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ATI-38861

Report No. 640/84

WELDING OF ARMOR

Summary of Ballistic Shock Test Results on  
1-1/2 Inch Homogeneous Armor "E" Plates Welded with  
Austenitic Electrodes and Tested at Aberdeen Proving Ground  
during the Period from 1 October 1942 through 31 March 1943

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Report No. 640/84  
Watertown Arsenal  
Problem No. D-7

4 August 1943

WELDING OF ARMOR

Summary of Ballistic Shock Test Results on  
1-1/2 Inch Homogeneous Armor "H" Plates Welded with  
Austenitic Electrodes and Tested at Aberdeen Proving Ground  
during the Period from 1 October 1942 through 31 March 1943

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OBJECT

To tabulate firing record data for subject plates and to present a comparison of ballistic shock performance of plates made with various materials and welding procedures.

SUMMARY

1. Data from 172 Aberdeen Proving Ground firing records have been tabulated on accompanying charts and tables.
2. Within the range of chemical composition of commercial rolled homogeneous armor, steel quality was indicated as having more influence on ballistic performance of hand welded plates than variations in chemical analysis. Armor compositions of very high hardenability have been successfully welded.
3. While superior ballistic performance was indicated for certain brands of electrodes, no grouping of electrodes according to chemical analysis was possible on the basis of ballistic efficiency.
4. Improved shock test results were obtained when two or more beads were deposited at the root, when stringer beads or overlapping beads rather than a full weave were used for the body, and when an annealing bead technique was employed.
5. Of twenty-six Unionmelt welded plates, only two were comparable in ballistic performance to satisfactory hand welded plates. These two plates failed the radiographic examination.

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## INTRODUCTION

On the accompanying charts (Appendix A) are tabulated data taken from 172 firing records representing qualification and development tests of H plates welded with austenitic electrodes. The tabulation includes all firing records received by this arsenal for H plates assembled from 1-1/2 inch thick homogeneous rolled or cast armor by welding with austenitic electrodes and fired at Aberdeen Proving Ground during the period from 1 October 1942 to 31 March 1943.

The purpose of these tabulations is to make available to persons concerned with welding of armored structures information as to ballistic performance of H plates made with various materials and procedures by commercial fabricators. A report (W.A. 640/73) giving a summary of ballistic test results on all 1 inch and 1-1/2 inch thick homogeneous armor H plates welded with ferritic electrodes and tested at Aberdeen Proving Ground through 25 February 1943 has been issued. A subsequent report will deal with development and qualification tests of H plates assembled from homogeneous rolled or cast armor of plate thicknesses other than 1-1/2 inch by welding with austenitic electrodes and fired at Aberdeen Proving Ground during the period of 1 October 1942 through 31 March 1943.

An index to Fabricators, Armor Manufacturers, and Electrode Manufacturers is given in Table I. The tabulation has been divided into three groups: (1) all plates assembled from rolled armor by hand welding; (2) all plates assembled from rolled armor by Unionmelt welding; (3) all plates assembled from cast armor by hand welding. There were no cast assemblies welded by the Unionmelt process. A summary of current ballistic shock test specification requirements for H plates welded with austenitic electrodes and a key to the tabulation method and symbols used in this report are included in Appendix A.

## GENERAL COMMENTS

Ballistic performance of H plates is best evaluated by amount of cracking for each round, but the cracking is influenced by the variables in the ballistic test as well as by those introduced by the materials and welding procedures. Therefore, it is necessary to make corrections or allowances for varying projectile velocities and effect of prior impacts when comparing amounts of cracking produced by the various impacts.

Tabulation of the average plate and average weld cracking of tested rolled plates grouped according to the severity of their ballistic testing, as shown in Table II, suggested the corrections for weld cracking given in Table III. Firing record data show cracking as located in weld metal, fusion zone, heat-affected zone or plate based only upon surface appearance. Experience has shown that a crack in the vicinity of the weld may proceed through portions of weld metal, fusion zone, and heat-affected zone regardless of surface appearance. For the purpose of the tables in this report all cracking within one-eighth inch of edge of weld is included as weld cracking and the remainder as plate cracking.

Plate cracking other than heat-affected zone cracking was negligible in the tested rolled plates as shown by Table II and so was not taken into consideration in evaluating the rolled H plates. Tabulation of the average plate and average weld cracking in cast plates (Table II) grouped according to the severity of the ballistic testing showed a very high ratio of plate to weld cracking. Inasmuch as virgin cast armor would not ordinarily develop cracking under the same testing conditions as those used for the welded plates, it is necessary to consider plate cracking in evaluating the cast H plates. Because the small number of tests included in Table II failed to show the severity of the ballistic test as an important variable, weld cracking was corrected in a manner similar to that used for the rolled plates and no attempt was made to correct plate cracking.

Generally, for a 75 mm. test projectile to produce weld cracking in 1-1/2 inch plate at a velocity of 1100 f/s, it must touch or overlap the weld. Rounds impacting at a distance from the center of impact to center of weld of over two inches are therefore considered unfair hits. In the rolled H plates there were twelve such rounds, only two of which produced more than two inches of cracking. These two rounds resulted in 36 inches and 16-1/4 inches of weld cracking, respectively, and because of these considerable amounts of cracking were included in the tables as fair rounds while the remaining unfair hits were omitted from these tabulations. In the cast assemblies there were 4 unfair hits, only one of which caused considerable cracking (8 inches of weld and 10-1/2 inches of plate). This round was included as a fair hit while the other 3 were omitted.

Decrease in temperature of the test plate at time of impact is known to have considerable effect in reducing the resistance to ballistic shock. Within the usual range of testing temperatures at Aberdeen Proving Ground, no correlation is evident between plate temperature and average weld or plate cracking for the plates included in these tabulations. However, one group of 10 plates welded by International Harvester Company and tested at 32°F. (lowest temperature of testing for any of the plates), performed badly. Although other variables were involved, temperature may have been an important factor contributing to the poor performance of these plates.

In Tables IV - XVI, changes in each of the more important variables introduced by welding materials and procedures are compared as to average amount of cracking per round after the corrections given in Table III for the severity of the ballistic testing had been made. This method of analysis is, of course, open to criticism unless a very large number of test results are available for each variable. The tables of this report are intended only to indicate trends and to encourage further observation and analysis.

## HAND WELDED, ROLLED ARMOR, H PLATES

### Fabricators - Table IV

The performance of H plates welded by any one fabricator must be evaluated in terms of the armor and electrodes used as well as the welding procedure and inspection control.

### Armor Data - Table V

Each composition of armor has been heat treated to a hardness level designed to pass the ballistic requirements for shock and penetration resistance of virgin armor, and an unwelded test plate has been tested from each heat of armor. Within the range of hardness which will meet this requirement, no correlation between plate hardness and average weld cracking is evident. Within the range of chemical compositions represented in Table V, no correlation is apparent between carbon and/or total alloy content and average weld cracking. With the exception of five plates from a .42 C, Mn-Cr-Mo-Si, heat which performed very poorly, there is little choice between armors of the upper and lower levels of C content and for hardenability listed in this table. This tabulation suggests that quality of steel (cleanliness and directional properties) is an important factor influencing the ballistic efficiency of a welded structure. In general, armor types which are usually very clean and armors which have been cross-rolled performed best.

### Electrodes - Table VI

Firing record data on electrode compositions and coatings very frequently were incomplete or questionable. When an electrode was used on a rather small number of plates, the results may have been influenced unduly by other factors. No correlation is shown between chemical composition of weld metal and amount of cracking. There is little difference in ballistic performance between plates welded with Mn-Mo modified (weld analysis - at least 1% Mn and 0.2% Mo) austenitic electrodes and those with Mn modified (weld analysis at least 1% Mn and no Mo) austenitic electrodes.

### Joint Design - Table VII

With one exception ("K" type bevel), all joints were prepared with double V bevels.

Root gap does not appear in these tests to be an important factor as evidenced by ballistic performance. An included angle of 60° shows up more favorably than one of 45°. The number of plates with other sizes of included angle was not large enough to make comparisons.

The table indicates that plates with flame-cut edges that have been treated so that the hardened area due to flame cutting is removed, either by grinding, machining, or flame softening, performed better than plates with untreated flame-cut edges.

## Welding Procedure - Table VIII

No correlation is apparent between the total number of passes and cracking. Some interesting trends as to influence of method of weld metal deposition are indicated. The use of two or more beads at root results in a slight improvement over the single root bead technique. The use of stringer beads, overlapping beads, or combinations of beads and layers, appears more desirable than a full weave technique for the body deposition. A multiple crown bead technique in which the last bead deposited does not touch the parent metal is indicated as preferable to a single crown bead technique.

Initial plate temperature varied from 70° to 200° F. No benefit of preheating within these ranges is apparent.

## Radiographic Examination - Table IX

Of the 93 rolled homogeneous manually welded H plates, 19 failed the radiographic examination. Eleven of these plates passed the ballistic shock test (based upon the standards given in Specification AXS-497, Rev. 3, prior to amendment of 25 June 1943). In general, as shown by Table IX, radiographic unsoundness is associated with increased weld cracking.

## UNIONMELT WELDED, ROLLED ARMOR, H PLATES

### Fabricators - Table X

As compared with manually welded rolled H plates, Unionmelt welded plates exhibit very inferior shock resistance. In several instances, plates that withstood one round fairly well, failed badly on subsequent rounds.

### Armor Data - Table XI

Three plates were assembled from Republic high alloy (4% Ni) armor. One plate was welded by one fabricator without the use of hand beads and failed on the first impact, while the other two plates welded by another fabricator stood up very well under ballistic impact. Three plates welded with 2.25 - 2.45 Cr, .71 Ni alloy armor plate performed poorly, as did other lower hardenability compositions.

Tables XII to XIV have been prepared to show variations in electrode, joint design, welding procedures, and radiographic results for the Unionmelt welded plates. Influences of these factors are not apparent from the data available for these tabulations. It is interesting to note that the two ballistically best Unionmelt welds failed the radiographic examination because of blowholes, weld metal cracks and incomplete fusion.

## HAND WELDED, CAST ARMOR, H PLATES

### Armor Data - Table XVI

Ballistic performance of cast armor H plates is more erratic than that of rolled plates, and in many instances the amount of cracking in the vicinity of the weld is exceeded by plate cracking. Since unwelded cast armor plate of the same chemical compositions would ordinarily be unaffected by the H plate shock test, it is apparent that the welding process was responsible in some way for the extensive plate cracking. A recent report\* has shown that good performance of armor at sub-zero temperatures or equivalently higher impact velocities at ordinary temperatures, is dependent upon development of a fully hardened microstructure during quenching. It would seem that the presence of a weld, with attendant high stresses and notching effect, initiates failure (under lesser ballistic shock than required for virgin plate) which then proceeds very rapidly through the weakest structure until the energy of impact has dissipated. If the armor plate has not been fully hardened during heat treatment, either due to insufficient alloy content or poor heat-treating practice, plate cracks are favored. If armor is properly hardened through during heat treatment most of the cracking should occur in the weld metal, fusion, and heat-affected zones.

Cast armor has generally been more deficient in deep hardening alloy elements than rolled armor, and cast armor is not subjected to as efficient a quenching practice as rolled armor with the result that many of the compositions shown in Table XVI are inadequate in hardenability. This table shows a definite trend toward decreased ratio of plate to weld cracking in the armor compositions known to be adequately heat treated. In the few instances where hardenability is comparatively good and plate cracking is excessive, steel quality, particularly radiographic unsoundness, appears to be a determining factor.

Strenuous efforts are being made to attain adequate hardenability in cast armor since this factor is of such importance in obtaining good ballistic performance at sub-zero temperatures and apparently also in welded plates. So long as a large proportion of the ballistic cracking is in the unaffected plate, no attempt at tabular comparison of welding variables seems justified. Presumably, cast armor is affected by welding variables in the same general manner as rolled armor.

\* W.A. Report No. 710/534, "Correlation of Metallurgical Properties with Low Temperature Shock Characteristics of 1 to 2 inch Low Alloy Cast Armor," August, 1943.



TABLE I

Index to Plates1-1/2 Inch Rolled Homogeneous Plate

Chart No.	No. of Plates	Fabricator	Armor Mfgr.	Electrode Mfgr.
1	2	American Loco.	Carnegie-Illinois	Harnischfeger
2	1	Baldwin Loco.	Disston	Lincoln Electric
3	2	Briggs Mfg.	Carnegie-Illinois	Crucible Steel Metal & Thermit
4	2	Chrysler- Plymouth	Carnegie-Illinois Ford	Alloy Rods Crucible Steel
5	1	Crucible Steel	Republic Steel	Crucible Steel
6-8	7	Federal Machine	Republic Great Lakes	Crucible Steel Harnischfeger Alloy Rods McKay
9-15	21	Fisher Tank	Great Lakes Jones & Laughlin Republic Steel	McKay Alloy Rods Reid-Avery
16	2	Fitzgibbons Boiler	Republic Steel	Harnischfeger Lincoln Electric Alloy Rods
17-18	4	Ford	Ford	Reid-Avery Crucible Steel Arcos Corp.
19	2	General Am. Trans.	Great Lakes	Crucible Steel McKay
20-21	4	General Motors Div. of Can.	Dominion Foundries and Steel	Lincoln Electric Harnischfeger
22	2	Ilco Ordnance	Republic Steel	Crucible Steel Metal & Thermit
23-29	21	International Harvester	Great Lakes Jones & Laughlin	Westinghouse El. & Mfg. Crucible Steel Page Steel & Wire McKay Alloy Rods

TABLE I (Cont.)

Chart No.	No. of Plates	Fabricator	Armor Mfr.	Electrode Mfr.
30	1	Lima Locomotive	Jones & Laughlin	Arcos Corp.
31	1	Midland Steel	Carnegie-Illinois	Crucible Steel
32-33	4	New York Air Brake	Jones & Laughlin Carnegie-Illinois	McKay Lincoln Electric Harnischfeger
34-35	5	Pressed Steel Car	Republic Steel Carnegie-Illinois	McKay
36-38	10	Pullman Standard	Republic Carnegie-Illinois	Reid-Avery Lincoln Electric Hollup & Champion McKay Metal & Thermit Champion Rivet Crucible Steel
39	1	York Safe & Lock Disston		Alloy Rods
<u>1-1/2 Inch Unionmelt Plates</u>				
40	1	American Loco.	Republic Steel	Linde Air Products
41	3	Fisher Tank	Great Lakes	McKay Linde Air Products Lincoln Electric
42	3	General Motors Div. of Can.	Dominion Foundries and Steel	Harnischfeger Lincoln Electric Linde Air Products
43-44	4	International Harvester	Great Lakes	Crucible Steel Linde Air Products
45-49	15	New York Air Brake	Republic Steel Jones & Laughlin Carnegie-Illinois	Alloy Rods McKay Lincoln Electric Linde Air Products

TABLE I (Cont.)

Chart No.	No. of Plates	Fabricator	Armor Mfr.	Electrode Mfr.
<u>1-1/2 Inch Cast Homogeneous</u>				
50-51	5	Chrysler Plymouth	American Continental Roll	A. O. Smith McKay Alloy Rods
52-56	12	Federal Machine	Ordnance Steel General Steel American Radiator Symington Gould Buckeye Steel Continental Roll Pratt & Letchworth	Harnischfeger McKay Alloy Rods
57	1	Firestone Tire and Rubber	Utility Electric	Page Steel and Wire
58-59	7	Fisher Tank	American	Alloy Rods
60-61	6	Ford	Ford	Crucible Reid-Avery Arcos Corp.
62	1	Heil	Wehr Steel	A. O. Smith
63-64	5	International Harvester	Ordnance Steel	McKay Metal & Thermit
65	2	Kay-Brunner	Utility Steel	McKay
66-67	3	Lima Loco.	Pittsburgh Steel	Lincoln Electric Arcos
68	2	Pacific Car and Foundry	Pacific Car and Foundry	McKay
69-70	5	Pressed Steel Car	Union Steel Castings	McKay Crucible
71	1	Pullman Standard	Sivyer Steel	Metal & Thermit

TABLE II

Ballistic Severity Table for Rolled H Plates

Vel. f/s	1st Round		2nd Round		3rd Round		4th Round	
	No. of Eds.	Av. Plate Cracking	No. of Eds.	Av. Plate Cracking	No. of Eds.	Av. Plate Cracking	No. of Eds.	Av. Plate Cracking
1176-1360*			42	1.93"	30	.80"	8	.63"
1126-1175	5	11.40"	23	.52	11	.73	2	13.37"
1075-1125	107	.27"	26	1.15	10		2	17.09
1025-1074	2		1				2	10.90
960-1024								2.00
								13.15"
								10.50
								10.00

Ballistic Severity Table for Cast H Plates

1126-1260*	7	9.43"	20	7.00"	14	3.57"	8	4.88"	6.75"
1176-1125	23	7.57	10	11.90	3			4.29"	
1025-1074	16	5.65	7	14.14	4	5.75		4.33	
975-1024	1	8.00	1	5.00				10.00	
900-974	1	3.00							

Note: Distance from center of impact to center of weld no more than 2 inches.

\* Specified Velocity Range

TABLE III

Weld Cracking Corrections for Ballistic Severity

(Center of impact no farther than 2" distant from center of weld)

Velocity f/s      1st Round      2nd Round      3rd Round      4th Round

Corrections for Rolled H Plates

1176-1300+	-1	-3	-5	-7
1126-1175	-.5	-2.5	-4.5	-6.5
1075-1125	0	-2	-4	-6
1025-1074	+.5	+2.5	+4.5	+6.5
950-1024	+1	+3	+5	+7

Corrections for Cast H Plates

1126-1200+	-1	-3	-5	-7
1076-1125	-.5	-2.5	-4.5	-6.5
1025-1075	0	-2	-4	-6
975-1024	+.5	+2.5	+4.5	+6.5
900- 974	+1	+3	+5	+7

TABLE IV

Fabricators of Hand Welded Rolled H Plates

<u>Armor Fabricator</u>	<u>No. of Plates</u>	<u>No. of Rounds</u>	<u>Av. Weld Crack- ing per Round (Corrected) (inches)</u>
American Locomotive	2	5	12.35
Baldwin Locomotive	1	3	6.25
Briggs	2	6	7.17
Chrysler Plymouth	2	6	7.58
Crucible Steel	1	4	11.44
Federal Machine	7	22	2.33
Fisher Tank	21	49	12.19*
Fitzgibbons	2	5	7.55
Ford Motor	4	7	15.43
General American Trans. Corp.	2	4	11.38
General Motors	4	10	8.40
Ilco Ordnance	2	6	6.71
International	21	51	7.72
Lima Locomotive	1	2	16.12
Midland Steel	1	3	9.33
New York Air Brake	4	10	13.45
Pressed Steel	5	11	6.05
Pullman Standard	10	27	7.88
Yerk Safe & Lock Co.	1	2	6.38

\* Includes one unfair round.

TABLE V

Armor Data for Hand Welded Rolled H Plates

Manufacturer	Armor Type	Chemical Composition	°F.	Heat Treatment Hold (hrs.)	Quench	Brinell Hardness	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
Dominion Foundries & Steel	V High Alloy	.26 C	1650	8 - 10	Air	277-285	4	10	8.45
		.57 Mn	1650	4	Water				
		.30 Si	1125-1150	5 - 6	Air				
		2.25 Cr							
Carnegie-Illinois	I Mn-Cr-Ni-Mo	.65 Ni							
		.28 Mo							
		.24 C	1544	1-1/2	Water	228-302	11	28	10.53
		.94 Mn	1058	1-1/4 - 2-1/4	Water				
	V High Alloy	.16 Si							
		.39 Cr							
		.92 Ni							
		.26 Mo							
	VI Special	.30 C			Not given	293	1	4	6.37
		.22 Mn							
		.07 Si							
		1.20 Cr							
	VI Special	3.23 Ni							
		.27 C			Not given	265-282	1	2	5.37
		1.28 Mn							
		.20 Si							
		.82 Ni							
		Average 3 Types					13	34	9.79

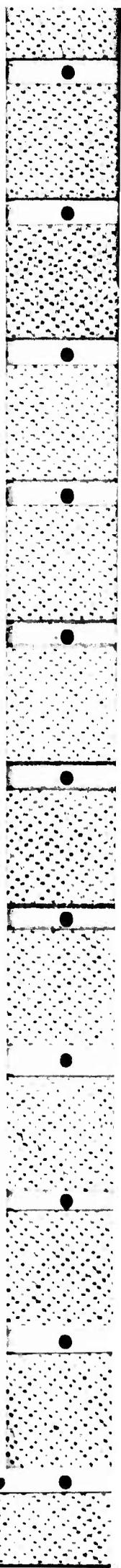


TABLE V (Cont.)

Manufacturer	Armor Type	Chemical Composition	°F.	Heat Treatment Hold (hrs.)	Quench	Brinell Hardness	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
Henry Disston & Sons	V High Alloy	.18 - .21 C	1425	2	Water	269-286	2	5	6.3
		.46 - .51 Mn							
		.20 - .23 Si							
		.09 - .10 Cr							
		4.66 - 4.77 Ni							
.31 - .34 Mo									
.05 - .10 V									
Ford Motor Co.	II Mn-Cr-Mo	.26 - .30 C	1650	4	Water	262-292	2	4	12.13
		1.35 - 1.42 Mn							
		.21 - .34 Si							
		.54 - .71 Cr							
		.03 - .11 Ni							
.42 - .45 Mo									
	V High Alloy	.23 - .24 C	1650	4	Water	---	3	5	15.9
		.64 Mn							
		.19 - .20 Si							
		1.40 - 1.61 Cr							
		.12 Ni							
.62 - .64 Mo									
Average 2 Types									
Great Lakes	IV Mn-Cr-Mo-Si	.26 - .32 C	1600-1650	1/2-3	Water	255-312	25	58	11.24
		.80 - .94 Mn							
		.67 - .81 Si							
		.60 - .70 Cr							
		.17 - .22 Mo							
.07 - .09 Zr									
Average 2 Types									
1600-1650 1/2-3 5 9 14.22									
1100-1260 1/2-4 25 58 11.24									

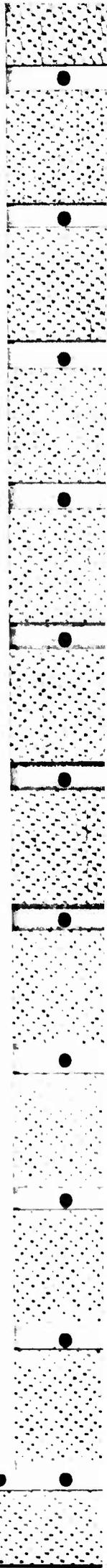




TABLE V (Cont.)

Manufacturer	Armor Type	Chemical Composition	°F. Hold (hrs.)	Heat Treatment	Quench	Brinell Hardness	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
Great Lakes	IV Mn-Cr-Mo-Si High C	.42 C	1600	2	Water	269	5	8	22.56*
		.71 Mn .79 Si .56 Cr .16 Mo .08 Zr	1150	4	Air				
Jones and Laughlin	III Mn-Mo	Average 2 Types					30	66	12.63
		.22 - .29 C	1625	1-3	Water	241-277	17	45	6.42
		1.50 - 1.68 Mn	1200	2-1/2 - 4	Air				
		.19 - .24 Si							
.41 - .52 Mo									
Republic	I Mn-Ni-Cr-Mo	.20 - .28 C	1600	3	Water	255-269	8	25	3.53
		.87 - 1.15 Mn	1200	3-1/2	Air				
		.27 - .28 Si							
		.67 - .98 Cr	1300	1	Air				
		.89 - .98 Ni	1600	3/4	Spray				
		.47 - .52 Mo	1200	1-1/2	-----				
	V High Alloy	.25 - .26 C	Not given			245-285	10	30	8.31
		.44 - .93 Mn							
		.19 - .27 Si							
		.22 - 1.53 Cr							
		3.80 - 4.05 Ni							
		.39 - .95 Mo							
	?	Not given					4	9	2.96
	Average 3 Types						22	64	5.68

\* Includes one unfair round.

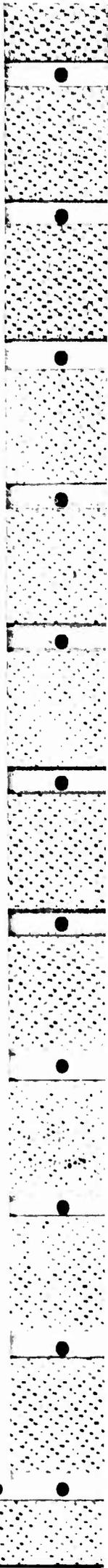


TABLE VI a

Electrode Data for Hand Welded Rolled H Plates

Electrode Mfg.	Brand	Weld Metal Composition	Coating	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
Alloy Rods	Armorarc Type A	.10 C	Titania	1	4	.75
		1.5 Mn .75 Si 19.0 Cr 9.25 Ni 3.0 Mo				
Arcos Corp.	Armorarc Type B	.08 - .14 C	Titania	13	34	10.18
		.03 - .75 Si				
		8.25 - 10.6 Ni				
		18.0 - 20.0 Cr 3.0 - 4.10 Mn				
		Average 2 Brands				
Arcos Corp.	Chromang	.09 - .10 C	Lime	2	4	15.19
		3.27 - 3.75 Mn				
		.32 - .75 Si				
		9.3 - 10.25 Ni 18.5 - 19.1 Cr .97 - 1.0 Mo				
		Average 2 Brands				
Champion Rivet Co.	308	.12 C		2	7	2.61
		3.75 Mn				
		19.0 Cr 10.0 Ni				

TABLE VI a (Cont.)

