



401/10-22

i desta

SEMI-ANNUAL REPORT

December, 1949

Corrosion Studies on Titenium and Zirconium Metals

L. B. Golden, I. R. Lene, and W. Mace

This investigation was initiated in June, 1947, to obtain quantitative data on the corrosion resistance of titanium and zirconium metals and their alloys to acids, bases, and salts. Since, from the utilitarian viewpoint, titanium may become a successful replacement for stainless steel, two of the more corrosion-resistant variaties, type 316 and Carpenter No. 20, have been used in parallel tests to obtain a basis for comparison. Also, since, for certain purposes, zirconium may become a replacement for the much less abundant tentalum metal, extensive tests have been made on the corrosion resistance of this metal.

During the past six months tests have been made on the corrosion resistance of titanium in solutions of phosphoric, hydrochloric, sulfuric, and nitric acids; also in mixtures of concentrated sulfuric and nitric scids. Titanium, zirconium, and stainless steels were tested in watersaturated chlorine gas and in chlorine-saturated water. The following compounds were used in carrying out tests on titanium and zirconium: ferric, aupric, mercuric, calcium, aluminum, zinc, and magnesium chlorides, and oxalic, formic, lactic, tartaric and tannic acids. A discussion of the verious tests follows.

Titanium - phosphoric acid:

し、ころいきをないないないないないのできょう

Titenium was tested in various concentrations of aerated phosphoric acid for six days at three different temperatures, 35° , 60° , and 100° C.

の地域には、「ないないないないないない」

くいたのないとないたがあるとないたのであたたがないたいため

÷.

December, 1949

Corrosion rates at 35° C ranged from a low of 0.13 mils per year in a 5 percent solution of the sold to a high of 29.7 mils per year in the concentrated (85 percent) acid. (See Table I). At 60° C rates varied from 0.74 m.p.y. in 5 percent acid to 367 m.p.v. in 85 percent acid. The corrosion resistance of titanium to phosphoric acid solutions at 100° C was very poor, since even in the 5 percent acid solution the rate was 202 m.p.y. When the concentration of the acid was raised to 50 percent, the rate was 1845 m.p.y.

Titanium - hydrochloric acid:

Titanium was tested in various concentrations of serated hydrochloric sold for six days at 35°, 60°, and 100° C. At 35° C corrosion rates were not appreciable until the concentration of sold exceeded 6 percent (Table I). Rates at 60° C ranged from 0.11 m.p.y. in 1 percent sold to 1098 m.p.y. in 20 percent sold. At 100° C rates varied from 0.35 m.p.y. in 0.5 percent sold to 938 m.p.y. in 4 percent sold.

Titanium - sulfuric acid:

Titanium was tested at 35° C in various concentrations of sulfuric acid which were kept saturated with oxygen-free nitrogen. Rates ranged from 8.00 m.p.y. in 5 percent acid to a maximum of 1640 m.z.y. in 80 percent acid (Table II).

Titanium - nitric scid:

Titanium was tested at 60° C in various concentrations of serated nitric acid. Corrosion rates were all less than 1 m.p.y. (Table II). <u>Titanium - sulfuric and nitric acid mixtures</u>:

Titanium samples were tested in non-serated and static mixtures of concentrated (96.5 percent) sulfuric acid and concentrated (69.5 percent)

December, 1949

Corrosion

A CALL AND A CALL AND

nitric soid at 35°, 60°, and 100° C. At 35° C corrosion rates ranged from a maximum of 10.6 mils per year in a mixture of 99 percent sulfuric - 1 percent nitric soid to a minimum of 0.28 mils per year in 1 percent sulfuric -99 percent nitric soid. When the concentration of sulfuric soid dropped below 50 percent the corrosion rates were all less than 3 mil per year (Table III). Colored oxide films were observed on all samples tested within the range of 80 percent sulfuric - 20 percent nitric soid to 20 percent sulfuric -80 percent nitric soid.

