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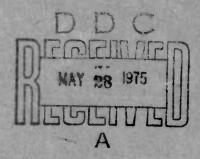
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EVALUATION TEST OF RADAR CHRONOGRAPH SET, NM87

ADB004019

December 1974

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Fire Control Development & Engineering Directorate

U.S. ARMY ARMAMENT COMMAND
FRANKFORD ARSENAL
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18. SUPPLEMENTARY NOTES

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Radar Chronograph Muzzle Velocity Measurements Velocimeter

20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The Norwegian Radar Chronograph Set, NM87 was evaluated by Frankford Arsenal from November 1972 through March 1974 to determine the capability of the NM87 to chronograph standard cannon artillery.

The NM87 was subjected to laboratory, environmental, and firing tests. From the results obtained to date, it is concluded that this chronograph is simple to operate, reliable, requires little maintenance,

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20. Abstract (cont.)

and is capable of the same order of precision as is possible with the M36 Radar Chronograph Set which is the item currently used for muzzle velocity measurements.

Report indicates some limitations and recommends improvements for utilization of the equipment.

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#### INTRODUCTION

The evaluation of the NM87 Radar Chronograph was authorized under PSTC Project #3-220132. The project was initiated as part of the Foreign Materiel Program to acquire sufficient test data to evaluate the operational performance, reliability, maintainability, and durability of the NM87 Radar Chronograph under actual tactical conditions.

### DESCRIPTION OF MATERIEL

The Radar Chronograph Set, Mera Bergen Model NM87, is designed to measure the muzzle velocity of field artillery weapons under actual tactical conditions. The NM87 consists of the following items:

Doppler Radar (Figure 1)
Chronograph (Figure 2)
Cable Reel Assembly (Figure 3)
Mounting Set
Transport Case

The doppler radar unit houses the transmitter/receiver, and is normally mounted directly on the gun carriage. The chronograph unit incorporates the logic circuits, the numeric display, the power distribution circuits, and all operational controls. The cable reel assembly consists of two cables; one cable is used for battery connection and one cable for power and signal transmission to the doppler radar and the chronograph.

The mounting set consists of brackets with necessary supports and screws to mount the doppler radar to the gun/carriage.

The transport case houses all the above mentioned items with the exception of the cable reel assembly.

The doppler radar transmits continuous power on a wavelength of approximately three centimeters. The radar beam is transmitted along the trajectory of the projectile by means of a parabolic antenna. When the projectile leaves the muzzle and enters the radar beam, some of the transmitted power is reflected and detected in the receiver. By counting doppler periods between transmission and reception of reflected radar emissions, the position of the projectile is determined independent of the velocity. After 2176 doppler periods (corresponding to a trajectory of 35 meters), an electronic gate is opened for a duration of 128 doppler periods (corresponding to a base length of 2 meters). During this time, the flight time of the projectile is measured and is presented in 1/4 microsecond units on a 5-digit numeric display. By means of conversion tables, the displayed reading is converted to velocity at the muzzle in meters/second.

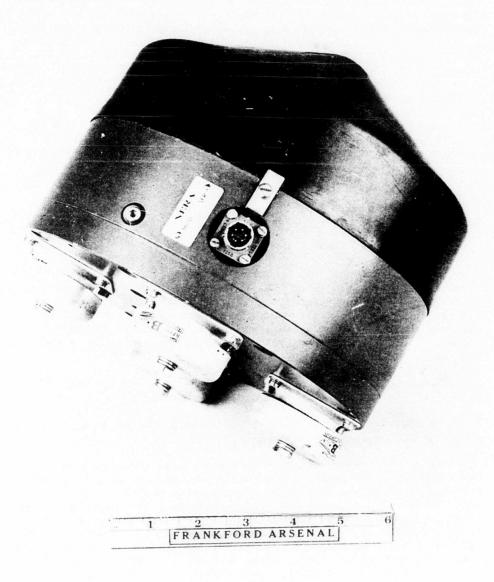


Figure 1. Radar Chronograph NM87, Doppler Radar

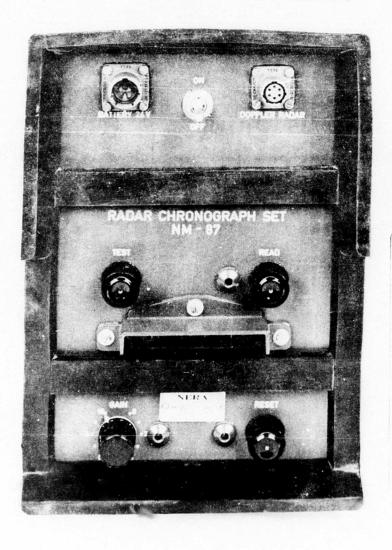


Figure 2. Chronograph NM87, Chronograph



Figure 3. Radar Chronograph NM87, Cable Reel Assembly

### **EVALUATION OBJECTIVES**

The objective of the evaluation program described herein was:

- a. Evaluation of the electrical and mechanical features of the NM87 Chronograph to determine whether it can be handled, operated, and maintained sefely by operating personnel in a field artillery environment.
- b. Eveluation of reliability, durability, and mainteinability of the NM87 Chronograph under actual tactical conditions, including exposure to ambient field conditions, the shock of repeated firings, and the ease or difficulty experienced in assembly and disessembly of the test item for firing tests.
- c. Comparison with other muzzle velocity meesuring devices in terms of advantages and disadvantages, state-of-the-art, end potential for savings in operation.

### RESULTS OF EVALUATION TEST PROGRAM

The NM87 is easy to install, simple to operate, rugged, reliable, and requires little maintenance. Its functional performance complies with the specification requirements furnished by the manufacturer.

It was not possible to design a firing test which would demonstrate the accuracy of the NM87. However, a series of firing tests were conducted which constituted an adequate performance demonstration. From the firing test data, inferences were drawn with regards to the precision of measurement, namely, that there is no indication of any statistically significant differences in precision between the NM87 and the other muzzle velocity measurement devices tested with standard weapon projectile combinations. Test data also revealed that the NM87 does not have the capability to reliably measure the muzzle velocity of 8-inch RAP projectiles fired at charge 9.

Our results relative to the precision of the NM87 were confirmed by the U.S. Army Ballistic Research Laboratories. The data gathered by Frankford Arsenal during this test were presented to the BRL for analysis. The data were analyzed in accordance with the methodology adopted by the U.S. and other NATO nations as the most efficient and unbiased means of estimating and comparing relative chronograph performance when two or more instruments are used to make simultaneous measurements of gun muszle velocities. It must be pointed out that the data reduction process did not include corrections for the recoil velocity of the doppler radar when it was mounted on the weapon.

### DETAILS OF EVALUATION TEST

### Introduction

The NM87 Radar Chronograph Set was tested in accordance with the evaluation schedule contained in Appendix A. Most of the criteria shown in this report were extracted from the supporting documents furnished by the manufacturer. Where no specific criteria were available, the ones used were based on experience and knowledge in the testing of similar types of items.

Upon receipt of the test item in November 1972, inspection and laboratory performance tests were conducted. At the conclusion of the laboratory tests, trial chronographings were conducted on various weapon ammunition combinations. All major adjustments, repairs, and modifications were performed by Frankford Arsenal personnel.

Most of the environmental tests were conducted at Frankford Arsenal. However, some environmental phases of the test were conducted concurrently with the firing accuracy tests. All testing on this program was completed in March 1974.

Discrepencies observed during the conduct of the evaluation program were reported to Frankford Arsenal by telephone, test reports, and equipment performance reports.

### Physical Characteristics

The test item and its accessories were visually inspected for workmanship and mechanical operability.

The test item was measured and weighed. The results were compared with the manufacturer's specified values. The complete weights and measurements are given in Table I.

All markings were visually inspected and found to meet the requirements of Standard MIL-STD 130.

It is possible to interchange component assemblies of the NM87 Chronograph with other radar chronograph sets. This was done during firing tests at Yuma Proving Ground in March 1974.

### TABLE I. Radar Chronograph, NM87 Weights and Measurements

### Doppler Radar (Figure 1)

| Weight28.5   | pounds |
|--------------|--------|
| Diameter 8.7 | inches |
| Depth 9.0    | inches |

### Chronograph (Figure 2)

| Weight 8.0 | pounds |
|------------|--------|
| Length10.6 | inches |
| Width 7.5  |        |
| Height 4.1 | inches |

### Cable Reel Assembly (Figure 3)

| Weight26.5 | pounds |
|------------|--------|
| Length14.4 | inches |
| Width12.6  |        |
| Height15.9 | inches |

### Transport Case W/E

| Weight84.0 | pounds |
|------------|--------|
| Length21.0 | inches |
| Width13.0  |        |
| Height15.0 | inches |

### Circuit Description

Refer to Block Diagram Figure 4.

The Gunn Oscillator generates a signal with a nominal frequency of 9525 MHz and an output power of approximately 20mW. The signal is fed via the circulator and the antenna elements to the antenna. The parabolic antenna directs the transmitter power in a narrow beam into the projectile trajectory.

A small part of the transmitter power is reflected because of mismatch in the antenna element and fed via the circulator to the frequency mixer. The reflected power is thus used as a local oscillator signal. The signal reflected from the projectile has its frequency changed due to the velocity of the projectile. This signal is below that of the transmitted frequency and the frequency difference, fd, is

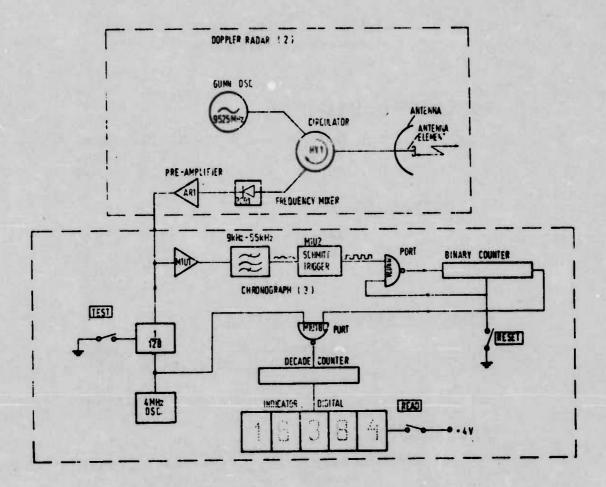


Figure 4. Radar Chronograph NM87, Block Schematic Diagram

given by Doppler's equation:

$$fd = \frac{2V}{\lambda}$$

where V = velocity of projectile

 $\lambda$  = wavelength of transmitted signal

The reflected signal is fed to the frequency mixer via the antenna, the antenna element, and the circulator.

In the frequency mixer, the reflected signal is mixed with the local oscillator signal. The output is a signal with a frequency

equal to the difference between the transmitted frequency and the reflected frequency. This signal is amplified in the preamplifier and then transmitted to the chronograph. Here, the signal is further amplified and fed via a band-pass filter to the Schmitt Trigger. The output of the Schmitt Trigger consists of square wave pulses with constant amplitude.

The square wave pulses are connected to a gate and then to a binary counter. After a preset number of pulses are counted, a gate (MIUISC), is opened and 1/4 microsecond clock pulses from the 4MHz oscillator are fed to the decade counter.

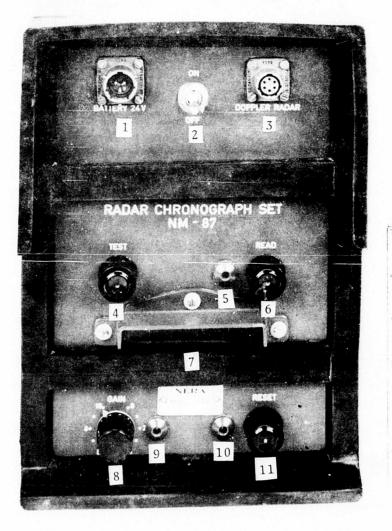
After a time determined by the duration of a predetermined number of doppler pulses, the gate is closed. The number of 1/4 microsecond pulses fed to the decade counter during this time interval, can be read on the 5-digit numeric indicator when the READ push button is depressed.

A control circuit is incorporated to check the operation of the chronograph. When the TEST push button is depressed, a simulated doppler signal is fed to the input amplifier of the chronograph. If the radar chronograph set is functioning correctly, the control signal generates a reading of 16348 ± 1 on the numeric indicator.

### Operator's Controls and Indicators

The numbers are referred to Figure 5.

- a. BATTERY 24V(1). Connector for connection of the power cable.
  - b. ON-OFF (2). Combined power switch and circuit breaker.
- c. DOPPLER RADAR (3). Connector for connection the signal and power cable between the doppler radar and the chronograph units.
- d. TEST (4). Push button switch which applies an internal simulated doppler signal to the input of the chronograph.
- e. READ indicator (5). Lit when information is stored in the register and is extinguished when the RESET button is pressed.
- f. READ (6). When this push button is pressed, the numeric display will display the information stored in the register.



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Figure 5. Radar Chronograph NM87, Operator's Controls and Indicators

- g. NUMERIC (7). Presents a 5-digit reading of the registered time interval. It is activated when the READ button is pressed.
  - h. GAIN (8). Potentiometer for adjustment of the gain.
- i. NOISE (9). Flashes for each noise or signal pulse which is received.
- j. RESET (10). Lit to indicate that the set is ready for operation and is extinguished when a reading is obtained or when one or more noise pulses are received.
- k. RESET (11). Push button is pressed to make the set ready for operation. It is pressed just before the shot is fired.

### Electrical Characteristics

The electrical performance characteristics of the NM87 were measured in accordance with the test methods and procedures delineated in Military Specification MTL-C-14816. This specification covers the performance requirements of the USA Standard M36 Radar Chronograph Set. The results were compared with the specific characteristics of the manufacturer's (NERA Bergen) documentation furnished with the equipment.

The electrical characteristics are given in Table II.

### Continuous Operation Test

The NM87 was set up in the normal operating mode. An operational test, relative power, and frequency test of the system performance was made and the results recorded. The chronograph was operated continuously eight hours a day for a period of five days. Performance tests were conducted periodically and the results compared with the initial test results. No failures, erratic readouts, or degradation of performance were observed during the continuous operation test.

### Safety Inspection

As configured, the NM87 presents no electrical or mechanical hazards to operating personnel. However, mounting the doppler radar, Figure 1, on the 155 MM M109, the 8-inch M110, and the 175 MM M107 in

### TABLE II. Radar Chronograph, NM87 Electrical Characteristics

### DOPPLER RADAR

Frequency
Output power
Antenna gain
Antenna beamwidth
Antenna polarization
Receiver sensitivity

9525 MHz 20mW 22dB 10° Vertical -88dBn

### CHRONOGRAPH

Velocity range Clock frequency Display 150 - 850 meter/second 4MHz 5-digit (solid state)

### POWER

Battery voltage Power consumption 24 volt Approximately 20W

accordance with the manufacturer's instructions constitutes a safety hazard to personnel (strain or rupture). This was confirmed by personnel of the Human Factors Engineering Division at Frankford Arsenal.

The doppler radar, which is removed as one unit, weighs 28.5 pounds. Two men are required to grasp and hold the doppler radar unit when mounting and setting up the equipment for operation. This places them in an awkward and unsafe position and is particularly hazardous if footing is unsure.

### Firing Tests

Firing tests were conducted at the U.S. Army Artillery Board, Fort Sill, OK during July and August 1973. The primary objective of this firing test program was to determine the capability of the NM87 to chronograph standard cannon artillery.

The NM87 was set to measure projectile velocities at 35 meters from the muzzle. The doppler radar was mounted on the 155 MM Howitzer, M109 as specified by the manufacturer. The rounds from the 105 MM Howitzer, M102 were chronographed with the doppler radar unit mounted on a tripod. To install the doppler radar on the 175 MM Gun M107 and the 8-inch Howitzer M110, a special mounting bracket was fabricated at Frankford Arsenal, see Figure 6. The radar chronograph set was mounted on these weapons as illustrated in Figure 7.

A summary of the firing data for 25 weapon/ammunition combinations fired at Fort Sill is presented in Table III. The displayed readouts obtained from the NUMERIC DISPLAY were converted to velocity (m/s) through the use of the conversion tables furnished with the Operator's Manual, TM 11-5 840 25/200-12.

Based on the number of rounds fired (501), the usage factor and the number of rounds successfully chronographed as shown in Table IV, the overall performance of the set is considered satisfactory.

The evaluation of the NM87 performance was made by comparison among three different muzzle velocity measuring systems (M36, MVR-103, and XMR). The instrumented technical data acquired at the test site were recorded on magnetic tape for use in subsequent analysis and to serve as a permanent record of the test firing.

The data used for analysis was derived from the FADAC computer which had been programmed to compute "normalized" muzzle velocity. This was accomplished by modifying the Cannon FADAC program to accept CHRON DELAY inputs in milliseconds instead of entering the delay gate setting as is normally done for the Radar Chronograph M36 (U.S. Army Standard) muzzle velocity extrapolation routine. All meteorological and ballistic data that affect the trajectory were also entered into the computer. The program scheme uses an automatic successive approximation procedure to adjust the stored muzzle velocity obtained from the test items until the computed quadrant elevation is equal to the input quadrant elevation.

The BRL analysis of the data is presented in Appendix B. A summary of some of the terms found in these data is contained on pages 3 and 4 of Appendix C.

An attempt by Rock Island Arsenal personnel to measure the projectile velocity of 8-inch RAP rounds (XM650E3) when fired at charge 9 utilizing the NM87, was unsuccessful during the week of 18 March 1974 at Yuma Proving Ground. The cause of failure was considered to be the fire ball associated with the XM650E3 projectile when fired at charge 9. The tube used for firing these rounds does not have a muszle brake. Therefore, the fire ball, instead of being thrown out sideways, is sucked behind the airborne projectile. The fire ball

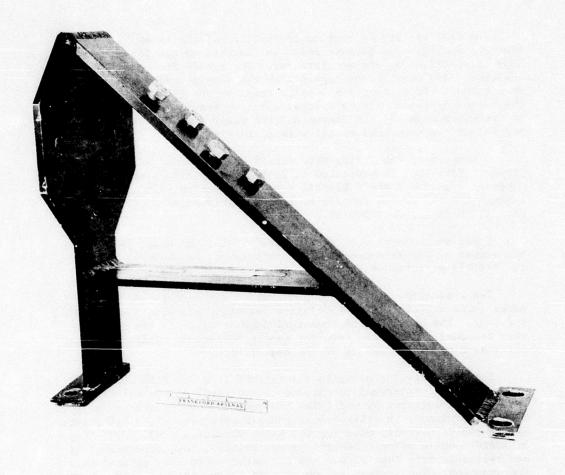


Figure 6. Radar Chronograph NM87, Special Mounting Bracket

appears as an extension to the projectile rear (the radar beam normally reflects off the projectile rear). Therefore, until the fire ball dissipates, the NM87 doppler radar had a very poor reflective target.

In order to investigate this theory, the doppler signal from the NM87 was simultaneously fed to both the signal processing section of the NM87 and to a Frankford Arsenal developed signal processing unit. This was accomplished by sampling the doppler signal from the unit, refer to Figure 4, and feeding it to the Frankford Arsenal processor. Utilizing this configuration, a firing test consisting of 15 rounds of the XM650E3 projectile, fired at charge 9, was conducted on 29 March 1974 at Yuma Proving Ground.

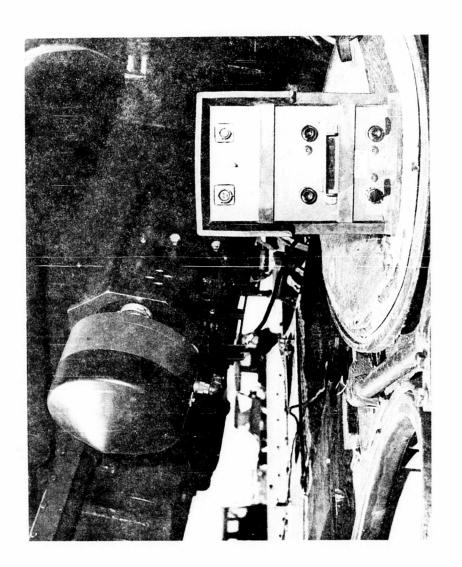


Figure 7. Installation of Radar Chronograph Set, NM87 on the 8-inch Howitzer M110

TABLE III. Radar Chronograph, NM87 Firing Data Summary Sheet

| WEAPON           | ZONE   | ROUN<br>FIRED | DS<br>RECRD | MEAN<br>VELOCITY<br>(m/s) | NOTE       |
|------------------|--------|---------------|-------------|---------------------------|------------|
| 105MM Howitzer,  | 1      | 22            | 22          | 184.6                     |            |
| M102             | 4      | 19(1)         | 19          | 269.8                     |            |
| M102             | 5      | 20(2)         | 20          | 316.2                     |            |
|                  | 7      | 5             | 5           | 485.2                     |            |
|                  | 7(RAP) | 9             | 2           |                           | A          |
| 155MM Howitzer,  | 1      | 20            | 20          | 200.1                     | В          |
| M109             | 3 G    | 20            | 20          | 277.1                     |            |
| MIUS             | 4 G    | 20            | 17          | 316.7                     | C          |
|                  | 5 G    | 20            | 20          | 371.5                     |            |
|                  | 3 W    | 20            | 20          | 281.4                     |            |
|                  | 4 W    | 20            | 20          | 321.9                     |            |
|                  | 5W     | 30            | 30          | 378.1                     |            |
|                  | 6W     | 19(2)         | 19          | 463.4                     | S) Its Int |
|                  | 7 W    | 19(3)         | 18          | 563.6                     | D          |
|                  | 7(RAP) | 4(3)          | 4           |                           | E          |
| 175MM Gun, M107  | 1      | 25            | 24          | 501.7                     | F          |
| 275              | 2      | 25            | 25          | 704.2                     | G          |
|                  | 3      | 30            | 30          | 915.6                     | Н          |
| 8-inch Howitzer, | 2      | 20            | 20          | 270.5                     |            |
| M110             | 3      | 20            | 20          | 303.9                     |            |
|                  | 4      | 19(3)         | 19          | 346.3                     |            |
|                  | 5 G    | 20(1)         | 20          | 415.7                     | I          |
|                  | 5 W    | 20            | 20          | 420.5                     |            |
|                  | 6 W    | 20            | 20          | 500.5                     |            |
|                  | 7 W    | 20            | 20          | 594.1                     |            |

### Notes:

The following comments disregard those rounds which were missed because of operator shortcomings such as:

- (1) ( .IN control not adjusted before firing .
- (2) Equipment not turned on or no input power.(3) Failure to reset before firing.

### Notes - Cont'd

- A Only two rounds were acquired during the mission. These readouts were so obviously in error that this mission was deleted for subsequent precision analysis. To date, it has not been determined if the NM87 is capable of chronographing RAP projectiles. It is unlikely that the problem experienced at the test site can be attributed to improper setup of equipment and/or an inexperienced operator.
- B Although the NM87 acquired all rounds fired, two of the readouts were deleted through a visual examination of the data. The measurements were found to be in error when compared to measurements of other data points of the same weapon/ammunition combination.
- C On three rounds the readout display was approximately twice the expected value (half the velocity) for this charge. The cause of the erroneous readout is unknown. It is definitely not a recording error.
- D One round was deleted when it was observed that the measurement was found to be in error when compared to measurements of other data points of the same weapon/ammunition combination.
- E The readouts obtained for the four rounds acquired were so inconsistent that this mission was deleted for subsequent precision analysis. To date, it has not been conclusively determined that the NM87 cannot chronograph RAP rounds.
- F Operator neglected to record the readout, the readout display before reset.
- G Although the NM87 acquired all rounds fired, one round generated a readout display approximately three times the expected value (1/3 the velocity) for this charge. The cause of the erroneous readout could not be determined.
- H Although the NM37 acquired all rounds fired during this mission, eight readings were deleted through a visual examination of the data. The measurements were found to be in error when compared to measurements of other data points of the same weapon/ammunition combination. It has been determined that the marginal performance of the equipment (22 out of 30 rounds) is due to operation beyond the design specification. The technical data furnished with the NM87 specifies an effective operating velocity range to 850 meters/second.
- I During the first nine rounds, only six readouts were correct. The remaining rounds were deleted because they did not compare with other data points of the same weapon/ammunition combination. Subsequent discussions with the operator revealed that during the first ten rounds, the GAIN control could have been incorrectly set.

### TABLE IV. Radar Chronograph, NM87 Summary of Firing Test Data

| Attempts to chronograph       | 486  |
|-------------------------------|------|
| Total rounds chronographed    | 474  |
| Total rounds missed           | 24*  |
| Chronographing percentage (%) | 92.6 |
| Set usage during firing (%)   | 97.0 |

### NOTES:

Total rounds fired - 501.

Rounds missed because of human error have not been considered in the calculations.

\*Includes erroneous readouts determined by comparison of measurements to other data points of the same weapon/ammunition combination.

The round by round data for this date is presented in Appendix D. The results of this firing test are shown in Table V. An examination of this data indicates that the NM87 correctly measured only one round of 15 rounds fired. The Frankford Arsenal signal processor, utilizing the common doppler signal from the NM87, measured eight rounds out of 15. It appears that the NM87 doppler radar is marginal relative to its ability to provide useable doppler signal from this weapon/projectile combination. The probable cause for failure is the fire ball experienced with this projectile when fired at charge 9.

#### Human Factors Evaluation

#### Doppler Radar

Because of the weight of the doppler radar (28.5 pounds), two men should be required to install this equipment on the weapon, one man to hold it in position, while a second man secures the mounting

TABLE V.

Radar Chronograph, NM87

Diring Data Summary Sheet for XM650E3 Projectile

|        |        | Velocity  | y/Range   |
|--------|--------|-----------|-----------|
|        |        | (m/:      | s - m )   |
| Round  |        | FA        | NM87      |
| Number | Charge | Processor | Processor |
| 914    | 9      | 791.4/28  | 578.8/35  |
| 915    | 9      | 000.0/0   | 794.1/35  |
| 916    | 9      | 794.9/28  | 763.8/35  |
| 917    | 9      | 789.6/140 | 442.5/35  |
| 918    | 9      | 000.0/0   | 746.0/35  |
| 919    | 9      | 000.0/0   | 442.5/35  |
| 920    | 9      | 791.4/126 | 429.0/35  |
| 921    | 9      | 793.5/28  | 438.8/35  |
| 922    | 9      | 000.0/0   | 562.5/35  |
| 923    | 9      | 797.1/28  | 789.5/35  |
| 924    | 9      | 791.2/126 | 502.7/35  |
| 925    | 9      | 000.0/0   | 655.5/35  |
| 926    | 9      | 000.0/0   | 643.9/35  |
| 927    | 9      | 795.4/28  | 770.9/35  |
| 928    | 9      | 000.0/0   | 424.5/35  |

hardware. With two men, installation on the M107, M109, and the M110 was accomplished in approximately five minutes, including cable hookup to the chronograph.

### Chronograph

Controls are well placed and clearly labeled. Recepticles are correctly positioned for right-angled cable connectors to route cables over the chronograph so as not to interfere with controls.

The TEST, READ, and RESET push buttons are well positioned for thumb operation when the chronograph is hand held. However, the push buttons should have rubber boots to prevent water entry into the chronograph. This could result in system malfunctions during freezing conditions. Further, the 5/8 inch diameter push buttons do not conform to MIL-STD 1472A which specifies 3/4 inch diameters.

At a weight of eight pounds, the chronograph is too heavy to be hand held for any length of time. It is suggested that a neck strap be used for hand held relief. The lower half of the outside facing edges of the rubber encasement should be rounded for greater palm comfort. Cable Reel Assembly

This assembly weighs 26.5 pounds end cen be carried by one man. However, it is quite awkward and should be carried by two men.

Mounting Set

There appears to be no human engineering problem with regards to the mounting sets, particularly when the swivel head wranch is utilized and since positional eccuracy is not critical.

Trensport Casa

The loaded transport case weighs 83.5 pounds and can be carried by two men if the lifting height does not exceed 4.5 feat.

### Technology and Methodology

The system is simple to operate, reliable, and capable of achiaving the same order of pracission as is possible with other velocity measurement methods. However, the most significant defact in the system is its failure to have indications of possible arroneous displays. The operator has no assurance that the values displayed on the chronograph readout are valid mussle velocity measurements.

The chronographing range for this system, a maximum of 35 meters, will be inadequate for weapon/projectile combinations in the 1975 - 1985 time frame. Changes in the target reflectivity of projectiles currently being developed will require increased range capabilities in order to capture the projectile in its trajectory.

