x 12"/ft x density

= 1.0625 x 12 x 0.1

- 1.275 1b/ft

(c) Calculate factor

Factor = perimeter (inches)
weight (pounds/foot)
= 9 inches
1.275 lb/ft

**7.06** 

- (d) This factor is used to determine the aluminum extrusion price.
- 1. From CED-EXTN-1: Base price is \$4.10/1b
- 2. From CED-EXTN-2: Multiplier is 1.10
- 3. From CED-EXTN-3: Setup cost is \$2.50/part
- 4. Inflation factor 1982: 1
- 5. Use recurring material cost/part formula:
- 6. Circumscribing circle size is 3+ inches.
  - From CED-EXTN-6, Nonrecurring Tool Cost (NRTC) is \$325.

# 4.4.2.4 Cost of Titanium Extrusion

#### Problem Statement

Determine the cost of a titanium "T" section of dimensions 3"  $\times$  1.5"  $\times$  0.250" (cross-sectional area = 1.0625 in.<sup>2</sup>)

Part length: 10 ft

Material: 6 A1-4V

Parts/ritplane: 2

STATE STATES OF THE STATES OF

Design quantity: 100

1. Weight/ft =  $1.0625 \times 12 \times 0.160$ 

= 2.04 lb/ft

- 2. From CED-EXTN-4: Base price is \$31.85/1b
- 3. From CED-EXTN-3: Setup cost is \$5.00/part
- 4. Inflation factor 1982: 1
- Recurring material cost/part
  - =  $(10 \text{ ft } \times 2.04 \text{ lb/ft } \times \$31.85/\text{lb} + \$5.00) \times 1$
- 6. From CED-EXTN-6, Nonrecurring Tool Cost (NRTC) is \$865.

# MATERIAL COST-ALUMINUM

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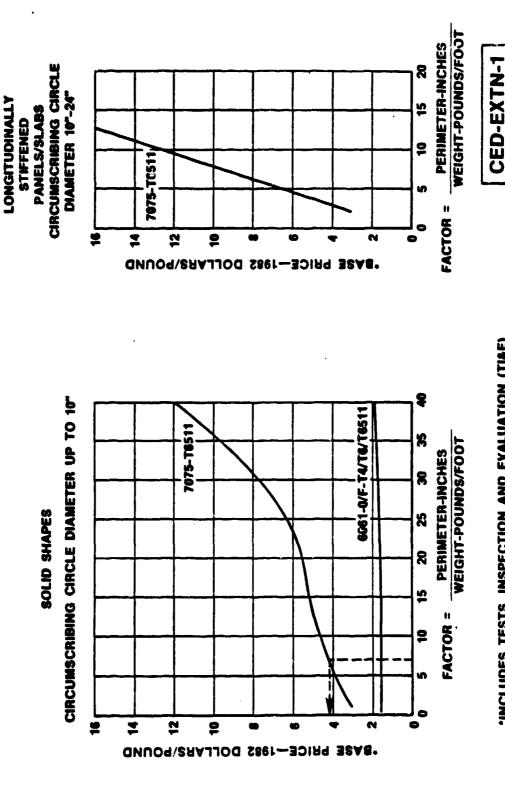


FIGURE 4.4-5. FORMAT USED IN EXAMPLE

INCLUDES TESTS, INSPECTION AND EVALUATION (TILE)

COST FOR THE AS-EXTRUDED MATERIAL

# MATERIAL COST—ALUMINUM

ALUMINUM		MULTIPLIER
ALLOY	TEMPER	MULTIPLIER
	T6	1.00
	T6511	1.00
7075	T73511	1.10
	T76511	1.10
	F	0.87
	0	0.89
	T6	1.20
	T6511	1.20
7178	T73511	1.32
	T76511	1.32
	F	1.04
	0	1.07
	T4	0.80
2024	T3511	0.80
	F	0.70
	0	0.71
	T6	0.67
2014	T6511	0.67
	F	0.58
	0	0.60
6061	Ali	1.00

CED-EXTN-2

FIGURE 4.4-6. FORMAT USED IN EXAMPLE

# MATERIAL—EXTRUSION SETUP COST FOR ALUMINUM, TITANIUM & STEEL

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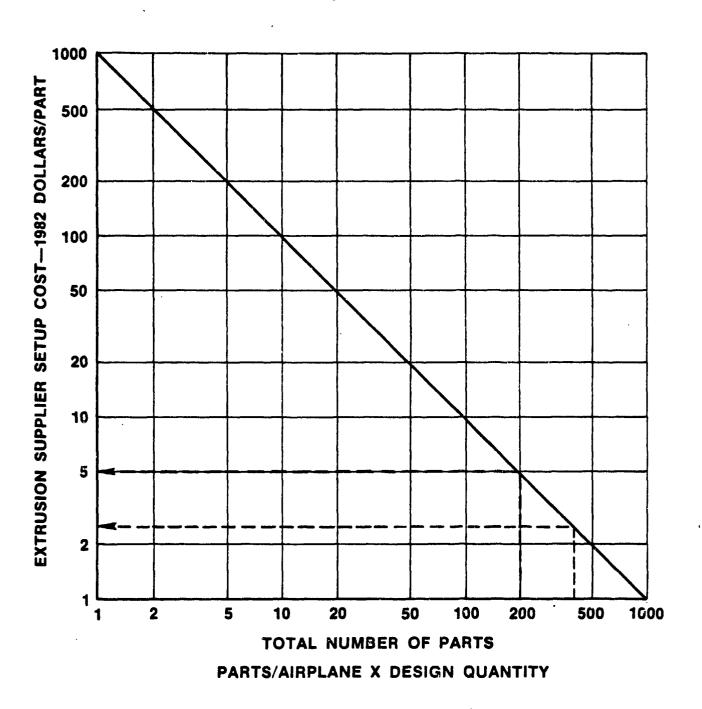
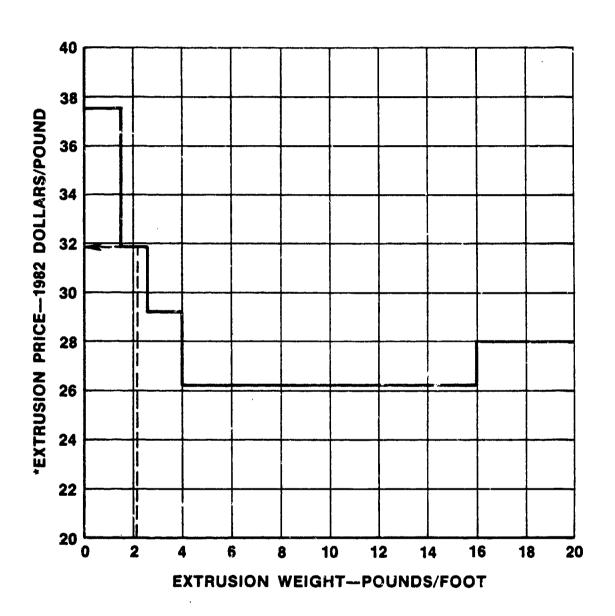


FIGURE 4.4-7. FORMAT USED IN EXAMPLE

**CED-EXTN-3** 

# MATERIAL COST—TITANIUM Ti 6AL-4V



\*INCLUDES TEST, INSPECTION, AND EVALUATION (TI&E) COST FOR THE AS-EXTRUDED MATERIAL.

FIGURE 4.4-8. FORMAT USED IN EXAMPLE

CED-EXTN-4

# MATERIAL COSTS - STEEL

Based upon limited historical cost data in the absence of published price schedules, approximate material costs for steel extrusions are:

•	1982 Cost*
Tow Alloy Steels	
4130, 4140, 4340, 8630	\$3.50/Lb
PH13-8Mo CRES	\$16.50/Lb

CED-EXTN-5

FIGURE 4.4-9. FORMAT USED IN EXAMPLE

<sup>\*</sup> Includes TI&E cost for the as-extruded material.

# SUPPLIER NONRECURRING TOOL COST CIRCUMSCRIBING CIRCLE UNDER 10" DIAMETER

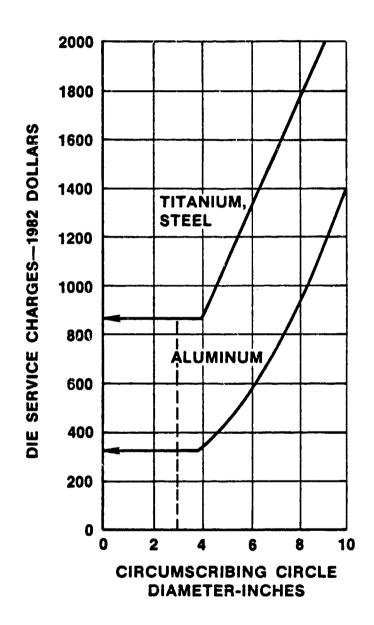


FIGURE 4.4-10. FORMAT USED IN EXAMPLE

**CED-EXTN-6** 

# SUPPLIER NONRECURRING TOOL COST FOR LONGITUDINALLY STIFFENED PANELS/SLABS CIRCUMSCRIBING CIRCLE DIAMETER 10"-22"

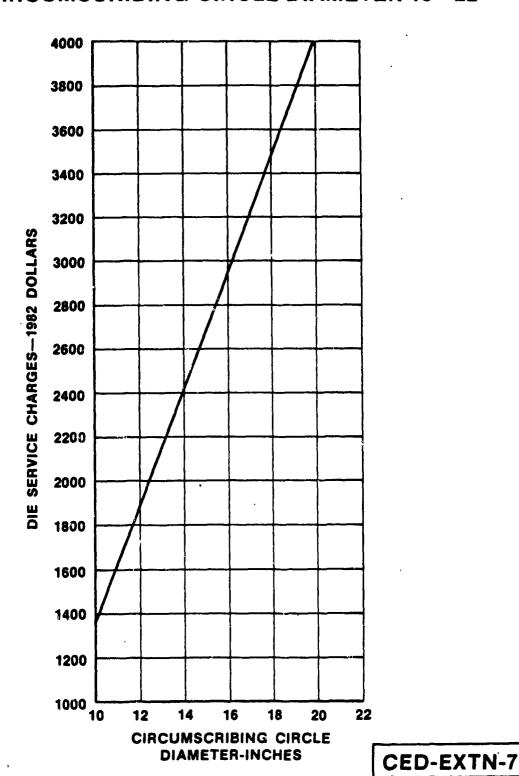


FIGURE 4.4-11. FORMAT USED IN EXAMPLE

4.4-15

# TABLE 4.4-1. EXTRUSIONS-COST WORKSHEET

RT NO.: DESCRIPTION:		DESIGNER:		DATE:	
MATERIAL COST		ALUMINUM ONLY:			
MATERIAL COST		inJ	Lb/Pt		
Se in.	Lb/In. <sup>3</sup> Lb/f	Portmeter	Weight	Factor	
Grees Section Area	N Density Weight	-			
Base Prime (C	:ED-EXTN) 8/L		plior (CED-EXTN-2)		
			EXTN-3) _ 8	/Part	
·	Airplane Total City.	•			
Mot1	Ft x Lb/Ft x Bose F	/Lb x *Multiplier	Setup "Infli	S(a)	
Pert Longitit	,			_	
_	Cool (CED-EXTN-			E(b)	
*Aluminum Only **k	nflation Factor to be Supplied by U			NONRECURRING	
FABRICATION COST		FORMAT NUMBER	RECURRING COST	COST	
		CED-EXTN-	MH	M	
BASE PART COST		DICE-EXTN-	MH	MI	
DICE		DICE-EXTN-	Men		
J. 1		CED-	MH	M	
	FABRICATION COST (UNIT 200)		(e) MH		
(e) Learning Curve Paster-	See Zabia Salam	<del></del>			
(f) Labor Rate			8 /MH	8 MH	
(g) Fabrication Coolrice:	umbas/Barble v a v ft		8 EA		
(h) Pabrication Cost—Non					
(11) 7 22 10 2 10 10 10 10 10 10 10 10 10 10 10 10 10	1000 mg(0 m 1)				
COST SUMMARY					
(a) Motorial Cool/Part				8	
(g) Pabrication Recurring	•				
(i) Design Quantity					
(j) Program Recurring Cost (a + g) i					
(b) Nenresuming Cost (a * g) 1 (b) Nenresuming Cost—Material				•	
(h) Nearrouning Coci-Fe					
(k) Nonrecurring Cost—To	PER (3 T 11)			8	
(m) Program Coat (j + k)					

†Length of extrusion required for surved (stratch formed) parts is part length + 2 feet

-			
Des. Gty	LC Feeter	Dec. Gty	LC Paster
1	2.26	200	1.17
10	1.79	200	1.86
25	1.50	<b>500</b>	1.02
50	1,44	750	0.96
100	1.30	1906	0.02

98% Learning Curve Faster to Conver Unit 209 Fermat cost to Cumulative Average cost for Various Design Quantities.

# 4.4.3 Parts Analyzed

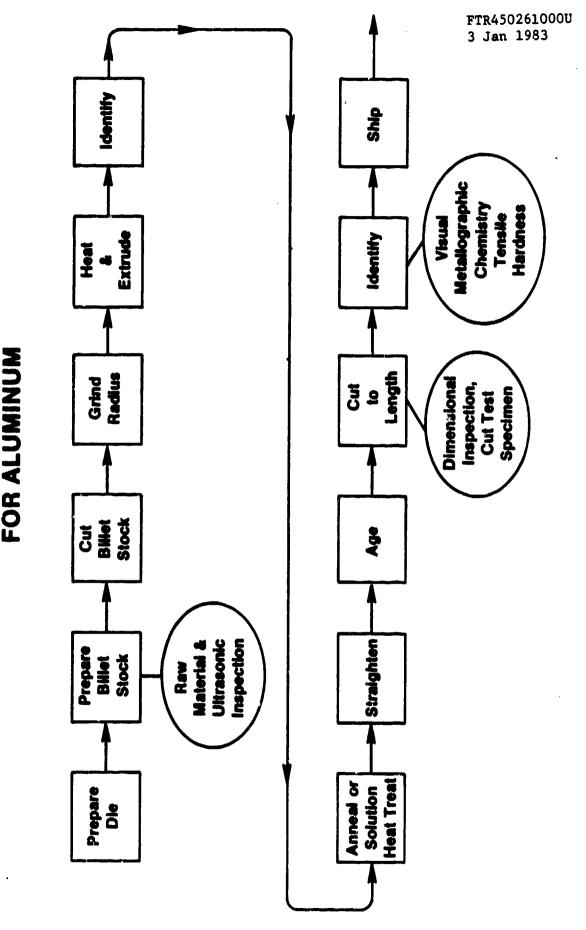
The data for the extruded base parts and designer-influenced cost elements (DICE) evaluated are applicable to the extruded shapes in Figure 4.4-12. As indicated in the ground rules in this section, manufacturing man-hour information is also provided for 6Al-4V titanium and also PH13-8 and 4340 steel extrusions. The manufacturing operations for aluminum, titanium, and steel extrusions are shown in Figures 4.4-13 to 4.4-15.

# MC/DG EXTRUSIONS—ALUMINUM

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# CED FORMATS FOR FABRICATION OF BASE PART SH INCLUDING DICE ARE VALID FOR THE EQUIVALENT TYPICAL SHAPES

	BASE PARTS	EQUIVALENT TYPICAL SHAPES		
4	EL, ET	\ EL, ET	UEL, UET	UEL, UET
AL ETRICA				<u> </u>
SYM—SYMMETRICAL UNSYM—UNSYMMETRICAL	90° ANGLE	EL, ET	UEL, LIET	BULBED
SYM—SYI UNSYM—		UET, EL	UNSYM ET	ANGLED ET
ESS	SO" TEE Symmetrical	ANGLED ET, EL	BULBED	UET, EL
AL LEG AL THICKNESS		UEL, ET	ANGLED ET	UET, EL
-UNEQUAL	90° JAY	ANGLED ET	BULBED	LIPPED EL, ET
UEL UET		ET, SYM	UET, EL	BULBED
LEG THICKNESS	90° I SYMMETRICAL	UEL, ET	ANGLED EL, ET	LIPPED EL, ET
EQUAL LEG		· IIIII		
EL—EO ET—EO	PANEL	<u> </u>	-11111	• 



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**EXTRUSION MANUFACTURING FLOW** 

FIGURE 4.4-13.

Hardness Tensile

Specimen Cut Test

Metallographic Chemistry

Dimensional Inspection,

Visual

E

FIGURE 4.4-14

### Identify Ship **EXTRUSION MANUFACTURING FLOW** & Extrude Lubricat Heat, **Identify** FOR TITANIUM AND STEEL Grind Redius Length 2 Straighten Cut Billet Stock t Uttrasonic Inspection Material Prepare Stock Biller H Annea

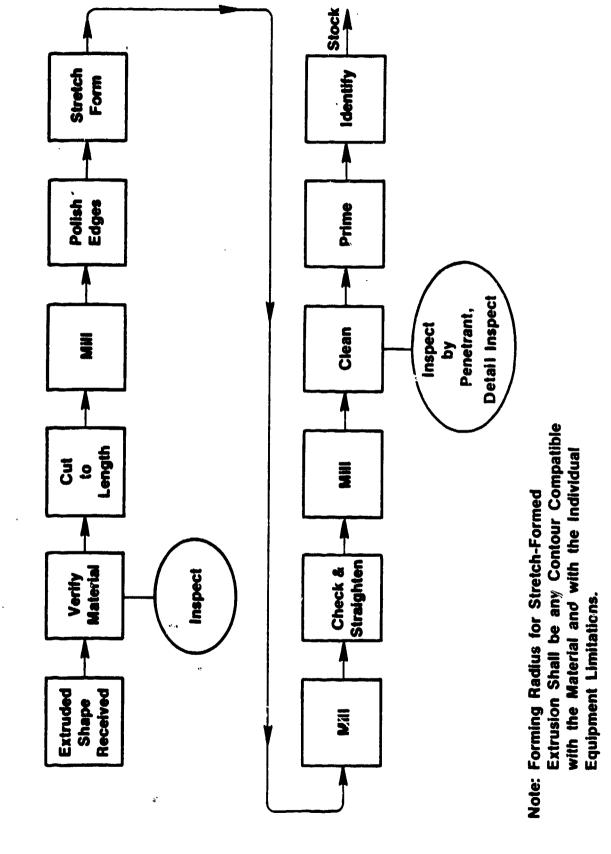
Prepare

충

4 Picke Send Blast 4.4-20

FIGURE 4.4-15.

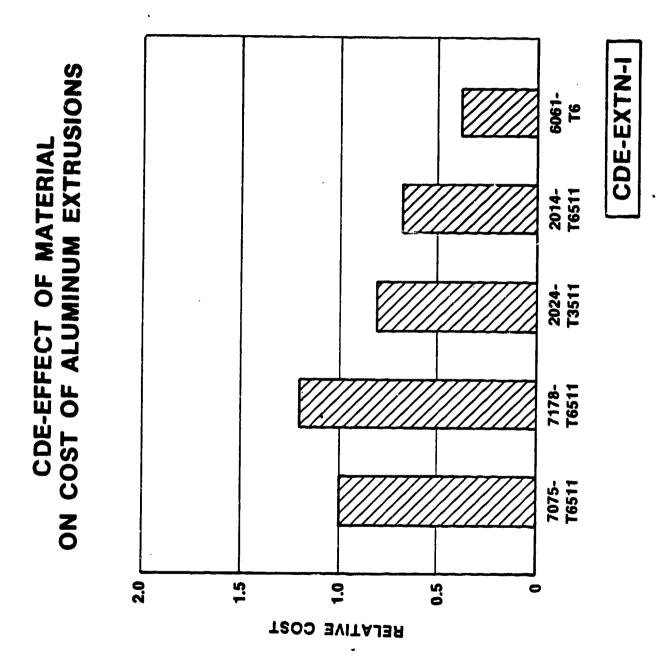
# TITANIUM AND STEEL CURVED SHAPES ONLY **EXTRUSION MANUFACTURING FLOW FOR**



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### 4.4.4 Extrusion Manufacturing Cost Data

The formats on the following pages provide designer guidance in extrusion selection and design and also enable cost trade studies to be conducted. The scope of the formats for extrusions is indicated in Section 4.4.2.

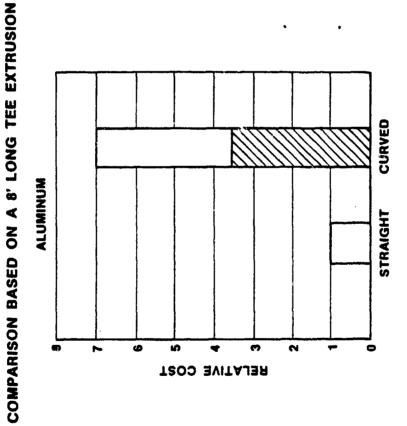


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CDE-EXTN-II CDE-EFFECT OF MATERIAL ON THE COST/FOOT OF AN EXTRUSION 1.50 4340 PH 13-8 **Ti 6AI-4V** 7075-T6511 RELATIVE COST

### CDE-EXTN-III

CDE-FABRICATION COST OF CURVED PARTS MADE FROM EXTRUSIONS

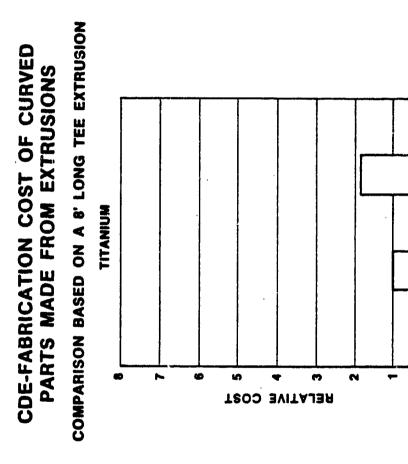


RECURRING

NRTC AMORTIZED OVER 200 PARTS

FOR BASELINE REFERENCE, SEE CED NO.

### CDE-EXTN-IV



RECURRING

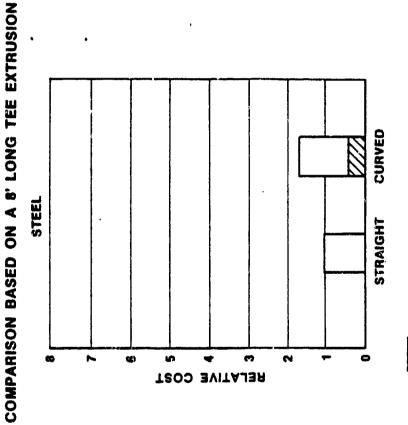
NRTC AMORTIZED OVER 200 PARTS

STRAIGHT

FOR BASELINE REFERENCE, SEE CED NO.

### CDE-EXTN-V





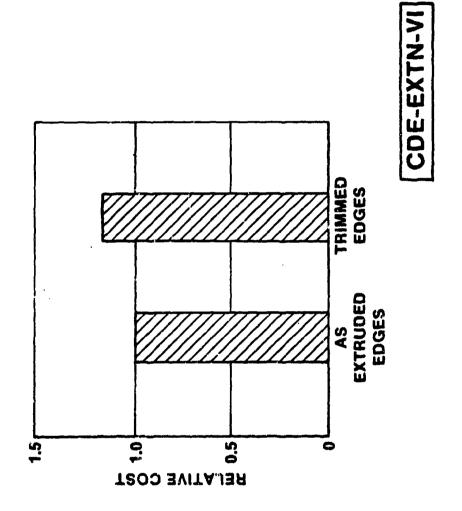
RECURRING

MITC AMORTIZED OVER 200 PARTS

FOR BASELINE REFERENCE, SEE CED NO.

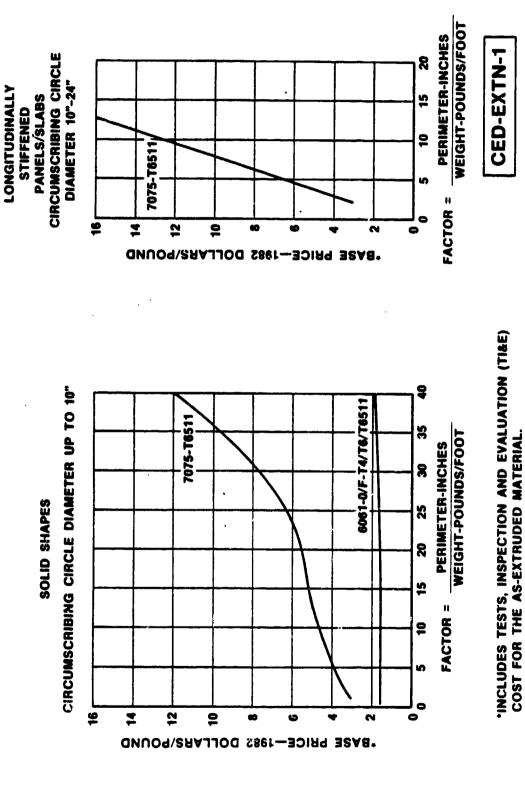
# CDE-COST IMPACT OF TRIMMED EDGES COMPARED TO AS EXTRUDED EDGES

COSTS INCLUDE MATERIAL, FABRICATION LABOR & NRTC BASED ON 7075-T6 ALUMINUM TEE 3" x 3" x 1/8" THICK 8' LONG FORMED TO A 60" RADIUS.



# MATERIAL COST-ALUMINUM

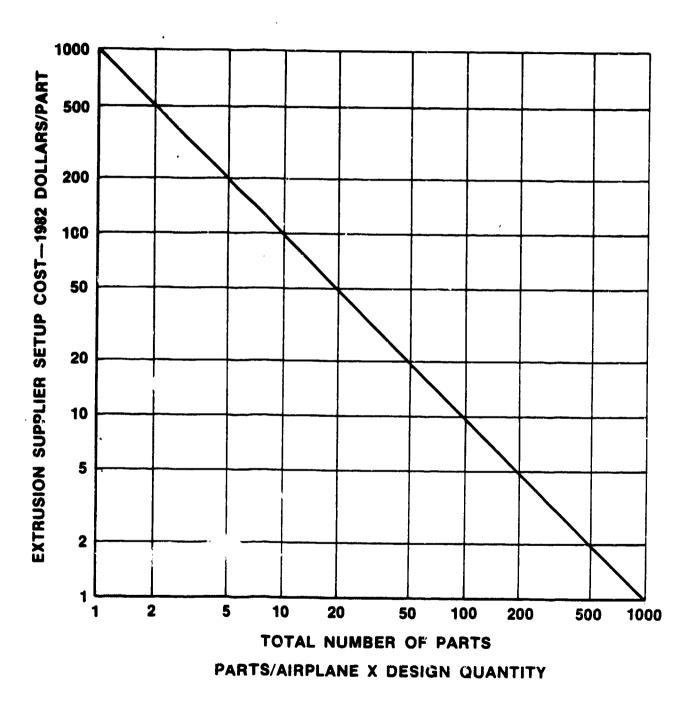
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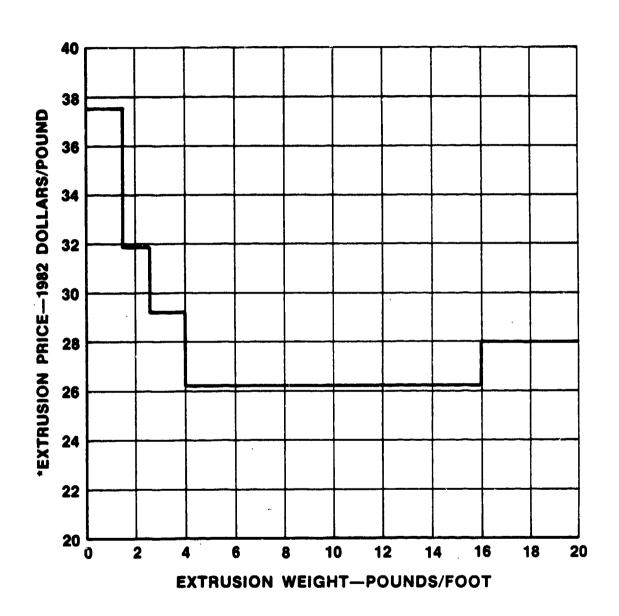
### MATERIAL COST—ALUMINUM

ALUMINUM		MIN TIPLIED
ALLOY	TEMPER	MULTIPLIER
	T6	1.00
	T6511	1.00
7075	T73511	1.10
	T76511	1.10
	F	0.87
	0	0.89
	T6	1.20
	T6511	1.20
7178	T73511	1.32
	T76511	1.32
	F	1.04
	0	1.07
2024	T4	0.80
	T3511	0.80
	F	0.70
	0	0.71
2014	T6	0.67
	T6511	0.67
	F	0.58
	0	0.60
6061	All	1.00

### MATERIAL—EXTRUSION SETUP COST FOR ALUMINUM, TITANIUM & STEEL



### MATERIAL COST—TITANIUM Ti 6AL-4V



\*INCLUDES TEST, INSPECTION, AND EVALUATION (TI&E) COST FOR THE AS-EXTRUDED MATERIAL.

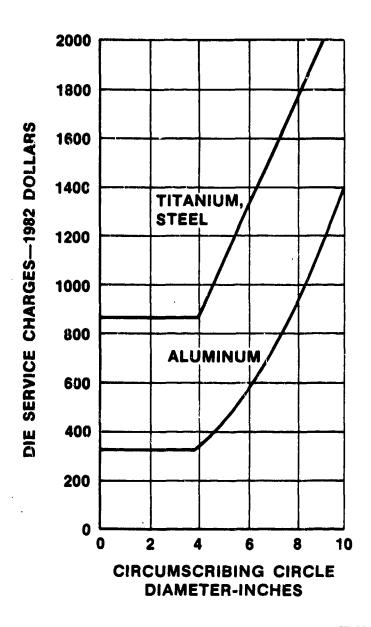
### MATERIAL COSTS - STEEL

Based upon limited historical cost data in the absence of published price schedules, approximate material costs for steel extrusions are:

	1982 Cost*
Low Alloy Steels	A2 50/73
4130, 4140, 4340, 8630	\$3.50/Lb
PH13-8Mo CRES	\$16.50/Lb

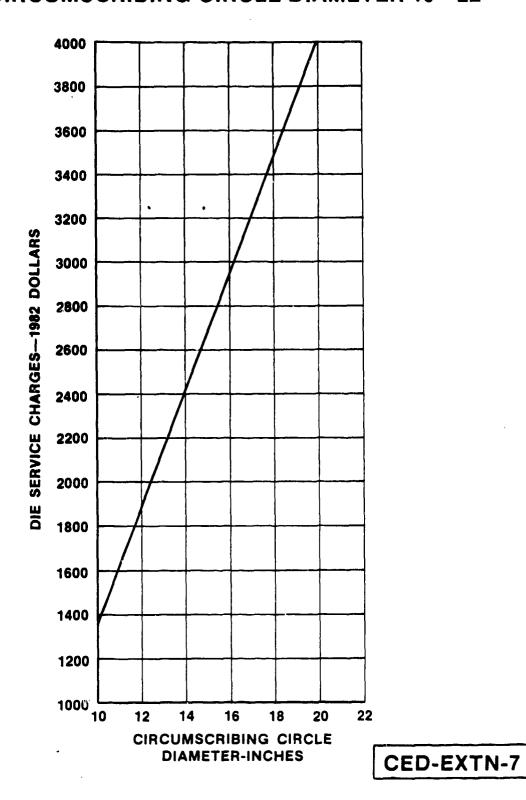
<sup>\*</sup> Includes T\*&E cost for the as-extruded material.

