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FEASIBILITY OF A SINGLE COMMON POWERTRAIN LUBRICANT-TRANSMISSION BENCH TESTING

INTERIM REPORT TFLRF No. 417

by Adam C. Brandt Edwin A. Frame

U.S. Army TARDEC Fuels and Lubricants Research Facility Southwest Research Institute[®] (SwRI[®]) San Antonio, TX

and

Allen S. Comfort U.S. Army TARDEC Force Projection Technologies Warren, Michigan

Contract No. DAAE-07-99-C-L053 (WD42)

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The goal o	f the Army Single C	ommon Powertrain	Lubricant (SCPL) prog	gram is to devel	op an all-season (arctic to desert),
fuel efficie	nt, multifunctional p	owertrain fluid with	extended drain capabi	ilities. SCPL mu	ast be able to properly function in
various me	echanical application	is including engine	crankcase lubrication	n, powershift ti	ransmission operation, and some
hydraulic s	vstem operation Sev	eral diesel engine cr	ankcase oils were eval	uated in powers	shift fluid bench tests to determine
the feasibil	ity of using engine of	l in this application	While none of the engi	ine oils nassed a	ll the bench tests, overall technical
foosibility	was domonstrated as	r in this application.	or near passing result	a with the slote of	of anging cile tested
leasionity	was demonstrated as (evidenced by passing	, of heat passing result	s with the state (of eligine ous tested.
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EXECUTIVE SUMMARY

The goal of the Army Single Common Powertrain Lubricant program SCPL is to develop an allseason (arctic to desert), fuel efficient, multifunctional powertrain fluid with extended drain capabilities. This program seeks to leverage state-of-the-art base oil and additive technologies to significantly improve upon current military lubricant products, and act as an enabler for future powertrain technologies. Due to the versatility desired in the SCPL program, candidate fluids must be able to properly function in various mechanical applications including engine crankcase lubrication, powershift transmission operation, and some hydraulic system operation. It is desired that SCPL meet or exceed minimum performance requirements when used in all of the above systems in operating environments varying from arctic to desert type conditions. Various test programs have been initiated to quantify candidate SCPL performance in each of the above applications. This report covers testing relating to the feasibility of incorporating powershift transmission performance in SCPL. Overall, the performance of various diesel engine oils tested in a variety of friction bench tests was determined. The results indicate that use of engine oils in military automatic/ powershift transmission applications is technically feasible as evidenced by passing or near passing friction bench test results with the slate of engine oils tested. This will enable the marriage of diesel engine oil performance with military automatic/powershift transmission performance in a SCPL.

FOREWORD/ACKNOWLEDGMENTS

The U.S. Army TARDEC Fuel and Lubricants Research Facility (TFLRF) located at Southwest Research Institute (SwRI), San Antonio, Texas, performed this work during the period January 2008 through January 2009 under Contract No. DAAE-07-99-C-L053. The U.S. Army Tank-Automotive RD&E Center, Force Projection Technologies, Warren, Michigan administered the project. Mr. Luis Villahermosa (RDTA-SIE-ES-FPT) served as the TARDEC contracting officer's technical representative.

The authors would like to acknowledge the contribution of the TFLRF technical support staff along with the administrative and report-processing support provided by the TFLRF administration staff.

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ACRONYMS AND ABBREVIATIONS

CAT – Caterpillar FRRET – friction retention kPa – kilopascals m/s – meters per second N-m – Newton Meters OEA – Oil Engine Arctic QPL – Qualified Products List SAE – Society of Automotive Engineers SCPL – Single Common Powertrain Lubricant sec- seconds SEQ - sequence SwRI – Southwest Research Institute TARDEC – Tanks Automotive Research and Development Engineering Center

TFLRF - TARDEC Fuels and Lubricants Research Facility

1.0 INTRODUCTION AND BACKGROUND

The US Army TARDEC Fuels and Lubricants Research Facility (TFLRF) located at Southwest Research Institute (SwRI) in San Antonio, TX, was tasked to determine the technical and economic feasibility of developing and implementing a Single Common Powertrain Lubricant (SCPL) for use in all combat tactical equipment currently using MIL-PRF-2104 [1] and MIL-PRF-46167D [2] lubricants. The project goal for the SCPL program is to develop an all-season (arctic to desert), fuel efficient, multi functional powertrain fluid with extended drain capabilities. This program seeks to leverage state-of-the-art base oil and additive technologies to significantly improve upon current military lubricant products, and act as an enabler for future powertrain technologies.

2.0 **OBJECTIVE**

Due to the versatility desired in the SCPL program, candidate fluids must be able to properly function in various mechanical applications including engine crankcase lubrication, powershift transmission operation, and some hydraulic system operation. Candidate oils must meet or exceeded minimum performance requirements when used in all of the above systems in operating environments varying from arctic to desert type conditions. Various test programs have been initiated at TFLRF to quantify candidate oil performance in each of the above applications. This report covers the feasibility testing relating to engine oil performance in powershift transmission applications.

3.0 APPROACH

To determine engine oil performance in powershift transmission applications, several oils were subjected to various commercial transmission oil testing procedures. Six initial engine oils were chosen for testing. Engine Oil viscosities ranged from SAE15W-40 grades consistent with MIL-

PRF-2104 oils, to OEA-30 MIL-PRF-46167 arctic grade oils. Each candidate oil and its qualified products list (QPL) number, where applicable, are listed below.

Description	Code No.
MIL-PRF-2104G, SAE 15W-40, QPL NO. PRI EO 0058 (S)	AL-27793
MIL-PRF-2104H, SAE 15W-40, EO 0068 (L)	AL-27876
MIL-PRF-2104G, SAE 5W-40, QPL NO. PRI EO 0067 (E)	AL-27252
MIL-PRF-46167D, OEA 30, QPL NO. ME-35 (C)	AL-27637
MIL-PRF-46167D, OEA 30 (New)	AL-27877
Experimental SAE 5W-40 (L)	AL-27875

The following tests were performed on each oil:

- Caterpillar TO-4 Friction Test
 - o TO-4 SEQ 1219 (Elastomeric)
 - TO-4 SEQ 1221 (Steering Brake Paper)
 - TO-4 SEQ 1222 (Wheel Brake Paper)
 - TO-4 SEQ 1223 (Transmission Paper)
 - TO-4 SEQ 1224 (Elastomeric)
 - TO-4 SEQ 1220 (OEA 30 (New) and Experimental 5W-40 (L) only)
 - TO-4 SEQ FRRET (OEA 30 (New) and Experimental 5W-40 (L) only)
- DEXRON-VI (OEA-30 ME-35 (C) and OEA 30 (New) only)
 - Band Clutch Friction
 - Plate Clutch Friction
 - Low Speed Clutch Friction and Torque Capacity
- John Deere JDQ-96 Brake Torque Retention & Friction (1000 cycles)
- Allison C4 Friction Test (Paper and Graphite, OEA 30 (New) only)

4.0 **RESULTS/DISCUSSIONS**

Top-level details of each testing procedure, and individual oil performance results are discussed in the following sections.

4.1 CAT TO-4

CAT TO-4 tests are designed to evaluate oils to determine if minimum performance requirements are met for fluids that are intended for use in CAT equipment. CAT specifies that the primary use for these types of fluids would be found in powershift transmissions, final drives, hydrostatic transmissions, torque converters, wheel brakes, steering brakes, and steering clutches. The TO-4 testing apparatus consists of a flywheel with a known inertial value, a variable speed AC motor, a stationary reaction plate, and a load cell to measure application forces. Various friction materials are attached to the flywheel and brought up to a specified speed with the variable speed motor. After reaching the desired speed, the kinetic energy is then absorbed by engaging the flywheel with the stationary reaction plate at various application pressures. The reaction plate is fitted with a complimentary steel plate of similar dimensions as the tested friction disk. The lubrication oil is applied to the friction surface from a feed line mounted on the reaction plate. A diagram of the testing apparatus is presented in Figure 1. The apparatus is used to measure the dynamic and static coefficient of friction, energy capability, wear resistance, and friction retention of each material and test fluid combination [3].



Figure 1. CAT TO-4 VC70 Testing Apparatus

The CAT TO-4 test is divided up into multiple sequences, with each sequence representing a different friction material being tested. Listed below are the seven sequences of the TO-4 test and their respective tested friction material:

- CAT TO-4 SEQ 1219 (Elastomeric)
- CAT TO-4 SEQ 1221 (Steering Brake Paper)
- CAT TO-4 SEQ 1222 (Wheel Brake Paper)
- CAT TO-4 SEQ 1223 (Transmission Paper)
- CAT TO-4 SEQ 1224 (CAT F37 Elastomeric)
- CAT TO-4 SEQ 1220*
- CAT TO-4 SEQ FRRET*

*Note – CAT TO-4 SEQ 1220 and FRRET are required testing procedures for all military spec oils, and were completed on the OEA 30 (New) and Experimental 5W-40 (L) oils only.

A torque versus time plot is generated for each friction material as the rotating flywheel is accelerated from its initial speed to a stop, and is used to calculate the coefficient of friction. The coefficient of friction is a dimensionless value that describes the ratio of frictional forces between two surfaces versus the force applying the two surfaces together. An example friction curve is presented in Figure 2. where rotational speed is the speed of the flywheel, and clutch pressure is the pressure applied between the friction disk and reaction plate. The resulting torque values can then be used to calculate the coefficient of friction between the two surfaces as a function of relative velocity, and application pressure. The dynamic coefficient of friction is the component of friction present when the two acting surfaces have a differential velocity between them. This can be seen in the flat portion of the torque curve as the rotational velocity decreases from its initial speed to zero. The static coefficient of friction is the component of friction is the differential velocity between the two acting surfaces goes to zero. This can be seen at the final torque spike towards the end of the torque curve.



Figure 2. Typical TO-4 Test Torque Response Curve

The importance of the torque curve is to determine the consistency of coefficient of friction over a wide variety of relative velocities and application pressures. If a flat torque curve exists in the dynamic range, the coefficient of friction remains relatively constant and the resulting behavior of the driveline components remain consistent. If the torque drastically shifts in the dynamic region, this means the dynamic coefficient of friction has changed and the driveline behavior can become inconsistent. This effect can be realized through a sudden grabbing or slipping during engagement or disengagement. An example curve showing this behavior is presented in Figure 3.



Figure 3. Non-typical TO-4 Torque Response Curve

From experience gained through testing, it has been found that multipurpose engine oils typically yield lower overall coefficient of friction values than transmission fluids. This should be taken into consideration when comparing engine oil performance in these tests. While some of the candidate oils failed to meet minimum coefficient of friction specifications, their overall behavior was consistent and yielded values only slightly lower than approved transmission fluids. In these types of situations, it is possible that the candidate oils performance would not prohibit its use in transmission applications. In addition, all candidate oils were only subjected to one round of TO-4 testing yielding single point data. Due to inherent variation in this testing, some borderline failures could be deemed passing with continued testing to gain more statistical significance in the results.

The resulting data for sequences 1219, 1221, 1222, 1223, and 1224 for each candidate oil was examined for trends by:

- Comparing the relative performance of oils by each sequence
- Comparing the relative performance of oils by similar viscosity grade

4.1.1 Performance by Test Sequence

Table 1 and Table 2 lists CAT TO-4 test results of each candidate oils and approximate magnitude of failure where applicable.

Table 1. TO4 Test Results

	OEA 30 ME-35 (C)	5W-40 EO 0067 (E)	15W-40 EO 0058 (S)	Experimental 5W-40 (L)	15W-40 EO 0068 (L)	OEA 30 (New)
	AL-27637-L	AL-27252-L	AL-27793-L	AL-27875-L	AL-27876-L	AL-27877-L
Caterpillar TO-4	27637-1	AL-27252-L	AL-27793-L	AI - 27875-I	AI - 27876-I	AI - 27877-1
SEQ 1219 (Elastomeric)	Test No. VC70-A-77-I	Test No. VC70-A-70-I	Test No. VC70-A-84-I	Test No. VC70-A-85-1	Test No. VC70-A-86-1	Test No. VC70-A-75-I
	Date Requested: 7/17/2007	Date Requested: 7/17/2007	Date Requested: 8/2/2007	Date Requested: 9/13/2007	Date Requested: 9/13/2007	Date Requested: 9/7/2007
	Date Started: 10/7/2007	Date Started: 8/8/07	Date Started: 11/8/07	Date Started: 11/16/07	Date Started: 11/24/2007	Date Started: 9/27/2007
	Date Finished: 10/11/2007*	Date Finished: 8/13/2007 *	Date Finished: 11/15/2007 *	Date Finished: 11/20/2007 *	Date Finished: 11/28/2007*	Date Finished: 10/2/2007*
Dynamic Coeficient vs Cycle	Fail - Approx min coef: 0.105 Approx test coef: 0.100	Fail - Approx min coef: 0.105 Approx test coef: 0.099	Fail - Approx min coef: 0.105 Approx test coef: 0.097	Fail - Approx min coef: 0.105 Approx test coef: 0.098	Fail - Approx min coef: 0.104 Approx test coef: 0.098	Fail - Approx min coef: 0.104 Approx tested coef: 0.097
Dynamic Coeficient vs Load	Fail - Approx min coef: 0.105 Approx test coef: 0.103	Fail - Approx min coef: 0.105 Approx test coef: 0.099	Fail - Approx min coef: 0.105 Approx test coef: 0.095	Fail - Approx min coef: 0.104 Approx test coef: 0.095	Fail - Approx min coef: 0.104 Approx test coef: 0.098	Fail - Approx min coef: 0.104 Approx test coef: 0.095
Dynamic Coeficient vs Speed	Fail - Below spec until tested speed increases above approx 35 m/s	Fail - Below spec until tested speed increases above approx 36 m/s	Fail - Below spec until tested speed increases above approx 36 m/s	Fail - Below spec until tested speed increases above approx 38 m/s	Fail - Below spec until tested speed increases above approx 36 m/s	Fail - Below spec until tested speed increases above approx 36 m/s
Energy Limit	Pass	Pass	Pass	Pass	Pass	Pass
Static Coeficient vs Load	Pass	Pass	Pass	Pass	Pass	Pass
Static Coeficient vs Speed	Pass	Pass	Pass	Pass	Pass	Pass
Energy Limit	Pass	Pass	Pass	Pass	Pass	Pass
Total Wear	0.033	0.026	0.022	0.015	0.013	0.007
Wear Limit	0.030	0.03	0.030	0.030	0.030	0.030
Caterpillar TO-4	27637-L	AL-27252-L	AL-27793-L	AL-27875-L	AL-27876-L	AL-27877-L
SEQ 1221 (Steering Brake Paper)	Test No. VC70-A-77-I	Test No. VC70-A-70-I	Test No. VC70-A-84-I	Test No. VC70-A-85-1	Test No. VC70-A-86-1	Test No. VC70-A-75-I
	Date Requested: 7/17/2007	Date Requested: 7/17/2007	Date Requested: 8/2/2007	Date Requested: 9/13/2007	Date Requested: 9/13/2007	Date Requested: 9/7/2007
	Date Started: 10/7/2007	Date Started: 8/8//07	Date Started: 11/8//07	Date Started: 11/16/07	Date Started: 11/24/2007	Date Started: 9/27/2007
	Date Finished: 10/11/2007*	Date Finished: 8/13/2007 *	Date Finished: 11/15/2007 *	Date Finished: 11/20/2007 *	Date Finished: 11/28/2007*	Date Finished: 10/2/2007*
Dynamic Coefficient vs Cycle	Pass	Pass	Pass	Pass	Pass	Pass
Dynamic Coeficient vs Load	Pass	Pass	Pass	Pass	Pass	Pass
Dynamic Coeficient vs Speed	Fail - Coef. within limits until tested speed increases above approx 24 m/s	Pass	Pass	Pass	Pass	Fail - Coef. within limits until tested speed increases above approx 21 m/s
Eperav Limit	Pass	Pass	Pass	Pass	Pass	Pass
	1 400	1 400	1 400	1 400	1 400	1 400
Static Coeficient vs Load	Pass	Pass	Pass	Pass	Pass	Fail - Borderline, marginally below spec throughout test duration (<0.005)
Static Coeficient vs Speed	Fail - Coef. within limits briefly at start of test then falls out of spec at approx 14 m/s	Pass	Pass	Pass	Pass	Fail - Coef. below limits at start of test and steadily decreases
Energy Limit	Pass	Pass	Pass	Pass	Pass	Pass
Total Wear	0.029	0.037	0.032	0.020	0.046	0.040
Wear Limit	0.070	0.070	0.070	0.070	0.070	0.070
Caterpillar TO-4	27637-L	AL-27252-L	AL-27793-L	AL-27875-L	AL-27876-L	AL-27877-L
SEQ 1222 (Wheel Brake Paper)	Test No. VC70-A-77-I	Test No. VC70-A-70-I	Test No. VC70-A-84-I	Test No. VC70-A-85-1	Test No. VC70-A-86-1	Test No. VC70-A-75-I
	Date Requested: 7/17/2007	Date Requested: 7/17/2007	Date Requested: 8/2/2007	Date Requested: 9/13/2007	Date Requested: 9/13/2007	Date Requested: 9/7/2007
	Date Started: 10/7/2007	Date Started: 8/8//07	Date Started: 11/8//07	Date Started: 11/16//07	Date Started: 11/24/2007	Date Started: 9/27/2007
	Date Finished: 10/11/2007*	Date Finished: 8/13/2007 *	Date Finished: 11/15/2007*	Date Finished: 11/20/2007 *	Date Finished: 11/28/2007*	Date Finished: 10/2/2007*
Dynamic Coeficient vs Cycle	Pass	Pass	Pass	Pass	Fail - Borderline, marginally below min spec throughout entire test (<0.005)	Pass
Dynamic Coeficient vs Load	Pass	Pass	Pass	Pass	Fail - Coef within limits at start of test, quickly falls below min spec through remainder of test	Pass
Dynamic Coeficient vs Speed	Pass	Pass	Fail - Coef. within limits at start of test, quickly falls below min spec through remainder of test	Fail - Coef. within limits at start of test, quickly falls below min spec through remainder of test	Fail - Coef below limits throughout test	Fail - Coef. within limits until tested speed increases above approx 19 m/s
Energy Limit	Pass	Pass	Pass	Pass	Pass	Pass
Static Coeficient vs Load	Fail - Coef. within limits at start of test and falls below after approx 1600 kPa	Pass	Pass	Fail - Coef. within limits at start of test, falls below limits after 800 kPa	Fail - Borderline, Coef. within limits at start of test and falls below after 900 kPA (<0.005)	Fail - Coef. within limits at start of test, falls below limits after approx 700 kPa
Static Coeficient vs Speed	Fail - Coef. at start below min spec and steadily decreases throughout test	Pass	Pass	Fail - Coef. at start below min spec. Coef increases at approx 20 m/s and satisfies limits at approx 24 m/s through remainder of test	Pass	Fail - Coef. at start below min spec. Coef increases at approx 21 m/s and satisfies limits at approx 25 m/s through remainder of test
Energy Limit	Pass	Pass	Pass	Pass	Pass	Pass
Total Wear	0.047	0.039	0.029	0.054	0.038	0.033
Wear Limit	0.070	0.07	0.070	0.070	0.070	0.070