Corrosion rates at 60° C ranged from a minimum of 0.10 mils per year in a mixture of 1 percent sulfuric - 99 percent nitric acid to a maximum of 75.0 mils per year in 99 percent sulfuric - 1 percent nitric acid. At 100° C rates ranged from 0.65 to 1000 m.p.y. over the same range of acid concentrations as those used at 60° C. When the concentration of sulfuric acid fell below 70 percent in the mixture of the two acids at 60° C, titanium was satisfactorily resistant. However, at 100° C the concentration of sulfuric acid above which the metal corroded excessively was only 30 percent. Colored oxide films were observed on all samples tested at 60° C and 100° C within the range of 80 percent sulfuric - 20 percent nitric acid to 1 percent sulfuric - 99 percent nitric acid.

Titanium - inorgenic chlorides:

Titanium was tested in serated solutions of magnesium, ferric, cupric, and mercuric chlorides in concentrations ranging from 1 to 20 percent and at three different temperatures, 35° , 60° , and 100° C. Corrosion rates in all instances were negligible (Table IV). Tests in aerated 5 and 10 percent calcium chloride at 35° C gave negligible rates, but when the metal was tested in 10 percent calcium chloride at 100° C one of the four

and the second second second second second second second second

1

ノインないのたいないないというない

C

December, 1949

samples tested had two large, deep pits which penetrated about halfway through the sample and which were filled with a white substance (presumably titanium dioxide). Other much smaller pits were also present. The corrosion rate for this sample was 3.74 mils per year. The same type of pitting was observed when titanium was tested in 25 percent calcium chloride solution at 100° C. Although the average corrosion rate was very .ow (0.61 m.p.y.), there were present about six fairly large pits per sample, some being quite deep, penetrating about halfway through the samples (i.e. about 0.020 inches deep).

Tests in serated 5 and 10 percent sluminum chloride solutions at 35° .C and in 10 percent sluminum chloride at 100° C gave zero or negligible corrosion rates. However, in 25 percent sluminum chloride at 100° C, ti-tanium was severely corroded. Three out of four samples were evenly corroded while the fourth contained num rous shallow pits similar to those formed in calcium chloride solutions.

Tests in aerated 5 and 20 percent zinc chloride solutions at 35° , 60° , and 100° C gave negligible corrosion rates. Although the corrosion rate for titanium in boiling 5 percent zinc chloride colution was zero since no weight loss occurred, numerous small pits were present on the surfaces of the samples. However, pitting was not as severe as that which had occurred in 25 vercent calcium chloride solution at 100° C.

Titanium, zirconium, and stainless steels - chlorine- saturated water and water-saturated chlorine:

Titenium, zirconium, and type 316 and Carpenter 20 stainless steels were tested at room temperature totally immersed in chlorine-saturated water for a period of 172 hours. Corrosion rates for titenium and zirconium were

December, 1949

Corrosion

and a state of the second s

*

155. And a water water .

Ċ

negligible, those for Carpenter 20 stainless steel very low, while the rates for type 316 stainless steel were appreciable (Table V).

However, when these metals and alloys were tested in an atmosphere of water-saturated chlorine, marked differences in corrosion resistance were observed. Titanium showed no evidence of corrosion with the exception of a very slight loss in weight. On the other hand, zirconium was only slightly resistant to an attack which was characterized by the formation on the surface of the metal of a voluminous moss-like or fungous-like gray-colored corrosion product. The underlying metal was badly pitted and in several instances the pits penetrated entirely through the sample. Zirconium metal prepared by the Foote Mineral Company (inlide process) was subjected to the same test and results similar to those with Bureau of Mines (magnesium reduction process) zirconium were obtained (Figures I-IV).

Titanium, zirconium, and stainless steel - oxalic scid:

Titanium exhibited poor corrosion resistance to even very dilute solutions of aereted oralic acid at elevated temperatures (Table VI). Even a 0.5 percent acid solution at 60° C gave a rate of 94.5 mils per year and higher percentages and temperatures gave correspondingly greater corrosion rates. In contrast, zirconium gave very low rates (less than 0.50 m.m.y.) in all concentrations of acid tested. In the concentrations tested, Carpenter 20 steinless steel resisted the corrosive action of oralic acid much better than titenium.