Electrode Mfg.	Brand	Weld Metal Composition	Coating	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
Crucible Steel	Armorize	.06 - .12 C	Titania	11	30	7.45
		1.70 - 2.10 Mn				
		.19 - .50 Si				
		18.5 - 19.6 Cr				
		8.06 - 10.7 Ni				
1.61 - 2.50 Mo						
		.20 V				
Harnischfeger	Rezistol	.07 - .11 C	Titania	2	3	12.92
		1.37 - 1.75 Mn				
		.28 - .31 Si				
		17.8 - 19.2 Cr				
		9.8 - 10.1 Ni				
1.09 - 2.26 Mo						
		Average 2 Brands				
Lincoln Electric	Smootharc AW-3 (AW-3A)	.10 - .13 C	Lime Titania ?	10	26	6.14
		1.38 - 1.83 Mn				
		.42 - .71 Si				
		18.49 - 20.4 Cr				
		10.3 - 10.9 Ni				
1.61 - 2.25 Mo						
		Average 2 Brands				
Lincoln Electric	Armorweld	.09 - .12 C	Lime Titania ?	3	9	8.81
		3.97 - 4.2 Mn				
		.04 - .85 Si				
		19.45 - 20.5 Cr				
		8.56 - 10.0 Ni				
		Not Given				
Lincoln Electric	Armorweld ARW-I		Lime	1	3	12.58
		Average 2 Brands		4	12	9.75

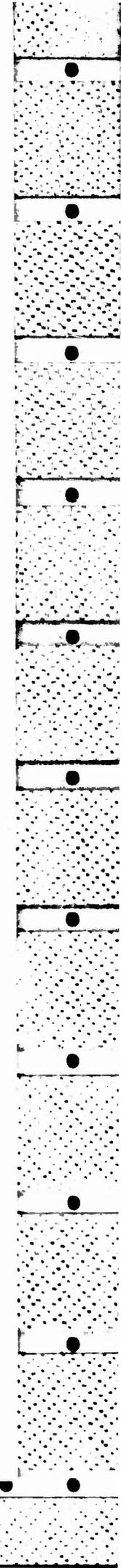


TABLE VI a (Cont.)

Electrode Mfg.	Metal & Thermit	Brand	Weld Metal Composition	Coating	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
McKay	Murex		.07 C	Titania	3	8	4.66
			1.15 - 1.19 Mn				
			.55 Si				
			18.8 - 19.0 Cr				
McKay	Armorloy A-5 (AC-5 ?)		9.93 - 10.0 Ni	Lime Titania ?	23	55	9.40
			2.10 - 2.13 Mo				
			.08 - .11 C				
			1.5 - 4.0 Mn				
			.03 - .53 Si				
			19.7 - 20.4 Cr				
McKay	Armorloy A-6		9.8 - 10.6 Ni		5	11	6.05
			.12 C				
			2.0 Mn				
			.5 Si				
Page	Stainless		Average 2 Brands	Titania	1	3	5.33
			1.61 - 2.06 Mn				
			.25 - .32 Si				
			17.98 - 19.02 Cr				
Reid-Avery	Raco		10.72 - 11.58 Ni	Titania	10	21	13.29*
			1.56 - 2.07 Mo				
			.09 - .11 C				
			4.0 - 4.35 Mn				
Reid-Avery	Raco		.02 - .75 Si				
			18.4 - 20.0 Cr				
			9.0 - 9.85 Ni				
			.81 - 1.25 Mo				

\* Includes one unfair round.

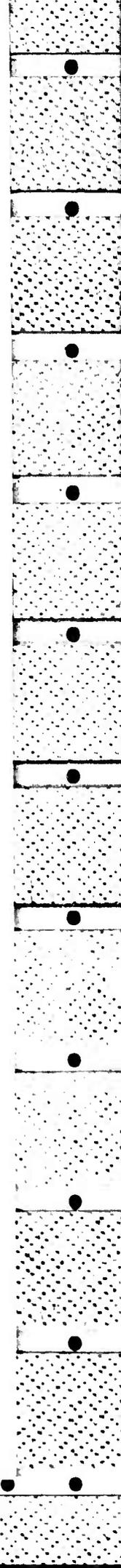


TABLE VI a (Cont.)

Electrode Mfg.	Brand	Weld Metal Composition	Coating	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
Westinghouse	—	.05 C 2.0 Mn .5 Si 18.5 Cr 1 Ni 1.6 Mo	Titania	1	3	4.58

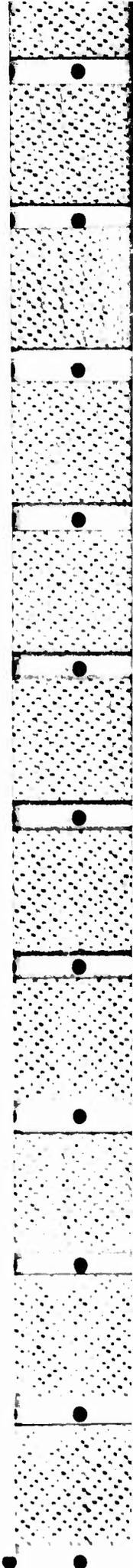


TABLE VI b

Electrode Type	Weld Analysis	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
Mn-Mo Mod. 18/8	At least 1% Mn and .2% Mo	46	113	7.94
Mn Mod. 18/8	At least 1% Mn	41	69	9.15
Mo Mod. 18/8	At least .5% Mo and less than 1% Mn	No plates		

TABLE VII

Joint Design Data for Hand Welded Rolled H Plates

Angle of Bevel	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)	Root Gap (inches)	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
45° DW	64	157	9.90*	1/8	3	6	6.96
60° DW	13	37	4.72	5/32	3	7	10.00
67½° DW	1	2	10.00	3/16	12	29	6.60
75° DW	1	2	3.75	1/4	14	36	7.65
90° DW	1	2	6.38	5/16	41	102	10.50*
				3/8	10	29	6.89
				7/16	2	5	2.90

Plate Preparation	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
Flame Cutting	19	48	10.64
Flame Cutting and Grinding, Machining, or Flame Softening	63	160	8.23
Buttering	4	9	8.44

\* Includes one unfair hit.

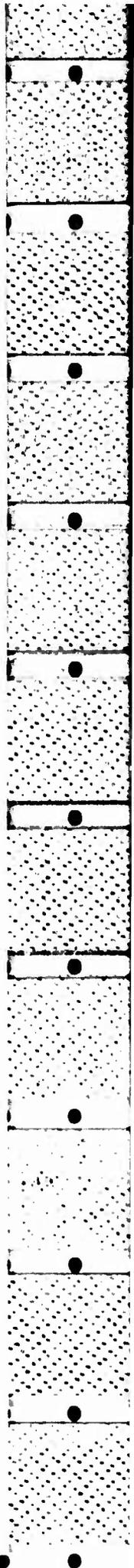


TABLE VIII

Welding Procedure for Hand Welded Rolled H Plates

No. of Passes	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)	No. of Passes	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
6	3	5	12.4	18	15	40	6.94
7	2	4	13.31	19	1	2	10.00
8	21	50	11.71*	20	2	5	7.55
9	7	19	10.20	21	3	7	5.21
10	3	6	6.83	22	2	4	6.44
11	4	9	14.11	23	1	2	5.13
12	3	8	10.87	24	2	6	6.67
13	2	6	5.17	25	2	4	10.25
14	3	9	3.44	26	2	6	8.25
15	4	11	7.07	27	1	3	6.25
16	7	18	10.33	28	1	4	0
17	1	2	13.00	56	1	3	.50

Backing	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
Copper	69	175	9.17
SAE 1015	1	2	16.13
No Backing	3	8	9.4

\* Includes one unfair round.

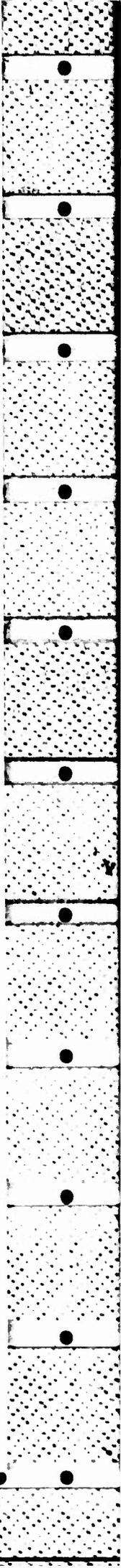




TABLE VIII (Cont.)

Root Deposition Type	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
I Single bead at root	8	18	10.40
II Two beads at root	81	204	8.98
More than two beads at root	4	11	3.64
Body Deposition			
Type			
I Layers only	54	133	10.34*
II Beads only	7	21	3.42
III Layers and beads	32	79	7.75
Crown Deposition			
Type			
I Single crown	41	96	11.27
II and III Multiple crown	52	137	7.17
Pre-heat			
°F	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
Room Temp.	53	130	9.13*
75 - 100	29	76	7.48
125	4	10	6.28
150	6	15	12.10
200	1	2	29.63

\* Includes one unfair round.

TABLE IX

Radiographic Data for Hand Welded Rolled H Plates

Radiographic Results	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
Passing	74	191	7.97*
Failing	97	42	12.82

-----

TABLE X

Unionmelt Fabricators

Fabricator	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
American Locomotive	1	1	22.00
Fisher Tank	3	4	31.56
General Motors of Canada	3	4	29.19
International	4	5	27.05
New York Air Brake	15	24	20.17*

\* Includes one unfair round.

TABLE XI

Armor Data for Unionmelt Welded Rolled H Plates

Manufacturer	Armor Type	Chemical Composition	°F	Heat Treatment Hold (hrs.)	Quench	Brinell Hardness	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corr.) (inches)
Carnegie-Illinois	V High Alloy	.30 C	1544	1-1/2	Water	228	1	1	34.0
		.98 Mn .47 Si .58 Cr .99 Ni .34 Mo	1050	2-1/4	Water				
Dominion Foundries and Steel	V High Alloy	.26 -	1650	10	Air	---	3	4	29.19
		.57 -	1650	6	Water				
		.34 -	1150	5	Air				
		2.25 - .71 - .28 -							
Great Lakes	IV Mn-Cr-Mo-Si	.26 -	1650	---	---	269-300	4	6	24.79
		.92 - .67 - .59 - .17 -	1150	2	Air				
	IV Mn-Cr-Mo-Si High C	.42 C	1600	2	Spray	269	3	3	37.58
		.71 Mn .79 Si .56 Cr .16 Mo .08 Zr	1150	4	---				
			1600	2	Water	269-286			
			1240	---	---				
Average 2 Types									29.06

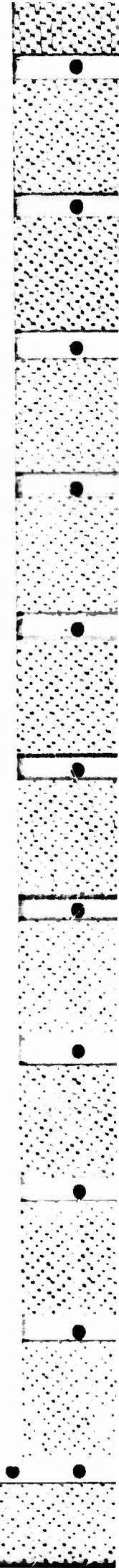


TABLE XI (Cont.)

Manufacturer	Armor Type	Chemical Composition	°F	Heat Treatment Hold (hrs.)	Quench	Brinell Hardness	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corr.) (inches)
Jones and Laughlin	III Mn-Mo	.25 C	1625	2-1/2	Water	275-300	11	14	28.36*
		1.50 Mn	1080	2-3/4	Air				
		.23 Si .41 Mo	1080	3	---				
Republic	V High Alloy	.24 -	1600	2-1/2	Water	252	3	8	5.47
		.47 Mn	1160	3-1/2	---				
		.22 Si .22 Cr 4.05 Ni .39 Mo							
I Mn-Ni-Cr-Mo		.24 C	1600	2-1/2	Water	---	1	2	15.63
		.71 Mn	1160	3-1/2	---				
		.26 Si .69 Cr 1.23 Ni .47 Mo							
Average 2 Types									
							4	10	7.50

\* Includes one unfair round.

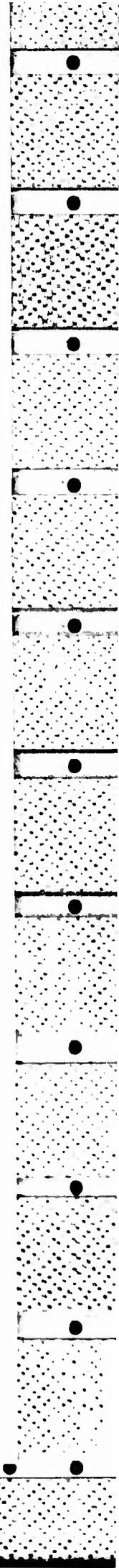




TABLE XII (Cont.)

Electrode Manufacturer	Brand	Weld Metal Composition	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
Harnischfeger and Linde Air	AW-3-A and Oxweld #41	AW-3-A Composition	2	2	33.88
		.10 - .13 C			
		1.38 - 1.83 Mn			
		.42 - .71 Si			
		18.49 - 20.40 Cr			
10.30 - 10.90 Ni					
1.61 - 2.25 Mo					
Crucible Steel and Linde Air	Armorize and Oxweld #42	Armorize Composition	4	5	27.05
		.06 - .12 C			
		1.70 - 2.10 Mn			
		.19 - .50 Si			
		18.50 - 19.60 Cr			
		8.06 - 10.70 Ni			
1.61 - 2.50 Mo					
		.20 V			
McKay and Linde Air	Armorloy AC-5 and Oxweld #42	Armorloy AC-5	1	1	36.00
		.12 C			
		.40 Mn ?			
		.80 Si			
		20.00 Cr			
9.70 Ni					
Alloy Rods and Linde Air	Armorloy and Oxweld #42	Not Given	7	8	27.97*
Alloy Rods and Linde Air	Armorarc and Oxweld #42		2	7	3.11

\* Includes one unfair round.

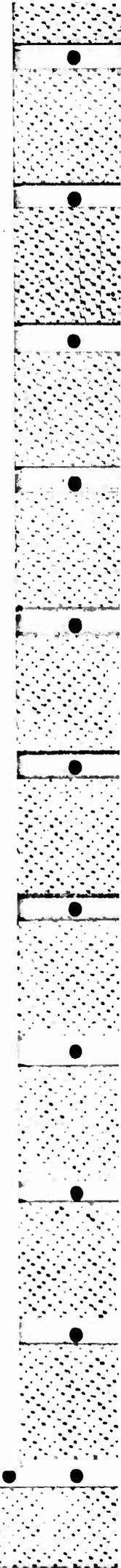


TABLE XIII

Joint Design Data for Unionmelt Welded Rolled H Plates

Angle of Bevel	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)	Root Gap (inches)	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
45°	19	28	22.65	3/16	4	5	27.05
90°	2	3	16.42	1/4	13	19	27.25
				5/16	3	4	31.56
				3/8	1	1	31.75

Plate Preparation	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
Flame cutting	5	9	9.94
Flame cutting and grinding	16	21	27.65*

\* Includes one unfair round.

TABLE XIV

Welding Procedure Data for Unionmelt Welded Rolled H Plates

No. of Passes	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)	Root Type Deposition	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
2 UM	2	2	29.00	I One hand bead at root	3	4	32.88*
1 Layer & 2 UM	2	3	27.33*	II Two hand beads at root	20	31	21.39
2 Layers & 2 UM	3	8	8.09				
3 Layers & 2 UM	2	2	40.63	More than two hand beads	1	1	31.75
4 Layers & 2 UM	14	19	26.26	Special No hand welding	2	2	29.00
5 Layers & 2 UM	1	2	13.63				
8 Layers & 2 UM	1	1	36.00	IV UM only	13	13	17.35*
9 Layers & 2 UM	1	1	36.00	V UM & hand beads	13	25	26.35

\* Includes one unfair round.



TABLE XIV (Cont.)

Preheat °F.	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
Room Temperature	11	13	32.48*
125	1	1	31.75
150 - 200	12	19	15.45
300	2	3	29.25

-----

TABLE XV

Radiographic Data for Unionmelt Welded Rolled H Plates

Radiographic Results	No. of Plates	No. of Rounds	Av. Weld Cracking per Round (Corrected) (inches)
Passing	14	19	25.84*
Failing	12	19	20.69

\* Includes one unfair round.





TABLE XVI (Cont.)

Manufacturer	Armor Type	Chemical Composition	Heat Treatment °F Hold(hrs.)	Quench	Brinell Hardness	No. of Plates	No. of Rounds	Av. Weld Crack- ing per Round (Corr.) (ins.)	Av. Plate Crack- ing per Round (inches)
Symington- Gould Corp.	II Mn-Cr-Mo	.26 C	1850	Air	255-258	1	2	12.37	4.38
		1.38 Mn	1650	Water					
		.35 Si	1150-1180	Water					
		.37 Cr							
		.40 Mo							
Union Steel Castings Co.	III Mn-Mo	.27 - .31 C	Not Given		220-285	5	9	5.64	19.5
		1.36 - 1.60 Mn							
		.34 - .42 Si							
		.53 - .57 Mo							
Utility Electric Steel	I Mn-Cr-Mo-Ni	.27 - .35 C	1850	Air	229	3	8	3.44	4.94
		1.07 Mn	1250	Air					
		.38 - .53 Si	1650-1600	Water					
		.47 - .50 Cr	1/3 -2						
		.63 - .74 Ni	1250-1200	Air					
		.21 - .31 Mo							
Wehr Steel Co.	I Mn-Cr-Mo-Ni	.33 C	Not Given		225	1	2	7.75	10.0
		.86 Mn							
		.46 Si							
		.84 Cr							
		.55 Ni ?							
		.45 Mo							

APPENDIX A

1. Key to tabulation method and symbols.
2. Specification requirements for H plates welded with austenitic electrodes.
3. Tabulation of firing record data on H plates welded with austenitic electrodes.

Ballistic data tabulated by:

Mary M. Sliny  
Jr. Statistical Clerk  
Watertown Arsenal

## KEY TO TABULATION METHOD AND SYMBOLS

Figure 2 is a sample tabulation of firing record data and gives a key to symbols and method of tabulation. A brief explanation of the items in the tabulation follows:

### 1. Identification of Test

Information in the first column identifies the test.

### 2. Armor Data

#### A. Plate Thickness

Plates in this tabulation are of 1-1/2 inch thick homogeneous armor.

#### B. Type Armor

The following types are used:

#### R (Rolled)

##### Typical Analysis

	<u>Type</u>	<u>C</u>	<u>Mn</u>	<u>Si</u>	<u>Cr</u>	<u>Mo</u>	<u>Ni</u>	<u>Zr</u>	
I	Mn-Ni-Cr-Mo	.26	1.15	.20	.60	.20	1.00		
II	Mn-Cr-Mo	.27	1.30	.25	.55	.42			
III	Mn-Mo	.25	1.60	.22	—	.37			
IV	Mn-Cr-Mo-Si	.27	.86	.79	.62	.17		.09	
V	High Alloy	(Compositions noted in tabulation)							
VI	Special	"	"	"	"	"			

#### C (Cast)

I	Mn-Cr-Mo-Ni	.32	.80	.35	.55	.40	.45		
II	Mn-Cr-Mc	.28	1.55	.45	.40	.12			
III	Mn-Mo	.30	1.58	.40	—	.30			
IV	Special	(Compositions noted in tabulation)							

#### C. Carbon Content

Carbon content is listed whenever given.

#### D. Brinell Hardness Number (BHN)

Brinell hardness number on both the front and back of plates is tabulated when given.

E. Process

This refers to the melting practice and is tabulated as open hearth, electric, basic or acid.

F. Heat Treatment

The temperature, time of hold, and type of quench and draw are recorded as given.

3. Electrode Data

These data, often incomplete, are listed as given in each firing record.

A. Type

Since alloys are sometimes added in the coating, electrodes are typed according to the chemical analysis of the weld metal when given.

The electrodes are typed as follows:

(1) (Austenitic)

I Mn-Mo Modified 18/8 (Cr-Ni-Fe Alloy)  
Weld Analysis - at least 1% Mn and .3% Mo

II Mn Modified 18/8 (Cr-Ni-Fe Alloy)  
Weld Analysis - at least 1% Mn and less than .3% Mo

III Mo Modified 18/8 (Cr-Ni-Fe Alloy)  
Weld Analysis - at least .3% Mo and less than 1% Mn

IV Special

B. and C. Trade Name and Coating

Trade names and types of coating are listed when given.

D. Current and Polarity

These data are tabulated as DC straight (str.), DC reversed (rev.), or AC.

4. Joint Design

A. Groove, etc.

This item includes the type of groove (Single V bevel or double V bevel), the included angle, and the width of the root face whenever given.

B. Root Gap

This is the distance between the plates as set up for welding.

C. Plate Preparation

This indicates whether the plate edges to be welded together were flame cut, ground, machined, buttered, etc.

5. Welding Procedure

A. Backing

Backing if used, i.e. back-up bar, chill, filler and spacer strips, is noted.

B. Deposition

Figure 3 shows how the weld deposition is broken up into the root, body, and crown types. The size electrode is noted with the number of passes, type of passes, and the current and voltage. Passes are divided into two kinds: (1) layer, if the pass bridges the gap; and (2), bead, if the pass does not bridge the gap.

C. Total Welding Time and Interpass Temperature

These are listed as given.

D. Remarks

Any comments on chipping, grinding, and other special techniques used and not noted above which affect the ballistic results are listed under "remarks."

6. Heat

Preheat and postheat are tabulated when given.

7. Ballistic Results

Unless otherwise specified, the 75 mm. TP projectile was used in the tests tabulated. Hits, velocity and location of each, cracking and remarks on cracking are listed. The types of weld and plate cracking are as follows:

- Type I Cracking in fusion or heat-affected zones on front and back of plate.
- Type II Cracking in fusion or heat-affected zones on one side of plate and weld metal on the other.



- Type III Cracking in weld metal on both front and back of plate.
- Type IV Star plate cracking.
- Type V Linear plate cracks.

The remarks on cracking and results of radiographic examination are recorded in the last column.

SPECIFICATION REQUIREMENTS FOR "H" WELDED PLATES

The following extracts from Specification AXS-497, Rev. 3, describe the present ballistic shock test:

Paragraph F-3a. (2) "Shock Tests. The welded plate shown in Fig. 1 shall be tested as shown below. Fig. 1 shows the areas designated for shock impacts. For the purpose of description these are divided in four 'specified areas' one above and one below the crossbar on each of the two vertical leg welds. Aiming points are indicated in Fig. 1.

"If the first round falls outside of the one of the four specified areas, another round shall be fired at a second specified area. If the second impact falls outside of the specified area and no cracking occurs in the weld, another round will be fired at a third specified area. This shall be continued until an impact is obtained within one of the four specified areas, but no more than four rounds will be fired at one plate. If the plate withstands all four rounds, all of which fall outside the specified areas, and the weld is not cracked, the plate will be considered acceptable."

BALLISTIC SHOCK TEST\*

Plate Thickness	Type	Projectile	Velocity f/s	Allowable Distance, Center of impact to center of weld	Maximum Allowable Cracking(1,2)**
1-1/2"	R.H.	75 mm. PP T21	1100	2"	15" 8"
1-1/2"	C.H.	75 mm. PP T21	1050 <sup>±</sup> 6f/s per .01"	2"	15" 8"

\* Effective during the period in which the plates in this tabulation were tested.

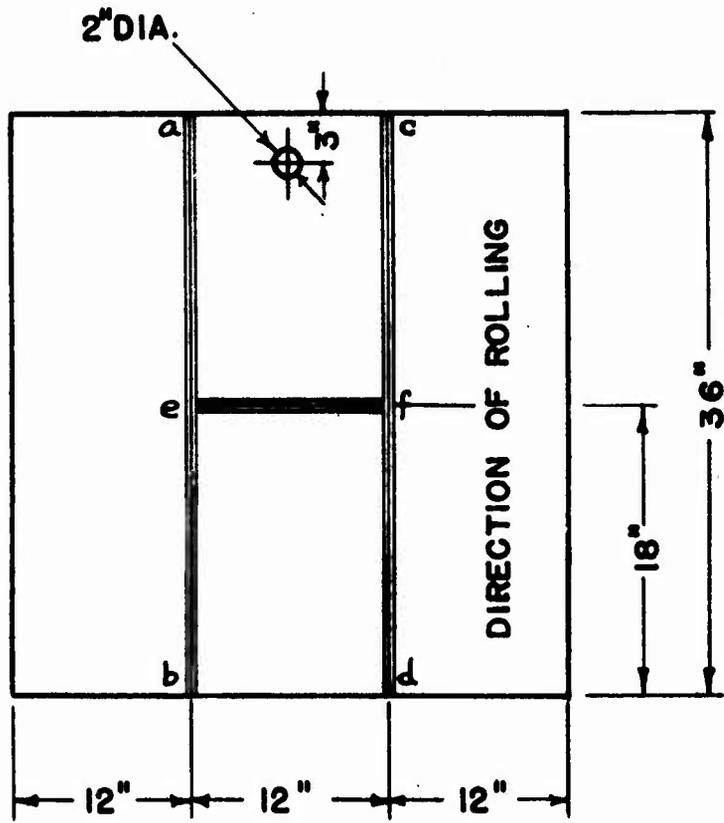
\*\* Notes:

1. Cracks in the armor parallel to the weld and within 1/8" of the edge of the weld shall be considered in the total weld cracking.
2. Limits of Armor Cracking - The maximum length of any plate crack originating or passing through the impact impression shall not exceed 8" as measured from the center of the impression. Any other plate crack shall not exceed a total of 8".

