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REPORT NO. 710/464

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Report No. 710/464 Watertown Arsenal (Problem No. D-8)

November 2, 1942

FLAME CUTTING OF ARMOR

1" Rolled Homogeneous Armor (0.30% C)

the g OBJECT

To determine the maximum hardness developed by flame cutting armor plate of 0.30% carbon grade at room temperature, and to determine the preheat necessary to reduce this hardness to 400 Brinell.

- 1. The maximum hardness developed in flame affected area in armor plate of compositions investigated when flame cut at room temperature is approximately 500 Brinell.
- 2. A preheat of 400° F. is sufficient to limit this maximum hardness to 400 Brinell.

Senior Welding Engineer

This document has been approved Ordnarice Department

Director of Laboratory

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INTRODUCTION

Armor plate of the 0.30% carbon grade has shown a tendency toward excessive hardening and cracking at edges flame cut without preheating. It was, therefore, suggested by members of the Subcommittee for Welding of Armor that a few tests be made at this ersenal to determine the extent of preheating necessary to minimize the tendency toward cracking. The opinion of members of the Subcommittee was that flame cut edges with a maximum hardness of 400 Brinell would not crack.

TEST PROCEDURE

One inch thick plates of armor with the desired carbon content which had been submitted to the Armor Section of the Laboratory for ballistic testing were obtained after completion of ballistic tests. Preliminary experiments indicated that the following flame cutting conditions gave a cut similar to those obtained in commercial practice and these conditions were observed in all tests,

Travel speed 14 inches per minute
Oxygen pressure 60 lbs. per sq. in.
Type of torch No. 2 Harris tip

Four flame cuts were made at room temperature, and 200°, 400°, and 600° F. preheats, respectively in a 6" x 12" plate, made by the Great Lakes Steel Coproration. Specimens were taken at the flame cut edge and surveyed for hardness. The 400° preheat appeared adequate in these tests. To check this an 18 inch cut was then made at 400° preheat in the long leg of an H plate which had been welded from armor plate, made by Simonds Saw and Steel Company. The hardness in 300 bevel cuts was then determined by making two 9 inch cuts, one at room temperature and the other at 400° preheat, in the other leg of the H plate. Location of all flame cuts and of hardness specimens is shown in Figure 1.

Preheating was carried out by heating the small specimens to 50° over the preheat temperature in a small heattreating furnace, then allowing them to cool in air to the proper temperature before making the flame cut. Preheating for the 9 and 18 inch cuts was carried out with a gas torch. Plate in the region where the out was to be made was heated to about 500 above the desired preheat temperature and flame cut was made after this area had cooled to proper temperature.

All final operating temperatures were determined by the use of Tempils.

Hardness surveys, macro- and microexaminations were them carried out as detailed below.

DATA AND DISCUSSION

1. Chemical Analyses

Results of chemical analyses were as follows:

6" x 12" plate (Great Lakes): -. 32% C, -. 82% Mn, . 71% Si, .025% 8, .036% P, .73%.Cr, .21% Mo, .09% Zr.

18" x 18" H plate (Simonds Saw and Steel): .33% C, 1.55% Mn, .18% Si, .016% S, .020% P, .06% Cr, .25% Mo

Provided that a quench is sufficiently severe to produce martensite, maximum hardness is largely a function of carbon content for a given heating and cooling cycle, as opposed to depth of hardening (hardenability) which is greatly influenced by added alloy. Hence; the difference in added alloys to these plates will not have a large effect on the maximum hardness observed in the flame cut edges, so long as the carbon contents are comparable. -destination of the very second second

Vickers Brinell hardness surveys were made on seven specimens taken from plates es indicated in Figure 1. Locations of Vickers Brinell impressions and tabulation of hardness readings are given in Figures 2 and 3. The first four specimens were from cuts made in identical menner except for preheat. Maximum hardnesses of 536 Vickers Brinell at room temperature, 498 at 200° F. preheat, 429 at 400° F. preheat, and 348 at 600° F. preheat were observed. Maximum plate hardness is 330 Vickers Brinell; thus the hardness of 429 Vickers (approximately 397 standard Brinell) in plate preheated to 4000 F. does not appear excessive.

Specimens 5 through 7 were taken at beginning, middle, and end of 18 inch cut. Maximum observed hardness was in specimen taken from end of cut and was approximately equal to 400 standard Brinell.