Titanium, zirconium, and stainless steel - formic acid:

Titenium showed negligible corrosion rates when tested in <u>serated</u> 90 percent formic acid at 60° C, and in <u>merated</u> 25 and 50 percent formic acid at 100° C (Table VI). However, when tested in boiling (non-cerated)

-5-

and the second

いたいというないないというなどのないないないないでいたことととなってい

December, 1949

25, 50, and 90 percent formic acid, corrosion rates were 96.0, 300, and 118 mils per years, respectively. These tests clearly demonstrate the important part played by oxygen in inhibiting corrosion under certain conditions. Zirconium gave rates of less than 0.2 m.p.y. for all concentrations of acid tested and Carpenter 20 stainless steel less than 7.0 m.p.y.

Titanium, zirconium, and stainless steel - lactic acid:

Titanium, zirconium, and Carpenter 20 stainless steel were each tested in various concentrations of aerated lactic acid. The only appreciable corrosion rate (12.2 m.z.y.) was that shown by the stainless steel in boiling 85 percent acid (Table VI).

Titanium, zirconium, and steinless steel - tertaric acid:

Titanium, zirconium, and Carpenter 20 stainless steel were each tested in various concentrations of aerated tarteric acid at 35° C. Corrosion rates were zero or negligible (Table VI).

Titanium end stainless steel - tannic scid:

Titenium and Carpenter 20 stainless steel showed zero or negligible corrosion rates when tested in 25 percent tennic acid solution (Table VI). Ziroonium and stainless steel - inorganic chloriles:

Zirconium and Carpenter 20 stainless steel were both tested in sereted solutions of calcium, aluminum, zinc, and megnesium chlorides in concentrations ranging from 5 to 20 percent and at three different temperatures, 35° , 60° , and 100° C. At 35° C rates for both metals were negligible. (See Table VII). Rates for zirconium were zero or negligible in all solutions tested at 60° and 100° C. Carpenter No. 20 stainless steel was eppreciebly corroded by 10 percent aluminum chloride solution at 60° and 100° C

-6-

December, 1949

Corrosion

とないないではないとないからいまたのできょうとう

Titanium and zirconium - sulfurous acid:

Titenium and zirconium samples were tested in sulfurous acid (6 percent solution of sulfur dioxide) at 60° C and 100° C. The tests were carried out under pressure in scaled glass tubes to prevent the loss of any sulfur dioxide from solution at these temperatures. Corrosion rates were negligible.

Titenium, zirconium, and steinless steel - boiling chromic acid:

Titanium, zirconium, and Carpenter 20 stainless steel were each tested in boiling chromic acid (10 percent CrO3) for a period of eleven days. The corrosion rates for the three metals were, respectively, 0.04, 0.00, and 91.0 mils per year.

Zirconium - nitrie sei::

Tests were made on zirconium in 10, 20, 30, 40, and 50 percent nitric ecid solutions at 60° C. Rates were all negligible (0.00 - 0.10 m.r.y.). Zirconium - boiling nitric acid test (Huey test):

Zirconium was tested in boiling 65 percent nitric acid for one 24hour and four 48-bour test periods. Corrosion rates for the successive periods were 0.44, 0.04, 0.08, 0.00, and 0.00 m.p.y., respectively, giving an average of 0.11 m.;.y.

Zirconium - phosphoric acid:

Zirconium was tested in boiling 85 percent phosphoric acid for sir days. The corrosion rate was very high (739 m.p.y.).

Stainless steel - boiling red fuming mitric acid:

Carpenter No. 20 stainless steel, when tested in boiling red fuming nitric acid for a period of eleven days, showed a corrosion rate of 16.1 mils per year. Identical tests using titanium and zirconium metals gave rates of

-7-

Story and

O

になったが見たいないので、人口という

いったい たったいとうたいとう

December, 1949

0.26 and 0.29 mils per year, respectively.