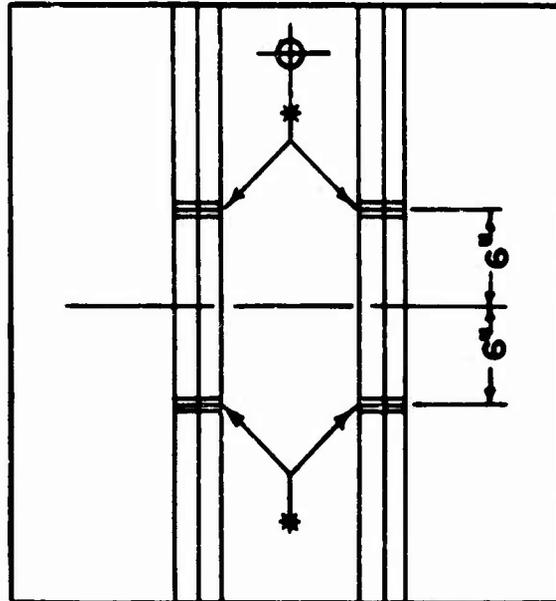
Amendment to Specification AXS-497, Rev. 3, effective as of June 25, 1943.

<u>Thickness</u>	<u>Type</u>	<u>Projectile</u>	<u>Striking Vel. <math>\pm 25</math></u>	<u>Allowable Weld Cracking</u>
1-1/2"	R.H.	75 mm. PP T21	1200 f/s	15"
1-1/2"	C.H.	75 mm. PP T21	1050 f/s	10"

WELD SEQUENCE:  
ab, cd, fe.



QUALIFICATION SHOCK TEST PLATE



\* INTENDED AIMING POINTS

FIG. 1



ROOT TYPES	TYPE I	TYPE II
DOUBLE V BEVEL	 <p>SINGLE ROOT BEAD AT CENTER OF ROOT</p>	 <p>MORE THAN ONE BEAD AT ROOT ETC.</p>
SINGLE V BEVEL	 <p>SINGLE BEAD BRIDGING ROOT GAP</p>	 <p>MORE THAN ONE BEAD BRIDGING ROOT GAP ETC.</p>

BODY TYPES	TYPE I	TYPE II	TYPE III	TYPE IV	TYPE V
DOUBLE V BEVEL	 <p>LAYERS ONLY</p>	 <p>BEADS ONLY</p>	 <p>LAYERS &amp; BEADS</p>	UNIONMELT	SPECIAL
SINGLE V BEVEL	 <p>LAYERS ONLY</p>	 <p>BEADS ONLY</p>	 <p>LAYERS &amp; BEADS</p>	UNIONMELT	SPECIAL

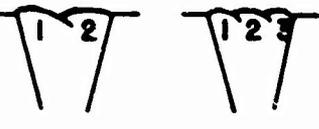
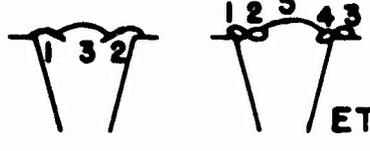
CROWN TYPES	TYPE I	TYPE II	TYPE III
DOUBLE V & SINGLE V BEVEL	 <p>SINGLE CROWN SINGLE PASS BRIDGES GAP</p>	 <p>MULTIPLE CROWN LAST BEAD TOUCHES PARENT METAL</p>	 <p>MULTIPLE CROWN LAST BEAD DOES NOT TOUCH PARENT METAL ETC.</p>

FIG. 3 WELD METAL DEPOSITION TYPES

REMARKS ON CRACKING RADIOGRAPHIC RESULTS, ETC.

TESTING DATA	ANNEAL DATA	BASE METAL	JOINT DESIGN	WELDING PROCEDURE	MEAT	H VEL. P/W	BALLISTICS RESULTS		REMARKS ON CRACKING RADIOGRAPHIC RESULTS, ETC.	
							LOCATION OF H	CRACKING		
A. FLOW	A. PLATE THICKNESS	A. TYPE	A. GROOVE, INCLUDED ANGLE, ROOT FACE	A. BACKING	A. PAZ	L.L.	R.L.	CRACK TYPE	AMT	
B. DATE OF TEST	B. TYPE	B. TRADE NAME	B. ROOT GAP	B. DEPOSITION SIZE EL. NO. TYPE AMT V	B. ROOT					
C. PLATE NO.	C. HARDEN CONTENT	C. COATING	C. PLATE PREPARATION	C. TOTAL WELDING TIME & ENTER PASS TEMPERATURE						
D. ADHESION	D. PREPARE	D. POLARITY								
E. SURFACE SPOT.	E. HEAT TREATMENT									
F. ADHESION	F. TEST METHOD									
A. AD-321 B. 3/9/43 C. 557 D. Carnegie-Ill- Inco Steel Co. E. Harnischfeger Corp. F. American Loco- motive Co.	A. 1-1/2" B. F-1 (.94Mn, .16Si, .54Cr, .98Ni, .40Mo) C. .25 D. Face 286. Beck 293 E. B.O.H. F. 1544 <sup>o</sup> F. 1 1/2 hrs. Water 1050 <sup>o</sup> F. 2 1/2 hrs. Water	A. A-1 (.11C, 1.59 Mn, .60Si, 18.49Cr, 10.51Ni, 1.61Mo) B. AW-3 C. Lime-TiO D. DC REV	A. 45 <sup>o</sup> DV B. 1/4" C. ---	A. Not given B. 1. I 3/16" 1a 120 - 25 1a 180 - 29 1a 260 - 28 1a 250 - 29 1a 1/4" 2b 240 - 29 1a 1/4" 1a 260 - 30 2b 230 - 28 1a 1/4" 1a 240 - 30 3. III 1/4" 3b 230 - 29 3b 240 - 29 C. 27 hrs. 1000 - 230 <sup>o</sup> F. D. 2 <sup>o</sup> (Hi Spot) chipped after sixth pass. One more pass in groove. Severe cracking along fusion zone in under side of root bead. This section was chipped and rewelded before completing the welding. Defect was not completely removed and the plate was submitted for development.	A. None B. None	1 1096 2 1147	1 1/2" 5/8"	5 <sup>o</sup> Imp 5 <sup>o</sup> U	I II II I II I II 28%	1 <sup>o</sup> Failed radiograph 2 <sup>o</sup> due to excessive 3 <sup>o</sup> cracking
A. AD-331 B. 3/19/43 C. 560 D. Carnegie-Ill- Inco Steel Co. E. Harnischfeger Corp. F. American Loco- motive Co.	A. 1-1/2" B. F-1 (.94Mn, .16Si, .54Cr, .98Ni, .40Mo) C. .25 D. Face 286 Beck 293 E. B.O.H. F. 1544 <sup>o</sup> F. 1 1/2 hrs. Water 1050 <sup>o</sup> F. 2 1/2 hrs. Water	A. A-1 (.12C, 1.83 Mn, .71Si, 18.5Cr, 10.3Ni, 2.16Mo) B. AW-3 C. Lime D. DC REV	A. 45 <sup>o</sup> DV B. 1/4" C. Flame Cutting	A. Not given B. 1. II 3/16" 1a 110 - 28 1a 200 - 28 1a 290 - 30 1a 310 - 30 3. III 1/4" 3b 290 - 30 C. 23 hrs. 1050 - 280 <sup>o</sup> F. D. 2 <sup>o</sup> (in test coupon) chipped after fourth pass.	A. 75 <sup>o</sup> F B. None	1 1103 2 1169 3 1195	2" 1"	6 1/2 <sup>o</sup> U 5 1/2 <sup>o</sup> Imp 4 1/2 <sup>o</sup> Imp	I II V III I I II III 4 1/2 <sup>o</sup>	6 <sup>o</sup> Passed radiograph 7 1/2 <sup>o</sup>

CONTRACTOR A. NAME B. DATE OF TEST C. PLATE NO. D. WELDING MANUFACTURER E. ELECTRODE MPOR. F. WELDING POSITION	ANODE DATA A. PLATE THICKNESS B. TYPE C. CATHODE CURRENT D. ON E. PROCESS F. HEAT TREATMENT G. TEMP TIME	ELECTRODE DATA A. TYPE B. TRADE NAME C. COATING D. CURRENT & POLARITY	JOINT DESIGN A. GROOVE, INCLUDES ANGLE, ROOT FACE B. ROOT GAP C. PLATE PREPARATION	WELDING PROCEDURE A. BACKING B. DEPOSITION SIZE EL. NO. TYPE AMP V. 1. ROOT TYPE 2. BODY TYPE 3. GROOVE TYPE C. TOTAL WELDING TIME & ENTER PASS TEMPERATURE D. REMARKS	HEAT A. PRE B. POST	H F/W	SALIENT DETAILS		REMARKS ON CRACKING RADIOGRAPHING RESULTS, ETC.
							LOCATION OF H L1 L2 L3	CRACKING TYPE	
A. AD-104 B. 11/7/43 C. 28 D. Henry Disston & Sons E. Lincoln Elec. F. Baldwin Loco-motive Works	A. 1-1/2" B. R-V C. (.48Mn, .23Si, .09Cr, 4.6GMn, .31Mo, .05V) D. Face 286 E. B.Elec. F. ---	A. A-II B. (.12C, 4.2 Mn, .8Si, 20.5Cr, 10.00Ni) C. Armco-weld D. Lime E. DC REV	A. DV B. 3/16" C. Flame Cutting	A. Not given B. 1. II 5/32" 2a 155 - 25 2. III 5/32" 1a 156 - 25 3/16" 2a 190 - 25 1/4" 7b 245 - 24 C. I remainder not given C. 12 hrs. --- D. ---	A. None B. None	1 2 3	1 L U 6"	I II III Imp D 6" Imp D I III 263	Passed radiograph

Weld Metal

A. PART NUMBER OR B. DATE OF TEST C. PLATE NO. D. ORDER NUMBER E. SUBJECTS SPEC. F. ORDER NUMBER		A. TYPE B. TRADE NAME C. CHEMISTRY D. COMPOSITION & POLARITY		A. PROCESSES B. PREPARE C. FLAME D. PLATE PREPARATION		A. SIZE B. SPEED C. EXPOSURE D. DEVELOPMENT E. TONING F. WASHING G. DRYING		A. TYPE B. SPEED C. EXPOSURE D. DEVELOPMENT E. TONING F. WASHING G. DRYING		A. TYPE B. SPEED C. EXPOSURE D. DEVELOPMENT E. TONING F. WASHING G. DRYING		A. TYPE B. SPEED C. EXPOSURE D. DEVELOPMENT E. TONING F. WASHING G. DRYING	
A. AD-323 B. 3/15/43 C. 39 D. Carnegie-Ill- Inole Steel Co E. Metal & Thermit Corp. F. Briggs Mfg. Co	A. 1-1/2" B. R-I (1.19Mn, .22Si, .75Cr, 1.07Ni, .26Mo) C. .27 D. Face 302 E. B.O.H. F. 1544 of 1 1/2 hrs. Water 1058 of 2 1/2 hrs. Water	A. A-I (.07C, 1.19 Mn, .55Si, 18.80Cr, 9.93Ni, 2.13Mo) B. Murex C. Titanium D. DC REV	A. 45°DF B. 5/16" C. Flame Cutting Grinding	A. Copper bar B. I II 1/4" 2a 190 - 24 3. I 5/16" 2a 325 - 30 3/8" 2a 400 - 32 3. I 3/8" 2a 400 - 32 C. 6 hrs. 70° - 170° D. Copper removed after first pass. Adhesions after second pass	1 1099 2 1199 1" 3 1092	1 1/2" R 7" U 7" D 1" 5" L 5" D	Imp I II III 6 1/2" 18"	Passed radiograph					
A. AD-383 B. 3/15/43 C. 40 D. Carnegie-Ill- Inole Steel Co E. Crucible Steel Corp. F. Briggs Mfg. Co	A. 1-1/2" B. R-I (1.19Mn, .22Si, .75Cr, 1.07Ni, .26Mo) C. .27 D. Face 302 E. B.O.H. F. 1544 of 1 1/2 hrs. Water 1058 of 2 1/2 hrs. Water	A. A-I (.08C, 1.77 Mn, .19Si, 19.38Cr, 10.60Ni, 2.14Mo) B. Armorigize C. Titanium D. DC REV	A. 45°DF B. 5/16" C. Flame Cutting Grinding	A. Copper bar B. I II 1/4" 2a 190 - 24 3. I 5/16" 2a 325 - 30 3/8" 2a 400 - 32 3. I 3/8" 2a 400 - 32 C. 6 hrs. 70° - 170° D. Copper removed after first pass. Adhesions after second pass	1 1100 2 1100 3 1170	1 1/2" L 7" D 6 1/2" U 7" U 1 1/2" R 1 1/2" R	Imp II I 36" 38"	Passed radiograph					











IDENTIFICATION	ANNEAL DATA	PLATE DATA	WELD DATA	PROCESSING	HEAT		SALIENT RESULTS		REMARKS ON CRACKING
					A. PAG B. FOOT	H VEL 7/8	LOCATION OF H L1 L2 L3	CRACKING LOG TYPE AMT	
A. PART NUMBER B. DATE OF TEST C. PLATE NO. D. ORDER NUMBER E. SOURCE OF SPEC. F. ORDER NUMBER	A. PLATE TENSILE B. TYPE C. GRADE D. SIZE E. PROCESS F. HEAT TREATMENT G. YIELD TENSILE	A. TYPE B. TRADE NAME C. COATING D. CURRENT & POLARITY	A. SIZE B. POSITION C. ROOT TYPE D. SLOTTED TYPE E. OTHER TYPE F. TOTAL WELDING TIME @ ENTER PASS G. REMARKS	A. WELDED B. NONE	A. PAG B. FOOT	H VEL 7/8	LOCATION OF H L1 L2 L3	CRACKING LOG TYPE AMT	REMARKS ON CRACKING RADIOGRAPHED REEL 13.87A
A. AD-246 B. 2/2/43 C. 40 D. Republic Steel Corp. E. McKay Co. F. Federal Machine & Welder Co.	A. 1-1/2" B. R-1 C. (.87Cn, .27Si, .67Cr, .89Mn, .52P) D. Face 255 Back 255 E. B. Elec. F. 1300F 1 hr. Anneal 1600F 3/4 hr. Spray 1200° 1-1/2 hrs.	A. A-II (.11C, 4.00 Mn, .55Si, 20.00Cr, 10.00Ni) B. Armco C. Lime D. DC REV	A. 60°DV B. 1/4" C. Flame Cutting Grinding	A. Copper back up B. 1. II 3/16" 2a 165 - 23 4b 255 - 24 2. II 1/4" 1b 280 - 24 1/4" 13b 285 - 28 3. III 1/4" 8b 285 - 28 C. 19.18 hrs. 70° - 213° D. Eight passes less in cross-bar Chipping in all passes except the last	A. 70° B. None	1 2 3 4	1 2 3 4	II III II III	Passed radiograph

INFORMATION	ANNEAL DATA	ELECTRODE DATA	JOINT DESIGN	WELDING PROCEDURE		QUALITY RESULTS		REMARKS ON CRACKING
				A. TYPE	B. DEPOSITION	A. P.W.	B. POST	
A. PART NO.	A. TYPE	A. TYPE	A. GROOVE	A. SIZE	A. WEL. V/S	A. L.I.	A. L.O.	
B. DATE OF TEST	B. R-IV	B. TRADE NAME	B. ANGLE	B. EL. SIZE	B. WEL. V/S	B. L.I.	B. L.O.	
C. PLATE NO.	C. .94Mn, .81Si, .70Cr, .22Mo	C. COATING	C. ROOT GAP	C. ROOT TYPE	C. WEL. V/S	C. L.I.	C. L.O.	
D. ARMOR MANUFACTURER	D. .33	D. CORROSION & POLARITY	D. PLATE PREPARATION	D. BODY TYPE	D. WEL. V/S	D. L.I.	D. L.O.	
E. ELECTRODE SPEC.	E. Face 269	E. AC DC REV	E. CUTTING	E. GROUP TYPE	E. WEL. V/S	E. L.I.	E. L.O.	
F. ANNEAL PARAMETERS	F. Back 269	F. AC DC REV	F. GRINDING	F. TOTAL WELDING TIME & INTER PASS TEMPERATURE	F. WEL. V/S	F. L.I.	F. L.O.	
	F. Basic	F. AC DC REV	F. GRINDING					
	F. 1650°F. 3 hrs. Water	F. AC DC REV	F. GRINDING					
	F. 1180°F. 4 hrs. Draw	F. AC DC REV	F. GRINDING					
A. AD-35	A. 1-1/2"	A. A	A. 45°DV	A. Copper bar	1 1099	3"	4"	I 13"
B. 10/2/43	B. R-IV	---	B. 5/16"	B. 1. II 3/16"	A. None	L	D	II 12"
C. 59	C. .94Mn, .81Si, .70Cr, .22Mo	B. Armorloy	C. Flame	1a 185 - 22	B. None			III 2"
D. Great Lakes	C. .33	C. Titanium	Cutting	1a 250 - 40				III 2"
E. Steel Corp.	D. Face 269	D. AC DC REV		1a 360 - 40				III 2"
F. McKay Rods Co.	D. Back 269			1a 440 - 40				III 2"
F. Fisher Tank Division	E. Basic			2a 575 - 40				III 2"
	F. 1650°F. 3 hrs. Water			C. 1.34 hrs. 190° - 420°F.				III 2"
	F. 1180°F. 4 hrs. Draw			D.				III 2"
A. AD-35	A. 1-1/2"	A. A	A. 45°DV	A. Copper bar	1 1097	1 1/2"	6"	I 13"
B. 10/2/43	B. R-IV	---	B. 5/16"	B. 1. II 3/16"	A. None	L	D	II 12"
C. 60	C. .94Mn, .81Si, .70Cr, .22Mo	B. Armorloy	C. Flame	1a 185 - 22	B. None			III 2"
D. Jones & Laughlin	C. .24	C. Titanium	Cutting	1a 250 - 40				III 2"
E. Alloy Rods Co.	D. Face 241	D. AC DC REV		1a 360 - 40				III 2"
F. Fisher Tank Division	D. Back 248			1a 440 - 40				III 2"
	E. Basic			2a 560 - 40				III 2"
	F. 1650°F. 3 hrs. Water			C. 1.43 hrs. 180° - 500°F.				III 2"
	F. 1210°F. 4 hrs. Draw			D.				III 2"
A. AD-98	A. 1-1/2"	A. A-II	A. 45°DV	A. Copper bar	1 1109	1"	4"	I 13"
B. 10/8/43	B. R-IV	(.08C, 1.5 Mn, .37Si, .20.9Cr, 10.6Mn, 1.25Mo)*	B. 5/16"	B. 1. II 3/16"	A. None	R	D	II 12"
C. 61	C. .94Mn, .81Si, .70Cr, .22Mo	B. .37Si, .20.9Cr, 10.6Mn, 1.25Mo)*	C. Flame	1a 185 - 22	B. None			III 2"
D. Great Lakes	C. .33	B. Basic	Cutting	1a 246 - 40				III 2"
E. Reed-Avery	D. Face 270	C. Titanium	Grinding	1a 360 - 40				III 2"
F. Fisher Tank Division	D. Back 270	D. AC DC REV		1a 440 - 40				III 2"
	E. Basic			2a 440 - 40				III 2"
	F. 1650°F. 3 hrs. Water			C. 1.56 hrs. 180° - 400°F.				III 2"
	F. 1180°F. 4 hrs. Draw			D.				III 2"
A. AD-100	A. 1-1/2"	A. A-II	A. 45°DV	A. Copper bar	1 1097	3"	5"	I 13"
B. 10/13/43	B. R-IV	(.08C, 1.5 Mn, .37Si, .20.9Cr, 10.6Mn, 1.25Mo)*	B. 5/16"	B. 1. II 3/16"	A. None	L	D	II 12"
C. 62	C. .94Mn, .81Si, .70Cr, .22Mo	B. .37Si, .20.9Cr, 10.6Mn, 1.25Mo)*	C. Flame	1a 185 - 22	B. None			III 2"
D. Great Lakes	C. .30	B. Armorloy	Cutting	1a 250 - 40				III 2"
E. McKay Rods Co.	D. Face 269	C. Titanium	Grinding	1a 360 - 40				III 2"
F. Fisher Tank Division	D. Back 269	D. AC DC REV		1a 440 - 40				III 2"
	E. Basic			2a 440 - 40				III 2"
	F. 1600°F. 2 hrs. Water			C. 1.56 hrs. 180° - 400°F.				III 2"
	F. 1150°F. 4 hrs. Draw			D.				III 2"

Weld Metal

A. TEST NUMBER B. DATE OF TEST C. PLATE NO. D. ORDER NUMBER E. MANUFACTURER F. ORDER NUMBER	A. PLATE TENSILE			A. TYPE			A. WELDING			A. FAT			A. CRACKING			A. RADIOGRAPH				
	1. TYPE	2. TENSILE MARK	3. COATING	4. COATING	5. COATING	6. PLATE POSITION	7. DEPOSITION	8. EL. NO. TYPE	9. TEST TYPE	10. TEST TYPE	11. TEST TYPE	12. TEST TYPE	13. TEST TYPE	14. TEST TYPE	15. TEST TYPE	16. TEST TYPE	17. TEST TYPE	18. TEST TYPE		
AD-100 10/13/42 Great Lakes Steel Co. Reid-Avery Co. Fisher Tank Division	A. 1-1/2" B. R-IV (.71Mn, .79Si, .56Cr, .16Mo, .08Zr) C. .42 D. Face 269 Back 269 E. --- F. ---	A. A- --- B. Paco C. Titania D. AC DC REV	A. 45°DV B. 5/16" C. Flame Cutting Grinding	A. Copper bar B. --- 1. IJ 3/16" 1a 185 - 22 2. I 5/16" 1a 360 - 40 3. I 3/8" 2a 440 - 40 3. I 3/8" 2a 440 - 40 C. 1.45 hrs 180° - 420°F D. ---	1. IJ 3/16" 1a 185 - 22 2. I 5/16" 1a 360 - 40 3. I 3/8" 2a 440 - 40 3. I 3/8" 2a 440 - 40 C. 1.55 hrs 190° - 420°F D. Grinding after 4th pass	A. None B. None	1 1092	1 1092	1 1092	1 1092	1 1092	1 1092	1 1092	1 1092	1 1092	1 1092	1 1092	1 1092	1 1092	
AD-10 10/21/42 Great Lakes Steel Corp. Reid-Avery Co. Fisher Tank Division	A. 1-1/2" B. R-IV (.92Mn, .79Si, .63Cr, .17Mo, .09Zr) C. .30 D. Face 269 Back 269 E. Basic F. 1650°F 3 hrs Water 1180°F Draw	A. A-I (.11C, 4.0 Mn, .75Si, 19.0Cr, 1.25Mo, 9.0Ni, ) B. Raco C. Titania D. AC DC REV	A. 45°DV B. 5/16" C. Flame Cutting Grinding	A. Copper bar B. --- 1. I 3/16" 1a 185 - 22 2. I 5/16" 1a 250 - 40 3. I 3/8" 2a 360 - 40 3. I 3/8" 2a 440 - 40 C. 1.55 hrs 190° - 420°F D. Grinding after 4th pass	A. Copper bar B. --- 1. I 3/16" 1a 185 - 22 2. I 5/16" 1a 250 - 40 3. I 3/8" 2a 360 - 40 3. I 3/8" 2a 440 - 40 C. 1.55 hrs 190° - 420°F D. Grinding after 4th pass	A. None B. None	1 1104	1 1104	1 1104	1 1104	1 1104	1 1104	1 1104	1 1104	1 1104	1 1104	1 1104	1 1104	1 1104	1 1104
AD-100 10/29/42 Great Lakes Steel Corp. Reid-Avery Co. Fisher Tank Division	A. 1-1/2" B. P-IV (.71Mn, .79Si, .56Cr, .16Mo, .08Zr) C. .42 D. Face 269 Back 269 E. Basic F. 1600°F 2 hrs Water 1150°F 4 hrs Draw	A. A-I (.11C, 4.0 Mn, .75Si, 19.0Cr, 9.0Ni, 1.25Mo) B. Raco C. Titania D. AC DC REV	A. 45°DV B. 5/16" C. Flame Cutting Grinding	A. Copper bar B. --- 1. I 3/16" 1a 185 - 22 2. I 5/16" 1a 250 - 40 3. I 3/8" 2a 360 - 40 3. I 3/8" 2a 440 - 40 C. 1.54 hrs 160° - 460°F D. Grinding after 4th pass	A. Copper bar B. --- 1. I 3/16" 1a 185 - 22 2. I 5/16" 1a 250 - 40 3. I 3/8" 2a 360 - 40 3. I 3/8" 2a 440 - 40 C. 1.54 hrs 160° - 460°F D. Grinding after 4th pass	A. None B. None	1 1107	1 1107	1 1107	1 1107	1 1107	1 1107	1 1107	1 1107	1 1107	1 1107	1 1107	1 1107	1 1107	1 1107