The component technology utilized in the NM87 is slightly behind the current state-of-the-art. The electronics in many areas of the doppler rader and chronograph assemblies, Figuras 8 and 9, is such that the size and weight of the NM87 can be reduced by raplacing discrete and small/medium scale integrated component assemblies with MOS/LSI (Metal oxide semiconductor/large scale integrated) circuitry.

### Reliability and Maintainability

Determination of the reliability of the system existing at the end of the evaluation is considered impractical in this report because no feilures were encountered during the test and evaluation phase. No maintenance difficulties were observed in satup or tear down of the

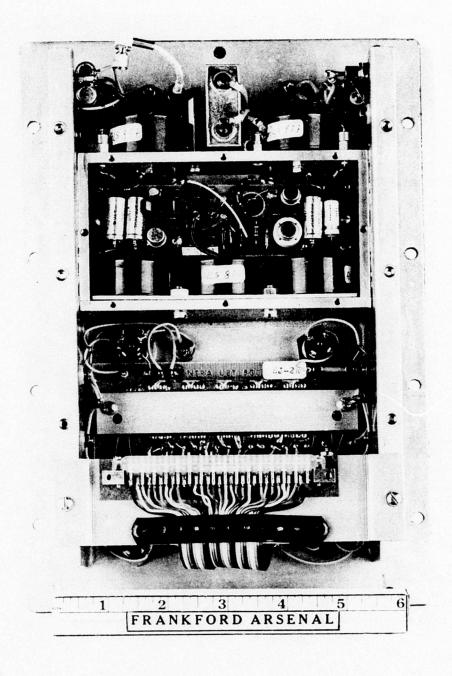


Figure 8. Radar Chronograph Set NM87, Digital Indicator and Voltage Regulator Assembly

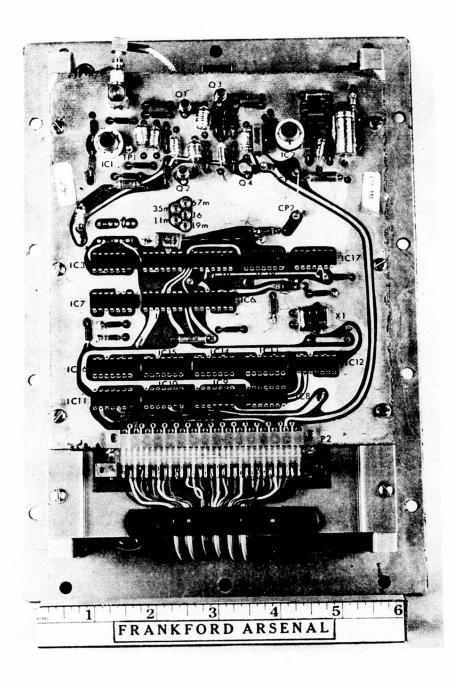


Figure 9. Radar Chronograph Set NM87, Digital Counter Assembly

major assemblies with either the tools or mounting sets provided with the system.

### Ruggedness

The NM87 is capable of withstanding exposure to the shock of repeated firings and transportation over cross country without adverse effects on operational performance. Further, it was not sensitive to weather and ambient light conditions.

### Adaptability

The NM87 is adaptable to all standard cannon artillery. It can be mounted on carriage to follow the azimuth and elevation of the tube with the mounting set surnished with the system; or other mounting brackets, see Figure 6, for special applications.

The system can also be mounted on a tripod with no adverse affect on performance. This permita greater versatility in deployment and reduces the initial set up time without any sacrifice of the required stability.

Because of the system's low power consumption, it is capable of being operated directly from vehicle power systems.

### CONCLUSIONS

There is no indication of any statistically significant differences in precision between the NM87 and other muzzle velocity measurement devices tested with standard weapon/projectile combinations.

Preliminary test data indicated that the NM87 does not have the capability to reliably measure the muzzle velocity of the XM650E3 projectile fired at charge 9 (8-inch RAP).

The NM87 is easy to install, simple to operate, rugged, reliable, and capable of achieving the same order of precision as is possible with other doppler radar velocity measurement devices.

### RECOMMENDATIONS

Error detecting features should be incorporated into the design to assure the operator that the values displayed on the chronograph readout are valid muzzle velocity measurements.

The chronographing range capability should be increased from the present maximum of 67 meters to 300 meters. Increased range capabilities will be required to chronograph projectiles under current develoment.

## APPENDIX A Radar Chronograph Set NM87 Evaluation Schedule - 18 September 1972

|   | M/DAYS  |
|---|---|
| Physical Inspection and Inventory       | 4   |
| Conformance of Physical Characteristics |   |
| with Test Item Specifications           | 5   |
| Safety Inspection                       | 5   |
| Electrical Characteristics              |   |
| Receiver Sensitivity                    | 20  |
| Doppler Frequency Response              | 20  |
| Transmitter Frequency                   | 5<br>5  |
| Transmitter Output                      | 5   |
| Calibration                             | 3   |
| Antenna Beamwidth                       | 4   |
| Antenna Gain                            | 8   |
| Boresighting                            | 6   |
| Monitor Circuits                        | 2   |
| Power Source                            | Š   |
| Power Consumption                       |   |
| Continuous Operation Test               | 4   |
| Firing Accuracy Test                    |   |
| Howitzer, 105MM                         | 15  |
| Howitzer, 8-inch                        | 15  |
| Howitzer, 155MM                         | 15  |
| Gun, 175MM                              | 15  |
| Ruggedness Test                         |   |
| Shock                                   | 4   |
| Vibration                               | 10  |
| Transport                               | 24  |
| Electromagnetic Inteference Tests       | 10  |
| Environmental Characteristics           |   |
| Low Temperature Test                    | 5   |
| High Temperature Test                   | 5   |
| Rain Test                               | 2   |
| Sand and Dust Test                      | 4   |
| Reliability Assessment                  | 20  |
| Maintainability Assessment              | 15  |
| Human Factors Assessment                | 20  |
| Physical Teardown                       | 25  |
| Determination of Special Features,      |   |
| Technology, and Methodology             | TOTAL TOTAL STATE OF THE STATE |
| Utilized in Test Item                   | 20  |

Fort Sill, Oklahoma, 8 - 23 August 1973 BRL Analysis - Customer Service Test APPENDIX

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,BRL ORRYON NORMALIZED DATA 105MM HOWITZER MID2,ZONE 1 , ROUNDS 200-221 DE - 350 MILS

| REAN  |       | 0.00   | 0.00      | 0000   | .77 03 |        | 177.07  | 178.43 | .78.05  |        | 160.08 | 190.68 | 183.75 | **     | 183.40 | 145.02 | 192.98 | 20 00  | 189.43 | 188,02 | 188.10 | 186.80 |         | 1900   | 187.07 | 187.17 | 188.12 | 20 30  | 2001   |           |        |        |           |       |        |          | PROB ERR 5.0785  |
|-------|-------|--------|-----------|--------|--------|--------|---------|--------|---------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|--------|--------|--------|--------|--------|--------|-----------|--------|--------|-----------|-------|--------|----------|------------------|
| KHR   |       | 0.00   | 0.00      | 178 30 |        | 0/0//1 | 176.30  | 178 20 |         | 0000/1 | 180.40 | 181.20 |        |        | 183.50 | 184.40 | .02 60 | 00.001 | 189.00 | 168.00 | 188.00 | 06 300 | 20001   | 189.00 | 185.70 | 185.90 | 187 70 |        | 188    |           | 184.31 | 20.201 | 767       |       | 3.032  |          | 4.5641           |
| NH=87 |       | 181.70 | 170.40    |        | 0000/1 | 177.90 | 177.90  |        | 0.001   | 179.40 | 190.40 | 00.00  |        | 100001 | 183.20 | 184.80 |        | 145.70 | 189.90 | 187.90 |        |        | 160.001 | 186.20 | 187.00 | .87 20 |        | 100.00 | 158.20 |           | 184.64 | 702 00 | 1000      | 4.094 | 2.964  |          | STNO DEV- 4.5641 |
| 6E-2  |       | 181.60 |           | 2000   | 178.50 | 177.60 | 176. AD |        | 178.10  | 178.50 | 180.10 |        | 181.10 | 183.60 | 183.10 |        |        | 192.60 | 189.60 | 187.60 |        | 180010 | 186.60  | 186.10 | 187.10 |        | 10/01  | 188.10 | 188.10 |           | ****** |        | 21.113    | 4.595 | 3,099  |          | 20.8314          |
| 66-1  |       |        |           | 1/9.10 | 170.10 | 177.60 |         | 11/10  | 179.10P | 179.10 |        | 10101  | 181.60 | 183,10 | 0. 200 |        | 143,00 | 193.60 | 180.60 |        | 10.01  | 187.60 | 187.10  | 184.60 |        | 10/400 | 187.10 | 187.60 | 187 60 |           | ***    | 104.00 | 19.830    | 4.453 | 3.004  |          | VAR1ANCE.        |
| #36-2 |       |        | 1010      | 179,30 | 178.60 | .78 KA |         | 177.20 | 178.50  | 170.00 |        | 181.00 | 179.60 | 184.00 |        | 184.00 | 185,30 | 193.00 | 400 40 | 00.061 | 188.30 | 188.30 | 187.00  | 07 70  | 00000  | 187.30 | 187.60 | 188.60 | 07     | na • au l |        | 184.86 | 21.484    | 4.635 | 400    | 2000     | AVERAGE          |
| H36-1 | •     |        | 000       | 00,0   | 00.0   |        | 178.30  | 177.30 | 178.30  |        | 0000/1 | 181.10 | 179.60 | 07 70  | 1000   | 143,70 | 145.40 | 07 100 |        | 100.10 | 188.70 | 188.70 | 187 40  |        | 180    | 187.70 | 188.10 | 188 70 |        | 188.70    |        | 145.05 | 23.054    |       |        | 30.50    | 184.661          |
| DATA  | -2104 |        | neleten 1 | •      |        | , .    |         | 10     | ,       |        |        | •      | •      |        | 2      | =      | 8      |        | 2      | -      |        |        |         |        |        |        |        |        |        |           |        | NEW    | Bour seas | 120   | 20 110 | PROB PRE | SPAND MEANS      |

MEASUMEMENTS FOUND TO BE DUTLIERS AT A 95% CONFIDENCE LEVEL ARF FOLLOWED BY 1 OR P. I indicates the Heasurement was found to be an Outlier when compared to measurements of the same data point by other instruments. P indicates the measurement was found to be an outlier when compared to measurements of the same data point by other instruments.

GPAND MEANS 184.661

\* INPICATES AN DUTLIER WHEN CONSIDERING THE DIFFERENCE RETWEEN INSTRUMENTS. (TWO INSTRUMENT CASE ONLY)

& INSTRUMENTS MITH 10 DATA POINTS EACH MERF USED IN THIS ANALYSIS.

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,BRL DBRYON NORMALIZED DATA 105MM MOWITZER MID2,ZONE 1 , ROUNDS 200-221 GE = 350 MILS

|                                  |            |          | 10.11.11.10.1                 |          |          |                        |
|----------------------------------|------------|----------|-------------------------------|----------|----------|------------------------|
|                                  | #36-1<br>A | H36-2    | 6E+1                          | 96-2     | NR-87    | X F                    |
| 1000                             | 0000       | 22.2394  | 21.0890                       | 21.9273  | 20.9943  | 21.3325                |
|                                  | 7010       | 0000     | 20.3484                       | 21,1659  | 20,2558  | 20.5223                |
|                                  | 0000       | 20 3484  | 00000                         | 20,3143  | 19.4091  | 19.7469                |
| 1-30                             | 20000      | 21 1650  | 20.3143                       | 0.000    | 20.1478  | 20,5453                |
| 2-26                             | 200000     | 20 2556  | 1607 61                       | 20,1478  | 0.000    | 19.6070                |
| N X X                            | 21,3325    | 20,6223  | 19.7469                       | 20,5453  | 19.6070  | 0.000                  |
| COV THELD INST                   | 107,5825   | 104,6319 | 100.9077                      | 104.1007 | 100.4140 | 101.8541               |
| COV EXCLD INST                   | 202,1630   | 205,1136 | 208.8377                      | 205,6448 | 209,3315 | 207.8914               |
| EST (SIGNA E1)<br>EST (SIGNA E1) | 0.2370     | 0.1426   | 0.3511                        | 0.0364   | 0.27288  | 0.2480                 |
| PRECISION RANK                   | •          | n        | •                             | _        | 2        | •                      |
|                                  | 400        |          | S PONA L SAV GREAT MANAGEMENT | RIANCE M | 20.650   | PARAM STR DEV. = 4.544 |

CHSTONER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGHST 73,8RL ORRYON NOPHALIZED DATA 105HM HD-172ER H102, ZONE 3 , ROUNDS 243-263 DE = 1250 HILS

|           |                                       |  |  | 0  |
|-----------|---------------------------------------|--|--|--|
| I W       | 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | 2 2 2 2 2 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3      | 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2                          | PROB ERR 1.1809  |
| X F F     | 241.70<br>238.50<br>236.90            | 232.90<br>232.50<br>232.50<br>234.00         | 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2                          | 2.543<br>1.595<br>1.076  |
| NH-87     | 60000                                 | 000000                                       |  | 0000<br>0000<br>0000<br>0000<br>0000<br>0000<br>0000<br>0000<br>0000   |
| 6E-2      | 239.30<br>239.30<br>237.30            | 000000<br>00000<br>00000<br>000000<br>000000 | 20000000000000000000000000000000000000                         | 235.53<br>3.1144<br>1.773<br>1.195<br>3.0652   |
| 9E-1<br>C | 241.80                                | 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2        | 2000<br>2000<br>2000<br>2000<br>2000<br>2000<br>2000<br>200    | 235.88<br>3.481<br>1.866<br>1.256<br>VAPIANCE  |
| H36-2     | 242.60                                |  | 20000000000000000000000000000000000000                         | 235.68<br>2.651<br>1.628<br>1.098<br>AVERABE   |
| 136-1     | _                                     |  | 2234.10<br>2235.40<br>2235.40<br>2235.40<br>2235.40<br>2235.40 | 236.22<br>3.566<br>1.372<br>1.263  |
| ATAC      |                                       | 801000                                       | 2222222222   | STAND BECK<br>STAND BECK<br>STAND BECK<br>PRODE ERRO<br>PRODE ERRO |

HEASHREMENTS FOUND TO BE DUTLIERS AT A 03% CONFIDENCE LEVFL ARE FOLLDAED BY I OR P.
I INDICATES THE WEASUREMENT WAS FOUND TO BE AN DUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.
P INDICATES THE MEASUREMENT WAS FOUND TO BE AN DUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.

S INSTRUMENTS MITH 20 DATA POINTS EACH MERE USED IN THIS ANALYSIS.

<sup>.</sup> INDICATES AN DUTLIER WHEN CONSTRERING THE DIFFERENCE BETWEEN INSTRUMENTS. (TWO INSTRUMENT CASE ONLY)

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,BRL OBRYON NORMALIZED DATA 185MM HOWITZER MIN2,ZONE 3 , ROUNDS 243-263 RE = 1250 MILS

. JULY-AUGUST 73,6PL DRRYON

|           |           | .00    | 77     |           | 070    | 0/0        | .03    |        |          | 220    | .75    | .93    | . 23   |        |          | 7.0    | 270,42 | 96.0   | 100    | 0.10   | N. C.  | 8.7    |        | 00.4   | 97.0   |        |        |        |          |         |       | PROB ERR- 0.9149 |
|-----------|-----------|--------|--------|-----------|--------|------------|--------|--------|----------|--------|--------|--------|--------|--------|----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------|---------|-------|------------------|
| 1         |           | •      | 270    |           | 2/0    | 269        | 269    |        | 202      | 270    | 270    | 269    | 27     |        | 7        | 72     | 27     | 27     | 58     | 26     | -      |        | 2      | 20     | 27     |        |        |        |          |         |       | PROB E           |
|           | # L       | 268.70 | 0000   | 2000      | 269.40 | 269.10     | 244 60 |        | 20/ 040  | 269.80 | 270.50 | 269.70 |        | 00.072 | 274.30   | 270.00 | 270.00 | 270.70 | 268.50 | 268.70 |        | 200.00 | 266.50 | 268.80 | 269.90 |        | 269.63 | 2.025  | 1.423    | 0.960   |       |                  |
|           | KH-87     |        |        | 2/0,40    | 269.00 | 240 AA     |        | 200,00 | 268.00   | 270.00 | 270 40 |        | 202.00 | 271.00 | 274,30 1 | 270.00 | 270.00 | 270.60 | 26. 50 |        | 200,00 | 269.20 | 269,30 | 269.30 | 270.00 |        | 269.85 | 1.802  | 1.342    |         |       | STND DEV= 1.3564 |
|           | 8E-2<br>0 |        | 268.90 | 270.60    | 270.10 |            | 269.00 | 269.10 | 268.10   | 270 10 | 0100/2 | 270.00 | 270,10 | 271.10 | 274.60 1 | 270.10 | 370.10 |        | 2/1010 | 269.10 | 269.10 | 269.60 | 969.60 | 240 40 | 00007  | 270.60 | 270.18 | 210    |          |         | 2.00  |                  |
|           | 66-1      |        | 269.60 | 271 60    |        | 2/1,10     | 269.60 | 969.60 | 0.000    | 10.60  | 2/1-10 | 271.60 | 269.60 | 271 10 | 275 60 T |        | 0101/2 | 2/1.10 | 271,10 | 269.60 | 269.60 | 269.60 | 940 40 | 20.00  | 269.60 | 271.10 |        | 60.072 | 2.104    | 1.471   | 260.0 |                  |
|           | H36-2     |        |        |           |        |            |        |        |          |        |        |        |        |        |          |        |        |        |        |        |        |        |        |        |        | 270.60 |        | 270.50 | 1.674    | 1.294   | 0.873 |                  |
| MURNALICE | 136-1     |        |        |           |        |            |        |        |          |        |        |        |        |        |          | _      |        |        |        |        |        |        |        |        |        | 270.70 |        | 270.54 | 1.655    | 1.286   | 0.868 |                  |
|           | DATA      | iniua  |        | DELETER 1 | ~      | <b>P</b> 7 | ,      | •      | <b>S</b> | •      |        |        |        |        | -        | =      | 12     |        |        |        | 2      | 9      | 17     | -      | 32     | 2      |        | MEAN   | VAPTANCE | 750 UNA |       |                  |

HEASHREWENTS FOUND TO BE OUTLIERS AT A OST CONFIDENCE LEVFL ARE FOLLOMED BY I OR P. I indicates the Weasurement has found to be an outlier when compared to measurements of the same data point by other instruments. P indicates the weasurement has found to be an outlier when compared to measurements of the same data point by other instruments.

. INDICATES AN DUTLIER WHEN CONSIDERING THE DIFFERENCE BETWEEN INSTRUMENTS, ITHO INSTRUMENT CASE ONLY)

6 INSTRUMENTS WITH 19 DATA POINTS EACH WERE USED IN THIS ANALYSIS.

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,8RL DORYON NORMALIZED DATA 105MM HOWITZER MIOZ,ZONE 4 , ROUNDS 222-241 BEF 180 HILS

|                   |         |        |   |                |                |                |                | 1.3200               |
|-------------------|---------|--------|---|----------------|----------------|----------------|----------------|----------------------|
|                   | E L     | 1.7461 | 0.000                                     | 9.1946         | 17.2911        | 0.0787         | •              | PARAM STD DEV        |
|                   | NH-87   | 1.6973 | 10000                                     | 8.0652         | 17.6205        | 0.0175         | -              | 1.766                |
| COVARIANCE HATRIX | 2.30    | 1.6504 | 0000                                      | 9.6990         | 17.7868        | 0.0104         | ~              | TANCE .              |
| COVARIAN          | 1.0     | 1,7254 | 0000                                      |                |                | 0.2128         | •              | PARAMETER VARIANCE . |
|                   | H 300.E | 1.6228 | 111111111111111111111111111111111111111   | 8.5717         | 17.9141        | 0.0372         | *              | 28.4057 PAR          |
|                   | - CE    | 0.0000 | 1.6504                                    |                | 18,0437        |                | •              |                      |
|                   |         | 100 H  | 1 2 0 0 K K K K K K K K K K K K K K K K K | COV INCLB INST | COV EXCLS INST | EST (SISHA E1) | PRECIOION RANK | TOTAL COVARIANCE"    |

CUSTOMER SERVICE TEST AT PORT SILL, CONDUCTED BY F.A., JULY-AUSUST 73,8RL DRRYON NORMALIZED DATA 105HH HOWITZER HID2,ZONE 5 , ROUNDS 266-264 BE = 208 - 200 HILS

| nEAN                                    | 000000000000000000000000000000000000000 |  |  | 20 00 00 00 00 00 00 00 00 00 00 00 00 0 |  | ROS ERRS: 049228 |
|---|---|--|--|--|--|------------------|
| 1                                       | 311                                     | 12 12 12 12 12 12 12 12 12 12 12 12 12 1             | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1    | 0000                                     |  | 1.3825           |
| •                                       | 9000                                    | 315.10   |  | 20000                                    |  | ST40 DEV-        |
| 8E-2<br>0                               | 317.60                                  | 8110<br>8110<br>8110<br>8110<br>10<br>10<br>10<br>10 | 00000000000000000000000000000000000000   |  | 0.000<br>0.000<br>0.000<br>0.000                             | 1.9113           |
| 1.0                                     | 317,60                                  |  |  | 00000<br>00000<br>00000                  | 0.00<br>4.00<br>4.00<br>4.00<br>4.00<br>4.00<br>4.00<br>4.00 | FAR SANCE        |
| H36-2                                   |   |  | 11111111111111111111111111111111111111   |  |  | AVERABE          |
|   |   |  | 000000                                   |  | 0000   | . 316.783        |
| 8 A T A T A T A T A T A T A T A T A T A | ETED 1                                  | 36LETED 5  | 00 - 00 00 00 00 00 00 00 00 00 00 00 00 | 34                                       | MEAN STAN BECK   | ORAND HEAN-      |

MEASUREMENTS FOUND TO BE OUTLIERS AT A 95% COMFIDENCE LEVEL ARE FOLLOWED BY I OR P.
I INDICATES THE HEASUREMENT HAS FOUND TO BE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME: DATA POINT BY OTHER INSTRUMENTS.
P INDICATES THE HEASUREMENT HAS FOUND TO BE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME: DATA POINT BY OTHER INSTRUMENTS.

. INDICATES AN OUTLIER WHEN CONSIDERINS THE DIFFERENCE SETHEEN INSTRUMENTS. (THO INSTRUMENT CASE ONLY)

S INSTRUMENTS WITH 19 DATA POINTS EACH MEPZ USED IN THIS ANALYSIS.

CUSTOMER BERVICE TEST AT FORT BILL, COMBUCTED BY F.A., JULY-AUBUST 73,8RL OBRYON MOMENTER MADAZZONE 5 , ROUNDS 266-284 OE = 208 - 200 MILS

| 5 10.5396 | 0.0000 10.5732 10.5 |
|-----------|---------------------|
| 5 0.11941 | 0.0000 0.0375 0.1   |
| D P 0     |                     |

| 20 X O X  |
|---|
| 73,8RL<br>093   |
| AUSUST  |
| 301-310   |
| ROUNDS  |
| ONDUCTE O   |
| BILL, C   |
| AT FORT   |
| 1081  |
| ED OATA   |
| CUSTOMER SERVICE TEST AT FORT SILL, COMBUCTED ST F.A., JULYMAUSUST 73, SRL DERYON NORMALIZED DATA 1958H MOMITZER MID2, ZOME 7 , ROUNDS 301H310, BE = 1093 |
|   |

|            | HEAN  | 000000000000000000000000000000000000000 | 486.87<br>486.87<br>488.10 | 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | 2004<br>2004<br>2006<br>2006<br>2006<br>2006 |  | PROB ERR 0.6997 |
|------------|-------|---|----------------------------|---------------------------------------|--|--|-----------------|
|            | X .   | 100.50                                  | 486.70                     | 405.40                                | 406.20                                       | 0000   | 1.0374          |
|            | MH-87 | 0.00                                    | 000                        |                                       | 000  | 0000   | -N30 0H4        |
|            | 3-    | 1 469.00 1                              | 486.50                     | 466.00                                | 485.50<br>485.00                             | 486.35<br>1,336<br>1,156<br>0,780  | 1.0763          |
|            | I.    | 1 00.00                                 | 100.00                     |                                       |  |  | *ZORVINYA       |
|            |       |   |                            |                                       |  |  |                 |
| A STATE OF |       |   |                            |                                       |  |  |                 |
|            | DATA  |   | N P 4                      | 801                                   |  | NAME OF STATE OF STAT | =               |
|            |       |   |                            |                                       |  |  | -               |

MEABUREMENTS FOUND TO BE OUTLIERS AT A 95% COMPIDENCE LEVEL ARE FOLLOMED ST I OR P. I INDICATES THE MEASUREMENT HAS FOUND TO BE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT ST STHER INSTRUMENTS. P INTICATES THE MEASUREMENT HAS FOUND TO BE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT ST STHER INSTRUMENTS.

. INDICATES AN OUTLIER WHEN CONSIDERING THE DIFFERENCE SETHEEN INSTRUMENTS. (THO INSTRUMENT CASE ONLY) S INSTRUMENTS MITH to DATA POINTS EACH MERE USED IN THIS ANALYSIS.

### COVARIANCE MATRIX

|  |        |   |              |         |         |         |                                  |         | :                   |
|--|--------|---|--------------|---------|---------|---------|----------------------------------|---------|---------------------|
|  | E E    | 000000000000000000000000000000000000000 | 1.1072       | 0.000   | 1.0322  | 1.0139  | 0.0160                           | •       | PARAM STD DEV       |
|  | N#=67  | 0.0000                                  | 000          | 0.0000  | 0.000   | 6.0000  | 0.00000                          | •       | 0.982               |
| STATE OF THE PARTY | -      | 000                                     |              | 1:1072  | 2.1211  | 0.8250  | 0,0400                           | •       |                     |
| The second second  | Ĭ.     | 000                                     | 0000         | 0.8250  | 1.4389  | 1.1072  | 0,2267                           |         | SAY GOVERN          |
|  | Ĭ.     | 1000                                    |              | 0000    | 0,000   | 0.000   | 0.0000.0                         |         | - ADDITION ADDITION |
|  | H 36-1 | DELETES<br>0.0000<br>0.0000             | 000          | 0.000   | 0.000   | 0.000   | 0.0000                           | •       |                     |
|  |        | 1 1 0 0 H                               | 86-1<br>86-2 | X X X   | LB INST | LB INST | BHA E1)<br>BHA E1)               | ON RANK |                     |
|  |        | DELETED                                 | 86.5         | DELETED | COV INC | COV EXC | EST (518MA E1)<br>EST (818MA E1) | PRECISI |                     |
|  |        |   |              |         |         |         |                                  |         |                     |

0.9910

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED SY F.A., JULY-AUBUST 73, SRL DRRYON

|                         |       |         |          |        |           |        |        |        |        |        |        |        |        |          |         |          | 11          |
|-------------------------|-------|---------|----------|--------|-----------|--------|--------|--------|--------|--------|--------|--------|--------|----------|---------|----------|-------------|
| 1077                    | HEAN  |         | 485,12   | 00.0   | 00.0      | 00.0   | 00.0   | 484,38 | 181.80 | 484.74 | 184.62 | 485,32 |        |          |         |          | ERR- 0.4841 |
| - 30                    |       |         | _        |        |           |        |        |        |        |        |        |        |        |          |         |          | PR08        |
| 311-320,                | X X   |         | 484,30   | 485.10 | 465,00    | 494.80 | 484,60 | 485,20 | 484.90 | 465.00 | 484.90 | 485,20 | 484.92 | 0.110    | 0.331   | 0.228    | 0.7177      |
| . ROUNDS                | NH-87 | DELETED | 00.0     | 00.0   | 00.0      | 00.00  | 00.0   | 00.0   | 00.0   | 00.0   | 00.0   | 0.00   | 00.00  | 00000    | 0.00    | 0.00     | STNO DEV-   |
| HOWITZER MIDZ, ZONE 7 , | 66-2  |         | 1 00.981 | 485.50 | 485.00    | 484.50 | 485.00 | 485.00 | 485.00 | 485,00 | 484.50 | 485.00 | 485.08 | 0.242    | 0,492   | 0.332    | 0.5151      |
|                         | 96-1  | נו      | 486.00   | 484.00 | 484.00    | 463,50 | 483.50 | 484.00 | 484.00 | 484.00 | 484.00 | 465.60 | 484.60 | 0.880    | 0.938   | 0.933    | VARIANCE=   |
| HORMALIZED DATA 105MM   | H36-2 |         | 486-10   | 485.10 | 485.10    | 484.70 | 85.10  | 465.50 | 485.50 | 485.10 | 485.10 | 485.80 | 485.52 | 0.154    | 0.392   | 0.264    | AVERABE     |
| NORMALIZED              | 1-98H | 4       | 483.20   | 481.20 | 00.0      | 00.0   | 00.0   | 482.20 | 484 60 | 484 60 | 484.60 | 465.00 | 484.03 | 101      | 1001    | 0.736    | 484.830     |
|                         | DATA  | POINT   |          | FTER 2 | DELETER T | 7      | 2      |        |        |        |        | 10,    | 200    | VADTANCE | ATU DEV | PROS ERR | BRAND MEAN- |

MEASUREMENTS FOUND TO SE OUTLIERS AT A 95% CONFIDENCE LEVFL ARE FOLLOWED SY I OR P. I indicates the measurement was found to se an outlier when compared to measurements of the same data point by other instruments. P indicates the meaburement was found to be an outlier when compared to measurements of the same data point by other instruments.