* * *

Future program:

The program for the immediate future will include a continuation of tests on titanium and zirconium metals with inorganic and organic acids and solutions of salts and bases at different concentrations and temperatures. Tests have just been started on the corrosion resistance of a series of titanium-zirconium alloys to materials used for rocket fuels. Simulated marine atmosphere tests (salt spray) will also be made. Galvanic corrosion research will be conducted on titanium and zirconium and their alloys. the web an age and

: •

• • • • • • • •

A REAL PROPERTY AND A REAL

C

•

Corrosion

December, 1949

TABLE I

T	Average corrosion rate			
Test Solution	6-day run, mils per year			
(percent by weight)	35° C	60° 0	100° C	
1.0 H3P04			0.12	
3.0 H3P04			62.0	
5.0 H3P04	0.13	0.74	202	
10 H3P04	0.30	1.50	455	
15 H3P04			480	
20 H3P04	0.60	13.7	685	
30 H3P04	0.77	59.0	1040	
32.5 H3P04	5.64			
35 H3P04	5.80		£	
37.5 H3P04	8.40			
40 H3P04	13.4	128	1550	
50 H3P04	18.5	179	1845	
60 H3P04	22.4	239		
70 H3P04	26.8	280		
80 H3P04	29.0	340		
85 HaPOA	29.7	367		
0.5 HC1			0.35	
1.0 HC1	0.23	0.11	18.5	
1.5 HC1			173	
2.0 HC1		0.64	272	
2.5 HC1			444	
3.0 HC1	0.29	0.38	696	
3.5 HC1			689	
4.0 HC1		42.6	938	
5.0 HCl	1.46	42.5		
6.0 HC1	2.44	131		
7.0 HC1		176		
7.5 HC1	20.8	· 1		
10.0 HC1	40.1	351		
12.5 HC1	59.5	604		
15.0 HCl	96.7	739		
17.5 HCl	122			
20.0 HCl	175	1095		
	-,,			

Titanium - Inorganic Acids (with meration)

with the second

support to - new

8

\$2

2

e.

and the second states of the second states of the second se

1)

December, 1949

• ;

ころうちょう ちょうちょう しょうちょう しょうちょう しょうしょう しょうしょう

TABLE II

Test solution Temperature (persent by weight) 0 C Aeration	Average corresion rate, 6-day run, ails per year
5 H_2SO_4 35 $N_2 - set'i.$ 10 H_2SO_4 35 $H_2 - sat'i.$ 20 H_2SO_4 35 $N_2 - sat'd.$ 30 H_2SO_4 35 $N_2 - sat'd.$ 40 H_2SO_4 35 $N_2 - sat'd.$ 50 H_2SO_4 35 $N_2 - sat'd.$ 60 H_2SO_4 35 $N_2 - sat'd.$ 70 H_2SO_4 35 $N_2 - sat'd.$ 70 H_2SO_4 35 $N_2 - sat'd.$ 75 H_2SO_4 35 $N_2 - sat'd.$ 80 H_2SO_4 35 $N_2 - sat'd.$ 80 H_2SO_4 35 $N_2 - sat'd.$ 96 H_2SO_4 35 $N_2 - sat'd.$ 96 H_2SO_4 35 $N_2 - sat'd.$ 96 H_2SO_4 35 $N_2 - sat'd.$ 10 HNO_3 60 $sir - sat'd.$ 20 HNO_3 60 $sir - sat'd.$ 30 HNO_3 60 $sir - sat'd.$ 40 HNO_3 60 $sir - sat'd.$ 50 HNO_3 60 $sir - sat'd.$ 60 HNO_3 60 $sir - sat'd.$	$ \begin{array}{r} 8.00\\ 47.5\\ 60.4\\ 152\\ 264\\ 95\\ 29.6\\ 16.9\\ 38.0\\ 1620 $