### SUPPLIER NONRECURRING TOOL COST CIRCUMSCRIBING CIRCLE UNDER 10" DIAMETER



### SUPPLIER NONRECURRING TOOL COST FOR LONGITUDINALLY STIFFENED PANELS/SLABS CIRCUMSCRIBING CIRCLE DIAMETER 10"-22"

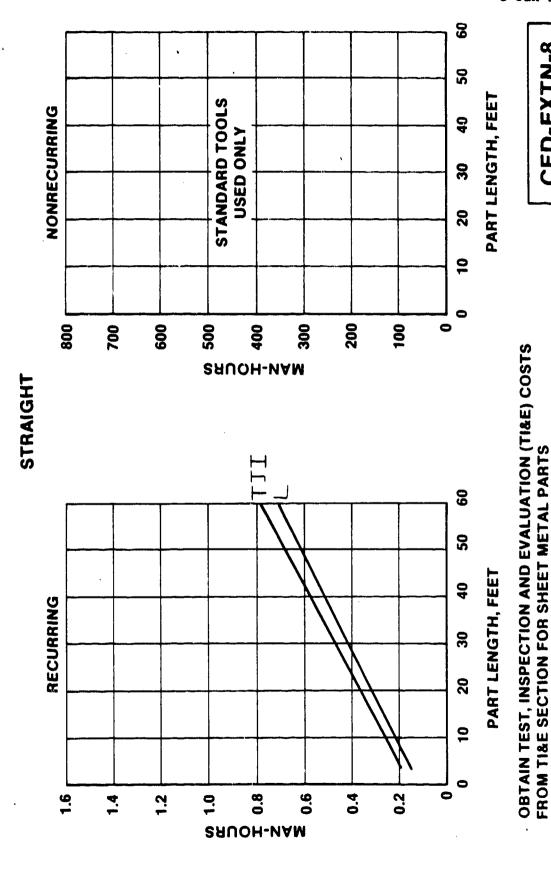
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CED-EXTN-8

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### **ALUMINUM EXTRUSIONS LINEAL SHAPES**

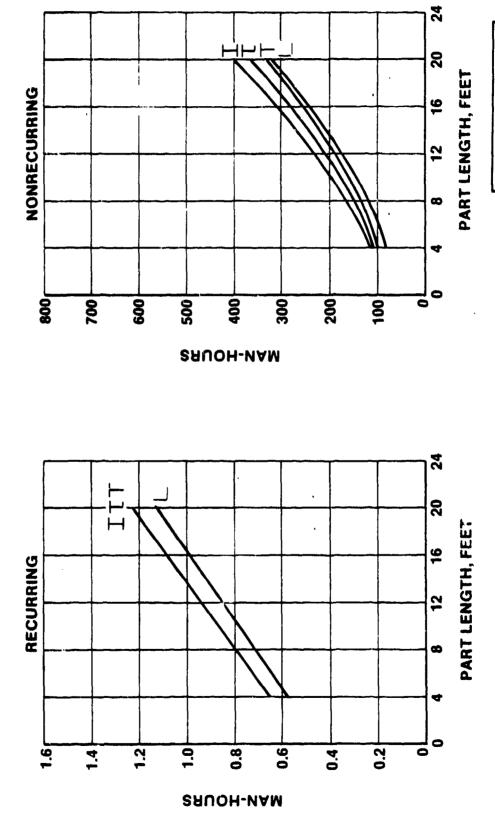


CED-EXTN-9

# ALUMINUM EXTRUSIONS LINEAL SHAPES

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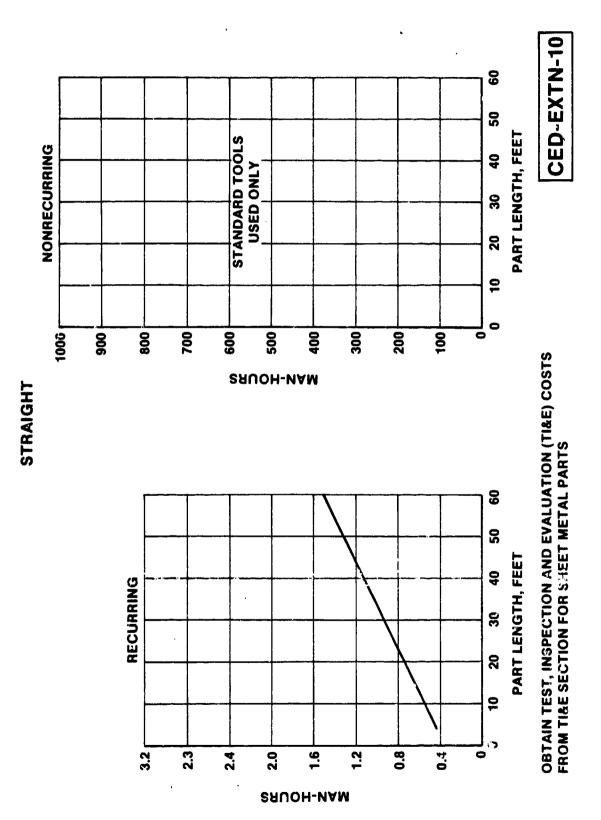
CYLINDRICALLY OR NON-CYLINDRICALLY CONTOURED



OBTAIN TEST, INSPECTION AND EVALUATION (TI&E) COSTS FROM TI&E SECTION FOR SHEET METAL PARTS

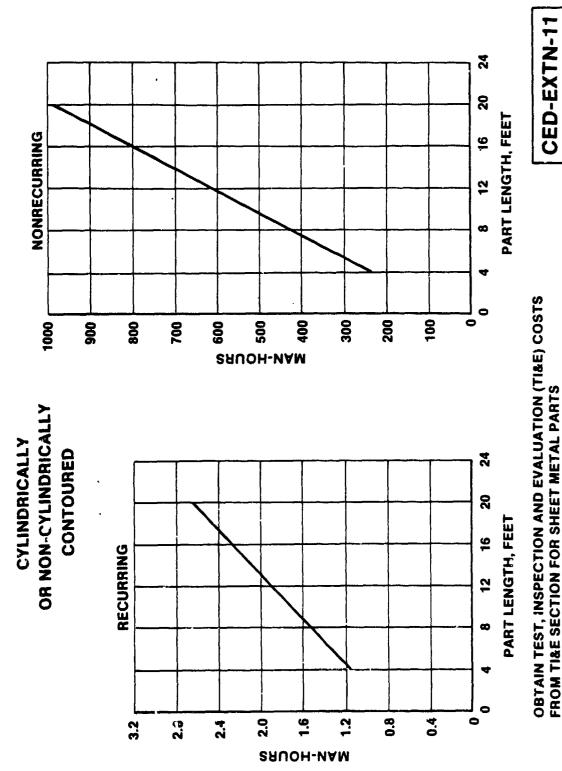
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## ALUMINUM EXTRUSIONS LONGITUDINALLY STIFFENED PANELS/SLABS



ALUMINUM EXTRUSIONS LONGITUDINALLY STIFFENED PANELS/SLABS

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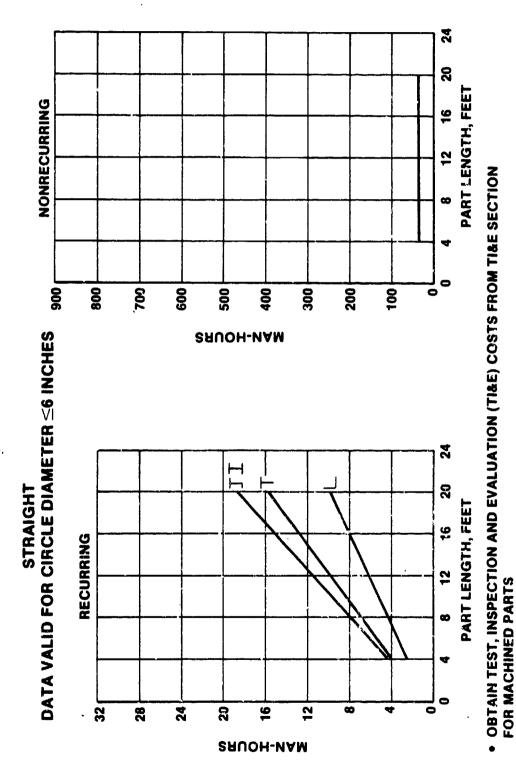


CED-EXTN-12

COST INCLUDES MACHINING TO ASSURE CONTAMINATION FREE, SMOOTH

SURFACE/EDGE

# TITANIUM EXTRUSIONS LINEAL SHAPES

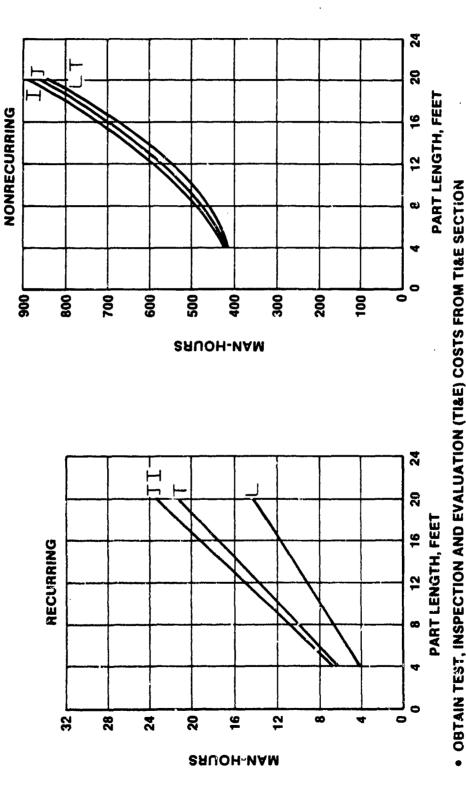


# TITANJUM EXTRUSIONS LINEAL SHAPES

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CYLINDRICALLY OR NON-CYLINDRICALLY CONTOURED DATA VALID FOR CIRCLE DIAMETER ≤6 INCHES

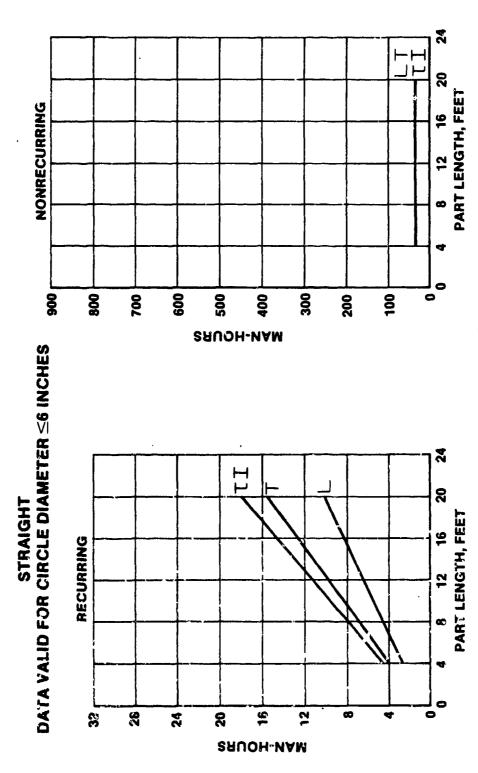


FOR MACHINED PARTS

CED-EXTN-13

COST INCLUDES MACHINING TO ASSURE CONTAMINATION FREE, SMOOTH SURFACE/EDGE

## STEEL EXTRUSIONS LINEAL SHAPES



MULTIPLY MAN-HOURS BY 1.06 WHEN EXTRUDED WEIGHT≥ 100 POUNDS

OBTAIN TEST, INSPECTION AND EVALUATION (TIME) COSTS FROM TIME SECTION FOR MACHINED PARTS

COST INCLUDES MACHINING TO ASSURE CONTAMINATION FREE, SMOOTH SURFACE/EDGE

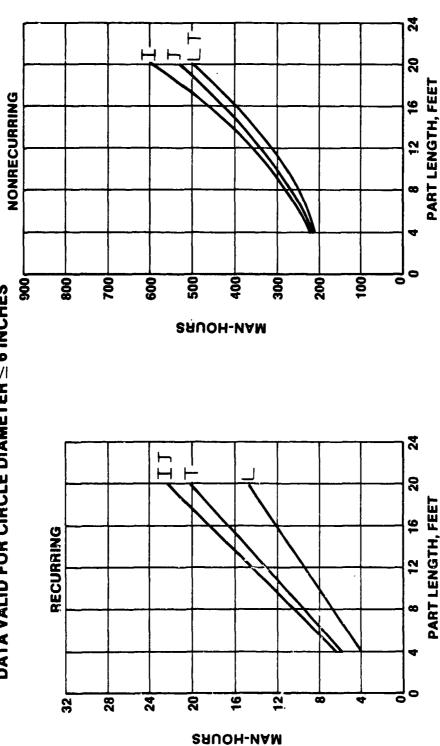
CED-EXTN-14

### STEEL EXTRUSIONS LINEAL SHAPES

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CYLINDRICALLY OR NON-CYLINDRICALLY CONTOURED DATA VALID FOR CIRCLE DIAMETER ≤ 6 INCHES



MULTIPLY MAN-HOURS BY 1.06 WHEN EXTRUDED WEIGHT  $\geq$  100 POUNDS

OBTAIN TEST, INSPECTION AND EVALUATION (TIME) COSTS FROM TIME SECTION FOR MACHINED PARTS

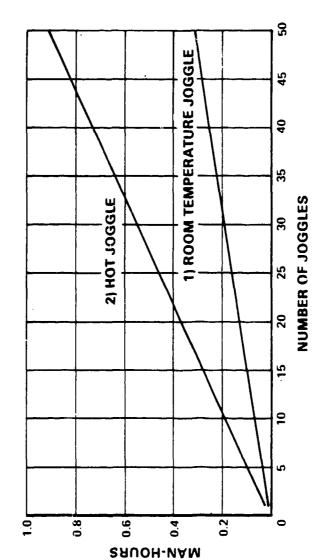
COST INCLUDES MACHINING TO ASSURE CONTAMINATION FREE, SMOOTH

SURFACE/EDGE

CED-EXTN-15

4.4-43

### EXTRUDED LINEAL PARTS JOGGLE RECURRING COST



1) USED FOR ALUMINUM AND STEEL PARTS 2) USED FOR TITANIUM PARTS

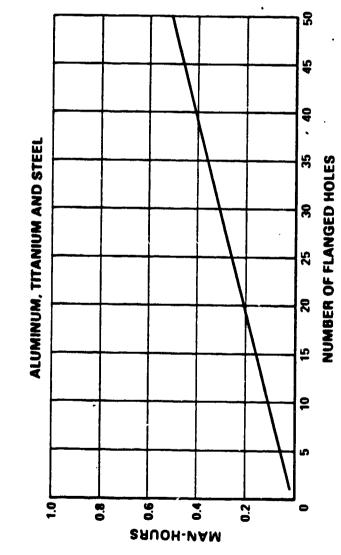
BASED ON USE OF STANDARD TOOLS

DICE-EXTN-1

### DICE-EXTN-2

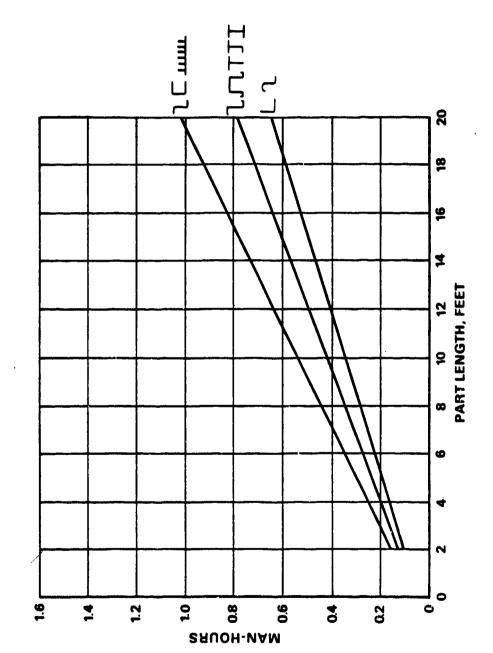
# EXTRUDED DISCRETE PARTS FLANGED HOLE RECURRING COST

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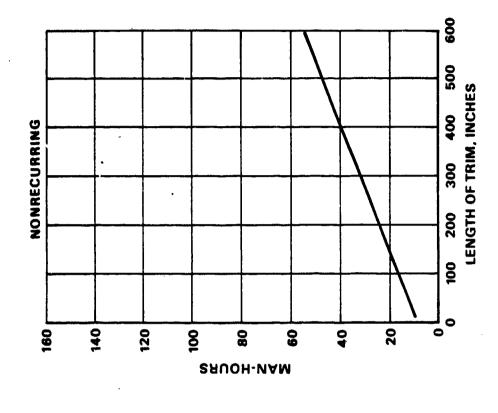
**BASED ON USE OF STANDARD TOOLS** 

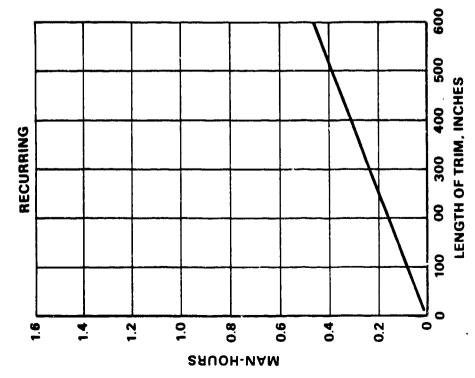




### DICE-EXTN-4

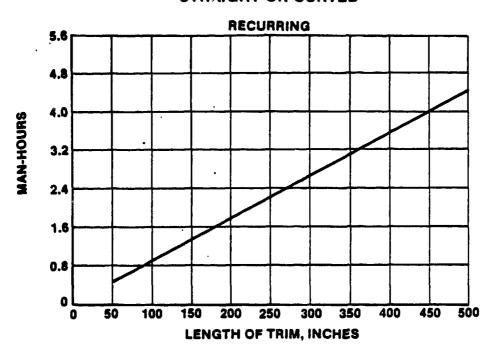
### ALUMINUM EXTRUSIONS LINEAL PARTS TRIM AFTER FORMING

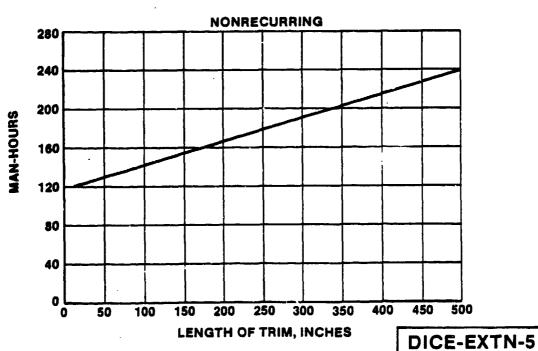




NOTE: EXTRAPOLATE TO 600"

### STEEL OR TITANIUM EXTRUSIONS TRIM EDGES STRAIGHT OR CURVED





### 4.4.5 Ground Rules for Extrusions Section

The following General and Detailed Ground Rules for the Extrusions Section were developed to establish the scope of the data required and to establish guidance to MC/DG application. Ground rules are necessary and important as they promote understanding, ensure consistency, uniformity, and accuracy in generating and integrating data into the formats.

### 4.4.5.1 General Ground Rules

The general ground rules are categorized under the following major groupings:

- (a) Extruded Discrete Parts
- (b) Materials
- (c) Manufacturing Methods
- (d) Facilities
- (e) Data Generation Recurring Costs
- (f) Data Generation Nonrecurring Costs
- (g) Support Function Modifiers.

### (a) Extruded Discrete Parts

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- (1) The extruded aerospace discrete parts selected will be representative of common structural parts required for both small and large aircraft. The parts will be selected such that a base part forms the foundation which the designer can modify as required to achieve the desired discrete part of structural configuration. Extruded discrete parts include stringers, longerons, frame rib and spar caps representing elements of major airframe structural subassemblies.
- (2) The discrete parts will be selected, where possible, to develop data for more than one manufacturing method. The data thereby enables the designer, using the MC/DG, to determine the most cost-competitive manufacturing method in trade-studies.
- (3) The selected discrete parts will be defined and dimensioned to adequately display the effect on part cost of DICE, e.g., joggles, trim, and lightening holes. Facility limitations

- will be used in determining the dimension ranges for the discrete part considered.
- (4) Support function modifiers will be excluded but can be handled in the preferred way by the aerospace company using the MC/DG.

### (b) Materials

- (1) The alloys selected for the discrete parts will be representative of the range of those more commonly used in the industry to enable a uniform data base to be established. The materials included are:
  - Aluminum
  - Titanium
  - Steel.
- (2) Raw material costs for the parts will be included in the MC/DG formats.
- (3) Material cost of nonrecurring tooling will not be included, except when this cost impacts a design decision, for example, for manufacturing certain discrete parts in titanium.

### (c) Manufacturing Methods

- (1) Only conventional manufacturing methods required to produce the extruded parts in the configurations selected will be considered. No emerging manufacturing methods will be evaluated.
- (2) A production, in contrast to a prototype environment will be assumed for the extruded discrete parts.
- (3) To generate an effective data base for each selected part, a factory operational sequence for each applicable manufacturing method will be established reflecting the most economical means of fabrication. This standardized sequence will be used by each airframe company team member to determine the part cost (man-hours).

(4) Tool families required to manufacture the various parts will be identified on the data collection forms.

### (d) Facilities

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(1) Only standard manufacturing facilities, available to the airframe industry, will be considered.

### (e) Data Generation - Recurring Costs

- (1) Recurring and nonrecurring man-hour data will be generated for the complete process of parts fabrication and will include all hands-on-factory direct labor operations from raw stock through forming, heat treatment, priming, etc., to storage of the part in preparation for assembly into the airframe.
- (2) The base-part cost (man-hours) will be generated for each part. The base-part cost will represent the sum of all standard hours associated with each part.
- (3) DICE, requiring added operations, will be treated as separate cost elements, and therefore, will not be included in the base-part cost.
- (4) The quantity for which the base-part cost will be determined is unit 200 and will be based on team member learning curves.
- (5) Labor cost data will be presented in man-hours. Material costs will be presented in 1982 dollars. The data submitted to BCL will be the base-part cost plus the costs (man-hours) of DICE associated with the discrete part design.
- (6) To demonstrate the impact of set up costs, lot releases of 25 parts will be used.
- (7) Set up time (man-hours) is the total set up time required to complete the part. The set up time will be amortized over the lot size and added to run times to obtain the base-part cost (man-hours).
- (8) Recurring tooling costs (tool maintenance, planning, etc.) will not be included.

- (9) In developing cost data for parts, each participating company will utilize its own proprietary learning curves.
- (10) The part cost, as derived by each airframe company, will be normalized by BCL to reflect an industry team average value for each discrete part and range of dimensions.
- (11) For proprietary reasons, realization factors (including PF&D), standard hours, and other business sensitive information employed at team member companies will not be included in the analysis on the data sheets or MC/DG formats.
- (12) No data provided by any team member will be disclosed to other team members, agencies, or to the public without whe expressed approval of the team member.

### (f) Data Generation - Nonrecurring Costs

- (1) Tool fabrication costs will be generated for each part type. In addition, tool design and tool planning costs will be evaluated with respect to their impact, to determine whether they should be included or omitted for the three material types.
- (2) The cost of production tooling, if included, will be restricted to contract or project tools only, for presentation in the MC/DG.
- (3) Nonrecurring tooling, including extrusion die, costs (NTRC) generated by the team companies will be normalized by BCL for presentation in the MC/DG.

### (g) Support Function Modifiers

(1) Additional effort other than factory labor, such as manufacturing engineering, will be excluded from the part cost data supplied to BCL. These modifiers may be included later by users of the MC/DG.

### 4.4.5.2 Detailed Ground Rules

The detailed ground rules are categorized under the following major groupings:

- (a) Materials
- (b) Size and Shape
- (c) Tolerances
- (d) Discrete Parts
- (e) Manufacturing Methods
- (f) Facilities
- (g) Contract Tooling.

### (a) Materials

- (1) The materials selected for sheet-metal discrete parts are:
  - Aluminum: 2024, 7075 and 6061
  - Titanium: 6Al-4V (annealed)
  - Steel: PH13-8 CRES and 4340.
- (2) Treatment required for any of these materials to increase physical properties or to improve formability will be indicated on the part sketches, data collection forms, and formats.
- (3) For aluminum, recent price sheets will be used. For titanium and steel, airframe company historical data will be used.
- (b) Size and Shape
  - (1) Maximum circle size: 24"
  - (2) Typical shapes will include:
    - Angles
    - Tees
    - J's
    - I's
    - Ribbed panel extruded flat
  - (3) Hollow extrusions not to be considered.

### (c) Tolerances

- (1) Industry accepted mill tolerances for extrusions and for discrete parts fabricated from extrusions will be considered.
- (2) Parts will be manufactured to a tolerance of ± 0.030 inch.

  The cost impact of tighter or more relaxed tolerances is considered to be a designer-influenced cost element (DICE).

### (d) Discrete Parts

- (1) Drawings of the extruded aerospace discrete parts showing configurations, dimensions, jeggles, holes, trim, heat
  treatment, etc., will be prepared so that each team member
  may estimate base standard hours in a consistent manner.
- (2) The cross-sectional dimensions of the lineal shapes will correspond to a maximum envelope of 6 inches diameter.
- (3) The operational sequence necessary to produce each part, as required by the detail drawings, will include every operation required to fabricate the part by the manufacturing method being evaluated, i.e., from the blank to completion ready for the storeroom and assembly into the airframe.
- (4) To facilitate trade-off studies, the discrete parts and MC/DG formats will indicate any thermal and/or chemical processing required such as heat treatment and anodizing, respectively, and also painting, prior to assembly, as specified on the detail drawing.

### (e) Manufacturing Methods

- (1) Forming methods used to fabricate the respective parts will be specified on part size matrices accompanying each drawing and on the data collection forms.
- (2) Where more than one manufacturing technology will be candidates to fabricate a discrete part, data will be generated for each method to reveal the comparative cost relationships to the designer.

### (f) Facilities

(1) The types of forming equipment utilized in the fabrication of the parts will be those listed in the part size matrix accompanying each extruded discrete part drawing.

### (g) Contract Tooling

- (1) Because of nonuniformity of tool nomenclature, each team member company will indicate (on the data collection forms) the tool family required to fabricate each discrete part. The nomenclature shown on the forms will be supplemented with information providing a complete tool description, i.e., Drill Press Fixture (DPF).
- (2) Tools to be included will be those required to manufacture the the tools, as well as those to make and check the parts, i.e., production check tools.
- (3) The average hours per tool type, individual tool estimate, etc., will be determined in accordance with standard procedures for determining cost at the facilities of each team member.

### 4.5 <u>Casting Section</u>

This section contains format selection aids, identification of the types of parts analyzed for data to determine the manufacturing man-hour data, examples of how the data are utilized in airframe design and a set of formats generated. These formats include cost-driver effects (CDE), cost estimating data (CED), and designer-influenced cost elements (DICE).

### 4.5.1 Formst Selection Aids

Format selection aids are presented to provide the user with a building-block approach to determine manufacturing cost data for alternative designs or processes. The designer can review the format selection trees and identify those areas that have an impact on his design. The formats provide cost-driver effects (CDE) for qualitative guidance to lowest cost and cost-estimating data (CED) in man-hours for conducting trade-off studies.

### CASTINGS COST DRIVER EFFECTS

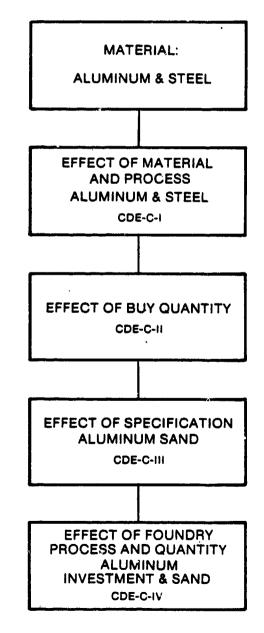
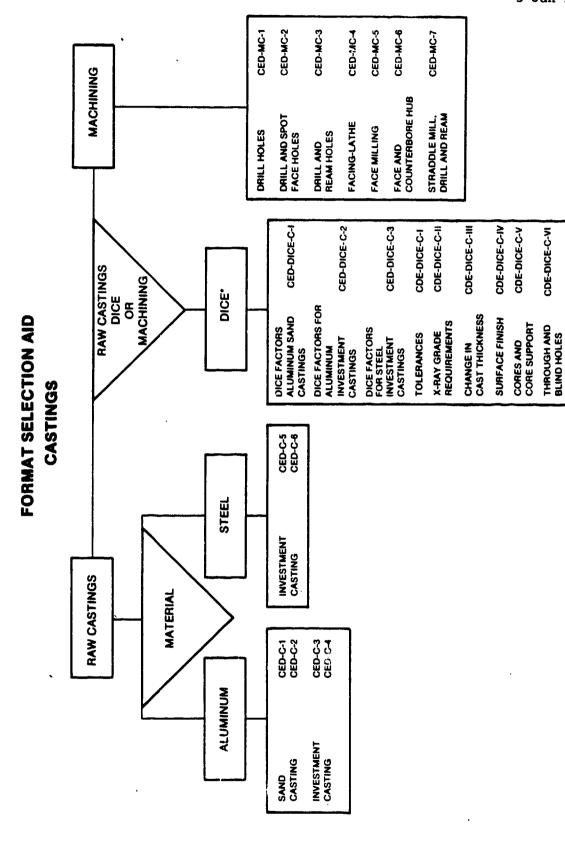


FIGURE 4.5-1



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FIGURE 4.5-2

\*DESIGNER-INFLUENCED COST ELEMENTS

### FORMAT SELECTION AID

### MACHINING OF CASTINGS

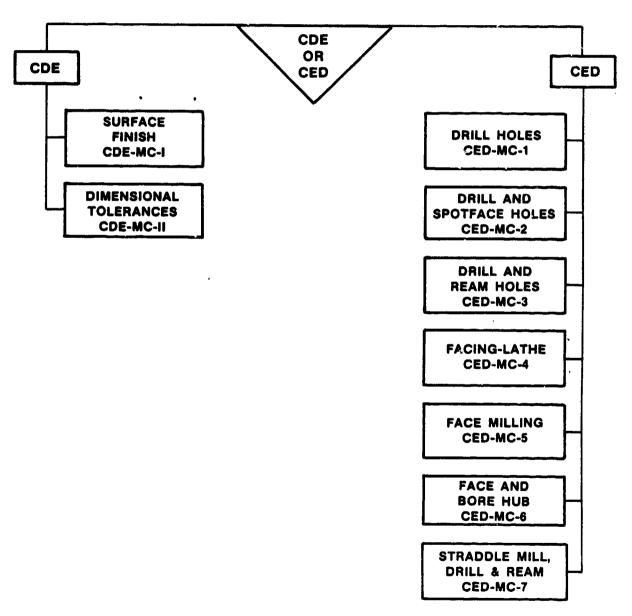


FIGURE 4.5-3

### 4.5.2 Example of Utilization

This example demonstrates how the data generated are utilized on a specific design problem. The example shows how to identify applicable formats, how to extract data from the formats, and provides a discussion on how the data are used to determine the part cost in man-hours or dollars. The MC/DG cost worksheet can be used to record the cost data for easy reference and to determine the total program cost (Figure 4.3-3). Specific worksheets for casting appear as Tables 4.5-2 and 4.5-3 (Machining of Castings).