IDENTIFICATION	ANNEAL DATA				ELASTICITY DATA			JOINT DESIGN			WELDING			PROCEDURE			HEAT			REMARKS																			
	A. FROM RECORD NO.	B. DATE OF TEST	C. PLATE NO.	D. ORDER MANUFACTURER	E. ELECTRODE SPEC.	F. AMPERAGE PARAMETER	A. TYPE	B. THICKNESS	C. NAME	D. COATING	E. CURRENT & POLARITY	A. GROOVE, INCLUDING ANGLE, ROOT FACE	B. ROOT GAP	C. PLATE PREPARATION	A. SAUING	B. DEPOSITION	C. SIZE & NO. TYPE	D. PASSES	E. ROOT TYPE		F. BODY TYPE	G. CRACK TYPE	H. TOTAL WELDING TIME	I. WELDER	J. WELDER	K. WELDER	L. WELDER	M. WELDER	N. WELDER	O. WELDER	P. WELDER	Q. WELDER	R. WELDER	S. WELDER	T. WELDER	U. WELDER	V. WELDER	W. WELDER	X. WELDER
A. AD-100 B. 10/21/43 C. 66 D. Great Lakes Steel Corp. E. Reid-Avery Co. F. Fisher Tank Division	A. 1-1/2" B. R-IV (.71Mn, .79Si, .56Cr, .16Mo, .08Zr) C. .43 D. Face 269 Back 269 E. Basic F. 1600°F. 2 hrs. Water 1150°F. Draw	A. A-I (.11C, 4.0 Mn, .75Si, 19.0Cr, 9.0Ni, 1.25Mo)* B. Raco C. Titania D. AC	A. 450V B. 5/16" C. Flame Grinding	A. Copper bar 1. II 3/16" 1a 185 - 40 2. I 1/4" 1a 250 - 40 5/16" 2a 360 - 40 3/8" 2a 440 - 40 3. I 3/8" 2a 440 - 40 C. 1.53 hrs. 160° - 460°F. D. Grinding after 1st pass.	1 1098 2 1104 3 1111	5" R 3 1/2" R 1" R	4" Imp U 6" D 5 1/2" D Imp	I 15 1/2" II 1 1/2" I 3 1/2" II 1 1/2" II 1 1/2" I 15 1/2" 33 1/2"	Passed radiograph																														
A. AD-100 B. 10/21/43 C. 67 D. Great Lakes Steel Corp. E. Reid-Avery Co. F. Fisher Tank Division	A. 1-1/2" B. R-IV (.92Mn, .79Si, .63 Cr, .17Mo, .09Zr) C. .30 D. Face 269 Back 269 E. Basic F. 1600°F. 2 hrs. Water 1150°F. 4 hrs. Draw	A. A-I (.11C, 4.0 Mn, .75Si, 19.0Cr, 9.0Ni, 1.25Mo)* B. Raco C. Titania D. AC	A. 450V B. 5/16" C. Flame Grinding	A. Copper bar 1. II 3/16" 1a 180 - 40 1/4" 1a 250 - 40 2. I 5/16" 2a 360 - 40 3/8" 2a 440 - 40 3. I 3/8" 2a 440 - 40 C. 1.50 hrs. 190° - 420°F. D. Grinding after 2nd pass.	1 1105 2 1161 3 1251	1" L 1" L X	5 1/2" U 6" D 7" D	I 4 1/2" II 26 1/2" 31	Passed radiograph																														
A. AD-99 B. 10/30/43 C. 68 D. Great Lakes Steel Corp. E. Alloy Rods Co. F. Fisher Tank Division	A. 1-1/2" B. R-IV (.90Mn, .81Si, .64Cr, .19Mo, .07Zr) C. .29 D. Face 263 Back 270 E. Basic F. 1675°F. 2 1/2 hrs. Water 1300°F. 2 1/2 hrs. Draw	A. A-II (.14C, 4.05 Mn, .34Si, 19.7Cr, 10.6Ni)* B. Armorare C. Titania D. AC DC REV	A. 450V B. 5/16" C. Flame Grinding	A. Copper bar 1. II 3/16" 1a 185 - 23 1/4" 1a 250 - 40 2. I 1/4" 1a 350 - 40 5/16" 3a 360 - 40 3. I 5/16" 2a 360 - 40 C. 1.59 hrs. 300° - 480°F. D. Grinding after 4th pass, also the fifth.	1 1095 2 1134	1" R X	7 1/2" Imp U 4 1/2" Imp D	II 2 1/2" III 6 1/2" I 36" V 3 1/2" 48 1/2"	Failed radiograph 6" crack in cross-bar																														

Weld Metal





IDENTIFICATION	ANODE DATA						ELECTRODE DATA			JOINT DESIGN			WELDING PROCEDURE			WEAT			BALLISTIC RESULTS			CRACKING			REMARKS ON CRACKING RADIOGRAPHING RESULTS, ETC.
	A. PARTS RECORD NO.	B. DATE OF TEST	C. PLATE NO.	D. MANUFACTURER	E. ELECTRODE OPER.	F. ANODE PARAMETER	A. TYPE	B. TRADE NAME	C. COATING	D. CURRENT & POLARITY	A. GROOVE, INCLUDED ANGLE, ROOT FACE	B. ROOT GAP	C. PLATE PREPARATION	A. BACKING	B. DEPOSITION SIZE SL. NO. TYPE AMPT V.	C. ROOT TYPE	D. ROOT TYPE	E. COVERS TYPE	F. TOTAL WELDING TIME & ENTER PASS TEMPERATURE	A. PAGE	B. POST	M. VEL. / %	N. LOCATION OF N. L. L. N. L. S. B.	O. CRACK TYPE	
A. AD-99 B. 10/31/42 C. 70 D. Great Lakes Steel Corp. E. Alloy Rods Co. F. Fisher Tank Division	A. 1-1/2" B. R-IV (.80Mn, .81Si, .64Cr, .19Mo, .07Zr) C. .29 D. Face 263 Back 270 E. Basic F. 1675F 2 1/2 hrs Water 1200F 2 1/2 hrs Draw	A. A-II (.08C, 3.60 Mn, .03Si, 19.3Cr, 10.2Ni, .012Mo)* B. Armorarc C. Titanium D. ---	A. 45°DV B. 5/16" C. ---	A. Copper bar B. 1. II 3/16" 1/4" 2. I 1/4" 5/16" 3. I 5/16" C. 2.02 hrs 198° - 500°F D. Grinding after 1st and 5th passes	A. 1500 F B. None	1 1100 2 1108	1" R 2 1"	5 1/2" Imp 6 1/2" 0	II 14 1/2" III 4 1/2" II 2 1/2" II 2 1/2"	Failed radiograph 2" deep seated crack in crossbar near right junction															
A. AD-99 B. 10/31/42 C. 71 D. Great Lakes Steel Corp. E. Alloy Rods Co. F. Fisher Tank Division	A. 1-1/2" B. R-IV (.80Mn, .81Si, .64Cr, .19Mo, .07Zr) C. .29 D. Face 263 Back 270 E. Basic F. 1675F 2 1/2 hrs Water 1200F 2 1/2 hrs Draw	A. A-II (.08C, 3.60 Mn, .03Si, 19.3Cr, 10.2Ni, .012Mo)* B. Armorarc C. Titanium D. ---	A. 45°DV B. 5/16" C. ---	A. Copper bar B. 1. II 3/16" 1/4" 2. I 1/4" 5/16" 3. I 5/16" C. 2.01 hrs 200° - 460°F D. Grinding after 3rd, 5th, and 7th passes	A. 1500 F B. None	1 1109 2 1158 3 1154	1 1/2" L 1" L 1" L	5 1/2" Imp 5 1/2" U 6 1/2" Imp 6 1/2" 0	I 2 1/2" II 3 1/2" V 6 1/2" I 3 1/2" I 6 1/2"	Passed radiograph															
A. AD-99 B. 10/31/42 C. 72 D. Great Lakes Steel Corp. E. Alloy Rods Co. F. Fisher Tank Division	A. 1-1/2" B. R-IV (.80Mn, .81Si, .64Cr, .19Mo, .07Zr) C. .29 D. Face 265 Back 265 E. Basic F. 1675F 2 1/2 hrs Water 1200F 2 1/2 hrs Air	A. A-II (.08C, 3.60 Mn, .03Si, 19.3Cr, 10.2Ni, .012Mo)* B. Armorarc C. Titanium D. AC DC REV	A. 45°DV B. 5/16" C. Flame Cutting Grinding	A. Copper bar B. 1. II 3/16" 1/4" 2. I 1/4" 5/16" 3. I 5/16" C. 2 hrs 180° - 500°F D.	A. 1500 F B. None	1 1120 2 1156 3 1209	X 1" R 1" R	3 1/2" Imp 6" Imp 6" D 6" D	II 2" III 3 1/2" II 6" III 3" I 16" II 1 1/2" II 4 1/2"	Passed radiograph															
		*Weld Metal																							









TESTING	MATERIAL	WELDING	WELDING	WELDING	WELDING	WELDING	WELDING	WELDING	WELDING	WELDING	WELDING
A. PART NO.	B. DATE OF TEST	C. PLATE NO.	D. WELDING METHOD	E. WELDING PROCEDURE	F. WELDING PARAMETERS	G. WELDING DEFECTS	H. WELDING RESULTS	I. WELDING DEFECTS	J. WELDING DEFECTS	K. WELDING DEFECTS	L. WELDING DEFECTS
A. AD-286 B. 2/25/43 C. W-57 D. Ford Motor Co. E. Arco Corp. F. Ford Motor Co.	A. 1-1/2" B. R-II (1.35Mn, .21Si, .54Cr, .03Ni, .45 Mo) C. .26 D. Face --- Back 262 E. Basic O.H. F. 16500 4 hrs. Water 1100° 6 hrs. Air Cool	A. A-I (.09C, 3.75 Mn, .75Si, 19.1Cr, 9.3Ni) 1.0Mo B. Chromang C. Lime D. DC REV	A. --- B. --- C. Flame Cutting	A. 3/16" Copper back up strip B. None 1. II 3/16" 2a 180 - 25 2. III 3/16" 10b 1a 180 - 25 3. III 3/16" 4b 180 - 25 C. 6 hrs. D.	1 1022 2 1048	A. None B. None	I 1022 II 1048	5/8" Imp U	1" R	Passed radiograph	
					Tested as cast armor by error						

WELDING PROCEDURE	WELDING POSITION	WELDING SPEED	WELDING METAL	WELDING METHOD	WELDING PARAMETERS	WELDING DEFECTS	WELDING RESULTS	WELDING TYPE	WELDING DATE	WELDING TESTS	WELDING RESULTS	WELDING RESULTS	
												WELDING TYPE	WELDING DATE
A. WELDING PROCEDURE	B. WELDING POSITION	C. WELDING SPEED	D. WELDING METAL	E. WELDING METHOD	F. WELDING PARAMETERS	G. WELDING DEFECTS	H. WELDING RESULTS	I. WELDING TYPE	J. WELDING DATE	K. WELDING TESTS	L. WELDING RESULTS	M. WELDING TYPE	N. WELDING DATE
A. AD-185 B. 1/13/43 C. 3-H D. Great Lakes E. Crucible Steel Co. F. Gen. American Trans. Corp.	A. 1-1/2" B. R-IV (.80Mn, .0751 .00Cr, .17Mo) C. .50 D. Face 269 Back 269 E. B.O.H. F. 1650 F. 2 hrs. Water 1210 F. 2 hrs. Air	A. A-I (.11C, 1.74 Mn, .31Si, 19.18Cr, 9.81Ni) B. Resistal C. Stainless D. Mineral Titanium Dioxide E. DC REV	A. 60°DV B. 3/16" C. Machining D. Buttering	A. Not given B. 1. II 5/32" 1a 100 - 25 3/16" 1a 200 - 25 2. III 3/16" 2a 300 - 25 11b 300 - 25 3. III 3/16" 10b 300 - 25 C. 14.30 hrs. 80° - 190° D.	A. None B. None	1103 1198	1" L 1/2" R	6 1/2" Imp 5 1/2" Imp U	V I II III 154	Passed radiograph			
A. AD-289 B. 3/3/43 C. 4-H D. Great Lakes E. The McKay Co. F. Gen. American Trans. Corp.	A. 1-1/2" B. R-IV (.93Mn, .78Si, .63Cr, .17Mo, .09Zr) C. .50 D. Face 263 Back 263 E. B.O.H. F. 1625 F. 1/2 hr. Water 1260 F. 3 hrs. Air	A. A-II (.11C 3.83 Mn, .38Si, 19.70Cr, 9.99Ni) B. Armolloy C. Titanium Base D. DC REV	A. 60°DV B. --- C. Flame Cutting	A. Not given B. 1. I 3/16" 1a 200 - 25 3/16" 2a 300 - 25 2b 275 - 28 3. III 1/4" 1b 200 - 25 3/16" 1b 200 - 28 5/16" 6b 200 - 30 C. 11 hrs. 90° - 190° D. Second pass was chipped and ground out	A. None B. 130	1100 1800	1 1/2" R 7/8" 5/8" Imp R U	6 1/2" Imp U	I 136"	Passed radiograph			



INFORMATION	ANNEAL DATA			PLATE DATA			WELDER DATA			WELDS			PROCEDURE			WELD			QUALITY RESULTS			REMARKS ON CRACKING RADIOGRAPHING RESULTS, ETC.			
	A. PLATE NO.	B. DATE OF TEST	C. PLATE NO.	D. MANUFACTURER	E. SIZE	F. SURFACE	G. SURFACE	H. SURFACE	I. SURFACE	J. SURFACE	K. SURFACE	L. SURFACE	M. SURFACE	N. SURFACE	O. SURFACE	P. SURFACE	Q. SURFACE	R. SURFACE	S. SURFACE	T. SURFACE	U. SURFACE	V. SURFACE	W. SURFACE	X. SURFACE	Y. SURFACE
A. AD-37 B. 10/8/42 C. 1 D. Dominion Foundries & Steel E. Lincoln Elec. F. Gen. Motors Div. of Canada	A. 1-1/2" B. R-V (.67Mn, .30Si, 2.26Cr, .65Ni .51Mo) C. .20 D. Face 377 Back 285 E. Elec. F. 1650°F 8 hrs Air 1650°F 4 hrs Water 1150°F 6 hrs Air	A. A B. --- C. Armoveld ARM-1 D. Lime DC REV	A. DV B. --- C. Flame Cutting Grinding	A. None B. 1. II 3/16" 2a 190 - 24 2. III 3/16" 1e 10b 190 - 24 5/32" 6b 145 - 22 1/4" 1b 245 - 30 3. III 3/16" 6b 190 - 24 C. 5.05 hrs --- D. One more pass in left leg and two pass in crossbar Chipping after all passes Cracking in the first two passes.	A. 100° F B. None C. 1094 D. 1091 1" R E. 1174 F. X G. X	A. Imp B. Imp C. Imp D. Imp	A. III B. III C. III D. III	A. Failed radiograph Lack of fusion present in lower left leg, crossbar, and upper right leg Slag inclusions in welds Welds ground flush																	
A. AD-133 B. 13/2/42 C. 2 D. Dominion Foundries & Steel E. Harnischfeger Corp. F. Gen. Motors Div. of Canada	A. 1-1/2" B. R-V (.58Mn, .50Si, 2.23Cr, .75Ni .37Mo) C. .29 D. --- E. Elec F. 1650°F 8 hrs Air 1650°F 6 hrs Water 1125°F 6 hrs Air	A. A B. AW-3 C. --- D. DC REV	A. DV B. 1/4" C. Flame Cutting Grinding	A. Coprer back up B. 1. II 5/32" 2a 150 - 18 2. III 1/4" 1a 230 - 20 1a 250 - 16 5/32" 6b 140 - 16 3. III 5/32" 4b 140 - 10 3/16" 2b 170 - 14 C. 4.45 hrs --- D. Chipping after all passes Cracking in first pass.	A. 125° F B. None C. 1089 D. 1186 E. 1186 1" F. R G. R	A. Imp B. D C. U D. Imp	A. III B. III C. III D. III	A. Passed radiograph																	
A. AD-194 B. 1/13/43 C. 3 D. Dominion Foundries & Steel E. Harnischfeger Corp. F. General Motors Div. of Canada	A. 1-1/2" B. R-V (.68Mn, .43Si, 2.26Cr, .71Ni, .31Mo) C. .26 D. --- E. Elec F. 1650°F 10 hrs Air 1650°F 6 hrs Water 1125°F 5 hrs Air	A. A-I (.13C, 1.64 Mn, .55Si, 19.3Cr, .71Ni, 10.4Al, 2.00Mo) B. AW 3-A C. --- D. DC REV	A. DV B. 1/4" C. Flame Cutting	A. Cop. r back up bar B. 1. II 1/4" 2a 240 - 16 2. I 5/16" 4a 300 - 20 3. III 5/32" 4b 140 - 16 1/4" 2b 300 - 20 C. 4 hrs. --- D. Chipping after all passes Cracking after first pass.	A. 125° F B. None C. 1091 D. 1155 E. 1091 1" F. R G. 7/8" R	A. Imp B. U C. Imp D. O	A. II B. III C. I D. II E. III F. II	A. Passed radiograph																	

Weld Metal

<p><b>TESTING DATA</b></p> <p>A. NAME OF TEST B. DATE C. PLATE NO. D. ORDER NUMBER E. DRAWING REF. F. ORDER NUMBER</p>	<p><b>PLATE THICKNESS</b></p> <p>A. TYPE B. SIZE C. GRADE D. DIM. E. WEIGHT F. TENSILE STRENGTH</p>	<p><b>WELDING DATA</b></p> <p>A. TYPE B. TRADE NAME C. COATING D. CURRENT &amp; POLARITY</p>	<p><b>WELDING PROCEDURE</b></p> <p>A. PROCEDURE B. ROOT GAP C. PLATE PREPARATION</p>	<p><b>TESTING DATA</b></p> <p>A. BACKING B. SPEED C. WELD TYPE D. WELD TYPE E. WELD TYPE F. WELD TYPE</p>	<p><b>TEST DATA</b></p> <p>A. SIZE B. NONE</p>	<p><b>TEST DATA</b></p> <p>A. SIZE B. NONE</p>	<p><b>TEST DATA</b></p> <p>A. SIZE B. NONE</p>	<p><b>TEST DATA</b></p> <p>A. SIZE B. NONE</p>	
<p>A. AD-192 B. 1/13/43 C. 4 D. Dominion Foundries &amp; Steel E. Harnischfeger Corp. F. General Motors Div. of Canada</p>	<p>A. 1-1/2" B. A-V C. (.66Mn, .43Si, .28Cr, .71Ni, .31Mo) D. .28 E. Elasco F. 1650 P. 10 hrs. Air 1650 P. 6 hrs. Water 1150 P. 5 hrs. Air</p>	<p>A. A-I (.13C, 1.64 Mn, .55Si, 19.3Cr, 10.4Al, 2.00Mo) B. AW 3-A C. --- D. DC REV</p>	<p>A. DV B. 1/4" C. Flame Cutting</p>	<p>A. Copper back up bar B. 1. II 1/4" 2a 270 - 10 2. III 1/4" 4b 270 - 18 3. III 5/16" 2a 310 - 20 4b 150 - 16 5. III 3/16" 2b 180 - 18 C. 4.30 hrs. --- D. Chipping after all passes Cracking after first pass.</p>	<p>A. 1250 P. B. None</p>	<p>1 D1113 1d 2 1206</p>	<p>62" U 5" D R</p>	<p>III Imp III O III Imp III V III 173 32</p>	<p>54" Passed radiograph</p>

Weld Metal





IDENTIFICATION	ANNEAL DATA	SURFACE DATA	COAT DESIGN	WELDING PROCEDURE	HEAT TREATMENT	M	VEL. F/8	BALLISTIC RESULTS		REMARKS ON CRACKING	
								LOCATION OF N	CRACKING		
A. FORD NUMBER	A. PLATE THICKNESS	A. TYPE	A. COAT, INCL. A. ADH. B. CAP	A. SALES	A. FACE B. POSE			L.L. R.L. G.B.	LOAD TYPE	AMT	
A. AD-82 B. 11/3/43 C. IHC-30 D. Jones & Laughlin E. McKay F. International Harvester Co.	A. 1-1/2" B. R-III (1.60Mn, .21S1 .42Mo) C. .28 D. Face 269 E. Back 269 F. B.O.H. 1200°F 1 hr Water 1200°F 2 1/2 hrs Air	A. A-IV (.12C, .40 Mn, .80Si, 20.Cr 9.7Ni) B. AC 5 C. Lime D. DC REV	A. 45°DV B. 3/16" C. Flame Cutting Grinding Descale	A. Not given B. 1. II 5/32" 3/16" 1/4" 1/4" 1/4" 2b 270 - 1b 255 - 3. III 5/32" 5/32" 1/4" 100° - 300°F C. 95 mine D.	A. 100° F B. None	1 2 3	1116 1217 1211	1 1/2" R L 1 1/2" R	5 1/2" U 7" D Imp 7 1/2" D O III 13 1/2"	II III I II III 1"	Passed radiograph
A. AD-82 B. 11/2/43 C. IHC-30 D. Jones & Laughlin E. McKay F. International Harvester Co.	A. 1-1/2" B. R-III (1.45Mn, .20S1 .44Mo) C. .23 D. Face 263 E. Back 263 F. B.O.H. 1200°F 1 hr Water 1200°F 2 1/2 hrs Air	A. A-IV (.12C, .40 Mn, .80Si, 20.Cr 9.7Ni) B. Armorloy C. Lime D. DC REV	A. 45°DV B. 3/16" C. Flame Cutting Grinding Descale	A. Not given B. 1. II 5/32" 3/16" 1/4" 1/4" 1/4" 3a 220 - 2a 260 - 1a 265 - C. 172 mins D.	A. 100° F B. None	1 2 3 4	1110 1112 1093 1090	2 1/2" L 1" R 2" R 1 1/2" L	5 1/2" U 6 1/2" D Imp 8" D O III 18"	II III II III II III 1"	Passed radiograph
A. AD-82 B. 11/3/42 C. IHC-31 D. Jones & Laughlin E. McKay F. International Harvester Co.	A. 1-1/2" B. R-III (1.55Mn, .23S1 .45Mo) C. .25 D. Face 255 E. Back 247 F. B.O.H. 1200°F 1 hr Water 1200°F 2 1/2 hrs Air	A. A-IV (.12C, .40Mn .80Si, .20.Cr 9.7Ni) B. Armorloy C. Lime D. DC REV	A. 45°DV B. 1/8" C. Flame Cutting Grinding Descale	A. Not given B. 1. II 5/32" 3/16" 1/4" 1/4" 1/4" 3a 250 - 2a 260 - 125° - 255°F C. 147 mine D.	A. 100° F B. None	1 2	1104 1206	1 1/2" R 1" R 2" R	6" Imp U 6 1/2" D Imp 1" R 8 1/2" II 24 1/2"	II I II II I II 1"	Passed radiograph