Specimens 8 and 9 were taken from middle of two 300 bevel flame cuts. A maximum hardness of 542 Vickers Brinell (approximately 494 standard Brinell) was observed in specimen from out made at room temperature, and a maximum of 366 Vickers Brinell (approximately: 340 standard Brinell) was observed in specimen from cut made with 400° F. preheat.

3. Macroexamination

Figure 4 shows a photomacrograph of specimen No. 2 after hardness survey and light etch with 1% nital. The thickness of the heat affected zone tapers from 3/16 inch at top of plate to 1/16 inch at bottom. This is typical of most of the flame cut specimens. However, the specimen taken at the beginning of the 18 inch flame cut showed a much wider heat affected zone where flame was held for a few seponds to start out. In this case the flame affected eres was softened rather than hardened.

A very narrow dark band was observed along flame cut edge in hardened zone of macroetched specimens. This band was examined at 350 magnification, Figure 4, and found to consist of ferrite, troostite, and some pearlite, indicating that the edge had been decarburized sufficiently to prevent full hardening. Immediately beyond ficiently to prevent full hardening. Immediately beyond the decarburized edge is the martensitic flame hardened zone, extending as far as the plate metal has been ... heated above the lower oritical temperature (approximately 13300 F.). Beyond, the hardened some is a softened zone where the heat of flame outting has tempered the hardness where the heat; of flame outting has tempered the hardness of the original plate with the reservoir of the original of the original

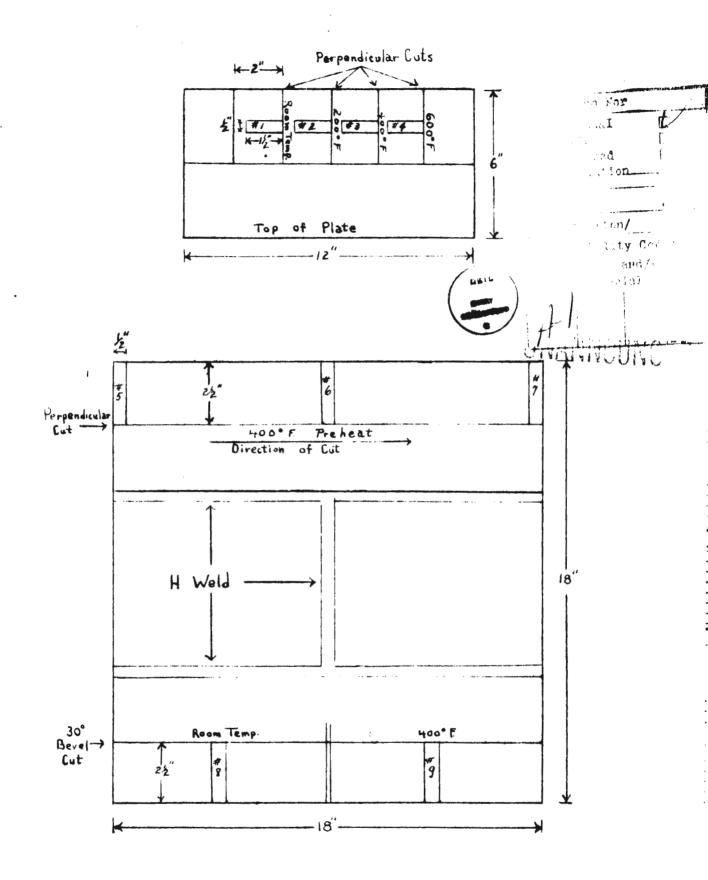
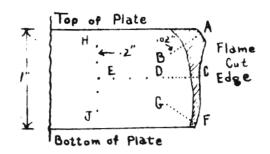


FIGURE 1. LOCATION OF HARDNESS SPECIMENS



LOCATION OF VICKERS BRINELL IMPRESSIONS

Three Inch Cut (Great Lakes).