### 4.5.2.1 Utilization Example for Bell Crank

### Problem Statement

Determine the cost (1980 dollars) for the aluminum bell crank shown in Figure 4.5-4. Cost elements are: Cost elements are:

- Base casting cost
- Designer-Influenced Cost Elements (DICE)
- Test, Inspection and Evaluation (TI&E) cost of raw casting
- · Cost of machining the casting to final dimensions.

The casting has a box volume of 144 in.<sup>3</sup>. The order will be for 100 units. Class I castings, produced to meet MIL-A-21180. Both sand and investment castings are to be considered.

### Procedure

The following procedures are used to determine the bell crank costs for investment castings.

### Sand Casting:

 Utilize the Format Selection Aids for Castings, Machining of Castings, and Castings Test, Inspection and Evaluation (TI&E) to determine the formats needed. In this case, the required formats (included in this section on the pages shown) are:

2. Obtain the base casting cost by reading box volume of 144 in.3 on the MIL-A-21180 base casting cost line of Format CED-C-3 (Fig. 4.5-13): \$90.

- 3. From CED-DICE-C-2 (Fig. 4.5-14), read the DICE factor table for a Class I casting: 1.0 + 0.10 = 1.1 DICE factor.
- 4. To determine the lot quantity factor, read the effect of a buy quantity of 100 units on casting cost from Format CDE-C-II (Fig. 4.5-15): 0.93.
- 5. From Format CED-TI&E-C-1 (Fig. 4.5-16), read the TI&E cost for a box volume of 144 in.3: \$16.
- 6. Read the nonrecurring tooling cost for a box volume of 144 in<sup>3</sup> from Format CED-C-4 (Fig. 4.5-17): \$5,000.

  NOTE: Some companies have a policy to include a check fixture (ICF). Estimated cost is equal to 30 percent of the base tooling cost: \$5,000 x 0.30 = \$1,500.
- 7. Read hole drilling cost (man-hours) from CED-MC-1 (Fig. 4.5-18). Three 0.25-in. diameter holes at 0.018 man-hour/hole = 0.054 man-hour.
- 8. Read drill and ream hole cost (man-hours) from CED-MC-3 (Fig. 4.5-19): Two 0.25-in. diameter holes at 0.023 man-hour/hole = 0.046 man-hour.
- 9. From CED-MC-1 (Fig. 4.5-18), read that drill hole tooling cost (man-hours) is equal to a base of 32 man-hours plus two man-hours/hole: 32 + (3 x 2) = 38 man-hours.
- 10. From CED-MC-3 (Fig. 4.5-19), read that drill and ream tooling cost (man-hours) is equal to a base of 32 man-hours plus two man-hours/hole: 32 + (2 x 2) = 36 man-hours.
- 11. Determine recurring base casting cost, which is the sum of the base casting cost (\$90) times the DICE factor (1.10) and lot quantity factor (0.93), plus TI&E cost (\$16): \$90 x 1.10 x 0.93 = \$92 + \$16 = \$108.
- 12. Determine nonrecurring base casting cost, which is the sum of the foundry tooling costs (\$5,000) and the ICF (\$1,500): \$5,000 + \$1,500 = \$6,500.
- 13. Determine recurring machining costs, which are the sum of the drilling man-hours (0.054) and drill and ream man-hours (0.046), times the learning curve factor for a 90 percent learning curve (Table 4.5-1) (1.30), times an assumed hourly wraparound rate of \$50: (0.054 + 0.046) x 1.30 x \$50 = \$6.50.
- 14. Determine nonrecurring machining costs, which are the sum of drill tooling man-hours (38) and drill and ream tooling man-hours (36) times an assumed rate of \$50: (38 + 36) x \$50 = \$3,700.
- 15. Determine total recurring costs for 100 units, which are the sum of the base casting recurring costs (\$108) and machining recurring costs (\$6.50) times 100: \$108 + \$6.50 = \$114.50 x 100 = \$11,450.

- 16. Determine total nonrecurring costs, which are the sum of the base casting nonrecurring cost (\$6,500) and the machining nonrecurring costs (\$3,700): \$6,500 + \$3,700 = \$10,200.
- 17. Determine total cost for 100 units, which is the sum of the total recurring cost (\$11,450) and the total non-recurring cost(\$10,200): \$11,450 + \$10,200 = \$21,650.
- 18. Determine total average cost per unit, which equals the total cost(\$21,650) divided by the quantity (100): \$21,650/100 = \$217/unit.

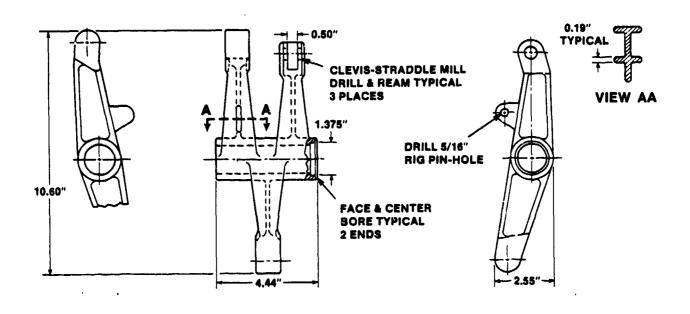
The results obtained show that the investment casting is less costly to produce than the sand casting (see following example) for the projected quantity of 100 units. The cost savings is \$31 per unit.

### Investment Casting:

- 1. Utilize the Format Selection Aids for Castings, Machining of Castings, and Castings Test, Inspection and Evaluation (TI&E) to determine formats needed.
- 2. Obtain the base casting cost by reading box volume of 144 in.<sup>3</sup> on the MIL-A-21180 base casting cost line of Format CED-C-1 (Figure 4.5-5): \$50.
- 3. From CED-DICE-C-1 (Fig. 4.5-6), read the DICE factors for a Class I casting (0.10) and poorly supported cores (0. 20): 1.0 + 0.10 + 0.20 = 1.30 DICE factor.
- 4. To determine the lot quantity factor, read the effect of a buy quantity of 100 units on casting cost from Format CDE-C-II (Figure 4.5-7): 0.93.
- 5. From Format CED-TI&E-C-1 (Fig. 4.5-8), read the TI&E cost for a box volume of 144 in.3: \$16.
- 6. Read the nonrecurring tooling cost for a box volume of 144 in. From Format CED-C-2 (Fig. 4.5-9): \$3,200.

  NOTE: Some companies have a policy to include a check fixture (ICF). Estimated cost is equal to 30 percent of the base tooling cost: \$3,200 x 0.30 = \$960.
- 7. Read drilling and spotfacing cost (man-hours) from CED-MC-2 (Fig. 4.5-10): Three 0.25-in. diameter holes @ 0.22 = 0.66 man-hour.
- 8. Read face milling cost (man-hours) for 3 in.<sup>2</sup> of milled area from CED-MC-5 (Fig. 4.5-11): 0.02 man-hour
- 9. Read clevis-straddle mill, drill, and ream cost (man-hours) from CED-MC-7 (Figure 4.5-12):
  - (a) 1.50 "A" dimension = 0.14 man-hour
  - (b) 0.74 "A" dimension = 2 @ 0.12 = 0.24 man-hour.

- 10. From CED-MC-2 (Fig. 4.5-10), read that drill and spot face tooling cost (man-hours) is equal to a base of 32 man-hours plus 2 man-hours for each three holes: 32 + (3 x 2) = 38 man-hours.
- 11. From CED-MC-5 (Fig. 4.5-11), read face milling tooling cost (man-hours): 57 man-hours.
- 12. From CED-MC-7 (Fig. 4.5-12), read that straddle mill, drill and ream tooling cost (man-hours) is equal to a base of 60 man-hours plus 15 man-hours for each of three clevises: 60 + (3 x 15) = 105 man-hours.
- 13. Determine recurring base casting cost, which is the sum of the base casting cost (\$50) factored by DICE (1.30) and lot quantity (0.93) plus the TI&E cost: \$50 x 1.30 x 0.93 = \$60.
- 14. Determine nonrecurring base casting cost, which is the sum of the foundry tooling cost (\$3,200) plus the ICF (\$960): \$3,200 + \$960 = \$4,160.
- 15. Determine recurring costs for machining casting, which are the sum of the man-hours for drilling and spotfacing (0.066); face milling (0.02); and clevis straddle milling, drilling, and reaming (0.38), times the learning curve factor for a 90 percent learning curve (Table 4.5-1) (1.30) times an assumed hourly wraparound rate of \$50: (0.066 + 0.02 + 0.38) x 1.30 x \$50 = \$30.
- 16. Determine nonrecurring machining costs, which are the sum of the man-hours for drill and spot-face tooling (38), mill tooling (57), and clevis straddle mill, drill, and ream tooling (105), times an assumed hourly wraparound rate of \$50: (38 + 57 + 105) x \$50 = \$10,000.
- 17. Determine total recurring costs for 100 units, which are the sum of the recurring costs for the base casting (\$76) and the machining recurring costs (\$30), times 100: \$76 + \$30 = \$106 x 100 = \$10,600.
- 18. Determine total nonrecurring costs, which are the sum of the base casting nonrecurring cost (\$4,160) and the machining nonrecurring cost (\$10,000): \$4,160 + \$10,000 = \$14,160.
- 19. Determine the total cost for 100 units, which is equal to the sum of the total recurring costs (\$10,600) and the total nonrecurring costs (\$14,160): \$10,600 + \$14,160 = \$24,760.
- 20. Determine total average cost per unit, which equals the total cost (\$24,760) divided by the quantity (100): \$24,760/100 = \$248/unit.



### BELLCRANK 365 T6 SAND CAST QQ-A-601

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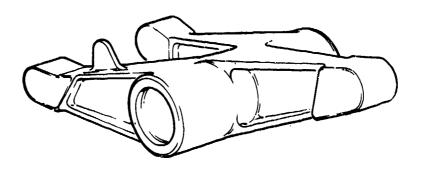
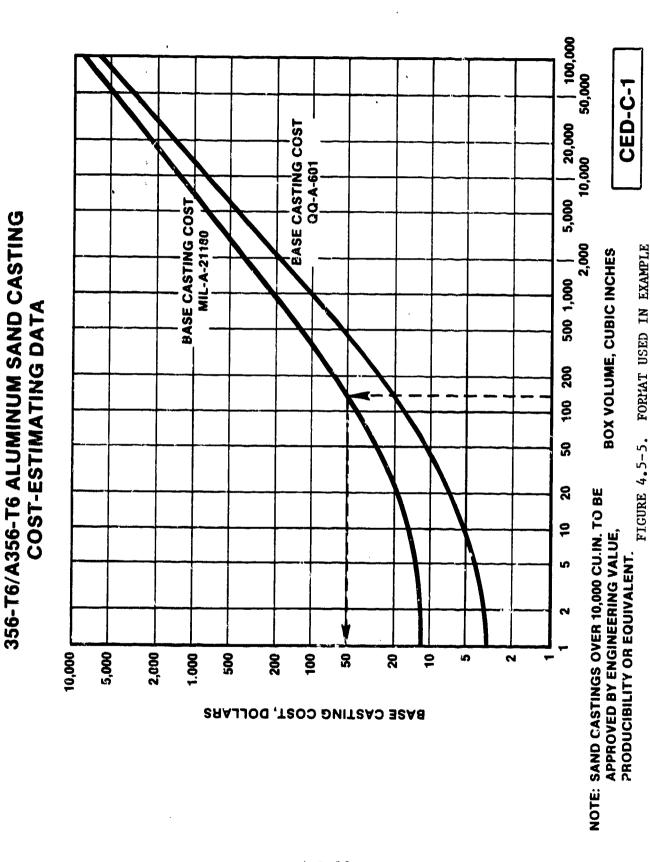


FIGURE 4.5-4. CAST PART ANALYZED



### DICE FACTOR FOR ALUMINUM SAND CASTINGS COST ESTIMATING DATA

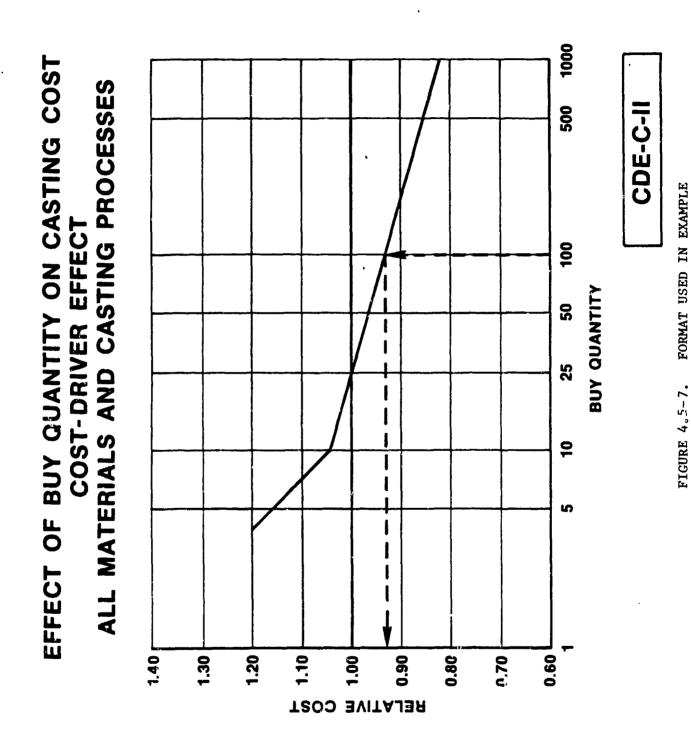
NOTE: DICE FACTOR EQUAL TO ONE PLUS SUM OF ALL APPLICABLE DICE FACTOR INCREMENTS IN TABLE. RESULTING DICE FACTOR USED TO MODIFY BASE CASTING COST.

DESIGN FEATURE	DICE FACTOR INCREMENT
CASTING CLASSIFICATION	
Cless 11	_
Class I	0.10
X-RAY GRADE	
j 0	_
D with C Areas	
C	0.05
C with B Areas	0.20 0.50
TOLENANCE - LENGTH/WIDTH	4.00
±0.003"/in. ±0.03" min	
±0.0025"/in. ±0.025" min	0.10
±0.002"/in. ±0.02" min	0.20
TOLERANCES - THICKNESS	
±0.03"	
±0.025"	0.10
±0.02"	0.20
SURFACE FINISH	
C50	
C25	
C20	0.15
FILLET RADII	
R = Wall Thickness	
R = 1/2 Wall Thickness	0.10
LOCAL THICK AREAS Under 0.25"	
0.25" to 0.50"	
0.50" (ο 1.0"	0.05
1.0" to 2.0"	0.20
Over 3.0"	0.30
THROUGH HOLES	
None Length/Diam. < 4	0.10
Length/Diam. 4-8**	0.25
BUIND HOUSE	
BLIND HOLES None	
Length/Diam. < 4	0.45
Length/Diam. 4-8**	0.60
NUMBER OF CORES	
1-3	0.10
4-7	0.30
8-11	0.50
12 UP	0.80
CORES	
Weil Supported	
Poorly Supported	0.20
SLENDERNESS RATIO (L/W OR T)	
L/W or L/T < 6	<del>-</del>
1./W or L/T 6-12 L/W or L/T > 12	0.10 0.25
5.4.0.0.7.7.15	V.43

<sup>\*\*</sup>Consult Value or Producibility for L/D Ratios Over 8

FIGURE 4.5-6. FORMAT USED IN EXAMPLE

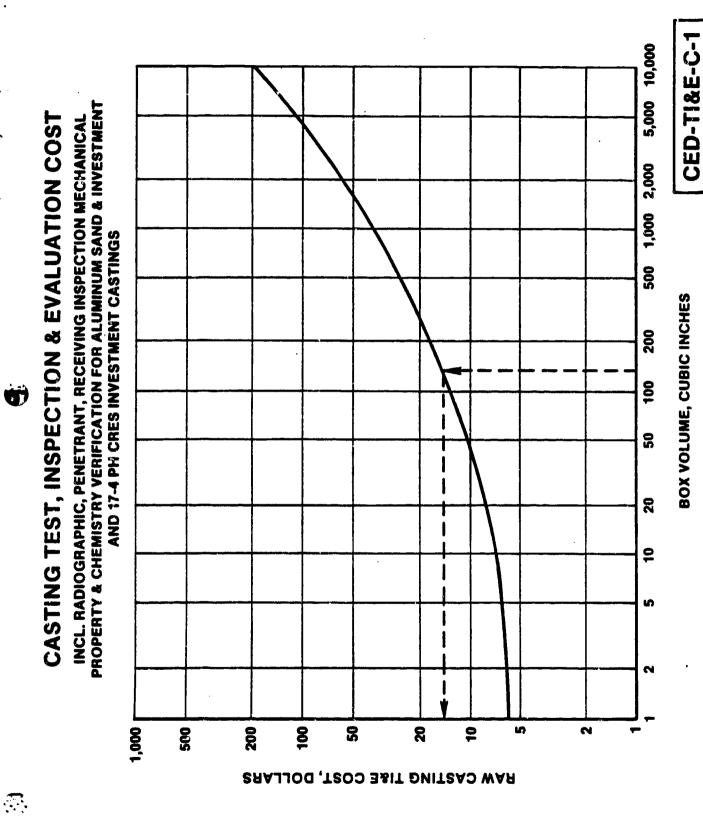
CED-DICE-C-1



4.5-12

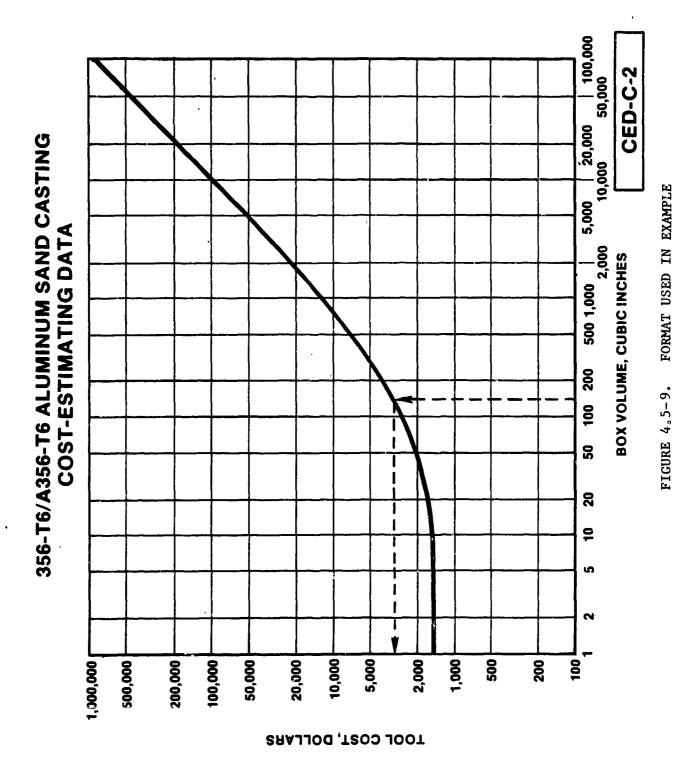
FORMAT USED IN EXAMPLE

FIGURE 4.5-8.



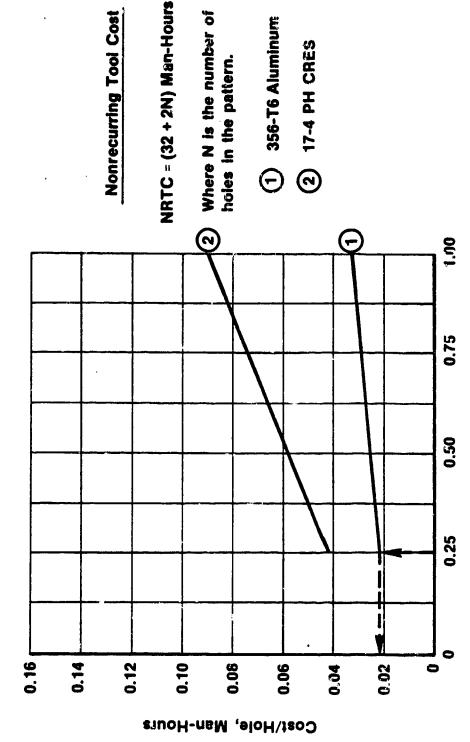
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7.7.4



4.5-14





L<sup>e</sup>

Hole Diameter, Inches

Cost/Part = (Cost/Hole • N) Man-Hours

CED-MC-2

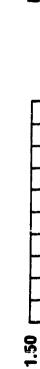
Cost data is vaild for hole depths up to twice the hole diameter.

FIGURE 4.5-10.

FORMAT USED IN EXAMPLE

## MACHINING OF CASTINGS FACE MILLING







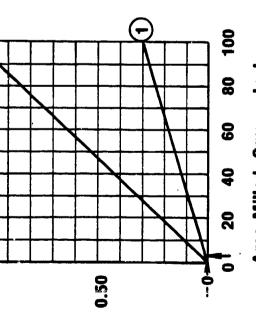
- (1)356/A 356-T6 Aluminum
- (2) 17-4PH CRES

8.

Step 1 — Determine the face milling cost for each surface machined.

Step 2 — Add the milling costs obtained in Step 1.

Step 3 — Obtain NRTC above.



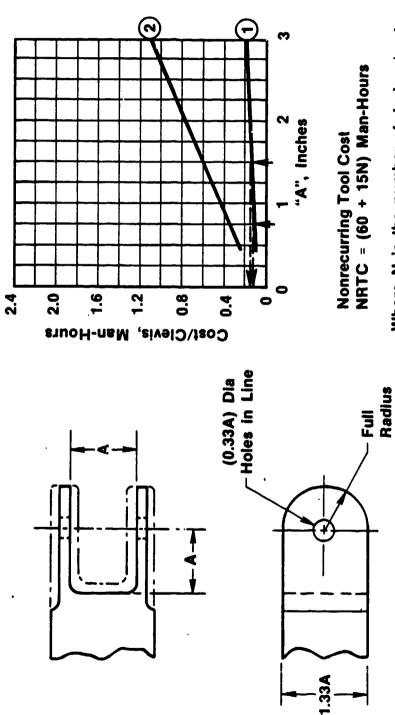
Area Milled, Square Inches

CED-MC-5

FIGURE 4.5-11. FORMAT USED IN EXAMPLE

## STRADDLE MILL, DRILL & REAM **MACHINING OF CASTINGS**

Company of the Compan



Where N is the number of clevises/part.

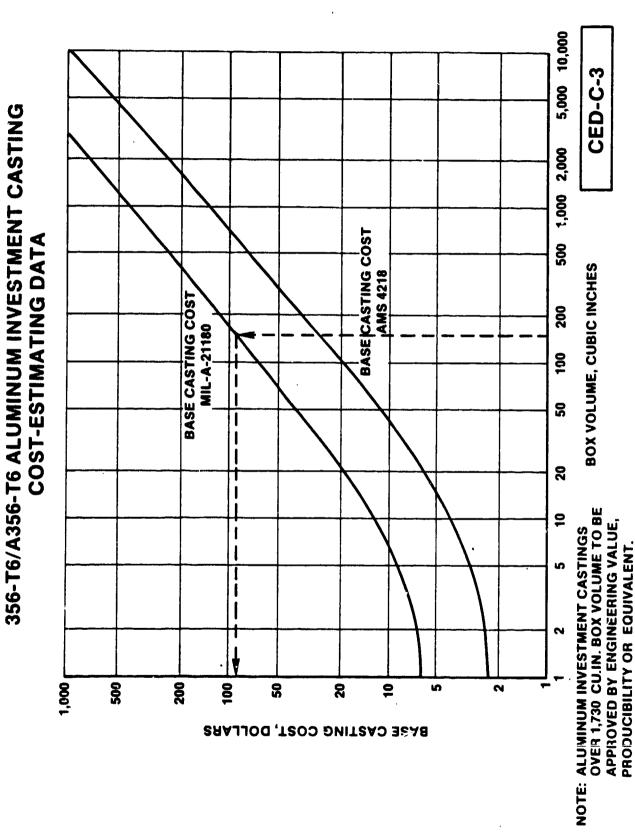
(1) 356-T6 Aluminum

(2) 17-4PH CRES

CED-MC-7

FIGURE 4.5-12. FORMAT USED IN EXAMPLE

FIGURE 4.5-13. FORMAT USED IN EXAMPLE



4.5-18

### DICE FACTORS FOR ALUMINUM INVESTMENT CASTINGS COST ESTIMATING DATA

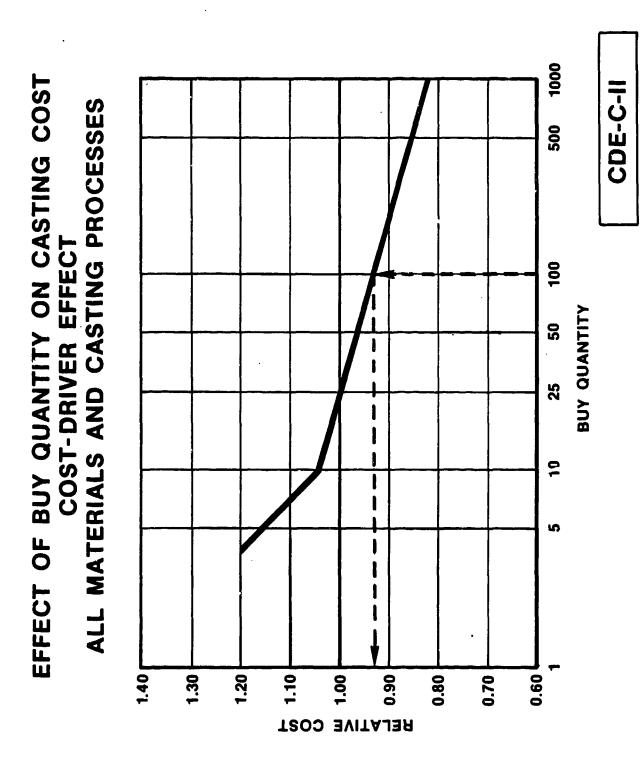
NOTE: DICE FACTOR EQUAL TO ONE PLUS SUM OF ALL APPLICABLE DICE FACTOR INCREMENTS IN TABLE. RESULTING DICE FACTOR USED TO MODIFY BASE CASTING COST.

DESIGN FEATURE	DICE FACTOR INCREMENT
CASTING CLASSIFICATION Class II Class I	0.10
X-RAY GRADE D D with C Areas	
C C with B Areas	0.10
TOLERANCE — LENGTH/WIDTH ±0.005"/in. ±0.010" min	0.50
±0.004"/in. ±0.010" min ±0.003"/in. ±0.010" min	0.20 0.50
TOLERANCE-THICKNESS ±0.010 ±0.004 ±0.005	0.10 0.20
SURFACE FINISH C12	_
C9 C6 FILLET RADII	Machine Machine
R = Wall Thickness R = 1/2 Wall Thickness	0.05
LOCAL THICK AREAS Under 0.25" Thick 0.25" to 0.50" 0.50" to 1.0" 1.0" to 2.0" Over 2.0"	0.10 0.25 0.50 1.00
THROUGH HOLES None Length/Dia. < 4 Length/Dia 4-8**	0.10 0.20
BLIND HOLES  None  Length/Dia. < 4  Length/Dis 4-8**	0.20 0.40
CORES (SOLUBLE WAX) None 1-2 Cores 3-6 Cores	0.10 0.30
SLENDERNESS (RATIO L/W OR T)  L/W or L/T < 6  L/W or L/T 6-12  L/W or L/T > 12	U.10 0.25

<sup>\*\*</sup>Consult Value or Producibility Engineer

FIGURE 4.5-14. FORMAT USED IN EXAMPLE

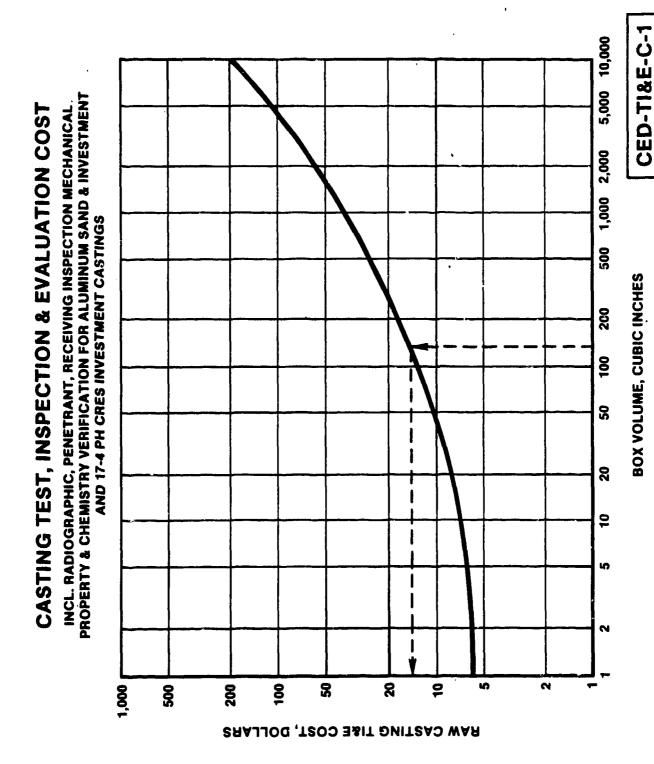
CED-DICE-C-2



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FIGURE 4.5-15. FORMAT USED IN EXAMPLE

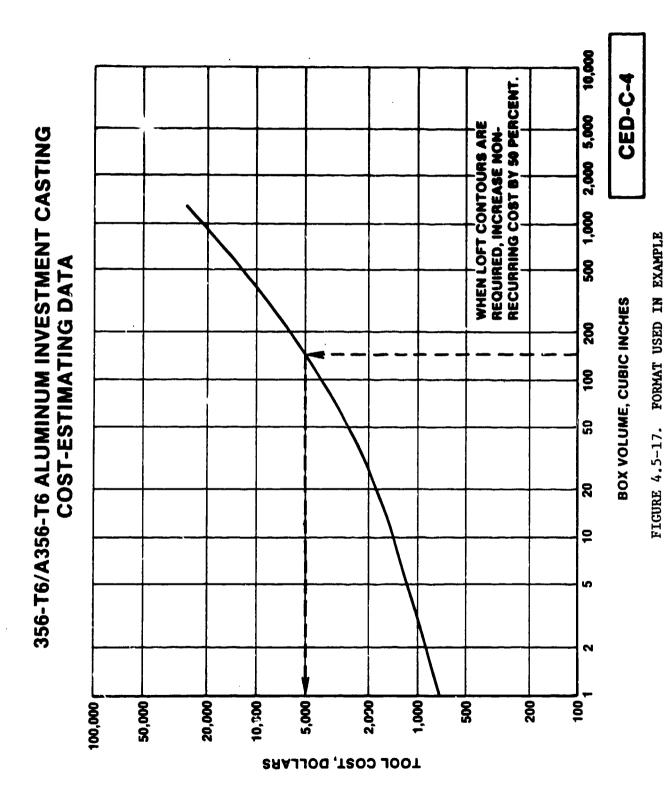
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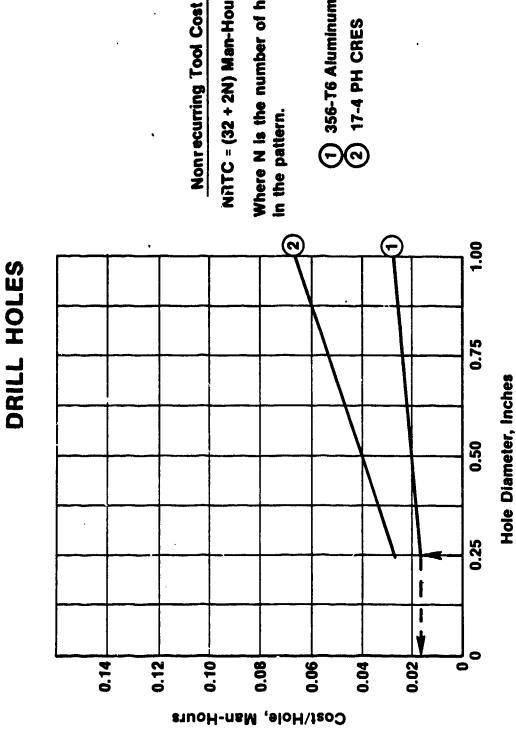
FIGURE 4.5-16. FORMAT USED IN EXAMPLE



4.5-22

# MACHINING OF CASTINGS

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Where N is the number of holes NRTC = (32 + 2N) Man-Hours (1) 356-T6 Aluminum (2) 17-4 PH CRES in the pattern.