Table 2. TO4 Test Results Continued

	OEA 30 ME-35 (C)	5W-40 EO 0067 (E)	15W-40 EO 0058 (S)	Experimental 5W-40 (L)	15W-40 EO 0068 (L)	OEA 30 (New)
Catornillar TO 4	276271	AL 27262	AL 27702	AL 27075-L	AL 27076	AL 27077-L
SEO 1223 (Transmission Danor)	27037-L Teet No. VC70 & 77 L	Tect No. VC70 & 70 J	TectNo VC70 A 94 I	Toot No. 1/070 A 95 1	Tect No. VC70 A 96 1	Tect No. VC70 & 75 L
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	Date Started: 10/7/2007	Date Started: 8/8//07	Date Started: 11/8//07	Date Started: 11/16//07	Date Started: 11/24/2007	Date Started: 9/27/2007
	Date Finished: 10/11/2007*	Date Finished: 8/13/2007 *	Date Finished: 11/15/2007 *	Date Finished: 11/20/2007 *	Date Finished: 11/28/2007*	Date Finished: 10/2/2007*
Dynamic Coeficient vs Cycle	Pass	Fail - Coef. below limits at start of test, Coef. meets limits after approx 75 cycles	Fail - Approx min spec: 0.105 Approx tested spec 0.103	Fail - Approx min spec 0.108 Approx tested spec: 0.100	Fail - Borderline below test at start and finish (<0.005)	Fail - Approx min spec 0.110 Approx tested spec: 0.101
Dynamic Coeficient vs Load	Pass	Fail: Tested coef. approx 0.005 below min at start and below 0.002 at end of test	Fail - Tested coef. approx 0.007 below min at start and below 0.004 at end of test	Fail - Tested coef, approx 0.02 below min at start and below 0.005 at end of test	Fail - Tested coef. approx 0.004 below min at start and marginally below at end of test	Fail - Tested coef. approx 0.015 below at start and 0.005 at end of test
Dynamic Coeficient vs Speed	Fail - Coef within limits at start of test, falls below min limit at approx 21 m/s	Fail - Coef, below limits at start of test and steadily decreases. Coef, begins to increase after 25 m/s, but still below spec	Fail - Coef. below limits at start of test and steadily decreases.	Fail - Coef below limits at start of test and steadily decreases	Fail - Coef below limits at start of test and steadily decreases	Fail - Coef below limits at start of test and steadily decreases
Energy Limit	Pass	Pass	Pass	Pass	Pass	Pass
Static Coeficient vs Load	Fail - Approx min coef 0.150 Approx tested coef: 0.135	Fail - Coef. below limits at start of test, Coef. meets limits after approx 1400 kPa	Fail - Approx min coef: 0.150 Approx tested coef: 0.140	Fail - Approx min coef: 0.150 Approx tested coef: 0.130	Fail - Approx min coef: 0.150 Approx tested coef: 0.140	Fail - Approx min coef: 0.150 Approx tested coef: 0.134
Static Coeficient vs Speed	Fail - Coef. at start below min limit and steadily decreases through out test	Fail - Borderline below spec until after 25 m/s	Fail - Coef. below limits for approx first half of test, meets limits at approx 24 m/s	Fail - Coef. below limits at start of test. Coef. increases at approx 22 m/s but remains below limits through duration of test	Fail - Coef. below limits at start of test, meets limits at approx 23 m/s	Fail - Coef below limits at start of test. Coef. increases at approx 25 m/s but remains below limits through duration of test
Energy Limit	Pass	Pass	Pass	Pass	Pass	Pass
Total Wear	0.044	0.022	0.035	0.032	0.037	0.033
Wear Limit	0.070	0.07	0.070	0.070	0.070	0.070
Caterpillar TO-4	27637-L	AL-27252-L	AL-27793-L	AL-27875-L	AL-27876-L	AL-27877-L
SEQ 1224 (Elastomeric)	Test No. VC70-A-77-I	Test No. VC70-A-70-I	Test No. VC70-A-84-I	Test No. VC70-A-85-1	Test No. VC70-A-86-1	Test No. VC70-A-75-I
	Date Requested: 7/17/2007	Date Requested: 7/17/2007	Date Requested: 8/2/2007	Date Requested: 9/13/2007	Date Requested: 9/13/2007	Date Requested: 9/7/2007
	Date Started: 10/7/2007	Date Started: 8/8//07	Date Started: 11/8//07	Date Started: 11/16//07	Date Started: 11/24/2007	Date Started: 9/27/2007
	Date Finished - 10/11/2007*	Date Finished: 8/13/2007 *	Date Finished: 11/15/2007 *	Date Finished: 11/20/2007 *	Date Finished: 11/28/2007*	Date Finished: 10/2/2007*
Dynamic Coeficient vs Cycle	Fail - Coef. within limits at start of test, falls below min limit near end at approx 450 cycles	Pass	Pass	Fail - Borderline, Coef. slightly below limits at start of test and is satisfactory after approx 180 cycles	Pass	Fail - Borderline, Coef. slightly below limits at start of test and is satisfactory after approx 170 cycles
Dynamic Coeficient vs Load	Fail - Coef. below limits for approx first quarter of test, meets limits after approx 800 kPa	Pass	Pass	Pass	Pass	Fail - Borderline, Coef. slightly below limits during middle of test (<0.005)
Dynamic Coeficient vs Speed	Pass	Pass	Pass	Pass	Pass	Fail - Borderling, Coef. marginally below at start of test, satisfactory throughout remainder (<0.005)
Energy Limit	Pass	Pass	Pass	Pass	Pass	Pass
Static Coeficient vs Load	Pass	Pass	Pass	Pass	Pass	Pass
Static Coeficient vs Speed	Pass	Fail - Coef within limits until increasing above max value at approx 37 m/s	Fail - Coef within limits until increasing above max value at approx 36 m/s	Fail - Coef. within limits until increasing above max value at approx 38 m/s	Fail - Coef. within limits until increasing above max value at approx 36 m/s	Fail - Coef within limits until increasing above max value at approx 35 m/s
Energy Limit	Pass	Pass	Pass	Pass	Pass	Pass
Total Wear	0.027	0.029	0.011	0.019	0.016	0.000
Wear Limit	0.040	0.040	0.040	0.040	0.040	0.040

Below are some generalizations from the data in shown Table 1 and Table 2 based on sequence number.

<u>Seq. 1219 (Raybestos Elastomeric)</u> – All candidate oils performed in a similar manner. Dynamic coefficient versus load and cycle values were slightly below spec but consistent between all candidate oils. Dynamic coefficient versus speed for all oils was below spec until relative speeds increased to 35-38 m/s. All static coefficients measured within reference fluid ranges.

<u>Seq. 1221 (Steering Brake Paper)</u> – All oils except arctic grades passed within reference oil specs. OEA 30 ME-35 (C) and OEA 30 (New) shared similar failures in the dynamic and static coefficient versus speed measurements.

Seq. 1222 (Wheel Brake Paper) – No failure patterns were identified within this sequence. 5W-40 EO 0067 (E) was the only oil to pass all tests.

<u>Seq. 1223 (Transmission Paper)</u> – All candidate oils performed in a similar manner. OEA 30 ME-35 (C) measured slightly better than other tested grades. Measured coefficient of friction values for dynamic versus load and cycle are slightly below reference oil specs for all remaining oils.

<u>Seq. 1224 (CAT F37 Elastomeric)</u> – All candidate oils with the exception of OEA 30 ME-35 (C) failed in a similar manner. Experimental 5W-40 (L) and OEA 30 (New) had some additional failures from the group, but were borderline in magnitude.

4.1.2 Performance by Viscosity Grade

Below lists the individual comparisons between candidate oils by viscosity grade.

5W-40 EO 0067 (E) and Experimental 5W-40 (L) in TO-4 sequences 1219, 1221-24:

- Seq. 1219 (Raybestos Elastomeric)—Nearly identical failures and error margins.
- Seq. 1221 (Steering Brake Paper)—Both passed all tests

- Seq. 1222 (Wheel Brake Paper)— 5W-40 EO 0067 (E) passed all tests with Experimental 5W-40 (L) falling out of error limits during three tests (static coefficient vs. load, static and dynamic coefficient vs. speed)
- Seq. 1223 (Transmission Paper)—Similar failures for both oils
- Seq. 1224 (CAT F37 Elastomeric)—Nearly identical failures and error margins. Experimental 5W-40 (L) had additional borderline failure of dynamic coefficient vs. cycle

15W-40 EO 0058 (S) and 15W-40 EO 0068 (L) in TO-4 sequences 1219, 1221-24:

- Seq. 1219 (Raybestos Elastomeric)—Nearly identical failures and error margins.
- Seq. 1221 (Steering Brake Paper)—Both oils passed all tests.
- Seq. 1222 (Wheel Brake Paper)— 15W-40 EO 0058 (S) failed dynamic coefficient vs. speed. 15W-40 EO 0068 (L) failed both dynamic coefficient vs. speed and load, with additional borderline failures in dynamic coefficient vs. cycle, and static coefficient vs. load.
- Seq. 1223 (Transmission Paper)—Nearly identical failures and error margins.
- Seq. 1224 (CAT F37 Elastomeric)—Nearly identical failures and error margins

OEA 30 ME-35 (C) and OEA 30 (New) in TO-4 sequences 1219, 1221-24:

- Seq. 1219 (Raybestos Elastomeric)—Nearly identical failures and error margins.
- Seq. 1221 (Steering Brake Paper)—Failures similar with the exception of OEA 30 (New) borderline failure in static coefficient vs. load.
- Seq. 1222 (Wheel Brake Paper)—OEA 30 (New) failed dynamic coefficient vs. speed but OEA 30 ME-35 (C) passed. Both oils failed the static coefficient vs. load test, but OEA 30 (New) failed at a lower 700kPa compared to 1600kPa for the OEA 30 ME-35 (C). Both oils start below limits for static coefficient vs. speed, but OEA 30 (New) increases within limits through test duration while OEA 30 ME-35 (C) remains below.
- Seq. 1223 (Transmission Paper)—OEA 30 (New) failed both dynamic coefficient vs. cycle and load, which OEA 30 ME-35 (C) oil passed. Remainder of failures nearly identical.

• Seq. 1224 (CAT F37 Elastomeric)—OEA 30 (New) did better with all of its failures except one being borderline. OEA 30 (New) failed static coefficient vs. speed after 35 m/s.

SEQ 1220 and FRRET were completed on the Experimental 5W-40 (L) and OEA 30 (New) in accordance to standard mil-spec oil testing requirements. Test results are presented in the same format as previously discussed TO-4 results. See Table 3 below for Seq. 1220 and FRRET results.

		Sequence	Dynamic Coefficient vs. Cycle	Dynamic Coefficient vs. Load	Static Coefficient vs. Load	Dynamic Coefficient vs. Speed	Static Coefficient vs. Speed	Energy Limit [P/CycleNo.]
	AL 27877	1220	FAIL	FAIL	PASS	FAIL	PASS	PASS
OLA 30 (New)	AL2/0//	FRRET			PA	SS		
Experimental	AL_27975	1220	PASS	PASS	PASS	PASS	PASS	PASS
5W-40 (L)	AL-2/0/J	FRRFT			FA	ÁII		

Table 3. Seq. 1220 and FRRET Results

4.2 DEXRON VI

Both arctic oil blends, OEA 30 ME-35 (C) and OEA 30 (New), were tested in Dexron VI friction tests as a basis to compare oil performance when used in automatic transmission applications requiring Dexron approved fluids. These tests included the Dexron VI band clutch, plate clutch, and low speed clutch friction tests. All of these tests are carried out using an SAE No. 2 friction test machine. An SAE No. 2 friction machine is similar in concept to the previously discussed CAT TO-4 test apparatus, whereas rotating clutch disks are engaged into a stationary reaction plate while recording the resulting torque value, clutch rotation speed, and application pressure.

The SAE No. 2 friction test machine can be operated in two different ways. The first option is to bring the clutch disks up to speed using the drive motor, then turning the motor off and engaging the disks to the stationary reaction plate. The second option is to engage the clutch disks to the reaction plate with the motor off, then turning on the motor and recording the static break away torque. The Dexron VI band and plate clutch tests follow the first format, while the low speed clutch test incorporates both formats.

Test results from the Dexron VI friction tests are presented in Table 4. Both oils passed the band and low speed clutch tests with satisfactory performance results meeting the Dexron VI specifications. For the plate clutch friction test, both oils failed to meet the required Dexron VI specifications.

	OEA 30 ME-35 (C) AL-27637	OEA 30 (New) AL-27877-L		
	Test No. BH3-4-164	Test No. BH3-8-169		
DEXRON-VI Band Clutch Eristian	Date Requested: 7/17/2007	Date Requested: 9/7/2007		
Band Clutch Friction	Date Started: 7/30/2007	Date Started: 9/14/2007		
	Date Finished: 8/6/2007*	Date Finished: 9/21/2007 *		
	Pass	Pass		
	AL-27637	AL-27877-L		
	Test No. HC-11-24-80	Test No. HC11-1-82		
DEXRON-VI	Date Requested: 7/17/2007	Date Requested: 9/7/2007		
Plate Clutch Friction	Date Started: 7/30/2007	Date Started: 9/11/2007		
	Date Finished: 8/7/2007*	Date Finished: 9/19/2007 *		
	Fail	Fail		
	AL-27637	AL-27877-L		
	Test No. 12-5-0363	Test No. LS12-5-0374		
DEXRON-VI	Date Requested: 7/17/2007	Date Requested: 9/7/2007		
Low Speed Clutch Friction	Date Started: 7/30/2007	Date Started: 9/10/2007		
	Date Finished: 7/31/2007*	Date Finished: 9/11/2007 *		
	Pass	Pass		

 Table 4. Dexron VI Friction Test Results

Similar to CAT TO-4 testing, further investigation was needed to quantify the oils relative performance. It was found that the low speed clutch failures were due to both oils not meeting the specified maximum torque of >90 Nm required by the plate clutch friction test. From the test results, it was found that both oils maintained a steady range of maximum torque, with values falling between 85-88 Nm. Although this torque value lies below the specifications set forth by the Dexron VI standards, it should be adequate to ensure functionality and durability when used in military equipment. Analysis of the torque capacity plots versus speed and clutch pressure shows the oils tested do not have any undesirable characteristics. Over the duration of testing, the overall clutch performance does not change with steady maximum torque values and a smooth transition from dynamic to static friction as the speed approaches zero. If the plots were to have shown substantial variation of the maximum torque measured throughout the test duration, or large torque spikes during the dynamic to static transition, the use of these oils could be

problematic. Neither of the tested oils displays these negative characteristics and should be considered capable to adequately perform in drivelines requiring the Dexron VI rated fluids.

4.3 JOHN DEERE JDQ-96

The John Deere JDQ-96 test procedure is used to determine brake noise (or chatter) and capacity of an immersed brake system provided by a candidate oil compared to a baseline reference oil. Testing is carried out using a John Deere 1400 series industrial axle powered by a full sized modified John Deere 4640 tractor. The sun pinion shaft is equipped with strain gauges to measure dynamic torque changes throughout a total of 30,000 braking cycles. Chatter tests are run after 1,000, 10,000, 20,000, and 30,000 braking cycles. Torque data is acquired for a variety of axle speeds and loads. Chatter is evaluated over 32°, 49°, 60°, and 71°C fluid temperatures with varying brake application pressures and wheel speeds.

Each candidate oil was subjected to the first 1,000 cycles of the standard 30,000-cycle test. Results are presented in Table 5. Torque variation is defined as the greatest difference between the maximum and minimum torque over a 0.2 second portion of the engagement event. SwRI torque variation is defined as the sum of all the differences between the maximum and minimum torque for each engagement. Relative capacity is the average torque value during the middle of an engagement.

	Reference Oil Range	OEA 30 ME-35 (C) AL-27637-L	OEA 30 (New) AL-27677-L
Torque Variation	59,000-100,00 Nm	85,000 Nm	158,000 Nm
SwRI Tq. Variation	750,000-1,250,000 Nm	1,115,000 Nm	2,200,000 Nm
Relative Capacity	330,000-350,000 Nm	365,000 Nm	345,000 Nm
Disk Thickness	Approx 7.5 mm	In Spec	In Spec
	Reference Oil Range	5W-40 EO 0067 (E) AL-27252-L	Experimental 5W-40 (L) AL-27875-L
Torque Variation	59,000-100,00 Nm	205,000 Nm	180,000 Nm
SwRI Tq. Variation	750,000-1,250,000 Nm	2,600,000 Nm	2,150,000 Nm
Relative Capacity	330,000-350,000 Nm	370,000 Nm	350,000 Nm
Disk Thickness	Approx 7.5 mm	In Spec	In Spec
	Reference Oil Range	15W-40 EO 0058 (S) AL-27793-L	15W-40 EO 0068 (L) AL-27876-L
Torque Variation	59,000-100,00 Nm		200,000 Nm
SwRI Tq. Variation	750,000-1,250,000 Nm	DNF-Testing stopped	2,500,000 Nm
Relative Capacity	330,000-350,000 Nm	chatter	335,000 Nm
Disk Thickness	Approx 7.5 mm	chatter	In Spec

 Table 5. John Deere JDQ-96 Test Results

Since testing only included the first 1,000 cycles of the standard JDQ test, all oils met the standard set by the reference oil for disk thickness. (*Note – The JDQ96 test with oil 15W-40 EO 0058 (S) was terminated early due to excessive chatter. Further investigation is needed to determine overall compatibility with equipment requiring fluids that meet JDQ96 specifications)

4.4 ALLISON C4

Similar to the Dexron VI friction tests, the Allison C4 paper and graphite high-energy friction tests are carried out in an SAE No.2 Friction Test Machine. This testing was carried out on the OEA 30 (New) fluid only. A pass-fail criterion for each fluid is based on a maximum allowed slip time and a minimum mid-point coefficient of friction value. Results for the OEA 30 (New) are presented in Table 6. The OEA 30 (new) passed both the paper and graphite tests.

Allison C4 Paper Test						
Property Spec Result @ Result @ P/F						
Slip Time (Max)	0.600	0.530	0.460	Р		
Mid-Point Fric. Coef. (Min)	0.085	0.095	0.110	Р		

Table 6. Allison C4 Friction Test (Graphite & Paper), OEA 30 (new)

Allison C4 Graphite Test						
Property	Spec	Result @ 100N	Result @ 10,000N	P/F		
Slip Time (Max)	0.81	0.73	0.78	Р		
Mid-Point Fric. Coef. (Min)	0.093	0.101	0.097	Р		

5.0 CONCLUSIONS

In addition to engine crankcase applications, a multifunctional lubricant must be capable of being used in military automatic/powershift transmission applications. To assess the feasibility of a SCPL, several engine oils were evaluated in industry standard transmission test procedures including selected: Allison C4, Caterpillar TO-4, and John Deere JDQ test procedures. Many of these industry transmission frictional tests utilize an SAE No. 2 friction testing machine. This machine measures the engagement properties of friction and reaction plates and test fluid over a wide range of speeds and application forces. It instantaneously records multiple parameters

including load applied, torque transmitted, and plate speed to determine overall torque capacity, dynamic and static coefficients of friction, and slip time. Results are then compared to a baseline fluid which brackets desired performance and determines pass or fail of a candidate fluid.

While the engine oils tested resulted in a mixture of passing and failing results, overall the performance was generally favorable. The most difficult requirement for any multifunctional oil is compatibility with the large variety of friction materials being used in transmission applications. The level of friction developed between the friction material and reaction plates determines the feel of the shift (i.e., harshness) and amount of torque that can be transmitted without the clutch slipping. Clutch damage can occur if the coefficient of friction between the friction material and the reaction plate is too low. Low friction during a clutch engagement results in long slip times and excessive heat buildup which can cause deposit formation on the friction and reaction plate surfaces (i.e., glazing). If the friction is too high, the result will be very short, abrupt shifts. Passenger car ATFs use friction modifiers to ensure smooth shifts. The downside of friction modification is that it can reduce the clutch holding capacity. Given the large mass and high torque of heavy-duty equipment, heavy-duty automatic/powershift transmission fluids are typically not friction modified. In fact, it is more typical to look for ways to maximize the friction in these transmissions. Formulators of multifunctional oils like those developed for military use must choose a formulation strategy that does not result in excessively low dynamic and static coefficients of friction.