∦ 73-hour run * 48-hour run

White the state of the second state of the sec

C

Corrosion

December, 1949

III ALEAT

Test Solution*	Average corrosion rate 6-day run, mils per year			
(percent by weight)	35° C	60° C	100° C	
100 H2SO4 + 0 HNO3 99 H2SO4 + 1 HNO3	209 10.6	 75.0	1000	
95 H2SO4 + 5 HNO3 90 H2SO4 + 10 HNO3	8.31 8.80	74.4 68.9	1060 1050	
$\begin{array}{c} 80 \ \text{H}_2\text{SO4} \ \ 1 \ \ 20 \ \ \text{HNO3} \\ 70 \ \ \text{H}_2\text{SO4} \ \ 1 \ \ 30 \ \ \text{HNO3} \\ 6 \ \ \text{H}_2\text{SO4} \ \ 1 \ \ 30 \ \ \text{HNO3} \\ \end{array}$	9.50 5.68	62.5 49.1	927 759	
$\begin{array}{r} 80 & H_2 \\ 50 & H_2 \\ 804 & + 50 & H \\ 803 \\ 40 & H_2 \\ 804 & + 60 & H \\ 803 \\ 804 $	1.42	15.7	265	
$30 H_2 SO_4 + 70 HNO_3$ 20 H_2 SO_4 + 80 HNO_3	0.34 0.38	2.36	37.0	
10 H2SO4 + 90 HNO3 5 H2SO4 + 95 HNO3	0.34 0.28	0.45 0.20	3.89 1.85	
$1 H_2 SO_4 \neq 99 HNO_3$ $0 H_2 SO_4 \neq 100 HNO_3$	0.28 0.45	0.10	0.65	

Titenium - Sulfuric and Nitric Acid Mixtures

* /sll solutions non-serated and static

÷

64 . 6 . .

Matheway and

あたいであるい いちょうしん ひょういんひん ちょうちょう たいちょうちょう

11

いたがないためにいたななないないないないであるなかのないないないないないのです。

€

Corrosion

December, 1949

TABLE IV

Cook Columban	Average corrosion rate			
(oncost by weight)	750 0	sy run, mils per	100 0	
(, ereance by werghe)		00 0	100 0	
l FeCl3	0.02		0.00	
5 F0C13	0.09		0.03	
1.0 FeC1 2	0.00		0.09	
15 FeC13	0.10		0.13	
20 FeC13	0.13		0.13	
$1 \operatorname{CuCl}{2}$	0.14		- 	
5 Oucl ₂	0.18			
10 Ou012	0.02			
15 CuCl2	0.02		_ -	
1 Hg012	0.02			
5 HgCl2	0.05	0.00		
10 HgC12			0.04	
st'd. sol'n. FgCl2	0.05	0.00	0.04	
5 CuCl2	0.00		~-	
10 CnCl2	0.07		0.29	
25 CeCl2			0.61	
5 A1013	0)0			
10 11013	0.00		0.09	
25 A1013			258	
5 ZnCl2	0.)6	0.00	0.20 (0.00*)	
20 ZnCl2	0.75	0.24	0.10	
5 MgCl2	0.00	0.00		
20 MgC12	0.14			

Titanium - Inorgenic Chlorides (with seration)

* Boiling and non-serated

iller and the

4. * * * >

STATISTICS AND ADDRESS OF

のないであるというのないのであると

「ないない」のないないないないないないないないないないです。 ひょう

C

TABLE V

Titanium, Zirconium, and Steinless Steels - Chlorine (Room Temperature)

	Test Solution	Avorage corresion rate			
Metal	(percent by weight)	172-hr. run, mils per year			
C.R. $Ti^{1/2}$ C.R. $2r^{2/2}$ 316 S.S. $3^{1/2}$ 20 S.S. $4^{1/2}$ C.R. Ti C.R. $2r$ 316 S.S.	Cl2 seturated H20 Cl2 seturated H20 Cl2 seturated H20 Cl2 seturated H20 Cl2 seturated H20 H20 seturated Cl2 H20 seturated Cl2 H20 seturated Cl2	0.10 0.56 15.4 1.46 0.07 192 527			
20 3.3.	ngo saturated C12	470			

 $\frac{1}{2}$ Cold rolled titanium $\frac{2}{2}$ Cold rolled zirconium

3/ Type 316 steinless steel 4/ Carpenter 20 stainless steel

-13-

٠

and the first of the second second

Corrosion

December, 1949

あいないので、このので、ないのというないないないないない

こうちょう とう 一般ない こういかい あまいい

;

2

たいまたので、このないないないないできたいできたいで、このないないできたいできたいできょう

TABLE VI

8 **(**

などないたいことがあたが

ŝ .