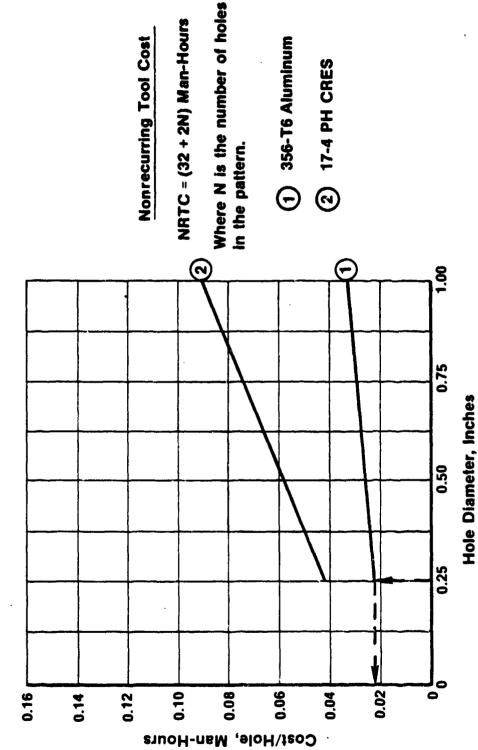
CED-MC-1

Cost data is valid for hole depths up to twice the hole diameter. Cost/Part = (Cost/Hole • N) Man-Hours

FIGURE 4.5-18. FORMAT USED IN EXAMPLE

## MACHINING OF CASTINGS DRILL AND REAM HOLES

AND THE TAXABLE PARTIES TO THE TREET OF THE TAXABLE PARTIES TO THE TREET OF THE TAXABLE PARTIES TO THE TAXABLE PARTIES.



1 356-T6 Aluminum

**17-4 PH CRES** 

CED-MC-3

Cost/Part = (Cost/Hole • N) Man-Hours

Cost data is valid for hole depths up to twice the hole diameter.

FIGURE 4.5-19. FORMAT USED IN EXAMPLE

TABLE 4.5-1

### FACTORS TO CONVERT THE MC/DG 200TH UNIT COST TO THE CUMULATIVE AVERAGE COST FOR THE DESIGN QUANTITY AND LEARNING CURVE INVOLVED

DESIGN	LEARNING			ING CL	CURVE-%		
QUANTITY	95	90	85	80	75	70	65
1	1.48	2.25	3.48	5.50	9.00	15.00	27.00
10	1.33	1.79	2.47	3.48	5.04	7.53	11.67
25.	1.25	1.59	2.05	2.71	3.68	5.13	7.43
50	1.19	1.44	1.79	2.22	2.85	3.76	5.14
100	1.13	1.30	1.52	1.80	2.18	2.73	3.51
200	1.08	1.17	1.30	1.45	1.66	1.95	2.36
350	1.04	1.08	1.14	1.22	1.33	1.48	1.70
500	1.01	1.02	1.05	1.09	1.15	1.24	1.38
750	0.98	0.96	9.96	0.96	0.97	1.01	1.09
1000	0.96	0.92	0.89	0.87	0.87	0.88	0.91

### TABLE 4.5-2 CASTING COST WORKSHEET

PREPARED BY:			DATE:		
DART TITLE			DESIGN QUANTITY		
PART TITLE		LOT QUANTITY			
MATERIAL	SPECIFICATION		FOUNDRY PROCESS		
Aluminum 356	QQ-A-601				
A356	MIL-A-21180		Sand		
Steel	AMS 4218		Investment		
17-4 PH	AMS 5355				
BOX VOLUME = W x L x T	Ţ				
ITEM					
RECURRING COST					
a) Base Cast Cost	(Ref	)	3		
b) DICE Factor	(Ref	)	·		
c) Lot Quantity Factor	(Ref	}			
d) Test Insp. & Eval. Cost	(Ref	)	8		
e) Inflation Factor					
f) Recurring Cost (a x b x c	t d)e		\$		
NONRECURRING COST g) Base Nonrecurring Cost	(Ref	)	8		
h) NR DICE Factor	(Ref	•			
I) Check Fixtures	(Ref		S		
j) Stalic Test Cost	(Rei	•	8		
e) Inflation Factor	•				
k) Nonrecurring Cost = (g x l	1 + i + j)e		8		
COST SUMMARY					
f) Recurring Cost/Part			\$		
I) Machining Cost/Part			\$		
m) Design Quantity					
n) Program Recurring Cost (	(f + 1)m		<u>\$</u>		
k) Nonrecurring Cost			5		
o) Program Total Cost (n + i	()		<u> </u>		
p) Total Cost/Part (a ÷ m)			\$		

### TABLE 4.5-3

### **CASTING MACHINING COST WORKSHEET**

MACHINING FEATURE	FORMAT	RECURRING COST	NONRECURRING COST
Holes - No Size			
Drill		[.	
Drill & Spotface			
Drill & Ream			
Cost Per Part		МН	мн
Flange Facing			
Mean Diam Width		•	•
Cost Per Part		МН	MH
Face Milling			
Area Milled Sq. In.			
Cost Per Part		мн	мн
Face & Counterbore Hub			
Ctrbore Diam No			]
Cost Per Part		МН	мн
Clevis-Str. Mill/Drill/Ream			
No Size			
Cost Per Part		MH	МН
Machining Cost (Unit 200) Per Part		Мн	мн
Learning Curve Factor			
Labor Rate		\$ /HR	S /HR
Machining Cost/Part*		\$	
Nonrecurring Cost			

<sup>\*</sup>Machining cost/part = U200 cost/part x LC factor x labor rate.

Des. Qty	LC Factor	Des. Qty	LC Factor	
1	2.25	200	1.17	
10	1.79	350	1.08	
25	1.59	500	1.02	
50	1.44	750	0.96	
100	1.30	1000	0.92	

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90% Learning Curve Factor to Convert Unit 200 Format Cost to Cumulative Average Cost for Various Design Quantity.

### 4.5.3 Cast Parts Analyzed

Examples of cast parts analyzed to determine the manufacturing manhours are shown in Figure 4.5-4. Designer-influenced cost elements (DICE) for castings can significantly increase manufacturing cost and therefore examples of DICE are shown in Figures 4.5-5 and 4.5-6.

It was considered convenient to classify castings into the groupings shown in Figure 4.5-4, i.e., simple, average and complex. These classifications are defined below:

### Simple Castings

### Type "A"

All tolerances, thicknesses, X-ray grade, cast surface finish > than recommended. Simple shapes, uniform sections, no coring required.

### Type "B"

May require one or two dimensions held tighter than recommended, or small local grade "B" X-ray requirements, or small local thin wall at one place. Regular shape casting with moderate wall thickness changes.

### Average Castings

### Type "C"

This casting may require separate cores, plus three or four dimensions are required tighter than recommended. Multi-piece or split mold. Several pockets or protrusions. Less than three cored holes.

### Type "D"

Requires approximately three complex cores or some soluble coring. Varying wall thicknesses. Several thin or thick webs. Small local surface requiring C-12 or C-6 cast surface finish. Local grade "B" X-ray requirements.

### Complex Castings

### Type "E"

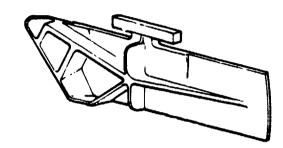
Several complex cores required with marginal L/D ratios. Thin and heavy sections up to seven or eight dimensions that require tolerancing tighter than standard. Up to 15 percent of casting requires grade "B" X-ray level.

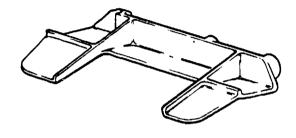
### Type "F"

25 percent of casting surface requires grade "B" X-ray level. One or more surfaces require C-12 or C-6 cast surface roughness. Multi-piece large tooling elements. Many thin or heavy webs. Many tight tolerances on location and thickness dimensions. Complex soluble coring required. Welded core support (chaplets) plugs required.

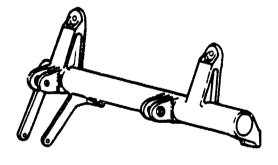
### SAMPLE PARTS USED TO DERIVE CASTING COST DATA FOR MC/DG

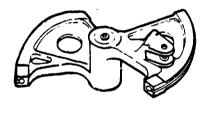
### SIMPLE CASTINGS





### AVERAGE COMPLEXITY CASTINGS





HIGH COMPLEXITY CASTING

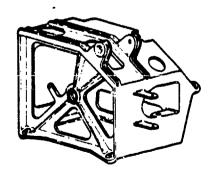
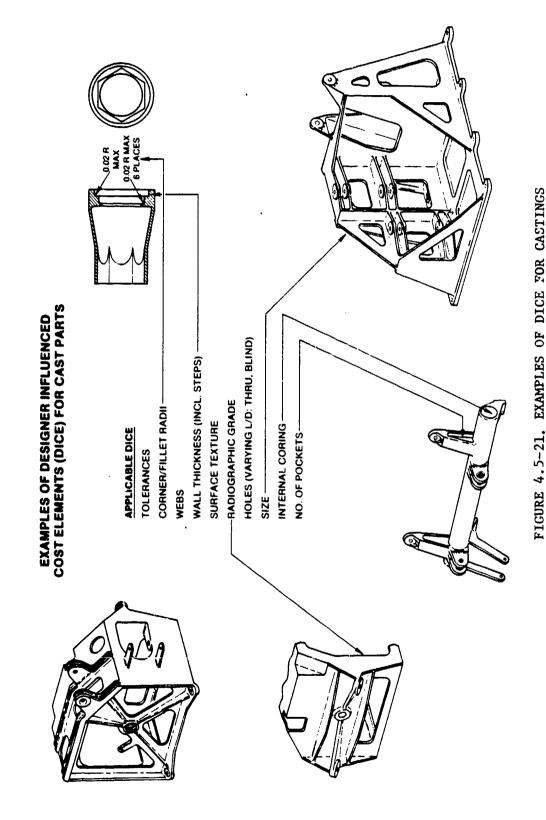


FIGURE 4.5-20



4.5-30

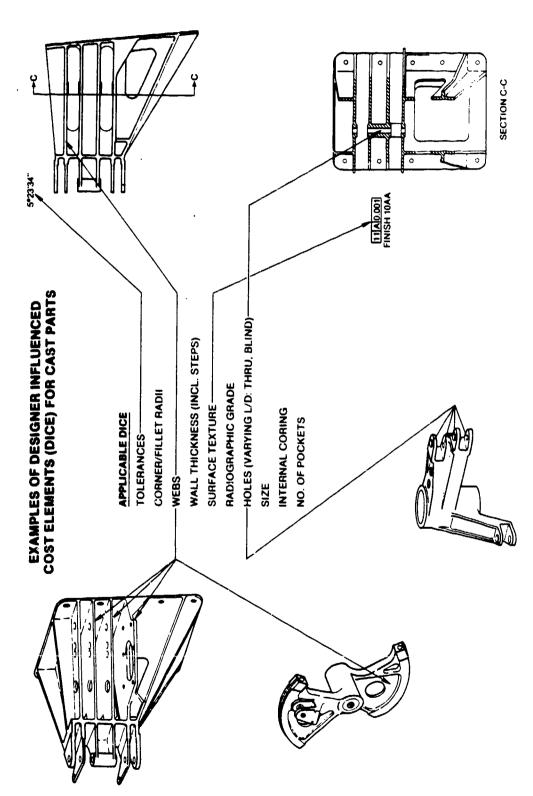
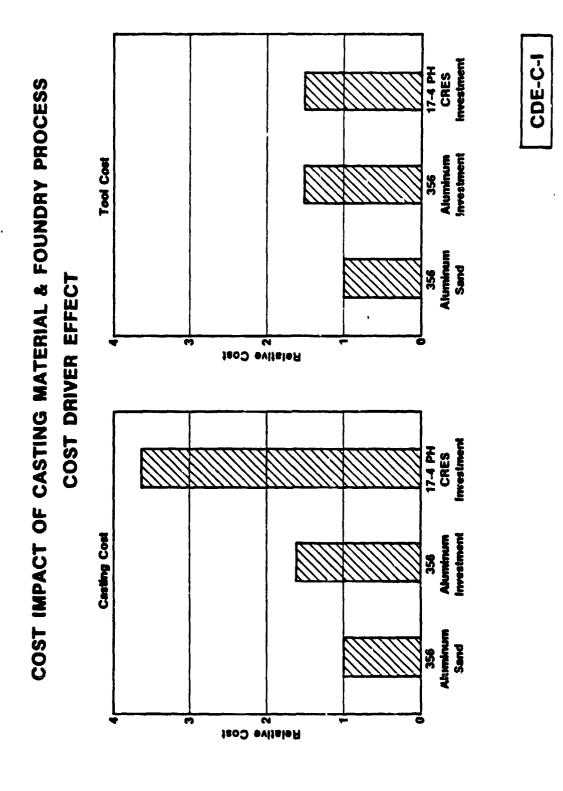


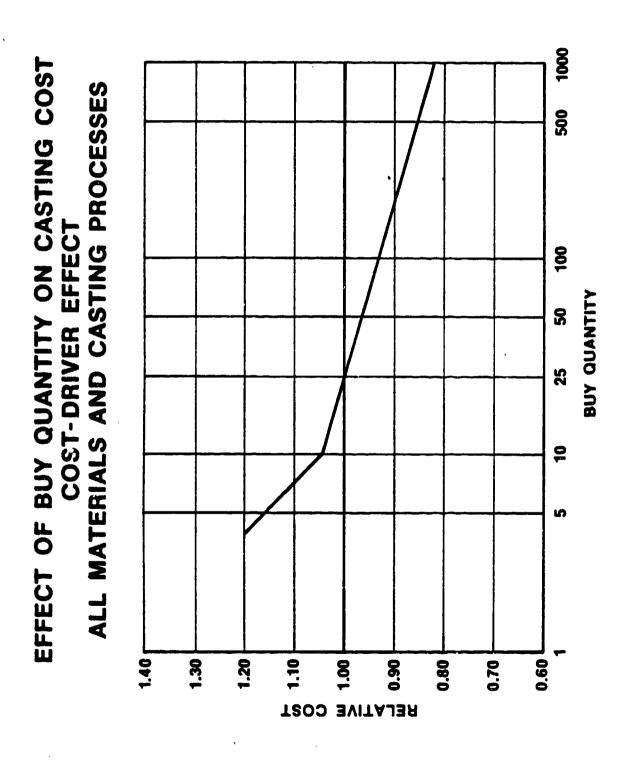
FIGURE 4.5-22. EXAMPLES OF DICE FOR CASTINGS

### 4.5.4 Data for Castings

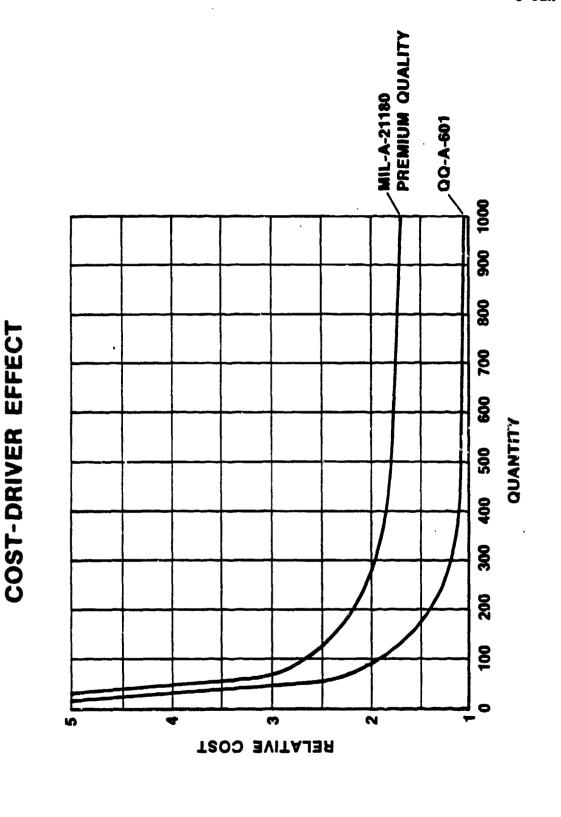
The data on the following pages provide designer guidance to lowest cost and also enable cost trade-off studies to be conducted in accordance with the formats shown on the selection aids (Figures 4.5-1 to 4.5-3). As castings require additional operations prior to assembly in an air-frame or other applications, formats to include the cost of machining are also included in this section (Formats CDE-MC-1, CDE-MC-II, and CED-MC-1 to CED-MC-6).



CDE-C-II



CDE-C-III



THE PARTY OF THE PROPERTY OF T

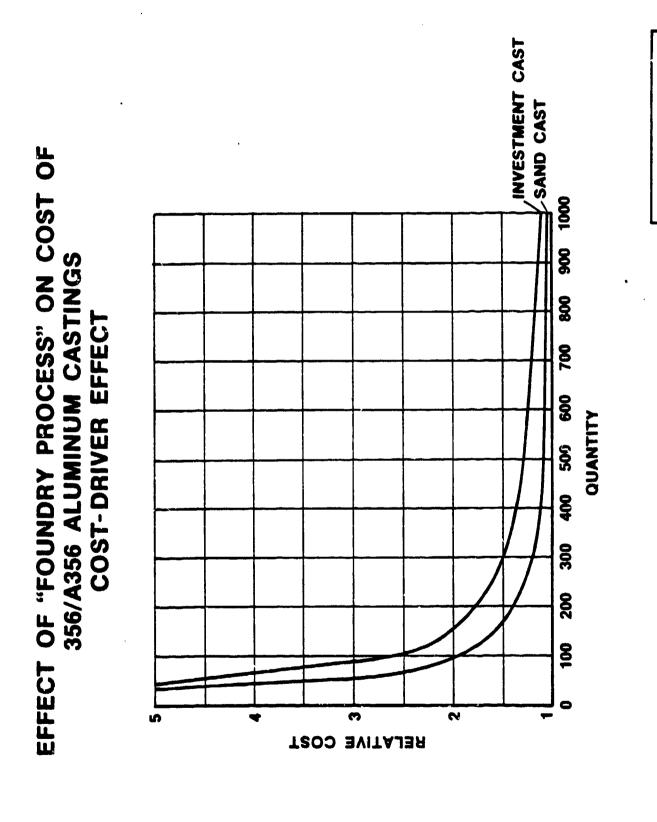
T

EFFECT OF "SPECIFICATION SELECTION" ON COST OF

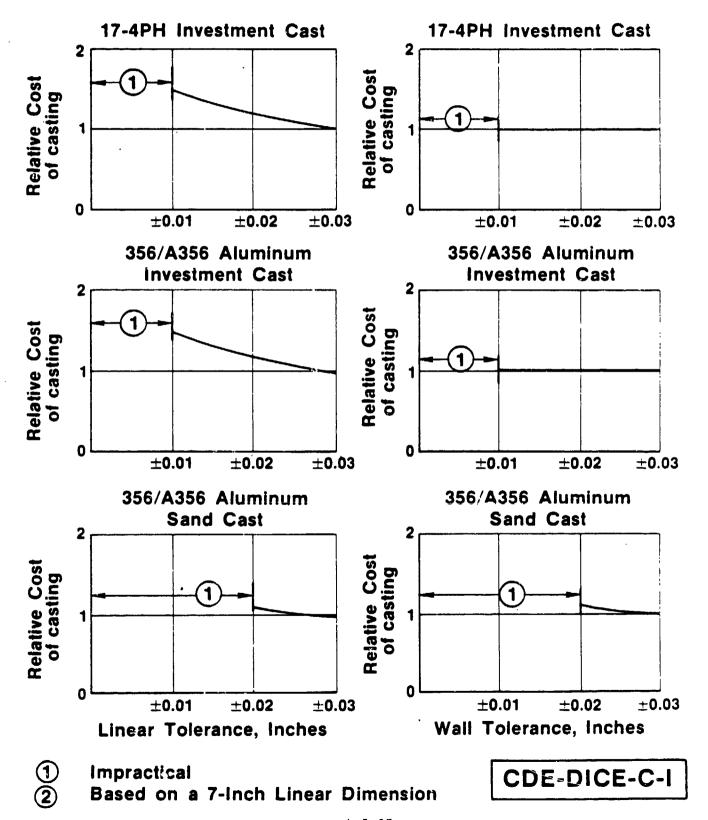
356/A356 ALUMINUM SAND CASTINGS

CDE-C-IV

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### CASTING TOLERANCES COST-DRIVER EFFECT



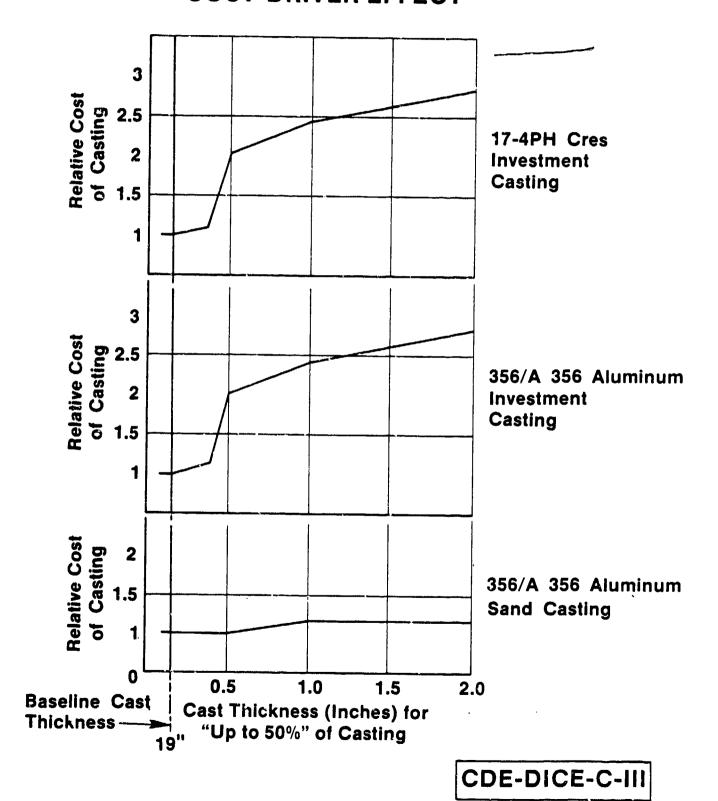
### X-RAY GRADE REQUIREMENT COST DRIVER EFFECT

CASTING MATERIAL & PROCESS	X—RAY GRADE	COST EFFECT
356/A356	D OR C	BASE
ALUMINUM	D OR C WITH 10% B	+15%
SAND CAST	D OR C WITH 50% B	+25%
·	8	+50%
356/A356	D OR C	BASE
ALUMINUM	D OR C WITH 10% B	+10%
INVESTMENT	D OR C WITH 50% B	+20%
CAST	В	+50%
	5.05.0	DAGE
17-4PH CRES	D OR C	BASE
INVESTMENT	D GR C WITH 10% B	+20%
CAST	D OR C WITH 50% B	+30%
	В	+60%

NOTE: X-Ray Grade A is an Impractical Requirement for General or Local Areas of Casting.

CDE-DICE-C-II

### COST IMPACT OF CHANGE IN CAST THICKNESS COST-DRIVER EFFECT



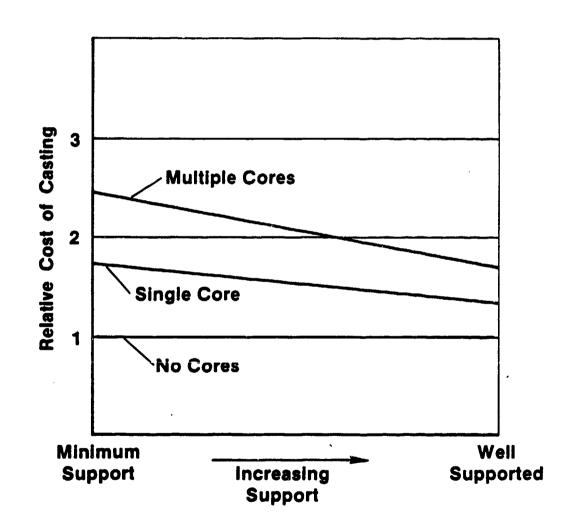
### CAST SURFACE FINISH COST-DRIVER EFFECT

Casting	Surface	•	Cost	Effort		
Cast Surface	Equivalent Machine	356/A356 Aluminum Sand Casting		356/A356 Aluminum & 17-4 Cres Invest- ment Casting		
Finish Designation			% of Surface		% of Surface	
		10%	50%	10%	50%	
C-25	250	Base	Base	Base	Base	
C-20	200	+10%	+20%	<b>1</b>	<b>A</b>	
C-15	150	+10%	1			
C-12	125	+10%	1	Base	Base	
C-9	90	1	1	1	1	
C-6	63	1	1	1	1	

1 Impractical

CDE-DICE-C-IV

### IMPACT OF CORES AND DEGREE OF CORE SUPPORT ON COST OF ALUMINUM SAND CASTINGS COST-DRIVER EFFECT



CDE-DICE-C-V

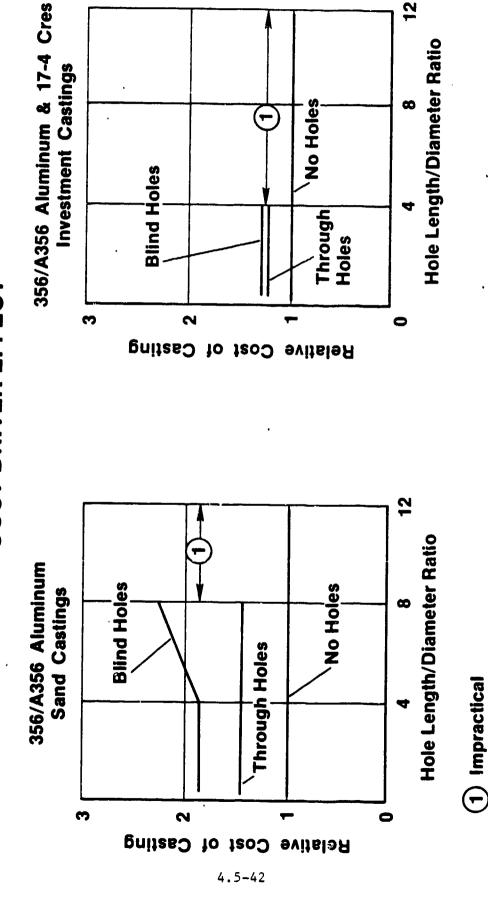
12

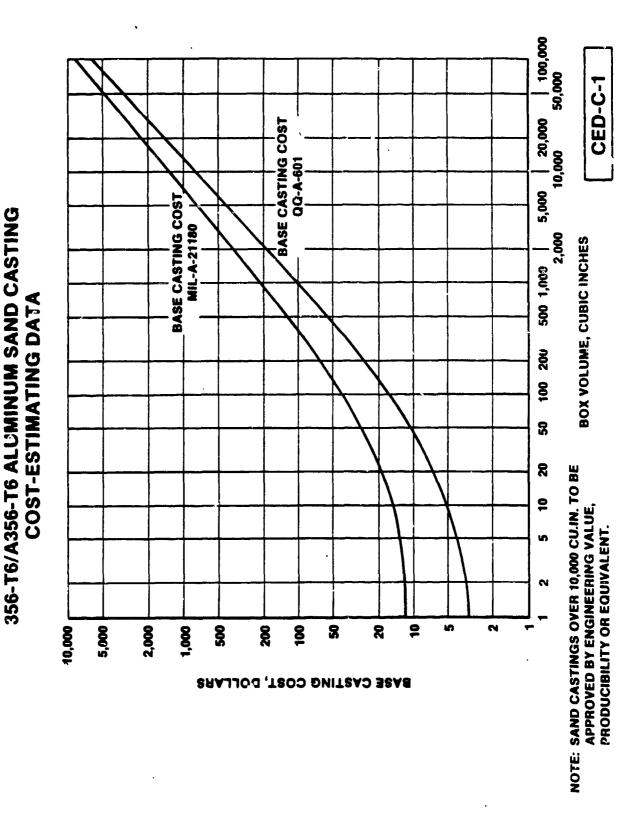
### CDE-DICE-C-VI

.