\*Weld Metal

MANUFACTURER A. PARTS ORDER NO. B. DATE OF TEST C. PLATE NO. D. ORDER NUMBER E. ORDER NUMBER F. ORDER NUMBER G. ORDER NUMBER H. ORDER NUMBER	ANNEAL DATA A. PLATE TREATMENT B. TYPE C. GARDEN CONTENT D. SOIL E. PROCESS F. HEAT TREATMENT G. TIME TIME ORDER	SLIPPER END A. TYPE B. TRAC NAME C. COATING D. CURRENT & POLARITY	JOINT PREP A. GROOVE INCLUDES B. ANGLE, ROOT FACE C. ROOT GAP D. PLATE PREPARATION	WELDING A. BACKING B. DEPOSITION SIZE EL. NO. TYPE AMR. V. C. ROOT TYPE D. GROWER TYPE E. TOTAL WELDING TIME & ENTER PASS TEMPERATURE F. REMARKS	HEAT A. PRE B. POST	H	BALLISTIC RESULTS		REMARKS ON CRACKING RADIOGRAPHING RESULTS, ETC.
							VEL. V/S	LOCATION OF H. L. L. N. L. G. L. LOC. TYPE AMR.	
A. AD-82 B. 11/2/42 C. IHC-32 D. Jones & Laughlin E. McKay F. International Harvester Co.	A. 1-1/2" B. R-III (1.45Mn, .20Si .44Mo) C. .23 D. Face 255 Back 241 E. F.O.H. F. 1625°F 1 hr Water 1200°F 2 1/2 hrs Air	A. A-IV (.12C, .40Mn, .80Si, .20Cr, 9.7Ni)* B. Armorloy C. Line D. DC REV	A. 45°DV B. 7/16" C. Flame Cutting Grinding Descale	A. Not Given B. 1. II 5/32" 2b 135 - 3/16" 1b 18C - 2. III 1/4" 2a 250 - 1/4" 1b 260 - 1/4" 1b 230 - 3. III 5/32" 4b 140 - 1/4" 2b 260 - C. 250 mins 150° - 250° D.	A. 100° F	1	1140	1 1/2" R 6" D 2 1/2" U 6" U 1099 1/2" L 1207 7 1/2" Imp 7 1/2" U 1214 6" L 2 1/2" D 2 1/2" D	Passed radiograph
A. AD-83 B. 11/2/42 C. IHC-33 D. Jones & Laughlin E. McKay F. International Harvester Co.	A. 1-1/2" B. R-III (1.53Mn, .22Si .47Mo) C. .23 D. Face 269 Back 262 E. B.O.H. F. 1625°F 1 hr Water 1200°F 2 hrs Air	A. A-IV (.12C, .40Mn, .80Si, .20Cr, 9.7Ni)* B. Armorloy C. Line D. DC REV	A. 45°DV B. 5/16" C. Flame Cutting Grinding Descale	A. Copper B. 1. II 3/16" 2a 175 - 2. III 1/4" 2a 260 - 1/4" 1b 255 - 1/4" 2b 250 - 3. III 5/32" 3b 135 - 1/4" 1b 140 - 1/4" 2b 250 - C. 485 mins 155° - 250°F D.	A. 90°F B. None	1	1104 1 1/2" R 1208 1 1/2" L 1220 1 1/2" L	5 1/2" U 7" D 7" Imp 7" D 7" Imp 5" I 14" II 3 1/2" I	Passed radiograph
A. AD-82 B. 11/2/42 C. IHC-34 D. Jones & Laughlin E. Crucible Steel F. International Harvester Co.	A. 1-1/2" B. R-III (1.45Mn, .20Si .44Mo) C. .23 D. Face 255 Back 255 E. B.O.H. F. 1625°F 1 hr Water 1200°F 2 1/2 hrs Air	A. A-I (.06C, .210Mn, .19Cr, 9.21Ni, 1.81Mo, .20V)* B. Armorize C. Extruded D. DC REV	A. 45°DV B. 5/16" C. Flame Cutting Grinding Descale	A. Copper B. 1. II 3/16" 1a 175 - 1/4" 1a 250 - 2. III 1/4" 2a 250 - 1/4" 2b 250 - 3. III 5/32" 2b 140 - 5/32" 2b 145 - 1/4" 2b 250 - C. 133 min 130° - 260°F D.	A. 100° F	1	1106 1 1/2" R 1201 1 1/2" R 1205 1 1/2" R 1245 1 1/2" R	5" U 7" D 7" D 5" U 7" D	Passed radiograph

\*Weld Metal

IDENTIFICATION	ANODE DATA			CATHODE DATA			WELDING PROCEDURE	HEAT		BALLBET RESULTS			REMARKS				
	A. PLATE THICKNESS	B. TYPE	C. COATING	A. TYPE	B. TYPE	C. POLARITY		A. P. A.	B. P. B.	H	V.L.	LOCATION OF N.L.L.		CRACKING			
A. DATE	B. DATE OF TEST	C. PLATE NO.	D. ANODE MANUFACTURER	E. CATHODE MANUFACTURER	F. ANODE FABRICATOR	A. SIZE	B. DEPOSITION	C. ROOT TYPE	D. SLOTTED TYPE	E. TOTAL WELDING TIME	F. ENTER PASS TEMPERATURE	A. P. A.	B. P. B.	C. P. C.	D. P. D.	E. P. E.	F. P. F.
A. AD-82 R. 11/2/42 C. IHC-35 D. Jones & Laughlin Co. E. Alloy Rods Co. F. International Harvester Co.	A. 1-1/2" B. R-III (1.45Mn, .22Si, .45Mo) C. .29 D. Face 269 Back 262 E. B.O.H. F. 1625°F 1 hr Water 1200°F 2 1/2 hrs Air	A. A-I (.10C, 1.5 Mn, .75Si, 19.0Cr, 9.25Ni, 3.00Mo)* B. Armerarc C. Tyre Bn D. DC REV	A. 45°DV B. 5/16" C. Flame Cutting Grinding Descable	A. 100° F B. None	1 1110 2 1198 3 1323 4 1198	1 1/4" R 1" R 2" L 3/4" L	6 1/2" D 5" U 6" U 6" D	Imp Imp Imp Imp	II 2 1/2" III 3 1/4" III 1 1/8"	Passed radiograph							
A. AD-82 R. 11/3/42 C. IHC-36 D. Jones & Laughlin E. McKay F. International Harvester Co.	A. 1-1/2" B. R-III (1.54Mn, .20Si, .52Mo) C. .27 D. Face 269 Back 259 E. B.O.H. F. 1625°F 1 hr Water 1200°F 2 1/2 hrs Air	A. A-IV (.12C, .4C Mn, .80Si, 20.0Cr, 9.7Ni)* B. Armerloy C. Lime D. DC REV	A. 45°DV B. 5/16" C. Flame Cutting Grinding Descable	A. 100° F B. None	1 1147 2 1203 3 1201 4 1211	1 1/4" R 3/4" L 1" R X	6" D 4 1/4" U 7" D 5 1/2" U	Imp Imp Imp Imp	II 2" III 3" III 1/2" I 4 1/4" III 1 1/2" III 1 1/2"	Passed radiograph							
A. AD-82 R. 11/2/42 C. IHC-37 D. Jones & Laughlin E. Crucible Steel F. International Harvester Co.	A. 1-1/2" B. R-III (1.68Mn, .21Si, .43Mo) C. .28 D. Face 269 Back 277 E. B.O.H. F. 1625°F 1 hr Water 1200°F 2 1/2 hrs Air	A. A-I (.06C, 2.10 Mn, 19.16 Cr, 9.21Ni, 1.61Mo, .20V)* B. Armerize C. Extruded D. ---	A. 45°DV B. 3/16" C. Flame Cutting Grinding Descable	A. 100° F B. None	1 1123 2 1219	3/4" R 3/4" R	6 1/2" D 4 1/4" U	Imp O Imp	I 6 1/4" II 6 1/4" III 2 1/4" I 2" I 6 1/4" II 7 1/4" II 3 3/4"	Passed radiograph							

\*Weld Metal  
of this type  
does not  
contain Mo.

IDENTIFICATION	ANVIL DATA	ELECTRODE DATA	JOINT DESIGN	WELDING PROCEDURES		HEAT TREATMENT	N	VEL. V/A	BALLISTIC RESULTS		REMARKS ON CRACKING RADIOGRAPHING RESULTS E.T.
				A. BACKING	B. DEPOSITION				A. SIZE	LOCATION OF N	
A. PLATE NUMBER	A. PLATE THICKNESS	A. TYPE	A. GROOVE	A. BACKING	A. DEPOSITION	A. SIZE	N	VEL. V/A	LOC. OF N	CRACKING	REMARKS ON CRACKING RADIOGRAPHING RESULTS E.T.
B. DATE OF TEST	B. TYPE	B. TRADE NAME	B. ANGLE	B. ROOT GAP	B. ROOT TYPE	B. ROOT GAP	N	VEL. V/A	LOC. OF N	CRACKING	REMARKS ON CRACKING RADIOGRAPHING RESULTS E.T.
C. PLATE NO.	C. CARBON CONTENT	C. COATING	C. FLAME	C. PLATE PREPARATION	C. ROOT TYPE	C. PLATE PREPARATION	N	VEL. V/A	LOC. OF N	CRACKING	REMARKS ON CRACKING RADIOGRAPHING RESULTS E.T.
D. ANVIL MANUFACTURER	D. SIZE	D. POLARITY	D. DC REV	D. DC REV	D. ROOT TYPE	D. DC REV	N	VEL. V/A	LOC. OF N	CRACKING	REMARKS ON CRACKING RADIOGRAPHING RESULTS E.T.
E. HEAT TREATMENT	E. PROCESS	E. POLARITY	E. DC REV	E. DC REV	E. ROOT TYPE	E. DC REV	N	VEL. V/A	LOC. OF N	CRACKING	REMARKS ON CRACKING RADIOGRAPHING RESULTS E.T.
F. ANVIL FABRICATOR	F. TENSILE	F. TENSILE	F. TENSILE	F. TENSILE	F. ROOT TYPE	F. TENSILE	N	VEL. V/A	LOC. OF N	CRACKING	REMARKS ON CRACKING RADIOGRAPHING RESULTS E.T.
A. AD-82 B. 11/2/42 C. IHC-58 D. Jones & Laughlin E. McKay F. International Harvester Co.	A. 1-1/2" B. R-II (.55Mn, .23Si, .45Mo) C. .25 D. Face 269 Back 277 E. B.O.H. F. 1635°F. 1 hr. Water 1200°F. 2 1/2 hrs. Air	A. A-II (.12C, 4.0Mn, .80Si, .20Cr, 9.7Ni)* B. Armorloy C. Lime D. DC REV	A. 450V B. 5/16" C. Flame Grinding Descaling	A. BACKING B. DEPOSITION C. ROOT TYPE D. ROOT TYPE E. TOTAL WELDING TIME & ENTER PASS TEMPERATURE	A.100° F. B. None C. None D. None	1 1110 X 2 1211	1 2	1110 1211	5 3/4" D 4" U 1" R 4" U	Imp I II 12" 16"	Passed radiograph
A. AD-287 B. 2/16/43 C. I.H.C. 58 D. Great Lakes Steel Corp. E. McKay Company F. International Harvester Co.	A. 1-1/2" B. R-IV (.92Mn, .79Si, .63Cr, .17Mo, .09Zr) C. .30 D. Face 269 Back 300 E. B.O.H. F. 1635°F. 2 hrs. Water 1200°F. 2 hrs. Air	A. A-II (.12C, 4.0Mn, .80Si, .20Cr, 9.7Ni)* B. Armorloy C. Lime D. DC REV	A. 450V B. 5/16" C. Flame Cutting Grinding	A. BACKING B. DEPOSITION C. ROOT TYPE D. ROOT TYPE E. TOTAL WELDING TIME & ENTER PASS TEMPERATURE	A.100° F. B.120° F.	1 1093 3/8 2 1169	1 2	1093 1169	6 3/4" D 5 1/4" U X	Imp I II 26" 28"	Passed radiograph
A. AD-287 B. 2/16/43 C. I.H.C. 58 D. Great Lakes Steel Corp. E. McKay Company F. International Harvester Co.	A. 1-1/2" B. R-IV (.71Mn, .79Si, .56Cr, .16Mo, .08Zr) C. .43 D. Face 269 Back 286 E. B.O.H. F. 1600°F. 2 hrs. Water 1240°F. 2 hrs. Air	A. A-II (.12C, 4.0Mn, .80Si, .20Cr, 9.7Ni)* B. Armorloy C. Lime D. DC REV	A. 450V B. 5/16" C. Flame Cutting Grinding	A. BACKING B. DEPOSITION C. ROOT TYPE D. ROOT TYPE E. TOTAL WELDING TIME & ENTER PASS TEMPERATURE	A.200° F. B. None	1 1113 1 3/8 L	1	1113	6" D	Imp I 23 1/4"	Passed radiograph

\*Weld Metal



IDENTIFICATION	ANNEAL DATA	BASE TIME DATA	WELDING PROCEDURE	WELDS	WELT	N	V/L	WELDING		WELT	WELT	WELT	WELT
								A. TYPE	B. NAME				
A. AD-287 B. 2/16/43 C. I.H.C. 47 D. Great Lakes E. Steel Corp. F. International G. Harvester Co.	A. PLATE THICKNESS B. TYPE C. GROSS WEIGHT D. SIZE E. PROCESS F. HEAT TREATMENT G. WELD TIME	A. TYPE B. NAME C. WEIGHT D. POLARITY	A. 45°DV B. 5/16" C. Flame Grinding	A. COPPER BACK UP B. 1. II 5/32" 1a 180 - 3/16" 1a 180 - 2. III 1/4" 2a 280 - 1/4" 4b 280 - 3. III 5/32" 4b 280 - 1/4" 4b 140 - 1/4" 2b 280 - C. 3.63 hrs. 1500° - 300°F. D. Grinding after first and third passes	A. 100° F B. None	1 1085	2 1093	3"	1" R	64" U 64" D	I 36"	Passed radiograph	
A. AD-287 B. 2/16/43 C. I.H.C. 48 D. Great Lakes E. Steel Corp. F. International G. Harvester Co.	A. PLATE THICKNESS B. TYPE C. GROSS WEIGHT D. SIZE E. PROCESS F. HEAT TREATMENT G. WELD TIME	A. TYPE B. NAME C. WEIGHT D. POLARITY	A. 45°DV B. 5/16" C. Flame Grinding	A. COPPER BACK UP B. 1. II 5/32" 1a 140 - 3/16" 1a 180 - 2. III 1/4" 2a 250 - 1/4" 2b 280 - 1/4" 1b 265 - 3. III 5/32" 4b 140 - 1/4" 2b 280 - C. 3.76 hrs. 1500° - 310°F D. Chipping and grinding, fifth, after first, second, fifth, 15th and 14th passes Chipping after 3rd, 4th 8th through 11th File S.91	A. 100° F B. None	1 1093	2 1211	3"	5/8" R	54" D 64" U 64" D	II 54" III 54" II 1" I 17" II 39"	Passed radiograph	
A. AD-287 B. 2/16/43 C. I.H.C. 49 D. Great Lakes E. Steel Corp. F. International G. Harvester Co.	A. PLATE THICKNESS B. TYPE C. GROSS WEIGHT D. SIZE E. PROCESS F. HEAT TREATMENT G. WELD TIME	A. TYPE B. NAME C. WEIGHT D. POLARITY	A. 45°DV B. 5/16" C. Flame Grinding	A. COPPER BACK UP B. 1. II 5/32" 1a 135 - 5/32" 1a 140 - 2. I 1/4" 4a 260 - 1/4" 3a 265 - 3. I 1/4" 2a 255 - C. 3.39 hrs. 1400° - 280°F. D. Grinding after 1st, 3rd, 5th, 7th 8th and 10th. Time 3.65 hrs.	A. 100° F B. None	1 1100	2 1175	3"	7" R	7" D 64" U	I 142" II 23" I 36" I 53"	Passed radiograph	



IDENTIFICATION	PLATE THICKNESS	MATERIAL DATA	WELDING DATA	PREPARATION	HEAT	WELDING	EXAMINATION
A. PART NUMBER	A. TYPE	A. GRADE, MANUFACTURER'S NAME, SHEET PAGE	A. BACKING	A. PREP	H. VOLTAGE	ELECTRODE	RESULTS
B. DATE OF TEST	B. THICKNESS	B. TENSILE	B. DEPOSITION	B. POST	I. WELDING	WELDING	RESULTS
C. PLATE NO.	C. SHEET NO.	C. GRADE	C. ROOT TYPE	C. POST	II. WELDING	WELDING	RESULTS
D. JONES & Laughlin	D. .28	D. 104C	D. 155	D. None	III. WELDING	WELDING	RESULTS
E. Arcos Corp.	E. .28	E. 18.50Cr	E. 210	E. None	IV. WELDING	WELDING	RESULTS
F. Lima Locomotive Tank Arsenal	F. B.O.H.	F. 10.25Ni	F. 245	F. None	V. WELDING	WELDING	RESULTS
AD-123 11/30/43	1-1/2" R-III (1.60Mn, .19Si, .52Mo)	A-I (.104C, 3.27 Mn, 32Si, 18.50Cr, 10.25Ni, .97Mo)*	A. Sas 1015 backing strip B. 1. II 5/32" 2a 155 - 20-30 2. III 3/16" 2a 4b 210 - 20-30 3. III 1/4" 6b 245 - 20-30 C. 6.30 hrs. 100° - 200°F D.	A. None B. None	1 1128 2 1198	3" 4 1/2" Imp 2" R 4 1/2" U 1" R	II 10" Passed radiograph I 6 1/2" II 19 1/2" 35 1/2"

Weld Metal

IDENTIFICATION	ANODE DATA	ELECTRODE DATA	JOINT DESIGN	WELDING PROCEDURE	WELD	BALLISTICS RESULTS		REMARKS OR UNUSUAL RADIOGRAPHIC RESULTS, ETC.	
						H	VEL. FT/S		LOCATION OF H
A. PART NUMBER OR DATE OF TEST	A. PLATE THICKNESS B. TYPE C. GASKET CONTENT D. SIZE E. PROCESS F. HEAT TREATMENT G. TENSILE CHARACTERISTICS	A. TYPE B. TRADE NAME C. COATING D. CURRENT & POLARITY	A. GROOVE, INCLUDED ANGLE, ROOT FACE B. ROOT GAP C. PLATE PREPARATION	A. BACKING B. DEPOSITION SIZE (L. NO. TYPE AMT. V) C. ROOT TYPE D. BODY TYPE E. COVER TYPE F. TOTAL WELDING TIME & ENTER PASS TEMPERATURE G. REMARKS	A. NONE B. POOR	1	1"	5 1/2"	Passed radiograph
A. AD-137 B. 12/17/42 C. CR-36 D. Carnegie Steel E. Crucible Co. F. Midland Steel Products	A. 1-1/2" B. R-I (1.01Mn, .19Si, .42Cr, 1.0%Ni, .37Mo) C. .24 D. --- E. B.O.H. F. ---	A. A-I (.12C, 1.90 Mn, .28Si, 18.54Cr, 8.06Ni, 2.15Mo)* B. Armorize C. TiO <sub>2</sub> D. AC STR	A. 450DV B. 1/4" C. Flame Cutting	A. Copper backing B. 1. II 3/16" 2a 160 - 22 2. III 1/4" 4a 220 - 25 3. III 3/16" 4b 160 - 22 C. 12 hrs 1/4" 2b 230 - 25 D. 155° - 320°F	A. None B. None	1 1121 2 1221 3 1202 1 1/2"	1" R 1/4" R 6" U Imp 6" U Imp	I 6 1/2" II 1 1/2" III 9 1/2" V 2 1/2" III 1" III 17 1/2" III 38 1/2"	

eWeld Metal

IDENTIFICATION	ANODE DATA	ELECTRODE DATA	JOINT DESIGN	WELDING PROCEDURE	HEAT	BALLISTIC RESULTS			REMARKS ON CRACKING	REMARKS ON RADIOGRAPHIC RESULTS
						M VEL. F/S	LOCATION OF H. L.L. R.L. O.B.	CRACKING LOC. TYPE AMT		
A. NAME AND NO.	A. PLATE THICKNESS	A. TYPE	A. GROOVE INCLUDED	A. BACKING	A. PAIR					
B. DATE OF TEST	B. TYPE	B. TRADE NAME	B. ANGLE, ROOT FACE	B. DEPOSITION	B. POST					
C. ANODE MANUFACTURER	C. CARBON CONTENT	C. COATING	C. ROOT GAP	C. ROOT TYPE						
D. ELECTRODE SPEC.	D. SIZE	D. CURRENT & POLARITY	D. PLATE PREPARATION	D. ROOT TYPE						
E. ANODE FABRICATOR	E. HEAT TREATMENT	E. PREP.	E. PREP.	E. ROOT TYPE						
	F. HEAT TREATMENT	F. PREP.	F. PREP.	F. ROOT TYPE						
	F. HEAT TREATMENT	F. PREP.	F. PREP.	F. ROOT TYPE						
A. AD-140	A. 1-1/2"	A. A-II	A. 45°DV	A. Copper back up strip 3/8"	A. None	1	1095	6" Imp	I	5" Failed radiograph
B. 12/5/42	B. R-III	(.12C, 4.00 Mn, .60Si, .23S1, .41Mo)	B. 5/16" Flame	1. II 3/16" 1a 170 -	B. None	2	1096	6" O	II 4" Excessive amount of incomplete fusion.	
C. NYAB-12	C. .25	B. Armorloy	C. Grinding	2. I 5/16" 1a 300 -		3	1090	6" U	III 1 1/2" crack near right weld junction.	
D. Jones & Laughlin	D. ---	C. Lime		3. I 3/8" 2a 410 -				6 1/2" Imp	I 1 1/2" Junction.	
E. McKay Company	E. B. Elsc.	D. DC REV		C. --- 70 - 375°F.				6 1/2" D	II 1 1/2" Junction.	
F. New York Air Brake Co.	F. ---			D. 3/8" welding rods used in welding. Copper strip ground out before pass #3 put in. A 9th pass was used so that final pass would be flush, 5/16" rod at 300 Amps used.				III 1 1/2" Junction.		
A. AD-135	A. 1-1/2"	A. A-I	A. 45°DV	A. Not given	A. None	1	1097	3" U		Passed radiograph
B. 12/11/42	B. R-III	(.112C, 1.5 Mn, .45Si, .23S1, .41Mo)	B. 1/4" Flame	1. II 3/16" 2a 150 - 25	B. None	2	1211	2 1/2" L		Lack of penetration evident in opened crack
C. NYAB-17	C. .25	B. Armorloy	C. Grinding	2. I 5/16" 1a 400 - 33		3	1183	1" D	I 1 1/2" Junction.	
D. Jones & Laughlin	D. ---	C. Lime		3. I 5/16" 1a 400 - 29				1" L	II 5 1/2" Junction.	
E. Harnischfeger Corp.	E. B.O.H.	B. AW-3		C. --- 90 - 190°F.				6 1/2" Imp	III 30"	
F. New York Air Brake Co.	F. ---	C. Titanium		D.						
A. AD-135	A. 1-1/2"	A. A-II	A. DV	A. Not given	A. None	1	1107	4 1/2" Imp	III	4 1/2" Failed radiograph
B. 12/11/42	B. R-III	(.10C, 4.00 Mn, .60Si, .23S1, .41Mo)	B. --- Flame	1. II 3/16" 1a 170 - 25	B. None	2	1199	1 1/2" L	III	Incomplete fusion
C. NYAB-19	C. .25	B. Armorloy	C. Grinding	2. I 5/16" 2a 310 - 25				6" U	I	Scattered gas pores
D. Jones & Laughlin	D. ---	C. Lime		3. I 5/16" 1a 310 - 25				1" L	II	Crater crack at left junction
E. Lincoln	E. B.O.H.	B. O.H.		C. 10 hrs. 1250 - 175°F.				4" D	III	1-1/2" weld crack
F. New York Air Brake Co.	F. ---	D. DC REV		D. One less pass in crossbar					II 8 1/2"	
									III 2 1/2"	
									III 4 1/2"	

Weld Metal

IDENTIFICATION	ANNEAL DATA	MATERIALS DATA	COAT DATA	WELDING	PROCEDURE	HEAT		BALLING RESULT		REMARKS OR COMMENTS	
						A. P. #	B. P. #	H. V. #	LOC. TYPE		CRACKING
A. PART NO.	A. PLATE NUMBER	A. TYPE	A. GRADE	A. SIZE	A. POSITION	A. P. #	A. P. #	H. V. #	LOC. TYPE	CRACKING	REMARKS
A. AD-340 B. 3/26/43 C. 37 D. Carnegie- Illinois E. Lincoln Elec. McKay Company F. New York Air Brake Company	A. 1-1/2" B. R- (.98Mn, .17Si, .58Cr, .99Ni, .34Mo) C. .30 D. Face 238 McKay 322 E. P.O.H. F. 1544 F. 1 1/2 hrs. Water 10500F. 1 1/2 hrs.	A. A. L. E. Co. (.12C, 3.50 Mn, .45Si, 19.0Cr, 8.5Ni) % McKay (.10C, 3.50 Mn, .80Si, 19.0Cr, 9.20Ni) % B. Armorweld C. Armorloy D. DC REV	A. 45 <sup>3</sup> DV B. 1/4" C. Flame Cutting Grinding	A. 1/4" round strip B. 1. II 5/32" 1a 155 - 25 5/32" 1a 160 - 27 2. I 3/16" 2a 225 - 30 1/4" 2a 300 - 30 3. I 5/16" 2a 425 - 30 C. 48 hrs. 75 - 90 D. Grinding after first and third passes. Crossbar has four more passes in body	A. None B. None	1 1106 2 1209 X	3" R	7 1/2" U 3 1/2" D 5" 13 1/2" 6" 35 1/2"	I II V I I II III	34" Passed radiograph	