The testing matrix consisted of 6 engine oils that were evaluated in 5 Caterpillar TO-4 test sequences (1219, 1221, 1222, 1223, and 1224). One arctic oil and an SAE 5W40 oil were tested in Caterpillar Sequence 1220 and FRRET. Six engine oils were tested for 1000 cycles of the JDQ-96 procedure. Two arctic engine oils were evaluated for friction performance by Dexron VI methods. Finally, one of the arctic engine oils was tested against the friction retention requirements of Allison C4 Paper and Graphitic materials. The summarized results were:

- None of the engine oils evaluated was able to pass all of the TO-4 requirements for sequences 1219, 1221, 1222, 1223, and 1224.
- All engine oils passed the wear limits of sequences 1219, 1221-1224.

- All engine oils passed the static friction requirements of sequence 1219.
- Oil E, SAE 5W40, passed all requirements for sequences 1221 and 1222.
- Except for the two arctic engine oils, all engine oils passed sequence 1222.
- Most engine oils failed all friction requirements of sequence 1223.
- Overall, TO-4 performance of engine oils could not be predicted by viscosity alone.
- Oil S, SAE 15W40, was not able to complete the initial 1000 cycles of JDQ-96 test. The test was terminated early because of excessive brake chatter.
- The two arctic oils passed the band clutch friction and low speed clutch friction of Dexron VI. Their clutch plate friction was stable, but slightly below the maximum required by Dexron VI.
- Oil OEA 30 (new) failed sequence 1220 and passed FRRET.
- Oil L (SAE 5W40) passed sequence 1220 and failed FRRET.
- Oil OEA 30 (new) passed the Allison C4 friction tests, both paper and graphite.

Overall, the friction bench tests indicate that use of engine oils in military automatic/ powershift transmission applications is technically feasible as evidenced by passing or near passing results with the slate of engine oils tested. This means it is feasible to combine diesel engine performance and military automatic/ powershift transmission performance in an SCPL.

6.0 **REFERENCES**

- MIL-PRF-2104J, "Lubricating Oil, Internal Combustion Engine, Combat/Tactical Service", 11 February 2014.
- [2] MIL-PRF-46167D, "Lubricating Oil, Internal Combustion Engine, Arctic", 27 January 2005.
- [3] TO-4, Caterpillar Inc. Transmission and Drivetrain Fluid Requirements, 23 June 2005.

APPENDIX A

SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

FUELS AND LUBRICANTS RESEARCH DIVISION

Report on

CATERPILLAR TO-4 FRICTION PROPERTIES, VC-70

Conducted for

ARMY LAB

Oil Code: AL-27252-L

Test Number: VC70-A-70-I

August 13, 2007

Submitted by:

2ale

Brian Koehler Principal Engineer Specialty & Driveline Fluids Evaluations



The results of this report relate only to the items tested. This report shall not be reproduced, except in full, without the written approval of Southwest Research Institute®.



Summary Sheet

Test start date: End of test date: Oil Code:August 8, August 13 AL-27252Sequence Number1219Dynamic Coefficient Vs. Cycle:FDynamic Coefficient Vs. Load:FDynamic Coefficient Vs. Speed:FEnergy Limit:PStatic Coefficient Vs. Cycle:PStatic Coefficient Vs. Load:P	2007 3, 2007 2-L N/A <u>N/A</u> <u>N/A</u>	1221 Р Р Р	1222 Р Р Р	1223 F F F	1224 P P	Friction Retention
Sequence Number1219Dynamic Coefficient Vs. Cycle:Dynamic Coefficient Vs. Load:Dynamic Coefficient Vs. Speed:Dynamic Coefficient Vs. Speed:Dynamic Coefficient Vs. Speed:Dynamic Coefficient Vs. Speed:Dynamic Coefficient Vs. Speed:Dynamic Coefficient Vs. Speed:Energy Limit:Static Coefficient Vs. Cycle:Static Coefficient Vs. Load:	N/A N/A N/A N/A	1221 P P	1222 Р Р	1223 F F	1224 	Friction Retention
Dynamic Coefficient F Static Coefficient P Static Coefficient Vs. Cycle: Static Coefficient Vs. Load:	N/A N/A N/A	Р Р	P P	F F	P P P	N/A
Dynamic Coefficient Vs. Load:FDynamic Coefficient Vs. Speed:FEnergy Limit:PStatic Coefficient Vs. Cycle:Static Coefficient Vs. Load:	N/A N/A N/A	P P	Р Р	F	P	
Dynamic Coefficient F Vs. Speed: F Energy Limit: P Static Coefficient Vs. Cycle: Static Coefficient Vs. Load:	N/A N/A	Р	<u>Р</u>	F	P	
Energy Limit: P Static Coefficient	<u>N/A</u>	P	P			
Static Coefficient Vs. Cycle: Static Coefficient Vs. Load: <u>P</u>				P	P	
Static Coefficient Vs. Load:P						N/A
Vs. Load: P						
	N/A	P	P	F	P	
Static Coefficient Vs. Speed:P	N/A	P	P	F	F	
Energy Limit: P	N/A	P	P	P	P	
Total Wear: 0.026	N/A	0.037	0.039	0.022	0.029	
Wear Limit: 0.030	N/A	0.070	0.070	0.070	0.040	
Comments: The limit lines shown in	n anab a	equences'	report were	generated us	ing the CAT	single grade
reference oil.	n each s			<u> </u>		

F = Fail

P = Pass N/A = Not Applicable

SOUTHWEST RESEARCH INSTITUTE I MACHINE OIL TEST AL-27252-L / LO-222424

Test name: A-70-I Test date: 08/8/07 Test description: AL-27252-L Oil type: AL-27252-L LO-222424 Viscosity: SAE 5W-40 Miscellaneous: Software version: 1.40 Run name & desc: I0706076 - AL-27252-L Run date: 08/08/07 Oil temperature: 82 degrees C Oil flow rate: 3.78 liter/minute Operator: HC Remarks: "I" MACHINE OIL TEST AL-27252-L / LO-222424 Sequence name: SE01219 Remarks: Use 1Y0708 Disc and 1Y3610 Plate Number of cycles run: 1080 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 1.0288 N-m-s² Result: Disc name & desc: 1Y0708 - Elastomeric Disc Material: Raybestos 6475-4 Rayflex Groove pattern: Single Lead Spiral - 12 Radial Miscellaneous: Use with 1Y3610 Steel Plate Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm): 128.21 Batch number: 14JA1-00005 Remarks: ELASTOMERIC Plate name & desc: 1Y3610 - Steel Plate Surface: 0.70 to 1.30 micron Roughness Miscellaneous: Install the side marked with the average roughness Batch number: 14JA1-00005 Remarks: 0.86 SURFACE FINISH Report limit name: LIM1219 - Reference run: I0706001 Limit file generated: 07/26/06 Report format name: REP1219 - ELASTOMERIC, RAYFLEX



1Y0708 DISC THICKNESS

	Oute	r Diam	eter	Inne	r Diam	eter
Loc	Ml	M2	M3	M1	M2	MЗ
1	4.98	4.97	4.96	4.98	4.97	4.96
2	4.98	4.97	4.96	4.98	4.97	4.96
3	4.98	4.97	4.96	4.99	4.97	4.96
4	4.98	4.96	4.95	4.98	4.96	4.95
5	4.98	4.96	4.95	4.98	4.96	4.95
6	4.98	4.96	4.95	4.98	4.96	4.95
Avg	4.98	4.96	4.96	4.98	4.96	4.96
	Compression set average wear: 0.016 M2 - M3 average Wear: 0.010					

Total Wear (all measurements in mm): 0.026





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Test name: A-70-I Test date: 08/8/07 Test description: AL-27252-L Oil type: AL-27252-L LO-222424 Viscosity: SAE 5W-40 Miscellaneous: Software version: 1.40 Run name & desc: I0706078 - AL-27252-L Run date: 08/09/07 82 degrees C Oil temperature: Oil flow rate: 3.78 liter/minute Operator: HC "I" MACHINE OIL TEST AL-27252-L / LO-222424 Remarks: Sequence name: SEQ1221 Remarks: Use 1Y0710 Disc and 1Y3610 Plate. Number of cycles run: 1057 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0710 - Steering Brake Paper Material: Raybestos 7894-4 Paper Groove pattern: 2 - 37 Multiple Parallel Use with 1Y3610 Steel Plate Miscellaneous: Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm): 128.21 Batch number: 23MR9-00001 Remarks: STEERING BRAKE PAPER Plate name & desc: 1Y3610 - Steel Plate Surface: 0.70 to 1.30 micron Roughness Miscellaneous: Install the side marked with the average roughness Batch number: 23MR9-00001 Remarks: 0.98 SURFACE FINISH Report limit name: LIM1221 - Reference run: I0706003 Limit file generated: 07/26/06 Report format name: REP1221 - STEERING BRAKE PAPER



1Y0710 DISC THICKNESS

	Oute	r Diam	eter	Inne	r Diam	eter
Loc	Ml	M2	MЗ	M1	M2	M3
1	5.04	5.01	5.00	5.04	5.01	5.00
2	5.04	5.01	5.00	5.04	5.01	5.00
3	5.03	5.01	5.00	5.03	5.01	5.00
4	5.03	5.00	4.99	5.03	5.00	4.99
5	5.03	5.01	4.99	5.03	5.00	4.99
6	5.02	5.00	4.99	5.02	5.00	4.99
Avg	5.03	5.01	4.99	5.03	5.01	4.99
	Compre	ession	set avera	ge wea	r: 0.	026

М2 average Wear: 11 MЗ 0.0

Total Wear (all measurements in mm): 0.037




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SOUTHWEST RESEARCH INSTITUTE I MACHINE OIL TEST AL-27252-L / LO-222424

Test name: A-70-I Test date: 08/8/07 Test description: AL-27252-L AL-27252-L LO-222424 Oil type: Viscosity: SAE 5W-40 Miscellaneous: Software version: 1.40 Run name & desc: I0706079 - AL-27252-L Run date: 08/10/07 Oil temperature: 82 degrees C Oil flow rate: 3.78 liter/minute HC Operator: Remarks: "I" MACHINE OIL TEST AL-27252-L / LO-222424 Sequence name: SE01222 Remarks: Use 1Y0711 Disc and 1Y0726 Plate Number of cycles run: 1155 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0711 - Wheel Brake Paper Material: Raybestos 7902-1 Paper Groove pattern: 2 - 37 Muicipie Ideal Use with 1Y0726 Steel Plate 2 - 37 Multiple Parallel Miscellaneous: Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm): 128.21 Batch number: 24FE9-00001 Remarks: WHEEL BRAKE PAPER Plate name & desc: 1Y0726 - Steel Plate Surface: 0.30 micron Maximum Roughness Miscellaneous: Install the side marked with the average roughness Batch number: 24FE9-00001 Remarks: 0.23 SURFACE FINISH Report limit name: LIM1222 - Reference run: I0706004 Limit file generated: 07/26/06 Report format name: REP1222 - WHEEL BRAKE PAPER



1Y0711 DISC THICKNESS

	Oute	er Diam	neter	Inne	r Diam	neter	
Loc	Ml	M2	M3	Ml	M2	MЗ	
1	5.00	4.96	4.95	5.00	4.96	4.95	
2	4.99	4.96	4.95	4.99	4.96	4.95	
3	5.00	4.97	4.96	4.99	4.97	4.96	
4	5.00	4.97	4.96	5.00	4.97	4.96	
5	4.98	4.94	4.94	4.98	4.95	4.94	
6	4.97	4.95	4.94	4.97	4.94	4.94	
Avg	4.99	4.96	4.95	4.99	4.96	4.95	
	Compr M2 -	ression M3 ave	set av rage We	erage wea: ar: 0.00	r: 0. 8	031	
	Total We	ar (al	1 measu:	rements in	n mm):	0.039	9

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SOUTHWEST RESEARCH INSTITUTE I MACHINE OIL TEST AL-27252-L / LO-222424

Test name: A-70-I Test date: 08/8/07 Test description: AL-27252-L Oil type: AL-27252-L LO-222424 Viscosity: SAE 5W-40 Miscellaneous: Software version: 1.40 Run name & desc: 10706080 - AL-27252-L Run date: 08/11/07 Oil temperature:82 degrees COil flow rate:3.78 liter/minute Operator: $_{
m JG}$ "I" MACHINE OIL TEST AL-27252-L / LO-222424 Remarks: Sequence name: SEQ1223 Remarks: Use 190 Use 1Y0712 Disc and 1Y0726 Plate Number of cycles run: 1040 Machine: Ι Coast down check run: 07/19/02 151.76 seconds Result: Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0712 - Transmission Paper Material:Raybestos 7901-2 PaperGroove pattern:2 - 37 Multiple ParallelMiscellaneous:Use with 1Y0726 Steel Plate Material: Raybestos 7901-2 Paper Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm): 128.21 Batch number: 27MR9-00001 Remarks: TRANSMISSION PAPER Plate name & desc:1Y0726 - Steel PlateSurface:0.30 micron Maximum RoughnessMiscellaneous:Install the side marked with the average roughnessBatch number:27MR9-00001Pemarks:0.18 SURFACE FINISH Report limit name: LIM1223 - Reference run: I0706006 Limit file generated: 07/26/06 Report format name: REP1223 - TRANSMISSION PAPER



1Y0712 DISC THICKNESS

	Outer	r Diame	eter	Inne	r Diame	eter
Loc	Ml	M2	M3	Ml	M2	M3
1	5.04	5.02	5.02	5.04	5.03	5.02
2	5.04	5.02	5.01	5.03	5.02	5.01
3	5.02	5.01	5.00	5.02	5.01	5.00
4	5.02	5.01	5.00	5.02	5.01	5.00
5	5.02	5.01	5.00	5.02	5.01	5.00
6	5.03	5.02	5.00	5.02	5.02	5.00
Avg	5.03	5.01	5.00	5.03	5.02	5.00
	Compre	ession	set averag	ge wear	c: 0.0	011

M2 - M3 average Wear: 0.011

Total Wear (all measurements in mm): 0.022





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Test name: A-70-I Test date: 08/8/07 Test description: AL-27252-L Oil type: AL-27252-L LO-222424 Viscosity: SAE 5W-40 Miscellaneous: Software version: 1.40 Run name & desc: 10706081 - AL-27252-L Run date: 08/13/07 Oil temperature: 82 degrees C Oil flow rate: 3.78 liter/minute Operator: JG I MACHINE OIL TEST AL-27252-L / LO-222424 Remarks: Sequence name: SEQ1224 Use 1Y0713 Disc and 8E4095 Plate Number of cycles run: 1093 Machine: Ι Coast down check run: 07/19/02 151.76 seconds Result: Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0713 - Elastomeric Disc Caterpillar F37 Material: Single Lead Spirar Use with 8E4095 Steel Plate Single Lead Spiral - 12 Radial Groove pattern: Miscellaneous: Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm): 128.21 Batch number: C63007FE1 Remarks: ELASTOMERIC Plate name & desc: 8E4095 - Steel Plate Surface: 0.70 to 1.00 micron Roughness Miscellaneous: Install the side marked with the average roughness Batch number: C63007FE1 Remarks: 0.82 SURFACE FINISH Report limit name: LIM1224 - Reference run: I0706007 Limit file generated: 07/26/06 Report format name: REP1224 - ELASTOMERIC, F37



1Y0713 DISC THICKNESS

	Ou	ter Diar	neter	Inne	r Diam	leter	
Loc	Ml	M2	МЗ	M1	M2	MЗ	
1	5.0	6 5.04	5.03	5.06	5.04	5.03	
2	5.0	6 5.04	5.03	5.06	5.04	5.03	
3	5.0	5 5.04	5.03	5.06	5.04	5.03	
4	5.0	6 5.04	5.03	5.06	5.04	5.03	
5	5.0	6 5.04	5.03	5.06	5.04	5.03	
6	5.0	6 5.04	5.03	5.06	5.04	5.03	
Avg	5.0	6 5.04	5.03	5.06	5.04	5.03	
	Comj M2	pression - M3 ave	n set av erage We	verage wea ear: 0.01	r: 0. 0	019	
	Total N	Wear (al	l measu	rements i	n mm):	0.02	9





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SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

Fuels and Lubricants Research Division

Report on

John Deere JDQ-96 Performed using 1400 Series Axle

Conducted for

ARMY LAB

AL-27252-L

Test Number 07804

October 11, 2007

Submitted by:

Michael D. Lochte Manager Specialty & Driveline Fluids Evaluations



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John Deere JDQ-96 Performed using 1400 Series Axle

General Information

Oil Code: AL-27252-L	E.O.T. Date: October 11, 2007
	· · · · · · · · · · · · · · · · · · ·

Purpose

The purpose of this test was to evaluate the anti-chatter properties of this oil on the brakes of a 1400 series John Deere Inboard Planetary Axle.

Test Procedure

The test was performed as specified by John Deere Product Engineering. The only changes made to the Deere procedure were those necessary to compensate for a different spiral bevel gear ratio. This procedure is proprietary to Deere and Company.

Data Interpretation

The capacity for each engagement is the average torque during the middle of the engagement. The torque variation is the greatest difference between the maximum and minimum torque recorded during any 0.2-second portion of the engagement. The SwRI variation is the sum of all differences between the maximum torque and minimum torque for each engagement. It is obtained by summing all torque variations of each 0.2-second time block of all engagements.

Test Number

The run number listed on this report is a random number and is not sequential. Only SwRI® can link this run number to JDQ-96, AL-27252-L, October 11, 2007.



John Deere JDQ-96 Performed using 1400 Series Axle

Results

Oil Code: AL-27252-L	E.O.T. Date: October 11, 2007

The candidate results can be compared to the baseline reference average. Pass or fail decisions are only made by John Deere Product Engineering. The current reference baseline average is the average of the five most recent tests.

Current Reference Baseline Average (N · m)											
	1,000 Cycles	10,000 Cycles	20,000 Cycles	30,000 Cycles	TOTAL						
Relative Capacity	338,535	338,534	341,629	343,274	1,361,972						
Torque Variation	79,214	84,272	79,152	74,708	317,346						

Results From Test Candidate AL-27252-L											
	1,000 Cycles	10,000 Cycles	20,000 Cycles	30,000 Cycles	TOTAL						
Relative Capacity	369,909										
Torque Variation	206,360										

Tables 1 of the Appendix contains chatter test results from 1,000cycles. Table 2 contains results of the five current baseline reference tests. Figures 1 through 4 are graphic presentations of candidate oil performance compared to baseline reference data.

Figure 5 is a graphic presentation of 1000-cycle reference results and AL-27252-L. Table 3 contains the history of reference tests.