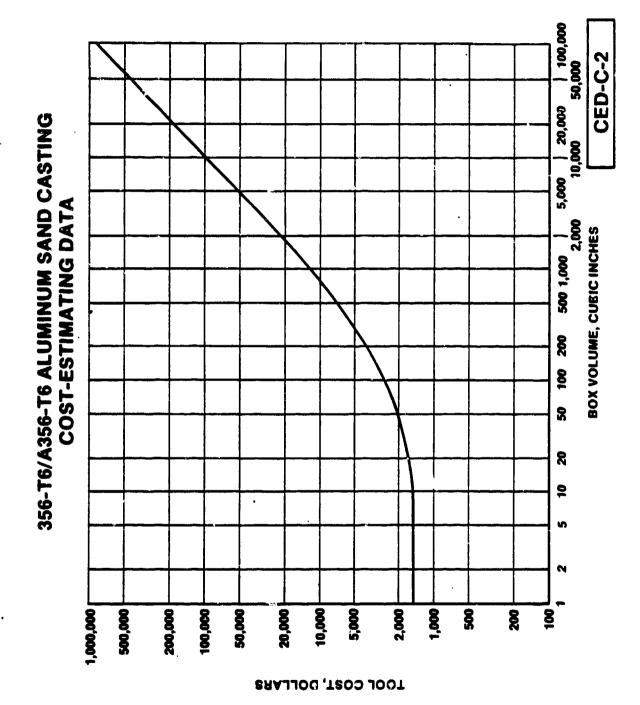
## EFFECT OF THROUGH & BLIND HOLES ON THE COST OF CASTINGS

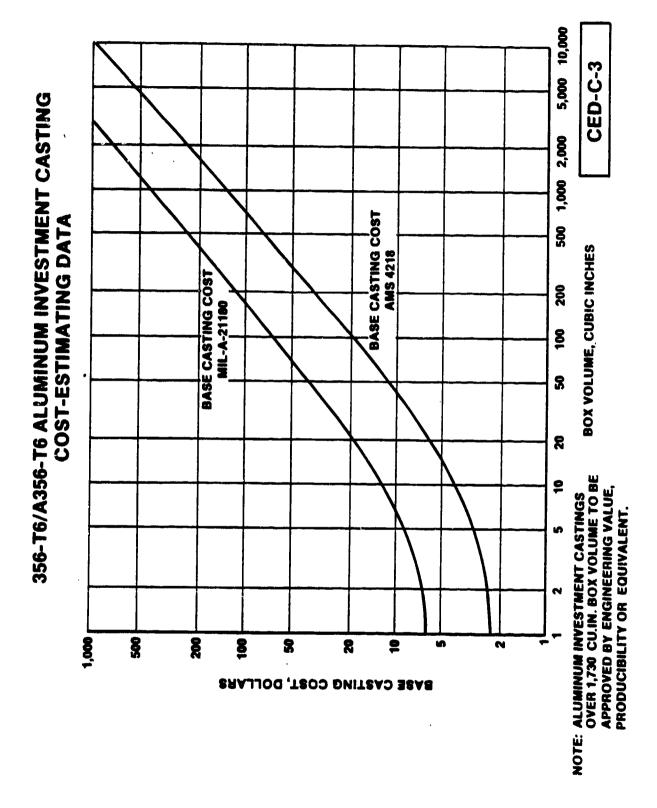
## **COST-DRIVER EFFECT**





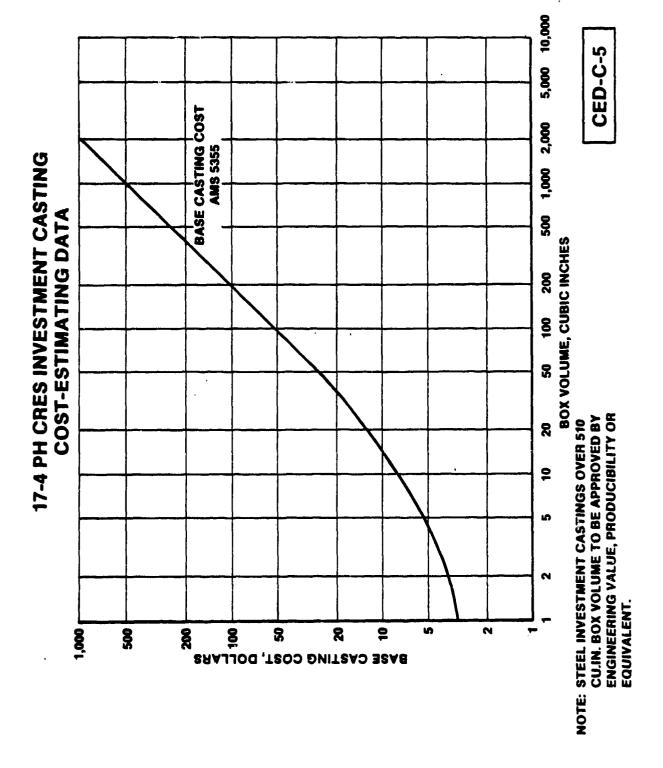
,然后,他们就是一个时间,他们就是一个时间,他们们就是一个时间,他们们们的一个时间,他们们们的一个时间,他们们们们们们们的一个时间,他们们们们们们们们们们们们们





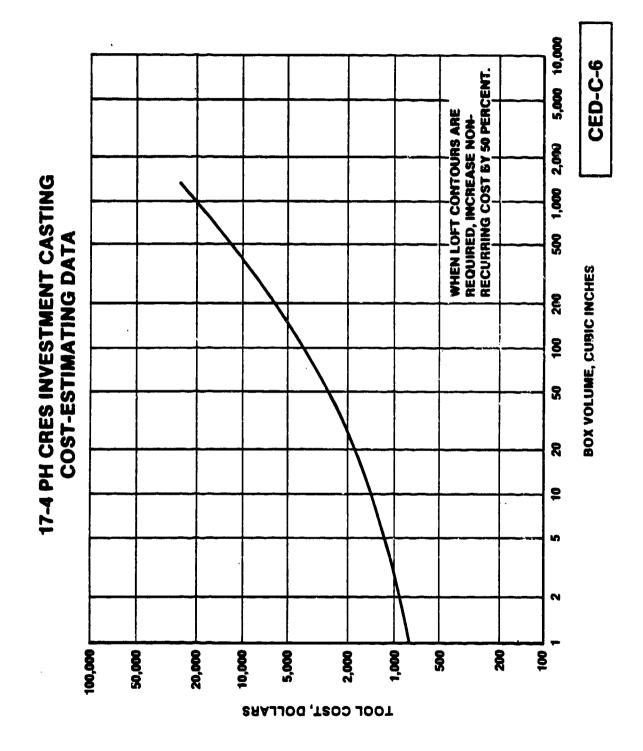
......

10,000 CED-C-4 WHEN LOFT CONTOURS ARE REQUIRED, INCREASE NON-RECURRING COST BY 50 PERCENT. 2,000 5,000 356-T6/A356-T6 ALUMINUM INVESTMENT CASTING 1,000 200 **COST-ESTIMATING DATA BOX VOLUME, CUBIC INCHES** 8 5 S ೩ 2 ~ 2 50,000 20,000 10,000 2,000 1,000 8 200 5,000 100,000 TOOL COST, DOLLARS



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### DICE FACTOR FOR ALUMINUM SAND CASTINGS COST ESTIMATING DATA

NOTE: DICE FACTOR EQUAL TO ONE PLUS SUM OF ALL APPLICABLE DICE FACTOR INCREMENTS IN TABLE. RESULTING DICE FACTOR USED TO MODIFY BASE CASTING COST.

	E FACTOR CREMENT
GASTING CLASSIFICATION	
Class II	
Class I	0.10
X-RAY GRADE	
D with C Areas	=
c	0.06
C with B Areas	0.20
•	0.50
TOLERANCE - LENGTH/WIDTH	
±0.003"/in. ±0.03" min ±0.0025"/in. ±0.025" min	0.10
±0.002"/in. ±0.02" min	0.20
TOLERANCES - THICKNESS	
z0.03"	
±0.036"	6.10
±9.02"	0.20
SURFACE FINISH	_
Cas	
C20	0.18
FILLET RADII	
R = Well Thiskness	
R = 1/2 Well Thinkness	0.10
LOCAL THICK AREAS	
0.26" to 0.00"	-
8.80" to 1.0" 1.0" to 3.0"	0.06 0.20
Over 2.9"	0.30
THROUGH HOLES	
None	
Longth/Diam. < 4 Longth/Diam. 4-2**	0.10 0.25
SLIND HOLES	
Langth/Diem. < 4	0.46
Longit/Diam. 4-8**	0.80
NUMBER OF CORES	
1-3	0.10
9-11	0.30 0.60
12 UP	0.00
CORES	
Well Supported	
Peorly Supported	0.20
SLENDERNESS RATIO (L/W OR 1)	
L/W or L/T < 6 L/W or L/T 6-12	0.10
L/W er L/T > 12	0.25

CED-DICE-C-1

<sup>\*\*</sup>Genouit Value or Producibility for L/D Ratios Over 8

### DICE FACTORS FOR ALUMINUM INVESTMENT CASTINGS COST ESTIMATING DATA

NOTE: DICE FACTOR EQUAL TO ONE PLUS SUM OF ALL APPLICABLE DICE FACTOR INCREMENTS IN TABLE, RESULTING DICE FACTOR USED TO MODIFY BASE CASTING COST.

DESIGN FEATURE	DICE FACTOR INCREMENT
CASTING CLASSIFICATION	
Ciesa II	
Cleas t	0.10
X-RAY GRADE	
0	_
D with C Areas	-
C with 8 Areas	0,10
•	0.50
TOLERANCE - LENGTH/WIDTH	
±9.006"/hı. ±0.010" min	_
±9.004"/in. ±0.010" min	0.20
±9.903"/in. ±9.010" min	0.50
TOLERANCE-THICKNESS	_
±0.010 ±0.000	0.10
±9.006	0.20
SURFACE FINISH	
C12	-
Ç0	Machine
C4	Machine
PILLET RADII	
R = Wall Thickness	_
R = 1/2 Well Thickness	0.06
LOCAL THICK AREAS Under 8.25" Thick	
0.25" to 0.50"	0.10
9.50° to 1.0° 1.0° to 2.0°	0.25 0.60
Over 8.0"	1.00
THROUGH HOLES	
None	-
Longth/Dia. < 4	0,10
Length/Dia 4-8**	0.20
BLIND HOLES	
None	
Length/Die. < 4 Length/Die 4-8**	0.20 0.40
CORES (SOLUBLE WAX)	
None 1-2 Gares	0.10
3-6 Cores	0.30
SLENDERNESS (RATIO L/W OR T)	_
L/W or L/T 6-12	0.10
L/W or L/T > 12	0.25

<sup>&</sup>quot;Consult Value or Producibility Engineer

CED-DICE-C-2

### DICE FACTOR FOR 17-PH CRES INVESTMENT CASTINGS COST ESTIMATING DATA

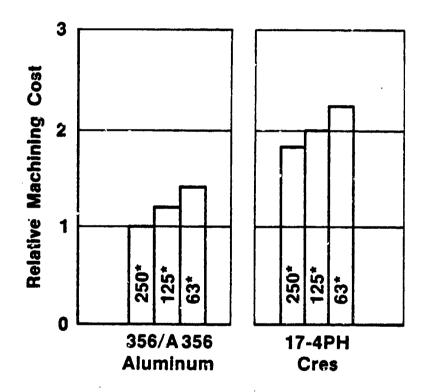
NOTE: DICE FACTOR EQUAL TO ONE PLUS SUM OF ALL APPLICABLE DICE FACTOR INCREMENTS IN TABLE. RESULTING DICE FACTOR USED TO MODIFY BASE CASTING COST.

DESIGN FEATURE	DICE FACTOR INCREMENT
CASTING CLASSIFICATION	
Cless II	_
Class ?	0.10
X-RAY GRADE	
<b>C</b>	_
D with C Areas	
C WITH B Areas	0.10
9	0.50
TOLERANCE - LENGTH/WIDTH	
±0.005"/in. ±0.010" min	
±0.004"/in. ±0.010" m/m	0.20
±0.003"/in. ±0.010" min	0.50
TOLERANCE-THICKNESS	
±0.010	
:±0.036	0.10
±0.005	0.20
SURFACE FINISH	
C13	
C9 C9	Machine
<del></del>	Machine
FILLET RADII	
R = Wall Thickness	
R = 1/2 Wall Thickness	0.05
LOCAL THICK AREAS Under 0.25" Thick	
0.25" to 0.50"	0.16
0.50" to 1.0"	0.25
1.0" to 2.0"	0.50
Over 2.0"	1.00
THROUGH HOLES	
Length/Dis. < 4	0.10
Length/Dia 4-8**	0.29
BLIND HOLES	
Nene .	
Length/Die. < 4	0.20
Length/blo 4-8**	9.40
CORES (SOLUBLE WAX)	
None	_
1-2 Cores	0.10
3-6 Cores	0.30
SLENDERNESS (RATIO L/W OR T)	
L/W or L/T < 6	_
L/W or 1/T 6-12	0.10
L/W or L/T > 12	0.25

<sup>\*\*</sup>Consult Value or Producibility Engineer

CED-DICE-C-3

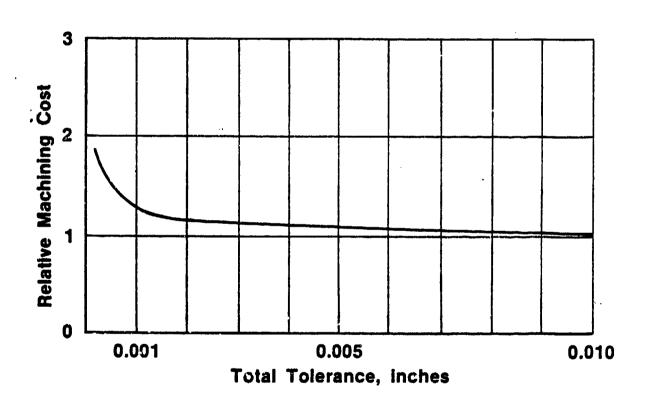
### MACHINING OF CASTINGS SURFACE FINISH COST-DRIVER EFFECT



\*Surface finish shown in micro-inches.

CDE-MC-I

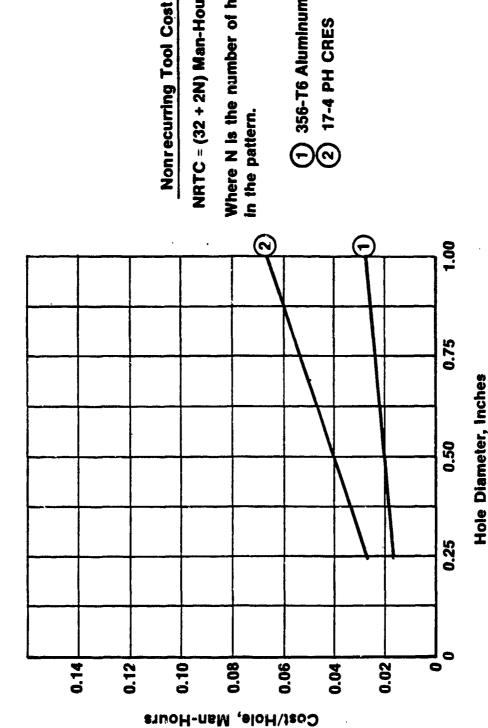
### MACHINING OF CASTINGS — DIMENSIONAL TOLERANCES COST-DRIVER EFFECT



CDE-MC-II

# MACHINING OF CASTINGS

### DRILL HOLES



Where N is the number of holes NRTC = (32 + 2N) Man-Hours in the pattern.

(1) 356-T6 Aluminum (2) 17-4 PH CRES

CED-MC-1

đ

Cost/Part = (Cost/Hole • N) Man-Hours

Cost data is valid for hole depths up to twice the hole diameter.

### CED-MC-2

## DRILL AND SPOTFACE HOLES MACHINING OF CASTINGS

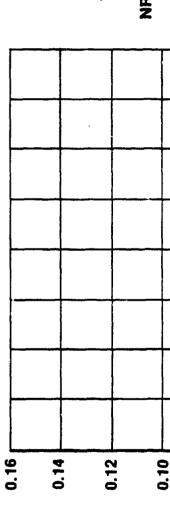
D











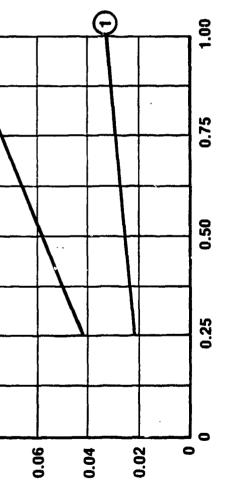
NRTC = (32 + 2N) Man-Hours

**Nonrecurring Tool Cost** 

Where N is the number of holes in the pattern. (Q)

(1) 356-T6 Aluminum

(2) 17-4 PH CRES



Hole Diameter, Inches

Cost/Part = (Cost/Hole • N) Man-Hours

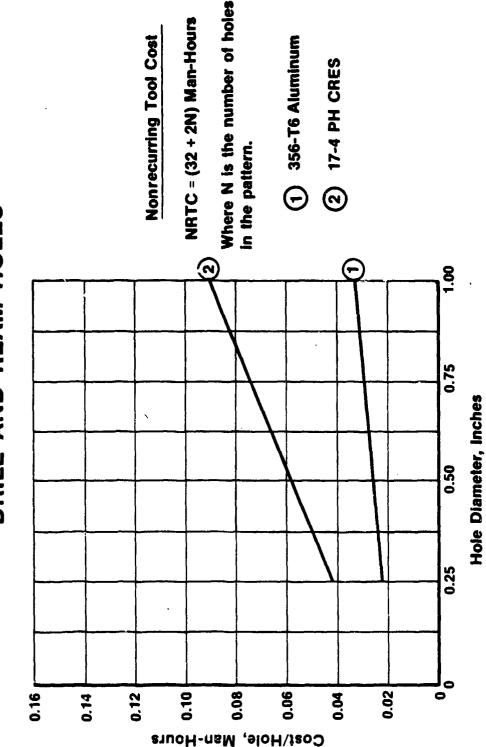
Cost data is valid for hole depths up to twice the hole diameter.

0.08

Cost/Hole, Man-Hours

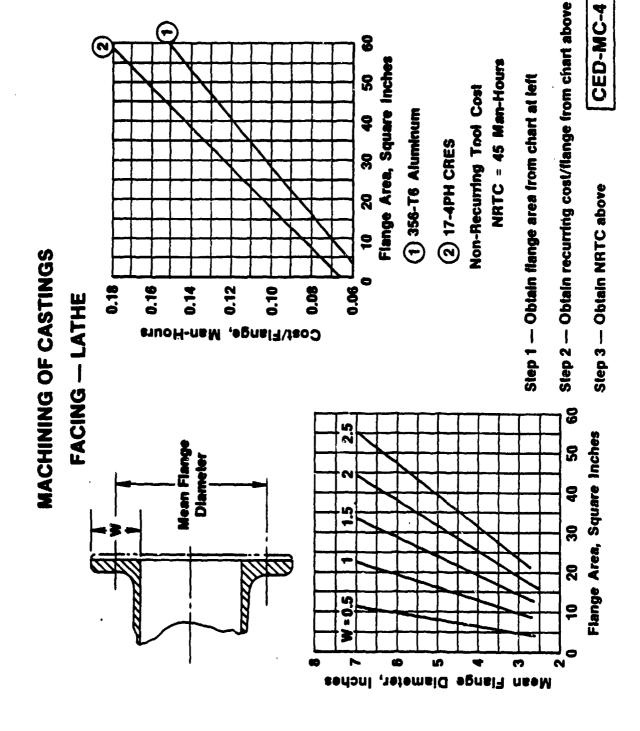
### CED-MC-3

# MACHINING OF CASTINGS DRILL AND REAM HOLES



Cost/Part = (Cost/Hole • N) Man-Hours

Cost data is valid for hole depths up to twice the hole diameter.



# MACHINING OF CASTINGS

## FACE MILLING



Nonrecurring Tool Cost NRTC = 57 Man-Hours

- (1)356/A 356-T6 Aluminum
- (2) 17-4PH CRES

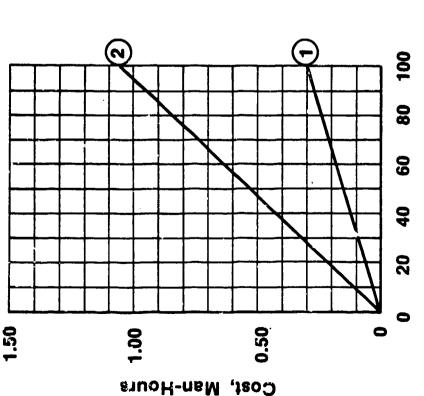
Step 1 — Determine the face milling cost for each surface machined.

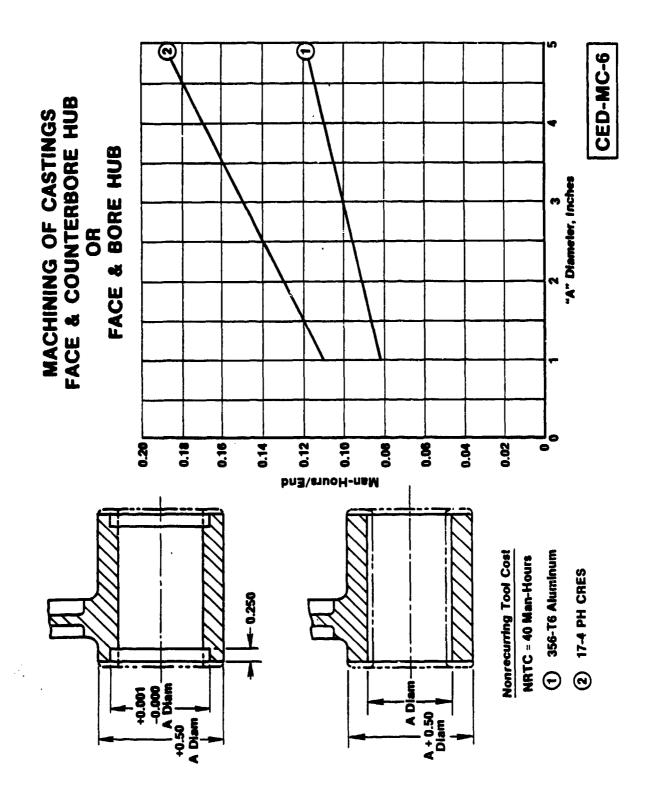
Step 2 — Add the milling costs obtained in Step 1.

Step 3 — Obtain NRTC above.



Area Milled, Square Inches





6560 WHILE BUILDS BYTTEN BUILDS BUILDS BUILDS COLLEGE BOSES BOOKERS COLLEGE COLLEGE

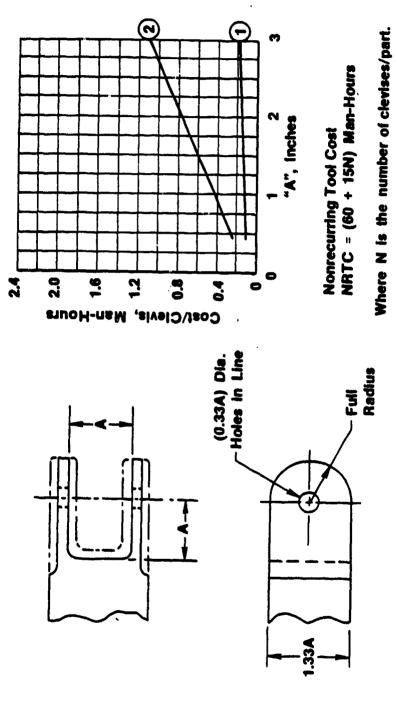
CED-MC-7

(1) 356-T6 Aluminum

(2) 17-4PH CRES

### MACHINING OF CASTINGS STRADDLE MILL, DRILL & REAM

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### 4.5.5 Ground Rules for Castings Section

The following General and Detailed Grounds Rules for the Castings Section were developed to establish the scope of the data required and to establish guidance to MC/DG application. Ground rules are necessary and important as they promote understanding, ensure consistency, uniformity, and accuracy in generating and integrating data into the formats.

### 4.5.5.1 General Ground Rules

The general ground rules are categorized under the following major groupings:

- (a) Casting Designs
- (b) Materials
- (c) Casting and Machining
- (d) Facilities
- (e) Data Generation Recurring Costs (including TI&E)
- (f) Castings TI&E Recurring Costs
- (g) Data Generation Nonrecurring Costs (including TI&E)
- (h) Support Function Modifiers
- (i) Test and Evaluation of Data.

### (a) Casting Designs

- (1) The casting designs selected will be representative of parts commonly required for both small and large aircraft. The parts will be selected such that a base part forms the foundation which the designer can modify as required to achieve the desired discrete part.
- (2) The castings will be selected, where possible, to develop data for more than one casting method. The data, thereby, enable the designer, using the MC/DG, to determine the most cost-competitive casting process in trade-studies.
- (3) The selected castings will adequately display in CED or CDE formats, the effect on cost of DICE (e.g., thin walls, core complexity, corner radii, and structural classification).

### (b) Materials

- (1) The alloys selected for the cast parts will be those commonly used in the industry to enable a uniform data base to be established. The materials included are:
  - Aluminum
  - Titanium
  - · Steel.

### (c) Casting and Machining

- (1) Only conventional casting processes, TI&E methods, and machining methods required to produce finished parts in the configurations selected will be considered. No emerging manufacturing methods will be evaluated.
- (2) A production, in contrast to a prototype environment, will be assumed for the cast machined parts.
- (3) To generate an effective data base for each selected part, a factory operational sequence utilized by the casting user will be established reflecting the most economical means of fabrication of the final part. This standardized sequence will be used by each team member to determine the part cost.
- (4) Requirements for tooling to machine and inspect the various parts will be identified on the data collection forms.

### (d) Facilities

(1) Only standard manufacturing and TI&E facilities, available to the airframe industry, will be considered.

### (e) Data Generation - Recurring Costs

(1) Recurring cost data (standard man-hours) will be generated for the complete fabrication process and will, therefore, include all the hands-on direct factory labor operations from receipt of the raw casting through storage of part in readiness for assembly into the airframe, excluding bearings,

- bushings, and threaded inserts. The data will also include the raw casting TI&E data.
- (2) Raw casting data presented in the MC/DG formats shall include total raw casting costs including TI&E with mechanical property verification.
- (3) Data will be generated separately for aluminum sand, aluminum investment, and steel investment castings. Data will be based on box volume using team companies' historical data.
- (4) Raw casting part costs will be generated for each type of casting.
- (5) The DICE elements will be treated as separate cost elements and, therefore, not included in the base-part cost, but will be displayed in CED or CDE formats.
- (6) Recurring tooling costs (tool maintenance, tool planning, etc.) will not be included.
- (7) The quantity for which the base part and the DICE costs will be determined is at unit 200. A lot release size of 25 will be applied.
- (8) The data submitted to BCL will be the raw casting part cost (man-hours or dollars) plus the DICE incremental factors associated with the discrete casting design.

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- (9) In developing the cost data for parts, each participating company may utilize its own proprietary improvement curves.
- (10) The part casting and DICE costs will be normalized by BCL to reflect an industry team average value.
- (11) For proprietary reasons, business sensitive information employed at team member contributing companies will not be presented in the MC/DG.
- (12) No data provided by any team member will be disclosed to other team members, agencies, or to the public without the expressed approval of the team member.

- (f) Castings TI&E Recurring Costs
  - The general ground rules for castings (paragraphs 2, 6, 7, 9, 11, and 12) also apply to the casting TI&E. The following are added for casting TI&E.
  - (2) Recurring cost data will be generated for TI&E functions required from the supplier to receiving stores, including outside laboratories.
  - (3) TI&E cost data for the raw castings only will be included.
  - (4) Costs will be presented in 1930 dollars.
  - (5) CED and/or CDE formats will display the following TI&E costs and data:
    - e Penetrant inspection
    - Radiographic inspection
    - Magnetic particle inspection
    - · Mechanical properties verification
    - Chemistry verification
    - · Dimensional inspection.
  - (6) TI&E cost data will be normalized by BCL to reflect an industry team average value.
- (g) Data Generation Nonrecurring Costs for Raw Castings and TI&E
  - (1) Tooling costs will be generated for each part type. TI&E fixture costs will be the responsibility of the user company where applicable.
  - (2) The cost of production tooling will be restricted to contra or project tools only for presentation in the MC/DG.
  - (3) First article Ti&E cost will be generated and displayed as part of the nonrecurring tooling cost.
  - (4) Nonrecurring fooling costs (NRTC) generated by the team companies will be normalized by BCL for presentation in the MC/DG.

### (h) Support Function Modifiers

(1) Additional effort other than factory labor and TI&E, i.e., planning and tool maintenance, will be excluded from the part cost data supplied to BCL. Other modifiers may be included later by the MC/DG users at airframe companies.

### (i) Test and Evaluation of Data

(1) Test and confirmation of the formats and integrated data will be accomplished by one team member. Each of the remaining team members will be provided with the evaluation. Any anomalies will be resolved and modifications incorporated as appropriate.

### 4.5.5.2 Detailed Ground Rules

The detailed ground rules are categorized under the following major groups:

- (a) Casting designs
- (b) Materials
- (c) Classification
- (d) Data generation recurring costs
- (e) TI&E functions.

### (a) Casting Designs

- (1) Each team member will review applicable casting designs and tabulate required data on the data collection sheets developed by the team.
- (2) Selected typical designs will be utilized for determination of user-associated costs (e.g., machining and finishing).
- (3) The castings analyzed by each team member will be classified by complexity type. This classification will be designated on the data collection form submitted to BCL.

Each team member company will submit to BCL a definition or a drawing or sketch illustrating their proposed understanding of these classifications.

### (b) Materials

(1) The materials and processes selected for castings are:

### • Aluminum

- A356 per MIL-A-21180 or company equivalent specification (sand or investment)
- 356 or A356 per QQ-A-601 (sand castings)
- 357 per MIL-A-21180 (sand castings)

### Steel

- 17-4PH CRES per AMS-5342, 5343, and 5344 or company equivalent specification

### Titanium

- Ti-6Al-4V Cond A (vacuum cast, investment or rammed graphite).

### (c) Classification

- (1) The basic use classification (Class I or II) shall be reported for each casting.
- (2) The casting quality shall comply with MIL-C-6021 or equivalent user company specification for X-ray grade.
- (3) The radiographic standard grade (A, B, C, or D) basis for each casting shall be reported. Special testing (e.g., static tests) used to complement inspection shall be identified.

### (d) Data Generation - Recurring Costs

(1) Data indicated on the data collection sheet will be gathered, as available, for the raw casting. TI&E costs associated with the raw casting will be established separately.

- (2) Machining (including cleaning and protective coatings) will be reported separately for typical parts utilizing standards and learning (improvement) curves, if applicable. TI&E costs for the user operations will not be included as a part of this task.
- (3) Machining cost data will be developed for the following basic machining parameters:
  - (a) Counter-bore and face-hub
  - (b) Drilled holes, drilled and reamed holes, drilled and spot-faced holes
  - (c) Circular-flange facing (lathe), flat-faced (mill)
  - (d) Straddle-mill and drill-clevis fittings.
- (4) Available cost data for titanium castings obtained from suppliers by BCL will be analyzed and formatted.