. INDICATES AN OUTLIER WHEN CONSIDERING THE DIFFERENCE BETWEEN INSTRUMENTS. (THO INSTRUMENT CASE ONLY)

5 INSTRUMENTS WITH 6 DATA POINTS EACH MERE USED IN THIS ANALYSIS.

#### COVARIANCE MATRIX

|            |   |         |                |                |                                  |                | 0.12                 |
|------------|---|---------|----------------|----------------|----------------------------------|----------------|----------------------|
|            |   |         |                |                |                                  |                | DEV                  |
| ×          | 10.0000   | 000     | -0.2807        | 0.4423         | 0.3237                           | •              | PARAM STD DEV        |
| NH-67      | 0000  |         | 0.000          | 0.0000         | 0.0000                           | •              | 0.016                |
| 2 6        | 0,1563  | 0,000   | 0.1533         | 0.0083         | 0.1664                           | ~              | TANCE -              |
| . C.       | 0.0240  | 0.0000  | 0.4840         | -0.3223        | 0.5843                           | •              | PARAMETER VARIANCE . |
| #36-2<br>6 | 0.1327  | 0.0000  | 0.2873         | -0,1257        | 0.00000                          | -              | 0.1417 PAS           |
| H36-1      | 0.0000  | 0.02233 | -0.3207        | 0.4823         | 1,4314                           | <b>s</b> n     |                      |
|            | # 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 |         | COV INCLD INST | COV EXCLD INST | EST (SIONA E1)<br>EST (SIONA E1) | PRECISION RANK |                      |
|            |   | DELETED | ×00            | ¥00            | EST                              | PRE            | i                    |

CUSTOMER BERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUBUST 73,8RL DBRYON NORMALIZED DATA 105MM HOWITZER MID2,ZONE 7, ROUNDS 322-326, BE- 405 MILS

| 4444<br>66666<br>7.7.8.8<br>8.0.00<br>9.000   |  | PROS ERRE 0.7936   |
|---|--|--|
| 4444<br>467,000<br>66,000<br>66,000<br>60,000   | 487.14<br>1.158<br>1.067<br>0.720  | 1.1766   |
| 4444<br>66666<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>6866<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68846<br>68 | 465.24<br>1.326<br>1.152<br>n.777  | STNO DEV   |
| 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4   | 10.288<br>10.188<br>10.788   | 1.3645   |
| 4444<br>6666<br>6776<br>6776<br>600<br>600<br>600<br>600  | 4000<br>6000<br>6000<br>6000<br>6000   | VAPTANCE   |
| 465<br>467.70<br>485.70<br>10<br>10   | 487.42<br>1.527<br>1.236<br>0.633  |  |
| 44444<br>44444<br>44444<br>44444<br>44444<br>44444<br>4444  | 2.22.0<br>1.401<br>1.005   |  |
| - N N 4 E   | VARIANCE<br>STAB OFF<br>PROS CRY   |  |
|   | 469.20 488.00 488.30 486.90 488.60 487.30 487.30 487.30 487.30 487.30 487.30 486.20 486.20 486.20 486.20 486.20 486.20 | 489,40 469,20 488,00 488,50 486,90 488,60 488,43<br>487,60 487,50 487,50 487,50 485,90 487,50 487,20<br>485,90 486,10 486,10 485,90 464,00P 466,20 485,67<br>485,90 486,10 485,90 464,00P 466,00 485,67<br>487,36 487,42 487,06 487,06 465,24 487,14<br>1,236 0,893 1,358 1,138 1,138<br>1,100 0,633 0,604 0,753 0,777 3,720 |

MEAGUREMENTS FOUND TO BE OUTLIERS AT A 95% CONFIDENCE LEVFL ARE FOLLOWED BY 1 OR P. 1 indicates the meagurement has found to be an outlier when compared to measurements of the same oata point by other instruments. 1 indicates the meagurement has found to be an outlier when compared to measurements of the same oata point by other instruments.

. INDICATES AN OUTLIER WHEN CONSIDERING THE DIFFERENCE SETWEEN INSTRUMENTS. (TWO INSTRUMENT CASE ONLY)

6 INSTRUMENTS MITH S DATA POINTS EACH MERE USED IN THIS ANALYSIS.

|                   | E L        | 1.0870         | 1.2205 | 6.2280     | 13.6045    | 0.0072     | ~              | PARAH STD DEV.       |
|-------------------|------------|----------------|--------|------------|------------|------------|----------------|----------------------|
|                   | NH-87      | 1.6995         | 1.2870 | 6.6060     | 13.2245    | 0.0073     | n              | 1.322                |
| COVARIANCE MATRIX | 96-2       | 1.5760         | 0000   | 6.5460     | 13.2865    | 0.00000    | -              | TANCE .              |
| COVARIAN          | 6E=1       | 1.2630         | 0.0000 | 5.2260     | 14.6065    | 0.1733     | •              | PARAMETER VARIANCE . |
|                   | #36-2<br>6 | 1.8235         | 1.0465 | 0,9660     | 12.8465    | 0.0172     | •              |                      |
|                   | #36-1      | 0.0000         | 1.5990 | 6.0710     | 11.7615    | 0.1708     | sn.            | 10.8325              |
|                   |            | H36-1<br>H36-2 | 122    | INCLD INST | EXCLD INST | (810HA E1) | PRECISION RANK |                      |
|                   |            |                |        | >00        | >00        | 55         | PREC           |                      |

1.1499

CONDUCTED BY F.A., JULY-AUGUST 73, BRL DBRYON

|            |         |          |          | 7 75   | -                | 417     | 7427            |
|------------|---------|----------|----------|--------|------------------|---------|-----------------|
| BATA       | H36-1   | #36-2    | 1-30     | 96-2   | NO-EZ            | XMX     | 24.34           |
|            |         | •        | O        | _      | •                |         |                 |
| -          |         |          |          |        | DELETED          | DELETED |                 |
| 5          |         | 4.49 Ann | 842.00   | 542.00 | 0.00             | 00.0    | 542.27          |
|            |         |          | 542 00   | 543.00 | 538.20           | 00.0    | 542.70          |
|            | 0000    |          | 277      | 848.00 | 00.0             | 00.0    | 542,67          |
|            |         | 234.00   | 00.00    |        | KK4 TO           | 0.00    | 00.00           |
|            |         | 544,90   | 00.0     | 264.50 | 000000           |         |                 |
|            |         | 547.30   | 545.50   | 548,50 | 00.0             | 0000    | 200             |
|            |         | 200      | 542.00   | 542,30 | 0.00             | 00.0    | 541.47          |
|            |         |          | 4.4K KA  | 545.50 | 00.0             | 00.0    | 545.73          |
|            | 000     |          |          | 847.00 | 00.0             | 00.0    | 546.67          |
|            | 00.0    | 000      | 00000    |        |                  | 840.10  | 543.97          |
|            | 00.0    | 243.90   | 244,00   | 244,00 |                  |         | 7. 37           |
|            | 00.0    | 546.60   | 545.00   | 545,50 | 00.0             | 244.80  | 20000           |
|            |         | E48.00   | 547.50   | 547.50 | 0.0              | 543,80  | 547.87          |
|            |         | X 48 X00 | 547.50   | 547.50 | 00.0             | 544.10  | 547.77          |
|            |         | 90       | 545.50   | 546.50 | 00.0             | 00.0    | 546.87          |
|            |         | 900      | 848.50   | 545.50 | 00.0             | 0.00    | 545.63          |
|            |         |          | 826.00   | 547.00 | 00.00            | 00°0    | 00.0            |
|            |         |          | 248 00   | 548.00 | 00.0             | 00.0    | 548,00          |
|            |         |          |          |        | 00.0             | 00.0    | 544.50          |
|            |         | 241.50   | 545,50   | 000000 |                  |         | 546.57          |
|            |         | 547.70   | 545,50   | 540.50 | 00.0             |         |                 |
|            | 0.00    | 547.70   | 547.50   | 548.50 | 00.0             | 00.0    | 24.196          |
| 77.77      | 00.0    | 545.36   | 545,21   | 545.72 | 00.0             | 0.00    |                 |
|            |         | 771.0    | 3.658    | 3.743  | 0.000            | 000.0   |                 |
|            |         | 100      | 1.013    | 1.935  | 0.000            | 00000   |                 |
|            | 0.00    | 2700     | 200      | 1.305  | 0.00             | 00000   |                 |
| 201        | 00000   |          |          |        |                  |         |                 |
| PANE MEANS | 426 430 | 2440774  | VARTANCE | 5.5150 | STND DEVE 2,3484 |         | PROB ERR 1.5840 |

MEASURCHENTS FOUND TO BE OUTLIERS AT A 95% CONFIDENCE LEVEL ARE FOLLOWED BY I DR P.
I INDICATED THE MEASUREMENT WAS FOUND TO BE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.
P INDICATES THE MEASUREMENT WAS FOUND TO BE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.

. INDICATED AN OUTLIER WHEN CONSIDERING THE DIFFERENCE BETWEEN INSTRUMENTS. (THO INSTRUMENT CASE ONLY)

3 INSTRUMENTS WITH 17 DATA POINTS EACH WERE USED IN THIS ANALYSIS.

CUSTOMER BERVICE TEST AT PORT BILL, CONDUCTED BY F.A., JULY-AUGUST 73,8RL DBRYON NORMALIZED DATA 105HH HOWITZER MIOZ,ZONE 7. (RAP), ROUNDS 327-345, GE - 405 MILS

| BELETED H36-1 0,0000 0, |                |       |            | COVARIANCE | CE MAINIA |        |                     |     |       |
|--|----------------|-------|------------|------------|-----------|--------|---------------------|-----|-------|
| H36=1 0,00000 0,0000 0, |                | #36-1 | #36-2<br>6 | 1-36       | 96-2      | NH-67  | XHR<br>F<br>OELETER |     |       |
| HH-67 0.00000 0.000000  |                |       | 0000       | 040        | 3.5324    | 0000   | 0000                |     |       |
| LB INST 0.0000 8.5475 7.9351 7.7771 0.0000 3.5524 1.1948 4.3528 0.0000 1844 E.3528 0.0000 |                |       | 000        | 00         | 0000      | 0.0000 | 0.0000              |     |       |
| 0.0000 4.1786 -0.0822 0.3188 0.0000<br>0.00000 2.04417 0.00000 0.56461 0.00000<br>0 3 1 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0  | COV INCLD INST |       | 8.8475     | 7.9351     | 7.777     | 0.000  | 0.000               |     |       |
| (BIBHA E1) 0.0000 4.1786 -0.0822 0.3188 0.0000 (BIBHA E1) 0.00000 2.04417 0.00000 0.56461 0.00000 (BIBHO RAWK 0 3 1 2 0 0 0.741 COVARIANCE 12.1299 PARAMETER VARIANCE - 4.043  | COV EXCLB INST |       | 3,5824     | 4.1946     | 4.3528    | 0.0000 | 0.000               |     |       |
| ANCE- 12:1299 PARAMETER VARIANCE - 4.043   | EST (SISHA E1) |       | 4.1786     | 0.00000    | 0.3188    | 0.0000 |                     |     |       |
| ANCE- 12:1299 PARAMETER VARIANCE - 4.043   | PRECISION RANK | •     | n          |            | 8         | •      | •                   |     |       |
|  | TOTAL COVARI   | ANCE. |            | RAHETER VA | - BANCE - | 4.043  | PARAH STR           | DEV | 2.010 |

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUSY 73,8RL DBRYOW

MEASUREMENTS FOUND TO BE BUTLIERS AT A 95% CONFIDENCE LEVEL ARE FOLLOMED BY I OR P.
I INDICATES THE HEASUREMENT HAS FOUND TO BE AN GUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.
P INDICATES THE MEASUREMENT HAS FOUND TO BE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.

BRAND MEANS

<sup>.</sup> INDICATES AN OUTLIER WHEN CONSIDERING THE DIFFERENCE BETWEEN INSTRUMENTS. (TWO INSTRUMENT CASE ONLY)

<sup>5</sup> INSTRUMENTS WITH 16 DATA POINTS EACH WERE USED IN THIS ANALYSIS.

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,8RL DBRYON NORMALIZED DATA 155MM MOWITZER, MIDG, ZONE 1, ROUNDS 401-420, DE = 460 MILS

|  |        |          | COVARIAN             | COVARIANCE MATRIX |         |               |      |        |
|--|--------|----------|----------------------|-------------------|---------|---------------|------|--------|
|  | #36-1  | H36-2    | 9£-1                 | aE-2              | Z = 0.7 | X X X         |      |        |
| H36-1                                    | 0.0000 | DELETED  | 0,6029               | 0.4815            | 0.1688  | 0.5394        |      |        |
| DELETED M36-2                            | 0.0000 | 0.000.0  | 0000                 | 0.5979            | 0.6450  | 0.8442        |      |        |
| 95.01                                    | 0.4815 | 0.000    | 0.5979               | 00-0-0            | 0.5042  | 0.6317        |      |        |
| NA N | 0.5394 | 0.0000   | 0.6450               | 0.5139            | 0.6317  | 0.0000        |      |        |
| COV THELD INST                           |        | 0.0000   | 2,6900               | 2.0973            | 2,2697  | 2.5290        |      |        |
| COV EXCLD INST                           |        | 0.000    | 3,1593               | 3,7520            | 3.5796  | 3,3203        |      |        |
| EST (518MA E1)                           | •      | 0.0000   | 0.1774               | 0.0673            | 0.1798  | 0.57681       |      |        |
| PERCISION RANK                           |        | •        | n                    | -                 |         | wn            |      |        |
|  |        | A 8000 P | PARAMETER VAR.ANCE . | R. ANCE .         | 0.585   | PARAM STD DEV | DEV. | 0.7648 |

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,BRL DBRYON NORMALIZED DATA 155MM HOWITZER, M109, ZONE 38 ROUNDS 481-500, 9E = 1219 MILS

|       |       |          |        |          |        |        |        |         |        |          |        |        |           |          |        |        |        |        |        |         |         |        |        |        |         |        |        |      |        |        |          |           |          |          | :                |   |
|-------|-------|----------|--------|----------|--------|--------|--------|---------|--------|----------|--------|--------|-----------|----------|--------|--------|--------|--------|--------|---------|---------|--------|--------|--------|---------|--------|--------|------|--------|--------|----------|-----------|----------|----------|------------------|---|
| REAN  |       |          | 00.0   | 275.37   | 277.05 | 276.85 |        | 2/0-12  | 277.05 | 277.28   |        |        | 276,55    | 277,90   | 276.98 |        | 00.012 | 276.75 | 276,88 | 276.68  |         | 100012 | 275,53 | 275,60 | 60. 445 | 2001/2 | 6/3060 |      |        |        |          |           |          |          | PROB ERR# 0.5244 | 1 |
| XHR   | •     |          | 271.:0 | 274.80   | 276.10 | 974 C  | 6/3010 | 275,507 | 276.10 | 374 100  | 01.012 | 00.0/2 | 275.50    | 277.30 1 | 278 70 | 0/00/3 | 275,30 | 275.70 | 278.90 |         | 0006/2  | 274,70 | 274.60 | 278.70 |         | 06.672 | 274,50 |      | 275.54 | 0.488  | 904      |           | 1/00     |          | 0.7775           |   |
| N4-87 | W     |          | 272,70 | 276.00   | 277.40 |        | 2//200 | 277.10  | 277.40 |          | 2// 10 | 278,00 | 277.00    | 278. AB  |        | 277.50 | 277.00 | 277.10 | 277 40 | 2000//2 | 2// .50 | 276.10 | 276.50 | 977 00 | 000117  | 277.50 | 275,80 |      | 277.11 | . 48.  |          | 1000      | 0.468    |          | STND DEV         |   |
| 9E-2  | E     |          | 00.0   | 278.40   | 946    | 04.0/2 | 276.90 | 276.90  | 276 00 | 0400/2   | 277,40 | 00.0   | 276.46    |          | 060//2 | 276.90 | 276.40 | 276 90 | 06.073 | 276.90  | 276.40  | 275.40 | 246 00 | 000000 | 270.40  | 276.90 | 275.40 |      | 276.57 |        | 0.4/1    | 0.586     | 0.463    |          | 0.6045           |   |
| 6E-1  | U     |          |        | 275 30   | 00.07  | 277,60 | 277.80 | 277 30  | 000.// | 2// , 60 | 277,80 | 00.0   |           | 00.775   | 277,80 | 277.80 | 277 30 |        | 2//000 | 277,30  | 277.30  | 27 TO  |        | 2/3,30 | 277,30  | 277.80 | 274 30 | 2000 | 277 08 | 2001/3 | 0.078    | 0.089     | 0.467    |          | VARIANCE         |   |
| 136-2 | •     | DEI ETER |        |          | 0.00   | 00.0   | 00.0   |         | 00.0   | 0.0      | 00.0   |        |           | 00.0     | 00.0   | 00.0   |        |        | 00.0   | 00.0    | 00.0    |        | 0000   | 06.0   | 00.0    |        |        | 00.0 |        | 0000   | 0000     | 00000     | 000      | 0.000    | AVERAGE          |   |
|       | •     |          |        |          |        |        |        |         |        |          |        |        |           | 000      | 00.0   |        |        | 00.0   | 00.0   | 00.0    |         |        | 0000   | 0.0    | 00.0    |        |        | 00.0 |        | 00.0   | 0000     | 000       |          | 00000    | 276.568          |   |
|       | PA-64 |          |        | ELETER 1 | ~      | 10     |        |         |        | •        |        |        | DELETER 8 | •        |        |        | -      | 12     | 13     |         |         | n      | 16     | 17     |         | D (    |        | 000  |        | IEAN   | VAPTANCE | 7 4 7 6 7 | 9140 654 | PROB ERR | BPAND MFANS      |   |
|       |       |          |        | -        |        |        |        |         |        |          |        |        | ī         |          |        |        |        |        |        |         |         | 13     |        |        |         |        | 4:     | 3    |        |        |          |           |          |          |                  |   |

MEABUREMENTS FOUND TO BE OUTLIERS AT A 95% CONFIDENCE LEVFL ARE FOLLOWED BY I OR P. I Indicates the Heasurement has found to be an Outlier when compared to measurements of the same data point by other instruments. P indicates the Heasurement has found to be an Outlier when compared to measurements of the same data point by other instruments.

. INDICATES AN OUTLIER WHEN CONSIDERING THE DIFFERENCE BETWEEN INSTRUMENTS. (TWO INSTRUMENT CASE ONLY)

4 INSTRUMENTS WITH 18 DATA POINTS EACH WERE USED IN THIS AVALYSIS.

CUSTOMER SERVICE TEST AT FORT SILL, CONOUCTED BY F.A., JULY-AUGUST 73,8RL DBRYON NORMALIZED DATA 155MM HOWITZER, MIDD, ZONE 30 ROUNDS 461-500, DE = 1219 MILS

|                   |            |                            |                           |            | •          |            |                | PARAH 870 0EV 0.7171 |
|-------------------|------------|----------------------------|---------------------------|------------|------------|------------|----------------|----------------------|
|                   | X X X      | 0.000                      | 0.4304                    | 1.4140     | 1.6716     | 0.1030     | ю              | PARAM BT             |
|                   | NH-B7      | 0.0000                     | 0000                      | 1.5052     | 1.5804     | 0.06634    | •              | 0.514                |
| COVARIANCE MATRIX | 0E-2<br>D  | 000000                     | 0000                      | 1.4873     | 1.5963     | 0.0119     | 2              | D. ANGE              |
| COVARIAN          | ee-1       | 0.000                      | 0.000<br>0.6029<br>0.6147 | 1.7647     | 1.3206     | 0.2416     |                | BUNGARY GREAT GAG    |
|                   | #36-2<br>6 | 0,0000<br>0,0000           | 0000                      | 0.000      | 0.000      | 0.00000    | •              | ***                  |
|                   | #36-1      | 0.0000<br>0.0000<br>0.0000 | 00000                     | 0.000      | 0.000      | 0.0000     | •              |                      |
|                   |            | EP #36-1                   | KE STATE                  | INCLD INST | EXCLD INST | (STONA E1) | PRECISION RANK |                      |
|                   |            | DELETER                    |                           | 200        | ×00        | 55         | PREC           |                      |

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,8PL DBRYON

| 816.40  815.20  816.40  816.40  816.40  816.40  816.20   | H36+2      | 6E-1 | 06-2    | 10-NA     | XHR     | MEAN           |
|--|------------|------|---------|-----------|---------|----------------|
| Def.   Per.  |            |      | c       |           |         |                |
| 236.40 315.20 316.20 315.20 31   |            |      | 315.20  | 315,60    | 313.60  | 0.00           |
| 235 0 315 20 316 20 316 60 317 30 318 50 314 20 314 20 314 20 314 20 314 20 314 20 314 20 314 60 314   |            |      | 316.20  | 316.70    | 314,40  | 315.88         |
| 235.50 315.20 315.20 316.60 0.00 311.60 314.20 314.20 314.20 0.00 311.60 314.20 314.20 314.20 0.00 311.60 314.10 314.20 3   | 0.00       |      | 316.70  | 317,30    | 315,50  | 316.62         |
| 23. 23. 23. 25. 27. 314.20 0.00 311.80 314.30 315.20 315.20 314.20 0.00 311.80 314.30 315.20 314.20 0.00 311.80 314.30 314.30 314.30 314.30 314.30 314.30 314.30 314.30 314.30 314.30 314.30 314.30 314.30 314.30 314.30 314.30 314.30 314.20 31   |            |      | 316.20  | 316.60    | 314,20  | 315,72         |
| 313.60 313.60 313.20 314.30 31   | .00        |      | 31.4 20 | 00.0      | 0.00    | 00.0           |
| 313.60 313.60 314.90 315.70 314.60 314.90 314.90 315.70 314.60 313.10 314.90 315.70 314.60 315.70 315.70 315.80 31   | 0.00 314.3 |      | 000000  | 0         | 311.80  | 00.00          |
| 314.90 31   | n.00 313.6 |      | 2000    | 05 012    | 314.10  | 315,60         |
| 314.30 314.30 314.30 314.30 314.20 314.70 314.70 314.70 312.60 31   | 0.00 314.9 |      | 313.20  |           | 414 10  | 313.98         |
| 314.90 314.90 315.70 314.20 314.90 315.70 314.20 312.60 312.60 313.70 314.20 314.30 314.20 31   | 00 314.3   |      | 314.20  | 314.50    | 010010  | 414 94         |
| 314.90 314.90 315.70 314.20 0.01 315.90 315.70 316.20  |            |      | 314.70  | 315,50    | 213.40  |                |
| 281 20 213.70 314.20 0.01 314.30   |            |      | 314.70  | 315.40    | 312.804 | 214.70         |
| 215.00 215.00 315.70 316.20 316.40 314.20 315.20 316.20 315.20 31   |            |      | 314.20  | 0.01      | 312.60  | 60.0           |
| 215.20<br>215.20<br>317.00<br>317.00<br>317.00<br>317.00<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20<br>318.20 |            |      | 316.20  | 316.40    | 314.30P | 315.60         |
| 315.20 31   | 00.        |      | 316.20  | 316.60    | 314.20  | 315.72         |
| 316.70 317.00 318.70 317.00 314.70 317.00 318.70 318.70 317.00 312.40 317.20 317.00 317.00 312.40 317.20 31   |            |      | 316.70  | 317,30    | 315.20  | 316.78         |
| 314.37 313.70 314.20 317.30 312.40 314.37 313.70 314.20 317.10 314.00 315.40 315.70 315.20 316.90 313.60 317.10 317.10 317.20 315.70 317.10 317.20 315.70 317.10 317.20 315.40 315.40 0.00 315.86 315.96 315.87 0.950 0.779 0.00 0.944 1.197 0.979   | 0.00       |      | 216.70  | 317.00    | 314,700 | 316.46         |
| 314.20 315.00   | 00.00      |      | 4.4 20  | 317.30    | 312,40  | 314,38         |
| 315.40 315.70 315.20 316.90 313.60 315.60 315.60 315.60 315.40 315.40 317.20 317.20 317.20 317.20 317.20 317.20 317.20 317.20 317.20 317.20 317.20 317.20 317.20 317.20 317.20 317.20 317.20 315.65 0.779 0.995 0.979 0.979 0.979 0.979  | 00         |      |         | 217 10    | 314.80P | 316.50         |
| 315.40 315.40 315.70 316.20 316.80 314.70 317.20 31   |            |      | 210.010 | 200       | 717.60  | 315.36         |
| 316.50 315.70 317.20 317.40 315.30P<br>317.10 317.70 317.20 317.40 315.30P<br>0.00 315.86 315.98 315.82 316.69 314.20<br>0.00 0.892 1.432 0.950 0.755 0.779<br>0.000 0.944 1.197 0.975 0.875 0.882   |            |      | 212.5   |           | 417 70  | N. N. O. N. N. |
| 317:10 317:10 317:20 317:20 317:40 313:30<br>0.00 315:86 315:95 315:82 316:69 314:20<br>0.000 0.892 1.432 0.950 0.755 0.779<br>0.000 0.944 1.197 0.975 0.875 0.882   | 20         |      | 316.20  | 310.00    |         | 70.41          |
| 0.00 315.86 315.98 315.82 316.69 0.000 0.892 1.432 0.950 0.765 0.765 0.000 0.944 1.197 0.975 0.875   |            |      | 317.20  | 317.40    | 315,307 | 210010         |
| 0.00 0.944 1.197 0.975 0.875 0.875   |            |      | 315.82  | 316.69    | 314.20  |                |
| 0.000 0.944 1.997 0.975 0.875  |            | ,    | 080     | 0.765     | 0.779   |                |
| 1000 C 10   |            |      | 2000    | 0.875     | 0.882   |                |
|  |            |      | 2/60    |           | 202     |                |
| 0.000 0.637 0.807  |            |      | 0.657   | 0.00      |         |                |
| BORT CHECKEN BANK  |            |      | 25.00   | STAN DEVE |         | JB ERR= 0.6621 |

I INDICATES THE MEASUREMENT HAS FOUND TO BE AN DUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINTS BY THE SAME INSTRUMENTS.

<sup>.</sup> INDICATES AN OUTLIER WHEN CONSIDERING THE DIFFERENCE RETWEEN INSTRUMENTS. (TWO INSTRUMENT CASE ONLY)

<sup>5</sup> INSTRUMENTS WITH 16 DATA POINTS EACH MERE USED IN THIS ANALYSIS.

