

①

PICATINNY ARSENAL TECHNICAL MEMORANDUM 1115

CALCULATION OF MAXIMUM
RATE OF DIELECTRIC HEATING
OF EXPLOSIVES

by
by

ALEXANDER MACKENZIE

DECEMBER 1962

H. J. MATSUGUMA ✓
Chief, Explosives
Research Section

Approved by:

L. H. Eriksen
L. H. ERIKSEN
Chief, Explosives and
Propellants Laboratory

Feltman Research Laboratories
Picatinny Arsenal
Dover, N. J.

AD-A955 144

DTIC FILE COPY

DTIC
SELLING
NOV 14 1981

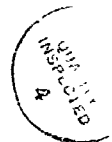
A

ACKNOWLEDGMENTS

Mr. Edmund E. Walbrecht for electrical measurements on the explosives. Complete details will be given in his forthcoming paper.

Messrs James E. Abel and F. R. Schwartz for discussions of induction time experiments and related chemistry.

Messrs Samuel Helf, Jack Alster and Dr. Joseph Cerny III for constructive criticism.



A-1

In many experiments done with explosives it is necessary to rapidly heat the explosive. The common technique is to introduce the heat by conduction. These experiments are difficult to treat theoretically because it's not at all clear what the temperature is at a small fraction of a second after the start of heat conduction. As a result interest is found in the rapid body heating of explosives where large thermal gradients can be avoided. The most obvious applicable technique is to use dielectric heating.

Before proceeding one would like to know what heating rates can be achieved placing no limit on the available power. In calculating this quantity one can argue in terms of a complex dielectric constant or an ideal condenser shunted by a resistor. Although the two approaches are essentially the same, the latter was used since it is more acceptable in the electronics laboratory.

For the resistor and lossless condenser in parallel the complex impedance is

$$1) Z^* = \frac{RX_C^2 - R^2X_C}{R^2 + X_C^2}$$

and R is the ratio of applied voltage to the current component in phase with the voltage.

This gives a phase angle χ

$$2) \tan \chi = -\frac{R}{X_C}, \text{ i.e. current leading}$$

For the average power P

$$3) P = V^2/R \quad \text{or}$$

$$4) P = \frac{V^2}{X_C \tan \chi}$$

Using MKS units and assuming a uniform field in the parallel plate condenser, the capacitive reactance is

$$5) X_C = \frac{d}{2\pi \epsilon_0 \epsilon_r A \omega}$$

where d is plate separation, A plate area, ϵ_r relative dielectric constant, ω frequency and ϵ_0 electric permittivity.

Using the maximum voltage that can be applied across the explosive

and introducing dielectric strength E.

$$6) V_{\max} = Ed = \sqrt{2} V$$

Combining equations 4, 5 and 6

$$7) P = \frac{\pi \epsilon_0 k E^2 f V}{\tan \gamma}$$

where V is the volume Ad in meters³.

Making use of the heat equation expressed in Joules

$$8) H = 10^6 \rho v s A T J$$

density ρ in gm/cm³, specific heat s in cal/gm°C, temperature ΔT in °C and J Joules/cal.

Equating Pt energy, from eq. 7 to eq. 8 and solving for the rate of change of temperature

$$9) \frac{\Delta T}{t} = \frac{\pi \epsilon_0 k f E^2}{10^6 J \rho s \tan \gamma}$$

$$10) \frac{\Delta T}{t} = 6.6 \times 10^{-18} \frac{k f E^2}{\rho s \tan \gamma}$$

In dielectric heating the loss angle- θ - is used where- θ - is the compliment of γ . Then

$$11) \frac{\Delta T}{t} = 6.6 \times 10^{-18} \frac{k f E^2 \tan \theta}{\rho s}$$

In condenser work where low losses are realized the dissipation factor, $\tan \theta$, is replaced by the power factor.

Some electrical measurements have been made on Comp B at low frequencies and room temperature. Some of the data below are from this work. The following values were used in equation 11.

For Comp B -

$$s = .3 \text{ cal/gm } ^\circ\text{C}$$

*Mr. Edmund E. Walbrecht of the Explosives Research Section, E&P Lab, FRL Picatinny Arsenal.

$$R = 3$$

$$E = 8 \times 10^6 \text{ volts/meter}$$

$$f = 50 \times 10^6 \text{ cycles/sec}$$

$$\text{Tan-}\theta = 4.5 \times 10^{-2}$$

$$\rho = 2 \text{ gm/cm}^3$$

Computing then $\frac{\Delta T}{t} = 4700^\circ\text{C/sec}$. This is the most rapid rate of heating

that can be achieved in Comp B at 50 megacycles per second no matter how much power is available. Additional power permits larger masses of explosive to be heated at this rate. Of course attempts to heat more rapidly by applying larger voltages will result in dielectric breakdown. Nevertheless higher rates can be achieved by using higher frequencies. However, to go appreciably above 50 mc/sec may introduce additional difficulties in circuit design and construction.

The power per unit volume is obtained from eq. 7 or eq. 8.

$$7) \frac{P_k}{V} = \frac{\pi \epsilon R f E^2}{10^9} \text{ Tan } \theta, \text{ watt/cm}^3 = 12 \text{ Kw/cm}^3$$

Then for one gram of Comp B the power required for maximum heating rate is 4 kilowatts.

Since the parameters used in the calculation are frequency and temperature dependent these results are approximate and subject to revision.

In conclusion the calculated heating rates and power requirements suggest that this technique has valuable applications in the explosives laboratory. The most apparent application is to the determination of induction time as a function of temperature for the short times. Presently induction times much below $\frac{1}{2}$ second are in considerable doubt.

With dielectric heating a temperature stop can be applied to the sample. Thermocouples for measuring sample temperature need not have a response of the order of the temperature rise time of the sample because the plateau would fall off very slowly. However, in the case of explosives, thermocouples must be fast enough to permit the measurement to be made before detonation occurs. Since the heat is generated uniformly through the volume of the sample thermal gradients arise from heat loss only. This effect can be minimized by a suitable choice of environment. In order to prevent electrical breakdown the surrounding must have greater dielectric strength (more properly dielectric strength times path length) than the sample. From both considerations, an evacuated container with internally reflecting