### (e) TI&E Functions

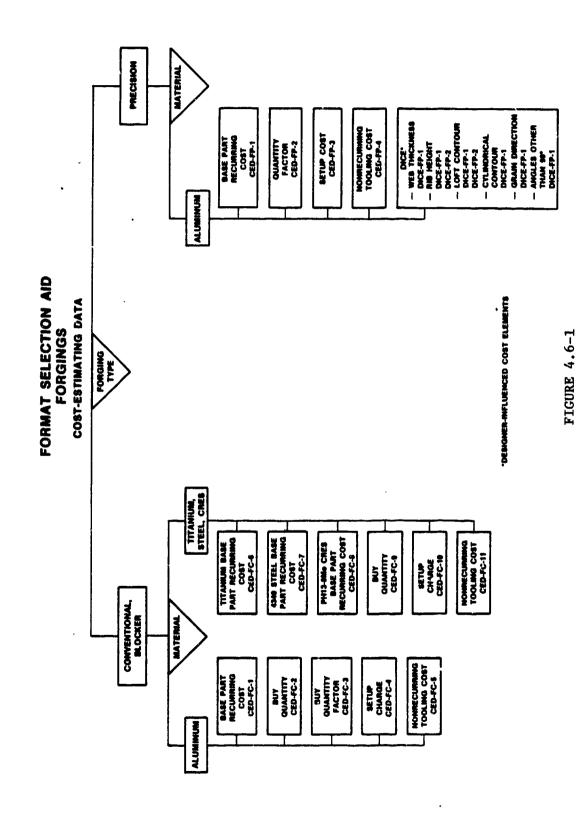
- (1) The following are typical TI&E operations that will be evaluated:
  - Chemistry
  - Mechanical properties
    - Separately cast test bars
    - Coupons from castings (prolongation)
    - Dissected castings
  - o Dimensional
  - Radiographic
  - Penetrant/magnetic
  - Surface finish
  - Pressure test
  - Static test (proof of design).

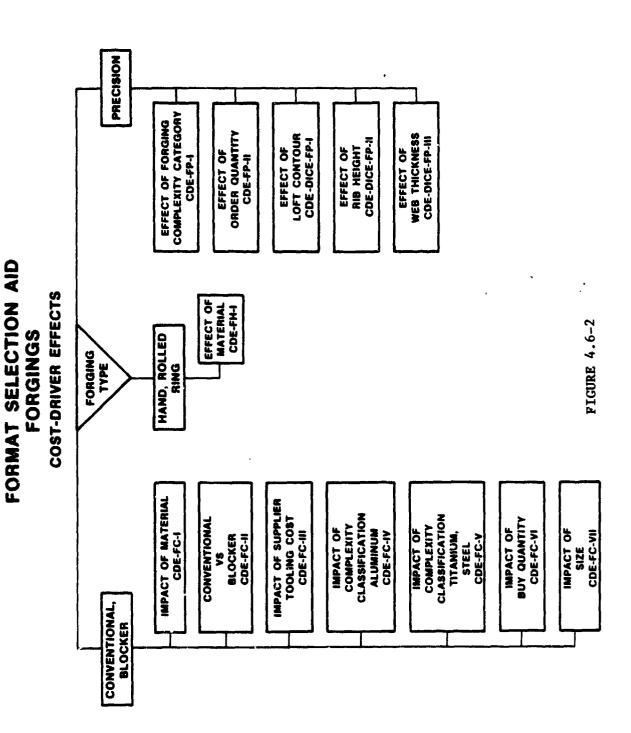
### 4.6 Forging Section

This section contains format selection aids, identification of the types of parts analyzed for data to determine the manufacturing man-hour data, examples of how the data are utilized in airframe design and a set of formats generated. These formats include cost-driver effects (CDE), cost estimating data (CED), and designer-influenced cost elements (DICE).

### 4.6.1 Format Selection Aids

Format selection aids are presented to provide the user with a building-block approach to determine manufacturing cost data for alternative designs or processes. The designer can review the format selection trees and identify those areas that have an impact on his design. The formats provide cost-driver effects (CDE) for qualitative guidance to lowest cost and cost-estimating data (CED) in man-hours for conducting trade studies.



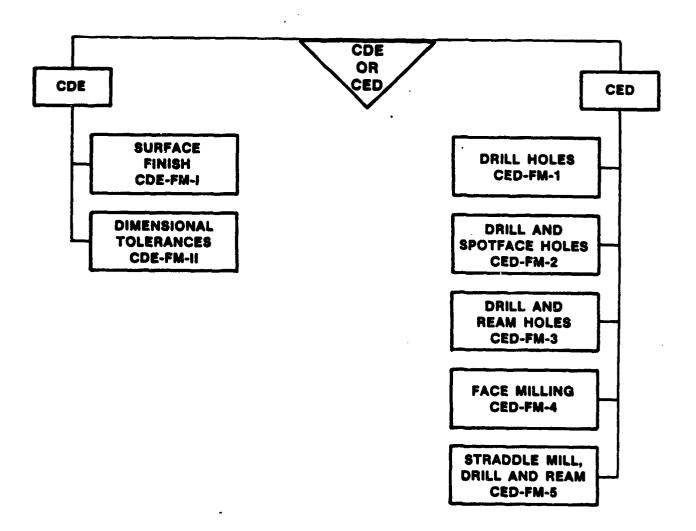


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### FORMAT SELECTION AID

### MACHINING OF FORGINGS



**FIGURE 4.6-3** 

#### 4.6.2 Example of Utilization

This example demonstrates how the data generated are utilized on a specific design problem. The example shows how to identify applicable formats, how to extract data from the formats, and provides a discussion on how the data are used to determine the part cost in man-hours or dollars. The MC/DG cost worksheet can be used to record the cost data for easy reference and to determine the total program cost. (Figure 3-3). Worksheets for forgings and also machining of forgings are provided in Tables 4.6-2 and 4.6-3.

#### 4.6.2.1 Utilization Example for Aluminum Precision Forging

#### Problem Statement

Determine the cost, in 1982 dollars per part, for the aluminum precision forging shown in the sketch on the following page. Test, inspection and evaluation (TI&E) costs are to be included in the cost of the forging. The dimensions are as shown in the part sketch. The design quantity is to be 200 units and the buy quantity is 50 units per buy.

#### Procedure

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The following procedure is used to determine the forging cost.

- 1. Obtain a copy of the MC/DG Forgings Cost Worksheet, and begin to fill in the necessary information.
- 2. Utilize the Format Selection Aid for Forgings Cost-Estimating Data (Figure 4.6-1).
- 3. Determine the formats to use. For this part, the following formats, which are included in this section, are required:
  - Base Part Manufacture
    - Base Part Recurring Cost: CED-FP-1 (Figure 4.6-6)
    - Quantity Factor: CED-FP-2 (Figure 4.6-7)
    - Setup Cost CED-FP-3 (Figure 4.6-8)
    - Nonrecurring Tooling Cost: CED-FP-4 (Figure 4.6-9)
  - Designer-Influenced Cost Elements
    - Web Thickness: DICE-FP-1 (Figure 4.6-10)
    - Rib Height: DICE-FP-1 (Figure 4.6-10)

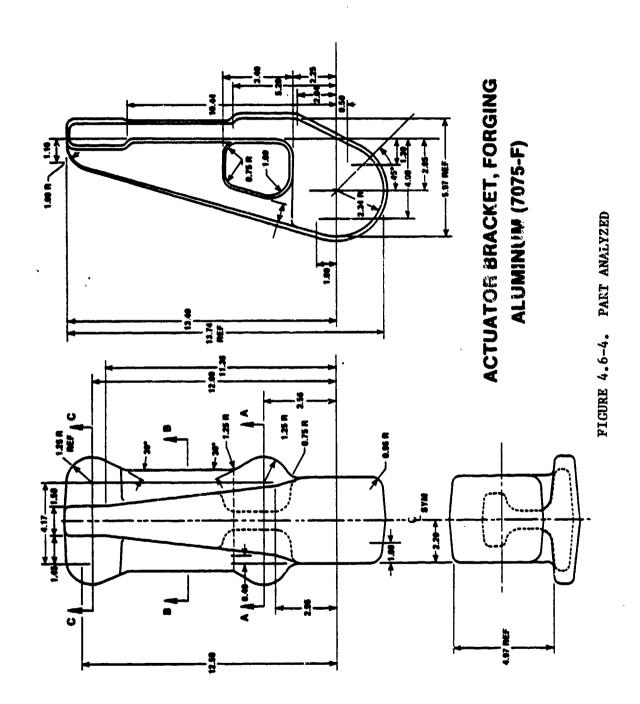
DICE-FP-2 (Figure 4.6-11).

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4. Study the formats to determine the required parameters and conditions and relate these to the part. The following parameters and conditions are required.

Format	Parameters, Conditions
CED-FP-1	Plan area Complexity classification
CED-FP-2	Order quantity
CED-FP-3 (Fig. 4.6-8)	Complexity classification Plan area Order quantity
CED-FP-4 (Fig. 4.6-9)	Plan area Complexity classification
DICE-FP-1 (Fig. 4.6-10)	Design feature Plan area Web thickness Rib height
DICE-FP-2 (Fig. 4.6-11)	Design feature Rib height.

- 5. Read the required data from the formats and enter the data onto the Forgings Cost Worksheet.
- 6. Perform the calculations indicated on the worksheet for recurring and nonrecurring cost.
- 7. Utilize the Format Selection Aid for Test, Inspection and Evaluation (TI&E) of Forgings (page 4.7.4-2).
- 8. Determine the format to use. In this case, Format CED-TI&E-F-1 (Fig. 4.6-12) is required.
- Study the format to determine necessary parameters and conditions. For CED-TI&E-F-1, forging type and inspection type are required.
- 10. From CED-TI&E-F-1, read the TI&E costs.
  - The first article inspection cost is the cost of one forging plus \$300.
  - The production TI&E cost is the cost of one forging plus \$300 per lot.
- 11. Substitute these values into the appropriate spaces on the worksheet and perform the indicated calculations to determine the program cost of TI&E.
- 12. Perform the calculations indicated in the Cost Summary section of the worksheet to determine the total cost per part of the forging. For this part, the total cost per part is \$218.



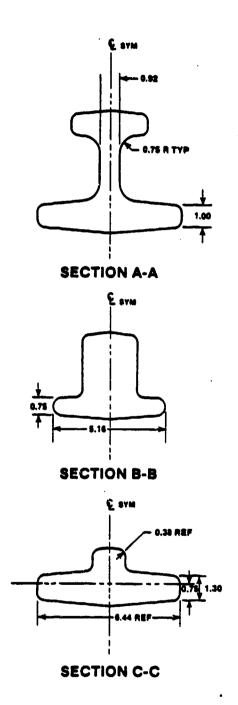
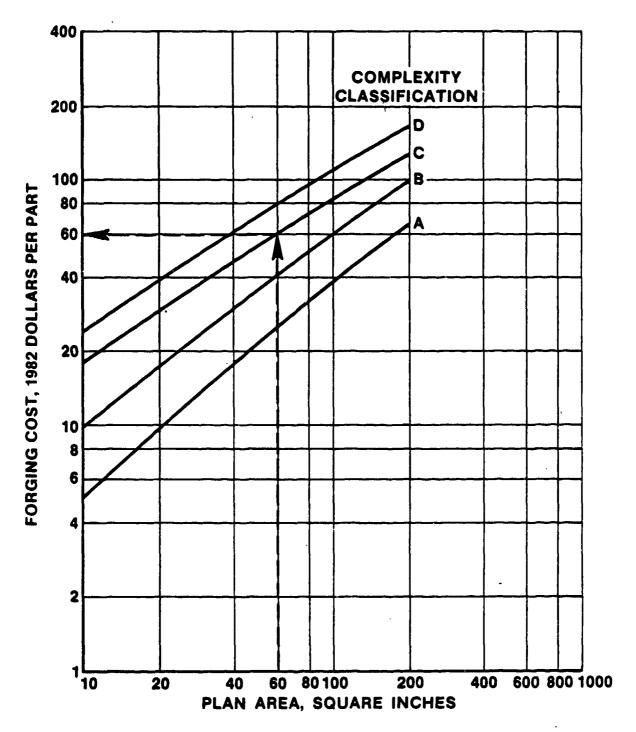


FIGURE 4.6-5. PART ANALYZED

#### ALUMINUM PRECISION FORGING BASE PART COST



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FIGURE 4.6-6. FORMAT USED IN EXAMPLE

CED-FP-1

### ALUMINUM PRECISION FORGINGS QUANTITY FACTOR

ORDER QUANTITY	FACTOR
UP TO 25	1.6
26 TO 50	1.35
51 TO 100	1.2
101 TO 200	1.1
201 UP	1.0

NOTE: IF ORDER QUANTITY IS NOT KNOWN, USE 1.35.

FIGURE 4.6-7. FORMAT USED IN EXAMPLE

CED-FP-2

ALUMINUM PRECISION FORGINGS SETUP COST

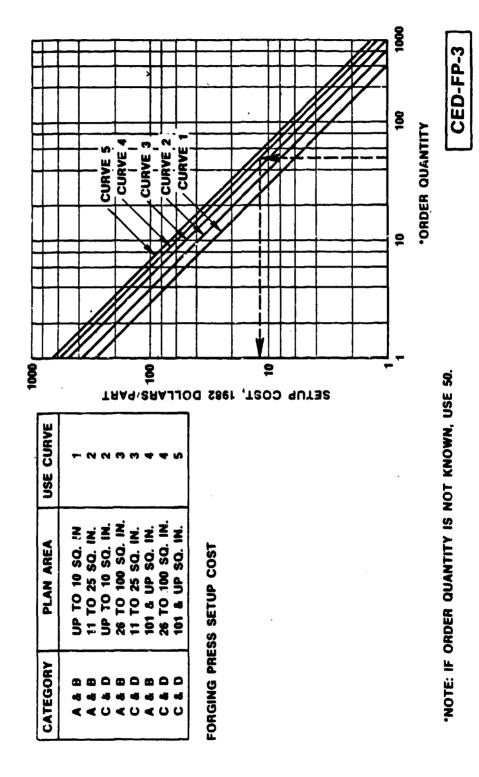
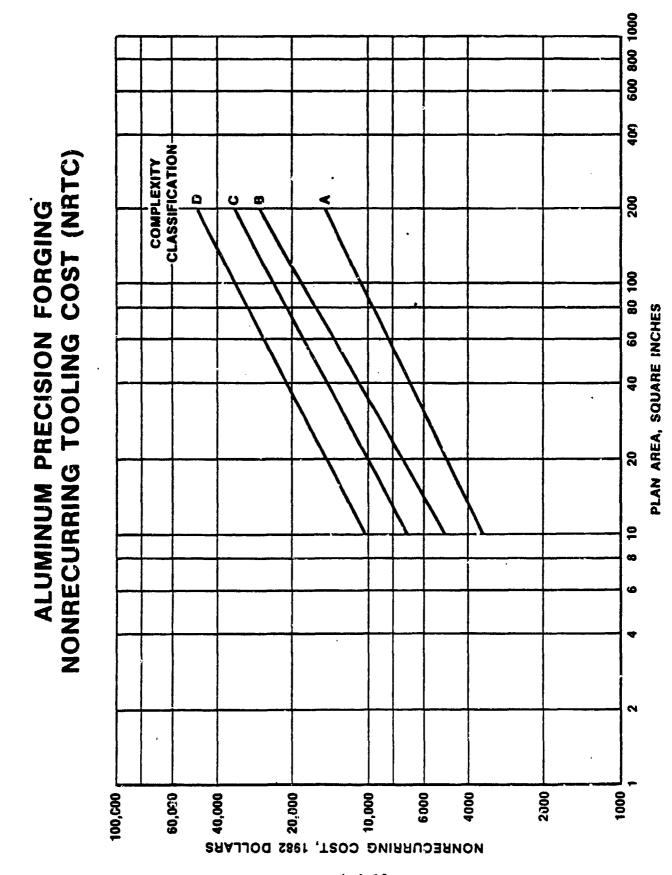


FIGURE 4.6-8. FORMAT USED IN EXAMPLE

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CED-FP-4

FIGURE 4.6-9. FORMAT USED IN EXAMPLE



## ALUMINUM PRECISION FORGING RECURRING COST DICE FACTOR

DESIG	DICE FACTOR		
WEB	·		
PLAN AREA	WEB THICKNESS		
UP TO 50 SQ. IN.	0.120	-	
	0.090		
51 TO 150 SQ. IN.	0.150		
	0.120	1.3	
151 TO 200 SQ. IN.	0.180	-	
	0.150	1.3	
RIB			
UP TO 1.50		_	
1.51 TO 2.00	ì	1.1	
2.01 TO 3.00		1.2	
3.01 TO 4.00		1.5	
4.01 TO 5.00		1.7	
5.01 TO 6.00		1.9	
SPECIAL			
LOFT CONTOUR		1.2	
CYLINDRICAL CON	CYLINDRICAL CONTOUR		
GRAIN DIRECTION			
ANGLES OTHER TH	IAN 90 DEGREE TO BASE	1.2 1.2	

NOTE: IF MORE THAN ONE (1) DESIGN FEATURE IS APPLICABLE, USE ONLY THE HIGHEST.

FIGURE 4.6-10 FORMAT USED IN EXAMPLE

DICE-FP-1

#### ALUMINUM PRECISION FORGING NONRECURRING COST DICE FACTOR

DESIGN FEATURE	DICE FACTOR
RIB HEIGHT	
UP TO 1.50	-
1.51 TO 2.00	1.05
2.01 TO 3.00	1.10
3.01 TO 4.00	1.25
4.01 TO 5.00	1.35
5.01 TO 6.00	1.45
LOFT CONTOUR	1.50

NOTE: IF MORE THAN (1) DESIGN FEATURE IS APPLICABLE USE ONLY THE HIGHEST.

DICE-FP-2

FIGURE 4.6-11. FORMAT USED IN EXAMPLE

# **ALUMINUM, TITANIUM, STEEL, CRES FORGINGS** TEST, INSPECTION, AND EVALUATION

INSPECTION	HAND AND ROLLED RING FORGINGS	HAND AND ROLLED BLOCKER, CONVENTIONAL RING FORGINGS & PRECISION FORGINGS
FIRST ARTICLE (NONRECURRING)	NOT APPLICABLE	COST OF ONE (1) FORGING +
		PLAN AREA 1982 \$ 100 SQ. IN. 300
		101-503 SQ. IN 400 501-1,000 SQ. IN. 500
PRODUCTION	\$300/LOT	(1) FOR

NOTE: COSTS IN 1982 DOLLARS ARE FOR BOTH SUPPLIER AND USER. ULTRASONIC INSPECTION COSTS TO BE ADDED.

FIGURE 4.6-12. FORMAT USED IN EXAMPLE

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# **ALUMINUM, TITANIUM, STEEL, CRES FORGINGS** TEST, INSPECTION, AND EVALUATION

INSPECTION	HAND AND ROLLED RING FORGINGS	HAND AND ROLLED BLOCKER, CONVENTIONAL RING FORGINGS & PRECISION FORGINGS
FIRST ARTICLE (NONRECURRING)	NOT APPLICABLE	COST OF ONE (1) FORGING +
		PLAN AREA 1982 \$ 100 SQ. IN. 300 101-500 SQ. IN 400 501-1,000 SQ. IN. 500 1,001 up 600
PRODUCTION	\$300/LOT	COST OF ONE (1) FORGING + \$300 PER LOT.

NOTE: COSTS IN 1982 DOLLARS ARE FOR BOTH SUPPLIER AND USER. ULTRASONIC INSPECTION COSTS TO BE ADDED.

FIGURE' 4.6-13. FORMA'T USED IN EXAMPLE

#### TABLE 4.6-1

#### **FORGING COST WORKSHEET**

TYPE	MATERIAL	DESIGN QUA		LOT QUANTITY:	PRECISION	NER: . DATE: TEST, INSP. & EVALUATION
						TEST, INST. E EVALUATIO
tend Ving	Aluminum TISAI-4V	.  8/35 L00	Weight Lb Base Cost	Category 8	Base Cost	First Article Cout
Hocker	4940	W10	\$/Lis	c	Setup Coet	One Foreine + \$=\$ _
30n~	Atr	TT	Setup Cost	Plan Area	\$Es.	
Precision	Veenum	WolghiL	\$/Lot	\$q. In.	DICE Factor	One Ferging + \$300 =\$
	PH Cree	Base Cost	81= L	Buy-Quantity	Rec	Ultraconic Insp. SE
	15-6	*/-	WH Die Factor	Factor	Nonrec	Intiation Factor
		<u>'L</u>		ļ		<u> </u>
RECURRIN						•
nane/	Ring Forging					
	Cost/Part = Weig	ht x Bose Cost x in	fletton Factor			
•	-			/Lb x	* \$	Each
Block	er Forging <sub>,</sub>		B			
	Cool/Part =   Wo	ight x Base Cost x	is x Pactor + Th	uy Qty. Inflation		
					\$	
	• [—	Lb x \$	<del></del>	/Lb x 0.8 x	_·	
	**	Each			•	•
	intional Forgi			_		
	CoorPort = Wo	aht z Boso Cost z	Buy City. Setup/ Festor Buy C	Lot Inflation		
	<b>,</b>	<b>-</b> : / = = = = = = = = = = = = = = = = = =	PERSON BUY C	ny. J Paster		1
	•	Lb = \$		Lb x	<del></del>	/Lot
	- \$ L	Each			•	, ,
Precis	ion Forging					
		Rec.DIC	E Buy City. • Sei	Inflation		
		Factor	- Factor	Feater		•
	** [	Each x		x	_ +\$	Each
	• • •	Each		ė		J
ONRECHE	RING COST					<del></del>
	er / Conventio	nei Foreine				
			Die _ inf	tetion	•	
Block	91					
Block	Test Cest = (L+	12"XM+12"XH+	Factor Fo	etor		
Block	Teel Cest = (L+			etor +12") x (	+14") x	
Block		+18") ;			+14") x	*
Block	= (	+18") ;			+14") x	
Slack:	* ( * \$ sion Foreina	+18") : 		+18") x (	+14") x	
Sleck:	* ( * \$ sion Foreina	+18") : 		+18") x (	+14"} z	
Sleck:	= ( = 8 sion Forging Tool Cost = Boo	+12") : Tool Cost x None	ue, DICE Inflation setor <sup>R</sup> Factor	+18") x (	· +14") z	
Sleck:	= ( = \$ pion Forging Teel Cost = Beel =	+18") : 	ue, DICE Inflation setor <sup>R</sup> Factor	+18") x (	+14") z	
Sleck:	= ( = 8 sion Forging Tool Cost = Boo	+12") : Tool Cost x None	ue, DICE Inflation setor <sup>R</sup> Fector	+18") x (	+14") z	
Slack: Precis	= ( = \$ pion Forging Teel Cost = Beel =	+12") : Tool Cost x None	ue, DICE Inflation setor <sup>R</sup> Fector	+18") x (	+14") z	
Slack: Precis	= ( = \$ sion Forging Tool Cost = Boo = = \$ Burnmary	+12") z	ve. DICE inflation actor x Fector	+12") x (		,
Black: Precis	= ( = \$ sion Forging Tool Cost = Boo = = \$ Burnmary	+12") z	ve. DICE inflation actor x Fector	+18") x (		,
Slack: Precis	= ( = \$ sion Forging Tool Cost = Boo = = \$ Burnmary	+12") z	ec. DICE inflation actor x Fector z z	+12") x (	ME Design Qt pt X Let Qty.	,
Slacki Precis	# ( # 8 # 6	Tool Cost x Nome Fig. 2 No. 2	in + Toel Ceet + Toel	+12") x (	ME Design Oty of E Let Gty. +8	,
Black: Precis	# ( # 8 # 6	Tool Cost x Nome Fig. 2 No. 2	in + Toel Ceet + Toel	+12") x (	ME Design Oty of E Let Gty. +8	,

1.7 %

#### TABLE 4.6-2

#### MACHINING COST WORKSHEET FOR FORGINGS

MACHINING FEATURE	FORMAT	RECURRING COST (MAN-HOURS)	NONRECURRING TOOLING COST (MAN-HOURS)
HOLES: NO SIZE			
drill Drill & Spotface Drill & Ream		-	
FACE MILLING AREA MILLEDIN <sup>2</sup>			
CLEVIS-STR. MILL, DRILL, AND REAM NOSIZE			
MACHINING COST (UNIT 200) PER PA	RT		
LEARNING CURVE FACTOR (SEE BEL	OW)		
LABOR RATE		\$ · /HR	\$ /HR
RECURRING MACHINING COST/PART	•	3	
NONRECURRING TOOLING COST (NRTC)			\$

\*RECURRING MACHINING COST/PART = UNIT 200 COST/PART = LEARNING CURVE FACTOR = LABOR RATE.

DESIGN QUANTITY	LEARNING CURVE FACTOR	DESIGN QUANTITY	LEARNING CURVE FACTOR
1	2.25	200	1.17
10	1.79	350	1.08
25	1.59	500	1.02
50	1.44	750	0.96
100	1.30	1000	0.92

90% LEARNING CURVE FACTOR TO CONVERT UNIT 200 FORMAT COST TO CUMULATIVE AVERAGE COST FOR VARIOUS DESIGN QUANTITIES.

Program Cost =				
(	*	+)	×	2
RECURRING MACHINING COST	Design Quantity	NRTC	INFLATION FACTOR**	
TOTAL COST PER PART	= PROGRAM COST/E	ESIGN QUANTII	TY = /	=
**IMELATION EACTOR SLIDE	I IED BY LISER'S COL	MDANY		

#### 4.6.3 Parts Analyzed

THE THE CONTROL OF THE PROPERTY OF THE PROPERT

The data for the forgings are applicable for parts such as shown in Figures 4.6-13 to 4.6-24. It will be noted that the parts have been classified as A, B, C, and D. Conventional and precision forgings are also indicated. The classifications are classified as follows:

#### CLASSIFICATION LEVELS OF COMPLEXITY FOR CONVENTIONAL FORGINGS

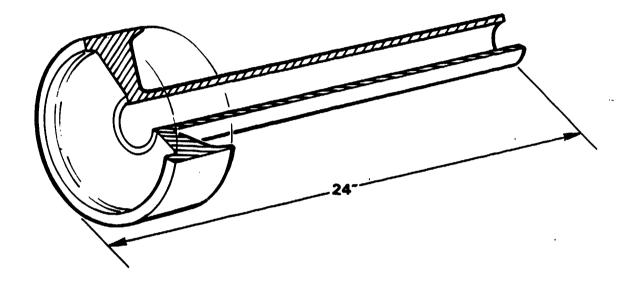
- A. Simple cylindrical, rectangular, and square shapes with minor features; and "L" shapes.
- B. Beams and frame sections such as "T" shapes, cruciform shapes, and channel cross-sectional shapes; open end shapes; and shallow flat boxes and bath tubs.
- C. Thin, flat or moderately contoured shapes (other than round).
- D. Box shapes, "H" shapes with enclosing ribs, inter- and circumscribing ribs, and circular wheel shapes with enclosing ribs.

#### CLASSIFICATION LEVELS OF COMPLEXITY FOR ALUMINUM PRECISION FORGINGS

- A. Simple cylindrical, rectangular, and square shapes with minor features; "L" shapes; three-sided corner clips; and thin, flat, or moderately contoured shapes.
- B. Beams and frame sections such as "T" shapes, cruciform shapes, and channel cross-sectional shapes; open end shapes; and shallow flat boxes and bath tubs.
- C. Box shapes, pocketed cross sectional "H" shapes, and circular shapes with enclosing ribs.
- D. "C" above with thin nonsymmetrical protrusions.

Note: For design proportions and/or tolerances that are closer than the standard design practices or are difficult to classify in the above classifications, consult value or producibility function in company utilizing MC/DG.