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUBUST 73,8RL OBATON NORMALIZED DATA 155MM HOWITZER, MID9, ZONE 48 ROUNDS 421-440, DE - 257 MILS

|                   |       |                   |                |                                       |                |                |                                  |                | V 0.836                   |
|-------------------|-------|-------------------|----------------|---------------------------------------|----------------|----------------|----------------------------------|----------------|---------------------------|
|                   | E X   | 0.0000            | 0.9067         | 0.3807                                | 2.8200         | 4.1810         | 0.0665                           | ~              | 0.700 PARAM STD DEV 0.836 |
|                   | 4H-67 | 0.0000            | 0.5071         | 0.0000                                | 1.7135         | 5.2875         | 0,58663                          | <b>80</b>      | 0.700                     |
| COVARIANCE MATRIX | AE-2  |                   |                | 0.4483                                | 3.1300         | 3.8710         | 0.0302                           | -              | PARAMETER VARIANCE -      |
| COVARI            | 96-1  | 0.000             | 0000           | 0.5071                                | 3,3660         | 3,6349         | 0.3551                           | •              | RAMETER V                 |
|                   | H36-2 | 000               | 9898           | 0.3774                                | 2.0724         | 4.0286         | 0.0772                           | 10             | A4 0100                   |
|                   | M36-1 | DELETED<br>0.0000 | 0000           | 000                                   | 0.000          | 0.000          | 0.00000                          | •              |                           |
|                   |       | DELETED M36-1     | 136-12<br>0E-1 | N N N N N N N N N N N N N N N N N N N | COV INCLD INST | COV EXCLD INST | EST (SIGNA E1)<br>EST (SIGNA E1) | PRECISION RANK | TOTAL COVERTANCE 7.0010   |

CUSTONER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,8RL DBRYON NORMALIZED DATA 155MM HOWITZER, M109, ZONE 56 ROUNDS 701-720, DE = 660 MILS

| M M M M M M M M M M M M M M M M M M M  | ERR= 0.9001 |
|--|-------------|
|  | P 208       |
| XHR<br>370,20P<br>3667,20<br>3669,00<br>370,20P<br>370,20P<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371,00<br>371, | 1.3345 PR   |
| NH-BY 37/2, 00 3669, 40 3669, 40 37/2, 40 37/2, 40 37/2, 40 37/2, 40 37/1, 90 37/2, 60 37/2, 60 37/2, 60 37/2, 60 37/2, 60 37/2, 60 37/2, 60 37/2, 60 37/2, 60 37/2, 60 37/2, 60 37/2, 60 37/2, 60 37/2, 60 37/2, 60 37/2, 60  | STND DEV-   |
| 05 = 2<br>0 3 / 2 0 0<br>0 3 / 2 0<br>0 3 /  | 1.7810      |
| 0 E = 1 C C C C C C C C C C C C C C C C C C  | VARIANCE-   |
| MUNITION OF THE PORT OF THE PO   | AVERAGE     |
| 1  | . 370.983   |
| THE TOP TO THE   | GRAND MEAN- |

MEASUREMENTS FOUND TO BE OUTLIERS AT A 95% CONFIDENCE LEVEL ARE FOLLOWED BY I OR P. I indicates the measurement was found to be an outlier when compared to measurements of the same data point by other instruments. P indicates the measurement was found to be an outlier when compared to measurements of the same data point by other instruments.

. INDICATES AN OUTLIER WHEN CONSIDERING THE DIFFERENCE BETWEEN INSTRUMENTS. (THO INSTRUMENT CASE ONLY) S INSTRUMENTS WITH 20 DATA POINTS EACH WERE USED IN THIS ANALYSIS.

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,8RL OBRYON NORHALIZED DATA 155MM HOWITZER, MID9, ZONE 58 ROUNDS 701-720, DE = 660 MILS

|   |        |                             | COVARIAN           | COVARIANCE MATRIX |        |                  |        |
|---|--------|-----------------------------|--------------------|-------------------|--------|------------------|--------|
|   | H36-1  | # 36 • 2                    | 3E-1               | 9E-2              | NH-87  | E E              |        |
| # 0 m 1 m 1 m 1 m 1 m 1 m 1 m 1 m 1 m 1 m | 0.000  | 0ELETER<br>0,0000<br>0,0000 | 1.6697             | 1.5879            | 1.6626 | 1.6771           |        |
| DELT TEL MODEL                            | 1.5879 | 0.000                       | 1.6382             | 0.0000            | 1.5482 | 1.7145           |        |
| X X X X X X X X X X X X X X X X X X X     | 1.6626 |                             | 1.5704             | 1,7145            | 1.6072 | 0.000            |        |
| TSAL GIBNI VOC                            | 6.5973 | 0.000                       | 6.5434             | 6.4827            | 6.3884 | 6.6639           |        |
| TONE AND AND                              | 9,7436 | 000000                      | 9.7974             | 9,4522            | 9.9525 | 9.6769           |        |
| EST (SIGNA E1)                            | 0.1770 | 0.00000                     | 0.1474             | 0.2108            | 0.0059 | 0.1933           |        |
| NAME OF STREET                            | n      | 0                           | 8                  |                   | -      | •                |        |
| TOTAL COVARIANCE                          |        | 16.3409 PA                  | PARAMETER VARIANCE | IRJANCE .         | 1.634  | PARAM STD GEV. # | 1.2753 |

| 73, BRL OBRYON<br>300 MILS  |
|---|
| F.A., JULY-AUGUST<br>NDS 441-460, GE =  |
| CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,8RL OBRYON<br>Normalized data 155mm Howitzer, Ming, 70ne 3W Rounds 441-460, GE = 300 MILS |
| E TEST AT FORT  |
| CUSTOMER SERVIC<br>NORMALIZED DATA  |

| POINT DELETED 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2  |        |         | , , ,  | 95-2     | NM-87            | XMR     | NEAN             | ,     |
|--|--------|---------|--------|----------|------------------|---------|------------------|-------|
| -004   | H36-1  | 8       | 0      | <u>.</u> | <b>.</b>         | •       |                  | /     |
| -007   | ELETED |         |        |          | ******           | 217 00  |                  | /     |
| . ~ ~ ~  | 76.80  | 278.10  | 277.20 | 277.70   | 200.00           | 00.772  |                  | /     |
| u 10 =   | AR 40  | 278.50  | 277.70 | 278.20   | 278,90           | 277.40  |                  | /     |
| n <b>•</b>   | 000    |         |        | 270.20   | 279.80           | 278.60  |                  | /     |
| •  | 70.20  | 06.675  | 00.00  | 200      | 278.00           | 277.60  |                  |       |
|  | 48.40  | 248.00  | 279.20 | 276.20   | 06.072           |         |                  |       |
|  | 48 00  | 282.20  | 281.70 | 281.70   | 282,30           | 281.00  |                  |       |
|  |        | 279.50  | 279.20 | 279.20   | 279.80           | 278.40  |                  |       |
|  |        | 00 100  | 284 20 | 282.70   | 283.40           | 281.90  |                  |       |
| 2  | 10.00  | 2000    | 284 70 | 282.70   | 283.40           | 281.80  |                  |       |
| ~  | 22,00  | 203.20  | 2000   |          | 370 00           | 278.40  |                  |       |
| •  | 00.70  | 279.80  | 279,20 | 07.6/2   | 20.00            |         |                  |       |
| •  | 00 98  | 282.50  | 283,20 | 282,70   | 283,30           | 20102   |                  |       |
| ::   | ***    | 254.60  | 275.60 | 276.20   | 276.40           | 275.10  |                  |       |
| מברבונה וו   |        | 280.80  | 281.10 | 280.70   | 281.10           | 279.40P |                  |       |
| 2:   |        | 28.3.50 | 283.70 | 283.20   | 283.60           | 282,10P | 283,22           |       |
| 2  |        |         |        | 0.00     | 282.60           | 281.30  |                  |       |
| DELETER 14 3   | 00000  | 00.202  |        | 281.70   | 282.40           | 280.70  |                  |       |
| 5.   | 220.65 | 202.202 | 001107 | 200      | 281.30           | 280.10  | 281.04           |       |
| 91   | 112.80 | 261,50  | 201,00 | 2000     |                  | 280 10  |                  |       |
| 17   | 952.40 | 280.80  | 281,60 | 280.70   | 20102            | 276     |                  |       |
|  | 06.30  | 276.70  | 277.60 | 277.70   | 278,20           | 00.072  |                  |       |
|  |        | 272.10  | 283.70 | 283.70   | 284.30           | 282,50  |                  |       |
| שברבובה זה   | 00.0   | 279.20  | 279,10 | 279.20   | 280.10           | 276.40  |                  |       |
| 77.13  |        | 280.97  | 281.01 | 280.74   | 281.36           | 279.84  |                  |       |
| 2000   |        | 1 0 4   | 107.7  | 3.249    | 3,180            | 3,233   |                  |       |
| VARIANCE   | 0000   | 2000    | 2,110  | 1.802    | 1,783            | 1.798   |                  |       |
| STATE TO STA | 000.0  | 1.363   | 1,429  | 1,216    | 1,203            | 1.213   |                  |       |
|  |        |         |        | 7.6466   | STAN DEV- 1.9096 |         | PROB ERR= 1.2880 | .2880 |

MEASUREMENTS FOUND TO BE OUTLIERS AT A 95% CONFIDENCE LEVEL ARE FOLLOWED BY I OR P. I Indicates the measuremen's was found to be an outlier when compared to measurements of the same data point by other instruments. P Indicates the measurement was found to be an outlier when compared to heasurements of the same data point by other instruments.

. INDICATES AN DUTLIER WHEN CONSIDERING THE DIFFERENCE BETWEEN INSTRUMENTS. (TWO INSTRUMENT CASE ONLY)

5 INSTRUMENTS WITH 14 DATA POINTS EACH WERE USED IN THIS ANALYSIS.

|                                  | CUSTONER         | SERV<br>ED DA | ICE TEST<br>TA 155HH | AT FORT SIL          | L, CONDUCT        | ED BY F.A. | CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 75,6KL UBKINORMALIZED DATA 155MM MOMITZER, M109, ZONE 3M ROUNDS 441-460, DE m 300 MILS | 300 HILS |
|----------------------------------|------------------|---------------|----------------------|----------------------|-------------------|------------|---|----------|
|                                  |                  |               |                      | COVARIAN             | COVARIANCE MATRIX |            |   |          |
|                                  | H36-1            |               | #36-2<br>B           | 9E-1                 | 0E-2              | ZH-B7      | SE S  |          |
| DELETED H36-1                    | DELETED<br>0.000 | 900           | 0.000                | 0.0000               | 0.0000            | 0.0000     | 0.0000  |          |
| 2 - 9P x                         |                  | 000           | 4.1312               | 000000               | 3.7548            | 3,7068     | 3.7478  |          |
| 6-16                             |                  | 0000          | 3,5665               | 3,7648               | 0.0000            | 3,2055     | 3.2176  |          |
| XXX XXX                          | 00               | 00000         | 8.8879<br>8.5898     | 3.7478               | 3,2176            | 3.1897     | 0.0000  |          |
| COV INCLD INST                   |                  | 0.000.0       | 14,8254              | 15,3507              | 13.7544           | 13,6399    | 13.7448   |          |
| COV EXCLD INST                   |                  | 0.000.0       | 20.0322              | 50.3069              | 21.9032           | 22.0177    | 21.9127   |          |
| EST (SIGNA E1)<br>EST (SIGNA E1) |                  | 0.0000        | 0.1400               | 0.1997               | 0.0220            | 0.0292     | 0.0131  |          |
| PRECISION RANK                   | ¥                | •             |                      | 10                   | 2                 | m          | 1   |          |
| TOTAL COVARIANCE                 | RIANCE           | 35.6          | 35.6576 P            | PARAMETER VARIANCE - | RIANCE .          | 3.566      | PARAM STD DEV 1.8883  | . 1.8863 |

CUSTOMER BERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,8RL OBRYON

|         | H36-2    | 96-1     | GE-2     | NH-87    | XHR    |          | MEAN             |
|---------|----------|----------|----------|----------|--------|----------|------------------|
|         | BELETED  | U        | •        | la.      |        |          |                  |
|         | 306.40   | 321,60   | 321,20   | 321.70   | 320.10 | <b>B</b> | 321.15           |
| 20      | 324.70   | 323,70   | 324,30   | 322.70   | 323.10 | 2        | 30.43            |
| 7.0     | 123.20   | 323,70   | 322.70   | 323.50   | 322.00 | ñ        | 20.08            |
| 20      | 121.80   | 321.20   | 321.20   | 315,40   | 320,40 | 'n       | 50.55            |
|         | 121.20   | 321.70   | 320.70   | 321,60   | 319,50 | 'n       | 20.02            |
|         | 122 10   | 321.70   | 322.70   | 320,20   | 321,00 | 'n       | 21.40            |
| 20      | 121.50   | 321.20   | 321.20   | 321,70   | 320,50 | ñ        | 21,15            |
| 04 711  | 122.10   | 325.20   | 324.30   | 327,60 1 | 322,90 | 'n       | 55.00            |
|         | 427.60   | 323.70   | 322.70   | 323,50   | 322,40 | 'n       | 23,07            |
|         | 121 . An | 321.20   | 321.20   | 322,10   | 320,30 | 'n       | 21.20            |
|         | 117.30   | 317.70 1 | 317,20 1 | 317,50   | 316,20 | - 3      | 17.15            |
|         | 00.0     | 321.20   | 320,20   | 320,70   | 319.40 | ë        | 20.38            |
| 000     | 00.0     | 323,20   | 322,20   | 322,80   | 321.10 | 'n       | 22.33            |
| 00.0    | 00.0     | 321.20   | 320,20   | 320,80   | 319,30 | 'n       | 20.38            |
| 00.0    | 00.0     | 321.20   | 321,20   | 322,10   | 319.80 | P        | 21.07            |
|         | 00.0     | 321.20   | 321.70   | 322,20   | 320.80 | 8        | 21.48            |
| 240 40  | 000      | 321.20   | 321.70   | 322,30   | 320,30 | n        | 21,38            |
| 00      | 320.00   | 321,70   | 322,20   | 322,60   | 320,50 | 8        | 21.75            |
|         | 320.40   | 00.0     | 320,20   | 320.80   | 318.70 |          | 00.0             |
| 00.0    | 00.0     | 321,20   | 320.70   | 321.20   | 319.50 | n        | 20.65            |
| 00.00   | 00.0     | 321,83   | 321.55   | 321.01   | 320.48 |          |                  |
|         | 0000     | 2.470    | 2.478    | 3,983    | 2.386  |          |                  |
| 000     | 0000     | 1.572    | 1.574    | 1.996    | 1.545  |          |                  |
| 000     | 0.000    | 1.060    | 1.062    | 1.346    | 1.042  |          |                  |
| 12: 44: | AVEDACE  | VARIANCE | 2.8292   | STAD DEV | 1.6620 | PROB     | PROB ERR# 1.1345 |

MEASUREMENTS FOUND TO BE OUTLIERS AT A 95% CONFIDENCE LEVEL ARE FOLLOWED BY I OR P.
I INDICATES THE MEASUREMENT WAS FOUND TO BE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINTS BY THE SAME INSTRUMENTS.
P INDICATES THE HEABUREMENT WAS FOUND TO BE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.

. INDICATES AN DUTLIER WHEN CONSIDERING THE DIFFERENCE BETWEEN INSTRUMENTS. (TWO INSTRUMENT CAGE ONLY)

A INSTRUMENTS MITH 19 DATA POINTS EACH MERE UBED IN THIS ANALYSIS.

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73, BRL OBRYON NORMALIZED DATA 15544 HOWITZER, MIGG, ZONE 4M ROUNDS 461-480, GE = 229 HILS

## COVARIANCE MATRIX

| ETED DELETED 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00 |       | M36-1    | H38-2   | 1-30       | 66-2     | NH-87  | KAR                           |        |
|--|-------|----------|---------|------------|----------|--------|-------------------------------|--------|
| 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.000 |       | DEI FTED | DELETED | ပ          | •        | ы      |                               |        |
| 0.0000 0. |       | 0000     | 000000  | 0.0000     | 000000   | 0.000  | 00000                         |        |
| 0.0000 0.0000 0.0000 2.2474 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.7.2474 0.0000 0.0000 0.7.2406 2.3889 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.25946 0.48574 1   |       | 0000     | 000000  | 000000     | 0.0000   | 0.0000 | 00000                         |        |
| 0.0000 0.0000 2.2474 0.0000<br>0.0000 0.0000 2.737 2.4842<br>0.0000 0.0000 7.241h 7.1005<br>0.0000 0.0000 7.2760 7.4172<br>0.0000 0.0000 0.0873 0.2169<br>0.00000 0.0000 0.25946 0.48574 1   |       | 0000     | 0.000   | 000000     | 2.2474   | 2,7337 | 2.2604                        |        |
| 0.0000 0.0000 7.2415 2.4842<br>0.0000 0.0000 7.2415 7.1005<br>0.0000 0.0000 7.2760 7.4172<br>0.0000 0.0000 0.0873 0.2169<br>0.00000 0.0000 0.25946 0.48574 1   |       |          | 0000    | 2.2474     | 000000   | 2.4842 | 2.3680                        |        |
| 0,0000 0,0000 7,241h 7,1005 0,0000 0,0000 7,2760 7,4172 0,0000 0,0000 0,0073 0,2169 0,0000 0,0000 0,25946 0,48574 1  |       | 0000     | 00000   | 2,7337     | 2,4842   | 00000  | 2.4229                        |        |
| 0.0000 0.0000 7.241h 7.1005<br>0.0000 0.0000 7.2760 7.4172<br>0.0000 0.0000 0.0873 0.2169<br>0.00000 0.00000 0.25946 0.48574 1   |       | 000000   | 000000  | 2.2806     | 2.3889   | 2.4229 | a.000n                        |        |
| 0,0000 0,0000 7.2760 7.4172<br>0,0000 0,0000 0,0073 0,2169<br>0,00000 0,0000 0,25946 0,49574 1   | NO.   | 0.000    | 0.000   | 7.2414     | 7.1005   | 7.6409 | 7.0524                        |        |
| 0,00000 0,00000 0,0873 0,2169 0,00000 0,00000 0,25946 0,48574 1  | NST   | 0.000    | 0.000   | 7.2760     | 7.4172   | 6.8770 | 7.4653                        |        |
| D  | 613   | 0.00000  | 0.0000  | 0.0873     | 0.2169   | 1.1812 | 0.1730                        |        |
|  | ANA   | •        | •       | •          | n        |        | 8                             |        |
|  | ARIAN |          |         | RAMETER VA | RIANCE . | 2.420  | 2.420 PARAM STR DEV. = 1.5555 | 1.5555 |

JULY-AUGUST 73, BRL OBRYON

| MEAN   | _  |         |        | 380,95 |        | 377,30P 378,30 |        |       |        |        | 374,80 376,35 |        | 375,70 376,73 |        |        |       |      | 378.40 379.50 |      |        |      | 176 10 0.00 | 377.30 378.70 |      |        |       | 377.80 378.57 | 378. | 378   | 373,40 374,20 | 373.   | 376,77 | 3,148    | 774      | 197 |
|--------|----|---------|--------|--------|--------|----------------|--------|-------|--------|--------|---------------|--------|---------------|--------|--------|-------|------|---------------|------|--------|------|-------------|---------------|------|--------|-------|---------------|------|-------|---------------|--------|--------|----------|----------|-----|
| XHR    | w. |         |        |        |        |                |        |       |        |        |               |        |               |        |        | P :   |      |               |      |        |      |             |               |      |        |       |               |      |       |               | 2      |        | 3,150 3, |          |     |
| VA-B7  |    |         |        |        |        |                |        |       |        |        |               |        |               | 377,20 |        | 376.9 |      | 380,30        |      |        |      |             | 378.80        |      | 380.10 |       |               |      |       | 90            | 00     |        |          |          |     |
| 9E=2   | 6  |         |        |        |        |                |        |       | 379.00 |        |               |        |               |        | 374.50 |       |      |               |      | 377.50 |      |             | 250.00        |      | 379.50 |       |               |      |       | 374           | 374.   | 377.89 |          |          |     |
| 65-1   | c  |         |        |        |        | 374.10         |        |       |        |        | 349.60        |        |               |        |        |       |      |               |      |        |      |             |               |      |        |       |               |      |       |               |        | 00,00  |          | 000.0    |     |
| M36-2  | •  | DELETER | 375.80 | 381.20 | 170.60 | 00.0           | 178 20 |       |        |        | 00.0          | 00.0   | 00.0          | 00.0   | 00.0   | 00.0  | 00.0 | 00.0          | 00.0 | 00.0   | 00.0 | 00.0        | 269.40        | 2000 | 3/2.00 | 00.00 | 00.0          | 00.0 | 00.00 | 00.0          | 00.0   | 0.0    |          | 00000    |     |
| 1.36-1 |    |         | 478 00 | 181 40 |        | 278 70         |        | 2,000 | 01.616 | 20.675 | 274 90        | 178.00 | 177.50        |        |        |       |      | 379.70        |      |        |      |             |               |      |        |       |               |      |       |               | 373.90 |        |          |          |     |
| 4444   |    | 2101    |        |        |        | •              | •      |       | • •    | •      | ۰ ۰           | `:     | ::            | : 2    |        | 2     | 5.   | 9             | 11   | 18     | 19   |             | DELETEN 21    | 22   | 23     | 7,7   | 2.6           | 2 2  |       |               | Se     | 2767   | 50000    | 756 6740 | 200 |

MEASUREMENTS FOUND TO BE DUTLIERS AT A 95% CONFIDENCE LEVEL ARE FOLLOMED BY I OR P.
I INDICATES THE MEASUREMENT WAS FOUND TO BE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.
P INDICATES THE MEASUREMENT WAS FOUND TO BE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.

4 INSTRUMENTS WITH 28 DATA POINTS EACH WERE USED IN THIS ANALYSIS.

<sup>.</sup> INDICATES AN DUTLIER WHEN CONSIDERING THE DIFFERENCE BETWEEN INSTRUMENTS. (TWO INSTRUMENT CASE ONLY)

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,8RL OBRYON NORMALIZED DATA 155MM HOW, MID9,5M ROUNDS 721-40,786-795,0E=666-680 MIL8

|                   | XXX F  | 3,1625  | 0.0000        | 2,6763       | 0.0000                                  | 9.0538         | 8.8004         | 0.0456                                  | -              |
|-------------------|--------|---------|---------------|--------------|---|----------------|----------------|---|----------------|
|                   | NH-67  | 3,0853  | 0.0000        | 2,7951       | 3.0130                                  | 6.6935         | 8.9608         | 0.2078                                  | <b>17</b>      |
| COVARIANCE MATRIX | 8E-2   | 2,9200  | 0000          | 00000        | 2,7951                                  | 8.5934         | 9.2408         | 0.3276                                  |                |
| COVARIAN          | 9E-1   | DELETED | 0.000         | 0000         | 00000.0                                 | 0.000          | 0,0000         | 0.0000000000000000000000000000000000000 | c              |
|                   | H 36-2 | DELETED | 0.000         |              | 00000                                   | 0.000          | 0.0000         | 0.00000                                 | •              |
|                   | H36-1  |         | 0.000         | 0.0000       | 3,0853                                  | 9.1678         | 8,6864         | 0,0966                                  | ~              |
|                   |        |         | DELETER #36-2 | DELETED GE-1 | V 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | COV INCLD INST | COV EXCLD INST | EST (SIGNA E1)<br>EST (SIGNA E1)        | PRECISION RANK |
|                   |        |         |               |              |   |                |                |   |                |

2.976 PARAH STR DEV. - 1.7250 PARAMETER VARIANCE . TOTAL COVARIANCE 17.0542

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,8RL OBRYON NORMALIZED DATA 155HM MOWITZER, HIDG, ZONE 6W ROUNDS 741-760, DE = 1111 MILS

| PATA .      | H36-1   | M36-2   | 65-1    | 9E-2   | N H - 87 | XFX     | HEAM   |
|-------------|---------|---------|---------|--------|----------|---------|--------|
|             |         | •       | U       | •      | <b>L</b> |         |        |
|             |         | DELETEN | DELETED |        |          |         |        |
|             | 141 70  | 00.00   | 00.0    | 461.10 | 461.60   | 460,30  | 461,18 |
| • •         | 00 797  |         | 00.0    | 464.10 | 464.10   | 462.30P | 463,62 |
|             |         |         |         | 447 60 | 463.30   | 461.60  | 462.80 |
| •           | m/*2u   |         |         |        |          | 460 001 | 44. 87 |
| •           | 442.00  | 00.0    | 00.0    | 462,10 | 492.00   | 402.000 | /6-100 |
| 100         | 464.00  | 00.0    | 00"0    | 453.60 | 464.10   | 462.20  | 463.48 |
| •           | 465.00  | 00.0    | 00 0    | 464.60 | 164.90   | 463.106 | 464.40 |
| •           | 445 00  | 00.0    | 00.0    | 465.10 | 465.00   | 463,30P | 164.60 |
| •           | 46.4.70 | 00.0    | 00.0    | 464.60 | 444.60   | 463.20P | 464.28 |
| •           | 464 30  | 00.0    | 00.0    | 464.10 | 464.10   | 462.40P | 450.70 |
|             | 46.9 30 | -       | 00.0    | 462.60 | 462.40   | 460.80  | 462,03 |
|             | 163 70  | 00.0    | 00.0    | 463.60 | 463.60   | 462.10P | 463,25 |
|             | 462.70  | 00.0    | 00.0    | 462.60 | 462,60   | 461.60P | 462.38 |
|             | 163.70  | 00.0    | 00.0    | 463.60 | 463.60   | 462.106 | 463.25 |
|             | 463.00  | 00.0    | 00.00   | 462.60 | 463.00   | 461.40  | 462.50 |
|             | 463.00  | 00.0    | 00.0    | 462.60 | 462.70   | 461.70  | 462.50 |
| 9           | 463.30  | 462.20  | 00.0    | 463.10 | 463,10   | 461.601 | 462.78 |
| nei eten 17 | 00 0    | 00.0    | 00.0    | 463.60 | 462.49   | 461.10  | 00.0   |
|             | 463.70  | 461.90  | 00.0    | 463.60 | 464.00   | 461.406 | 463,18 |
| •           | 463.00  | 00.00   | 00.0    | 462,60 | 463.00   | 461.30  | 462,48 |
| DELETER 20  | 465.70  | 00.0    | 00.0    | 465.60 | 0.00     | 0.00    | 0.00   |
| HEAN        | 463.43  | 00.00   | 00.00   | 463.32 | 463,43   | 461.81  |        |
|             | 0.948   | 0.00    | 00000   | 1.007  | 0.935    | 0.786   |        |
|             | 0.974   | 0000    | 0000    | 1.003  | 0.967    | 984.0   |        |
|             | 0.657   | 0.000   | 0000    | 0.677  | 0.652    | 0.596   |        |
|             |         |         |         |        |          |         |        |

MEASUMEMENTS FOUND TO BE OUTLIERS AT A 95% CONFIDENCE LEVEL ARE FOLLOHED BY 1 OR P. I Indicates the Weasurement was found to be an outlier when compared to measurements of the bate data points by other instruments. P indicates the measurement was found to be an outlier when compared to measurements of the bate data point by other instruments.