Oil Code: AL-27252-L

E.O.T. Date: October 11, 2007

Appendix

Tables

- 1. Table 1 Durability results 1,000 cycles Candidate Oil
- Table 2 Reference Data Compared to Candidate Data
 Figure 1 & Figure 2 Torque Variation Chart
- 4. Figure 3 & Figure 4 Relative Capacity & Average Disk Thickness Chart
- 5. Figure 5 Graphic presentation of 1000 cycle reference results & Candidate
- 6. Table 3 History of reference tests

October 11, 2007

TABLE 1: JDQ-96 DURABILITY TEST RESULTS 1,000 CYCLES

SwRI Oil Code

LO-222424

Sponsor Oil Code AL-27252-L

	1	T	T																· · · ·			
	0	Temp.	72	20	69	72	72	72	72	73	72	72	73	72	71	20	70	70	71	71	20	71
	il Temp. 71°	Variation	2670	4190	3140	3810	4630	2080	1940	2290	1970	2220	2770	2090	980	1320	2820	3140	3750	6100	6240	. 6540
(1		Torque	4992	4670	4381	4595	4344	4655	4545	4681	4477	4443	4738	4477	1897	2728	3403	4406	5543	6434	7383	8528
TION in Nr		Temp.	61	60	59	59	60	60	61	61	61	61	59	60	61	59	60	60	59	59	59	59
and VARIA	I Temp. 60°(Variation	3320	2780	3420	3880	4250	1920	1740	2190	1860	2110	1870	1530	006	1070	2950	3050	3340	3770	4100	6640
S (TORQUE	Ō	Torque	4689	4545	4310	4234	4161	4453	4453	4572	4357	4397	4470	4341	1846	2725	3397	4386	5359	6319	7262	8285
ST RESULT	0	Temp.	50	49	49	49	50	50	51	51	50	51	50	51	50	49	49	49	49	49	49	49
RIATION TE	il Temp. 49°(Variation	2190	2360	2890	3320	1460	1770	1610	1740	1420	1570	1490	1380	740	950	2750	3080	3080	3260	4410	5690
TORQUE VA	0	Torque	4398	4622	4230	4231	4492	4492	4447	4523	4240	4215	4396	4290	1800	2684	3245	4257	5189	6182	7274	8302
•	0	Temp.	29	29	29	29	29	30	31	31	33	32	32	33	34	33	33	33	33	33	33	33
	Dil Temp. 32°(Variation	3620	2550	2920	1090	1060	1330	1210	1420	1310	1070	960	1050	580	700	750	2810	3070	3120	3440	3760
	U	Torque	4083	4281	4233	4325	4358	4398	4389	4497	4434	4079	4251	4230	1786	2657	3545	4248	5158	6142	7152	8280
Brake	Press.	(kPa)	3831	3831	3831	3831	3831	3831	3831	3831	3831	3831	3831	3831	1532	2300	3065	3831	4598	5364	6130	7050
Axle	Speed	(rpm)	ω	10	15	20	25	30	35	40	45	50	55	60	15	15	15	15	15	15	15	15

11 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			
	Relative	Torque	SwRI
Temp	Capacity	Variation	Variation
(°C)	(MM)	(MM)	(MM)
32	90,524	37,820	557,440
49	91,506	47,160	649,060
60	92,561	56,690	728,540
71	95,319	64,690	774,330
TOTAL	369,909	206,360	2,709,370

TABLE 2: JDQ-96 REFERENCE DATA COMPARED TO CANDIDATE DATA

EOT Date: October 11, 2007 Oil Code : AL-27252-L

Reference Oil Coded : 692	X31111i			-	Average Facing
	Cycles	Relative Capacity	Torque Variation	SwRI Variation	Thickness
First Reference Run					(millimeters)
	1,000	326,304	57,420	730,050	7.60
	10,000	331,809	64,900	804,030	7.50
	20,000	345,325	69,500	899,880	7.44
	30,000	341,770	66,210	810,190	7.39
	Total	1,345,208	258,030	3,244,150	
Second Reference Run					
	1,000	337,791	66,660	848,580	7.60
	10,000	338,055	92,240	1,129,330	7.55
	20,000	343,166	77,010	1,001,920	7.49
	30,000	350,470	73,280	863,980	7.44
	Total	1,369,482	309,190	3,843,810	
Third Reference Run					
	1,000	339,375	100,390	1,204,240	7.56
	10,000	335,754	106,780	1,079,450	7.52
	20,000	334,120	84,770	1,030,270	7.49
	30,000	335,614	79,620	1,021,190	7.47
	Total	1,344,863	371,560	4,335,150	
Fourth Reference Run					
Run on new backing pla	1,000	343,906	79,990	1,020,120	7.48
and piston	10,000	343,056	72,520	893,570	7.30
	20,000	342,668	69,920	885,870	7.07
	30,000	345,315	70,360	833,920	6.90
	Total	1,374,945	292,790	3,633,480	
Invalid test run on same	1,000	348,860	132,110	1,721,010	
backing plate and pistor	10,000	323,093	153,860	1,919,720	
as test above was run on					
Fifth Reference Run	4 000	0.45.000			
most recent run	1,000	345,296	91,610	1,125,260	7.50
Run on new backing	10,000	343,999	84,920	1,019,400	7.33
plate and piston	20,000	342,864	94,060	1,264,070	7.22
	30,000 Total	343,201	84,070	1,052,400	7.11
AL 07050 L	Total	1,375,360 Condidate (300,160	4,461,130	
AL-2/232-L	1 000			0 700 070	
	1,000	309,909	206,360	2,709,370	
	10,000				
	20,000				
	30,000	200.000	000 000	0 700 070	
	Total	369,909	206,360	2,709,370	









Figure 3

AL-27252-L

Table 3

October 11, 2007

History of 1000 cycle reference tests.

	То	rque variation at 1000 cycles
69X31111k	1999 brake disk	103,360
69X31111k	1997 brake disk	129,540
69X31111k	2000 brake disk	121,120
69X31111k	2000 brake disk	129,620
69X31111K	2000 brake disk	135,700
69X31111k	2000 Drake disk	138,760
69X31111k	2000GDD brake di	140,830
69X31111k	2000GDD brake	124 310
69X31111k	2000 GDD brake	131 860
69X31111k	2000 GDD brake	105,000
69X31111k	2000 GDD brake	109.220
69X31111k	2000 GDD brake	142,510
69X31111k	2000 GDD brake	128,080
69X31111k	2000 GDD brake	109,100
69X31111k	2000 GDD brake	111,800
69X31111k	2000 GDD brake	90,070
69X31111k	2000 GDD brake	90,810
60Y21111k	2000 GDD brake	79,930
60Y31111k	2000 GDD brake	79,930
69X31111k	2000 GDD brake	81 220
69X31111k	2000 GDD brake	85 570
68X31111k	2000 GDD brake	64 170
69X31111k	2000 GDD brake	67.390
69X31111k	2000 GDD brake	82.410
69X31111k	2000 GDD brake	96,730
69X31111k	2000 GDD brake	90,390
69X31111K	2000 GDD brake	99,960
69X31111k	2000 GDD brake	87,380
69X31111k	2000 GDD brake	74,720
69X31111k	2000 GDD blake	74,940
69X31111k	2000 GDD brake	03,900
69X31111k	2000 GDD brake	74.300
69X31111k	2000 GDD brake	90.950
69X31111k	2000 GDD brake	83.190
69X31111k	2000 GDD brake	105,210
69X31111k	2000 GDD brake	91,960
69X31111k	2000 GDD brake	97,320
69X31111k	2000 GDD brake	75,040
69X31111k	2000 brake disk	86,060
69X31111k	2000 brake disk	68,590
69X31111K	2003 brake disk	57,420
60Y31111k	2003 brake disk	60,330
69X31111k	2003 brake disk	76,260
69X31111k	2003 brake disk	80,210 84 EEO
69X31111k	2003 brake disk	66,660
69X31111k	2003 brake disk	84 760
69X31111k	2003 brake disk	87.800
69X31111k	2003 brake disk	100.390
69X31111k	2003 brake disk	96,620
69X31111k	2003 brake disk	106,710
69X31111k	2003 brake disk	123,110
69X31111k	NEW BACKING PI	79,990
69X31111k		98,440
69X31111k		106,370
69X31111K		110,040
097311118		127,550
09731111K 698311112	invalid nun	122 140
UUNITHK		132,110
607311114	NEW BACKING	04 040
USASTITIK	mate and piston	91,010
607344446	NEW BACKING	00.000
09X31111K	Plate and piston	92,230
602311116	plate used for 1	90.000
UUAUTIIK	same brake nlate	09,200
	and piston as	
AL-27252-L	above	206,360





Figure 5

SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

FUELS AND LUBRICANTS RESEARCH DIVISION

Report on

CATERPILLAR TO-4 FRICTION PROPERTIES, VC-70

Conducted for

SwRI ARMY LAB

Oil Code: AL-27637-L

Test Number: VC70-A-77-I

October 11, 2007

Submitted by: Brian Koehler

Principal Engineer Specialty & Driveline Fluids Evaluations



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CATERPILLAR TO-4 FRICTION PROPERTIES, VC-70



Summary Sheet

Company: Test Number: Test start date: End of test date: Oil Code:	SwRI A VC70-A Octobe Octobe AL-276	rmy Lab \-77-I r 7, 2007 r 11, 2007 37-L					
Sequence Number	1219	N/A	1221	1222	1223	1224	Friction Retention
Dynamic Coefficient Vs. Cycle:	F	N/A	P	P	P	F	N/A
Dynamic Coefficient Vs. Load:	F	<u>N/A</u>	P	P	P	F	
Dynamic Coefficient Vs. Speed:	F	N/A	F	P	F	P	
Energy Limit:	P	N/A	P	P	P	Р	
Static Coefficient Vs. Cycle:							N/A
Static Coefficient Vs. Load:	P	N/A	P	F	F	P	
Static Coefficient Vs. Speed:	P	_N/A	F	F	F	P	
Energy Limit:	P	N/A	P	P	P	P	
Total Wear:	0.033	N/A	0.029	0.047	0.044	0.027	
Wear Limit:	0.030	N/A	0.070	0.070	0.070	0.070	
Comments:							
					· · · · · · · · · · · · · · · · · · ·		

F = Fail P = Pass N/A = Not Applicable

Test name: A-77-I Test date: 10/06/07 I Machine AL-27637-L Test description: Oil type: AL-27637-L/LO-224425 Viscosity: 30 Miscellaneous: Software version: 1.40 I0706098 - AL-27637-L / LO-224425 Run name & desc: Run date: 10/07/07 82 degrees C Oil temperature: 3.78 liter/minute Oil flow rate: Operator: mtd I machine oil test AL-27637-L / LO-224425 Remarks: Sequence name: SE01219 Use 1Y0708 Disc and 1Y3610 Plate Remarks: Number of cycles run: 1139 Machine: Ι Coast down check run: 07/19/02 151.76 seconds Result: Inertia check run: 07/19/02 Result: 1.0288 N-m-s² 1Y0708 - Elastomeric Disc Disc name & desc: Raybestos 6475-4 Rayflex Material: Single Lead Spiral - 12 Radial Groove pattern: Use with 1Y3610 Steel Plate Miscellaneous: Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius 128.21 (mm) : Batch number: 26NO0-00004 Remarks: Elastomeric 1Y3610 - Steel Plate Plate name & desc: Surface: 0.70 to 1.30 micron Roughness Miscellaneous: Install the side marked with the average roughness Batch number: 26N00-00004 0.90 surface finish Remarks: LIM1219 - Reference run: I0706090 Report limit name: Limit file generated: 09/24/07 REP1219 - ELASTOMERIC, RAYFLEX Report format name:



1Y0708 DISC THICKNESS

	Outer Diameter			Inner Diameter		
Loc	Ml	M2	MЗ	Ml	M2	MЗ
1	4.99	4.96	4.95	4.98	4.95	4.95
2	4.99	4.97	4.96	4.98	4.95	4.94
3	4.99	4.96	4.95	4.98	4.96	4.95
4	4.99	4.95	4.95	4.98	4.95	4.95
5	4.98	4.95	4.95	4.98	4.95	4.95
6	4.98	4.95	4.95	4.98	4.95	4.95
Avg	4.99	4.96	4.95	4.98	4.95	4.95
	Compression set average wear: 0.029 M2 - M3 average Wear: 0.004					

Total Wear (all measurements in mm): 0.033







Southwest research institute I machine oil test AL-27637-L/LO-224425

Test name: A-77-I Test date: 10/06/07 Test description: I Machine AL-27637-L Oil type: AL-27637-L/LO-224425 Viscosity: 30 Miscellaneous: Software version: 1.40 10706099 - AL-27637-L / LO-224425 Run name & desc: Run date: 10/08/07 82 degrees C Oil temperature: 3.78 liter/minute Oil flow rate: Operator: HC "I" machine oil test AL-27637-L / LO-224425 Remarks: Sequence name: SE01221 Use 1Y0710 Disc and 1Y3610 Plate. Remarks: Number of cycles run: 1018 Machine: Τ Coast down check run: 07/19/02 151.76 seconds Result: Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0710 - Steering Brake Paper Material: Raybestos 7894-4 Paper 2 - 37 Multiple Parallel Groove pattern: Miscellaneous: Use with 1Y3610 Steel Plate Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm): 128.21 Batch number: 23MR9-00001 Remarks: Steering Brake Paper 1Y3610 - Steel Plate Plate name & desc: 0.70 to 1.30 micron Roughness Surface: Install the side marked with the average roughness Miscellaneous: 23MR9-00001 Batch number: Remarks: 0.83 Surface Finish Report limit name: LIM1221 - Reference run: I0706003 Limit file generated: 07/26/06 REP1221 - STEERING BRAKE PAPER Report format name:


1Y0710 DISC THICKNESS

	Outer	c Diame	eter	Inne	r Diam	eter
Loc	Ml	M2	MЗ	M1	M2	MЗ
1	5.04	5.02	5.01	5.04	5.02	5.01
2	5.05	5.02	5.01	5.05	5.02	5.01
3	5.03	5.02	5.01	5.03	5.01	5.01
4	5.03	5.01	5.00	5.03	5.01	5.00
5	5.02	5.01	5.00	5.03	5.01	5.00
6	5.04	5.02	5.01	5.04	5.02	5.01
Avg	5.04	5.02	5.01	5.04	5.01	5.01
	Compre M2 - N	ession 13 avei	set averag rage Wear:	ge wea: 0.001	r: 0.(9	020

Total Wear (all measurements in mm): 0.029







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Test name: A-77-I 10/06/07 Test date: I Machine AL-27637-L Test description: AL-27637-L/LO-224425 Oil type: Viscosity: 30 Miscellaneous: Software version: 1.40 Run name & desc: I0706100 - AL-27637-L Run date: 10/09/07 Oil temperature: 82 degrees C Oil flow rate: 3.78 liter/minute Operator: HC "I" machine oil test AL-27637-L / LO-224425 Remarks: Sequence name: SE01222 Use 1Y0711 Disc and 1Y0726 Plate Remarks: Number of cycles run: 1117 Machine: T Coast down check run: 07/19/02 151.76 seconds Result: Inertia check run: 07/19/02 1.0288 N-m-s² Result: Disc name & desc: 1Y0711 - Wheel Brake Paper Raybestos 7902-1 Paper Material: 2 - 37 Multiple Parallel Groove pattern: Use with 1Y0726 Steel Plate Miscellaneous: Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm) : 128.21 Batch number: 24FE9-00001 Wheel Brake Paper Remarks: 1Y0726 - Steel Plate Plate name & desc: Surface: 0.30 micron Maximum Roughness Miscellaneous: Install the side marked with the average roughness 24FE9-00001 Batch number: 0.23 Surface Finish Remarks: LIM1222 - Reference run: I0706004 Report limit name: Limit file generated: 07/26/06 REP1222 - WHEEL BRAKE PAPER Report format name:



1Y0711 DISC THICKNESS

	Outer	r Diame	eter	Inne	r Diam	eter
Loc	Ml	M2	MЗ	M1	M2	MЗ
1	4.99	4.95	4.94	4.99	4.96	4.95
2	4.99	4.96	4.94	4.99	4.96	4.95
3	4.99	4.96	4.94	4.99	4.96	4.95
4	4.99	4.96	4.94	4.99	4.96	4.94
5	4.99	4.96	4.94	4.99	4.96	4.95
6	4.99	4.95	4.93	4.98	4.94	4.94
Avg	4.99	4.96	4.94	4.99	4.96	4.95
	Compre M2 - N	ession 13 ave:	set averag age Wear:	ge wea: 0.014	r: 0.(1	032

Total Wear (all measurements in mm): 0.047





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Southwest research institute I machine oil test AL-27637-L/LO-224425

Test name: A-77-I Test date: 10/06/07 I Machine AL-27637-L Test description: Oil type: AL-27637-L/LO-224425 Viscosity: 30 Miscellaneous: Software version: 1.40 Run name & desc: I0706101 - AL-27637-L 10/10/07 Run date: Oil temperature: 82 degrees C 3.78 liter/minute Oil flow rate: Operator: HC "I" machine oil test AL-27637-L / LO-224425 Remarks: Sequence name: SE01223 Use 1Y0712 Disc and 1Y0726 Plate Remarks: Number of cycles run: 1006 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds 07/19/02 Inertia check run: Result: 1.0288 N-m-s² Disc name & desc: 1Y0712 - Transmission Paper Material: Raybestos 7901-2 Paper 2 - 37 Multiple Parallel Groove pattern: Miscellaneous: Use with 1Y0726 Steel Plate Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm) : 128.21 Batch number: 27MR9-00001 Transmission Paper Remarks: Plate name & desc: 1Y0726 - Steel Plate 0.30 micron Maximum Roughness Surface: Install the side marked with the average roughness Miscellaneous: Batch number: 27MR9-00001 Remarks: 0.20 Surface Finish Report limit name: LIM1223 - Reference run: I0706006 Limit file generated: 07/26/06 Report format name: REP1223 - TRANSMISSION PAPER



1Y0712 DISC THICKNESS

	Oute	r Diam	eter	Inne	r Diam	eter	
Loc	M1	M2	МЗ	M1	M2	МЗ	
1	5.00	4.97	4.95	5.00	4.98	4.96	
2	4.99	4.96	4.95	4.99	4.96	4.95	
3	4.98	4.95	4.94	4.98	4.95	4.94	
4	4.99	4.95	4.94	4.99	4.95	4.94	
5	4.98	4.95	4.94	4.98	4.95	4.94	
6	5.00	4.96	4.95	5.00	4.96	4.95	
Avg	4.99	4.96	4.94	4.99	4.96	4.95	
	Compr M2 -	ession M3 ave	set ave rage Wea	rage wea r: 0.01	r: 0. 2	033	
	Total We	ar (al	1 measur	ements i	n mm):	0.04	4







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Test name: A-77-I Test date: 10/06/07 Test description: I Machine AL-27637-L AL-27637-L/LO-224425 Oil type: Viscosity: 30 Miscellaneous: Software version: 1.40 I0706102 - AL-27637-L Run name & desc: Run date: 10/11/07 Oil temperature: 82 degrees C Oil flow rate: 3.78 liter/minute Operator: HC I machine oil test AL-27637-L / LO-224425 Remarks: Sequence name: SE01224 Remarks: Use 1Y0713 Disc and 8E4095 Plate Number of cycles run: 1126 Ι Machine: Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0713 - Elastomeric Disc Material: Caterpillar F37 Single Lead Spiral - 12 Radial Groove pattern: Miscellaneous: Use with 8E4095 Steel Plate Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm) : 128.21 Batch number: C63007FE1 Remarks: Elastomeric 8E4095 - Steel Plate Plate name & desc: Surface: 0.70 to 1.00 micron Roughness Miscellaneous: Install the side marked with the average roughness Batch number: C63007FE1 0.87 Surface Finish Remarks: LIM1224 - Reference run: I0706007 Report limit name: Limit file generated: 07/26/06 Report format name: REP1224 - ELASTOMERIC, F37



1Y0713 DISC THICKNESS

	Outer	c Diame	eter	Inne	r Diam	eter
Loc	Ml	M2	M3	M1	M2	MЗ
1	5.03	5.03	4.99	5.03	5.03	5.01
2	5.03	5.03	5.00	5.03	5.03	5.00
3	5.03	5.03	5.00	5.03	5.03	5.01
4	5.03	5.03	5.00	5.03	5.03	5.01
5	5.03	5.03	5.00	5.03	5.03	5.01
6	5.03	5.03	5.00	5.03	5.03	5.00
Avg	5.03	5.03	5.00	5.03	5.03	5.01
	Compre M2 - N	ession 13 avei	set averag age Wear:	ge wea: 0.02	r: 0.0 7	000

Total Wear (all measurements in mm): 0.027







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SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

Fuels And Lubricants Research Division

Report on

DEXRON® VI BAND CLUTCH FRICTION TEST

Conducted For

SwRI ARMY LAB

Oil Code: AL-27637-L

Test Number: BH3-4-164

August 6, 2007

Submitted by:

Christopher Barker ' Research Engineer Specialty & Driveline Fluids Evaluation



The results of this report relate only to the fluid tested. This report shall not be reproduced except in full without the written approval of Southwest Research Institute®

DEXRON[®]-VI Band Friction - 150 HOURS

Program Code: AL-27637-L Status: EOT Test Cycles: 36,000 Test Performance:

Start Date: 7/30/2007 EOT Date: 8/6/2007 Run Number: BH3-4-164 EOT Parts Condition:

Band: 4L60 **Drum:** 4L60

st Time [h]	Cvcles	Stop	Time	Midpoin	it Torque	Max Torque IN-m1	End T	orque	Tor	- Mid que	Shift Energy
		0.35	0.55	180	290	Report	. ^	200	v	120	(15.7-16.3)
0	10	0.40		260		335	308		75		16.0
1	240	0.43		213		355	352		142		16.0
2	480	0.43		210		341	335		131		16.0
3	720	0.44	Three	208	Three	305	299	Three	97	Three	16.0
4	960	0.45	Point	203	Point	312	282	Point	109	Point	16.0
5	1,200	0.45	Average	202	Average	320	312	Average	118	Average	16.0
10	2,400	0.47	0.46	202	200	313	312	306	111	112	16.0
15	3,600	0.47	0.47	196	202	302	295	306	106	108	16.0
20	4,800	0.46	0.46	208	206	316	312	290	108	91	16.2
25	6,000	0.46	0.46	215	213	274	262	271	59	73	16.2
30	7,200	0.46	0.46	215	215	267	239	253	52	55	16.2
35	8,400	0.46	0.46	216	216	271	257	252	55	53	16.1
40	9,600	0.46	0.46	216	213	269	260	246	53	54	16.2
45	10,800	0.46	0.46	207	209	262	220	232	55	53	16.2
50	12,000	0.46	0.46	204	205	253	217	217	50	51	16.3
55	13,200	0.47	0.47	205	203	254	215	216	48	49	16.3
60	14,400	0.47	0.47	201	205	248	216	224	48	50	16.4
65	15,600	0.47	0.47	210	205	262	243	224	53	51	16.5
20	16,800	0.47	0.47	206	207	257	213	235	52	56	16.6
75	18,000	0.48	0.47	207	205	271	249	227	64	56	16.7
80	19,200	0.48	0.48	203	205	254	217	242	51	61	16.8
85	20,400	0.48	0.48	206	206	274	259	240	69	62	16.9
90	21,600	0.48	0.48	210	208	278	244	248	67	11	17.1
95	22,800	0.49	0.49	209	209	285	241	242	76	67	17.2
100	24,000	0.49	0.49	208	202	266	242	243	58	71	17.5

DEXRON[®]-VI Band Friction - 150 HOURS

Program Code: AL-27637-L Status: EOT Test Cycles: 36,000 Test Performance:

Start Date: 7/30/2007 EOT Date: 8/6/2007 Run Number: BH3-4-164 EOT Parts Condition:

Band: 4L60 **Drum:** 4L60

e	Cycles	Stop	Time	Midpoin	t Torque m]	Max Torque [N·m]	End T [N	endue m]	Tor	- Mid eup	Shift Energy [kJ]
1		0.35	CC.U	180	790	Keport	^	200	v	120	(15.7-16.3)
	25,200	0.48	0.49	190	195	270	246	237	80	67	16.0
	26,400	0.50	0.49	187	188	251	224	227	64	75	15.8
	27,600	0.49	0.50	188	189	270	210	220	82	62	15.8
	28,800	0.50	0.50	192	189	233	226	216	41	02	15.8
	30,000	0.50	0.50	188	190	276	213	221	87	61	15.8
	31,200	0.50	0.50	189	187	245	223	213	56	11	15.7
	32,400	0.50	0.50	183	187	270	205	216	87	67	15.7
	33,600	0.50	0.50	188	184	247	219	217	59	75	15.8
	34,800	0.50	0.50	182	184	260	226	224	78	65	15.7
	36,000	0.51	0.50	182	182	240	228	227	57	68	15.7

												-												·												
				Energy	(KJ)	(15.7-16.3)	16.0	16.0	16.0	16.0	16.0	16.0	16.0	16.0	16.2	16.2	16.2	16.1	16.2	16.2	16.3	16.3	16.4	16.5	16.6	16.7	16.8	16.9	17.1	17.2	17.5					
				q	Nm)	0				Three	Point	Average	306	306	290	271	253	252	246	232	217	216	224	224	235	227	242	240	248	242	243					
Sa-	7/30/2007	8/6/2007		Ē	Torq.(>20	308	352	335	299	282	312	312	295	312	262	239	257	260	220	217	215	216	243	213	249	217	259	244	241	242					
	Start of Test:	End of Test :		Maximum	Torq.(Nm)	(Report)	335	355	341	305	312	320	313	302	316	274	267	271	269	262	253	254	248	262	257	271	254	274	278	285	266					
			c	d-Mid	l.(Nm)	120				Three	Point	Average	107	104	84	59	37	36	33	24	12	13	19	19	28	21	37	34	40	33	41					
te®	4L60	4L60	50 ml/mir	Enc	Toro	v	48	139	125	91	79	110	110	66	104	47	24	41	44	14	14	10	15	33	8	42	14	53	34	32	33					
arch Institu	t Research Institut	Drum :	Air Flow:	ax-Mid	q.(Nm)	<120				Three	Point	Average	112	108	91	73	55	53	54	53	51	49	50	51	56	56	61	62	71	67	71					
t Rese		16.38 KJ 137.1 C 303.2 KPa	KPa	M	Tor		75	142	131	97	109	118	111	106	108	59	52	55	53	55	50	48	48	53	52	64	51	69	67	76	58					
outhwes	16.38		303.2 I	ooint	(m)	90)				Three	Point	Average	200	202	206	213	215	216	213	209	205	203	205	205	207	205	205	206	208	209	202					
S	Energy:	L Temp.:	Apply:	Midpo	Torq.(Torq.(Torq.(Torq.(I	Torq.(h	Torq.(N	(180-2	260	213	210	208	203	202	202	196	208	215	215	216	216	207	204	205	201	210	206	207	203	206	210	209	208
				ement	(Sec)	-0.55)				Three	Point	Average	0.46	0.47	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.47	0.47	0.47	0.47	0.47	0.48	0.48	0.48	0.49	0.49					
	3H3-4-164	NL-27637-I		Engag	Time	(0.35 -	0.40	0.43	0.43	0.44	0.45	0.45	0.47	0.47	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.47	0.47	0.47	0.47	0.48	0.48	0.48	0.48	0.49	0.49					
	st Number: E	luid Code: /		Total	Cycles		10	240	480	720	960	1,200	2,400	3,600	4,800	6,000	7,200	8,400	9,600	10,800	12,000	13,200	14,400	15,600	16,800	18,000	19,200	20,400	21,600	22,800	24,000					
	Tes	uL.		Test	Hour		0	~	2	ო	4	5	10	15	20	25	30	35	40	45	50	55	09	65	70	75	80	85	06	95	100					

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				inergy	(KJ)	5.7-16.3)	16.0	15.8	15.8	15.8	15.8	15.7	15.7	15.8	15.7	15.7
						Ű										
Ø				End	J.(Nm)	200	237	227	220	216	221	213	216	217	224	227
3 a -	7/30/2007	8/6/2007			Torc	^	246	224	210	226	213	223	205	219	226	228
	Start of Test:	End of Test :		Maximum	Torq.(Nm)	(Report)	270	251	270	233	276	245	270	247	260	240
			_	1-Mid	.(Nm)	120	42	38	31	27	31	27	29	32	40	45
ute®	4L60	4L60	50 ml/mir	Enc	Torq	v	57	37	22	35	24	34	22	31	44	46
arch Institu	Band :	Drum :	Air Flow:	ax-Mid	rq.(Nm)	<120	67	75	62	20	61	77	67	75	65	68
st Rese	R	с	KPa	Σ	To		80	64	82	41	87	56	87	59	78	57
Southwe	16.38	137.1	303.2	oint	(mV	90)	195	188	189	189	190	187	187	184	184	182
(U	Energy:	Temp.:	Apply:	Midpo	Torq.(I	(180-2	190	187	188	192	188	189	183	188	182	182
				lement	(Sec)	-0.55)	0.49	0.49	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
	BH3-4-164	AL-27637-I		Engag	Time	(0.35	0.48	0.50	0.49	0.50	0.50	0.50	0.50	0.50	0.50	0.51
	st Number:	Fluid Code: ,		Total	Cycles		25,200	26,400	27,600	28,800	30,000	31,200	32,400	33,600	34,800	36,000
	Te			Test	Hour		105	110	115	120	125	130	135	140	145	150



Southwest Research Institute ®

DEXRON® VI Band Friction Test Parts Rating

Sponsor Code: AL-27637-L Run Number: BH3-4-164 EOT Date: 08-06-07 Cycles: 36,000 Hours: 150

Band: The fiber area is completely darkened with light glazing and trace/light stress cracks. Handling marks are also visible. Fiber material is damaged at one end of the band

Drum: There are no cracks. Dark gray tracking marks and light discoloration is also visible.

SwRI Rating: Pass

Rater: Art Sanchez Date: 08-07-2007

Comments: This test was conducted using 4L60 Drum And 4L60 Band.

*Pending GM ATF Committee approval



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SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

FUELS AND LUBRICANTS RESEARCH DIVISION

Report on DEXRON[®] VI LOW SPEED CLUTCH FRICTION AND TORQUE CAPACITY CHARACTERIZATION

Conducted for

ARMY LAB

Oil Code:

AL-27637-L

Test Numbers: LS12-5-0363

July 31, 2007

Submitted by:

Matthew Jackson Principal Engineer Specialty & Driveline Fluids Evaluation



The results of this report relate only to the fluid tested. This report shall not be reproduced, except in full, without the written approval of Southwest Research Institute.

DEXRON[®] VI - LOW SPEED - NEW OIL

Program Code: AL-27637-L Status: EOT Test Cycles: 306 Test Performance: Pass Start Date: 7/30/2007 EOT Date: 7/31/2007 Run Number: LS12-5-0363 EOT Parts Condition: Pass

	Sliding Speed	40°C Coefficients Apply Pressure [kPa]			90°C Coefficients Apply Pressure [kPa]			120°C Coefficients Apply Pressure [kPa]		
Slip Speed										
[r/min]	[m/s]	273	683	1044	273	683	1 1044	273	683	1044
1	0.007	0.129	0.131	0.130	0.114	0.117	0.114	0.107	0.107	0.107
2	0.014	0.133	0.134	0.132	0.118	0,119	0.117	0,110	0.110	0.110
4	0.028	0.136	0.136	0.134	0.122	0.121	0.120	0.114	0.113	0.112
8	0.056	0.139	0.138	0.135	0.126	0.125	0.122	0.117	0.116	0.115
16	0.112	0.140	0.139	0.136	0.128	0.127	0.124	0.120	0.119	0.117
24	0.168	0.142	0.139	0.137	0.130	0.127	0.126	0.122	0.121	0.119
30	0.210	0.142	0.139	0.136	0.131	0.128	0.125	0.123	0.122	0.119
40	0.280	0.141	0.139	0.136	0.132	0.128	0.126	0.124	0.122	0.119
70	0.490	0.142	0.136	0.133	0.132	0.127	0.125	0.125	0.122	0.119
80	0.560	0.141	0.135	0.132	0.132	0.127	0.124	0.125	0.122	0.119
100	0.700	0.140	0.134	0.131	0.132	0.127	0.123	0.126	0.122	0.118
135	0.946	0.139	0.132	0.128	0,132	0.125	0.121	0.126	0.121	0.116
170	1.191	0.138	0.130	0.126	0.132	0.124	0.119	0.126	0.119	0.115
235	1.646	0.136	0.127	0.122	0.130	0.121	0.116	0.125	0.118	0.112

DEXRON[®] VI - LOW SPEED - USED CYCLING TEST OIL

Program Code: Status: Test Cycles: Test Performance: Start Date: EOT Date: Run Number: EOT Parts Condition:

	Silding Speed [m/s]	40°C Coefficients Apply Pressure [kPa]			90°C Coefficients Apply Pressure [kPa]			120°C Coefficients Apply Pressure [kPa]		
Slip Speed [r/min]										
		273	683	1044	273	683	1044	273	683	1044
1	0,000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
2	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
4	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
8	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
16	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
24	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
30	0.000	0.000	0.000	0,000	0.000	0.000	0.000	0.000	0.000	0.000
40	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
70	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
80	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
100	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
135	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
170	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
235	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000



Test Rig Overview

The GM Low Speed Clutch Friction Test Rig utilizes a 30 hp variable speed electric drive that provides input power to a Greening SAE No. 2 Universal Wet Friction Material Test Machine through a speed-reducing gearbox. Test fluid is drawn from the bottom of the test head, externally circulated using a small gear pump, and returned at the clutch centerline. This is done to more closely simulate fluid flow within a transmission.

Since the clutch cannot be slipped to achieve heating between engagements, an external heat source is employed to achieve the high fluid temperatures required by the test procedure. Silicon oil from an external bath is circulated through the test head "water jacket" chamber (in place of the normal cooling water). Temperature control of the silicon bath is achieved using immersion heaters and a shell-and-tube heat exchanger.

Procedure Overview

A clutch pack consists of one fiber plate installed between two steel plates. Both steel plates are instrumented with thermocouples to record plate interface temperatures during the clutch engagements. Once the test rig is assembled and filled with test fluid, the clutch is applied three times (at a rotational speed of 0 rpm) to ensure saturation of the friction plate.

Discrete Data

The clutch is slipped at fourteen discrete rotational speeds, repeated for nine different pressure and temperature combinations. The discrete conditions for SAE Standard clutch plates are listed below.

Rotational	Apply Pressure	Fluid			
Speed (rpm)	(kPa)	Temperature (°C)			
1					
2	273				
4		40			
8					
16					
24					
30	683				
40		90			
70					
80					
100					
135	1044	120			
170					
235					

(Note: The use of different clutch plates will necessitate adjustment of the speed and pressure conditions to match the slip speeds and surface pressures encountered by the SAE Standard plates.)



At each discrete speed condition, the clutch is slipped for three seconds following stabilization of the apply force. Target times for data collection are 0.3, 1.0, and 2.9 seconds. The clutch pack is then rotated at 100 rpm (with the apply pressure released) until the separator plate temperatures are stabilized within 3 °C of the bulk fluid temperature.

Sweep Data

Once all speed data has been recorded for a given pressure and temperature combination, sweep data is collected. During a sweep, the clutch is applied and the rotational speed is ramped from 0 rpm to maximum in 20 seconds. The clutch is then held at maximum speed for 5 seconds, then ramped to 0 rpm in 20 seconds. One sweep is performed for every pressure and temperature combination.

Breakaway Data

At the conclusion of each sweep, two static breakaways are performed. In each breakaway, speed is set at 0 rpm and the clutch applied at the given pressure condition. The electric drive then increases power to the test head until the clutch "breaks away." Immediately following breakaway, the clutch is slipped for 3 seconds at 5 rpm. The first breakaway is performed immediately following the conclusion of the sweep, with the second following after the separator plate temperatures are stabilized within 3 °C of the bulk fluid temperature.

Friction Map

Completion of the 126 speed-pressure-temperature clutch slip combinations and their associated sweeps and breakaways constitutes a friction map.

Break-In

Following the initial friction map, a break-in procedure is performed. Break-in consists of continuously slipping the clutch for ten minutes at 120 °C, 683 kPa, and 100 rpm. (Note that break-in conditions must also be adjusted when using plates other than SAE standard.) The ten-minute engagement is performed three times with a one minute release period between each apply cycle.

Post Break-In

Upon completion of the break-in, a complete friction map is performed (as described above). This results in two complete sets of data – an initial "pre-break-in" friction map and a final "post-break-in" map.

New and Used Fluid

Two full tests are conducted on each fluid. The first test is conducted on new, unused fluid. The second test is conducted on identical fluid that was previously run in another test (typically the GM Cycling test).

Upon completion of the initial test on new fluid, the rig is allowed to drain for a minimum of 30 minutes. Since the used fluid test is conducted on the same clutch pack used to test the new fluid, the test head is not disassembled between runs. (For this reason, clutch pack measurements give an indication of overall wear only, as final measurements are not conducted until the completion of the second test.)



After the rig has been fully drained, the used fluid (which has been filtered to remove any debris from previous testing) is installed and the test repeated.

Data Interpretation

A friction coefficient is calculated for each discrete data combination. The coefficient is calculated according to the following equation:

$$\mu = \frac{T}{PARN}$$

where

T = Torque (Nm) P = Pressure (kPa) A = Apply Piston Area (m²) R = Mean Friction Radius (m) N = Active Friction Surfaces

Test Report

Per sponsor request, only the new fluid portion of the test was conducted. The test report consists of nine plots displaying the variation of coefficient with slip speed at each temperature and pressure combination, two charts summarizing friction map data from the new and used fluid tests (not run in this case), and clutch pack wear measurements.