Weld Metal













IDENTIFICATION	ANODE DATA	CATHODE DATA	JOINT DESIGN	WELDER	WELD	WEAT	BALLING RESULTS			REMARKS ON CRACKING		
							H	V	L			
A. FORD NUMBER NO.	A. PLATE THICKNESS	A. TYPE	A. GROUND WALLS	A. SA OILING	A. None	A. None	L.L.	M.L.	U.B.	CRACKING	REMARKS ON CRACKING	
B. DATE OF TEST	B. TYPE	B. TRADE NAME	B. ROOT GAP	B. DESCRIPTION	B. None	B. None	1"	1"	6"	III	6"	
C. PLATE NO.	C. CARBON CONTENT	C. COATING	C. PLATE PREPARATION	C. I	C. None	C. None	R	R	3/8"	III	3/8"	
D. ASSESS INFORMATION	D. SIZE	D. CURRENT & POLARITY	D. PLATE PREPARATION	D. I	D. None	D. None	U	U	1"	III	1"	
E. ELECTRIC SUPPLY	E. PROCESS	E. WEAT TREATMENT	E. WEAT TREATMENT	E. I	E. None	E. None	D	D	1"	III	1"	
F. AMPER REGULATOR	F. WEAT TIME	F. WEAT TIME	F. WEAT TIME	F. I	F. None	F. None	15"	15"	1"	III	15"	
A. AD-336 B. 3/23/43 C. 1 D. Henry Disston & Sons E. Alloy Rods Co F. York Safe & Lock Co.	A. 1-1/2" B. R-V (.51Mn, .20Si, .10Cr, 4.77Ni, .34Mo, .10V) C. .21 D. Face 269 Back 263 E. O.H. F. 1425 <sup>o</sup> F. 2 hrs. Water	A. A-II (.10C, 4.00 Mn, .35Si, 19.5Cr, 10.00Ni)* B. Armorarc C. Titania D. DC REV	A. 90 <sup>o</sup> DV B. 1/8" C. ---	A. None B. I 1/8" 1a 200 - 30 I 3/16" 2a 300 - 35 1/4" 6a 375 - 35 3. I 1/4" 2a 375 - 35 C. 9:30 hrs. 80 <sup>o</sup> - 230 <sup>o</sup> F. D.	A. None B. None	A. None B. None	1"	1"	6"	III	6"	Passed radiograph

\*Weld Metal

PLATE NO. AND A. PLATE NUMBER B. DATE OF TEST C. PLATE NO. D. ASER MANUFACTURER E. ELECTRODE SPON. F. AMPER FLOW-DIRECTION	PLATE THICKNESS A. TYPE B. COATING C. CORROSION D. PROCESS E. HEAT TREATMENT F. VIBRATION	PLATE NAME A. TYPE B. TRADE NAME C. COATING D. CORROSION E. POLARITY	JOINT A. GROOVE, WELDER'S ANGLE, JOINT FACE B. JOINT GAP C. PLATE PREPARATION	WELDING A. BACKING B. DEPOSITION C. ROOT TYPE D. BODY TYPE E. CRACK TYPE F. TOTAL WELDING TIME & ENTER PASS TEMPERATURE	HEAT A. PAW B. POST	BALLING RESULTS			REMARKS	
						N	V/L V/S	LOCATION OF N L.L. K.L. G.B.		
A. AD-53 B. 10/8/42 C. 295 D. Republic Steel Corp. E. Linde Air Products F. American Loco- motive Company	A. 1-1/2" B. F.V. C. .47Mo, .2281, .22Cr, 4.05Ni, .39Mn D. Face 253 Back 245 E. --- F. ---	A. A-1 (.20C, 3.01 Mn, .60Si, 17.42Cr, 11.50Ni, .37Mo) B. Oxweld 441 C. 12X200 20 Melt (Flux) D. AC	A. 45°DV B. --- C. Flame Cutting Grindir	A. Spacer strip 25-20 B. Special Unionmelt Two passes 1/4" 2UM 850 - 1100 - 35 - 36 C. 40.68 mins. 1450 - 1550F D. Crater on end tab	A. 1500 F. B. None	N	1104	1" 6" R D	I 104 II 84 III 3 V 14	Failed radiograph 2" weld crack in upper left leg 1-1/2" deep seated weld crack in crossbar Large blowholes in lower right leg Lower half of legs are 22" long

\*Weld Metal

IDENTIFICATION A. PART NUMBER NO. B. DATE OF TEST C. PLATE NO. D. ASSEMBLY MANUFACTURER E. ELECTRODE BRAND F. ASSEMBLY MANUFACTURER	ANODE DATA A. PLATE THICKNESS B. TYPE C. GASKON CONTENT D. BURN E. PROCESS F. HEAT TREATMENT G. TEMP TIME CHURN	ELECTRODE DATA A. TYPE B. TRADE NAME C. COATING D. CURRENT & POLARITY	JOINT DESIGN A. GROOVES INCLUDED B. ANGLE, ROOT FACE C. ROOT GAP D. PLATE PREPARATION	WELDING PROCEDURE A. BACKING B. DEPOSITION C. ROOT TYPE D. BODY TYPE E. CROWN TYPE F. TOTAL WELDING TIME & ENTER PASS TEMPERATURE G. REMARKS	HEAT A. PRE B. POST	BALLING RESULTS		REMARKS ON CRACKING RADIOGRAPHIC RESULTS, ETC.
						H. VEL. P/S	I. LOCATION OF N. L.L. M.L. C.B.	
A. AD-100 B. 10/21/42 C. U-19 D. Great Lakes Steel Corp. E. Molay Company F. Fisher Tank Products Division	A. 1-1/2" B. R-IV (.71Mn, .79Si, .56Cr, .16Mo, .08Zr) C. .43 D. Face 269 Back 269 E. Basic F. 1600°F, 2 hrs. Spray 1150°F, 4 hrs. Draw	A. A B. Armorloy Oxweld #43 C. --- D. DC REV	A. 45°DV B. 5/16" C. Flame Cutting Grinding	A. Copper bar B. 1. II 3/16" 2a 185 - 22 3a 185 - 22 2. V 3/16" 2a 185 - 22 3a 185 - 22 1/4" 1UM 980 - 35 1/4" 1UM 1200 - 35 C. 2.08 hrs. 1900 - 400°F. D. Grinding after 4th pass.	A. None B. None	1 1105	1 36" II 40"	I 36" II 40" Failed radiograph Deep seated weld cracks along crossbar and lower legs
A. AD-100 B. 10/21/42 C. U-20 D. Great Lakes Steel Corp. E. Molay Company F. Fisher Tank Products Division	A. 1-1/2" B. R-IV (.92Mn, .79Si, .53Cr, .17Mo, .09Zr) C. .30 D. Face 269 Back 269 E. Basic F. 1600°F, 2 hrs. Spray 1150°F, 4 hrs. Draw	A. A B. Armorloy Oxweld #43 C. Titania D. AC	A. 45°DV B. 5/16" C. Flame Cutting Grinding	A. Copper bar B. 1. II 3/16" 2a 185 - 22 3a 185 - 22 2. V 3/16" 2a 185 - 22 3a 185 - 22 1/4" 1UM 900 - 36 1/4" 1UM 1200 - 36 C. 2.08 hrs. 2000 - 340°F. D. Grinding after last pass.	A. None B. None	1 1100 2 1096	1 18" II 39"	I 18" II 39" Failed radiograph Lower right leg and crossbar are entirely cracked up in the weld
A. AD-116 B. 12/12/42 C. U-21 D. Great Lakes Steel Corp. E. Linde Air Products Division F. Fisher Tank Division	A. 1-1/2" B. R-IV (.94Mn, .67Si, .59Cr, .18Mo, .09Zr) C. .29 D. --- E. Basic F. ---	A. A B. Armorweld #43 C. Titania D. DC REV	A. 45°DV B. 5/16" C. Flame Cutting Grinding	A. Copper bar B. 1. I 3/16" 1a 185 - 22 2a 185 - 22 2. V 3/16" 1a 185 - 22 2a 185 - 22 1/4" 1UM 840 - 35 1/4" 1UM 1000 - 35 C. 1.52 hrs. 2800 - 340°F. D.	A. None B. None	1 1098	1 37" II 61" II 104" II 51" II 49"	I 37" II 61" II 104" II 51" II 49" Passed radiograph 1-1/8" crater crack in crossbar weld

INVESTIGATION	ARMOR DATA	ELECTRODE DATA	JOINT DESIGN	WELDING PROCEDURE	HEAT TREATMENT	RADIATION RESULTS			REMARKS ON CRACKING		
						H	VEL. F/S	LOCATION OF H. CRACKING			
A. FIRM SOURCE NO.	A. PLATE THICKNESS	A. TYPE	A. GROOVE, INCLUDED	A. BACKING	A. PRE	L.L.	R.L.	O.B.	LOC. TYPE	ANY	
B. DATE OF TEST	B. TYPE	B. TRADE NAME	B. ROOT GAP	B. DEPOSITION	B. POST						
C. PLATE NO.	C. CARBON CONTENT	C. COATING	C. FLAME	C. ROOT TYPE	C. TYPE						
D. ARMOR MANUFACTURER	D. SWH	D. CURRENT & POLARITY	D. CUTTING	D. ROOT TYPE	D. TYPE						
E. ELECTRODE SUPPL.	E. PHOSPHOR	E. POLARITY	E. GRINDING	E. COGNITIVE	E. TYPE						
F. ARMOR FABRICATOR	F. TENSILE	F. TENSILE	F. TENSILE	F. TOTAL WELDING TIME & INTER PASS TEMPERATURE	F. TYPE						
A. AD-194 B. 1/13/43 C. 8 D. Dominion Foundries & Steel Ltd. E. Haralshofeger Corp. Linde Air Products F. General Motors Div. of Canada	A. 1-1/2" B. R-V (.69Mn, .39Si, 2.45Cr, .71Ni, .30Mo) C. .26 D. --- E. --- F. 1650°F. 10 hrs. Air 1650°F. 6 hrs. Water 1150°F. 5 hrs. Air	A. A --- B. AW 3-A Oxweld #41 C. --- D. ---	A. DV B. 3/8" C. Flame Cutting	A. Copper back up bar B. 1. II 1/4" 3a 230 - 16 2. IV 3/16" 2UM 1000 - 35 C. 2.15 hrs. 1100 - 130°F. D. Chipping after all passes. Cracking after first two passes. Hand and automatic welding	A. 125° F. B. None	1	1099	1/2" L	6" U	I II 312 54	26" Failed radiograph Crossbar is en- tirely cracked 2" crack at end of weld
A. AD-214 B. 1/27/43 C. 9 D. Dominion Foundries & Steel Ltd. E. Lincoln Elec. Products F. General Motors Div. of Canada	A. 1-1/2" B. R-V (.57Mn, .34Si, 2.25Cr, .72Ni, .28Mo) C. .28 D. --- E. Elec. F. 1650°F. 10 hrs. Air 1650°F. 6 hrs. Water 1150°F. 5 hrs. Air	A. A --- B. Armorweld ARW-1 Oxweld #41 C. --- D. AC	A. DV B. 1/4" C. Flame Cutting Grinding	A. Copper back up bar B. 1. II 5/32" 2a 150 - 16 2. V 1/4" 2a 240 - 16 1/4" 1UM 900 - 35 1/4" 1UM 1050 - 35 C. 2.15 hrs. 1250 - 270°F. D. Chipping after first pass. Hand and automatic welding.	A. Yes B. None	1	1105	7/8" R	6" U	I II III V I II III V 572	13" Failed radiograph Excessive crossbar cracks 3/4" crack originates from blowhole in cross- bar
A. AD-283 B. 2/26/43 C. 10 D. Dominion Foundries & Steel Ltd. E. Haralshofeger Corp. Linde Air Products F. General Motors Div. of Canada	A. 1-1/2" B. R-V (.57Mn, .34Si, 2.25Cr, .72Ni, .28Mo) C. .28 D. --- E. Elec. F. 1650°F. 10 hrs. Air 1650°F. 6 hrs. Water 1150°F. 5 hrs. Air	A. A --- B. AW 3-A Oxweld #41 C. --- D. AC	A. DV B. 1/4" C. Flame Cutting Grinding	A. Copper back up bar B. 1. II 3/16" 1a 170 - 10 2. V 1/4" 2a 210 - 16 1/4" 1UM 950 - 35 1/4" 1UM 1000 - 35 C. 2.45 hrs. 1300 - 300°F. D. Chipping after first pass. Hand and automatic welding.	A. None B. None	1	1098		6" U	I	36" Failed radiograph Cracks at inter- section of legs & crossbar. 3/4" crack at right junction. Crater crack at left junction.





<p>IDENTIFICATION</p> <p>A. PART NUMBER OR B. PART OR TEST C. PLATE NO. D. DATE MANUFACTURED E. SUBSTRATE SPEC. F. ANVIL FABRICATOR</p>	<p>ANVIL DATA</p> <p>A. PLATE THICKNESS B. TYPE C. COMPOSITION D. SIZE E. PROCESS F. HEAT TREATMENT G. TENSILE YIELD</p>	<p>PLATE DATA</p> <p>A. TYPE B. TRADE NAME C. COATING D. COMPOSITION E. POLARITY</p>	<p>TEST METHODS</p> <p>A. COATING INSPECTION B. SURFACE C. PLATE PREPARATION</p>	<p>WELDING PROCEDURE</p> <p>A. BACKING B. DEPOSITION C. WELD TYPE D. WELD TYPE E. WELD TYPE F. TOTAL WELDING TIME G. WELDING TEMPERATURE</p>	<p>HEAT</p> <p>A. MAX B. POST</p>	<p>N. VIL. #</p>	<p>BALLISTIC RESULTS</p> <p>A. LOCATION OF H B. L.L. N.L. O.E. L</p>	<p>CRACKING</p> <p>A. CRACK TYPE B. AMT</p>	<p>REMARKS ON CRACKING</p> <p>A. REPAIRING RESULTS B. TEST</p>
<p>A. AD-287 B. 2/16/43 C. I.R.C. G3 D. Great Lakes Steel Corp. E. Crucible Steel F. Linde Air Products G. International Harvester Co.</p>	<p>A. 1-1/2" B. R-IV C. (.71Mn, .79Si, .56Cr, .16Mo, .082r) D. Face 269 Back 286 E. B.O.H. F. 1600<sup>hr</sup>. 2 hrs. Water G. 1240<sup>hr</sup>. 2 hrs. Air</p>	<p>A. A-II B. (.06C, 2.10 Mn, 19.16 Cr, 9.22Ni, 1.61Mo, .20V) C. (.25C, 3.90 Mn, .56Si, 7.5Cr, 9.10Mn, .25Mo) D. Oxweld E. Titanium F. DC REV</p>	<p>A. 450V B. 3/16" C. Flame Cutting Grinding</p>	<p>A. Copper back up B. 1. II 5/32" 1a 145 - 3/16" 1a 175 - 3/16" 2a 180 - 3/16" 2b 175 - 3/16" 2UM 760 - 31 C. 240 mins. 145° - 300° D. Grinding after first pass. Time 90 mins. Hand and automatic welding.</p>	<p>A. 175° B. None</p>	<p>1 1102</p>	<p>X</p>	<p>71<sup>D</sup> Imp III 36"</p>	<p>Passed radiograph 1/2" crack at left junction</p>

Weld Metal

GENERAL INFORMATION		ANNEAL DATA		ELECTRODE DATA		JOINT DESIGN		PROCEDURE		HEAT		RADIATION RESULTS		REMARKS ON CRACKING								
A. WORK ORDER NO.	B. DATE OF TEST	C. PLATE NO.	D. ANNEAL MANUFACTURER	E. ELECTRODE SPEC.	F. ANNEAL PARAMETERS	A. TYPE	B. TRADE NAME	C. COATING	D. CURRENT & POLARITY	A. SAW CUTTING	B. DEPOSITION SIZE EL. NO. TYPE AMR V	C. ROOT TYPE	D. GROOVE TYPE	E. TOTAL WELDING TIME & INTER PASS TEMPERATURE	A. PRE	B. POST	H	VEL. V/S	LOC. LOCATION OF H L.I. R.L. G.B.	CRACKING LAD. TYPE AMT	REMARKS ON CRACKING RADIOGRAPHIC RESULTS (RT)	
A. AD-126 B. 10/20/43 C. NYAB-10 D. Republic Steel Corp. E. Alley Nods Linde Air Products F. New York Air Brake Company	A. 1-1/2" B. R-V (.47Mn, .23Si, .22Cr, 4.05Ni, .39Mo) C. .28 D. --- E. B.Elec. F. ---	A. A B. --- C. Oxweld #42 D. --- E. AC	A. 450DV B. --- C. Flame Cutting	A. Not Given B. --- C. 160 - 25 1UM 900 - 32 1UM 1050 - 32 200°F. D. Plate 40"x36"x1-1/2" used. Also 4"x4"x1-1/2" tabs used at start of weld. Extra 4" of plate and tabs out off after welding.	A. 200° B. None F. C. None	1 1110 2 1151 3 1203 4 1229	1 1/2" R 5" D 5 1/2" U 7 1/2" U 1" D 1" U	III III III I II I II III III	1 1/2" R 5" D 5 1/2" U 7 1/2" U 1" D 1" U	1 1/2" R 5" D 5 1/2" U 7 1/2" U 1" D 1" U	1 1/2" R 5" D 5 1/2" U 7 1/2" U 1" D 1" U	1 1/2" R 5" D 5 1/2" U 7 1/2" U 1" D 1" U	1 1/2" R 5" D 5 1/2" U 7 1/2" U 1" D 1" U	1 1/2" R 5" D 5 1/2" U 7 1/2" U 1" D 1" U	1 1/2" R 5" D 5 1/2" U 7 1/2" U 1" D 1" U	1 1/2" R 5" D 5 1/2" U 7 1/2" U 1" D 1" U	1 1/2" R 5" D 5 1/2" U 7 1/2" U 1" D 1" U	1 1/2" R 5" D 5 1/2" U 7 1/2" U 1" D 1" U	1 1/2" R 5" D 5 1/2" U 7 1/2" U 1" D 1" U	1 1/2" R 5" D 5 1/2" U 7 1/2" U 1" D 1" U	1 1/2" R 5" D 5 1/2" U 7 1/2" U 1" D 1" U	Failed radiograph Cracks running through blowholes in crossbar. Several large gas pockets in lower right leg
A. AD-126 B. 10/29/43 C. NYAB-11 D. Republic Steel Corp. E. Alloy Nods Linde Air Products F. New York Air Brake Company	A. 1-1/2" B. R-V (.47Mn, .23Si, .22Cr, 4.05Ni, .39Mo) C. .28 D. --- E. B.Elec. F. ---	A. A B. --- C. Oxweld #42 D. --- E. AC	A. 450DV B. --- C. Flame Cutting	A. Not Given B. --- C. 160 - 28 2UM 850 - 32 150°F. D. Plate 40"x36"x1-1/2" used. Extra 4" of plate out off after welding.	A. 150° B. None F. C. None	1 1111 2 1145 3 1215	1 1/2" R 4" U 4 1/2" U	Imp II III II II II III	1 1/2" R 4" U 4 1/2" U	1 1/2" R 4" U 4 1/2" U	1 1/2" R 4" U 4 1/2" U	1 1/2" R 4" U 4 1/2" U	1 1/2" R 4" U 4 1/2" U	1 1/2" R 4" U 4 1/2" U	1 1/2" R 4" U 4 1/2" U	1 1/2" R 4" U 4 1/2" U	1 1/2" R 4" U 4 1/2" U	1 1/2" R 4" U 4 1/2" U	1 1/2" R 4" U 4 1/2" U	1 1/2" R 4" U 4 1/2" U	1 1/2" R 4" U 4 1/2" U	Failed radiograph Large amount of incomplete fusion. Large blowholes from which cracks originate.
A. AD-140 B. 12/5/42 C. NYAB-13 D. Jones & Laughlin E. Linde Air Products F. New York Air Brake Company	A. 1-1/2" B. R-III (.50Mn, .23Si, .41Mo) C. .25 D. --- E. B.O.H. F. ---	A. A B. --- C. Oxweld #42 D. --- E. AC	A. 450DV B. 1/4" C. Flame Cutting	A. None B. Special Unionmelt 1/4" 1UM 900 - 32 1/4" 1UM 1050 - 32 C. --- D. ---	A. None B. None	1 1096	1 1/2" R 5" D	Imp I	1 1/2" R 5" D	1 1/2" R 5" D	1 1/2" R 5" D	1 1/2" R 5" D	1 1/2" R 5" D	1 1/2" R 5" D	1 1/2" R 5" D	1 1/2" R 5" D	1 1/2" R 5" D	1 1/2" R 5" D	1 1/2" R 5" D	1 1/2" R 5" D	1 1/2" R 5" D	Failed radiograph 2-1/2" weld and plate crack and 1" plate cracks near right weld junction. Transverse cracks in left weld junction. 1-1/2" deep seated crack. Incomplete fusion in crossbar
A. AD-140 B. 12/5/42 C. NYAB-14 D. Jones & Laughlin E. McKay Company Linde Air Products F. New York Air Brake Company	A. 1-1/2" B. R-III (.50Mn, .23Si, .41Mo) C. .25 D. --- E. B.O.H. F. ---	A. A B. --- C. Oxweld #42 D. --- E. AC	A. 450DV B. 1/4" C. Flame Grinding	A. None B. First four passes hand welded, unionmelt was automatic	A. None B. None	1 1102	1 1/2" R 6" U	Imp I	1 1/2" R 6" U	1 1/2" R 6" U	1 1/2" R 6" U	1 1/2" R 6" U	1 1/2" R 6" U	1 1/2" R 6" U	1 1/2" R 6" U	1 1/2" R 6" U	1 1/2" R 6" U	1 1/2" R 6" U	1 1/2" R 6" U	1 1/2" R 6" U	1 1/2" R 6" U	Passed radiograph



IDENTIFICATION A. FROM RECORD NO. B. DATE OF TEST C. PLATE NO. D. ANNEAL MANUFACTURER E. ELECTRODE INFO. F. ANNEAL FABRICATOR	ANNEAL DATA A. PLATE THICKNESS B. TYPE C. GASKET CONTENT D. SHIM E. PROCESS F. HEAT TREATMENT G. TEST TIME CUSTOM	ELECTRODE DATA A. TYPE B. TRADE NAME C. COATING D. CURRENT & POLARITY	JOINT DESIGN A. GROOVE, INCLUDED ANGLE, ROOT FACE B. ROOT GAP C. PLATE PREPARATION	WELDING PROCEDURE A. BACKING B. DEPOSITION SEE EL. NO. TYPE AND V. 1. ROOT TYPE 2. BODY TYPE 3. GROUND TYPE C. TOTAL WELDING TIME & WATER PASS TEMPERATURE	HEAT A. PRE B. POST	BALLISTIC RESULTS		REMARKS ON CRACKING RADIOGRAPHIC RESULTS, ETC.
						H VEL. P/S	LOCATION OF H CRACKING L.L. R.L. G.B. LOC. TYPE AMT	
A. AD-159 B. 12/28/43 C. 27 D. Jones & Laughlin E. McKay Company F. Linde Air Products G. New York Air Brake Company	A. 1-1/2" B. R-III (1.50Mn, .23Si, .41Mo) C. .25 D. Face 286 E. Back 283 F. B.O.H. G. 1625°F. 2 1/2 hrs. Water 1080°F. 2 1/2 hrs. Air	A. A B. Oxweld #42 C. --- D. AC	A. 45°DV B. 1/4" C. Flame Cutting Grinding	A. None B. 1. II 3/16" 2a 200 - 25 2. V 1/4" 2a 330 - 28 1/4" 2UM 950 - 33 C. 12 hrs. 100° - 250°F. D. First four passes were hand welded, last two are automatic	A. None B. None	1090 2 1094	6" L 1 1/2" R 5 1/2" D 4 1/2" Imp U	Passed radiograph I 36"
A. AD-159 B. 12/28/43 C. 29 D. Jones & Laughlin E. McKay Company F. Linde Air Products G. New York Air Brake Company	A. 1-1/2" B. R-III (1.50Mn, .23Si, .41Mo) C. .25 D. Face 286 E. Back 275 F. B.O.H. G. 1625°F. 2 1/2 hrs. Water 1080°F. 2 1/2 hrs. Air	A. A B. Oxweld #42 C. --- D. AC	A. 45°DV B. 1/4" C. Flame Cutting Grinding	A. Not given B. 1. II 3/16" 2a 200 - 25 2. V 1/4" 2a 330 - 28 1/4" 2UM 950 - 33 C. 12 hrs. 100° - 250°F. D. First four passes were hand welded, other two are automatic	A. None B. None	1099 1 1099	6 3/8" O D Imp 1 1/2" R I 15" III 3" II 1 1/2" 29"	Passed radiograph I 10" II 15" III 3" II 1 1/2" 29"
A. AD-245 B. 2/9/43 C. 30-j-1 D. Jones & Laughlin E. Linde Air Products F. New York Air Brake Company	A. 1-1/2" B. R-III (1.50Mn, .23Si, .41Mo) C. .25 D. Face 302 E. Back 300 F. B.O.H. G. 1625°F. 2 1/2 hrs. Water 1080°F. 2 1/2 hrs. Air 1080°F. 3 hrs.	A. A B. Oxweld #42 C. --- D. AC	A. 90°DV B. 1/4" C. ---	A. Copper backing B. 1. II 3/16" 1a 175 - 25 3/16" 1a 180 - 26 2. V 3/16" 2a 180 - 26 3/16" 2UM 720 - 33 C. --- D. 2" long dam hand welded at ends to start and stop Unionmelt on. Hand wells were surface ground before the Unionmelt was applied. Plate was allowed to cool down between Unionmelt passes. Plate was ground after copper backing strip was removed to smooth up bottom.	A. 1500 F. Hand 200°F. Auto- B. None	1 1101	X 6" Imp D	Passed radiograph I 28" II 7 1/2" I 36" Crossbar only 9-1/2" long