+ INDICATES AN OUTLIER WHEN CONSIDERING THE DIFFERENCE BETWEEN INSTRUMENTS. (TWO INSTRUMENT CASE ONLY)

A INSTRUMENTS WITH 18 DATA POINTS EACH MERE USED IN THIS ANALYSIS.

| 5  |   |
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| 2  | 0   |
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| 4  | <b>E</b>  |
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|    | -   |
|    | W   |
|    | SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULIANUES BERVICE TEST AT FORT SILL, CONDUCTED ROUNDS 741-760, OF # 1111 MILS |
|    | 8   |
|    |   |
|    | -   |
|    |   |
|    |   |

|  | 0.0<br>888<br>80   |
|--|--|
|  |  |
|  | 0.0249<br>0.0000<br>0.0000<br>0.0000<br>2.4467<br>2.7799<br>0.0813<br>0.28511<br>4<br>4  |
|  | 0.9208<br>0.9208<br>0.09405<br>0.09405<br>0.7979<br>2.6592<br>2.6592<br>2.5674<br>0.0181<br>0.13435  |
| •                                      |  |
| STEER, MIOS. ZONE<br>COVARIANCE MATRIX | nelete<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000<br>0,0000 |
| 1554H HOM                              | DELETED<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>2.2266  |
| HER SERVIC                             | 000<br>2200<br>2200<br>2200<br>2201<br>2201<br>2201<br>2201  |
| CUSTO                                  | E  |
|  | DELETED H36"1 DELETED H36"2 DELETED H66"2 NH"87 KHR COV EXCLD ING COV EXCLD ING EST (SIGHA E EST (SIGHA E  |

CHATAMER SERVICE TEST AT FART SILL, CONDUCTER BY F.A., JULY-AUGUST 73, RPL DRRYON

| DATA         | H36-1   | H36-2   | 05-1    | GE-2     | VE-137 | KHR    | MEAN   |
|--------------|---------|---------|---------|----------|--------|--------|--------|
| PATER        | •       | •       | ပ       | c        | L.     |        |        |
|              | DELFTED | DELETER | DELETED |          |        |        |        |
| NEI ETEN 1   | 0.00    | 00.0    | 9.00    | 551.70   | 00.0   | 560.00 | 00.0   |
|              | 00.0    | 00.0    | 0.00    | 563.00 I | 543,50 | 562.63 | 563.03 |
| Bei even 1   | 00      | 00.0    | 0.00    | 566.50   | 266.30 | 559.90 | 0.00   |
|              |         | 0       | 0.0     | 535.10   | 364.00 | 564.90 | 0.0    |
| יבר ביני י   |         |         | -       | 264.00   | 555.60 | 563.50 | 00.0   |
| 0512720      |         |         | 0       | 545.00   | 565,60 | 564.60 | 545.07 |
|              |         | -       | 00.0    | 566.10   | 560.90 | 565.00 | 564.00 |
|              |         |         | 0       | 564.20   | 550.00 | 563.50 | 562.23 |
|              |         |         |         | 245.00   | 546.40 | 565.50 | 00.0   |
| שבו בגבט יי  |         | 0       | 00.0    | 553.00   | 564.10 | 563.50 | 0.0    |
|              | 844 90  |         | 00.0    | 266.00   | 546.30 | 565.30 | 565.87 |
| 11           | 864 40  |         | 00.0    | 547.40   | 0.00   | 542.50 | 00.0   |
| מברבינה וכ   | 365.40  | 00.0    | 00.0    | 165.50   | 545.40 | 564.90 | 545.33 |
| BEI CTER . 4 | 446 90  | 00.0    | 00.0    | 560.20   | 545.50 | 565.20 | 00.0   |
|              | 00 0    | 00.0    | 00.0    | 264.00   | 566.50 | 565.50 | 566.00 |
| Se eres      |         | 0       | 00.0    | 166.80   | 540.40 | 0.00   | 00.0   |
|              |         |         |         | 265.00   | 552.40 | 564.50 | 00.0   |
| מבור וביי ול |         |         | 00.0    | 365.00   | 545.40 | 564.00 | 564.80 |
|              |         |         | -       | 868.50   | 957.19 | 565.00 | 562.53 |
| . 6.         | 500.00  | 0.00    | 00.0    | 266.00   | 556.20 | 545.70 | 545.97 |
| MEAN         | 00.0    | 0.00    | 00.0    | 565.23   | 563.61 | 564.61 |        |
| VADTANCE     | 0.00    | 00000   | 0000    | 0.940    | 11.601 | 0.943  |        |
| ATAN DEV     | 000     | 0000    | 0000    | 0.990    | 3.406  | 0.971  |        |
|              | 000.0   | 0000    | 000.0   | 0.668    | 2.297  | 0.655  |        |
|              |         |         |         |          |        |        |        |

MEASUREMENTS FOUND TO BE DUTLIERS AT A OSZ CONFIDENCE LEVEL ARE FOLLOWED AY I OR P. I INDICATES THE WEASUREMENT WAS FOUND IN RE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF OTHER DATA POINTS BY THE SAME INSTRUMENTS. P INDICATES THE WEASUREMENT WAS FOUND IN RE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.

. INDICATES AN DUTLIER WHEN CONSIDERING THE DIFFERENCE RETWEEN INSTRUMENTS. (THO LASTRUMENT CASE ONLY)

3 TASTRIBEUTS WITH IN DATA POINTS EACH MERE USED IN THIS ANALYSIS.

CHSTAMER SERVICE TEST AT FORT STILL, CANDHCTED BY F.A., JULY-AUGHST 73,8RL DRRYON NOBALIZED DATA 155MM MONITZER, 4109, ZONE 74, ROHUNS 761 - 780, OE = 319 MILS

#### 0.876 PARAM STR OFV. = 0.9358 0.00000 1.8673 n.7597 0.7597 0.000.0 10.8289 3.29073 0.0274 1.6906 m CH-H7 COVARIANCE MATRIX 0.0000 0.2329 1.6871 0.9399 PARA-ETER VARIANCE = 000000 0.0000 0.000 361 FTEB 0.0000 0.0000 0.0000 0.0000 0.00000 0.000 0.000.0 C 2.6270 0.0000 DELETER 0.000 0.000 C TOTAL COVARTANCE EST (SIGNA FL) CON INCLD INST CON FYCLD INST PRFCISION RANK DELFTEN 43A-1 DELFTEN 43A-2 NELFTEN GF-1 AM-187

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUBUST 73,BPL ORRYON NORMALIZED DATA 17544 GUY, HIO7,ZONE I, ROHNDS 971-995, DE = 306 MILS

|        |          |          | Sn0.25 | 500.63 | 503,15  | A0.008  |         | 501.08 | 0.00   | 501.37    | 800 SO | 20.200 | 503.07  | 503.60  | 501.00 | 0.00   | 500.35     | 00.0   | 0.00       | 496.80   | 503,20     | 408.03 | 502,27 | 502.18   | 503.13  | 502,40 | 504.40 | 501.77 | 20 20 20 | 00.000  |        |           |       |          | Pons FRRs 1.2057 |
|--------|----------|----------|--------|--------|---------|---------|---------|--------|--------|-----------|--------|--------|---------|---------|--------|--------|------------|--------|------------|----------|------------|--------|--------|----------|---------|--------|--------|--------|----------|---------|--------|-----------|-------|----------|------------------|
| •      |          | DELETEN  | 0.00   | 0.00   | 00.0    |         |         | 60.0   | 0.00   | 200.00    |        |        | C . C   | 00.0    | CC.C   | 0.00   | 0.00       | 0.00   | 0.00       | 0.00     | 0.00       | 00.0   | 00.0   | 00.0     | 00.0    | 00.0   | 00.0   | 00.00  |          |         | 00.0   | 000.0     | 000.0 | 0.00     |                  |
| •      | L        |          | 500.40 | 500.40 | 502.50  |         | 200.000 | 502.20 | 00.0   | KA . 40   |        | 593.40 | 502.50P | 504.30  | 501.90 | 503,30 | 540.50     | 500.60 | 503.20     | 496.70 1 | 503.20     | 498.00 | 502.20 | 202.10   | 502.80P | 502.30 | 804.30 | 201.40 |          | 5,2,40  | 501.72 | 3.395     | 1.843 | 1.243    | - Nag 6720       |
|        | <b>c</b> |          | 500.20 | 500.20 | RA 2 20 | 20000   | 900.70  | 502,20 | 502.20 | 200       | 020100 | 502,20 | 503,20  | 500 20P | 501.70 | 503.20 | 500.20     | 500.70 | 503.20     | 1 02 907 | 502.70     | 407.30 | KO1 70 | Soi. 70  | 403.20  | Kn2.70 | 804 70 | 201    | 0.701    | 502.70  | Sn1.38 | 3,691     | 1.921 | 1.296    |                  |
| 1      | ပ        |          | 499.80 | 501.30 | 407 40  | 20.000  | 501.80P | 501.80 | 507 10 |           | 501.50 | 501.80 | 503.30  | 505.30  | 501.70 | 503.30 | 400 40     | A. 008 | 804 40     | 704 70 1 | 201 10     | 106 20 |        | E C 2 40 | ROT 200 | 20. 20 | 02-100 | 2000   | m/•1mc   | 503.20  | 501.61 | 3.539     | 1.908 | 1.287    |                  |
| 7-904  | •        |          | 500.60 |        |         | 300.000 | 500.60  | R01.70 | 40 100 | 2000      | 501.00 | 502.60 | 503.30  | 404.60  | 502.30 | -      |            |        | 278 60     | 37.3°50  |            | 000000 |        | 205      | 202.00  |        | 10.200 | 504.40 | 50Z.30   | 505.30P | 502.23 | 4.034     | 2,000 | 1.355    | -                |
| 1-07.1 | 4        | DEI ETFO | 00 00  |        |         |         |         |        |        |           | 55.5   | 00.0   | 00.0    | 00      |        |        |            | 00.0   |            |          |            |        |        |          | 0000    |        | n.n.   | 00.0   | 00.0     | 00.0    |        | 000       | 000.0 | 000.0    |                  |
| ATAR   | POLCE    |          |        |        | 7       | יים     | •       |        |        | nell'il n | 7      | •      | •       |         |        |        | meteren 12 | 21     | DELETER 14 | LP 12 15 | <u>e</u> ! | 1      |        | 0        | 20      | 21     | 22     | 23     | 24       | 25      | MEAN   | S-No town | 200   | PROB ERR |                  |

MEASUREMENTS FOUND TO BE OUTLIERS AT A 95% CONFIDENCE LEVFL ARF FOLLOWED BY I OR P.
I INDICATES THE MEASUREMENT WAS FOUND TO BE AN OUTLIER WHFN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.
P INDICATES THE MEASUREMENT WAS FOUND TO BE AN OUTLIER WHFN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.

<sup>.</sup> INNICATES AN OUTLIER WHEN CONSIDERING THE DIFFERENCE RETLEEN INSTRUMENTS. (TWO INSTRUMENT CASE ONLY)

A INSTRUMENTS WITH 21 DATA POINTS EACH WERE USED IN THIS ANALYSIS.

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73, BRL ORRYON NORMALIZED DATA 175MM GUY, MIO7, ZONE 1, ROUNDS 971-995, 9E = 306 MILS

|              |  | 37 0.0000      | 13 0,00000                       |
|--------------|--|----------------|----------------------------------|
| E E          | 0 W W W 0 C  | 9.8337         | 0,0757                           |
| 7 6          | 000000000000000000000000000000000000000                                      | 9.2309         | 0.9736                           |
| 96<br>0<br>0 | 3.0000   | 9.7688         | 0,3839                           |
| H36-2        | 00 N N N 0 0 0 0 N N N 0 0 0 0 N N N 0 | 10,2494        | 0,2986                           |
| #36-I        |  | 0.0000         | 0.00000                          |
|              | 20 0 1 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1                                     | 0 1 kg r       | 2<br>HA E11                      |
|              | DELFTER  | COV EXCLD INST | EST (SIGHA E1)<br>EST (SIGHA E1) |

CHRTCHER SERVICE TEST AT FORT SILL, CONOUCTED BY F.A., JULY-AUGUST 73,8PL OBRYON NORMALIZED DATA 175HH GUY, HID7,20NE 2, ROHNOS 941-96", .F = 325 HILS

|       |          |        |        | 00.00   | 00.00     |           |        |           | 00.0      | •         |        |        | 704.50  | 700.34    | n 7n7.12 | 0 204.00 | 705.16  | 705.12  | 4. 202 | 01.00   | 9 6 7 9 9 6 | 703.04 | n 7n5.72 | 0 2020 | 00.0   | n 7n7.52   | n 702,58 |         |        |        |        | •      |          |          |          | 0        |  |
|-------|----------|--------|--------|---------|-----------|-----------|--------|-----------|-----------|-----------|--------|--------|---------|-----------|----------|----------|---------|---------|--------|---------|-------------|--------|----------|--------|--------|------------|----------|---------|--------|--------|--------|--------|----------|----------|----------|----------|--|
|       |          | DELETE | 0.00   | 701.20  | 704.7     |           | 0.00   | 704,3     | 0.0       |           | 101.50 | 0.0    | 704.5   | 0.0       | 0        | C 0      | C       |         |        |         | 0.0         | c .    | C . C    | C. C   | c.c    | 0.0        | C. E     | 0.00    |        |        |        | 0.00   |          | 0.000    | 0.000    | 0.00     |  |
| VA-EX | <b>L</b> |        | 710.60 | 704.40  | 207 .0    | 01.01     | 701.40 | 706.50    | 700 KD    | 000       | 703.80 | 704.00 | 499.20P | 1404. APA | 706.70   | 707      | 708 40  |         | 704.90 | 206.907 | 703.40      | 703.40 | 705.60   | 705.00 | 273.A0 | 707.40     | 702.40   | 707 40  |        | 703.00 | 200901 | 204.24 |          | 3.0.0    | 2.832    | 1.910    |  |
| GE-2  | -        |        | 109.50 | 103.00  |           | 04.007    | 707.30 | 706.30    |           | 700,00    | 703.30 | 703.80 | 706.30  | 701.30    | 706.80   | 70.7     |         | 00.00/  | 704.80 | 706.80  | 7n3.30      | 703.30 | 705.40   | 704.80 | 707.3  | 707.30     | 702.AD   |         | 000/0/ | 703.80 | 706.30 |        | , ma. no | 3.114    | 1.745    | 1.190    |  |
| SE-1  | ပ        |        | 100.50 | 70.2 80 |           | 706.30    | 700.80 | 706 40    | 00000     | 700.30    | 703,30 | 703.60 | 705 80  | 700 80    |          |          | 703.00  | 705,30  | 705.30 | 707.30  | 703.80      | 703.80 | 705.30   | 705.80 | 707    | 706        |          |         | 7.00   | 703.30 | 706,30 |        | 704.80   | 3,173    | 1.781    | 1.202    |  |
| H36-2 | •        |        | 700 40 |         |           | 00.0      | 450.16 |           | 0.00      | 682.30    | 704.60 | 704.90 | 70 70   |           |          | /0/      | 704.604 | 704.000 | 705.60 | 707.40  | 704.00      | 707 40 | 706 30   | 105 60 | 100    |            |          | 783.311 | 704.00 | 704.30 | 707.40 |        | 705.44   | 3,345    | 1.829    | 1.234    |  |
| M36-1 | •        |        | 4.0.0  | 2/01/1  | 703.00    | 707.10    | 701 60 |           | 757.1n    | 698.90    | 704.00 | 70.460 |         | 11.0 m    | 7n1.3n   | 707.40   | 704.00  | 705.30  | 705.00 | 707 40  | 707 60      |        | 706.60   |        | 00.00/ | 704.00     | 707.70   | 701.60  | 707.40 | 704.00 | 706.30 |        | 705.01   | 1. 437   |          | 1.250    |  |
| DATA  | TNICO    |        |        | MELPTE! | DELFTER 2 | DELETER 3 |        | DELPTER 4 | DELFTED 5 | AFIFTER A |        | •      |         |           | -        | =        | 12      | 1.3     | 7      |         |             |        |          |        |        | DELETEN 20 | 7        | 22      | 23     | 76     | 25     |        | 7441     | NABTANOF | 200 0000 | 200 2000 |  |

HEASHREWENTS FOUND TO BE OUTLIERS AT A OSX CONFIDENCE LEVFL ARE FOLLOWED BY I OR P.
I INDICATES THE WEASUREMENT HAS FOUND TO BE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.
P INDICATES THE MEASUREMENT HAS FOUND TO BE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.

<sup>.</sup> INNICATES AN NUTLIER WHEN CONSIDERING THE DIFFERENCF BETWEEN INSTRUMENTS. (TWO INSTRUMENT CASE ONLY)

S INSTRUMENTS WITH 18 DATA POINTS EACH WERE USED IN THIS AVALYSIS.

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,8RL OBRYON NORMALIZED DATA 175MM GUV, MIO7,20NE 2, ROHNDS 941-965, QE = 32R MILS

| Aber a ven mee meet |        |            |                   |          |         |         |                                  |
|---------------------|--------|------------|-------------------|----------|---------|---------|----------------------------------|
|                     | c      | <b>L</b> D | 60                | 2        | •       | 7       | PRECISION RANK                   |
|                     | 0.0000 | 1.91025    | 0.2002            | 0.0649   | 0.3547  | 0.0603  | EST (SIBNA E1)<br>EST (SIGNA F1) |
|                     | 0.000  | 18.7341    | 20.0160           | 20.6248  | 20.8019 | 20.0722 | COV EXCLD INST                   |
|                     | 0.000  | 14.9822    | 12,6003           | 13,0915  | 12.9144 | 13,6442 | COV INCLD INST                   |
|                     | 0.000  | 0.000.0    | 3.5507            | 3.8448   | 0.0000  | 3,9545  | DELETED XMR                      |
|                     | 0.000  | 3.5507     | 0.000             | 3.0261   |         | 3.21/3  | 95-1                             |
|                     | 0.000  | 3.848      | 1 0061            | 20000    | 0.000   | 3,2639  | M36-2                            |
|                     | 0.000  | 3,9545     | 3,2085            | 3,2173   | 3,2639  | 0.000   | H36-1                            |
|                     | XMR    | NH-87      | 8E-2              | 9E-1     | 136-2   | #36-1   |                                  |
|                     |        |            | COVARIANCE MATRIX | COVARIAN |         |         |                                  |

CHRYTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,8PL OBRYON

| PROB ERR= 2.0907 |          | STAN NEV= 3.0996 | 3-6077                                  | AVEDAGE VARIANCES |         | •        |              |
|------------------|----------|------------------|---|-------------------|---------|----------|--------------|
|                  |          | 00000            | 1.006                                   | 1.086             | 2,693   | 2,835    | Sent Fee     |
|                  |          | 0000             | 1.491                                   | 1.410             | 3,993   | 4.204    | TAN DEV      |
|                  |          | 0.00             | 2.224                                   | 2.594             | 15,942  | 17.671   | TANTE OF     |
|                  | 00.0     | 00.0             | 915.56                                  | 915.66            | 914.97  | 914.62   | 24.54        |
|                  |          |                  | • |                   | 695.71  | 913.40   | DELETEN 30   |
| 0.00             | 911,30   | 913.60           | 00 110                                  |                   | 908.40  | 906.30   |              |
| 911.00           | 912.60   | 914.60           | 00.4.00                                 |                   | 919.50  | 916,80   | 2            |
| 916.15           | 913,80   | 915.80           | 916.40                                  | 915 90            | 2000    | 00 BUB   |              |
|                  | 908.40   | 011.00           | 910.90                                  | 010.40            | 04 100  | 00000    | DELETER 20   |
|                  | 0.0      | 869.00           | 016.91                                  | 916.90            | 841.00  |          | 2            |
|                  | 11.      | 913.80           | 913,90                                  | 913.90            | 915.50  | 000      |              |
| 00000            |          | 258.60           | 014.40                                  | 913.90            | 886.00  | - SOE    | 20 6469 24   |
| 0.0              | 20.01    | 297.10           | 914.90                                  | 914.40            | 06.916  |          | מברניוניו כל |
| A . A . O        | 915.10   | 873.00           | 914.40                                  | 913.90            | 847.40  | 00000    |              |
|                  | 909.40   | 907.60           | 911.90                                  | 911.40 1          | 1 00100 | 1 00 000 | ? ?          |
| 200              | 912.80   | 915.00           | 915.40                                  | 914.90            | 015.80  |          | 2 6          |
|                  | 914.00   | 916.00           | 916.40                                  | 915,90            | 917.90  | 00.7.00  | שברביוניו נט |
|                  | 11.0     | 562.00           | 914.40                                  | 917.90            | 665.80  |          | 1            |
| 200              | 00.0     | 917.20           | 017.40                                  | 916.90            | 010     |          | 9            |
| 20.419           | 912.10   | 914.00           | 914.40                                  | 017.40            | 00.7.0  |          | 6            |
| 915.25           | 912.60   | 915.00           | 914.90                                  | 00 2 0            |         | 910.016  | -            |
| 916,12           | 913.60   | 916,20           | 915,90                                  | 00 2 00           |         | 914.4"   | DELETER 13   |
| 00.00            | 911.90   | 00.0             | 914.40                                  | 015 40            |         | 905,00   | DELETER 12   |
| 00.0             | 913.40   | 915.00           | 915.40                                  |                   | 10100   | 914.80   | DELETER 11   |
| 0.00             | 912,10   | 914.80           | 0.00                                    | 017.40            | 91/00   | 918,50   | 6-           |
| 917.85           | 915.00   | 917.80           | 917.40                                  | 200               | 02.619  | 916.10   | •            |
| 915.52           | 0.00     | 00.0             | 00.4.0                                  |                   | 914.80  | 913.40   | ~            |
| 914.50           | 912,20   | 914.80           | 914 40                                  |                   | 910.91  | 916.10   | _            |
| 916.95           | 914.80   | 917.20           | 916.90                                  | 0017              | 9.010   | 16.516   | •            |
| 917.30           | 915.60   | 918.20           | 917.90                                  | 017 00            | 915.20  | 916.1"   | 5            |
| 915,52           | 913.00   | 915.80           | 015.0                                   |                   | 0.00    | 917.90   | DELETER 4    |
| 00.0             | 014.90   | 917.40           | 917.40                                  | 017 00            | 00.715  | 917.90   | <b>1</b> 20  |
| 017.05           | 0.00     | 910.40           | 917.40                                  | 917 40            |         | 11016    | ~            |
| 915.10           | 0.00     | 914.60           | 914.90                                  | 915.90            | 200     |          | DELETED 1    |
| 0.00             | 00.0     | 915.60           | 914.90                                  | 25 0001           | 20 7 10 |          |              |
|                  | DELETER  | DELETER          |   | 3                 |         | <        | Polut        |
|                  | <b>L</b> | w                |   |                   | 2-001   | H36-1    | DATA         |
|                  | × ×      | NH-87            | GE-2                                    | 26-1              | - 126   |          |              |

MEASUREMENTS FOUND TO BE OUTLIERS AT A 95% CONFIDENCE LEVFL ARF FOLLOMED BY 1 OR P. I INDICATES THE WEASUREMENT WAS FOUND TO BE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS. P INDICATES THE WEASUREMENT WAS FOUND TO RE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.

4 INSTRUMENTS WITH 19 DATA POINTS EACH AERF USED IN THIS ANALYSIS.

<sup>.</sup> INDICATES AN DUTLIER AMEN CONSIDERING THE DIFFERENCE RETWEEN INSTRUMENTS. (THO INSTRUMENT CASE ONLY)

CUSTOMER SERVICE TEST AT FURT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,6RL DBRYON NORMALIZED DATA 175HH GUN, HIO7,ZONE 3, ROHNDS 901-930, GE = 500 HILS

# COVARIANCE MATRIX

|                     |                                       |                              |                |                |                |                | 2.4828                     |
|---------------------|---------------------------------------|------------------------------|----------------|----------------|----------------|----------------|----------------------------|
| XHR<br>F<br>OELETED | cccccccccccc                          |                              | 0.0000         | 00000          | 0.0000         |                | 6.164 PARAM STR DEV 2.4828 |
| E E                 | 0000                                  | 00000                        | 0.000          | 0.000          | 0.0000         | •              | 6.164                      |
| 96-2                | 2.2200                                | 000000                       | 11.6782        | 25.3082        | 2.8743         | 6              | - JONE                     |
| 1-30                | 5.4623<br>4.9671<br>0.0000<br>2.2200  | 0.0000                       | 12.6494        | 24,3370        | 2.2730         | -              | PARAMETER VARIANCE .       |
| H35-2               | 14.8789<br>0.0000<br>4.9671           | 0.000.0                      | 24,3957        | 12,5908        | 3,8754         | n              |                            |
| H36-1               | 5.4523                                |                              | 25.2496        | 11,7368        | 4,7506         |                | ICE= 36.5                  |
|                     | I I I I I I I I I I I I I I I I I I I | DELETER NH-87<br>DELETER XMR | COV INCLD INST | COV EXCLD INST | EST (STANA E1) | PRECISION RANK | TOTAL COVARIANCES 35.9865  |

CUSTOMER SERVICE TEST AT PORT SILL, CONDUCTED BY F.A., JULY-AUBUST 73,8RL OSRYON

| DELETED C C C C C C C C C C C C C C C C C C C |
|---|
|   |

MEABUREMENTS FOUND TO BE OUTLIERS AT A 95% CONFIDENCE LEVEL ARE FOLLOWED BY I OR P. I Indicates the meaburement was found to be an duflier when compared to measurements of the same data point by other instruments. P Indicates the measurement was found to be an duflier when compared to measurements of the same data point by other instruments.

. INTICATES AN OUTLIER WHEN CONSIDERING THE DIFFERENCE BETWEEN INSTRUMENTS. ITWO INSTRUMENT CASE ONLY)

S INSTRUMENTS WITH 20 DATA POINTS EACH WERE USED IN THIS ANALYSIS.

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,BRL DBRYON NORMALIZED DATA A-INCH HOWITZER, MI10, ZONE 2, ROUNDS 601-620, DE = 598 MILS

|   |           |          | COVARIA    | COVARIANCE MATRIX |         |                           |      |
|---|-----------|----------|------------|-------------------|---------|---------------------------|------|
|   | M36-1     | M36-2    | 1-30       | 9E-2              | NH-87   | XHR                       |      |
|   |           | BEL ETER | O          |                   | w       |                           |      |
| N36-1                                       | 000000    | 000000   | 1,1877     | 1.1813            | 1.1944  | 1.1188                    |      |
| DELETED M36-2                               | 0.000     | 0.000    | 000000     | 0.000             | 0.0000  | 0.0000                    |      |
| GE-1  | 1.1877    | 0.000    | 000000     | 1,1400            | 1.1449  | 1.0865                    |      |
| 96-2  | 1.1813    | 000000   | 1.1400     | 0.0000            | 1.1180  | 1.0504                    |      |
| NH-87                                       | 1.1944    | 0.000    | 1.1449     | 1-1180            | 0.000   | 1.0790                    |      |
| XHR   | 1.1188    | 0.000    | 1.0866     | 1.0504            | 1.0790  | 0.0000                    |      |
| COV INCLD INST                              | 4.6822    | 0.000    | 4.5593     | 4.4897            | 4.5363  | 4.3348                    |      |
| COV EXCLD INST                              | 6.6190    | 0.000    | 6.7419     | 6.8114            | 6.7648  | 6.9663                    |      |
| EST (SIGNA E1)<br>EST (SIGNA E1)            | 0.0653    | 0.0000   | 0.1992     | 0.05352           | 0.00000 | 0.0721                    |      |
| PRECISION RANK                              | •         | c        | 16         | ~                 | -       | •                         |      |
| TOTAL COVARIANCE 11.3011 PARAMETER VARIANCE | NCE= 11.3 | 3011 PA  | PAMETER VA | RIANCE -          | 1.130   | 1-130 PARAH STD DEV 1-063 | 90 0 |

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,8RL DSRYON

| 1 302.00<br>2 303.43<br>3 304.43<br>4 303.40<br>8 303.40 | H36=2   | 05-1     | 00-0   | -                | 072     | MAN              |
|--|---------|----------|--------|------------------|---------|------------------|
| N P 4 B  |         |          | 95-26  | NH=87            | ANK     |                  |
| - a n - s  | e       | u        | •      | w                |         |                  |
| - 21 10 4 10   |         | 30.5 20  | 301.70 | 302,50           | 301,50  | 302,33           |
| N P W M  |         | 101 70   | 302.70 | 303.20           | 302,30  | 303.05           |
| n <b>4 1</b> 0   |         | 401      | 103.70 | 304.40           | 303,70  | 304.05           |
| • 10   |         | 2020     | 302.20 | 303.10           | 302,10  | 302,92           |
| n  |         | 287.20   | 303.70 | 309.20           | 308,60  | 00.00            |
| •  |         | 303.70   | 302,70 | 303.40           | 302,50  | 303.23           |
|  |         | 303.20   | 303,20 | 304.10           | 303,00  | 0.00             |
| מברבובוו / מברבובוו                                      |         | 305.20   | 303,70 | 304.90           | 304.20  | 304.58           |
|  |         | 103.20   | 302.70 | 303,50           | 302.50  | 303.17           |
| 200  |         | 303.20   | 303.20 | 304.00           | 306.50P | 304.18           |
| 20 102 nl  |         | 303 20   | 302.70 | 303,70           | 302,40  | 303,25           |
| = :  |         | 303.70   | 303.20 | 304.20           | 302,90  | 00.0             |
| DELETER 12 SEE ON  |         | 305.20   | 303.70 | 304,60           | 305,60  | 304.35           |
| SP TOP OF  |         | 303,20   | 303,20 | 304.00           | 302,90  | 303.62           |
|  |         | 305.20   | 303.70 | 304.90           | 303,50  | 304.62           |
|  |         | 101.20   | 303.20 | 304.00           | 304.80  | 303.93           |
| 2  |         | 101 20   | 302.70 | 303,60           | 302,50  | 00.00            |
| DELETER (7 SUS, TO                                       |         | 101 20   | 303.20 | 303,90           | 302,70  | 800.00           |
| 9 9  |         | 303.20   | 303.20 | 303.80           | 00.0    | 00.0             |
| 20 305,00  | 304.50  | 305.20   | 303,70 | 304,60           | 303.40  | 304.40           |
| MEAN TOA. 18   |         | 303.87   | 303.07 | 303.01           | 303.37  |                  |
| ,  |         | 0.738    | 0.374  | 0.486            | 1.929   |                  |
| STATE OF V   |         | 0.950    | 0.611  | 0.697            | 1.380   |                  |
| PROB ERR 0,462   | 0.593   | 0.879    | 0.412  | 0.470            | 0.037   |                  |
|  | 7040774 | VARIANCE | 0.7947 | STND DEV= 0.8915 |         | PROB ERR= 0.6013 |

MEASUREMENTS FOUND TO BE OUTLIERS AT A 95% CONFIDENCE LEVEL ARE FOLLOMED BY 1 OR P.
1 INDICATES THE MEASUREMENT WAS FOUND TO BE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.
P INDICATES THE MEASUREMENT WAS FOUND TO BE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.