# FORGING CLASSIFICATION "A" CONVENTIONAL FORGING



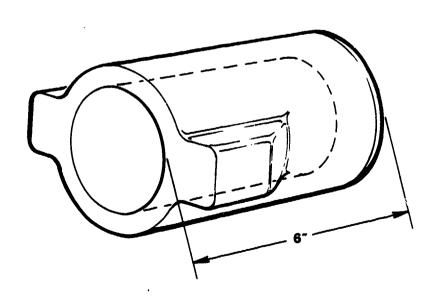
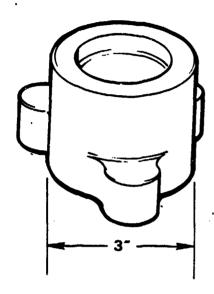
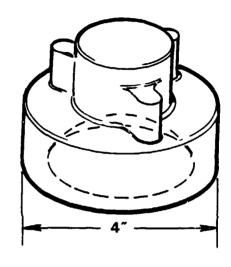


FIGURE 4.6-14

## FORGING CLASSIFICATION "A" CONVENTIONAL FORGING



City



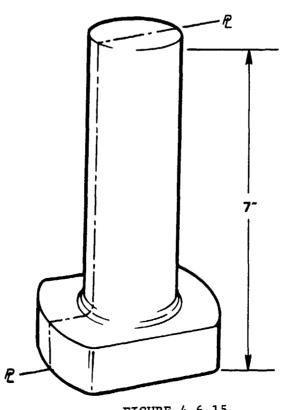


FIGURE 4.6-15

# FORGING CLASSIFICATION "A" PRECISION FORGING

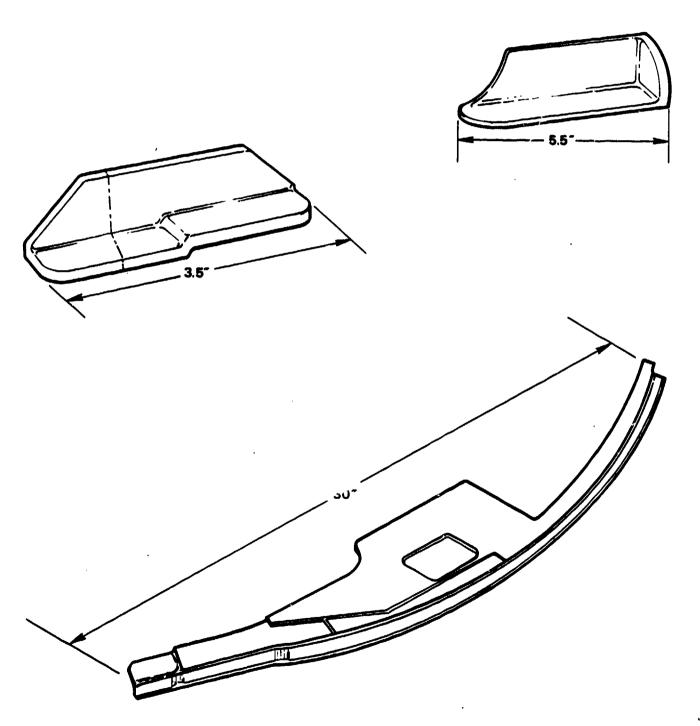
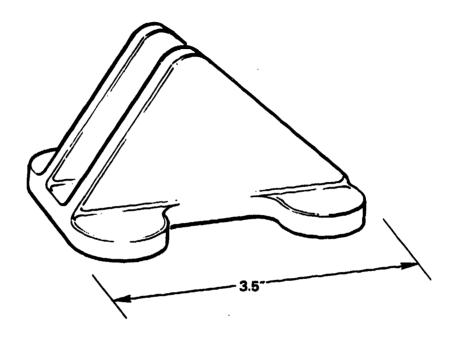
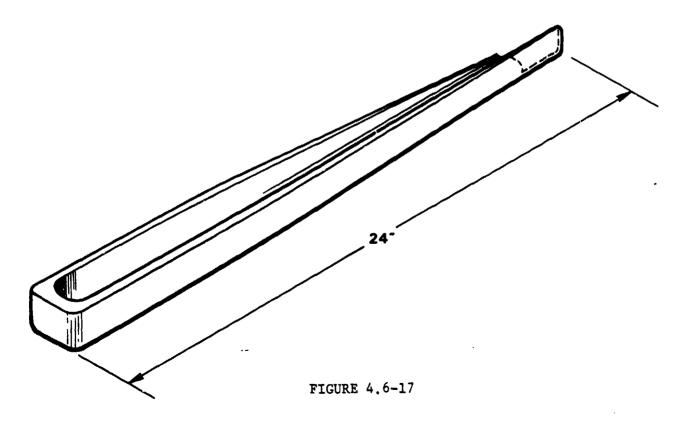


FIGURE 4.6-16

# FORGING CLASSIFICATION "B" PRECISION FORGING

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# FORGING CLASSIFICATION "B" CONVENTIONAL FORGING

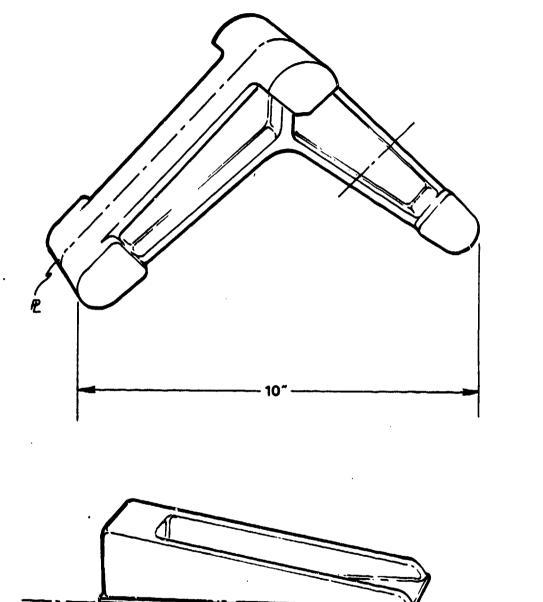
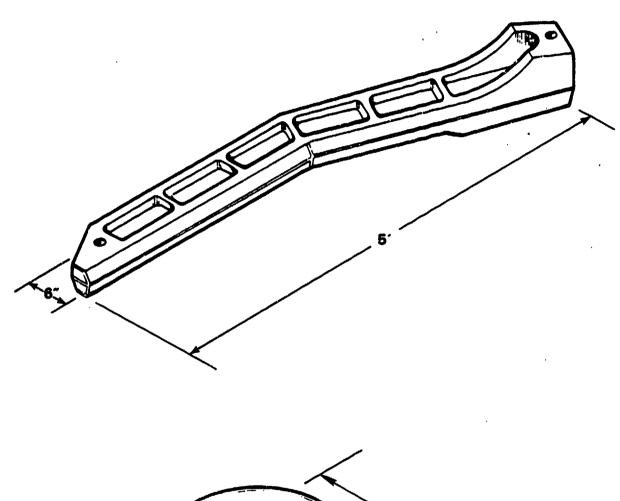


FIGURE 4.6-18

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# FORGING CLASSIFICATION "B" CONVENTIONAL FORGING



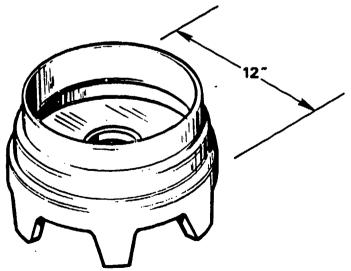
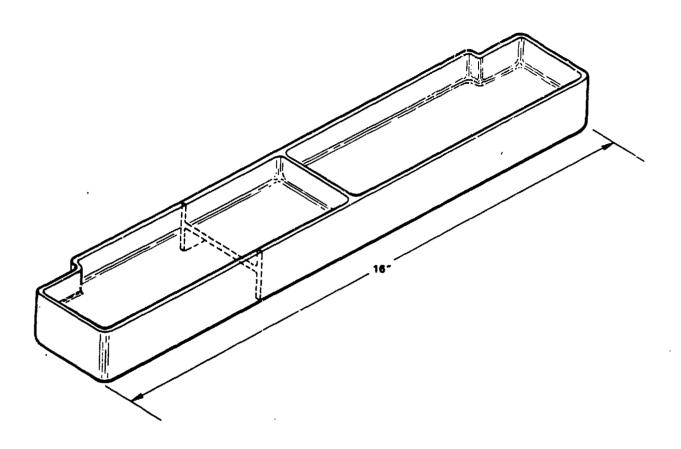
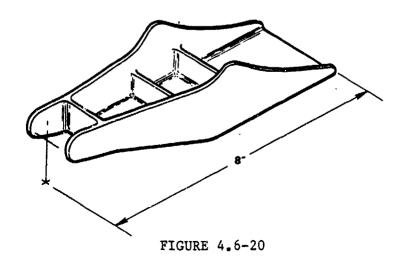


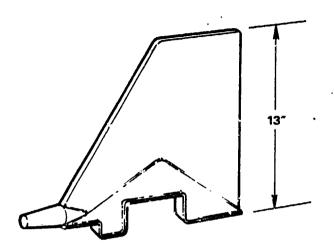
FIGURE 4.6-19

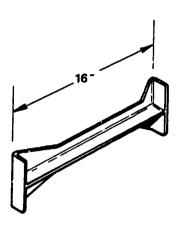
# FORGING CLASSIFICATION "C" PRECISION FORGING





# FORGING CLASSIFICATION "C" CONVENTIONAL FORGING







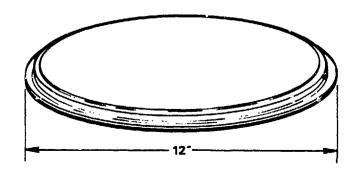
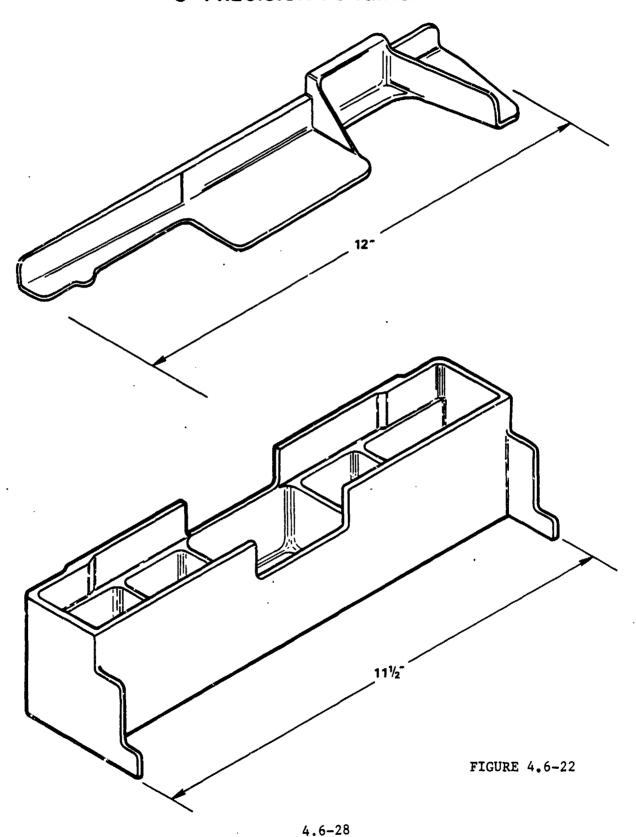


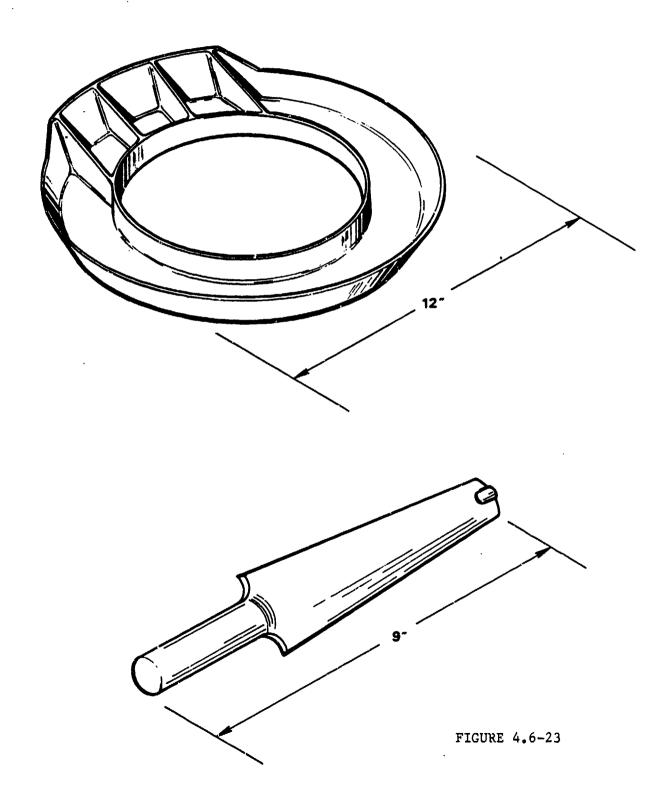
FIGURE 4.6-21

FTR450261000U 3 Jan 1983

# FORGING CLASSIFICATION "C" PRECISION FORGING



# FORGING CLASSIFICATION "D" PRECISION FORGING



# FORGING CLASSIFICATION "D" CONVENTIONAL FORGING

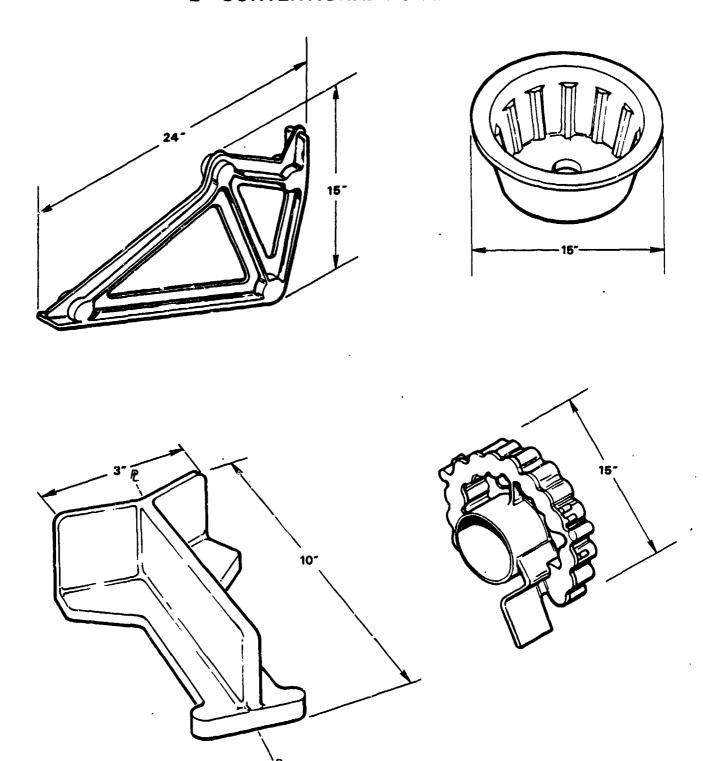


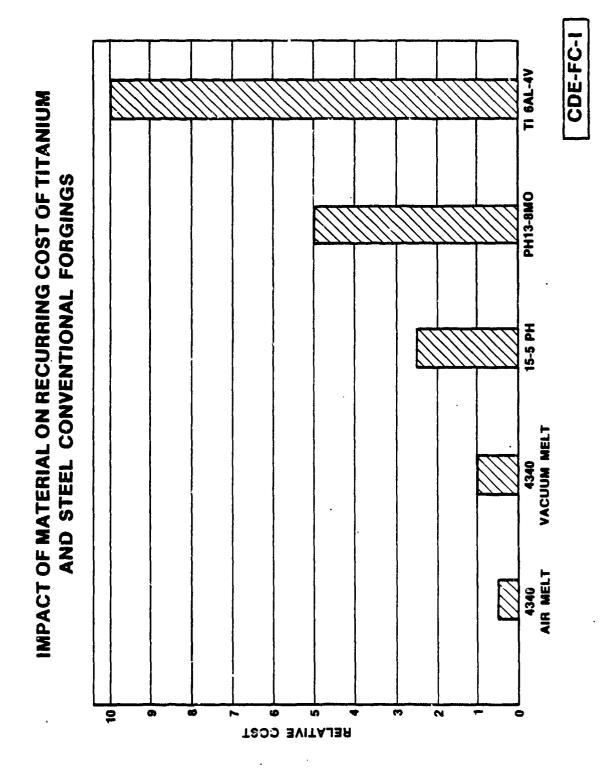
FIGURE 4.6-24

#### 4.6.4 Forging Manufacturing Cost Data

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The formats on the following pages provide designer guidance to lowest cost and also enable cost trade-studies to be conducted. As forgings are normally machined, the extent of which is function of the forging type, formats are also included on the cost of machining.

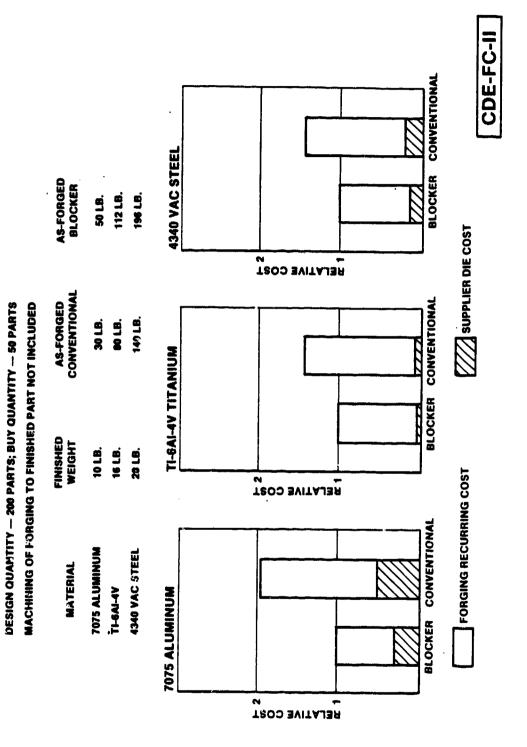


# COST OF CONVENTIONAL VS. BLOCKER FORGINGS

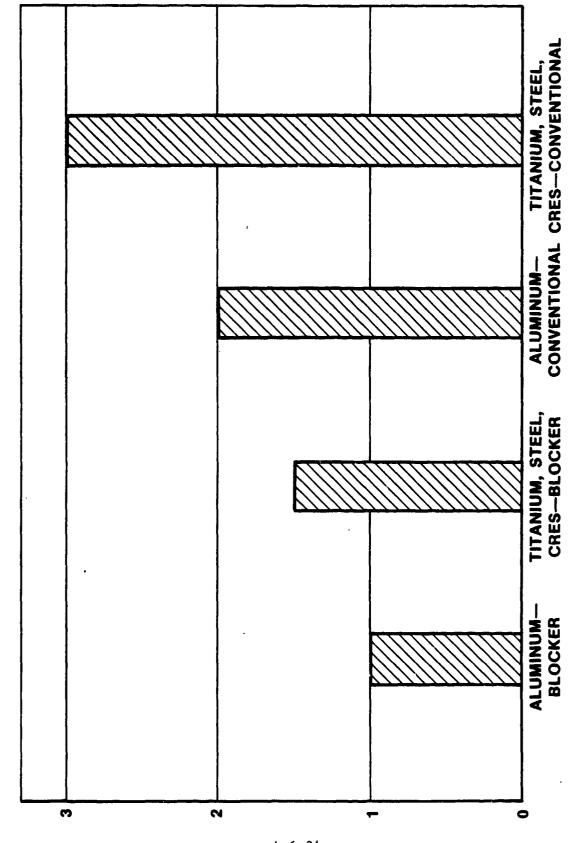
FIWISHED PART — VOLUME — 100 CU IN.; PLAN AREA — 170 SQ. IN.; L-36", W-6", H-3"

PREMISES

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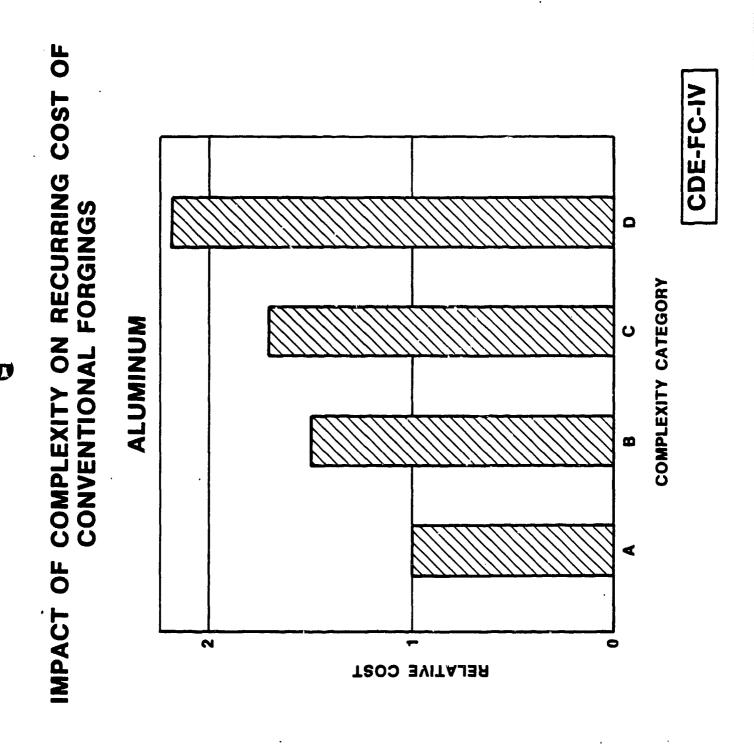


N



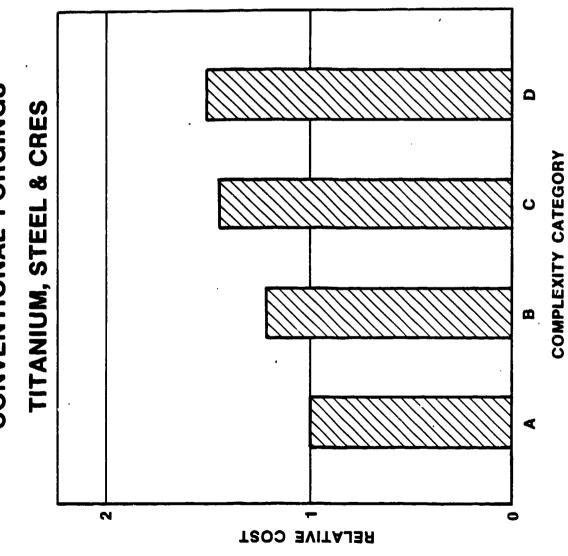
SEL MONTON REGISTED TO SELECT TO SEL

IMPACT OF SUPPLIER TOOLING COST

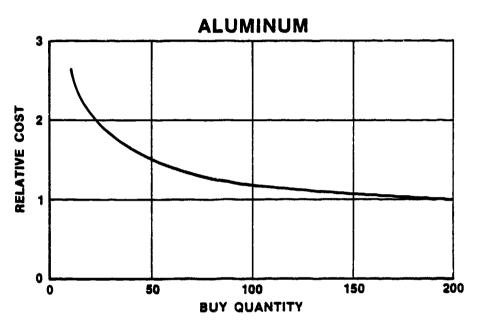


THE REPORT OF THE PROPERTY OF

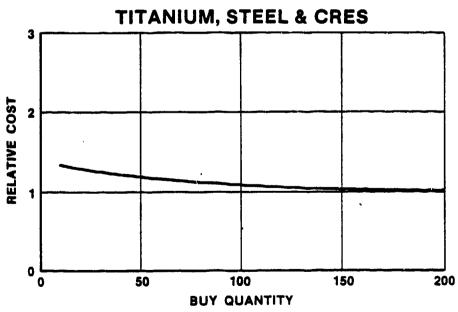




#### IMPACT OF BUY QUANTITY ON RECURRING COST OF CONVENTIONAL FORGINGS

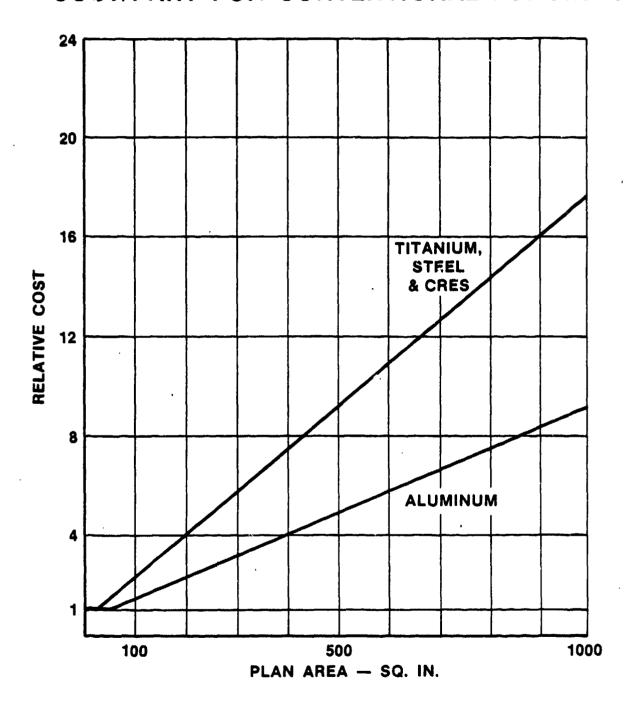


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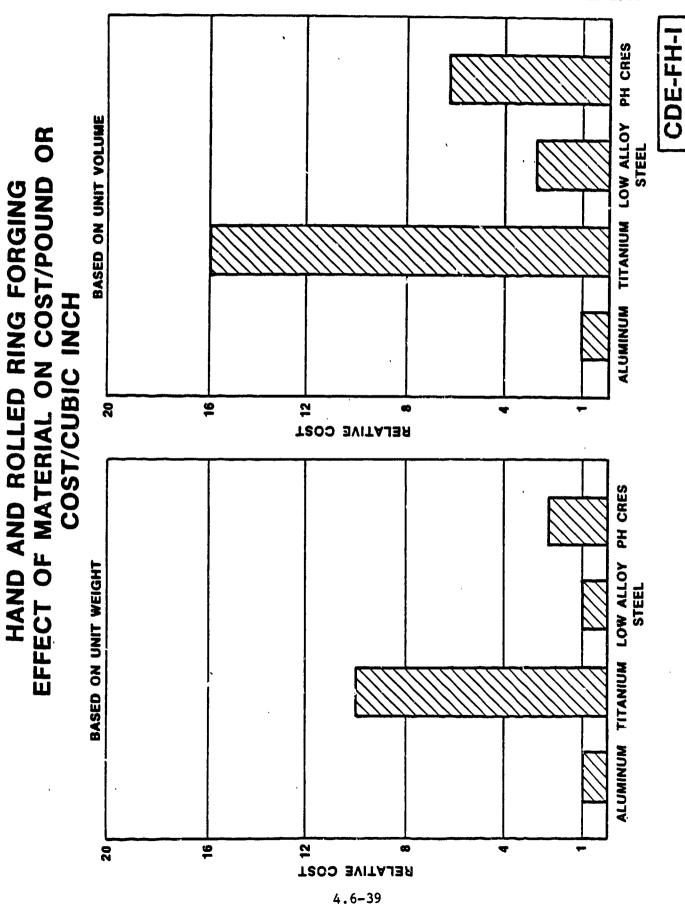
CDE-FC-VI

# IMPACT OF FORGING SIZE (PLAN AREA) ON THE SETUP COST/PART FOR CONVENTIONAL FORGINGS

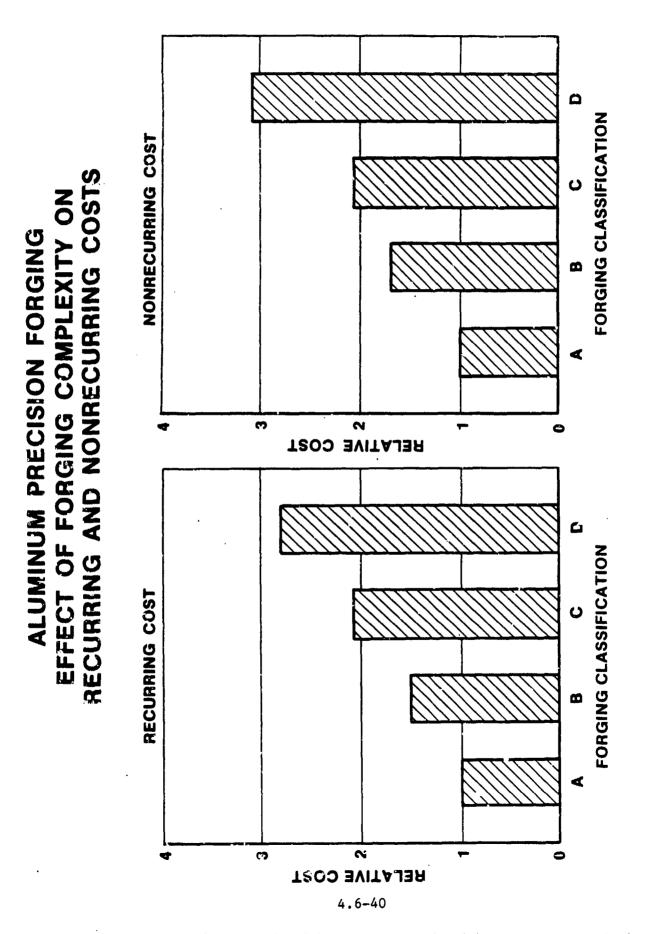


NOTE: BASED ON BUY QUANTITY OF 25

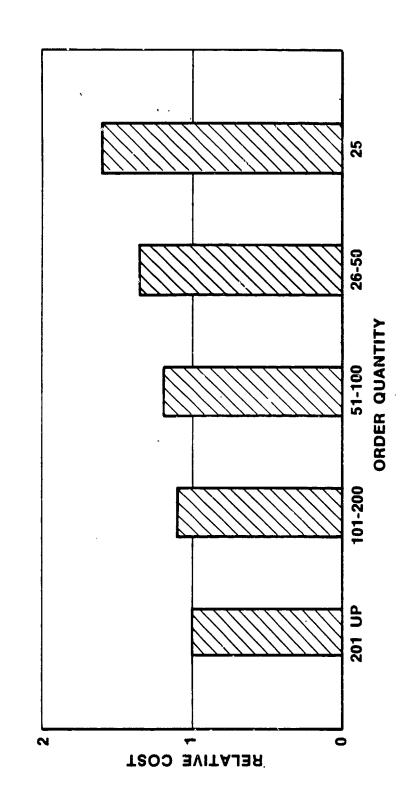
CDE-FC-VII



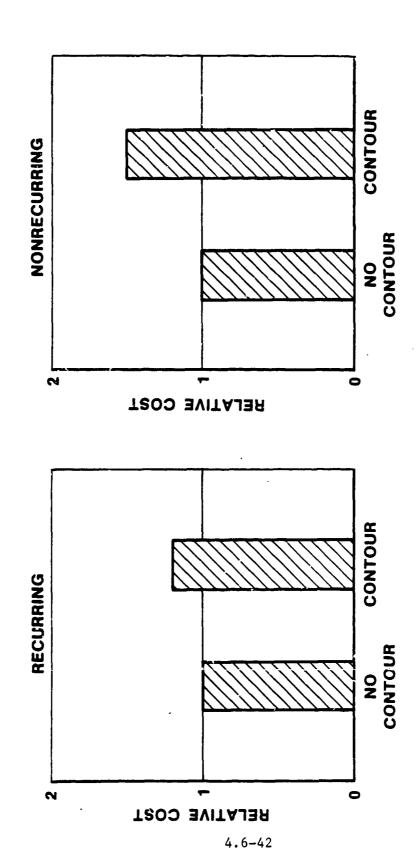
CDE-FP-I







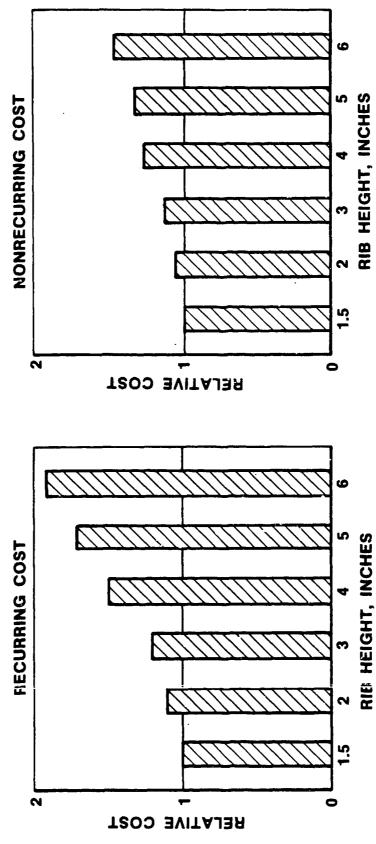




# EFFECT OF RIB HEIGHT ON RECURRING NONRECURRING COST ALUMINUM PRECISION FORGINGS

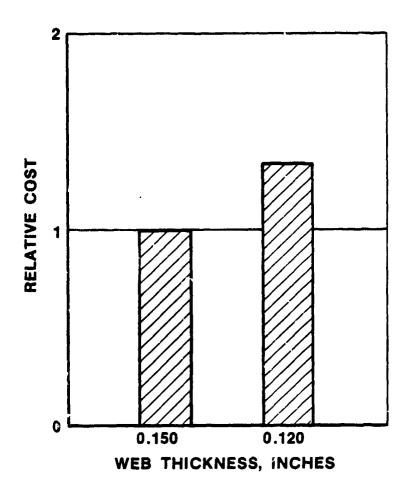
THE THE WORLD WINDS TO SELECT THE WORLD TO SELECT THE SELECTION OF THE SEL

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NOTE: BASEI) ON A 100 SQ. IN. CLASSIFICATION "D" FORGING

### ALUMINUM PRECISION FORGING EFFECT OF FORGED WEB THICKNESS ON RECURRING COST

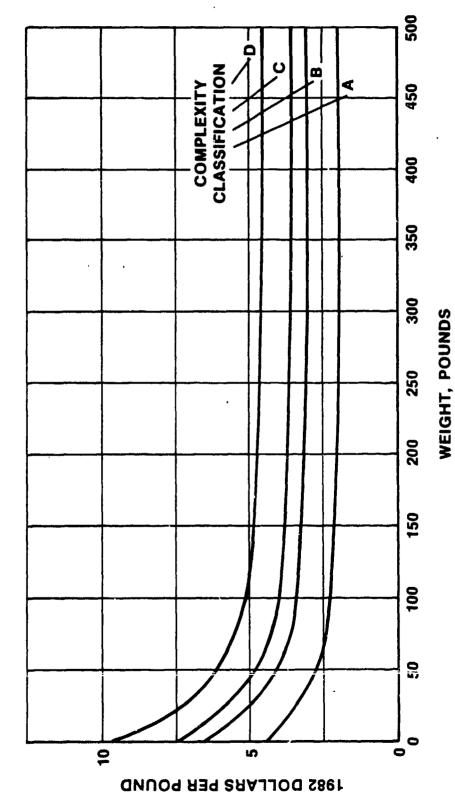


NOTE: BASED ON A 100 SQ. IN. FORGING

CDE-DICE-FP-III

CED-FC-1

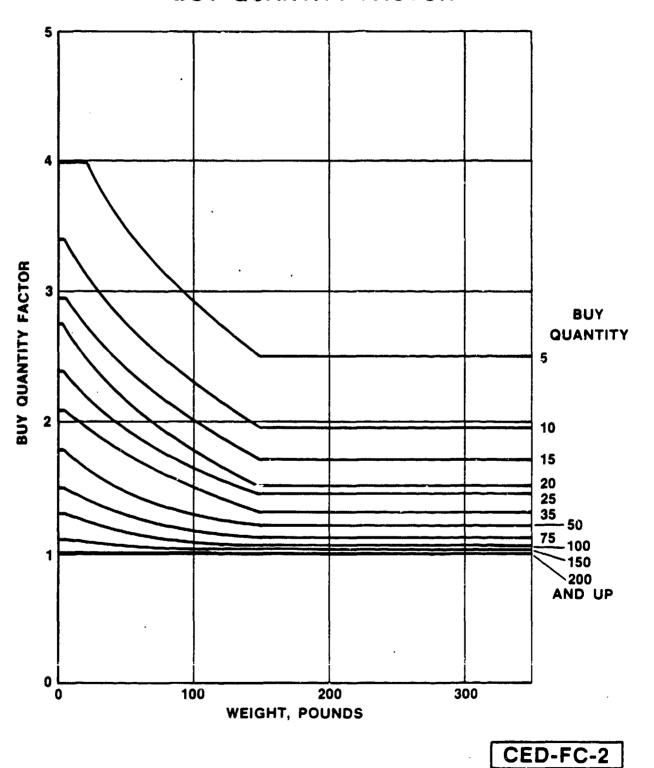
## **ALUMINUM CONVENTIONAL DIE FORGINGS BASE RECURRING COST**