PLATE NO.	DATE OF TEST	PLATE NO.	PLATE ORIENT	EXPOSURE DATA	EXPOSURE DATA	DEVELOPER	WELDS	PROCEDURE	MEAT	H	VEL. F/W	RADIATING RESULTS		REMARKS ON CRACKING									
												LOCATION OF R. L.L.	CRACKING										
A. TYPE	B. TYPE	C. TYPE	D. TYPE	E. TYPE	F. TYPE	G. TYPE	A. SAULTING	B. DEFLECTION	C. SIZE EL.	D. NO. TYPE	E. AMT V.	1. ROOT TYPE	2. CORNER TYPE	3. TOTAL WELDING TIME	4. ENTER PASS TEMPERATURE	5. A. None	6. B. None	7. A. None	8. B. None	9. A. None	10. B. None	11. A. None	12. B. None
AD-127	11/23/42	1-1/2"	C-II	(.10C Mn, .35Si, .37P, .40Mo)	26	Face 255 Back 258	E. B. Eleo.	1950°F. 7 hrs. Air 1650°F. 5 hrs. Water 1150°-1180°F. 6 hrs. Water	A. A-II (.10C, 3.95 Mn, .55Si, 20.10Cr, 10.20Ni) B. Armorloy C. Lime-Mn D. DC REV	GOODY 3/16" Flame Cutting Grinding Buttering	A. None B. I 3/16" 1a 160 - 22 III 3/16" 3a 160 - 22 1/4" 6b 195 - 24 III 3/16" 4b 160 - 22 1/4" 2b 195 - 24 C. 12.02 hrs. 70° - 1950°F. D. Grinding after all but first and last passes. Time 2.25 hrs. One more pass in crossbar	A. None B. None	1 950	4" U	Imp	I 3/16" II 3/16" V 3/16"	Passed radiograph Large amount of piping and porosity present in cast plate						
AD-120	12/12/42	1-1/2"	C-III	(.158Mn, .44Si, .42Mo)	.27	Face 212 Back 228	---	1825°F. 8 hrs. Air 1625°F. 3 hrs. Water 1200°F. 6 hrs. Water	A. A-II (.11C, 3.90 Mn, .55Si, 20.00Cr, 10.00Ni) B. Armorloy C. Lime-Mn D. AC	GOODY 1/4" Flame Cutting Grinding Buttering	A. None B. I 3/16" 1a 150 - 22 II 3/16" 1b 150 - 22 3/16" 1b 165 - 23 3/16" 1b 180 - 23 1/4" 1b 200 - 22 1/4" 1b 180 - 24 1/4" 1b 210 - 24 1/4" 1b 230 - 24 1/4" 9b 225 - 24 III 3/16" 4b 185 - 23 1/4" 2b 250 - 24 C. 22.21 hrs. 70° - 2120°F. D. Grinding after all but first two and last two passes. Time 2.05 hrs. Five less passes in crossbar.	A. 70°F. B. None	1 1072 2 1084 3 1169	1 1/2" R 7 1/2" U 5 1/2" D 2" L 4" U 16 1/2"	Imp U Imp D Imp U	II 4" V 6" II 2" V 4" V 16"	Passed radiograph						
AD-129	12/12/42	1-1/2"	C-I	(.79Mn, .38Si, .49Cr, .53Ni, .44Mo)	.35	Face 255 Back 235	ACID-O.H. 1550°F. 8 hrs. Water 1180°F. 10 hrs. Water	A. A-II (.11C, 3.90 Mn, .55Si, 20.00Cr, 10.00Ni) B. Armorloy C. Lime-Mn D. AC	GOODY 3/16" Flame Cutting Grinding Buttering	A. None B. I 3/16" 1a 180 - 22 1/4" 1a 190 - 23 1/4" 1a 260 - 25 1/4" 1a 270 - 26 1/4" 2a 280 - 28 1/4" 1a 285 - 28 1/4" 1a 250 - 25 C. 6 hrs. 70° - 212°F. D. Chipping in fourth pass. Time 2.15 hrs.	A. 70°F. B. None	1 1040 2 1038	2 1/8" R 7/8" R	7" U 8" D	I 1 1/2" II 6" V 10 1/2" I 4" II 3" V 16" 40"	Passed radiograph							

Weld Metal

IDENTIFICATION		SPECIFIC DATA		SAMPLING DATA		PREPARATION		EXAMINATION		RESULTS	
A. PART NO.	B. DATE OF TEST	C. PLATE NO.	D. MANUFACTURER	E. ELECTRODE SPEC.	F. WELDER	G. WELD TYPE	H. WELD POSITION	I. WELD SIZE	J. WELD TYPE	K. WELD POSITION	L. WELD TYPE
AD-120	12/13/42	33	Pratt & Letchworth Company	3/16"	3/16"	60°DV	3/16"	1066	1066	1066	1066
AD-246	2/8/43	34	Pratt & Letchworth Company	3/16"	3/16"	60°DV	3/16"	1153	1153	1153	1153

ANALYSIS		EXAMINATION		RESULTS	
A. TYPE	B. NAME	C. TYPE	D. NAME	E. TYPE	F. NAME
A. II	(.11C, 3.90 Mn, .55Si, 20.00Cr, 10.00Ni)	1066	1066	1066	1066
A. I	(.11C, 1.68 Mn, .65Si, 18.8Cr, 10.3Ni, 1.92Mo)	1153	1153	1153	1153

Weld Metal

IDENTIFICATION	ANODE DATA	ELECTRODE DATA	JOINT DESIGN	WELDING PROCEDURE	HEAT	H	VEL. F/S	BALLISTIC RESULTS		REMARKS OR GRADING	
								LOCATION OF H	GRADING		
A. PIANO NUMBER OR DATE OF TEST	A. PLATE THICKNESS	A. TYPE	A. GROOVE, INCLUDED ANGLE, ROOT FACE	A. SA ORING	A. FACE			L.I.	R.L.	LOC TYPE	
B. PLATE NO.	B. TYPE	B. TRADE NAME	B. ROOT GAP	B. DEPOSITION SIZE EL. NO. TYPE AMT V.	B. POOR						
C. ANODE MANUFACTURER	C. GASKET CONTENT	C. COATING	C. PLATE PREPARATION	C. ROOTY TYPE							
D. ELECTRODE INFO.	D. SIZE	D. CURRENT & POLARITY	D. PLATE PREPARATION	D. SMOOTH TYPE							
E. ANODE PREPARATION	E. PROCESS	E. POLARITY	E. PLATE PREPARATION	E. TOTAL WELDING TIME & WTER PASS TEMPERATURE							
F. WELD TREATMENT	F. WELD TREATMENT	F. WELD TREATMENT	F. WELD TREATMENT	F. REMARKS							
A. AE-246 B. 2/2/43 C. 36 D. Swingleton Gould Corp. Pratt & Lott D. Face 258 worth Company E. Back 255 E. Harnischfeger Corp. F. Federal Mach- ine & Welder Company	A. 1-1/2" B. C-II S.O.Co. (1.47Mn, .32Si, .43Cr, .35Mo) C. .30 D. Face 258 E. Back 255 F. 1850°F. 7 hrs. Air 1850°F. 5 hrs. Water 1180°F. 6 hrs. Water Z. C-III FEL.Co. (1.42Mn, .24Si, .31Mo) C. .27 D. Face 255 E. Back 255 F. B.O.H. 1725°F. 3 hrs. Air 1835°F. 3 hrs. Water 1050°F. 4 hrs. Air	A. A-I (.13C, 1.58 Mn, .64Si, 19.00Cr, 9.7Ni, 1.98Mo) B. Smoothhard C. AE-3 MO D. DC REV	A. GOOD B. 5/16" C. Flame Cutting Grinding	A. Not Given B. 1. I 5/32" 1a 116 - 18 5/32" 1a 116 - 18 5/32" 3a 120 - 20 3/16" 2a 170 - 24 3. I 3/16" 2a 170 - 24 C. 13.10 hrs. 750 - 1250F. D. Upper and lower center sections are Pratt & Letchworth; left and right sections are Swingleton Gould Corp. Chipping in all passes.	A. 70°F. B. None	1 2	11055 21065	2 1	5 U 1 R 4 D	I 11 V 18 I 5 V 14 40	11 Passed radiograph

Weld Metal





IDENTIFICATION A. PART NUMBER B. DATE OF TEST C. PLATE NO. D. ALLOY MANUFACTURER E. SURFACE AREA F. ANGLE OF ORIENTATION	ANVIL DATA A. TYPE B. CARBON CONTENT C. SIZE D. PROCESS E. RELAY TREATMENT F. TIME TIME CORRECT	BATHING MEDIA A. TYPE B. NAME C. CONCENTRATION D. POLARITY	TEST MEDIA A. CATHODE, MILLIGRAMS B. ANODE, MILLIGRAMS C. ROOT GAP D. PLATE PREPARATION	WELDER A. BACKING B. DEPOSITION SIZE EL. RA TYPE AMT V. C. ROOT TYPE D. ROOT TYPE E. ROOT TYPE F. TOTAL WELDING TIME & WELD PASS TEMPERATURE	SEAL A. FILL B. FLOW	R. V/L	SAMPLING OF W. L.		CRACKING LOC TYPE AMT	REMARKS OR COMMENTS DATE		
							LI	UL				
A. AD-99 B. 10/30/42 C. 74 D. American Steel Foundries E. Alloy Rods Co. F. Fisher Tank Division	A. 1-1/2" B. C-II (1.52Mn, .4781, .35Cr, .16Mo) C. .26 D. Face 197 E. --- F. ---	A. A-II (.08C, 3.60 Mn, .01981, 19.3Cr, 10.2Ni, .012Mo) B. Armorarc C. Titanium D. AC DC REV	A. 45°DV B. 5/16" C. Flame D. Cutting E. Grinding	A. Copper bar B. 1. II 3/16" 1a 185 - 22 1a 250 - 40 1a 350 - 40 2a 360 - 40 3. I 5/16" 3a 360 - 40 C. 2.13 hrs 250° - 420°F D. Grinding after fifth pass	A. 150° F	1	1111	2" R	5" U	II III	1 1	Passed radiograph
A. AD-224 B. 11/10/42 C. 75 D. American Steel Foundries E. Alloy Rods Co. F. Fisher Tank Division	A. 1-1/2" B. C-II (1.53Mn, .4881, .36Cr, .16Mo) C. .26 D. Face 197 E. --- F. ---	A. A-II (.08C, 3.60 Mn, .0381, 19.3Cr, 10.2Ni, .012Mo) B. Armorarc C. Titanium D. AC DC REV	A. 45°DV B. 5/16" C. Flame D. Cutting E. Grinding	A. Copper bar B. 1. II 3/16" 1a 185 - 22 1a 250 - 40 1a 350 - 40 2a 360 - 40 3. I 5/16" 3a 360 - 40 C. 2.14 hrs 180° - 420°F D.	A. 150° F	1	1101	2 1/2" R	6" U			Passed radiograph
A. AD-224 B. 11/10/42 C. 76 D. American Steel Foundries E. Alloy Rods Co. F. Fisher Tank Division	A. 1-1/2" B. C-II (1.52Mn, .4781, .35Cr, .16Mo) C. .29 D. Face 197 E. --- F. ---	A. A-II (.08C, 3.60 Mn, .01981, 19.3Cr, 10.2Ni, .012Mo) B. Armorarc C. Titanium D. AC DC REV	A. 45°DV B. 5/16" C. Flame D. Cutting E. Grinding	A. Copper bar B. 1. II 3/16" 1a 185 - 22 1a 250 - 40 1a 350 - 40 2a 360 - 40 3. I 5/16" 3a 360 - 40 C. 2.07 hrs 300° - 460°F D.	A. 150° F	1	1113	1" R	6" U	II III	4"	Failed radiograph 1-5/8" crack near right weld junction
A. AD-224 B. 11/16/42 C. 77 D. American Steel Foundries E. Alloy Rods Co. F. Fisher Tank Division	A. 1-1/2" B. C-II (1.52Mn, .4851, .36Cr, .16Mo) C. .26 D. Face 197 E. --- F. ---	A. A-II (.08C, 3.60 Mn, .0381, 19.3Cr, 10.2Ni, .012Mo) B. Armorarc C. Titanium D. AC DC REV	A. 45°DV B. 5/16" C. Flame D. Cutting E. Grinding	A. Copper bar B. 1. II 3/16" 1a 185 - 22 1a 250 - 40 1a 350 - 40 2a 360 - 40 3. I 5/16" 3a 360 - 40 C. 2.05 hrs 190° - 460°F D.	A. 150° F	1	1070	1 1/2" R	9" U			Passed radiograph

Weld Metal

A. TEST NUMBER B. DATE OF TEST C. PLATE NO. D. FABRICATOR E. ORDER NUMBER F. ORDER DATE	A. PLATE THICKNESS		A. TYPE		A. GRADE		A. GRADE		A. GRADE		A. GRADE		A. GRADE		A. GRADE		A. GRADE		A. GRADE	
	1	2	1	2	1	2	1	2	1	2	1	2	1	2	1	2	1	2	1	2
AD-224 11/10/42 American Steel Foundries Alloy Rods Co. Fisher Tank Division	1-1/2" C-11 (1.53Mn, .48S) .36Cr, .16Mo C. .26 D. Face 197 Back 197 E. --- F. ---	A. A-II (.08C, 3.60 Mn, .038S, 19.3Cr, .16Mo) 10.2Mn, .012Mo) B. Armorarc C. Titanium D. AC DC REV	A. 450DY B. 5/16" C. Flame Cutting Grinding	A. Copper bar 1. II 3/16" 1a 185 - 22 1a 250 - 40 2. I 1/4" 1a 250 - 40 4a 360 - 40 3. I 5/16" 2a 360 - 40 C. 2.10 hrs 200° - 530°F D.	A.150° F B. None	1 1115	1° R	4 1/2" D	0	III 10 1/2"	Passed radiograph 1-1/8" crack in crossbar									
AD-224 11/7/42 American Steel Foundries Alloy Rods Co. Fisher Tank Division	1-1/2" C-11 (1.53Mn, .48S) .36Cr, .16Mo C. .26 D. Face 197 Back 197 E. --- F. ---	A. A-II (.08C, 3.60 Mn, .038S, 19.3Cr, .16Mo) 10.2Mn, .012Mo) B. Armorarc C. Titanium D. AC DC REV	A. 450DY B. 5/16" C. Flame Cutting Grinding	A. Copper bar 1. II 3/16" 1a 185 - 22 1a 250 - 40 2. I 1/4" 1a 250 - 40 4a 360 - 40 3. I 5/16" 2a 360 - 40 C. 2.01 hrs 190° - 520°F D.	A.150° F B. None	1 1063 2 1083 3 1305 4 1257	2° L 1 1/2" R 1" R 1 1/2" R 5 1/2" U Imp I 3" II 3 1/2" III 5 1/2" V 9 1/2" 35	8° U 6 1/2" R 8 1/2" D 8 1/2" D 1 1/2" R 5 1/2" U	0	III 3 1/2"	Passed radiograph									
AD-216 1/27/43 American Steel Foundries Alloy Rods Co. Fisher Tank Division	1-1/2" C-11 (1.35Mn, .27Cr, .016Mo) C. .32 D. --- E. --- F. ---	A. A-II (.13C, 3.06 Mn, .038S, 18.99Cr, 8.29Mn, .109Mo) B. Armorarc C. Titanium D. AC DC REV	A. 450DY B. 5/16" C. Flame Cutting Grinding	A. Copper 1. II 3/16" 1a 185 - 22 1a 250 - 40 2. I 1/4" 1a 250 - 40 5/16" 3/16" 3. I 1/8" C. 1.50 hrs. 260° - 560°F D.	A. None B. None	1 1065 2 1194	7/8" R 1" R	6 1/2" U Imp 6 1/2" D Imp 0	0	I 10 1/2" I 14" II 9" V 7 1/2" I 4 1/2"	Passed radiograph									

Weld Metal





TEST NAME	PLATE NUMBER	MATERIAL	WELDING PROCEDURE	WELDING POSITION	WELDING SPEED	WELDING CURRENT	WELDING VOLTAGE	WELDING TIME	WELDING DEFECTS	WELDING DEFECTS	WELDING DEFECTS	WELDING DEFECTS	WELDING DEFECTS	WELDING DEFECTS		WELDING DEFECTS	WELDING DEFECTS	WELDING DEFECTS	
														WELDING DEFECTS	WELDING DEFECTS				
A. TEST NAME	B. PLATE NUMBER	C. MATERIAL	D. WELDING PROCEDURE	E. WELDING POSITION	F. WELDING SPEED	G. WELDING CURRENT	H. WELDING VOLTAGE	I. WELDING TIME	J. WELDING DEFECTS	K. WELDING DEFECTS	L. WELDING DEFECTS	M. WELDING DEFECTS	N. WELDING DEFECTS	O. WELDING DEFECTS	P. WELDING DEFECTS	Q. WELDING DEFECTS	R. WELDING DEFECTS	S. WELDING DEFECTS	
A. AD-275 B. 2/17/43 C. W-106 D. Ford Motor Co. Corp. E. Crucible Steel F. Ford Motor Co. Corp.	A. 1-1/2" B. C C. W-106 D. Ford Motor Co. Corp. E. Crucible Steel F. Ford Motor Co. Corp.	Basic-Elec. hrs. Air 1800 5 1700 3 hrs. Water 1100 8 hrs. Water	A. 45°DV B. 1/4" C. Flame Cutting	A. A B. --- C. --- D. AC REV	A. Copper strip B. --- C. --- D. Chipping in all passes	A. None B. None	1 1114 2 1220	1" R 6 1/4" D 6 1/4" U 1" L	I 12 III 2 V 5 I 11 II 4 V 18 43	Imp D Imp U	1" R 6 1/4" D 6 1/4" U 1" L	1 1114 2 1220	A. None B. None	1 1114 2 1220	1" R 6 1/4" D 6 1/4" U 1" L	I 12 III 2 V 5 I 11 II 4 V 18 43	Imp D Imp U	1" R 6 1/4" D 6 1/4" U 1" L	Passed radiograph
A/ AD-275 B. 2/17/43 C. W-107 D. Ford Motor Co. Corp. E. Crucible Steel F. Ford Motor Co. Corp.	A. 1-1/2" B. C C. W-107 D. Ford Motor Co. Corp. E. Crucible Steel F. Ford Motor Co. Corp.	Basic-Elec. hrs. Air 1800 5 1700 3 hrs. Water 1100 8 hrs. Water	A. 45°DV B. 1/4" C. Flame Cutting	A. A B. --- C. --- D. AC DC REV	A. Copper strip B. --- C. --- D. Chipping after all passes	A. None B. None	1 1091	1" L 5 1/4" D	I 12 II 2 V 15 30	Imp D	1" L 5 1/4" D	1 1091	A. None B. None	1 1091	1" L 5 1/4" D	I 12 II 2 V 15 30	Imp D	1" L 5 1/4" D	Passed radiograph
A. AD-275 B. 2/17/43 C. W-114 D. Ford Motor Co. Corp. E. Crucible Steel F. Ford Motor Co. Corp.	A. 1-1/2" B. C C. W-114 D. Ford Motor Co. Corp. E. Crucible Steel F. Ford Motor Co. Corp.	Basic-Elec. hrs. Air 1800 5 1700 3 hrs. Water 1100 8 hrs. Water	A. 45°DV B. 1/4" C. Flame Cutting	A. A B. --- C. --- D. DC REV	A. Copper strip B. --- C. --- D. Chipping after all passes	A. None B. None	1 1139 2 1263	1" L 5 1/4" D 5 1/4" X	I 13 II 7 V 14 35	Imp D	1" L 5 1/4" D 5 1/4" X	1 1139 2 1263	A. None B. None	1 1139 2 1263	1" L 5 1/4" D 5 1/4" X	I 13 II 7 V 14 35	Imp D	1" L 5 1/4" D 5 1/4" X	Passed radiograph

TESTING DATA	PLATE DATA	WELD DATA	WELDING DATA	WELDING PROCEDURE	WELDING RESULTS	TESTING DATA	PLATE DATA	WELD DATA	WELDING DATA	WELDING PROCEDURE	WELDING RESULTS	TESTING DATA
A. PART NO.	B. DATE OF TEST	C. PLATE NO.	D. PLATE MANUFACTURER	E. PLATE TYPE	F. PLATE THICKNESS	G. WELD TYPE	H. WELD POSITION	I. WELDING METHOD	J. WELDING PARAMETERS	K. WELDING RESULTS	L. WELDING DEFECTS	M. WELDING COMMENTS
A. AD-131 B. 12/3/43 C. H-C-16 D. Wehr Steel Co. E. A. O. Smith Corp. F. The Heli Co.	A. 1-1/2" B. 3-I (.060in., 46517 .04Cr., 055Mn .45Mo) C. .33 D. Face 255 Back 255 E. --- F. ---	A. A-I (.08C 3.5 Mn., 3581, 19, Cr. 10, Ni, 1. Mo) B. S.W. 164 C. Lime D. DC REV	A. GOOD B. 3/16" C. Machining	A. Not Given B. 1. I 3/16" 2. III 3/16" 3. III 1/4" C. 21 hrs D.	A. 1200 B. None C. 1039 D. 1040 E. 1046	A. 3 1/2" B. 4 1/2" C. 4 1/2" D. 4 1/2"	A. II B. III C. V D. I E. III F. V G. III H. V I. III J. V K. III L. V M. III N. V O. III P. V Q. III R. V S. III T. V U. III V. V W. III X. V Y. III Z. V AA. III AB. V AC. III AD. V AE. III AF. V AG. III AH. V AI. III AJ. V AK. III AL. V AM. III AN. V AO. III AP. V AQ. III AR. V AS. III AT. V AU. III AV. V AW. III AX. V AY. III AZ. V BA. III BB. V BC. III BD. V BE. III BF. V BG. III BH. V BI. III BJ. V BK. III BL. V BM. III BN. V BO. III BP. V BQ. III BR. V BS. III BT. V BU. III BV. V BW. III BX. V BY. III BZ. V CA. III CB. V CC. III CD. V CE. III CF. V CG. III CH. V CI. III CJ. V CK. III CL. V CM. III CN. V CO. III CP. V CQ. III CR. V CS. III CT. V CU. III CV. V CW. III CX. V CY. III CZ. V DA. III DB. V DC. III DD. V DE. III DF. V DG. III DH. V DI. III DJ. V DK. III DL. V DM. III DN. V DO. III DP. V DQ. III DR. V DS. III DT. V DU. III DV. V DW. III DX. V DY. III DZ. V EA. III EB. V EC. III ED. V EE. III EF. V EG. III EH. V EI. III EJ. V EK. III EL. V EM. III EN. V EO. III EP. V EQ. III ER. V ES. III ET. V EU. III EV. V EW. III EX. V EY. III EZ. V FA. III FB. V FC. III FD. V FE. III FF. V FG. III FH. V FI. III FJ. V FK. III FL. V FM. III FN. V FO. III FP. V FQ. III FR. V FS. III FT. V FU. III FV. V FW. III FX. V FY. III FZ. V GA. III GB. V GC. III GD. V GE. III GF. V GG. III GH. V GI. III GJ. V GK. III GL. V GM. III GN. V GO. III GP. V GQ. III GR. V GS. III GT. V GU. III GV. V GW. III GX. V GY. III GZ. V HA. III HB. V HC. III HD. V HE. III HF. V HG. III HH. V HI. III HJ. V HK. III HL. V HM. III HN. V HO. III HP. V HQ. III HR. V HS. III HT. V HU. III HV. V HW. III HX. V HY. III HZ. V IA. III IB. V IC. III ID. V IE. III IF. V IG. III IH. V II. III IJ. V IK. III IL. V IM. III IN. V IO. III IP. V IQ. III IR. V IS. III IT. V IU. III IV. V IW. III IX. V IY. III IZ. V JA. III JB. V JC. III JD. V JE. III JF. V JG. III JH. V JI. III JJ. V JK. III JL. V JM. III JN. V JO. III JP. V JQ. III JR. V JS. III JT. V JU. III JV. V JW. III JX. V JY. III JZ. V KA. III KB. V KC. III KD. V KE. III KF. V KG. III KH. V KI. III KJ. V KK. III KL. V KM. III KN. V KO. III KP. V KQ. III KR. V KS. III KT. V KU. III KV. V KW. III KX. V KY. III KZ. V LA. III LB. V LC. III LD. V LE. III LF. V LG. III LH. V LI. III LJ. V LK. III LL. V LM. III LN. V LO. III LP. V LQ. III LR. V LS. III LT. V LU. III LV. V LW. III LX. V LY. III LZ. V MA. III MB. V MC. III MD. V ME. III MF. V MG. III MH. V MI. III MJ. V MK. III ML. V MM. III MN. V MO. III MP. V MQ. III MR. V MS. III MT. V MU. III MV. V MW. III MX. V MY. III MZ. V NA. III NB. V NC. III ND. V NE. III NF. V NG. III NH. V NI. III NJ. V NK. III NL. V NM. III NN. V NO. III NP. V NQ. III NR. V NS. III NT. V NU. III NV. V NW. III NX. V NY. III NZ. V OA. III OB. V OC. III OD. V OE. III OF. V OG. III OH. V OI. III OJ. V OK. III OL. V OM. III ON. V OO. III OP. V OQ. III OR. V OS. III OT. V OU. III OV. V OW. III OX. V OY. III OZ. V PA. III PB. V PC. III PD. V PE. III PF. V PG. III PH. V PI. III PJ. V PK. III PL. V PM. III PN. V PO. III PP. V PQ. III PR. V PS. III PT. V PU. III PV. V PW. III PX. V PY. III PZ. V QA. III QB. V QC. III QD. V QE. III QF. V QG. III QH. V QI. III QJ. V QK. III QL. V QM. III QN. V QO. III QP. V QQ. III QR. V QS. III QT. V QU. III QV. V QW. III QX. V QY. III QZ. V RA. III RB. V RC. III RD. V RE. III RF. V RG. III RH. V RI. III RJ. V RK. III RL. V RM. III RN. V RO. III RP. V RQ. III RR. V RS. III RT. V RU. III RV. V RW. III RX. V RY. III RZ. V SA. III SB. V SC. III SD. V SE. III SF. V SG. III SH. V SI. III SJ. V SK. III SL. V SM. III SN. V SO. III SP. V SQ. III SR. V SS. III ST. V SU. III SV. V SW. III SX. V SY. III SZ. V TA. III TB. V TC. III TD. V TE. III TF. V TG. III TH. V TI. III TJ. V TK. III TL. V TM. III TN. V TO. III TP. V TQ. III TR. V TS. III TT. V TU. III TV. V TW. III TX. V TY. III TZ. V UA. III UB. V UC. III UD. V UE. III UF. V UG. III UH. V UI. III UJ. V UK. III UL. V UM. III UN. V UO. III UP. V UQ. III UR. V US. III UT. V UU. III UV. V UW. III UX. V UY. III UZ. V VA. III VB. V VC. III VD. V VE. III VF. V VG. III VH. V VI. III VJ. V VK. III VL. V VM. III VN. V VO. III VP. V VQ. III VR. V VS. III VT. V VU. III VV. V VW. III VX. V VY. III VZ. V WA. III WB. V WC. III WD. V WE. III WF. V WG. III WH. V WI. III WJ. V WK. III WL. V WM. III WN. V WO. III WP. V WQ. III WR. V WS. III WT. V WU. III WV. V WW. III WX. V WY. III WZ. V XA. III XB. V XC. III XD. V XE. III XF. V XG. III XH. V XI. III XJ. V XK. III XL. V XM. III XN. V XO. III XP. V XQ. III XR. V XS. III XT. V XU. III XV. V XW. III XX. V XY. III XZ. V YA. III YB. V YC. III YD. V YE. III YF. V YG. III YH. V YI. III YJ. V YK. III YL. V YM. III YN. V YO. III YP. V YQ. III YR. V YS. III YT. V YU. III YV. V YW. III YX. V YY. III YZ. V ZA. III ZB. V ZC. III ZD. V ZE. III ZF. V ZG. III ZH. V ZI. III ZJ. V ZK. III ZL. V ZM. III ZN. V ZO. III ZP. V ZQ. III ZR. V ZS. III ZT. V ZU. III ZV. V ZW. III ZX. V ZY. III ZZ. V					