. INDICATES AN OUTLIER WHEN CONSIDERING THE DIFFERENCE BETWEEN INSTRUMENTS. (THO INSTRUMENT CASE ONLY;

6 INSTRUMENTS WITH 15 DATA POINTS EACH WERE USED IN THIS ANALYSIS.

|                                  |         |         | COVARIAN | COVARIANCE MATRIX |         |                         |          |      |
|----------------------------------|---------|---------|----------|-------------------|---------|-------------------------|----------|------|
|                                  | #36-1   | #3A-2   | 96-1     | 96-2              | 48-87   | X X X                   |          |      |
| 1000                             |         | 0000    | 0.4214   | 0.3971            | 0.4660  | 0.5730                  |          |      |
| 10001                            |         | 0000    | 0.1750   | 0.3357            | 0,4014  | 0.2557                  |          |      |
| NOOK W                           | 7500    | 0.1750  | 00000    | 0.3274            | 0,4226  | 0.3548                  |          |      |
|                                  | 107.0   | 0 3357  | 0.3274   | 000000            | 0.4126  | 0.5533                  |          |      |
| 20.00                            |         | 7107-0  | 0.4226   | 0.4126            | 0.0000  | 0,6054                  |          |      |
| XXX                              | 0.5730  | 0.2557  | 0.3548   | 0.5533            | 0.6054  | 0.0000                  |          |      |
| COV INCLD INST                   | 2,2226  | 1.5329  | 1.7012   | 2.0262            | 2.3080  | 2.3422                  |          |      |
| COV EXCLB INST                   | 3,844   | 4,5337  | 4,3653   | 4.0403            | 3,7585  | 3,7243                  |          |      |
| EST (BIBHA E1)<br>EST (BIBHA E1) | 0.00000 | 0,6131  | 0.4942   | -0.0326           | 0.00000 | 1.16824                 |          |      |
| PRECISION RANK                   | ~       | •       | •        | n                 | -       | •                       |          |      |
|                                  |         | 10 2000 |          | - 4000            | 707-0   | PARAH STR DEV. = 0.6360 | .V. = 0. | .636 |

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,8RL DERYON NORMALIZED DATA 8-INCH HIMITZER,MIIO,ZONE 4, ROUNDS 121-640, BE - 335 MILS

|   | MONTHE |         |        |         |        |        |         |  |
|---|--------|---------|--------|---------|--------|--------|---------|--|
| ****                                    | #36m1  | H36-2   | 96-1   | 0E-2    | NH+87  | XHR    | MEAN    |  |
| TATOL                                   | •      | •       | v      | _       | 'n     |        |         |  |
|   |        | DELETER |        |         | 97 97- | 448 60 | 36.548  |  |
|   | 347.40 | 00.0    | 345.20 | 345.20  | 2000   |        | 448 02  |  |
| - (                                     | 146.40 | 00.0    | 345.20 | 344.20  | 345.40 | 242.90 | 30000   |  |
| 7                                       |        |         | 148 20 | 343.70  | 345.30 | 343.90 | 344.82  |  |
| 2                                       | 346.00 |         | 20000  | 17.4.70 | 348.80 | 344.50 | 345.48  |  |
| •                                       | 346.70 | 00.0    | 2000   |         | 246 30 | 145 An | 345.84  |  |
|   | 147 40 | 0000    | 345.20 | 344.70  | 200000 |        | 248 02  |  |
|   | 247    | 00.0    | 345.20 | 345.20  | 340.40 | 343.40 | 34.0000 |  |
|   |        |         | 147 30 | 345.70  | 347.10 | 346.10 | 340.04  |  |
| _                                       | 348,10 |         | 200    | 2.4.70  | 346.10 | 345.10 | 345.70  |  |
| •                                       | 347.40 | 00.0    | 3000   |         |        | 244 00 | 344.92  |  |
| •                                       | 44.40  | 00'0    | 345.20 | 343.70  | 243.00 |        | 248 62  |  |
|   |        | 000     | 345.20 | 344.70  | 346.10 | 345.10 | 343.62  |  |
| 10                                      | 200    |         | 148 70 | 345.20  | 00.0   | 349.00 | 0.00    |  |
| SELFTEN 11                              | 347.60 | 200.000 | 0.000  | 200     | 147 AB | 346.30 | 347.42  |  |
| 12                                      | 348.60 | 348.10  | 347.70 | 240.00  |        | 000    | 000     |  |
| TI USLE LE                              | 348.60 | 348.10  | 347.70 | 340.20  | 00000  |        |         |  |
| 100000000000000000000000000000000000000 | 246 20 | 07-971  | 345.20 | 343.70  | 345.10 | 344.   |         |  |
|   | 2000   | 200     | 347.20 | 346.70  | 348.00 | 351.30 | 2000    |  |
| 13                                      | 344.00 | 00000   | 77     | 145.20  | 346.40 | 345.40 | 345.98  |  |
| 91                                      | 347.20 | 347.20  | 242.   |         | 247    | 750.40 | 00.0    |  |
| ner eren 17                             | 347.60 | 347.40  | 00.0   |         |        | 148 00 | 98.89   |  |
|   | 346.80 | 346.00  | 345.20 | 344.70  | 240.10 |        | 24.     |  |
|   |        | 440 00  | 347.20 | 345.70  | 347.20 | 340.10 | 20000   |  |
| -                                       | 2010   |         |        | 17 272  | 346.40 | 345.40 | 340.10  |  |
| 20                                      | 347.60 | 321,10  | 343.79 | 2.000   |        |        |         |  |
|   |        | 00      | 148.70 | 344.09  | 346.31 | 345.49 |         |  |
| MEAN                                    | 347.24 |         |        | 37.0    | 0.703  | 2.789  |         |  |
| VARIANCE                                | 0.405  | 0000    | 0.420  |         |        | 1.670  |         |  |
| STAD DEV                                | 0.778  | U.00n   | 0.405  | 074.0   | 778 6  | 1.127  |         |  |
| BOUR FRE                                | 0.525  | 0,000   | 0.411  | 020.0   | 00000  | 1      |         |  |
| 273 61.64                               |        |         |        |         |        |        |         |  |

MEASUREMENTS FOUND TO BE OUTLIERS AT A 95% CONFIDENCE LEVFL ARE FOLLOWED BY 1 OR P. I indicates the measurement was found to be an dutlier when compared to measurements of the same data point by other instruments. P indicates the measurement was found to be an dutlier when compared to measurements of the same data point by other instruments.

PROB ERR= 0.7241

STND DEV= 1.0736

1.1526

AVERAGE VARIANCE

345.965

BRAND MEAN-

. INDICATES AN OUTLIER WHEN CONSIDERING THE DIFFERENCE BETWEEN INSTRUMENTS. ITWO INSTRUMENT CASE ONLY)

5 INSTRUMENTS WITH 17 DATA POINTS EACH WERE USED IN THIS ANALYSIS.

CUSTOMER SER:ICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73, BRL DSRYON NORMALIZED DATA 8-INCH HOWITZER, MIIO, ZONE 4, ROUNDS 621-640, DE - 335 MILS

|                   | 4H-87 KHR | 0.6347 1.0050 | 0.6463 | 1.1450        | 1 3,1743 4,3027 | 5.0852 3.956R  | 1 -0.0365 1.2975<br>4 0.00000 1.13906 | <b>s</b>       |  |
|-------------------|-----------|---------------|--------|---------------|-----------------|----------------|---------------------------------------|----------------|--|
| COVARIANCE MATRIX | 8E-1 8E-2 |               |        | 0.9662 1.1962 | 2.8529 3.2971   | 5.4065 4.9624  | 0.2945 0.0241                         |                |  |
|                   |           | 0,0000        | 0000   |               | 0.000           | 0.000.0        | 0.0000                                | •              |  |
|                   | #36-1     | 0.00          | 0.5649 | 0.6347        | 2.8528          | 5.3675         | 0.0536                                | •              |  |
|                   |           | H36-1         | 06-1   | 7             | COV INCLD INST  | COV EXCLD INST | EST (SIGMA E1)                        | PRECISION RANK |  |

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73, BRL DBRYON

| DATA       | H36-1     | H36-2  | 65-1     | 0E-2   | NH-87  | XHR        | HEAN   |
|------------|-----------|--------|----------|--------|--------|------------|--------|
| POINT      | •         | •      | ပ        | c      | ы      | <b>L</b> . |        |
| DE FYEN    | 000       | 415.50 | 417.80   | 416.30 | 00.0   | 415.70     | 00.0   |
|            | UL 717    | 415.00 | 415.80   | 415.30 | 416.00 | 414.80     | 415.67 |
| <b>4</b> P |           | 415.10 | 415.80   | 414.30 | 415.40 | 414.80     | 415.17 |
|            | 0 E 8 . 7 | 414.80 | 415.30   | 414.80 | 00.0   | 413,80     | 00.0   |
|            | 9 2 17    | 01.8.7 | 415.80   | 414.30 | 415,10 | 413,90     | 414.97 |
| •          | 9.7       | 415.50 | 415.80   | 414.30 | 415.40 | 414.70     | 415,30 |
| •          |           | 418.50 | 415.80   | 414.30 | 415.40 | 414.20     | 415,13 |
|            |           | 718.10 | 415.30   | 414.80 | 00.0   | 414.10     | 0.00   |
| DELETER D  |           | 418.50 | 415.80   | 414.30 | 00.0   | 414.00     | 00.00  |
|            |           | 415.10 | 415.80   | 414.30 | 415.40 | 414.00     | 415.03 |
|            |           | 713    | 415.80   | 414.80 | 415,50 | 414.30     | 415,35 |
|            | 00 817    | 415.10 | 415.30 1 | 414.30 | 414.90 | 413.80     | 414.83 |
| V P        | 200       | 415.50 | 415.80   | 414.80 | 415,60 | 414.90     | 415,42 |
|            | 04 417    | 416.50 | 415.80   | 415.80 | 416,50 | 415.40     | 416.10 |
|            | OK 917    | 415.80 | 415.80   | 415.30 | 416.00 | 414.70     | 415.65 |
| Fr 14      |           | 415.50 | 415.80   | 414.30 | 415.20 | 414.00     | 00.0   |
| DE 6769 47 |           | 415.50 | 415.80   | 414.80 | 415.40 | 414.20     | 00.0   |
|            |           | 416-10 | 415.60   | 417.80 | 416.30 | 415.70     | 00.0   |
|            | 00 917    | 416.50 | 415.80   | 415.80 | 416.50 | 415.60     | 416.18 |
| 20         | 416.60    | 416.10 | 415.80   | 414.30 | 416.10 | 414.80     | 415.62 |
| MEAN       | 414.05    | 415.65 | 415.76   | 414.76 | 415.68 | 414.61     |        |
| PIANCE     | 0 200     | 0.249  | 0.019    | 0.353  | 0.252  | 0,301      |        |
| 750 0750   | 457       | 067    | 0.139    | 0.594  | 0.502  | 0.548      |        |
| . 10 00    |           |        |          |        |        |            |        |

MEASUREMENTS FOUND TO BE OUTLIERS AT A 95% CONFIDENCE LEVEL ARE FOLLOMED BY I OR P.
I INDICATES THE MEASUREMENT WAS FOUND TO BE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINTS BY THE SAME INSTRUMENTS.
P INDICATES THE MEASUREMENT WAS FOUND TO BE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.

PROB ERR= 0.3239

0.2305 STND DEV- 0.4801

AVERAGE VARIANCE-

415.417

GRAND MEANS

<sup>.</sup> INDICATES AN OUTLIER AMEN CONSIDERING THE DIFFERENCE BETWEEN INSTRUMENTS. (TWO INSTRUMENT CASE ONLY)

A INSTRUMENTS WITH 13 DATA POINTS EACH WERE USED IN THIS ANALYSIS.

CONDUCTED BY F.A., JULY-AUGUST 73,8RL DERYON

|                                  |       | 25   | STONER SERV | TA N-INCH | HOWITZER, H | 1110, ZONE S      | G, ROUNDS | CUSTOMER SERVICE TEST AT FORT SILL, COMBUCTED BY THE SOL-820, RE = 1110 MILS NORMALIZED DATA 1-1NCH HOWITZER, MIIO, ZONE 56, ROUNDS BOI-820, RE = 1110 MILS | 1110 | 411.8 |
|----------------------------------|-------|------|-------------|-----------|-------------|-------------------|-----------|---|------|-------|
|                                  |       |      |             |           | COVARIAN    | COVARIANCE MATRIX |           |   |      |       |
|                                  |       |      | H35-1       | #3A-2     | 3<br>3      | 9E-2              | ZH-87     | r<br>gr   |      |       |
|                                  | H36-1 | ٠. ( | 00000       | 0.2135    | 0.0186      | 0,2561            | 0.2128    | 0.2221  |      |       |
|                                  | 6E-1  | N    | 0.0186      | 0,0228    | 0.0000      | 0.0192            | 0.2490    | 0.2462  |      |       |
|                                  | AH-67 | 22   | 0.2001      | 0.2337    | 0.0324      | 0.2490            | 0.0000    | 0.2427  |      |       |
| COV INCLD INST                   | כרו   | TENT | 0.8606      | 0.9315    | 0.1266      | 0.0500            | 0.9706    | 0.9542  |      |       |
| COV EXCLB INST                   | כרו   | INST | 1.5411      | 1.4703    | 2.2751      | 1.4418            | 1.4312    | 1.4475  |      |       |
| EST (SIGHA E1)<br>EST (SIGHA E1) | THE I | E11  | 0.0192      | 0.0238    | 0.1961      | 0,1128            | 0.0068    | 0.25264   |      |       |
|                                  |       |      |             |           |             |                   |           |   |      |       |

TOTAL COVARIANCE - 2.4017 PARAMETER VARIANCE -

0.160 PARAH STR DEV. = 0.4001

COV EXCLO INST EST (SIGHA E1)

PRECISION RANK

CHSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,8RL DBRYON NORMALIZED DATA A-INCH HOWITZER,MIIO,ZONE 5W, ROUNDS B21-840, QE - 518 MILS

|       |          |         |        |           |        |        |        |         |        |        |           |        |        |        |        |        |        |        |        |            |        |             |        |        |        |        |        |        |        |          |               |       |          | 0.66/3           |
|-------|----------|---------|--------|-----------|--------|--------|--------|---------|--------|--------|-----------|--------|--------|--------|--------|--------|--------|--------|--------|------------|--------|-------------|--------|--------|--------|--------|--------|--------|--------|----------|---------------|-------|----------|------------------|
| HEAN  |          |         | 0.00   | 22.30     | 20.90  | 20.93  | 20 00  |         | 120.07 | 000    | 121.38    | 121.15 | 1.0 78 | ,      | 122.95 | 0.0    | 120 A2 |        | 000    | 120.78     | 00.0   | 81.161      |        | 00000  | 419.87 | 421.65 |        |        |        |          |               |       |          | M M              |
|       |          |         |        |           |        |        |        |         |        |        |           |        |        |        |        |        |        |        |        |            |        |             |        |        |        |        |        |        |        |          |               |       | - 1      | 200              |
| XHR   | <b>L</b> |         | 00.0   | 422.50    | 420.60 | 421 00 |        | 00.020  | 420.10 | 426.50 | 422.An    | 421.00 |        | 461.10 | 422.80 | 420.90 |        | 421.00 | 0.00   | 420.60     | 420.80 | 42.64       | 66.12  | 421.40 | 419.8n | 421.70 |        | 421.29 | 0.841  | 0 017    |               | H.519 |          | 0.9896           |
| N4-67 |          |         | 420.20 | 05.127    | 420.50 | 720 80 | 000000 | 419.00F | 420.20 | 421.80 | 420.20    | 731 00 |        | 420.10 | 421.90 | 410 AO |        | 450.10 | 419.60 | 420.00     | 410.40 | 100         | 450.50 | 421.60 | 419.50 | 430    |        | 420.53 | 028 0  |          |               | 167.0 |          | STAB DEV= 0.9896 |
| nE-2  | •        | DELETED | 0.00   | 00.0      |        |        | Du     | 475.10  | 363.10 | 0.00   | 286.10    |        | 243.1" | 535.0n |        |        | 0      | C . C  | 0.0    | 00 0       |        | 461.10      | 0.00   | 391.20 | 184.00 |        | 402.10 | 0.00   | 000    | 0.00     | D.0.0         | 0.00  |          | 0.0704           |
| GE-1  | ပ        | DELFTED | 417.80 | 280 70    |        |        | 20.0   | 398.00  | 00.0   |        | 00,307    |        |        | 168.00 | 462.00 |        | Bu. B  | 00.0   | 380.10 |            |        | 418.00      | 443.50 | 00 067 | 00.00  | 61.5   | 407.60 | 0      |        | - D - D  | 0.00          | 0000  |          | VANTANCE         |
| 636-2 | •        | ,       | 421 40 |           |        | 421.nu | 421.00 | 120.70  | 40.40  |        | 10.22     | 421."" | 421.40 | 420.40 |        | 422.   | 421.00 | 421.00 | 419 00 |            | 421.00 | 120.40      | 421.40 | 422 70 |        | 420.00 | 455.00 | 17     | *****  | 0.438    | 0.799         | 0.5.0 |          | AVERAGE          |
|       | 1-000    |         |        |           |        |        |        |         |        |        |           |        |        | -      |        |        |        |        |        |            |        |             |        |        |        |        | 421.80 |        | 421.34 | 1.908    | 1881          | 620   |          | . 421.137        |
|       | 4140     |         |        | DELFTER 1 | ~      | 100    |        |         |        | •      | DELETER 7 | c      | •      |        |        | 11     | -2     |        | 0 :    | DELETER 14 | -      | NEI FTEN 16 |        |        | :      | 0      | 5      |        | 24 38  | VARIANCE | 2 6 2 6 2 6 9 | 1000  | PRUS EAR | GRAND MEAN       |

HEASUREMENTS FOUND TO BE OUTLIERS AT A 95% CONFIDENCE LEVEL ARE FOLLO4ED BY I OR P. I indicates the Heasurement aas found to be an dutlier when compared to measurements of the same data point by other instruments. P indicates the Heasurement was found to be an dutlier when compared to measurements of the same data point by other instruments.

<sup>.</sup> INDICATES AN OUTLIER WHEN CONSIDERING THE DIFFERENCE RETWEEN INSTRUMENTS. (TWO INSTRUMENT CASE ONLY)

<sup>4</sup> INSTRUMENTS WITH 15 DATA POINTS EACH WERE USED IN THIS ANALYSIS.

ICTEN BY F.A. JULY-AUGUST 73.BRL ORRYON

| NORMALIZED DATA R-INCH HINITZER, MIIO, ZONE SH, ROUNDS BZI-NAO, UE - 120 |         | £ £ C                                   | er e   | 20             | 82             | 85                               |                | DARAM STR NEV. = 0.7763 |
|--|---------|---|--|----------------|----------------|----------------------------------|----------------|-------------------------|
| 124  | M M M   | 0.5898                                  | 0.0000                                       | 1.5459         | 2.0882         | 0.71185                          | <b>P</b> 2     | HYDYG                   |
| ** **  | ZH - 67 | 0.5399                                  | 0.0000                                       | 1.6545         | 1.9795         | 0.0863                           | ~              | 707 0                   |
| COVARIANCE MATRIX  | 9E-2    | 0.0000                                  | 000000000000000000000000000000000000000      | 0.000          | 00000          | 0.0000                           | •              |                         |
| COVARIAN   | AE-1    | 0.000                                   | 00000  | 0.000          | 0.000          | 0.0000.0                         | c              |                         |
| TA A-INCH  | #35+2   | 0.8891                                  | 0.00   | 1.9290         | 1.7050         | 0.00000                          | -              |                         |
| MALIZED DA   | H35-1   | 0.0000                                  | 0000   | 2,1387         | 1.4953         | 0.9810                           | •              |                         |
| 2 2  |         | 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 06[FTED 06-1<br>NFLFTED 06-2<br>NM-07<br>MM- | COV INCLD INST | CAV EXCLP INST | EST (SIGHA F1)<br>FST (SIGHA F1) | PRECISION RANK |                         |

CHSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,BRL DBRYON NORMALIZED DATA B-INCH MOMITZER,MIIO,ZONE SW. ROUNDS BSI-890 OF # 518 MILS

|       |         |        |           |            |        |        |        |         |            |   | 0.6964    |
|-------|---------|--------|-----------|------------|--------|--------|--------|---------|------------|---|-----------|
| MEAN  | 00      | 0.0    | 0.00      | 20.30      | 3.90   | 3.60   | 3.03   | 11.10   | 11.20      |   | ERR-      |
|       |         |        |           |            | -      | 7      | *      | 7       |            |   | PROB      |
| X HR  | 6       |        | 0.00      | 422.20     | 423.50 | 423.70 | 423.20 | 421.40  | 422.50     | 422.59<br>0.671<br>0.819<br>0.553       | 1.0324    |
| N# 87 | DELETED |        | 421.43    | 0.00       |        |        | 000    | 0.00    | 0.00       |   | STAB BEV= |
| GF-2  | OFLETER | •      | 379.10    | 430.20     | 407.10 | 473.40 |        | 419.30  | 00.0       |   | 1.0659    |
| 6E-1  | DELETED |        | 06 111    | 458.00     | 407.40 | 420,30 | 50.0   | C       | 0.00       |   | VARIANCE= |
| 436-2 |         | 423.40 | 422.70    | 421.40     | 422,40 | 424.00 | 423.30 | 422./10 | 423.00     | 422.44<br>0.915<br>0.903                | AVERAGE   |
| 136-1 | Ż       | 423,80 | 423.20    | 423.50     | 422.20 | 424.20 | 423.80 | 423.20  | 420.AA     | 1.719<br>1.719<br>1.808<br>0.882        | 422.676   |
| DATA  |         | -      | neleten 2 | m <b>4</b> | , w    | •      | 1      | <       | • <u>-</u> | S C C C C C C C C C C C C C C C C C C C | 24 60     |

MFASHREMENTS FOUND TO BE DUTLIERS AT A 95% CONFIDENCE LEVFL ARE FOLLOWED BY I OR P.
I INDICATES THE HEASHREWENT WAS FOUND TO-8E AN DUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY THER INSTRUMENTS.
P INDICATES THE HEASHREWENT WAS FOUND TO RE AN DUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS. . INDICATES AN DUTLIER WHEN CONSIDERING THE DIFFERENCE BETWEEN INSTRUMENTS. (TWO INSTRUMENT CASE ONLY)

AVERAGE VARIANCES

422.676

3 INSTRUMENTS WITH 7 DATA POINTS EACH MERE USED IN THIS ANALYSIS.

# COVARIANCE MATRIX

|           |                                  |   |                |                |                |                | . 0.9212           |
|-----------|----------------------------------|---|----------------|----------------|----------------|----------------|--------------------|
|           | 1.0133                           | 0.0000  | 1.6207         | 0.9250         | 0.0000         | -              | PARAM STO BEV      |
| AH-87 XHR | 0.0000 1<br>0.0000 1<br>0.0000 0 |   | 1 0000 1       | n.n.n.n        | 0.00000        | •              | 0.849 PAR          |
| 6E-2      | 0.000<br>0.000<br>0.000          |   | 0000-0         | 0.0000         | 0.0000         | c              | - BONFIN           |
| 9E-1      | 0.0000<br>0.0000                 |   | 0.000          | 0.000          | 0.0000         | •              | PARAMETER VARIANCE |
| H36-2     | 0.9250                           |   | 1.5324         | 1.0133         | 0.2971         | 2              | 2.5457 PA          |
| 1-36-1    | 0.0000                           | 0.0000  | 1.9383         | n.6n74         | 0.3790         | n              |                    |
|           | *36-1<br>*36-2                   | neleten 9F-1<br>Deleten 48-2<br>neleten 48-97 | CON INCLO INST | CON EXCLU 14ST | EST (SIGNA FI) | PRECISION RANK | TOTAL COVARIANCE.  |

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,BRL OBRYON NORMALIZED DATA B-INCH HOWITZER,MIIO,ZONE 6W, ROUNDS 841-860, OF = 362 HILS

|           |          |          |        |          | F        | 97>       | NAM              |
|-----------|----------|----------|--------|----------|----------|-----------|------------------|
| BATA      | H36-1    | M36-2    | GE-1   | GE-2     |          |           |                  |
| POTHT     | 4        |          | 5      | •        | •        |           |                  |
|           | ***      |          | 400 An | 499.80   | 500.30   | 500,20    | 00.0             |
| DELETER 1 | 505.90   |          |        | 500 TO   | 501.10   | 501.10    | 501.12           |
| ~         | 501.80   | 000000   | 00.100 |          | 200.10   | 100.00    | 500.10           |
| •         | 20070    | 500.30   | 10.667 |          |          |           | A. 108           |
| •         | 60. 30   | 401.60   | 501.30 | 500.80   | 501.30   | 12.00c    | 21               |
| • •       |          |          | 20.30  | 501.30   | 501.80   | 500.30    | 501.35           |
|           | Sn2,10   | 90109    |        | 00 007   | 500.40   | 499.40    | 500,32           |
| c         | 500.70   | 500.30   | 501.30 | 449      |          | 100 70    | 400.52           |
| •         | KAN 40   | 407.900  | 100.80 | 409.30   | 00.006   |           |                  |
| `         |          | 00 007   | 400.30 | 498.80   | 190.60   | 06.66     | 444.03           |
| •         | attanc   |          |        | R.00.30  | 500.90   | 100.007   | 500.87           |
| •         | 501.4n   | 200      |        | 100      | KOD. 20  | 500.10    | 500.07           |
| •         | 500.70   | 500,30   | 449.00 | 30.00    |          | 404 60    | 500.50           |
|           | KAN 70   | 300.30   | 503.30 | 400.80   | 2000     | 00.000    |                  |
| 1         |          | 801 30   | 501.80 | 500,30   | 501.10   | 07.664    | 96.000           |
| 12        | 0.100    | 0, 00,   | 400 80 | 409.30   | 06.667   | 498.20    | 499.40           |
| 13        | 11.006   |          | 400    | 408.30   | 06.867   | 497.20P   | 498.62           |
| -         | 1000     | 496.90   |        |          | 400 AN   | 407 . ROP | 409.08           |
| 15        | 100.70   | 09.607   | 499.30 |          | 1 00 100 | 20.00     | 502.85           |
|           | 1 08 FOR | 503.40 1 | 503.80 | 502,30 1 | 2000.00  |           | 17 000           |
|           |          | 800 A0   | 501.30 | 500.30   | 500.70   | 408.00    | 0000             |
|           |          |          | 100    | 400.30   | 500.20   | 498.30    | 740.05           |
| =         | "Z" UUS  | 900      |        | 400 40   | 500.60   | 498.70    | 500.40           |
| •         | 501.10   | 800.00   | 201,00 |          | 000      | 407 40    | 400-17           |
| 5.        | 500.10   | 100.00   | 400.30 | 498.40   | 000.66   | •         |                  |
|           |          | .,       | 400 AO | 400.83   | 500.49   | 100.23    |                  |
| MEAN      |          |          |        | 010      | 0.870    | 1.382     |                  |
| ARTANCE   |          | 1.336    | 1000   | 2000     | E 0 0    | 1.176     |                  |
| TAD DEV   |          | 1.156    | 1.304  |          |          | 701       |                  |
| PROB ERR  | 10.668   | 0.780    | 0.420  | 0.650    |          |           |                  |
|           |          |          |        |          |          |           | 1444 0 -007 0000 |

MEASUREHENTS FOUND TO BE OUTLIERS AT A 95% CONFIDENCE LEVEL ARE FOLLOWED BY I OR P. I indicates the measurement was found to be an outlier when compared to measurements of the same data point by other instruments. P Indicates the heasurement was found to be an outlier when compared to measurements of the same data point by other instruments.