Appendix

- 1. Coefficient vs. Slip Speed Plot: 40 °C / 273 kPa
- 2. Coefficient vs. Slip Speed Plot: 40 °C / 683 kPa
- 3. Coefficient vs. Slip Speed Plot: 40 °C / 1044 kPa
- 4. Coefficient vs. Slip Speed Plot: 90 °C / 273 kPa
- 5. Coefficient vs. Slip Speed Plot: 90 °C / 683 kPa
- 6. Coefficient vs. Slip Speed Plot: 90 °C / 1044 kPa
- 7. Coefficient vs. Slip Speed Plot: 120 °C / 273 kPa
- 8. Coefficient vs. Slip Speed Plot: 120 °C / 683 kPa
- 9. Coefficient vs. Slip Speed Plot: 120 °C / 1044 kPa
- 10. Clutch Pack Wear Measurements



AL-27637-L, 40°C, 273 kPa Apply Pressure



AL-27637-L, 40°C, 683 kPa Apply Pressure



AL-27637-L, 40°C, 1044 kPa Apply Pressure




New Fluid Test Number: LS12-5-0363

















AL-27637-L, 120°C, 683 kPa Apply Pressure



------New - - Used

AL-27637-L, 120°C, 1044 kPa Apply Pressure

SOUTHWEST RESEARCH INSTITUTE®

GM LOW SPEED CLUTCH FRICTION AND TORQUE CAPACITY CHARACTERIZATION



Candidate I	Fluid: AL-2763	7-L T	est Number	: LS12-5-03	63 XOD	Completion	Date : 7/31/2	2007
Plates	Location of Tooth	Near Inner	Diameter	Near Outer I	Diameter	Inner Diameter	Average Overall	Outer
	(Clockwise)	Before	After	Before	After	Change	Change	Change
			FRIC	TION MATERIAL				
	Тор	1.7630	1.6580	1.7650	1.7020	0.1050		0.0630
2	120	1.7660	1.6710	1.7640	1.7070	0.0950		0.0570
	240	1.7690	1.6780	1.7690	1.7090	0.0910		0.0600
_	Average					0.0970	0.0785	0.0600
			STEE	L SEPARATORS		1		
	Тор	1.7480	1,7480	1.7480	1.7480	0.0000		0.0000
1	120	1.7510	1.7510	1.7510	1.7500	0.0000	N	0.0010
	240	1.7530	1.7530	1.7530	1.7530	0.0000	1	0.0000
	Average					0.0000	0.0002	0.0003
	Тор	1.7460	1.7460	1.7460	1.7460	0.0000		0.0000
3	120	1.7460	1.7460	1.7460	1.7460	0.0000		0.0000
	240	1.7420	1.7420	1.7420	1.7420	0.0000		0.0000
	Average					0.0000	0.0000	0.0000

PLATE CONDITION AT E.O.T.: PLATES IN GOOD CONDITION WITH NO UNUSUAL DISCOLORATION

(Anything Unusual)

Test Date:

4/11/2007

Operator's Name:

MARK HOLMES

Reviewed By (Signature and Date)

8/8/07

Pack ID#: 4000

SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

Fuels And Lubricants Research Division

Report on

DEXRON® VI PLATE CLUTCH FRICTION TEST

Conducted For

SwRI ARMY LAB

Oil Code: AL-27637-L

Test Number: **HC11-24-80**

August 7, 2007

Submitted by:

Christopher Barker Research Engineer Specialty & Driveline Fluids Evaluation



The results of this report relate only to the fluid tested. This report shall not be reproduced except in full without the written approval of Southwest Research Institute®

DEXRON[®]-VI Plate Friction - 200 HOURS

Program Code: AL-27637-L Status: EOT Test Cycles: 36,000 Test Performance:

Start Date: 7/30/2007 EOT Date: 8/7/2007 Run Number: HC11-24-80 EOT Parts Condition:

Fiber Plates: GMPT-0506 Steel Plates: GMPT-0506 Delta Travel [mm]: 0.356 mm

Shim Energy [kJ] 15.4.45.0	10.01 - 4.01	0.01	1.01	1.61	15.8	15.8	15.8	15.8	15.8	15.8	15.8	10.0	0.01	15.8	15.8	15.8	15.8	15.7	15.0	45.7	1.61	15.8	15.8	15.7	15.8	45.7	10.1	13.8	141
aupror b		1	1	F		Foint	Average	5	-	6	4 6	0	?	-2	ç	-2	5				-	-	-	-	0				
Max - Mi [N	6		7-	± ;	-	2	6	5	0	6			2	7-	-5	-5	-	-	-	1	-	-	-1	7	0	0			2
l orque				Three	Doint	LOIN	Average	102	98	94	91	80		88	88	87	87	87	87	87	01	10	81	87	87	87	86	and	00
Maximum [N-n ~	89	00	100	100	100	100	IUI	102	16	93	91	89	00	00	88	87	87	87	86	87	87	10	10	87	87	86	86	BR	20
End I orque [N·m] Report	81	69	60	101	80	800	RR	91	83	11	73	02	44	21	80	69	11	68	69	69	60	20	N	69	11	11	102	71	100 mm
m] 105				Three	Point	Average	Aveiage	98	97	96	94	92	10		20	89	88	88	88	88	88	87	10	8/	87	87	86	86	
N] 08	88	91	94	86	86	an	8	BI	97	96	94	92	91	00	20	88	88	88	88	88	87	87	10	10	87	87	86	98	
1.05				Three	Point	Averane		LR.O	0.92	0.94	0.95	0.97	0.98	000	00.0	00.1	0.99	1.00	1.00	1.00	1.00	1 00	101	10.1	1.01	1.02	1.02	1.03	
atop [s 0.85	1.02	0.96	0.93	0.91	0.91	06.0	100	18.0	0.92	0.94	0.96	0.95	0.99	0 00	100	00.1	1.00	0.99	1.01	1.00	1.00	1.00	1 00		1.01	1.01	1.03	1.03	
Cycles	10	180	360	540	720	006		0001	2,700	3,600	4,500	5,400	6,300	7.200	8 100	00000	9,000	9,900	10,800	11,700	12,600	13,500	14 400	1000	002'01	16,200	17,100	18,000	
Ξ	0.1	1	2	3	4	5	10	44	2 00	20	52	30	35	40	45	04	00	00	09	60	20	75	80	SC SC	00	90	95	100	

DEXRON[®]-VI Plate Friction - 200 HOURS

Program Code: AL-27637-L Status: EOT Test Cycles: 36,000 Test Performance:

Start Date: 7/30/2007 EOT Date: 8/7/2007 Run Number: HC11-24-80 EOT Parts Condition:

Fiber Plates: GMPT-0506 Steel Plates: GMPT-0506 Delta Travel [mm]: 0.356 mm

Shirt Energy [kJ]	15.4 - 16.0	15.7	15.8	157	15.8	15.8	15.7	15.7	15.8	15.7	15.8	15.8	15.7	15.8	15.8	15.8	15.7	15.7	15.8	15.0	15.8
[N-m]	< 30		1	•		40	•	10													2 4
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maximum [N-n	00	80	86	86	86	86	86	86	86	86	85	86	86	87	87	88	86	87	88	88	88
End 1 orque	110day		71	71	71	71	72	11	11	72	73	73	73	11	70	74	11	73	73	73	73
m] 105	RF P	3	85	85	85	8	84	83	83	83	83	83	83	83	84	84	84	84	85	85	85
N) NB	86	3	85	85	85	84	84	83	83	83	83	83	83	83	84	84	84	84	85	85	86
105	1 03		1.03	1.03	1.04	1.04	1.05	1.05	1.06	1.06	1.06	1.06	1.06	1.07	1.06	1.06	1.05	1.05	1.05	1.05	1.05
stop [s] 0.85	1.02		1.03	1.03	1.04	1.04	1.04	1.06	1.06	1.07	1.06	1.05	1.07	1.06	1.09	1.05	1.06	1.05	1.06	1.05	1.05
Cycles	18.900	10 000	18,800	20,700	21,600	22,500	23,400	24,300	25,200	26,100	27,000	27,900	28,800	29,700	30,600	31,500	32,400	33,300	34,200	35,100	36,000
E	105	110	011	611	120	125	130	135	140	145	150	155	160	165	170	175	180	185	190	195	200

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K		e			Energy		(10)	(10.4 - 10.0)	0.01	15.7	15.7	15.8	15.8	15.8	15.8	15.8	15 R	15.8	0. u	0.01	0.01	0.0	15.8	8.01	15.7	15.8	15.7	15.8	15.8	15.7	15.8	15.7	15.8	15.7
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		0			Jement	(Sec)	o 1.05)				Three	Point	Averade	2000	0.91	0.92	0.94	0.95	0.97	0.98	0.99	1.00	0.99	1.00	1.00	1.00	1 00	00.7	00.1	1.0.1	1.01	1.02	1.02	1.03
		HC11-24-8	AL-27637-I		Engag	Time	(0.85 t	1.02	0.96	0.93	0.91	0.91	06.0	2000	1.9.0	0.9Z	0.94	0.96	0.95	0.99	0.99	1.00	1.00	0.99	1.01	1.00	1 00		00.1	00.1	1.0.1	1.01	1.03	1.03
		est Number:	Fluid Code:		Total	Cycles		10	180	360	540	720	006	1 800	000'-	2,000	3,000	4,500	5,400	6,300	7,200	8,100	9,000	9,900	10,800	11,700	12.600	13 500	14 400	14,400	10,000	10,200	17,100	18,000
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	2						(mn).	(Keport)	71	71	71	71	71	. 64	77	Ľ	71	72	73	73	73	71	20	74	71	73	2.2	73	73
		7/30/2007	8/7/2007	0 356 mm		(Nim)			86	86	86	86	86	90	8	QD	86	86	86	86	86	86	87	87	87	87	88	88	88
		Start of Test:	End of Test :	Delta Travel	Movin Movin	Tora		R~)	80	86	86	86	86	86 B	00	00	86	86	85	86	86	87	87	88	86	87	88	88	88
y		506	506	c	d-Mid	(MM) ((<u>0</u>	-14	-14	-14	-13	, - 6, -	5 5	4 4	71-	7	-10	-10	-11	-12	-12	-12	-11	-12	-12	-12	-13
ummar	ute®	GMPT-0	GMPT-0	50 ml/mi			<u>-</u>		<u>.</u>	4	-14	-14	-13	-12	: -1-	1 ¢	7 - 17		-10	-10	-10	-12	-13	-10	-13	-12	-12	-12	-13
tion Test S	arch Institu	Fibers	Steels	Air Flow:	ax-Mid	ra.(Nm)	<30)			-	2	7	2	2	0	1 9	n (ო	ო	ო	ო	ო	ო	e	ო	ო	e	ო	с
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GM P	0	Energy:	Temp.:	Apply:	Midpo	Torq.(N	(80-10	86 AB	010	C o	85	85	84	84	83	83	0 0	S G	83	83	83	83	84	84	84	84	85	C8	86
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		HC11-24-8(AL-27637-L		Engage	Time ((0.85 tc	1.02	1 03		1.03	1.04	1.04	1.04	1.06	1.06	1 07	00.1	00.1 10 L	40.1 60.1	10.1	00.1		cn. 1	0.	c0.1	1.06	- 100 L	cn.1
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		Τe			Test	Hour		105	110	4 1 1		120	C71	130	135	140	145	150		180	197	201 021	175		200	200	105	000	222



Southwest Research Institute ®

DEXRON®VI Plate Friction Test Parts Condition Rating

Sponsor Code: AL-27637-L Run Number: HC11-24-80 EOT Date: 08-7-2007 Cycles: 36,000 Hours: 200

Fiber Plates: The inner and outer facing areas are completely darkened with light glazing and medium wear. Outer facing area has heavy flaking and the inner facing area has light/medium flaking.

Steel Plates: Outer steel plate shows light heat discoloration and light scratching and light wear and no hot spots. Inner steel plate shows medium heat discoloration and light wear and light scratching and no hot spots.

SwRI Rating: Fail

Rater: Art Sanchez Date: 08-09-2007

Comments: This test was conducted using GMPT 0506 test kit.

*Pending GM ATF committee approval



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SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

Fuels and Lubricants Research Division

Report on

John Deere JDQ-96 Performed using 1400 Series Axle

Conducted for

ARMY LAB

AL-27637-L

Test Number 07649

October 15, 2007

Submitted by:

W nW

Michael D. Lochte Manager Specialty & Driveline Fluids Evaluations



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John Deere JDQ-96 Performed using 1400 Series Axle

General Information

Oil Code: AL-27637-L	E.O.T. Date: October 15, 2007

Purpose

The purpose of this test was to evaluate the anti-chatter properties of this oil on the brakes of a 1400 series John Deere Inboard Planetary Axle.

Test Procedure

The test was performed as specified by John Deere Product Engineering. The only changes made to the Deere procedure were those necessary to compensate for a different spiral bevel gear ratio. This procedure is proprietary to Deere and Company.

Data Interpretation

The capacity for each engagement is the average torque during the middle of the engagement. The torque variation is the greatest difference between the maximum and minimum torque recorded during any 0.2-second portion of the engagement. The SwRI variation is the sum of all differences between the maximum torque and minimum torque for each engagement. It is obtained by summing all torque variations of each 0.2-second time block of all engagements.

Test Number

The run number listed on this report is a random number and is not sequential. Only SwRI® can link this run number to JDQ-96, AL-27637-L, October 15, 2007.



John Deere JDQ-96 Performed using 1400 Series Axle

Results

Oil Code: AL-27637-L	E.O.T. Date: October 15, 2007

The candidate results can be compared to the baseline reference average. Pass or fail decisions are only made by John Deere Product Engineering. The current reference baseline average is the average of the five most recent tests.

Current Reference Baseline Average (N · m)									
-	1,000 Cycles	10,000 Cycles	20,000 Cycles	30,000 Cycles	TOTAL				
Relative Capacity	338,535	338,534	341,629	343,274	1,361,972				
Torque Variation	79,214	84,272	79,152	74,708	317,346				

	Results From Test Candidate AL-27637-L							
	1,000 Cycles	10,000 Cycles	20,000 Cycles	30,000 Cycles	TOTAL			
Relative Capacity	367,565							
Torque Variation	86,470							

Tables 1 of the Appendix contains chatter test results from 1,000cycles. Table 2 contains results of the five current baseline reference tests. Figures 1 through 4 are graphic presentations of candidate oil performance compared to baseline reference data.

Figure 5 is a graphic presentation of 1000-cycle reference results and AL-27637-L. Table 3 contains the history of reference tests.

Oil Code: AL-27637-L

E.O.T. Date: October 15, 2007

Appendix

Tables

- 1. Table 1 Durability results 1,000 cycles Candidate Oil
- 2. Table 2 Reference Data Compared to Candidate Data
- 3. Figure 1 & Figure 2 Torque Variation Chart
- 4. Figure 3 & Figure 4 Relative Capacity & Average Disk Thickness Chart
- 5. Figure 5 Graphic presentation of 1000 cycle reference results & Candidate
- 6. Table 3 History of reference tests

October 15, 2007

TABLE 1: JDQ-96 DURABILITY TEST RESULTS 1,000 CYCLES

SwRI Oil Code

LO-222425

Sponsor Oil Code AL-27637-L

с С	Temp	72	20	70	71	72	71	71	71	71	71	71	71	20	71	20	69	71	20	20	70
0il Temp. 71°	Variation	130	490	120	300	650	1080	1080	1070	1120	1250	1030	1000	690	660	850	950	610	820	630	640
	Torque	4620	4554	3955	4194	4290	4256	4349	4357	4262	4263	4281	4234	2012	2766	3644	4517	5280	6062	6939	7601
0	Temp.	61	60	59	60	61	61	59	59	60	61	61	61	61	59	58	57	59	58	59	59
il Temp. 60°(Variation	1060	1130	470	870	840	950	1080	1180	1200	1030	1100	1030	740	910	1140	1210	750	630	880	1140
õ	Torque	4673	4649	4314	4385	4392	4380	4330	4361	4322	4330	4286	4270	2043	2868	3643	4516	5242	5747	6682	7643
0	Temp.	51	50	49	49	49	50	50	50	50	51	49	49	49	48	47	48	48	48	49	49
il Temp. 49°(Variation	460	780	006	1070	1120	1210	1130	1170	1250	1160	1180	1130	750	930	1020	930	1030	1090	1170	1160
Õ	Torque	4627	4633	4493	4444	4389	4386	4303	4374	4295	4244	4366	4302	2026	2882	3667	4503	5353	6222	6981	7897
0	Temp.	26	26	26	26	27	28	28	30	30	31	33	33	31	31	31	31	31	31	31	31
il Temp. 32°	Variation	2450	2460	2970	1080	1060	1100	980	1080	1010	960	850	880	720	870	930	2460	2460	2430	2370	2200
	Torque	4608	4490	4457	4602	4509	4484	4403	4471	4344	4289	4381	4286	1973	2843	3677	4539	5509	6371	7242	8191
Press.	(kPa)	3831	3831	3831	3831	3831	3831	3831	3831	3831	3831	3831	3831	1532	2300	3065	3831	4598	5364	6130	7050
Speed	(rpm)	ω	10	15	20	25	30	35	40	45	50	55	60	15	15	15	15	15	15	15	15
	Speed Press. Oil Temp. 32°C Oil Temp. 49°C Oil Temp. 60°C Oil Temp. 71°C	Speed Press. Oil Temp. 32°C Oil Temp. 49°C Oil Temp. 60°C Oil Temp. 71°C (rpm) (kPa) Torque Variation Temp. Temp. Temp.	SpeedPress.Oil Temp. 32°COil Temp. 49°COil Temp. 60°COil Temp. 71°C(rpm)(kPa)TorqueVariationTemp.TorqueVariationTemp.8383146082450264627460514673106061462013072	Speed Press. Oil Temp. 32°C Oil Temp. 49°C Oil Temp. 60°C Oil Temp. 71°C (rpm) (kPa) Torque Variation Temp. Torque Variation Temp. Torque Variation Temp. 71°C 8 3831 4608 2450 26 4627 460 51 4673 1060 61 4620 72 10 3831 4490 2460 26 4633 780 50 4649 1130 60 4554 490 70	Speed Press. Oil Temp. 32°C Oil Temp. 49°C Oil Temp. 60°C Oil Temp. 71°C (rpm) (kPa) Torque Variation Temp. Torque Variation Temp. Torque Variation Temp. 71°C 8 3831 4608 2450 26 460 51 4673 1060 61 4620 72 10 3831 4490 2460 26 4633 780 50 4649 1130 60 4554 490 70 15 3831 4457 2970 26 4493 900 49 4314 470 59 3955 120 70	Speed Press. 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	Relative	Torone	SwRI
		00000	
Temp	Capacity	Variation	Variation
(°C)	(MM)	(MM)	(MM)
32	93,669	31,320	390,060
49	92,386	20,640	285,560
60	91,075	19,340	249,820
71	90,436	15,170	182,130
TOTAL	367,565	86,470	1,107,570
		2(2))	

TABLE 2: JDQ-96 REFERENCE DATA COMPARED TO CANDIDATE DATA

EOT Date: October 15, 2007 Oil Code : AL-27637-L

Reference Oil Coded : 69)	X31111i			-	Average Facing
	Cycles	Relative Capacity	Torque Variation	SwRI Variation	Thickness
First Reference Run					(millimeters)
	1,000	326,304	57,420	730,050	7.60
	10,000	331,809	64,900	804,030	7.50
	20,000	345,325	69,500	899,880	7.44
	30,000	341,770	66,210	810,190	7.39
	Total	1,345,208	258,030	3,244,150	
Second Reference Run					
	1,000	337,791	66,660	848,580	7.60
	10,000	338,055	92,240	1,129,330	7.55
	20,000	343,166	77,010	1,001,920	7.49
	30,000	350,470	73,280	863,980	7.44
	Total	1,369,482	309,190	3,843,810	
Third Reference Run					
	1,000	339,375	100,390	1,204,240	7.56
	10,000	335,754	106,780	1,079,450	7.52
	20,000	334,120	84,770	1,030,270	7.49
	30,000	335,614	79,620	1,021,190	7.47
	Total	1,344,863	371,560	4,335,150	
Fourth Reference Run					
Run on new backing pla	1,000	343,906	79,990	1,020,120	7.48
and piston	10,000	343,056	72,520	893,570	7.30
	20,000	342,668	69,920	885,870	7.07
	30,000	345,315	70,360	833,920	6.90
	Total	1,374,945	292,790	3,633,480	
Invalid test run on same	1,000	348,860	132,110	1,721,010	
backing plate and pistor	10,000	323,093	153,860	1,919,720	
as test above was run on					
Fifth Reference Run					
most recent run	1,000	345,296	91,610	1,125,260	7.50
Run on new backing	10,000	343,999	84,920	1,019,400	7.33
plate and piston	20,000	342,864	94,560	1,264,070	7.22
	30,000	343,201	84,070	1,052,400	7.11
	Total	1,375,360	355,160	4,461,130	
AL-27637-L		Candidate	Oil Test Results		
	1,000	367,565	86,470	1,107,570	
	10,000				
	20,000				
	30,000				,
	Total	367,565	86,470	1,107,570	









Figure 3

AL-27637-L

Table 3

History of 1000 cycle reference tests.