NOTE: BLOCKER FORGING BASE RECURRING COST IS 80 PERCENT OF **CLASSIFICATION "A" BASE RECURRING COST.** 

**BASE RECURRING COST**, 54-9.7

### ALUMINUM CONVENTIONAL AND BLOCKER DIE FORGINGS BUY QUANTITY FACTOR



### ALUMINUM CONVENTIONAL AND BLOCKER DIE FORGINGS SETUP CHARGE PER LOT

SIZE	CHARGE/CLASSIFICATION			
	"A"	"B"	"C"	"D"
50 SQUARE INCHES & UNDER	200	200	250	300
51-100 SQUARE INCHES	350	400	450	500
101-250 SQUARE INCHES	600	700	700	800
251-499 SQUARE INCHES	900	1,000	1,000	1,200
500-999 SQUARE INCHES	2,000	2,400	2,800	3,100
1000-1999 SQUARE INCHES	3,500	3,500	3,700	3,700
2000 SQUARE INCHES & OVER	4,200	4,200	4,200	4,200

NOTE: FOR BLOCKER FORGING, USE SETUP CHARGE PER LOT FOR CLASSIFICATION "A"

CED-FC-3

### CED-FC-4

# ALUMINUM CONVENTIONAL AND BLOCKER DIE FORGINGS MONRECURRING TOOLING COST (NRTC)

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TO DETERMINE THE NONRECURRING TOOLING COST, UTILIZE THE FOLLOWING FORMULA:

[(L + 12)  $\approx$  (W + 12)  $\approx$  (T + 14)]  $\approx$  METHOD FACTOR  $\approx$  INFLATION FACTOR = NRTC

METHOD FACTORS

METHOD	FACTOR
BLOCKER	1
CONVENTIONAL	-
WITH FLATBACK	•
CONVENTIONAL	2

T = THICKNESS

L = LIENGTH W = WIDTH NOTE: INFLATION FACTOR TO BE SUPPLIED BY INDIVIDUAL USER COMPANY.

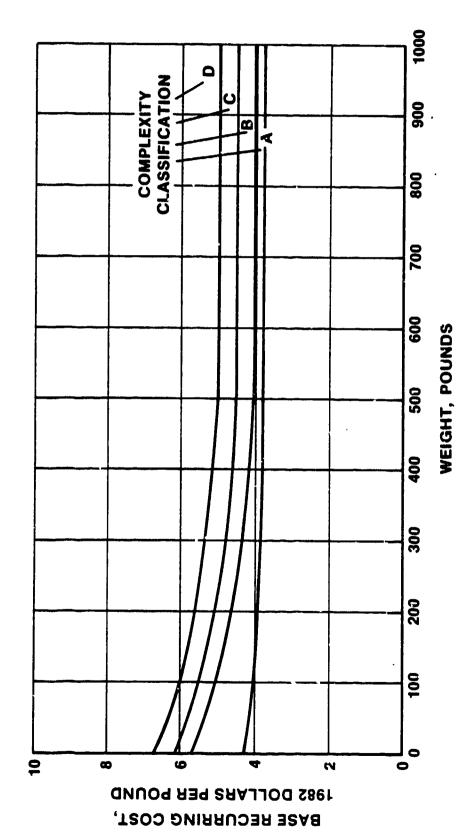
4.6-48

CED-FC-5 1,600 **○** TITANIUM 6AL-4V CONVENTIONAL DIE FORGING CLASSIFICATION O COMPLEXITY 906 8 ٧, 800 NOTE: BLOCKER FORGING BASE RECURRING COST IS 80 PERCENT OF 700 BASE RECURRING COST 8 **CLASSIFICATION "A" BASE RECURRING COST.** WEIGHT, POUNDS 200 **\$** 300 200 100 8 8 2 2 BASE RECURRING COST, 1982 DOLLARS PER POUND

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4340 STEEL CONVENTIONAL DIE FORGING **BASE RECURRING COST** 



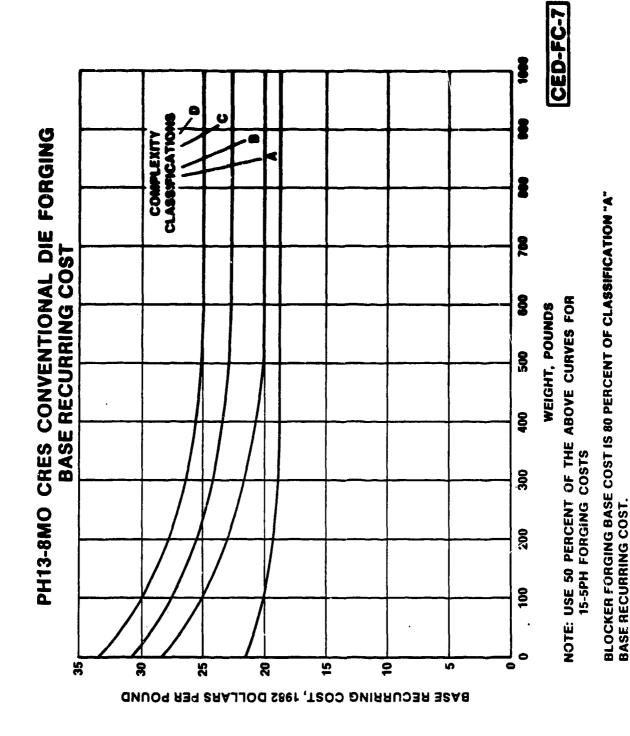
NOTE: THE CURVES REPRESENT VACUUM ARC MELT (VAR), FOR AIR WELT USE 50 PERCENT OF CURVES.

BLOCKER FORGING BASE RECURRING COST IS 80 PERCENT OF CLASSIFICATION "A" BASE RECURRING COST.

CED-FC-6

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# TITANIUM, STEEL AND CRES CONVENTIONAL/BLOCKER **DIE FORGING BUY QUANTITY**

FACTOR	1.0	1.1	1.2	1.25	1.35
QUÅNTITY	201	101-200	51-100	26-50	10-25

THE LISTED FACTORS ARE TO BE APPLIFD TO TITANIUM, STEEL AND CRES DIE FORGINGS BASED UPON THE BUY QUANTITY.

FOR EXTREMELY LARGE FORGINGS OVER 500 POUNDS, CONSULT DESIGN PRODUCIBILITY.

### TITANIUM, STEEL AND CRES CONVENTIONAL AND BLOCKER DIE FORGING SETUP CHARGE PER LOT

SIZE	CHARGE/CLASSIFICATION			
	"A"	"B"	"C"	"D"
25 SQUARE INCHES & UNDER	200	200	250	300
26-50 SQUARE INCHES	350	400	450	500
51-125 SQUARE INCHES	600	700	700	800
126-250 SQUARE INCHES	900	1,000	1,000	1,200
251-500 SQUARE INCHES	2,000	2,400	2,800	3,100
500-1000 SQUARE INCHES	3,500	3,500	3,700	3,700
1000 SQUARE INCHES & OVER	4,200	4,200	4,200	4,200

NOTE: FOR BLOCKER FORGINGS, USE CLASSIFICATION "A" SETUP CHARGE PER LOT.

CED-FC-9

## TITANIUM, STEEL AND CRES CONVENTIONAL NONRECURRING TOOLING COST (NRTC) **AND BLOCKER DIE FORGINGS**

TO DETERMINE THE NONRECURRING TOOLING COST, UTILIZE THE FOLLOWING FORMULA:  $[(L+12) \times (W+12) \times (T+14)] \times METHOD FACTOR \times INFLATION FACTOR = NRTC$ 

## METHOD FACTORS

1.5 1.5 WITH FLATBACK CONVENTIONAL CONVENTIONAL BLOCKER METHOD

T = THICKNESS

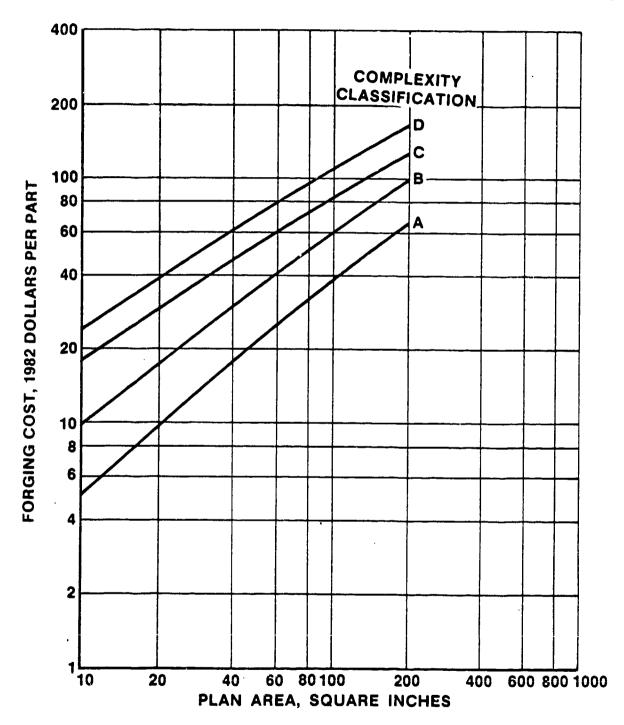
L = LENGTH W = WIDTH

WHERE

FACTOR

NOTE: INFLATION FACTOR TO BE SUPPLIED BY INDIVIDUAL USER COMPANY.

### ALUMINUM PRECISION FORGING BASE PART COST



CED-FP-1

### ALUMINUM PRECISION FORGINGS QUANTITY FACTOR

ORDER QUANTITY	FACTOR
10 TO 25	1.6
26 TO 50	1.35
51 TO 100	1.2
101 TO 200	1.1
201 UP	1.0

NOTE: IF ORDER QUANTITY IS NOT KNOWN, USE 1.35.

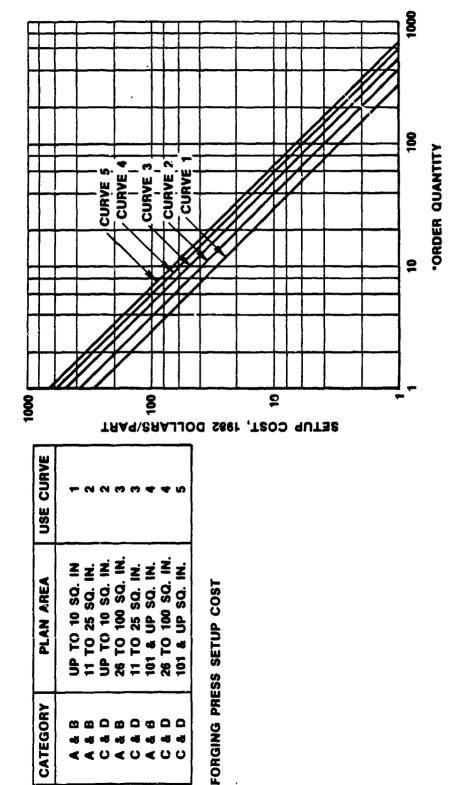
CED-FP-2

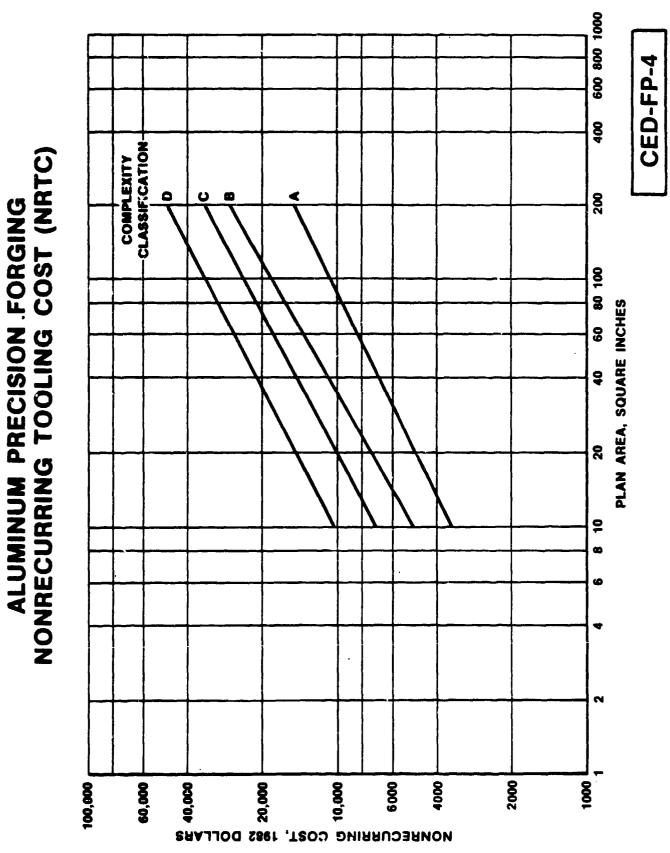
CED-FP-3

ALUMINUM PRECISION FORGINGS SETUP COST

THE PARTY OF THE P

(1)





### ALUMINUM PRECISION FORGING RECURRING COST DICE FACTOR

DESIGN FEATURE		DICE FACTOR
WEB THICKNESS		
PLAN AREA	WEB THICKNESS	
UP TO 50 SQ. IN.	0.120	-
	0.090	1.3
51 TO 150 SQ. IN.	0.150	-
	0.120	1.3
151 TO 200 SQ. IN.	0.180	-
	0.150	1.3
RIB	HEIGHT	
UP TO 1.50		_
1.51 TO 2.00		1.1
2.01 TO 3.00	]	1.2
3.01 TO 4.00		1.5
4.01 TO 5.00		1.7
5.01 TO 6.00		1.9
SPECIAL	CONDITIONS	
LOFT CONTOUR		1.2
CYLINDRICAL CONTOUR		1.2
GRAIN DIRECTION		1.2
ANGLES OTHER THAN 90 DEGREE TO BASE		1.2

NOTE: IF MORE THAN ONE (1) DESIGN FEATURE IS APPLICABLE, USE ONLY THE HIGHEST.

DICE-FP-1

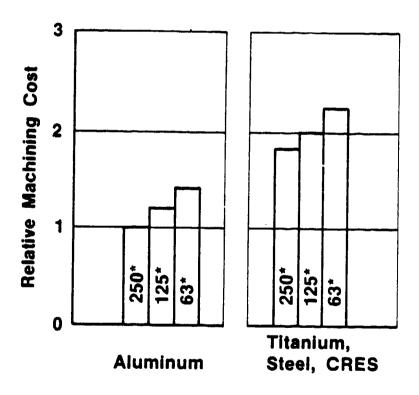
### ALUMINUM PRECISION FORGING NONRECURRING COST DICE FACTOR

DESIGN FEATURE	DICE FACTOR
RIB HEIGHT	
UP TO 1.50	
1.51 TO 2.00	1.05
2.01 TO 3.00	1.10
3.01 TO 4.00	1.25
4.01 TO 5.00	1.35
5.01 TO 6.00	1.45
LOFT CONTOUR	1.50

NOTE: IF MORE THAN (1) DESIGN FEATURE IS APPLICABLE USE ONLY THE HIGHEST.

DICE-FP-2

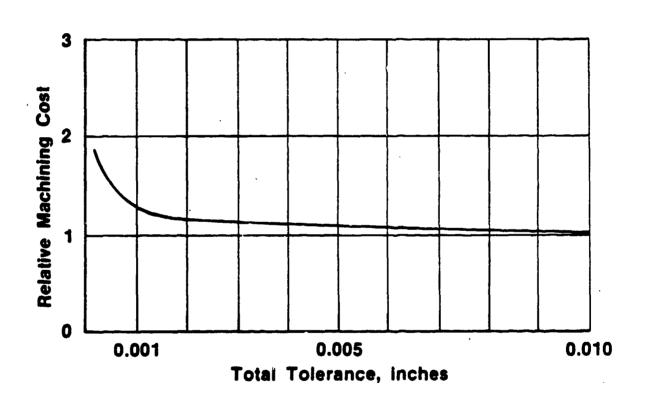
### MACHINING OF FORGINGS SURFACE FINISH COST-DRIVER EFFECT



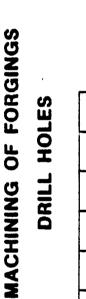
\*Surface finish shown in micro-inches.

CDE-FM-I

### MACHINING OF FORGINGS— DIMENSIONAL TOLERANCES COST-DRIVER EFFECT



CDE-FM-II

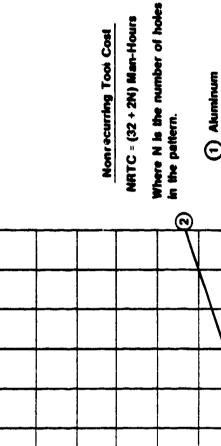


0.14

0.12

0.10

Ü



1 Akuminum
2 Thenkum,
Steel, CRES

Hole Diameter, Inches

8.

0.50

0.25

0.02

9.6

Cost data is valid for hole depths up to twice the hole diameter.

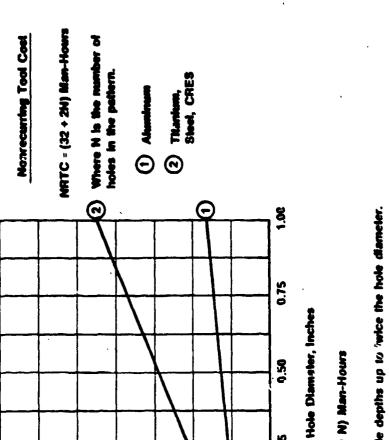
Cost/Part = (Cost/Hole • N) Man-Hours

CED-FM-1

90.0

90.0

Cost/Hole, Man-Hours



DRILL AND SPOTFACE HOLES

9.16

0.14

0.12

9.16

MACHINING OF FORGINGS

以为为<u>有</u>国际的分别基础的各种基础的分别基础的分别

Cost/Part = (Cost/Hole • N) Man-Hours

Cost date is valid for hole depths up to hwice the hole diameter.

0.02

Z

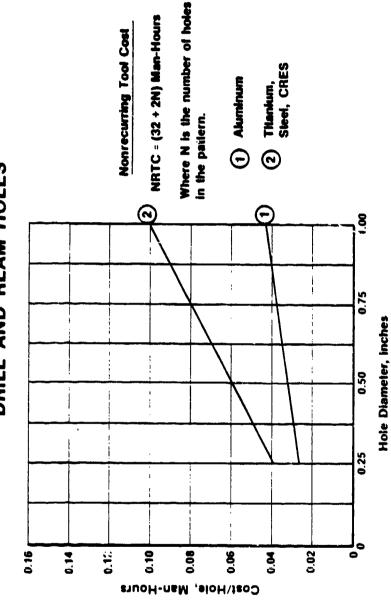
8

8

Cost/Hole, Man-Hours







Cost/Part = (Cost/Hole • N) Man-Hours

Cost data is valid for hole depths up to twice the hole diameter.

.;

### MACHINING OF FORGINGS FACE MILLING



NRTC = 57 Man-Hours

Nonrecurring Tool Cost

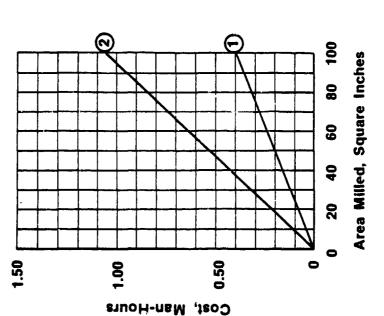
(1) ALUMINUM

(2) TITANIUM, STEEL, CRES Step 1 — Determine the face milling cost for each surface machined.

Step 2 — Add the milling costs obtained in Step 1.

Step 3 — Obtain NRTC above.

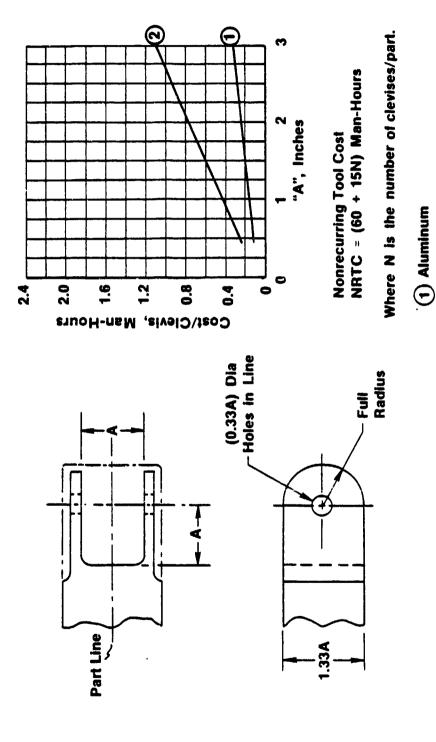




CED-FM-5

2) Titanium, Steel, CRES

MACHINING OF FORGINGS STRADDLE MILL, DRILL & REAM



### 4.6.5 Ground Rules for Forging Section

The following General and Detailed Ground Rules for the Forging Section were developed to establish the scope of the data required and to establish guidance to MC/DG application. Ground rules are necessary and important as they promote understanding, ensure consistency, uniformity, and accuracy in generating and integrating data into the formats.

### 4.6.5.1 General Ground Rules

The General Ground Rules are categorized under the following major groups:

- (a) Forging Types
- (b) Materials
- (c) Forging and Applicable Machining (Limited)
- (d) Machining
- (e) Facilities
- (f) Data Generation Recurring Costs (including Forging TI&E)
- (g) Forging TI&E Recurring Costs
- (h) Data Generation Nonrecurring Costs (including Forging TI&E)
- (i) Support Function Modifiers
- (j) Test and Evaluation of Data.

### (a) Forging Types

- (1) The forging types selected will be representative of parts commonly required for both small and large aircraft. The parts will be selected such that a base part forms the foundation from which the desired discrete part can be fabricated.
- (2) The forgings will be selected, where possible, to develop data for more than one forging method. The data thereby enable the designer, using the MC/DG, to perform a tradestudy to evolve the most cost-effective discrete part.
- (3) The selected forgings will adequately display, by CED and CDE formats, the effect on cost of DICE.

### (b) Materials

- (1) The materials selected for the forged parts will be those commonly used in the industry to enable a uniform data base to be established. The materials included are:
  - Aluminum

- Titanium
- Steel.

### (c) Forgings and Machining

- (1) Only conventional forging processes and TI&E methods will be considered. No emerging manufacturing methods will be evaluated.
- (2) A production, in contrast to a prototype environment, will be assumed for the forged parts.
- (3) To generate an effective data base for each selected part, a factory operational sequence utilized by the user will be established reflecting the most economical means of fabrication of the final part. This standardized sequence will be used by each team member to determine the part cost.

### (d) Machining

(1) Limited machining data, as reflected in the MC/DG section on machining of castings, will be utilized for the forging section.

### (e) Facilities

- (1) Only standard manufacturing and TI&E facilities, will be considered.
- (f) Data Generation Recurring Costs
  - (1) Recurring cost data will be generated for the raw forging types being considered, and will include TI&E and mechanical property verification.

    4.6-69

- (2) Data will be generated separately for aluminum blocker, conventional, and precision forgings and titanium and steel blocker, and conventional forgings. Data to be based on plan area using historical data of the team airframe companies. Hand and ring forging cost methods will be developed.
- (3) The DICE elements will be treated as separate cost elements, and therefore, not included in the base-part cost, but will be displayed using CED and CDE formats.
- (4) In-house recurring tooling costs (tool maintenance, tool planning, etc.) will not be included.
- (5) The quantity for which the base part and the DICE costs will be determined is at unit 200. A lot release size of 25 will be applied.
- (6) The data submitted to BCL will be the raw forging part cost (dollars) plus the DICE incremental factors associated with the discrete forging design.
- (7) In developing the cost data for parts, each participating company may utilize its own proprietary improvement curves.
- (8) The base part and DICE costs will be normalized by BCL to reflect an industry average value.
- (9) For proprietary reasons, business sensitive information employed at team member contributing companies to determine the data, will not be presented in the MC/DG.
- (10) No data provided by any team member will be disclosed to other team members, agencies, or to the public without the expressed approval of the team member.

### (g) Forging - TI&E Recurring Costs

- (1) The applicable ground rules for data generation for forgings will be applied to the TIEE recurring cost.
- (2) Recurring cost data will be generated for TI&E functions required from the supplier to receiving stores, including outside laboratories.
- (3) TIEE cost data for the raw forging only will be included.

- (4) Costs will be presented in 1982 dollars.
- (5) CED and/or CDE formats will display the following TI&E costs and data, when applicable, to provide meaningful cost data to the designer:
  - Penetrant Inspection
  - Ultrasonic Inspection
  - Magnetic Particle Inspection
  - Mechanical Properties Verification
  - Chemistry Verification
  - Dimensional Inspection.
- (6) TI&E cost data will be normalized by BCL to reflect an industry team average value.
- (h) Data Generation Nonrecurring Costs for Raw Forgings and TI&E
  - (1) Tooling costs will be generated for each part type. TI&E fixture costs will be the responsibility of the user company where applicable.
  - (2) The cost of production tooling will be restricted to contract or project tools only for presentation in the MC/DG.
  - (3) First article TI&E cost will be generated and displayed as part of the nonrecurring tooling cost.
  - (4) Nonrecurring tooling costs (NRTC) generated by the team companies will be normalized by BCL for presentation in the MC/DG.
- (i) Support Function Modifiers

(1) Additional effort other than factory labor and TI&E, i.e., planning and tool maintenance, will be excluded from the part cost data supplied to BCL. Other modifiers may be included later by the MC/DG users at airframe companies.

### (j) Test and Evaluation of Data

(1) Test and confirmation of the formats and integrated data will be accomplished by one of the MC/DG team members. Each of the remaining team members will be provided with the evaluation. Any anomalies will be resolved and modifications incorporated as appropriate.

### 4.6.5.2 Detailed Ground Rules

The detailed ground rules are categorized under the following major groups:

- (a) Forging Types
- (b) Materials
- (c) Data Generation Recurring Costs
- (d) Data Generation Nonrecurring Costs
- (e) TI&E Functions

### (a) Forging Types

- (1) Each team member will review applicable forging designs and tabulate required data on the data collection sheets developed by the team.
- (2) Selected typical designs will be utilized for determination of user-associated costs (e.g., machining).
- (3) The forgings analyzed by each team member will be classified by material and type. This classification will be designated on the data collection form submitted to BCL. Each team member company will submit drawings or sketches to BCL illustrating their understanding of these forging types.

### (b) Meterials

(1) The materials and processes selected for the following forging types are:

### Aluminum

- 7075 or equivalent hand, ring, blocker, conventional die, and precision forgings.

### • Titanium

- Ti-6Al-4V annealed hand, ring, blocker, and conventional forging.

### • Steel

- 4340 or equivalent hand, ring, blocker and conventional forging.

### (c) Data Generation - Recurring Costs

- (1) Data indicated on the data collection sheet will be gathered, as available, for the raw forging. TI&E costs associated with the raw forging will be established separately.
- (2) Machining cost data previously developed for castings for the basic machining parameters listed below, will be reviewed for applicability to forgings. TI&E costs for the user operations will not be included as a part of this task.
  - (a) Counter-bore and face-hub
  - (b) Drilled holes, drilled and reamed holes, drilled and spot-faced holes
  - (c) Circular-flange facing (lathe), flat-faced (mill)
  - (d) Stradle-mill and drill-clevis fittings.
- (d) Data generation Nonrecurring Costs for Raw Forgings and TI&E
  - (1) Tooling costs will be generated for each part type. TI&E fixture costs will be the responsibility of the user company where applicable.

### (e) TI&E Functions

- (1) The following are typical TI&E operations that will be evaluated for cost impact:
  - e Chemistry

- Mechanical Properties
  - Separate test bars
  - Coupons from forgings (prolongation)
  - Dissected forgings
- Dimensional
- Ultrasonic · ·
- e Penetrant/Magnetic.