. INDICATES AN DUTLIER WHEN CONSIDERING THE DIFFERENCE BETWEEN INSTRUMENTS. (TWO INSTRUMENT CASE ONLY)

6 INSTRUMENTS WITH 19 DATA POINTS EACH WERE USED IN THIS ANALYSIS.

| E<br>X                                  |                | 164 0.8382<br>101 0.8286<br>186 0.0010 | 353 4.1923<br>330 9.9060 | 179 0.6957<br>00n 0.83410        | 2 6<br>40 PARAH STD DEV. = 0.9695       |
|---|----------------|--|--------------------------|----------------------------------|---|
| 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - | 0.9130         | 0.8854.0.8286                          | 4,5953                   | 0.0179                           | 2 0.040                                 |
| E-1 GE-2                                | 0.9246         | 0.0000                                 | 4,6545                   | 0.11129                          | E #074.04                               |
| 3E-1                                    | 1.0778         | 1.0594                                 | 5,1694                   | 0.6862                           | 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 |
| 136-2                                   | 0.9955         | 0.9360                                 | 4,7407                   | 0,3711                           | •                                       |
| H36-1                                   | 0.0000         | 0.9130                                 | 4.A353                   | -0.0264                          | _ :                                     |
|   | 135-1<br>135-1 | - C Z X                                | COV EXCLD INST           | EST (SIGNA F1)<br>FST (SIGNA F1) | PRECISION RANK 1 4 55 3                 |

CUSTOMER SERVICE TEST AT FORT SILL, CONDUCTED BY F.A., JULY-AUGUST 73,8RL DBRYON NORMALIZED DATA 8-1NCH HOMITZER,MIIO,ZONE 7W, ROUNDS 861-680, GE = 277 MILS

| 1    |         |       | 593,92  | .22    | 25      |        |        | ==        | .00      | 9.0       |        |         | Į.     | 50.    | .65    | .97     | 25     |        |         | 20.    |        | .95    | 97.    | 7.4    |          |        |        |        |          |          |       | RR- 1.4846 |
|------|---------|-------|---------|--------|---------|--------|--------|-----------|----------|-----------|--------|---------|--------|--------|--------|---------|--------|--------|---------|--------|--------|--------|--------|--------|----------|--------|--------|--------|----------|----------|-------|------------|
| NVJN | 1       |       |         |        |         |        |        |           |          |           |        |         |        |        |        |         |        |        |         |        |        |        |        |        |          |        |        |        | ٠.       |          |       | PROB ERR   |
| •    | Y W     |       | 592.10P | 591.80 | ROR AD  |        | 01.060 | 592.90    | 00.0     |           | 293.00 | 2000.70 | 593.An | 588.60 | 586.10 | 500.00  | K02 70 | 7.56.  | 290.90  | 549.20 | 591.60 | 590.00 | SAO A  |        | 200      | 588.5  | 590.9  |        | 3460     |          | 66.1  | 2,2011     |
|      | 70-87   |       | 594,30  | 593.00 | E07 70  | 201010 | 592.RO | ROR AN    | NO. 40 A | 20000     | 505.60 | 502.AD  | 595.00 | 591.60 | 500.40 | 20 202  | 2000   | 940.50 | 594.10  | 502.20 | 694.60 | K04 70 | 200 10 | 2.50   | 242.50   | 292.50 | 594.08 |        |          |          | 1,295 | STAD DEV   |
|      | AE-2    | -     | 593.80  | 503 TO |         | 500.80 | 592.30 |           |          | 243.411   | 404.80 | 591.An  | 605.30 | 500 A0 |        |         | 00.000 | 605.30 | 593.30  | 501.30 | ROT BO |        | 040    | 205.31 | 590.38   | 501.80 | 201 24 | 23.00  | 3.911    | 1.00     | 1.333 | 4.0447     |
|      | GE-1    | ပ     | 401 An  |        | 250,000 | 507.3n | 801 TO |           | 205.80   | 593.80    | 595.30 | 593.30  | KOK 30 |        |        | 100 Car | 505.3n | 595.30 | KOT R.0 | 401 AO |        | 00.000 | 242.30 | 593.30 | 591.30   | 591.80 | 70-07  | 243.60 | 3.791    | 1.947    | 1,313 | - SOLANGE  |
|      | 136-2   | æ     | 97 70   |        | 193.911 | 197.70 | 9      |           | 206.00   | 594.20    | 100.00 | 800 00  | 20 30  | 000000 | 200°   | 800° au | 906.00 | 495.70 | 00 70   |        |        | 204.40 | 993.AU | 593.2n | 585.10 I | 592.6n | ;      | 594.05 | P.00.4   | 2.840    | 1.915 | 2040574    |
|      | H36-1 H |       |         |        |         |        |        |           |          |           |        |         |        |        |        |         |        |        |         |        |        |        |        |        |          | 503.30 |        | 594.37 | 4.005    | 2.001    | 1.350 |            |
|      | DATA    | PATER |         | -      | ~       | •      | ,      | DELETER 4 | •        | SELETER 6 |        |         | •      | •      | =      | Ξ       |        | •      | e :     | •      | 13     | ٤_     | -13    | 78     |          | 200    |        | MEAN   | VADTANCE | ATAN DEV |       |            |

MEASUREMENTS FOUND TO RE DUTLIERS AT A 95% CONFIDENCE LEVEL ARE FOLLOWED BY I OR P.
I INDICATES THE MFASUREMENT WAS FOUND TO RE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.
P INDICATES THE MFASUREMENT WAS FOUND TO BE AN OUTLIER WHEN COMPARED TO MEASUREMENTS OF THE SAME DATA POINT BY OTHER INSTRUMENTS.

. INSTRUMENT CASE ONSIDERING THE DIFFERENCE RETHEEN INSTRUMENTS. (THO INSTRUMENT CASE ONLY)

6 INSTRUMENTS WITH IR DATA POINTS EACH WERE USED IN THIS ANALYSIS.

INDUCTED BY F.A., JULY-AUGUST 73,8RL DBRYON

| 7 H1LS  |                   |           |        |         |        |        |        |            |              |                |                | 1.9892        |
|---|-------------------|-----------|--------|---------|--------|--------|--------|------------|--------------|----------------|----------------|---------------|
| = 27  |                   |           |        |         |        |        |        |            |              |                |                |               |
| CUSTONEY SERVICE LESS AT FOR HAMITYER, MILO, ZONE 7M, ROUNDS 851-880, DE = 277 MILS NORMALIZED DATA A-TNCH HAMITYER, MILO, ZONE 7M, ROUNDS 851-880, DE = 277 MILS |                   | r<br>F    | 4.2182 | 4.2814  | 4.3569 | 4.2000 |        | 21.7676    | 37.5836      | 0.6631         | ur.            | PARAM STR BEV |
| W. ROUNDS   |                   | ZH-R7     | 3.6805 | 3.5686  | 3,7225 | 0.000  | 4.2000 | 18.5785    | 40.7727      | 0.3344         | •              | 1 047         |
| 110,20NE 7  | COVARIANCE MATRIX | 6E-2      | 3.8275 | . 6944  | 00000  | 3,7225 | 4.3569 | 19.7013    | 39.6499      | 0.00000        | -              |               |
| HUMITTER, H   | COVARTAN          | aE-1<br>C | 3.6755 | 3. 3.50 | 1,6944 | 3.5686 | 4.2814 | 19.0699    | 40.2813      | 0.1910         | ~              |               |
| TA A-TNCH   |                   | H3A-2     | 4.0576 | 0.000   | 2000   | 3.4048 | 4.7112 | 20,1256    | 39.2256      | 3,9362         | c              |               |
| MALIZED DA  |                   | H36-1     | 0.000  | 4.0576  | 3.6755 | 3.6806 | 4.2182 | 19.4594    | 39.4916      | 0.2101         | n              |               |
| P C P   |                   |           | #36-1  | H36-2   | 1-36   | NA - 2 | KHR    | THELD THST | EXCI II INST | EST (STONA FL) | PRECISION RANK |               |
|   |                   |           |        |         |        |        |        | 200        | CO           | FST            | 0              |               |

| 18.5      |
|--|
| INST   |
| 19 20 20 20 20 20 20 20 20 20 20 20 20 20  |
| 19 770,75711   |
| 19 370,72018   0,00000   0,00000   0,100000   0,10000   0,10000   0,10000   0,10000   0,10000   0,10000   0,10000   0,10000   0,10000    |
| 19 316,7811  |
| 10 444, 33000   1,4134   0,41745   0,14745   0,41000   0,41745   1,4134   0,41745      |
| 15 455,27041   0,00000   0,1735   0,11179   0,00000   0,1735   0,11179   0,00000   0,1735   0,11179   0,00000   0,1735   0,11179   0,00000   0,1735   0,11179   0,00000   0,1735   0,11179   0,00000   0,1735   0,11179   0,00000   0,1735   0,11179   0,00000   0,1735   0,1735   0,00000   0,000000   0,00000   0,00000   0,00000   0,00000   0,00000   0,00000   0,00000   0,00000   0,00000   0,000000   0,000000   0,000000   0,000000   0,000000   0,000000   0,00000   0,00000   0,00000   0,   |
| 17 445,47041   0.00000   |
| ISSM   SIL SHIMMAY   SIL SHIMMAX   SIL SHI   |
| ISSET   SILVARY   STATE   ST   |
| STEEN   STEE   |
| 1457   Privite   |
| 145.7   POINTS   PARA   |
| 1   100, 100   0.000   |
| 1  |
| # 175, Anthon 0, 1700 0, 1000 0, 1000 0, 1000 0, 1000 0, 1000 0, 1700  |
| 1  |
| 14 201, 2429 0 0,00000 0,10000 0,12001 0,1200 0,12004     14 10, 2429 0 0,00000 0,00000 0,12000 0,12004     15 10, 20000 0,00000 0,00000 0,12000 0,12004     15 10, 20000 0,00000 0,00000 0,23209   0,10000 0,10000 0,12000     15 10, 20000 0,00000 0,00000 0,23209   0,10000 0,10000 0,10000     15 10, 20000 0,00000 0,00000 0,23209   0,23209   0,00000 0,10000 0,10000     15 10, 20000 0,00000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,000000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00000 0,00000 0,00000 0,00000 0,00000 0,00000 0,00000     15 10, 20000 0,00   |
| 19 331, 44079   0,00000   0,00000   0,00000   0,2004   0,2004   0,000000   0,000000   0,00000   0,000000   0,000000   0,000000   0,000000   0,000000   0,000000   0,000000   0,000000   0,000000   0,000000   0,0000000   0,00000000   |
| 10 SA4_48333   |
| 10 \$AA_48333  |
| STRING   STATE   STA   |
| STATE   STATE   COLSTONER Service Test, at Fort Sill by Frankford Arsenal July-Aug 73   1857   187   |
| STANA FIL SHAMARY   MEAN   W34-1   MIA-2   RE-1   RE-2   W4-A7   XMR   ROUNDS   2   2   2   2   2   2   2   2   2  |
| ISTAN FILSHWARY   MEAN   WIGHT   MIGHT   MEAN   MEAN   MOUNDS   MEAN   MEA   |
| 19   15   19   15   19   15   19   15   19   19  |
| #### #################################   |
| ### ##################################   |
| ### ### ### ### ### ### ### ### ### ##   |
| HEAN MAN-1 M3A-2 RE-1 SEC-2 NM-57 XMR ROUNDS ZONE COSTONE ATSAN DOUGH TEST OF THE STATE OF THE S |
| Customer Service Test, at Fort Sili by Frankford Arsenal July-Aug 73  HEAN MINA-1 MINA-2 RE-1 SE-2 NM-97 KMR ROUNDS ZONE  1, 2210 N. 0.5334 N. 0.000 N. 0.0243 -0.00755 1.29746 601-620 Z  2, 41667 N. 0.1921 N. 0.2944 N. 0.02413 -0.03551 1.29746 621-610 S  2, 41667 N. 0.1921 N. 0.2974 N. 0.02413 -0.03243 N. 0.0553 SE-640 SE  1, 13667 N. 0.192 N. 0.0000 N. 0.0000 N. 0.0000 N. 0.00000 SE  1, 13667 N. 0.192 N. 0.0000 N. 0.0000 N. 0.0000 N. 0.0027 SE  2, 2779 N. 0.2743 N. 0.27107 N. 0.0000 N. 0.0000 N. 0.0000 SE  3, 2779 N. 0.2743 N. 19100 N. 0.00704 N. 33439 N. 66306 861-880 7   |
| #FAU H3A-1 H3A-2 RE-1 5E-9 NH-97 KHR ROUNDS ZONE  1,22101  |
| HEAN MIN-1 MIN-2 RE-1 SE-2 NM-97 KHR ROUNDS ZONE  S. A. S.   |
| POINTS NFAN M3A-1 M3A-2 RE-1 BE-2 NM-97 KHR ROHNIS ZONE 10 270,22100 0.0535 0.00000 0.19917 0.00285 -0.00019 0.07206 601-620 Z 17 345,04433 -0.03574 0.61308 0.49415 -0.03263 -0.06185 1.20746 621-640 S 13 415,04167 0.01921 0.02747 0.1941 0.11277 0.07618 1.20746 621-640 SC 13 415,04167 0.01921 0.02747 0.1941 0.11277 0.07618 0.0673 801-820 SC 15 421,13657 0.01921 0.02747 0.00000 0.00000 0.00000 -0.0272 881-890 SW 18 593,02778 0.21912 3.93615 0.19100 -0.00704 0.33439 0.66306 861-880 7  |
| 20 270,22100 0.0535 0.00000 0.19917 0.00285 -0.00019 0.07206 601.620 2 21 370,22100 0.05584 0.00000 0.29447 0.0243 -0.05185 1.29744 621-650 3 17 345,94471 0.05384 0.00000 0.29447 0.02413 -0.03435 1.29744 621-650 56 13 415,41667 0.01921 0.02747 0.19410 0.11277 0.00631 1.29744 621-650 56 13 415,41667 0.01921 0.02747 0.19410 0.00000 0.00000 0.00000 0.0672 881-890 58 14 422,47619 0.02743 0.27197 0.000000  |
|  |
| 13 415-41553   |
| 13 415-4167 n.01921 n.07379 n.19410 0.11277 n.00681 n.04583 801-820 56 13 421-13457 n.01921 n.07937 n.06000 0.00635 n.06753 821-80 58 15 421-13457 n.08102 n.07937 n.06000 n.00000 n.07000 n.07429 881-800 58 14 572-47819 n.072643 0.37107 n.68422 0.01239 n.01792 0.66306 861-800 7  |
| 15 421-13667 N. OFFICE - N. OFFICE N |
| 7 422-47419 6.37965 6.29714 6.00000 6.00000 6.00000 6.002729 881-890 58<br>19 560-27719 -6.0243 6.37107 6.6842 6.01239 -6.01792 6.6436 841-860 6<br>18 593,42778 6.21012 3.93615 6.19100 -6.06704 6.33439 6.66306 861-880 7  |
| 19 500 27719 -0.02643 0.37107 0.6882 0.01239 -0.01792 0.6536 841-850 0   |
| 403.42778 n.21012 3.93615 n.19100 -0.00704 0.33439 0.66306 861-880 7   |
|  |

|  | Straw at   Straw at   Straw    |          |              |     |          |       |  |              |           |               |                |               |           |           |      |    |
|--|--|----------|--------------|-----|----------|-------|--|--------------|-----------|---------------|----------------|---------------|-----------|-----------|------|----|
| First   Firs   | 15   15   15   15   15   15   15   15  | 5        | AHELSI       | ~ [ |          | 4447  |  |              | 100       | M HOWITZER    | 1102           |               | _         |           |      |    |
| STATE   STAT   | 19   20   20   20   20   20   20   20   2  |          |              |     |          |       | 4.16.  | 4.16.2       | £ 5.0     | C - 10        | 78-FN          | e I x         | ROUNINS   | ZONE      | 36   |    |
| 12   12   12   12   12   12   12   12  | 19 202-2014   0,00000  |          | INST         |     |          |       | 0 21732  | 0 2 2 2 2    | F 35108   | 0.03675       | 0.07446        | 0.24401       | 200-220   | -         | 350  |    |
|  |  |          | e 1          |     |          |       | 20090  | 246.45       | 0.4670    | 0.13547       | 0.0000         | 0.07575       | 243-263   | n         | 1250 |    |
|  |  |          | r. ·         |     |          |       | 41000  | 0.5718       | 0 21283   | 0.31838       | 0.91749        | 0.07466       | 221-241   | •         | 130  |    |
|  |  |          | <b>c</b> 1   |     | -        | 7     |  | 0.7750       | 11961 0   | 0.14902       | 965000         | 0.17.119      | 265-284   | Ŋ         | 200  |    |
| 17 445,4944   0,10000  | 19 545,47941   0.00000 0.17374   0.10744   0.10744   0.00754   311-320   7 405   1927   0.00754   1927   0.00754   1927   0.00754   1927   1927   0.00754   1927   0.00754   1927   0.00754   1927   0.00754   1927   0.00754   1927   0.00754   1927   0.00754   1927   0.00754   1927   0.00754   1927   0.00754   1927   0.00754    |          | <b>v</b> . 1 |     |          |       | 00000  | 00000        | 0 22667   | 0.3400        | 0.000.0        | 0.01630       | 301-310   | 7         | 1093 |    |
| 1  | 17 445, 2041   0,00000   1,17475   1,17475   1,17475   1,1747   1,0477   1,0477      |          | <b>P</b> : 1 |     | -        |       |  | 9000         | 68428     | 0.14659       | 0.0000         | 0.32372       | 311-320   | 7         | 1077 |    |
| 17 545, 5941   0, 10.00   4, 1744   0, 10.00   0, 11879   0, 10.00   0, 11879   0, 10.00   0, 11879   0, 10.00   0, 11879   0, 10.00   0, 11879   0, 10.00   0, 11879   0, 10.00   0, 11879   0, 10.00   0, 11879   0, 10.00   0, 11879   0, 118   | 17 545, 2041   0,0000   4,1744   0,1100   0,11   |          | r            |     | E ¥      |       | 1.4.104  | 0 01725      | 0 17325   | -0.90175      | 0,00725        | 0.00725       | 322-326   | 7         |      | -3 |
| SETAN ELI SUPPLAY   STATE      | SSTEAN STATES  |          | e n          |     | -        | 545   | 0.0000   | 4.17464      | -n. na224 | 0. 11479      | ח.חחחח.        | . 0.0000      | 327-345   |           |      | ริ |
| STITULE   STITULE   STATE      | STITUM FILE SITTUM FILE   STATE   ST   |          |              |     |          |       | Į  |              |           |               | thank ford Ame | any-vini ich  | [27       |           |      |    |
| STEAM FILE SHIPMARY  | STRING   S   |          |              |     |          |       | Cust   | omer Service |           |               | rational Ara   | Cuat out and  |           |           |      |    |
| 1971   1974      | TAST   PATE   STATE    |          | 30.00        | 2   | 200      | 3     |  |              | 15        | SAN INNITZER  | MICO           |               | 7         |           |      |    |
| 1487   POTENT   VEAN    | HAST   PRINK   VEAN   WASTIA   | 123      | I SI RAA     |     |          |       |  |              |           |               |                |               |           | 2000      | į    |    |
|  |  |          |              | 2   | 127.5    | WA AP | #36-1  | 436-2        | 65-1      | GE-2          | 15-41          | KHR           | ROUNDS    | ZONE      | 200  |    |
|  |  |          | - 22         |     | ; -      | 1001  | 0.07142  | 0.000.0      | 0.177.19  | 0.96731       | 4.17977        | 0.33272       | 401-420   |           | 23.0 |    |
|  |  |          |              |     |          | 276   | 0,00000  | กลกกล        | n.24175   | 0.41185       | 0.00440        | 0.10.103      | 501-100   | 3 5       | 6171 |    |
| STATE   STAT   | STATE   STAT   |          | * *          |     |          |       | 00000  | 0.07720      | 0.35503   | 0.03016       | 0.78966        | 0.06549       | 421-130   | 2 5       | 167  |    |
| 14 201   | 14 260 74429 0 0,0000 0,14000 0,1300 0,131   |          | r. w         |     | 2.0      | 170   | 0 17495  | חיטטיט       | 0.14739   | 0.210HS       | 10500.0        | 0.19335       | 701-720   | i i       | 000  |    |
| 0 321,4079   0 07612   0 07612   0 07572   0 07670   0 07572   0 07670   0 07672   0   | 19   19   19   19   19   19   19   19  |          | د ۱          |     |          |       | 00000  | 0.14609      | 170010    | 0.02195       | 6.0203         | 0.01.511      | 441-160   | ***       | 300  |    |
| 10 SA4_4833  | 10 374, 25500   0.05717   0.00000   0.05740   0.57740   0.04744   721, 753   0.04744   721, 753   0.04744   0.0474   |          | c. •         |     |          |       | 00000  | 0.0000       | 0.947.12  | n.21571       | 1.14121        | 0.17302       | 461-480   | 2 3       | 677  |    |
| 18 462-99861   0.07612 0.00000   0.000000   0.00000   0.00000   0.00000   0.00000   0.00000   0.00000   0.00000   0.00000   0.00000   0.00000   0.00000   0.00000   0.00000   0.00000   0.00000   0.00000   0.00000   0.00000   0.000000   0.000000   0.000000   0.000000   0.000000   0.000000   0.000000   0.000000   0.000000   0.000000   0.000000   0.000000   0.000000   0.000000   0.0000000   0.0000000   0.0000000   0.00000000   | 18 440,99861   0.02612   0.02612   0.02612   0.01020     |          | ٧,           |     |          | 377   | 0 09587  | 0.0000       | 0,0000    | 0.32760       | N.20784        | 0.04564       | 1767-797  | 2         | 2/0  |    |
| 1   544,48333   0,0000   0,0000   0,2329   10,0000   0,0000   0  | 10 504,42333   0,000000   0,00000   0,00000   0,00000   0,00000   0,00000   0,00000   0,00000   0,00000   0,00000    |          | •            |     |          |       |  | 20000        | 00000     | 0.0657.5      | 0.01405        | 0.01129       | 741-760   | 20        |      |    |
| Stepa Fil Simmary  | Stewa File Simmanay   Customer Scrutco Test, at Fort Sill by Frankford Arsenal July-Aug 73   Stewa File Simmanay   Handle   Alfa-2   GE-1   Aft-2   GE-1   Aft-2   GE-1   Aft-2   GE-1   Aft-2   Aft   |          | ₹ 1          |     |          | 407   | 20000  | 0.000        | 00000     | 0.23289       | 10. A2nA9      | -0.1644       | 761-780   | *         | 319  |    |
| STRANG FIL STAMMARY  | STRANK FILE STINMARY   STRANK SCTVICG TEST, ST FORT SILL By Frankford Arsenal July-Aug 73   STRANK FILE   STRANK SCTVICG TEST, STRANK SCTVICG TEST, STRANK SCTVICG TO STRANK   |          | <b>P</b> :   |     | -        | e.    |  |              |           |               |                |               |           |           |      |    |
| STEMA FILSHMARY   STATE   ST   | 17554 GDW, NIOT  |          |              |     |          |       | l de la constant de l | mer Scryico  | H         | rt Sill by F  | rankford Ars   | enal July-Aug |           |           |      |    |
| SIGNAL FILSHMARY   | SIGNA F   SINMARY   SINM   |          |              |     |          |       |  |              | 1753      | GIN. H107     |                |               |           |           |      |    |
| STRANG   S   | STRAM FILENING   STRAM   STR   | -        |              | ~   |          | 2011  |  |              |           |               |                |               |           |           |      |    |
| 1 SIGNA ELL SUPPLIES  2  | Signature  | 6-<br>6- |              | 4   |          | 2447  |  |              |           |               |                | 3             | Summod    | ZONE      | 30   |    |
| ## 21 501,78333 0.00000 0.35472 0.24729 0.20323 0.00000 941-955 2  ## 10 915,20132 4.75047 3.87543 7.27297 2.47429 0.00000 0.01930 3  ## 10 915,20132 4.75047 3.87543 7.27297 2.47429 0.00000 901-930 3  ## 10 915,20132 4.75047 0.05531 0.00000 0.00000 0.000000 0.00000 301-930 3  ## 11 819******  ## 12 915,20132 4.75047 0.27297 2.47429 0.00000 0.00000 301-930 3  ## 13 915,20132 0.37045 0.00000 0.00000 0.00000 0.00000 0.00000 301-930 301-9 | SIGNA   SAMPARY   SAMPAR   |          | 1000         | ā   | 1:41     |       | 1-98%  | 434-2        | 1-39      |               | / W- W W       |               | MUNICON 2 | -         | 200  |    |
| SIGNA ELI SUMMAKY  SIGNA ELI SUMMAKY  INST PRINTS REAN HAK-1 HAS-2 GEORGE CONTROL OF CON | 19 915,20132   4,7504   3,8742   0,0442   0,2022   3,04401   0,00000   901-930   3   19 915,20132   4,7504   3,8743   2,27297   2,37429   0,00000   901-930   3   19 915,20132   4,7504   3,8743   2,27297   2,37429   0,00000   901-930   3   19 915,20101   0,07206   001-930   3   19 915,20101   0,07206   001-920   2   1   10,07206   0,01000   2   1   10,07206   0,01000   2   1   10,07206   0,01000   2   1   10,07206   0,01000   2   1   10,07206   0,01000   2   1   10,07206   |          |              |     |          | 511.7 | 0.0000   | 0.29A5A      | D. 38.334 |               |                |               | 590-180   | . 7       | 325  |    |
| 19 915,20132   4,750Ac 3,87543 9,27297 2,37429 0,00000 0 0000000 0 0000000 0 000000 0 0000   | 19 915,20132   4,750AC 3,87543 2,7797 2,47479 0,00000 0,00000 0 0 0 0 0 0 0 0 0 0 0  |          |              |     |          | 7.114 | 0.06031  | 0.35.472     | 0.04492   |               |                |               | 001-010   | 94        | 200  |    |
| SIGNA E11 SUPPLAY  (SIGNA E11 SUPPLAY)  (SIGNA SUPPLAY)  (SIGNA E11 SUPP | ESIGNA ELI SUMMARY  INST POINTS HEAN MAK-1 MAK-2 GE-1 GE-2 NM-57 KM9 ROHANS ZONE  1 AND 277.22100 0.06335 0.06000 0.19917 0.00285 -0.0019 0.0726 601-520 2  1 AND 378.34 -0.03574 0.61306 0.49415 -0.03263 0.0726 0.1-660 3  1 AND 378.5433 -0.03574 0.06300 0.1927 0.00583 1.2246 621-660 3  1 AND 378.5433 -0.03757 0.19415 -0.03763 0.50673 821-840 58  1 AND 378.5457 0.20714 0.0000 0.0000 0.00722 0.69572 821-840  1 AND 378.5457 0.29714 0.0000 0.0000 0.01792 0.69572 841-860 6  1 AND 378.5779 -0.07537 0.0000 0.0000 0.01792 0.66306 861-880 7   |          | •            |     | -        | 915   | 4.75060  | 3.87543      | 2,27297   |               |                |               |           |           |      |    |
| SIGNA E11 SUPPLAY  (SIGNA E11 SUPPLACE TOSE, at Fore Sill by Frankford Arsemal July-Aug 73  (SIGNA E11 SUPPLACE  ( | ESIGNA ELI SUMMARY  INST POINTS HEAN MAK-1 MAK-2 GE-1 GE-2 NM-57 KMM ROMINIS ZONE  T DO 270.22100 0.06535 0.06000 0.1027 0.00265 0.1020 2  T 30.354333 0.06335 0.40415 0.03263 0.06535 821-660 3  T 345.5667 5.3524 0.06300 0.1027 0.00631 1.2046 621-650 4  T 345.5667 5.3524 0.06300 0.1027 0.0653 0.50673 821-840 58  T 345.5667 5.3524 0.06300 0.1027 0.0663 0.50673 821-840 58  T 345.5667 0.35102 0.06000 0.00000 0.0663 0.50673 821-840 58  T 3500.27719 -5.02643 0.2774 0.06000 0.06074 0.33439 0.66306 861-880 7  |          |              |     |          |       |  |              |           |               |                |               | ſ         |           |      |    |
| 8 INCH HOWITZER, MID  8 INCH HOWITZER, MID  1 SIMMARY  1 STATE HOLD BY THE BOUNDS AND BY THE BOUNDS AND BY THE BOUNDS AND BY TO STATE AND BY THE BOUNDS AND BY TO STATE AND BY | SIGNA E11 SUMMARY   ROLLING   RE-1   SE-2   NM-57   KMR   ROLLING   ZONE   |          |              |     |          |       | Custo  | mer Service  |           | Sill by       | rankford Ars   | enal July-Aug |           |           |      |    |
| SIGNA E     SUMMARY  | SIGNA E     SUMMARY  |          |              | •   |          |       |  |              | 8 INC     | H HOWITZER, ! | 9110           |               |           |           |      |    |
| ST POINTS  | INST POINTS KFAN HAA-1 HAA-2 GE-1 GE-2 NH-97 KHR HOLLD 2  5 0.0 270.2710.0 0.06835 0.06020 0.07265 -0.00019 0.07206 601-620 2  4 15 303.44333 -0.03574 0.61306 0.44415 -0.0355 1.05440 0.11-660 3  5 17 345.61467 0.61306 0.44415 -0.0355 1.05440 621-630 4  5 18 415.41467 0.61304 0.61437 0.11527 0.01239 0.06373 81-840 5K  5 19 500.27719 -0.02774 0.00000 0.0000 0.01792 0.66372 81-840 641-880 6  5 18 593.42778 0.21012 3.93615 0.19100 -0.00704 0.33439 0.66306 861-880 7  | EST      |              |     | 1: v.    | HARKY |  |              |           |               |                | 11/4          | 9,000     | 2002      | ë    |    |
| 57 Prints  | NST   PRINTS   1744   1744   1744   1746     |          |              |     |          |       | 476-1  | C=37#        | 65-1      | 6E-2          |                | KHR           | KUKUK     | COLUMN TO | ÷ 5  |    |
|  | # 13 A03 A0333   |          | INST         | •   | -2-6     |       | 35.65.0  | 00000        |           |               |                |               | 079-109   | , ,       | 0.01 |    |
| 17 345, 14.41   1.05,164   1.00,100   1.20447   0.12413   1.20446   0.11-0.0 56   1.20446   0.11-0.0 56   1.20446   0.11-0.0 56   1.20446   0.11-0.0 56   1.20456      |  |          | •            |     |          | 2     | 8450   | 0.61308      |           |               |                |               | 641-440   | 3 -       | 135  |    |
|  |  |          | •            |     | -        | 2     | 28.26.7  |              |           |               |                |               | 0.0-170   | , ;       | 1110 |    |
| 4 15 415.4747 0.96402 -0.07937 0.00000 0.00000 0.00675 0.50673 821-840 50 15 4221-12.647 0.95402 0.00000 0.00000 0.000000 0.000000 0.000000  | A 13 412-4770  |          | <b>r</b> .   |     |          | 340   | 200000   |              |           |               |                |               |           | 2 ?       | 9    |    |
| 1 15 421-15-77 | 4 15 421-12-77 15-75 16- |          | <            |     | -        | 415   | 20430  |              |           |               |                |               |           | e 1       |      |    |
| 3 7 427-67719 -0.027643 0.27107 0.68622 0.01239 -0.01792 0.69572 841-860 0 13 593.42778 0.21012 3.93615 0.19100 -0.06704 0.33439 0.66306 861-880 7   | 3 7 422-7515 3 1 5 500,27719 -0.01240 -0.01249 -0.01792 0.64572 541-860 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1  |          | 7            |     | -        | 421   | NO OFF   |              |           |               |                |               |           | E .       | 910  |    |
| 18 503.42778 0.21012 3.93615 0.19100 -0.03439 0.66306 861-880  | A 13 503,42778 n,21012 3,93515 n,19100 +0,00704 0,33439 0,66306 861-880 /  |          | ~            |     |          | 422   | F 900 6-   |              |           |               |                |               |           | ø :       | 797  |    |
|  | • 46   |          | •            |     | <b>.</b> | 200   | 0.21012  |              |           |               |                |               |           | -         | 117  |    |
|  | * "ric" .  |          | c            |     | •        |       |  |              |           |               |                |               |           |           |      |    |