		Torque variation at 1000 cycles
69X31111k	1999 brake disk	103,360
69X31111k	1997 brake disk	129,540
69X31111k	2000 brake disk	121,120
69X31111k	2000 brake disk	129,620
69X31111k	2000 brake disk	135,700
69X31111K	2000 brake disk	138,760
60Y21111k	2000GDD brake di	140,830
60Y31111k	2000GDD brake	124 310
69X31111k	2000 GDD brake	131 860
69X31111k	2000 GDD brake	105,010
69X31111k	2000 GDD brake	109.220
69X31111k	2000 GDD brake	142,510
69X31111k	2000 GDD brake	128,080
69X31111k	2000 GDD brake	109,100
69X31111k	2000 GDD brake	111,800
69X31111k	2000 GDD brake	90,070
69X31111k	2000 GDD brake	90,810
69X31111k	2000 GDD brake	79,930
69X31111k	2000 GDD brake	79,930
69X31111k	2000 GDD brake	83,190
69X31111k	2000 GDD brake	81,220
69X31111K	2000 GDD brake	85,570
68X31111K	2000 GDD brake	64,170
69X31111K	2000 GDD brake	67,390
69X31111k	2000 GDD brake	82,410
69X31111k	2000 GDD brake	90.390
69X31111k	2000 GDD brake	99.960
69X31111k	2000 GDD brake	87,380
69X31111k	2000 GDD brake	74,720
69X31111k	2000 GDD brake	74,940
69X31111k	2000 GDD brake	85,980
69X31111k	2000 GDD brake	94,410
69X31111k	2000 GDD brake	74,300
69X31111k	2000 GDD brake	90,950
69X31111k	2000 GDD brake	83,190
69X31111k	2000 GDD brake	105,210
69X31111k	2000 GDD brake	91,960
69X31111k	2000 GDD brake	97,320
69X31111k	2000 GDD brake	75,040
69X31111k	2000 brake disk	86,060
69X31111K	2000 brake disk	68,590
69X31111K	2003 Drake disk	57,420
09A31111K 60X21111k	2003 brake disk	50,330 76,260
60Y31111k	2003 brake disk	86.210
60X31111k	2003 brake disk	84 550
69X31111k	2003 brake disk	66 660
69X31111k	2003 brake disk	84 760
69X31111k	2003 brake disk	87 800
69X31111k	2003 brake disk	100.390
69X31111k	2003 brake disk	96,620
69X31111k	2003 brake disk	106,710
69X31111k	2003 brake disk	123,110
69X31111k	NEW BACKING PI	79,990
69X31111k		98,440
69X31111k		106,370
69X31111k		110,040
69X31111k		127,550
69X31111k		111,280
69X31111k	invalid run	132,110
	NEW BACKING	
69X31111k	Plate and piston	91,610
	NEW BACKING	
69X31111k	Plate and piston	92,230
	plate used for 1	
69X31111k	test	89,200
	same brake plate	
	and piston as	
AL-27637-L	above	86,470





Figure 5

SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

Fuels and Lubricants Research Division

Report on

John Deere JDQ-96 Performed using 1400 Series Axle

Conducted for

ARMY LAB

AL-27793-L

Test Number 07981

October 12, 2007

Submitted by:

n

Michael D. Lochte
Manager
Specialty & Driveline Fluids
Evaluations



The results of this report relate only to the items tested. This report shall not be reproduced, except in full, without the written approval of Southwest Research Institute®.



John Deere JDQ-96 Performed using 1400 Series Axle

General Information

Oil Code: AL-27793-L	E.O.T. Date: October 12 2007

Purpose

The purpose of this test was to evaluate the anti-chatter properties of this oil on the brakes of a 1400 series John Deere Inboard Planetary Axle.

Test Procedure

The test was performed as specified by John Deere Product Engineering. The only changes made to the Deere procedure were those necessary to compensate for a different spiral bevel gear ratio. This procedure is proprietary to Deere and Company.

Data Interpretation

The capacity for each engagement is the average torque during the middle of the engagement. The torque variation is the greatest difference between the maximum and minimum torque recorded during any 0.2-second portion of the engagement. The SwRI variation is the sum of all differences between the maximum torque and minimum torque for each engagement. It is obtained by summing all torque variations of each 0.2-second time block of all engagements.

Test Number

The run number listed on this report is a random number and is not sequential. Only SwRI® can link this run number to JDQ-96, AL-27793-L, October 12, 2007.



John Deere JDQ-96 Performed using 1400 Series Axle

Results

Oil Code: AL-27793-L	E.O.T. Date: October 12, 2007

The candidate results can be compared to the baseline reference average. Pass or fail decisions are only made by John Deere Product Engineering. The current reference baseline average is the average of the five most recent tests.

Current Reference Baseline Average (N · m)									
	1,000 Cycles	10,000 Cycles	20,000 Cycles	30,000 Cycles	TOTAL				
Relative Capacity	338,535	338,534	341,629	343,274	1,361,972				
Torque Variation	79,214	84,272	79,152	74,708	317,346				

Results From Test Candidate AL-27793-L								
	1,000 Cycles	10,000 Cycles	20,000 Cycles	30,000 Cycles	TOTAL			
Relative Capacity								
Torque Variation								

Tables 1 of the Appendix contains chatter test results from 1,000cycles.
John Deere JDQ-96 Performed using 1400 Series Axle

Oil Code: AL-27793-L

E.O.T. Date: October 12, 2007

Appendix

Tables

1. Table 1 - Durability results 1,000 cycles Candidate Oil

October 12, 2007

This oil created too much noise and vibration in the axle. The test was suspended after 441 cycles out of intended 1000 cycles. No Torque variation data was taken for fear of damaging the equipment.

SwRI Oil Code

swri code

AL-27793-L Sponsor Oil Code

		Temp	0		0) O	0 0	0	, 0	0	0	0	0	0	0	0	0	0	0	0	0	0
	I Temp. 71°C	Variation	C		0 0	, 0	0 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	C
	ō	Toraue		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
FION in Nm		Temp,	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
and VARIA	I Temp. 60°C	Variation	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
TS (TORQUE	Ö	Torque	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
ST RESUL	il Temp. 49°C	Temp.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
RIATION TE		Variation	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
TORQUE VA	Ö	Torque	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	U	Temp.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	Jil Temp. 32°	Variation	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
		Torque	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Brake	Press.	(kPa)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Axle	Speed	(rpm)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
																						- 1

—			r				<u> </u>
SwRI	Variation	(MM)	0	0	0	0	0
Torque	Variation	(MM)	0	0	0	0	0
Relative	Capacity	(MM)	0	0	0	0	0
	Temp	(°C)	32	49	60	71	TOTAL

SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

FUELS AND LUBRICANTS RESEARCH DIVISION

Report on

CATERPILLAR TO-4 FRICTION PROPERTIES, VC-70

Conducted for

SWRI ARMY LAB

Oil Code: AL-27875-L

Test Number: VC70-A-85-I

November 20, 2007

Submitted by:

Brian Koehler Principal Engineer Specialty & Driveline Fluids Evaluations





CATERPILLAR TO-4 FRICTION PROPERTIES, VC-70



Summary Sheet

Company: Test Number: Test start date: End of test date: Oil Code:	SWRI VC70- Noven Noven AL-278	ARMY LAB A-85-I nber 16, 200 nber 20, 200 375-L)7)7				
Sequence Number	1219	1220	1221	1222	1223	1224	Friction Retention
Dynamic Coefficient Vs. Cycle:	F	N/A	P	P	F	F	N/A
Dynamic Coefficient Vs. Load:	F	N/A	P	P	F	P	
Dynamic Coefficient Vs. Speed:	F	N/A	P	F	F	P	
Energy Limit:	P	N/A	P	P	P	P	
Static Coefficient Vs. Cycle:							N/A
Static Coefficient							
/s. Load:	P	N/A	P	F	F	P	
Static Coefficient /s. Speed:	P	N/A	P	F	F	F	
Energy Limit:	P	N/A	P	P	P	P	
Total Wear:	0.015	N/A	0.020	0.054	0.032	0.019	
Vear Limit:	0.030	0.040	0.070	0.070	0.070	0.040	
Comments:	The limit in this sta	lines show Ind.	n are from	the last tin	ne the strai	ght grade C	CAT reference oil was ru

Test name: A-85-I Test date: 11/15/07 Test description: IMachineAL-27875-1 Oil type: AL-27875-L/LO-224036 Viscosity: 5W-40 Miscellaneous: Software version: 1.40 Run name & desc: I0706119 - AL-27875-L Run date: 11/16/07 Oil temperature: 82 degrees C Oil flow rate: 3.78 liter/minute Operator: JG Remarks: I Machine oil test AL-27875-L / LO-224036 Sequence name: SE01219 Remarks: Use 1Y0708 Disc and 1Y3610 Plate Number of cycles run: 1169 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0708 - Elastomeric Disc Material: Raybestos 6475-4 Rayflex Single Lead Spiral - 12 Radial Groove pattern: Miscellaneous: Use with 1Y3610 Steel Plate Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm) : 128.21 Batch number: 26NO0-00004 Remarks: Elastomeric Plate name & desc: 1Y3610 - Steel Plate Surface: 0.70 to 1.30 micron Roughness Install the side marked with the average roughness Miscellaneous: Batch number: 26NO0-00004 Remarks: 1.02 Surface finish LIM1219 - Reference run: I0706090 Report limit name: Limit file generated: 09/24/07 Report format name: REP1219 - ELASTOMERIC, RAYFLEX



1Y0708 DISC THICKNESS

	Oute	r Diam	leter	Inner Diameter							
Loc	Ml	M2	M3	M1	M2	MЗ					
1	4.96	4.95	4.94	4.95	4.95	4.94					
2	4.97	4.96	4.95	4.96	4.95	4.94					
3	4.96	4.96	4.95	4.96	4.95	4.94					
4	4.96	4.96	4.95	4.96	4.95	4.94					
5	4.96	4.96	4.95	4.95	4.95	4.94					
6	4.96	4.96	4.94	4.95	4.95	4.94					
Avg	4.96	4.96	4.95	4.96	4.95	4.94					
	Compression set average wear: 0.004 M2 - M3 average Wear: 0.011										









Test name: A-85-I Test date: 11/15/07 Test description: IMachineAL-27875-1 Oil type: AL-27875-L/LO-224036 Viscosity: 5W-40 Miscellaneous: Software version: 1.40 Run name & desc: I0706120 - AL-27875-L Run date: 11/17/07 82 degrees C Oil temperature: Oil flow rate: 3.78 liter/minute MTD Operator: "I" MACHINE OIL TEST AL-27875-L / LO-224036 Remarks: Sequence name: SE01221 Remarks: Use 1Y0710 Disc and 1Y3610 Plate. Number of cycles run: 1085 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0710 - Steering Brake Paper Material: Raybestos 7894-4 Paper Groove pattern: 2 - 37 Multiple Parallel Miscellaneous: Use with 1Y3610 Steel Plate Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm) : 128.21 Batch number: 23MR9-00001 Remarks: STEERING BRAKE PAPER Plate name & desc: 1Y3610 - Steel Plate Surface: 0.70 to 1.30 micron Roughness Miscellaneous: Install the side marked with the average roughness Batch number: 23MR9-00001 Remarks: 0.93 Surface Finish Report limit name: LIM1221 - Reference run: I0706003 Limit file generated: 07/26/06 Report format name: REP1221 - STEERING BRAKE PAPER



1Y0710 DISC THICKNESS

T	Oute	r Diam	eter	Inner Diameter							
LOC	ΜT	ΜZ	M3	Μ⊥	M2	M3					
1	5.01	4.99	4.99	5.01	5.00	5.00					
2	5.02	5.00	4.99	5.02	5.00	4.99					
3	5.02	5.01	5.00	5.02	5.01	5.00					
4	5.02	5.01	5.01	5.02	5.01	5.00					
5	5.01	5.00	4.99	5.01	5.00	4.99					
6	5.01	5.00	4.99	5.01	5.00	4.99					
Avg	5.02	5.00	4.99	5.02	5.00	5.00					
	Compression set average wear: 0.013 M2 - M3 average Wear: 0.008										









Page 12 of 27

Test name: A-85-I Test date: 11/15/07 Test description: IMachineAL-27875-1 Oil type: AL-27875-L/LO-224036 Viscosity: 5W-40 Miscellaneous: Software version: 1.40 Run name & desc: I0706121 - AL-27875-L Run date: 11/18/07 Oil temperature: 82 degrees C Oil flow rate: 3.78 liter/minute Operator: JG Remarks: Machine I Oil Test AL-27875-L / LO-224036 Sequence name: SE01222 Use 1Y0711 Disc and 1Y0726 Plate Remarks: Number of cycles run: 1195 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0711 - Wheel Brake Paper Material: Raybestos 7902-1 Paper Groove pattern: 2 - 37 Multiple Parallel Miscellaneous: Use with 1Y0726 Steel Plate Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius 128.21 (mm) : Batch number: 24FE9-00001 Remarks: Wheel brake paper Plate name & desc: 1Y0726 - Steel Plate 0.30 micron Maximum Roughness Surface: Install the side marked with the average roughness Miscellaneous: Batch number: 24FE9-00001 Remarks: 0.20 Surface Finish Report limit name: LIM1222 - Reference run: I0706004 Limit file generated: 07/26/06 Report format name: REP1222 - WHEEL BRAKE PAPER



1Y0711 DISC THICKNESS

	Oute	r Diam	eter	Inner Diameter							
Loc	M1	M2	M3	M1	M2	M3					
1	4.90	4.85	4.84	4.90	4.86	4.85					
2	4.89	4.84	4.83	4.89	4.85	4.84					
3	4.89	4.84	4.83	4.89	4.85	4.84					
4	4.91	4.86	4.85	4.91	4.86	4.86					
5	4.91	4.87	4.86	4.91	4.87	4.87					
6	4.91	4.86	4.85	4.91	4.86	4.85					
Avg	4.90	4.85	4.84	4.90	4.86	4.85					
	Compression set average wear: 0.046 M2 - M3 average Wear: 0.008										









Test name: A-85-I Test date: 11/15/07 Test description: IMachineAL-27875-1 AL-27875-L/LO-224036 Oil type: Viscosity: 5W-40 Miscellaneous: Software version: 1.40 Run name & desc: I0706122 - AL-27875-L Run date: 11/19/07 Oil temperature: 82 degrees C Oil flow rate: 3.78 liter/minute Operator: JG "I" MACHINE OIL TEST AL-27875-L / LO-224036 Remarks: Sequence name: SE01223 Remarks: Use 1Y0712 Disc and 1Y0726 Plate Number of cycles run: 1006 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0712 - Transmission Paper Material: Raybestos 7901-2 Paper Groove pattern: 2 - 37 Multiple Parallel Miscellaneous: Use with 1Y0726 Steel Plate Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm) : 128.21 Batch number: 27MR9-00001 Remarks: TRANSMISSION PAPER Plate name & desc: 1Y0726 - Steel Plate Surface: 0.30 micron Maximum Roughness Miscellaneous: Install the side marked with the average roughness Batch number: 27MR9-00001 Remarks: 0.21 Surface Finish LIM1223 - Reference run: I0706006 Report limit name: Limit file generated: 07/26/06 Report format name: REP1223 - TRANSMISSION PAPER



1Y0712 DISC THICKNESS

	Oute	r Diam	eter	Inner Diameter							
Loc	Ml	M2	M3	M1	M2	MЗ					
1	5.01	4.99	4.98	5.01	4.99	4.98					
2	5.02	4.99	4.98	5.02	4.99	4.98					
3	5.03	5.01	5.00	5.03	5.01	4.99					
4	5.02	5.00	4.99	5.02	5.00	4.99					
5	5.01	4.98	4.98	5.01	4.99	4.98					
6	5.01	4.99	4.98	5.01	4.99	4.98					
Avg	5.02	4.99	4.99	5.02	5.00	4.98					
	Compression set average wear: 0.022 M2 - M3 average Wear: 0.010										









Southwest research institute I machine oil test AL-27875-L/L)-224036

Test name: A-85-I Test date: 11/15/07 Test description: IMachineAL-27875-1 Oil type: AL-27875-L/LO-224036 Viscosity: 5W-40 Miscellaneous: Software version: 1.40 Run name & desc: I0706123 - AL-27875-L Run date: 11/20/07 Oil temperature: 82 degrees C 3.78 liter/minute Oil flow rate: Operator: hc Remarks: "I" MACHINE OIL TEST AL-27875-L / LO-224036 Sequence name: SE01224 Remarks: Use 1Y0713 Disc and 8E4095 Plate Number of cycles run: 1085 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² 1Y0713 - Elastomeric Disc Disc name & desc: Caterpillar F37 Material: Groove pattern: Single Lead Spiral - 12 Radial Miscellaneous: Use with 8E4095 Steel Plate Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm) : 128.21 Batch number: C63007FE1 Remarks: ELASTOMERIC Plate name & desc: 8E4095 - Steel Plate Surface: 0.70 to 1.00 micron Roughness Miscellaneous: Install the side marked with the average roughness Batch number: C63007FE1 Remarks: 0.89 SURFACE FINISH LIM1224 - Reference run: I0706007 Report limit name: Limit file generated: 07/26/06 Report format name: REP1224 - ELASTOMERIC, F37



1Y0713 DISC THICKNESS

	Oute	r Diam	leter	Inner Diameter				
Loc	Ml	M2	M3	M1	M2	MЗ		
1	5.05	5.04	5.03	5.05	5.04	5.03		
2	5.05	5.04	5.03	5.05	5.04	5.03		
3	5.05	5.04	5.03	5.05	5.04	5.03		
4	5.05	5.04	5.03	5.05	5.04	5.03		
5	5.04	5.04	5.03	5.05	5.04	5.03		
6	5.05	5.04	5.03	5.05	5.04	5.03		
Avg	5.05	5.04	5.03	5.05	5.04	5.03		
	Compr M2 -	ession M3 ave	set aven rage Wean	cage weat	r: 0. 0	009		









SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

Fuels and Lubricants Research Division

Report on

CATERPILLAR TO-4 FRICTION PROPERTIES, VC-70

Conducted for

SWRI-ARMY LAB

Oil Code: AL-27875-L

Test Number: VC70-A-100-I

January 24, 2008

Submitted by: 24

Brian Koehler Principal Engineer Specialty & Driveline Fluids Evaluations



The results of this report relate only to the fluid tested.

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CATERPILLAR TO-4 FRICTION PROPERTIES, VC-70



Summary Sheet

Company: Test Number: Test start date: End of test date: Oil Code:	SWR VC70 Janua Janua AL-27	I-ARMY LAB I-A-100-I ary 19, 2008 ary 24, 2008 '875-L					
Sequence Number	N/A	1220	N/A	N/A	N/A	N/A	Friction Retention
Dynamic Coefficient Vs. Cycle:	N/A	Р	N/A	N/A	N/A	<u>N/A</u>	F
Dynamic Coefficient Vs. Load:	_ <u>N/A</u>	P	N/A	N/A	N/A	N/A	
Dynamic Coefficient Vs. Speed:	N/A	P	<u>N/A</u>	N/A	_ N /A	N/A	
Energy Limit:	_N/A	P	N/A	N/A	_N/A	N/A	
Static Coefficient Vs. Cycle:							N/A
Static Coefficient Vs. Load:	N/A	P	N/A	_N/A	N/A	_N/A	
Static Coefficient Vs. Speed:	N/A	P	_N/A	<u>N/A</u>	N/A	<u>N/A</u>	
Energy Limit:	N/A	P	_N/A	<u>N/A</u>	N/A	N/A	
Total Wear:	N/A	0.015	N/A	N/A	N/A	N/A	
Wear Limit:	N/A	0.040	N/A	N/A	N/A	N/A	
Comments:	The limit	ts shown are f	for the las	t time the (CAT TO-4	straight grad	le reference oil was run.