A. NAME OF TEST	B. DATE TEST MADE	C. TYPE OF TEST	D. TEST PROCEDURE	E. TEST RESULTS	F. TESTER'S NAME	G. TESTER'S ADDRESS	H. TESTER'S PHONE	I. TESTER'S CITY	
<p>A. AD-269 B. 2/15/43 C. I.H.C. 45 D. Ord. Steel Fdry. E. McKay Company F. International Harvester Co.</p>	<p>A. 1-1/2" B. C-III (1.55% Mn, .44Si, .42Mo) C. .28 D. Face --- Back 267 E. B.O.H. F. 1750F. 2 1/2 hrs. Air 1575F. 1 1/2 hrs. Water 1125F. 4 hrs. Air</p>	<p>A. A-II (.12C, 4.0 Mn, .80Si, 20.0Cr, 9.7Ni) B. Armorloy C. Lime D. DC REV</p>	<p>A. 450DY B. 5/16" C. Flame Cutting Grinding</p>	<p>A. Copper back up bar B. 1. II 5/32" 1a 140 - 3/16" 1a 180 - 2. III 1/4" 2a 260 - 4b 250 - 3. III 5/32" 4b 140 - 1/4" 2b 260 - C. 3.50 hrs. 140° - 330° F. D. Cracking in first pass, ground out</p>	<p>A.100° F B. None</p>	<p>1 1104 2 1143 3 1214</p>	<p>6 1/2" U 5/8" R 6" L 5 1/2" R 5 1/2" U 3" L</p>	<p>II Imp I 2" II 6" III 3" V 13"</p>	<p>Passed radiograph</p>
<p>A. AD-269 B. 2/15/43 C. I.H.C. 46 D. Ord. Steel E. McKay Company F. International Harvester Co.</p>	<p>A. 1-1/2" B. C-III (1.55% Mn, .44Si, .42Mo) C. .28 D. Face 245 Back 359 E. B.O.H. F. 1750F. 2 1/2 hrs. Air 1575F. 1 1/2 hrs. Water 1125F. 4 hrs. Air</p>	<p>A. A-II (.12C, 4.0 Mn, .80Si, 20.0Cr, 9.7Ni) B. Armorloy C. Lime D. DC REV</p>	<p>A. 450DY B. 5/16" C. Flame Cutting Grinding</p>	<p>A. Copper back up bar B. 1. II 5/32" 1a 140 - 3/16" 1a 180 - 2. III 1/4" 2a 260 - 4b 250 - 3. III 5/32" 4b 140 - 1/4" 2b 260 - C. 3.5 hrs. 150° - 330° F. D.</p>	<p>A.100° F B. None</p>	<p>1 1144 2 1236 3 1233</p>	<p>4 1/2" U 7 1/2" R 7 1/2" D 5/8" L 7" D</p>	<p>III Imp I 3" II 5" V 2 1/2" I 1 1/2" I 13"</p>	<p>Passed radiograph</p>
<p>A. AD-269 B. 2/15/43 C. I.H.C. 50 D. Ord. Steel E. McKay Company F. International Harvester Co.</p>	<p>A. 1-1/2" B. C-III (1.55% Mn, .44Si, .42Mo) C. .28 D. Face 268 Back 375 E. B.O.H. F. 1750F. 2 1/2 hrs. Air 1575F. 1 1/2 hrs. Water 1125F. 4 hrs. Air</p>	<p>A. A-II (.12C, 4.0 Mn, .80Si, 20.0Cr, 9.7Ni) B. Armorloy C. Lime D. DC REV</p>	<p>A. 450DY B. 5/16" C. Flame Cutting Grinding</p>	<p>A. Copper back up bar B. 1. II 5/32" 1a 140 - 3/16" 1a 180 - 2. III 1/4" 3a 260 - 4b 250 - 3. III 5/32" 4b 140 - 1/4" 2b 260 - C. 3.49 hrs. 140° - 330° F. D. Grinding after first pass</p>	<p>A.100° F B. None</p>	<p>1 1132 2 1168</p>	<p>6 1/2" D 7/8" R 5 1/2" U</p>	<p>II V 1 1/2" I 4 1/2" II 36" V 45"</p>	<p>Passed radiograph</p>





A. PART NUMBER B. DATE OF TEST C. PLATE NO. D. ORDER NUMBER E. DRAWING NO. F. GROUP NUMBER	A. PLATE NUMBER B. TYPE C. ORDER NUMBER D. SIZE E. PROCESS F. TEST TEMPERATURE G. TEST CODE	A. WIRE B. WIRE SIZE C. COATING D. CURRENT E. POLARITY	A. PREP. METHOD B. SIZE C. PLATE NUMBER	A. BACKING STRIP B. TYPE C. SIZE D. TEMPERATURE	A. NONE B. NONE	A. NONE B. NONE	A. NONE B. NONE	A. PART NUMBER B. DATE OF TEST C. PLATE NO. D. ORDER NUMBER E. DRAWING NO. F. GROUP NUMBER
A. AD-263 B. 2/16/43 C. G-5501-2-1 D. Pittsburgh Steel Fdry. E. Lincoln Elec. Co. F. Lima Locomotive Tank Arsenal	A. 1-1/2" B. C-I C. (.03Mn, .40Si, .53Cr, .50Ni, .48Mo) D. Face 269 hrs. Air 1200°F. 6 hrs. Furnace 1600°F. 6 hrs. Water 1150°F. 6 hrs. in Furnace to 700°F. in air	A. A- B. Armoweld C. --- D. DC REV	A. 60°DV B. 3/16" C. Machining	A. 1/4" backing strip See 1015 B. 1. II 5/32" 2a 170 - 30 2. II 5/32" 4b 170 - 30 3/16" 4b 250 - 30 1/4" 4b 270 - 30 3. III 5/16" 6b 300 - 30 C. 9 hrs. D. Backing removed after first bead.	A. None B. None	1 1055	I 23" II 30" 23"	A. AD-263 B. 2/16/43 C. 7-5501-3-1 D. Pittsburgh Steel Fdry. E. Arcon Corp. F. Lima Locomotive Tank Arsenal
A. AD-263 B. 2/16/43 C. 7-5501-3-1 D. Pittsburgh Steel Fdry. E. Arcon Corp. F. Lima Locomotive Tank Arsenal	A. 1-1/2" B. C-I C. (.03Mn, .40Si, .53Cr, .50Ni, .48Mo) D. Face 269 hrs. Air 1200°F. 6 hrs. Furnace 1600°F. 6 hrs. Water 1150°F. 6 hrs. in Furnace to 700°F. in air	A. A-I (.10C, 3.27 Mn, .32Si, 18.50Cr, 10.25Ni, .97Mo) B. Chromang C. Lime D. DC REV	A. 60°DV B. 3/16" C. Machining	A. 1/4" Mild Steel SAE 1015 B. 1. II 5/32" 1a 170 - 30 5/32" 1a 175 - 30 2. II 5/32" 4b 170 - 30 3. III 1/4" 6b 200 - 30 C. 9 hrs. D. Backing removed after first pass.	A. None B. None	1 1091 2 1219	I 2" II 7" III 4" I 18" II 17" V 8" 57"	A. AD-263 B. 2/16/43 C. 7-5501-3-1 D. Pittsburgh Steel Fdry. E. Arcon Corp. F. Lima Locomotive Tank Arsenal

A. TEST B. DATE OF TEST C. NAME OF OPERATOR D. NAME OF WORKSHOP E. NAME OF WORKER F. NAME OF PLANT	A. TYPE OF TEST B. CURRENT C. SIZE D. PROCESS E. MOUNTING METHOD F. MOUNTING MATERIAL	A. TYPE OF WELD B. WELDING MACHINE C. WELDING POLARITY	A. COATING B. SURFACE PREPARATION C. PLATE PREPARATION	A. BACKING B. DEPOSITION RATE C. DEPOSITION TYPE D. COATING TYPE E. TOTAL WELDING TIME & ENTER PASS TEMPERATURE	A. NONE B. NONE	A. NONE B. NONE	A. NONE B. NONE	A. NONE B. NONE	
A. AD-327 B. 3/15/43 C. 8-5501-2-1 D. Pittsburgh Steel Fdry. E. Lincoln Elec. Co. F. Lima Locomotive Tank Arsenal	A. 1-1/2" B. C-I (1.03Mn, .40Si, .53Cr, .50Ni, .48Mo) C. .30 D. Face 269 Back 277 E. B.O.H. F. 1850 F. 6 hrs. Air 1200 F. 6 hrs. Furnace 1600 F. 6 hrs. Water 1150 F. 8 hrs. Furnace to 700 F. Air	A. A --- B. Armoweld C. Lime D. DC REV	A. 600V B. 1/4" C. Machining	A. 3/8" Backing strip SAE 1015 B. 1. II 5/32" 2b 160 - 30 2. II 5/32" 2b 175 - 30 3. II 3/16" 4b 210 - 30 4. II 5/16" 4b 250 - 30 5. II 5/16" 4b 290 - 30 C. 9 hrs. D. 70° - 210°F.	A. None B. None	1 LO43 2 1101	7 1/2" Imp D 1 1/4" R 7 1/4" U Imp	I II II II III V 3 1/2 6 1/2 1 1/2 4 5 1/2 5 1/2 3 1/2	Passed radiograph 6 1/2 lg. amount of shrinkage in plates



A. PART NUMBER	B. PART NAME	C. PART SPECIFICATION	D. PART MATERIAL	E. PART WEIGHT	F. PART DIMENSIONS	G. PART FINISH	H. PART TOLERANCES	I. PART COMMENTS
A. AD-160 B. 1/1/43 C. 10 D. Pacific Car & Fdry. Co. E. McKay Company F. Pacific Car & Fdry. Co.	A. 1-1/2" B. C-III (1.00Mn, .64Si, .42Mo) C. .21 D. Face 207 E. Back 212 F. Basis Elec, 1850 F. 6 hrs. Air 1635 F. .3 hrs. Water 1200 F. .4 hrs. Air	A. A-I (.10C, 4.50 Mn, 18.5Cr, 9.9Ni, .40Mo) B. Armorloy C. A-5 D. DC REV	A. 300 DV B. 3/16" C. Machining	A. None B. 1. II 5/32" 1a 130 - 18 5/32" 1a 145 - 22 2. I 3/16" 6a 180 - 28 3. III 5/32" 4b 145 - 22 3/16" 2b 180 - 28 C. 9:10 hrs. D. 200° - 300°F.	A. None B. 11091 C. 1113 D. 1"	X	62" D 4" U	Failed radiograph 20" incomplete 64" fusion in left leg 14" incomplete 47" fusion in right 54" leg
A. AD-160 B. 1/1/43 C. 13 D. Pacific Car & Fdry. Co. E. McKay Company F. Pacific Car & Fdry. Co.	A. 1-1/2" B. C-III (1.10Mn, .66Si, .47Mo) C. .21 D. Face 197 E. Back 201 F. Basis Elec, 1850 F. 6 hrs. Air 1635 F. .3 hrs. Water 1300 F. .4 hrs. Air	A. A-I (.10C, 4.50 Mn, 18.5Cr, 8.9Ni, .40) B. Armorloy C. Lime D. DC REV	A. 300 DV B. 3/16" C. Machining	A. Mc=2 B. 1. II 5/32" 1a 130 - 18 5/32" 1a 145 - 22 2. I 3/16" 6a 180 - 28 3. III 5/32" 4b 145 - 22 3/16" 2b 180 - 28 C. 9:40 hrs. D. 200° - 300°F.	A. None B. 1034 C. 14" D. R	8" D	Imp	Failed radiograph 34" incomplete 34" fusion in left leg 40" fusion in right 47" leg Some piping in cast plate

Weld Metal

A. FOUNDRY NO. B. DATE OF TEST C. PLATE NO. D. ORDER NUMBER E. SUBJECTS SPEC. F. ANALYST	A. TYPE B. YIELD STRENGTH C. TENSILE STRENGTH D. ELONGATION E. REDUCTION OF AREA F. HARDNESS	A. TYPE B. YIELD STRENGTH C. TENSILE STRENGTH D. ELONGATION E. REDUCTION OF AREA F. HARDNESS	A. TYPE B. YIELD STRENGTH C. TENSILE STRENGTH D. ELONGATION E. REDUCTION OF AREA F. HARDNESS	A. TYPE B. YIELD STRENGTH C. TENSILE STRENGTH D. ELONGATION E. REDUCTION OF AREA F. HARDNESS	A. TYPE B. YIELD STRENGTH C. TENSILE STRENGTH D. ELONGATION E. REDUCTION OF AREA F. HARDNESS	A. TYPE B. YIELD STRENGTH C. TENSILE STRENGTH D. ELONGATION E. REDUCTION OF AREA F. HARDNESS	A. TYPE B. YIELD STRENGTH C. TENSILE STRENGTH D. ELONGATION E. REDUCTION OF AREA F. HARDNESS	A. TYPE B. YIELD STRENGTH C. TENSILE STRENGTH D. ELONGATION E. REDUCTION OF AREA F. HARDNESS	
<p>A. AD-236 B. 2/11/43 C. M-29 D. Union Steel Casting Co. E. McKay Company F. Pressed Steel Car Company</p>	<p>A. 1-1/2" B. C-III (1.46Mn, .4281, .55Mo) C. .30 D. Face 265 Back 265 E. --- F. ---</p>	<p>A. A (.12C, .200 Mn, .5081, 18.7-28.5 Cr, 9.5-10.7Ni, 1.5-2.85 Mo) B. A-6 C. Slag D. AC STR</p>	<p>A. DV B. --- C. ---</p>	<p>A. Not given B. 1. II 3/16" 1a 170 - 290 - 3. III 5/16" 5a 290 - 5/16" 2b 390 - 3. II 5/16" 2b 300 - 4b 290 - C. 22 hrs. remainder not given D. Grinding after 1st, 2nd, 6th, 9th and 15th passes One less pass in right leg</p>	<p>A. 70°F B. None</p>	<p>2 1/2" L 1049 3 1052 1 1/2" R 3 1048 1 1/2" L</p>	<p>4 1/2" U 6" Imp 4 1/2" U</p>	<p>V III V II 22 1/2"</p>	<p>Passed radiograph Large amount of shrinkage around right weld junction</p>
<p>A. AD-271 B. 2/19/43 C. M-32 D. Union Steel Casting Co. E. Crucible Steel F. Pressed Steel Car Company</p>	<p>A. 1-1/2" B. C-III (1.59Mn, .34 Si, .55Mo) C. .28 D. Face 267 Back 257 E. --- F. ---</p>	<p>A. A (.12C, .75 Si, 1.60-2.0Mn, 20.5-23.5 Cr, 9.5-11.0Ni) B. Reziitol C. Slag D. DC REV</p>	<p>A. DV B. --- C. Flame Cutting Grinding</p>	<p>A. Not given B. 1. II 5/32" 2a 160 - 25 3. II 5/32" 4b 160 - 25 3/16" 10b 190 - 25 remainder not given C. 28 hrs. 150° - 300°F. D. Cracking after first pass Grinding after first, fourth and eight passes Three more passes in right leg and five more in crossbar</p>	<p>A. 70°F B. None</p>	<p>3" L 1113</p>	<p>7" D</p>	<p>I II III V</p>	<p>Failed radiograph Two 1-1/2" weld cracks, one 1-1/2" weld crack Shrinkage cracks in upper left leg plate</p>
<p>A. AD-271 B. 2/19/43 C. M-34 D. Union Steel Casting Co. E. Crucible Steel F. Pressed Steel Car Company</p>	<p>A. 1-1/2" B. C-III 1057-A (1.52Mn, .38Si, .53Mo) C-III 93-B (1.60Mn, .36Si, .54Mo) C-III 1066-A (1.55Mn, .35Si, .55Mo) C. .30 .27 .31 D. Face 285 Back 285 Face 227 Back 220 Face 285 Back 285 E. --- F. ---</p>	<p>A. A (.12C, .75Si, 1.60-2.0Mn, 20.5-23.5 Cr, 9.5-11.0Ni) B. Reziitol C. Slag D. DC REV</p>	<p>A. DV B. --- C. Flame Cutting Grinding</p>	<p>A. Not given B. 1. II 5/32" 1a 120 - 25 5/32" 1a 130 - 25 5/32" 2a 130 - 25 5/32" 2a 130 - 25 3/16" 2a 150 - 25 5/32" 1a 130 - 25 3/16" 2a 150 - 25 C. 22 hrs. 150° - 300°F. D. Grinding after 1st, 4th, 5th, and ninth passes. Three less passes in crossbar. Left leg of 1057-A, right leg of 93-B, upper center section and lower center section of 1066-A</p>	<p>A. 70°F B. None</p>	<p>1 1/2" L 1104</p>	<p>8" D 7 1/2" U</p>	<p>I II V I II V 68</p>	<p>Welds acceptable Plats is unsound Shrinkage cracks, gas pockets and inclusions in plates adjacent to weld deposits</p>



SPECIFICATIONS	MATERIALS	PLATE THICKNESS	WELDING PROCEDURE	WELDING PROCEDURE	WELDING PROCEDURE	WELDING PROCEDURE	WELDING PROCEDURE	WELDING PROCEDURE	WELDING PROCEDURE	WELDING PROCEDURE	WELDING PROCEDURE	WELDING PROCEDURE	WELDING PROCEDURE		REMARKS ON CORROSION	
													WELDING PROCEDURE	WELDING PROCEDURE		
A. NAME AND NO. OF TEST B. PLATE NO. C. MANUFACTURER D. GRADE E. TENSILE STRENGTH F. YIELD POINT	A. TYPE B. GRADE C. TENSILE STRENGTH D. YIELD POINT E. ELONGATION F. REDUCTION OF AREA	A. TYPE B. GRADE C. TENSILE STRENGTH D. YIELD POINT E. ELONGATION F. REDUCTION OF AREA	A. TYPE B. GRADE C. TENSILE STRENGTH D. YIELD POINT E. ELONGATION F. REDUCTION OF AREA	A. TYPE B. GRADE C. TENSILE STRENGTH D. YIELD POINT E. ELONGATION F. REDUCTION OF AREA	A. TYPE B. GRADE C. TENSILE STRENGTH D. YIELD POINT E. ELONGATION F. REDUCTION OF AREA	A. TYPE B. GRADE C. TENSILE STRENGTH D. YIELD POINT E. ELONGATION F. REDUCTION OF AREA	A. TYPE B. GRADE C. TENSILE STRENGTH D. YIELD POINT E. ELONGATION F. REDUCTION OF AREA	A. TYPE B. GRADE C. TENSILE STRENGTH D. YIELD POINT E. ELONGATION F. REDUCTION OF AREA	A. TYPE B. GRADE C. TENSILE STRENGTH D. YIELD POINT E. ELONGATION F. REDUCTION OF AREA	A. TYPE B. GRADE C. TENSILE STRENGTH D. YIELD POINT E. ELONGATION F. REDUCTION OF AREA	A. TYPE B. GRADE C. TENSILE STRENGTH D. YIELD POINT E. ELONGATION F. REDUCTION OF AREA	A. TYPE B. GRADE C. TENSILE STRENGTH D. YIELD POINT E. ELONGATION F. REDUCTION OF AREA	A. TYPE B. GRADE C. TENSILE STRENGTH D. YIELD POINT E. ELONGATION F. REDUCTION OF AREA	A. TYPE B. GRADE C. TENSILE STRENGTH D. YIELD POINT E. ELONGATION F. REDUCTION OF AREA	A. TYPE B. GRADE C. TENSILE STRENGTH D. YIELD POINT E. ELONGATION F. REDUCTION OF AREA	A. TYPE B. GRADE C. TENSILE STRENGTH D. YIELD POINT E. ELONGATION F. REDUCTION OF AREA
A. AD-244 B. 2/11/43 C. MGH-57 D. Stryer Steel Casting Co. E. Metal & Thermit Corp. F. Pullman Standard Car Mfg. Co.	A. 1-1/2" B. C-I (.86Mn, .43Si, .44Cr, .46Mn, .46Mn) C. .30 D. Face 235 Back 235 E. Acid-Elec. F. ---	A. A- B. Murex C. --- D. DC REV	A. 45° DV B. 3/8" C. Flame Cutting Grinding	A. Copper backing B. 1. II 1/4" 1a 250 - 28 5/16" 1a 280 - 32 2. I 5/16" 6a 280 - 32 3. III 5/16" 6b 280 - 32 C. 8 hrs. 225° - 320° D. Cracking after second pass. Chipping after all passes.	A. None B. None	1 1107 2 1161	X 3 3/4" D 6" U	II III II V	1" 2" 2 1/2" 5"	Passed radiograph						

RESTRICTED

TITLE: Welding of Armor

ATI- 38861

AUTHOR(S): Turkalo, Anna M.; Herres, S. A.  
 ORIGINATING AGENCY: Watertown Arsenal, Watertown, Mass.  
 PUBLISHED BY: (Same)

DIVISION

(None)

ORIG. AGENCY CO.

R-640/84

PUBLISHED AGENCY CO.

(Same)

DATE	COE. CLAS.	COUNTRY	LANGUAGE	PAGE	DESCRIPTION
Aug '43	Restr.	U. S.	Eng.	115	tables, diagrs

## ABSTRACT:

Some 172 firing record data for 1 1/2 in. homogeneous armor "H" plates, welded with austenitic electrodes, are tabulated, and a comparison is made of the ballistic shock performance of plates manufactured with various materials and welding procedures. Within the range of chemical composition of commercial rolled homogeneous armor, steel quality was indicated as having more effect on ballistic performance of hand welded plates than variations in chemical analysis. Of 28 Unimelt welded plates, only two were comparable in ballistic performance to satisfactory hand-welded plates. Cast assemblies showed a higher proportion of cracking in the unaffected plate than in the weld, fusion, and heat-affected zones. It was found that the ratio of plate to weld cracking decreases with increase in hardenability and with improvement in radiographic soundness of cast armor.

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DIVISION: Ordnance and Armament (22)  
 SECTION: Armor (5)

SUBJECT HEADINGS: Armor plate - Welding (11532); Armor plate, Welded - Stresses (11530)

ATI SHEET NO.: R-22-5-23

Air Documents Division, Intelligence Department  
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