APPENDIX C
Correspondence - BRL to FA, AMXBR-EB-FT, 11 January 1974



DEPARTMENT OF THE ARMYMr.0'Bryon/jm/4227
U.S. ARMY BALLISTIC RESEARCH LABORATORIES
ABERDEEN PROVING GROUND. MARYLAND 21005

AMXBR-EB-FT

11 January 1974

SUBJECT: Customer Service Test Results of Chronographs, Fort Sill, Oklahoma, July-August 1973

Commander
Frankford Arsenal
ATTN: SARFA-FCF-E
Bridge & Tacony Streets
Philadelphia, PA 19137

## 1. References:

- a. Frankford Arsenal (FA) Customer Service Test conducted at Fort Sill, July-August 1973.
- b. Telecons with Mr. F. Richter, FA, during period June-December 1973.
- c. Letter from FA dated 19 July 1973, to BRL, subject: Customer Service Test of Chronographs, Fort Sill, Oklahoma.
- d. Letter to ARMCOM dated 3 July 1973, subject: Customer Service Test of Chronographs, Fort Sill, Oklahoma
- 2. As requested by reference 1.c., BRL has analyzed the data of the referenced customer service test using methodology adopted by the U.S. and other NATO nations as the most efficient and unbiased means of estimating and comparing relative chronograph performance when two or more instruments are used to make simultaneous measurements of gun muzzle velocities. STANAG 4114 and ARDC TN 12 (AD732428) provide the rationale for the discussion and results that follow.
- 3. The data gathered at Fort Sill during this test were presented to the BRL in three different forms. First, the raw velocity observations were given. These velocities simply reflect what numbers were found on the display

readouts directly from the chronographs themselves. this set of data, a second set which was corrected for frequency was generated. The third and final set of data that was given to the BRL was a set of "normalized" data. These data were obtained by feeding the chronograph readings corrected for frequency into the FADAC computer and letting the FADAC program routine compute muzzle velocity. This last set of data was ued as the basis for all of the performance estimates to follow. It must be pointed out here that one very vital part of the data reduction process was omitted from the test results and this was correction for parallax. Unlike magnetic coils and most sky screens, doppler chronographs typically must be offset from the trajectory to avoid destruction by the shot and also, as in the case where several chronographs are being used at one time, the logistics of chronograph placement caused some to be farther away from the trajectory line than others. The importance of these parallax corrections has already been discussed with FA as well as the vital bearing that they have on our data analysis, however, due to lack of time and complexity in re-reducing all data tapes, BRL was asked to make chronograph estimates based on the normalized data provided. Four different models of chronographs were used in the test. There were two M36 doppler radars (M36-1, M36-2), two General Electric doppler radars (GE-1, GE-2), a Norwegian doppler radar (NM-87) and a Frankford Arsenal doppler radar prototype (XMR).

- 4. Missing data, maverick readings, and outliers had to be considered in this data analysis since a matrix with entries in every cell was necessary to obtain performance estimates properly.
- a. Where a chronograph was turned off, intentionally or unintentionally, and failed to obtain a reading, either the data from all chronographs for that specific round were deleted or consideration of other readings from that same chronograph for that specific weapon/zone/QE were also deleted, thereby maintaining a full matrix of observations.
- b. Where maverick readings (obviously extremely far from true) were encountered, these were treated as missing data.
- c. The computer program contains an outlier test which is designed to detect values which are statistically not part of the same population in which they are found. Two different

analyses were performed. The first looked at possible outlying observations within each round fired (i.e., did one chronograph record a significantly different reading than all other chronographs simultaneously looking at the same round). This test was performed on every round from every weapon contained in the service test. The second outlier test looked at possible outliers for each chronograph over each group of projectiles fixed at every initial condition (weapon/zone/QE combination). These tests were performed at the 99 percent level of confidence and data points were deleted only when they were detected as outliers by both tests.

- 5. Detecting a small constant bias in velocity measurement has always been a problem in chronograph tests. It is for this reason that the BRL, in its letter to ARMCOM on 3 July 1973 suggested that methods independent of doppler radar be used to observe velocity. Methods such as sky screens (optical) or coils (electromagnetic) were suggested as techniques which should also be used in this test since independent detection modes not dependent on doppler radar techniques would minimize the possibility of bias errors remaining undetected. This suggestion was not acted upon due to a number of reasons, and, hence, only the doppler method of velocity observation is common to all six devices. With no independent measurement being available, we must, therefore, assume that the real (unbiased true), velocity falls somewhere midway between all observations of the doppler radars.
- 6. The measurement related to successive shots, but produced by the same instrument, differs not only by the value of the instrumental error of the chronograph but, also, and often to a considerably greater degree, by the value of the random deviation of the velocity of each successive shell. Hence, traditional analysis of variance techniques could not be applied effectively to determine the accuracy and precision of the instrumentation since projectile velocity is not, in itself, a repeatable phenomenon. The methodology used by BRL takes into account these problems and computes unbiased estimates of random errors of measurement for each chronograph. These estimates are contained in Inclosure 1. Below is a brief summary of some of the terms found in these data.

"Mean" - simple arithmetic mean

"Variance" - variance of all observations in column appearing immediately above (except deleted data)

"stnd dev" - standard deviation (square root of variance)

"prob err" - .6745 of standard deviation

"grand mean" - mean of all data considered

"average variance" - arithmetic average of variances from all instruments considered

"covariance matrix" - included simply as computational information

"cov incld inst" - included simply as computational information

"cov excld inst" - included simply as computational information

\*"est (sigma<sup>2</sup>e<sub>1</sub>)" - unbiased estimate of variance in random precision error (est  $\sigma^2$ e<sub>1</sub>)

\*"est (sigma  $e_1$ )" - (est  $\sigma_{e_1}$ )

"precision rank" - a simple numerical ranking of size of each precision estimate with smallest being ranked 1

"total covariance" - included simply for computational information

"parameter variance" - estimate of the real round-toround muzzle velocity variance
due to propellant and tube
influences but free of chronograph
precision errors

The quantities marked with an asterisk (\*) above occasionally are negative due to the statistical approach used. There is no reason for alarm when these estimates become negative since (a) they are best estimates of precision and because, in some cases, the precisions are very small numerically, the estimates do occasionally fall into the negative region and, (b) these negative numbers are only slightly negative and can be treated as zero. If more information on this is desired, volume 43, pp 243-264 of the June 1948 edition of the journal of the American Statistical Association gives a comprehensive explanation.

- 7. Chronograph performance is dependent upon many factors including
  - a. velocity level being measured,
  - b. quadrant elevation (QE) of weapon,
  - c. shell cross-sectional area and surface irregularities,
  - d. baseline length,
  - e. blast and muzzle flash,
  - f. weather conditions,
  - g. skill of chronograph operators.

Looking at the test in light of each of these factors, we can make the following observations.

- a. Although the test encompassed a velocity span of approximate 730 m/s (185 m/s to 915 m/s), a linear least squares fit of precision versus velocity showed significance in the first order term only for the 175mm gun over zones 1, 2 and 3. Other systems generally showed little degradation in precision due to changing velocity levels.
- b. Since only one true replication is included (shell, weapon, and zone identical with only QE altered), that being the 105mm howitzer, zone 7, firing both at 1077 and 1093 mils, no conclusive statement can be made. Past studies have shown that doppler radar chronographs are much less affected by elevation change than instruments dependent on optical techniques.

- Caliber size did not seem to affect the ability of any chronograph to lock on and measure. The RAP shell which possess a very irregular base which fosters poor reflectivity did cause problems for some of the systems, the 105mm RAP caused erratic behavior patterns for the M36-1 as well as the XMR system. Unfortunately NM87 was turned off during the 105 RAP firing, but the reason for this has not been noted on the data sheets submitted to BRL. Only five (5) 155mm RAP projectiles were fired and of these five shell, no chronograph obtained a reading for every shot. The GE-2 unit and the NM87 obtained readings for four out of these five however, there is no way of determining which unit, if either, was reading precisely. As the result of studying the test plan drawn up by Frankford Arsenal in June, which included a small number of RAP shell to be fired, BRL recommended shortly before the test that "these hollow base shell be part of the test plan since recent tests have shown that radar tracking of these shell is more difficult due to irregularities of reflection from shell base." Since these types of shell will be encountered in the field in increasing numbers in the years just ahead, it is unfortunate that only 24 out of the approximately 800 shell expended in the subject test were from the RAP family.
- d. None of the chronograph systems possessed a particularly long or short baseline so no discussion will be made of the effects of baselength.
- The influence of blast and muzzle flash was a major factor in this test. The 8-inch howitzer, zone 5, white bag, because of its internal ballistic burning behavior, produces a large muzzle flash pattern. Looking at the results of the two occasions fired at this zone, it is immediately obvious that the flash caused serious degradation in the performance of both GE units. Not only were 50 percent of the data lost completely but the other data gathered for the most part were erroneous. The M36 units did not seem to encounter a significant data loss, but their precision errors did increase and were significantly higher than the lower zones measured. The NM87 performance and precision was good for the first data set (rounds 821-840), however, later, under identical conditions with the second set (rounds 881-890), the same unit became erratic. This is not consistent with past performance of the unit and it is suspected that the data omissions in the second data set do not reflect the instrument's true ability and typical behavior. The XMR unit was quite consistent in obtaining readings but,

in this case, was not as precise as the NM87 ( $\sigma^2_{NM87}$  = .08635

vs  $\sigma^2_{\text{NMR}}$  = .50673). Although the 175mm gun did not exhibit

the muzzle flash that the 8-inch howitzer, zone 5W, displayed, the blast (shock or overpressure) from the 175mm gun zone 3 was the maximum encountered during the test. The effects of muzzle flash caused sizeable data loss for some chronographs. Blast overpressure, on the other hand, although it caused some random data loss, caused precision to degrade also. The pooled variance in precision error for the M36 and GE systems (the only systems in the 175mm matrix) was approximately 3.4 m/s. The XMR experienced a cracked wave guide as a result of this overpressure.

- f. Weather conditions are often a consideration in chronograph operation. No data on prevailing weather was submitted to BRL as part of the data package and since normalization (extrapolation thru prevailing weather) was performed on the data by means of a FADAC computer by Frankford Arsenal, no meaningful comment on weather influences can be made.
- g. Operators familiar with their equipment were present at the test site. A total of five trained soldiers were operating the two M36 systems. General Electric had an instrumentation van with two skilled operators highly trained in the usage of their systems. Frankford Arsenal had an instrumentation van which was manned by people familiar with the XMR from its inception. The only system which did not have its own trained crew was the NM87 which is foreign made. This system was mounted on top of an excess M36 tripod. Past results of the NM87 with trained crews and developers operating it showed highly of the NM87 with trained crews and developers operating it showed highly successful and reliable results. ( $\sigma_{\rm e} \simeq .05\%$  V). Hence, the results shown in this

test for the NM87, although not bad, are not necessarily representative of the system's capabilities given a crew with the equivalent familiarity as the other systems used in this test.

8. Inclosure 2 is a summary sheet displaying the precision estimates of all of the systems tested. Two sets of data, 155mm howitzer, zone 7 RAP (rounds 781-785) and the 8-inch

howitzer, zone 5W (881-890), were not computed since data omissions prevented a large enough data matrix to determine meaningful precision estimates. Overall, no single system possessed a significantly better or worse precision than the others. On the basis of the test data alone, all that can be said concerning precision is that the pooled precision error of all systems for all conditions was held at approximately .15 percent of average velocity. It is unfortunate that the data given to BRL for analyses was not corrected for parallax since, for example, a projectile which is being tracked in a 50 foot gate beginning 25 feet from the gun by a chronograph located four feet laterally from the muzzle could experience velocity errors of the order of .4 percent. If all gating were over the same distance and triggering dependent only on distance for on-off, the errors would only be bias errors which would not affect precision estimates, however, since baselengths vary between chronographs and some have fixed gates in time (M36 and XMR), the precision estimates made are affected by parallax.

9. The summary to accompany this data analysis which will be prepared by Frankford Arsenal will hopefully elaborate on the specific reasons for data omissions throughout the test. The conclusions of the BRL regarding this test is that the data gap problem, i.e., lack of obtaining a reading, was a more serious problem than the precision of the reading itself. In the field application, consistent readings are of vital importance and data gaps regardless of the reason are intolerable.

Chief, Firing Tables Branch Exterior Ballistics Laboratory

FOR THE DIRECTOR:

2 Incls

CF (w/o Incl 1)

RIA, Attn: Dr. k. Moore OCRD, Attn: LTC Ganahl

NWL, Attn: Code EPE, Mr. L. Raymond RIA, Attn: AMSAR-RDT, Dr. E. J. Haug

APPENDIX D Test Data - Yuma Proving Ground, Yuma, Arizona - 29 March 1974

| Solition   Charge   NM87   FA   NM 67   FA   NM 65   St4.2   St4.2   St21.5   St 621.9   St 91.3   St4.2   St4.2   St 1.2     | CHARGE NM87 FA NM 87 FA  12976 544.2 2 621.5 35 621.9 22  19294 000.0 99 418.0  | 1      | Jens 1750 |        | PROCE 250R | SOR   |     | DATA  | RE       | DATA REDUCTION | No. of the last |
|--|---|--------|-----------|--------|------------|-------|-----|-------|----------|----------------|-----------------|
| MIO6 7 12976 564.2 2 621.5 35 621.9 22 MIO6 7 19294 000.0 99 418.0   | M106 7 12976 564.2 2 621.5 35 621.9 22 M106 7 19294 000.0 99 418.0  | S INCh | TOWINGER  |        | 10.11      | FA    | t   | S WN  | -        | FA             |                 |
| MIO6 7 12976 564.2 2 621.5 35 621.9 CC  MIO6 9 19294 000.0 99 448.0 ——  10155 000.0 99 794.1 ——  10558 721.1 2 763.8 794.9 28  108225 7/6.3 10 442.5 789.6 140  18222 000.0 99 442.5 789.6 140  18222 000.0 99 442.5 789.6 140  18796 7:7.9 9 429.0 791.4 126  18796 7:7.9 9 429.0 791.4 126  18797 719.8 2 438.8 793.5 28  18377 719.8 2 438.8 793.5 28  16042 7/7.7 9 502.7 791.2 126  12303 000.0 99 643.9 ——  12524 000.0 99 643.9 ——  10461 721.5 2 770.9 126 643.9 ——  105995 000.0 99 424.5 (   | MIO6 7 12976 564.2 2 621.5 35 621.9 CC  MIO6 9 19294 000.0 99 448.0 ———  I 10155 000.0 99 794.1 ———  I 1055 000.0 99 794.1 ———  I 1055 000.0 99 794.1 ———  I 1055 000.0 99 746.0 ———  I 1050 000.0 99 746.0 ————  I 1050 000.0 99 746.0 ————  I 1050 000.0 99 746.0 —————  I 1050 000.0 99 746.0 ————————————————————————————————————   | ON O   | PRO       | CHARGE | NMO        |       | †   | Ī     |          | 1              |                 |
| Mio6 9 19294 000.0 99 448.5   797.4 28   78.6 140   10155 000.0 99 794.1   | Mio6 9 19294  | 210    | M106      | 7      | 12976      | 564.2 | 2   | 621.5 | 35       |                |                 |
| XM650E3 9   13932   717.9 8   573.8   79/4   28   10155   000.0 99   794.1   | XM650E3 9   13932   717.9 8   573.8   797.4   28   10155   000.0 99   794.1   | 010    | MIOR      | o      | 19294      | 200   | 66  | 4/8.0 | 4        |                | 1               |
| 10155   000.0 99 794.1   | 10155   000.0 99 794.1  | 213    | VMACAES   | 0      | 13932      | 717.9 | 00  | 573.8 |          |                |                 |
| 10558   721.1   2   743.8   794.9 28   782.5   776.3   10   442.5   789.6   40   18225   10   442.5   789.6   40   18222   200.0 99   746.0   791.4   126   18796   717.7 9 9   429.0   791.4   126   18797   719.8   2   438.8   793.5   28   793.5   126   16042   777.7 9   502.7   791.2   126   12303   200.0 99   643.9   795.4   28   10461   721.5   2   770.9   795.4   28   10461   721.5   2   770.9   10461   721.5   2   770.9   10461   721.5   2   770.9   106.0   10   10   10   10   10   10   10   | 18225   721.1   2 763.8   794.9 28   782.5   776.3   10 442.5   789.6   40   18222   200.0   99 746.0   791.4   126   18377   719.8   2 439.8   793.5   29   793.5   28   793.5   29   793.5   28   793.5   29   793.5   28   793.5   29   29   29   29   | 416    | - I       | -      | 10155      |       | 66  | 1.461 |          | 1              |                 |
| 18225 7/6.3   1942.5 7/89,6   40   18225   194.3   10   1942.5   | 18225 7/6.3 to 442.5 789,6 t40  18222 600.0 99 746.0  18222 600.0 99 442.5  18377 719.8 2 438.8 793.5 28  18377 719.8 2 438.8 793.5 28  1 18377 719.8 2 438.8 793.5 28  1 18377 719.8 2 438.8 793.5 28  1 18377 719.8 2 438.8 793.5 28  1 18377 719.8 2 438.8 793.5 28  1 18377 719.8 2 438.8 793.5 28  1 12303 000.0 99 643.9 255.7 791.2 126  1 12524 000.0 99 643.9 795.4 28  1 1945i 721.5 2 770.9 795.4 28  1 1945i 721.5 2 770.9 795.4 28   | 315    |           |        | 10558      |       | 2   | 763.8 |          | 794.9 28       |                 |
| 18222  | 18222   | 916    | 1         |        | 10225      | 7/4.3 | 0   | 442.5 |          | 789,6 140      |                 |
| 18222   200.0 99   442.5   | 18222   | 116    |           |        | 13562      |       | 0   | 177   |          | 1              |                 |
| 18796   77.7 9 9 442.5 28   791.4   78   71.7 9 9 429.0   791.4   78   71.7 9 9 429.0   791.4   78   71.7 9 9 429.0   791.4   78   71.7 9 9 542.5   792.1 28   792.1   791.2   78   792.1   791.2   78   792.1   791.2   792.1   791.2   792.1   792 | 18796   71.79   9   442.5   791.4   786   18796   71.79   9   429.0   791.4   786   793.5   28   793.5   28   793.5   28   793.5   28   793.5   28   793.5   28   793.5   28   793.5   28   793.5   28   793.5   28   793.5 | 818    |           |        | 0/80/      | 0,000 | 2 3 | 140.0 | F        | 1              |                 |
| 18796 71.79 9 429.0 791.4 126   18377 719.8 2 438.8 793.5 28   19377 719.8 2 438.8 793.5 28   19214 723.1 2 789.5 797.1 28   16042 717.7 9 502.7 791.2 126   12524 0.00.0 99 643.9   12524 0.00.0 99 643.9   10461 721.5 2 770.9 795.4 28   10461 721.5 2 770.9   19995 0.00.0 99 424.5  | 18796 717.9 9 429.0 791.4 126   18377 719.8 2 438.8 793.5 28   18377 719.8 2 438.8 793.5 28   16214 723.1 2 789.5 797.1 28   16042 777.7 9 502.7 791.2 126   12524 0.00.0 99 643.9   10461 721.5 2 770.9 795.4 28   10461 721.5 2 770.9   19995 0.00.0 99 424.5   | 616    |           |        | 18222      | 0.000 | 20  | 442.5 | Ŧ        |                | -               |
| 18377 719.8 2 438.8 793.5 28   193.5 28   193.5 28   193.5 28   193.5 28   193.5 28   193.5 28   193.5 28   193.5 28   193.5 28   193.5 28   193.5 2   193 | 18377 719.8 2 438.8 793.5 28   | 000    | 1         |        | 18796      | 7:7.9 | a   | 459.0 | -        |                |                 |
| 14337   000.0 99 542,5   | 14337   000.0 99 562,5  | 200    |           |        | 18377      | 719.8 | 2   | 438.8 | _        |                |                 |
| 10214 723.1 2 789.5 797.1 28   16.042 7/7.7 9 502.7 791.2 126   12.303 000.0 99 643.9   12.524 0.00.0 99 643.9   10.461 721.5 2 770.9   795.4 28   10.461 721.5 2 770.9   795.4 28     19.995 0.00.0 99 424.5  | 10214 723.1 2 789.5 797.1 28  | 761    | +         |        | 14227      | 0.000 | 66  | 5,295 |          | †              |                 |
| 16042 7/7.7 9 502.7 791.2 126   12303 000.0 99 643.9   | 16042 7/7.7 9 502.7 791.2 126   12303 0000 99 455.5   | 226    | 1         | +      | 7.007      | 722.1 | ^   | 789.5 |          |                | 8               |
| 1,6042 7/7, 1 9 502.7<br>1,2303 0000 99 455.5<br>1,2524 000.0 99 443.9<br>1,9995 000.0 99 424.5 ♥ ———————————————————————————————————  | 16042 7/7.1 9 502.1   12303   12524   000.0 99 643.9   795.4 28   10461   721.5 2 770.9   795.4 28     19995   000.0 99 424.5   | 923    |           | -      | 17701      |       | ,   | 1     |          |                | 7               |
| 12303 0000 99 455.5   12524 0.00.0 99 643.9   1046  726.5   770.9   795.4 28   1046  | 12303 0000 99 455.5   12524 000.0 99 643.9   795.4 28   10461 724.5 2 770.9 795.4 28   19995 000.0 99 424.5   | 924    |           |        | 16042      | 1111  | 7   | 202.1 | +        | -              |                 |
| 12524 0.00.0 99 643.9   795.4 28   1046  721.5 2 770.9   795.4 28   1046   | 12524 0.00.0 99 643.9   795.4 28   1046  721.5 2 770.9   795.4 28   19995 000.0 99 424.5  | 925    |           |        | 12303      | 0000  | 8   | 655.5 | +        |                |                 |
| 10461 724.5 2 770.9 795.4 28<br>1,9995 000.0 99 424.5 ♥ ———————————————————————————————————  | 1046  721.5 2 770.9 795.4 28<br>  18995 000.0 99 424.5  | 937    |           |        | 12524      | 0.000 |     | 643.9 | +        |                |                 |
| (4) (8) (8) (8) (8) (8) (8) (8) (8) (8) (8   | (A) (B) (C) (B) (E) (E) (B) (C) (C) (C) (C) (C) (C) (C) (C) (C) (C  | 200    | -         | -      | 10461      | 721.5 | ٧   | 720.9 | +        |                | 0               |
|  | (A) (B) (C) (C) (C) (C) (C) (C) (C) (C) (C) (C  | 176    |           |        | 18995      | 0.000 | 66  | 424.5 | •        | 1              |                 |
|  | EDANK FORD ARSENAL WORKSHEET  | 200    | +         |        | •          | @     | 0   | 0     | <u>@</u> | <b>©</b>       |                 |
|  | EDANKFORD ARSENAL WORKSHEET   |        | +         | -      | ,          | 1     | 1   |       | _        |                | (YPG)           |

# DATA REDUCTION METHODOLOGY

## 1. Legend

A = NM87 Chronograph Readout (.25  $\times$  10<sup>-6</sup> seconds)

B = FA Processor Readout (meters/second)

C = FA Processor Gate Number

D = NM87 calculated velocity (meters/second)

E = NM87 Range (35 meters - fixed)

F = FA Processor calculated velocity (meters/second)

G = FA Processor Range (meters)

# 2. Sample Calculation: Round Number 912

#### a. NM87

Velocity = 
$$\frac{\text{Base length}}{\text{Chronograph readout}}$$
= 
$$\frac{2.016*4.0*10^{-6}}{\text{Chronograph readout (A)}}$$
= 
$$\frac{8.064*10^{-6}}{12976}$$
= 
$$621.5 \text{ meters/second}$$

### b. FA Processor

Velocity = K\*FA Processor Readout (B)

where K is the correction factor for the transmitter frequency difference between the NM87 Radar Chronograph Set and the FA Processor<sup>1</sup>

$$K = \frac{10.500}{9525} = 1.10236$$
Velocity = 1.1024\*564.2

= 621.9 meters/second

Range = Velocity (F)\*Gate Number (C)\*GW

where GW is gate width of FA Processor = .0178 seconds.

= 621.9\*2\*.0178

= 22 meters

<sup>1</sup> The FA Processor was developed by the Systems Development Division at Frankford Arsenal.

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