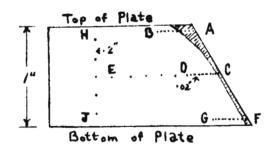
Specimen 1					2				3										
Preheat Room Temp.				200° F				400° P				600° F							
AB	תח	TF	FG	HJ	AB	CD	DF	FG	HJ	AB	CD	DE	FG	HJ	AB	CD	DE	FG	HJ
429	519	322	36 3	322	478	429	306	345	3 30	383	370	312	502	327	525	527	512	512	325
437	514	3 3 0	3 90	330	498	409	597	359	504	425	385	506	502	509	545	322	514	506	512
3 8 7	536	350	339	350	498	287	292	514	504	417	550	304	504	512	348	2 85	314	299	322
304	508		292	330	488	283		527	504	429	289		299	314	548	258		297	514
312	450		314	322	453	294		333	3 30	421	283		317	307	5 39	276		514	526
325	387		322		380	294		339		376	302		519		522	294		525	
325	306		322		354	504		339		348	512		519		512	306		550	
325	304		322		325	3 09		359		359	522		319		506	31 2		356	
319	51 9		322		502	30 9		342		304	322		319		2 97	317		527	
319	322		322		509	5 09		336		287	322		517		268	317		330	

Fighteen Inch Cut (Simonds Saw and Steel)

	Specimen		5				•	6		•			7		
	Star	rt o	Flo	ame (Cut	Cen	ter	of F.	lame	Cut	End	of 1	Plan	Cut	E
	AB	CD	DF	FG	ĦJ	AB	CD	DE	FO	HJ	AB	CD	DE	FG	HJ
	504	304	317	272	825	551	397	504	360	30 6	397	380	272	363	276
Preheat	312	309	314	289	5 22	566	317	287	5 2 2	297	455	536	276	551	2 66
	51 2	297	314	289	319	360	304	281	312	287	594	5 02	279	556	274
400° F	2 94	292		289	314	506	274		504	289	376	274		527	274
	294	297		292	514	319	2 8 5		287	299	548	270		29 9	2 65
	312	302		304		319	274		234		330	268		299	
	30 2	294		289		302	270		294		309	276		302	
	292	289		289		309	272		292		302	268		506	
	281	289		289		281	285		302		302	266		314	
	289	285		297		270	287		299		306	266		299	

FIGURE 2. VICKERS BRINFLL HARDNESSFS STRAIGHT CUT

(See Fig. 1 for Specimen Location)



LOCATION OF VICKERS BRINELL INPRESSIONS

Wine Inch Cut (Simonds Saw and Steel)

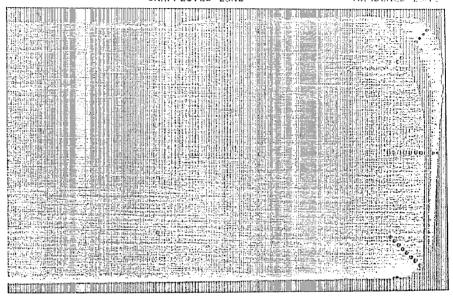
Fre	heat	Root	a Ter	p.	400° F						
AB	60	DE	70	HJ	AB	CD	DE	FG	HJ		
556	566	514	459	279	527	536	276	514	297		
5 42	38 0	50 9	514	292	566	312	287	517	299		
536	287	314	59 0	294	354	502	274	504	287		
542	3 12	514	36 0	309	527	274	276	297	292		
525	512	514	522	299	556	262	279	294	289		
514	209		294		559	262		279			
455	514		504		519	27 0		276			
405	517		512		304	279		294	•		
287	514		504		294	276		292			
	814		506		294	288		292			

FIGURE 5. VICKERS BRINELL HARDNESSES 80°BEVEL CUT

(See Fig. 1 for Specimen Location)

UNAFFECTED ZONE

HARDENED ZONE



FLAME CUT EDGE

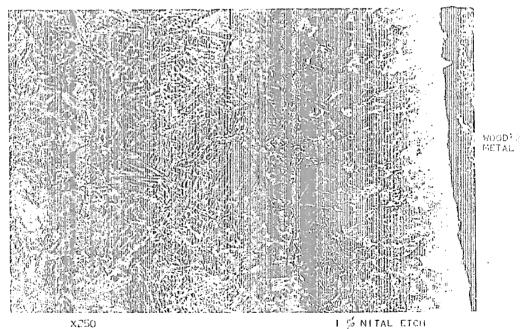
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1 % NITAL ETCH

CROSS SECTION SHOWING EXTENT OF HARDENED ZONE AND LOCATION OF HARDNESS IMPRESSIONS.

HARDENED ZONE

DECARBURIZED ZONE



DECARBURIZED ZONE AT FLAME CUT, SURFACE.

FIGURE $\frac{4}{\pi}$