Titanium, Zirconium and Stainless Steel - Organic Acids (with seration)

		Average corresion rate			
	Test Solution	6-day run, mils per year			ear
Metal	(percent by weight)	35° C	60° C	100° C	Boiling
2/		1	T		
C.R. TI	0.5 oxalic	0.55	94.5	82.0	;
C.R. Ti	l oxelic	5.96	177	828*	ç
$C.R. 7r^{2}$	1 oxelic	0.13	0.20		\$
20 S.S.2/	l oxalic	0.08	1.30		
C.R. TI	5 oralic	4.94	368	1290*	÷
C.R. Zr	5 oxalic	0.29	0.30		·
20 S.S.	5 ovelic	0.25	2.67	·	
C.R. Ti	10 oxelic	0.58	450	1240*	
C.R. Zr	10 oxelic	0.48		•	
20 S.S.	10 oxalic	0.19		·	
C.R. Ti	25 oxalic	J	470	1945*	, * <i>*</i> *
C.R. 14	10 formia			0.18	i 0.00
C.R. 2r	10 formic				0.00
20 5.8.	10 formic				6.30
C.R. T1	25 formic	ľ		0.04	96.0
C.R. Zr	25 formic				0.09
20 S.S.	25 formic				. 6.27
C.R. Ti	50 formie			0.94	300
C.R. Zr	50 formic				0.19
20 S.S.	50 formic			·	1.92
C.R. Ti	90 formic	5 0.33	0.91		. 118
C.R. Zr	90 formic	0.12			0.16
20 S.S.	90 formic	0.17	~		1.11
C.R. Ti	25 lactic	0.03			
C.R. Zr	25 lactic	0.03			·
C.R. Ti	50 lectic	0.08			,
C.R. Zr	50 lactic	0.00			
C.R. Ti	85 lectic	• 0.00		0.33	0.40
C.R. Zr	85 lactic	0.00			0.09
20 3.5.	85 lectic	0.00		۰	12.2
C.R. TI	10 tartaric	0.00			
7.R. Zr	10 tertaric	0.00			
20 S.3.	10 tartaric	0.00			
C.R. Ti	25 terteric	0.00			
C.R. Zr	25 tartarie	* 0.00			[
20 S.S.	25 tartaric	0.07			
C. <u>R.</u> 71	50 tartaric	0.08			
20 S.S.	50 tartaric	0.08			
C.R. TI	25 tannic	0.00	0.00	0.00	
20 S.S.	25 tennic	0.00	0.00	0.29	
				·	

 $\frac{1}{2}$ Cold rolled titanium $\frac{2}{2}$ Cold rolled zirconium $\frac{3}{2}$ Carpenter 20 stainless ateel

* three-day run

boiling solutions were nonaerated

NY INAN

the Training of the second day

and the state of the second

PRINT NAMES

and a start and a start and the start and th

> MALES ...

C

December, 1949

TABLE VII

Average corrosion rate lest solution b-day run, mils per year C 60° C 100 35° C Metal (percent by weight) 100° C C.R. $2r^{1/2}$ 0.00 5 CeC12 -----C.R. 3r 20 S.S.² 0.00 10 CaCl2 0.00 0.00 10 CaC12 0.01 0.04 0.11 5 4101 2 C.R. Zr 0.00 -----C.R. Zr 10 ,1013 0.02 0.00 0.00 20 8.3. 10 A1013 0.39 14.4 45.2 C.R. Zr 5 ZnC12 0.01 0.08 0.04(0.00*) 20 5.5. 5 ZnC12 0.04 0.15 31.3(6.)5* 20 ZnCl2 C.R. Zr 0.02 ------20 5.9. 20 3nC12 0.05 --------C.R. Cr 0.00 5 MgC12 0.02 ----20 3.8. 5 MgCl2 0.07 0.00 - -C.R. Zr 20 MgC12 0.15 0.90 ... 20 8.8. 20 Mg012 0.09 ------ -

Zirconium and Stainless Steel - Inorgania Chioriles (with aeration)

1/ Cold rolled zirconium

2/ Carpenter 20 steinless steel

* boiling and non-serated







Pig. 2 Xl Zirconium after 172 hours exposure in an atmosphere of water-saturated chlorinc. Average corrosion rate was 192 mils per year.







Fig. 4 X1 Carponter 10. 20 stainless steel after 172 hours exposure in an atmosphere of water-saturated chlorine. Average corrosion rate was 473 mils per year.