Southwest Research Institute I machine oil test AL-27875-L / LO-224036

Test name: A-100-I 01/19/08 Test date: Test description: AL-27875-L Oil type: AL-27875-L /LO-224036 Viscosity: 5W-40 Miscellaneous: Software version: 1.40 Run name & desc: I0706163 - AL-27875-L / LO-224036 01/19/08 Run date: 115 degrees C Oil temperature: Oil flow rate: 3.78 liter/minute Operator: JG Remarks: I Machine oil test AL-27875-L / LO-224036 Sequence name: SEOFRRET USE 1Y0709 DISC AND 1Y0726 PLATE (8E7351 GROUP) Remarks: Number of cycles run: 25100 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0709 - Sintered Bronze Material: Raybestos 1349-ET Bronze Single Lead Spiral - 12 Radial Groove pattern: Use with 8E4095 Steel Plate for performance run Miscellaneous: Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm) : 128.21 Batch number: 12FE1-00010 Remarks: Sintered bronze Plate name & desc: 1Y0726 - Steel Plate Surface: 0.30 micron Maximum Roughness Miscellaneous: Install the side marked with the average roughness Batch number: 12FE1-00010 Remarks: 0.14 surface finish Report limit name: LIMFRRET - Reference run: 10706151 Limit file generated: 01/14/08 **REPFRRET - FRICTION RETENTION** Report format name:



Coefficient

Test name: A-100-I Test date: 01/19/08 Test description: AL-27875-L AL-27875-L /LO-224036 Oil type: Viscosity: 5W-40 Miscellaneous: Software version: 1.40 Run name & desc: I0706164 - AL-27875-L Run date: 01/24/08 Oil temperature: 82 degrees C Oil flow rate: 3.78 liter/minute Operator: mtd Remarks: AL-27875-L / LO-224036 Sequence name: SE01220 Use 1Y0709 Disc and 8E4095 Plate Remarks: Number of cycles run: 1079 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0709 - Sintered Bronze Material: Raybestos 1349-ET Bronze Single Lead Spiral - 12 Radial Groove pattern: Miscellaneous: Use with 8E4095 Steel Plate for performance run Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm): 128.21 Batch number: 12FE1-00010 Remarks: Sintered bronze Plate name & desc: 8E4095 - Steel Plate Surface: 0.70 to 1.00 micron Roughness Miscellaneous: Install the side marked with the average roughness Batch number: 12FE1-00010 Remarks: 0.87 surface finish Report limit name: LIM1220 - Reference run: I0706159 Limit file generated: 01/15/08 Report format name: REP1220 - SINTERED BRONZE



1Y0709 DISC THICKNESS

	Oute	r Diam	eter	Inner Diameter					
Loc	Ml	M2	МЗ	Ml	M2	M3			
1	5.01	4.99	4.99	5.01	5.00	4.99			
2	5.00	4.99	4.99	5.01	4.99	4.99			
3	5.00	4.99	4.99	5.01	5.00	4.99			
4	4.99	4.98	4.98	4.99	4.98	4.98			
5	5.00	5.00	4.99	5.01	5.00	5.00			
6	5.01	5.00	4.99	5.01	4.99	4.99			
Avg	5.00	4.99	4.99	5.01	4.99	4.99			
	Compre M2 - N	ession 13 avei	set averag rage Wear:	ge wea: 0.003	r: 0.(3)12			





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SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

Fuels and Lubricants Research Division

Report on

John Deere JDQ-96 Performed using 1400 Series Axle

Conducted for

ARMY LAB

AL-27875-L

Test Number 07019

October 16, 2007

Submitted by:

Michael Jorese

Michael D. Lochte Manager Specialty & Driveline Fluids Evaluations



The results of this report relate only to the items tested. This report shall not be reproduced, except in full, without the written approval of Southwest Research Institute®.



John Deere JDQ-96 Performed using 1400 Series Axle

General Information

Purpose

The purpose of this test was to evaluate the anti-chatter properties of this oil on the brakes of a 1400 series John Deere Inboard Planetary Axle.

Test Procedure

The test was performed as specified by John Deere Product Engineering. The only changes made to the Deere procedure were those necessary to compensate for a different spiral bevel gear ratio. This procedure is proprietary to Deere and Company.

Data Interpretation

The capacity for each engagement is the average torque during the middle of the engagement. The torque variation is the greatest difference between the maximum and minimum torque recorded during any 0.2-second portion of the engagement. The SwRI variation is the sum of all differences between the maximum torque and minimum torque for each engagement. It is obtained by summing all torque variations of each 0.2-second time block of all engagements.

Test Number

The run number listed on this report is a random number and is not sequential. Only SwRI® can link this run number to JDQ-96, AL-27875-L, October 16, 2007.



John Deere JDQ-96 Performed using 1400 Series Axle

Results

Oil Code: AL-27875-L E.O.T. Date: October 16, 2007
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The candidate results can be compared to the baseline reference average. Pass or fail decisions are only made by John Deere Product Engineering. The current reference baseline average is the average of the five most recent tests.

	Current Reference Baseline Average (N · m)									
	1,000 Cycles	10,000 Cycles	20,000 Cycles	30,000 Cycles	TOTAL					
Relative Capacity	338,535	338,534	341,629	343,274	1,361,972					
Torque Variation	79,214	84,272	79,152	74,708	317,346					

	Results From Test Candidate AL-27875-L										
	1,000 Cycles	10,000 Cycles	20,000 Cycles	30,000 Cycles	TOTAL						
Relative Capacity	348.512										
Torque Variation	179,060										

Tables 1 of the Appendix contains chatter test results from 1,000cycles. Table 2 contains results of the five current baseline reference tests. Figures 1 through 4 are graphic presentations of candidate oil performance compared to baseline reference data.

Figure 5 is a graphic presentation of 1000-cycle reference results and AL-27875-L. Table 3 contains the history of reference tests.

Oil Code: AL-27875-L

E.O.T. Date: October 16, 2007

Appendix

Tables

- 1. Table 1 Durability results 1,000 cycles Candidate Oil
- 2. Table 2 Reference Data Compared to Candidate Data
- 3. Figure 1 & Figure 2 Torque Variation Chart
- 4. Figure 3 & Figure 4 Relative Capacity & Average Disk Thickness Chart
- 5. Figure 5 Graphic presentation of 1000 cycle reference results & Candidate
- 6. Table 3 History of reference tests

October 16, 2007

TABLE 1: JDQ-96 DURABILITY TEST RESULTS 1,000 CYCLES

SwRI Oil Code

LO-224036

Sponsor Oil Code AL-27875-L

—			-																			
	0	Temp.	72	71	71	72	72	73	73	72	72	72	73	72	72	71	71	70	70	71	71	71
	il Temp. 71°(Variation	2320	2340	2870	3640	4390	1700	1590	1630	1610	1560	1540	1520	006	1030	2570	2950	2920	5190	3770	4250
(1	0	Torque	4564	4314	4405	4248	4125	4464	4340	4358	4223	4177	4346	4194	1805	2614	3186	4075	5026	6255	7214	8289
TION in Nrr	0	Temp.	62	60	59	58	59	60	60	61	61	61	61	61	60	59	59	60	60	60	60	60
and VARIA	il Temp. 60°(Variation	2340	2310	2900	3400	3940	1210	1170	1330	1360	1330	1260	1200	800	1760	2750	2830	3000	3230	3740	3640
TS (TORQUE	0	Torque	4464	4250	3962	3931	3865	4080	4044	4071	3952	3934	4125	4016	1751	2409	3189	4132	5076	5944	6893	7932
ST RESUL	0	Temp.	51	49	49	48	48	49	49	50	50	51	48	49	50	49	47	50	50	50	50	50
<i>IRIATION TE</i>	il Temp. 49°(Variation	2270	2290	2920	3610	3720	1100	960	1030	1130	1100	066	1000	740	880	2800	2840	2780	3090	4420	3300
TORQUE VA	0	Torque	4280	4212	3998	4000	3948	4189	4113	4178	4084	4048	3943	3920	1740	2606	3168	4135	5106	5970	6921	7875
•	0	Temp.	25	26	26	26	26	26	27	28	29	30	31	33	32	31	31	31	31	31	31	32
	0il Temp. 32°(Variation	4030	4260	3120	720	760	780	710	190	770	740	690	780	450	630	2780	2990	3080	2940	4460	4820
		Torque	3914	4235	4055	4051	4104	4125	4103	4138	4093	4049	4052	4062	1633	2463	3108	3963	4925	5944	6908	7911
Brake	Press.	(kPa)	3831	3831	3831	3831	3831	3831	3831	3831	3831	3831	3831	3831	1532	2300	3065	3831	4598	5364	6130	7050
Axle	Speed	(rpm)	ω	10	15	20	25	30	35	40	45	50	55	60	15	15	15	15	15	15	15	15

	Relative	Torque	SwRI
Temp	Capacity	Variation	Variation
(°C)	(MM)	(Nm)	(MM)
32	85,836	40,300	537,410
49	86,434	42,970	489,820
60	86,019	45,500	525,270
71	90,222	50,290	584,580
TOTAL	348,512	179,060	2,137,080

TABLE 2: JDQ-96 REFERENCE DATA COMPARED TO CANDIDATE DATA

EOT Date: October 16, 2007 Oil Code : AL-27875-L

Reference Oil Coded : 692	X31111i			-	Average Facing
	Cycles	Relative Capacity	Torque Variation	SwRI Variation	Thickness
First Reference Run					(millimeters)
	1,000	326,304	57,420	730,050	7.60
	10,000	331,809	64,900	804,030	7.50
	20,000	345,325	69,500	899,880	7.44
	30,000	341,770	66,210	810,190	7.39
	Total	1,345,208	258,030	3,244,150	
Second Reference Run					
	1,000	337,791	66,660	848,580	7.60
	10,000	338,055	92,240	1,129,330	7.55
	20,000	343,166	77,010	1,001,920	7.49
	30,000	350,470	73,280	863,980	7.44
	Total	1,369,482	309,190	3,843,810	
Third Reference Run					
	1,000	339,375	100,390	1,204,240	7.56
	10,000	335,754	106,780	1,079,450	7.52
	20,000	334,120	84,770	1,030,270	7.49
	30,000	335,614	79,620	1,021,190	7.47
	Total	1,344,863	371,560	4,335,150	
Fourth Reference Run					
Run on new backing pla	1,000	343,906	79,990	1,020,120	7.48
and piston	10,000	343,056	72,520	893,570	7.30
	20,000	342,668	69,920	885,870	7.07
	30,000	345,315	70,360	833,920	6.90
	Total	1,374,945	292,790	3,633,480	
Invalid test run on same	1,000	348,860	132,110	1,721,010	
backing plate and pistor	10,000	323,093	153,860	1,919,720	
as test above was run on					
Fifth Reference Run					
most recent run	1,000	345,296	91,610	1,125,260	7.50
Run on new backing	10,000	343,999	84, 9 20	1,019,400	7.33
plate and piston	20,000	342,864	94,560	1,264,070	7.22
	30,000	343,201	84,070	1,052,400	7.11
	Total	1,375,360	355,160	4,461,130	
AL-27875-L		Candidate (Oil Test Results		
	1,000	348,512	179,060	2,137,080	
	10,000				
	20,000				
	30,000				
	Total	348,512	179,060	2,137,080	









October 16, 2007

History of 1000 cycle reference tests.

		Torque variation at 1000 cycles
69X31111k	1999 brake disk	103,360
69X31111K	1997 brake disk	129,540
60Y31111k	2000 brake disk	121,120
69X31111k	2000 brake disk	135 700
69X31111k	2000 brake disk	138 760
69X31111k	2000GDD brake di	140,830
69X31111k	2000GDD brake	144.820
69X31111k	2000GDD brake	124,310
69X31111k	2000 GDD brake	131,860
69X31111k	2000 GDD brake	105,010
69X31111k	2000 GDD brake	109,220
69X31111k	2000 GDD brake	142,510
69X31111K	2000 GDD brake	128,080
69X31111k	2000 GDD brake	109,100
69X31111k	2000 GDD brake	90.070
69X31111k	2000 GDD brake	90,810
69X31111k	2000 GDD brake	79,930
69X31111k	2000 GDD brake	79,930
69X31111k	2000 GDD brake	83,190
69X31111k	2000 GDD brake	81,220
69X31111k	2000 GDD brake	85,570
68X31111k	2000 GDD brake	64,170
69X31111K	2000 GDD brake	67,390
69X31111k	2000 GDD brake	96 730
69X31111k	2000 GDD brake	90,390
69X31111k	2000 GDD brake	99,960
69X31111k	2000 GDD brake	87,380
69X31111k	2000 GDD brake	74,720
69X31111k	2000 GDD brake	74,940
69X31111K	2000 GDD brake	85,980
60X31111k	2000 GDD brake	94,410
69X31111k	2000 GDD blake	90.950
69X31111k	2000 GDD brake	83,190
69X31111k	2000 GDD brake	105.210
69X31111k	2000 GDD brake	91,960
69X31111k	2000 GDD brake	97,320
69X31111k	2000 GDD brake	75,040
69X31111k	2000 brake disk	86,060
69X31111K	2000 brake disk	68,590
69X31111K	2003 brake disk	57,420
69X31111k	2003 brake disk	76 260
69X31111k	2003 brake disk	86 210
69X31111k	2003 brake disk	84.550
69X31111k	2003 brake disk	66,660
69X31111k	2003 brake disk	84,760
69X31111k	2003 brake disk	87,800
69X31111k	2003 brake disk	100,390
69X31111k	2003 brake disk	96,620
69X31111K	2003 brake disk	106,710
60Y21111k		70,000
69X31111k	NEW BACKING FI	98.440
69X31111k		106.370
69X31111k		110.040
69X31111k		127,550
69X31111k		111,280
69X31111k	invalid run	132,110
	NEW BACKING	
69X31111k	Plate and piston	91,610
	NEW BACKING	
69X31111k	Plate and piston	92,230
	plate used for 1	
69X31111k	test	89,200
	same brake plate	
Al -27875-I	and pistori ds	179.060
	00010	175,000





Figure 5

October 16, 2007

SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

FUELS AND LUBRICANTS RESEARCH DIVISION

Report on

CATERPILLAR TO-4 FRICTION PROPERTIES, VC-70

Conducted for

SWRI ARMY LAB

Oil Code: AL-27876-L

Test Number: VC70-A-86-I

November 28, 2007

Submitted by:

Brian Koehler

Principal Engineer Specialty & Driveline Fluids Evaluations



CATERPILLAR TO-4 FRICTION PROPERTIES, VC-70



Summary Sheet

Company: Test Number: Test start date: End of test date: Oil Code:	SWRI VC70-, Nover Nover AL-278	ARMY LAB A-86-I Iber 24, 2007 Iber 28, 2007 376-L					
Sequence Number	1219	1220	1221	1222	1223	1224	Friction Retention
Dynamic Coefficient Vs. Cycle:	F	N/A	P	F	F	P	N/A
Dynamic Coefficient Vs. Load:	F	N/A	P	F	F	P	
Dynamic Coefficient Vs. Speed:	F	N/A	P	F	F	P	
Energy Limit:	P	N/A	P	P	P	P	
Static Coefficient Vs. Cycle:							N/A
Static Coefficient Vs. Load:	P	N/A	P	F	F	P	
Static Coefficient Vs. Speed:	P	N/A	P	P	F	F	
Energy Limit:	<u>P</u>	N/A	P	P	P	P	
Total Wear:	0.013	<u>N/A</u>	0.046	0.038	0.037	0.016	
Wear Limit:	0.030	0.040	0.070	0.070	0.070	0.040	
Comments: with the single grade C	The limits AT referer	s shown on th nce oil.	ese report	pages are f	from the last	time the tes	t stand was referenced

F = Fail P = Pass N/A = Not Applicable

Test name: A-86-I Test date: 11/21/07 Test description: I MACHINE AL-27876-L Oil type: Viscosity: Miscellaneous: Software version: 1.40 Run name & desc: I0706124 - AL-27876-L Run date: 11/24/07 Oil temperature: 82 degrees C Oil flow rate: 3.78 liter/minute Operator: JG Remarks: "I" MACHINE OIL TEST AL-27876-L / LO-224037 Sequence name: SE01219 Remarks: Use 1Y0708 Disc and 1Y3610 Plate Number of cycles run: 1094 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0708 - Elastomeric Disc Material: Raybestos 6475-4 Rayflex Single Lead Spiral - 12 Radial Groove pattern: Use with 1Y3610 Steel Plate Miscellaneous: Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm) : 128.21 Batch number: 26NO0-00004 Remarks: ELASTOMERIC Plate name & desc: 1Y3610 - Steel Plate Surface: 0.70 to 1.30 micron Roughness Miscellaneous: Install the side marked with the average roughness Batch number: 26N00-00004 Remarks: 0.88 SURFACE FINISH Report limit name: LIM1219 - Reference run: I0706090 Limit file generated: 09/24/07 Report format name: REP1219 - ELASTOMERIC, RAYFLEX



1Y0708 DISC THICKNESS

	Outer	c Diame	eter	Inne	r Diam	eter
Loc	Ml	M2	MЗ	M1	M2	M3
1	4.96	4.95	4.95	4.96	4.94	4.94
2	4.96	4.95	4.95	4.96	4.94	4.94
3	4.96	4.95	4.95	4.96	4.95	4.95
4	4.97	4.96	4.96	4.97	4.96	4.96
5	4.97	4.96	4.96	4.97	4.96	4.96
6	4.97	4.96	4.96	4.97	4.95	4.95
Avg	4.97	4.95	4.95	4.97	4.95	4.95
	Compre M2 - N	ession 13 avei	set averag rage Wear:	ge wear 0.000	r: 0.()13





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Test name: A-86-I 11/21/07 Test date: Test description: I MACHINE AL-27876-L Oil type: Viscosity: Miscellaneous: Software version: 1.40 Run name & desc: I0706125 - AL-27876-L Run date: 11/25/07 Oil temperature: 82 degrees C Oil flow rate: 3.78 liter/minute Operator: JG Remarks: "I" MACHINE OIL TEST AL-27876-L / LO-224037 Sequence name: SE01221 Remarks: Use 1Y0710 Disc and 1Y3610 Plate. Number of cycles run: 1113 Machine: Ι Coast down check run: 07/19/02 151.76 seconds Result: 07/19/02 Inertia check run: Result: 1.0288 N-m-s² Disc name & desc: 1Y0710 - Steering Brake Paper Raybestos 7894-4 Paper Material: 2 - 37 Multiple Parallel Groove pattern: Miscellaneous: Use with 1Y3610 Steel Plate Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius 128.21 (mm) : Batch number: 23MR9-00001 Remarks: STEERING BRAKE PAPER Plate name & desc: 1Y3610 - Steel Plate Surface: 0.70 to 1.30 micron Roughness Miscellaneous: Install the side marked with the average roughness Batch number: 23MR9-00001 Remarks: 0.87 SURFACE FINISH Report limit name: LIM1221 - Reference run: I0706003 Limit file generated: 07/26/06 Report format name: REP1221 - STEERING BRAKE PAPER



1Y0710 DISC THICKNESS

	Oute	r Diam	eter	Inne	r Diam	eter
Loc	Ml	M2	M3	Ml	M2	МЗ
1	5.06	5.02	5.01	5.06	5.03	5.02
2	5.06	5.02	5.01	5.06	5.02	5.01
3	5.06	5.02	5.01	5.06	5.02	5.01
4	5.05	5.02	5.01	5.05	5.02	5.01
5	5.06	5.03	5.02	5.06	5.03	5.02
6	5.07	5.03	5.02	5.07	5.03	5.02
Avg	5.06	5.02	5.01	5.06	5.03	5.01
	Compre M2 - N	ession M3 ave:	set averag rage Wear:	ge wea: 0.01	r: 0. 0	036





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Test name: A-86-I Test date: 11/21/07 Test description: I MACHINE AL-27876-L Oil type: Viscosity: Miscellaneous: Software version: 1.40 Run name & desc: I0706126 - AL-27876-L Run date: 11/26/07 82 degrees C Oil temperature: Oil flow rate: 3.78 liter/minute Operator: JG Remarks: "I" MACHINE OIL TEST AL-27876-L / LO-224037 Sequence name: SE01222 Remarks: Use 1Y0711 Disc and 1Y0726 Plate Number of cycles run: 1142 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0711 - Wheel Brake Paper Material: Raybestos 7902-1 Paper 2 - 37 Multiple Parallel Groove pattern: Miscellaneous: Use with 1Y0726 Steel Plate Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm) : 128.21 Batch number: 24FE9-00001 Remarks: WHEEL BRAKE PAPER Plate name & desc: 1Y0726 - Steel Plate Surface: 0.30 micron Maximum Roughness Miscellaneous: Install the side marked with the average roughness Batch number: 24FE9-00001 0.19 SURFACE FINISH Remarks: LIM1222 - Reference run: I0706004 Report limit name: Limit file generated: 07/26/06 REP1222 - WHEEL BRAKE PAPER Report format name:



1Y0711 DISC THICKNESS

	Oute	r Diam	eter	Inne	r Diam	eter
Loc	Ml	M2	M3	M1	M2	МЗ
1	4.88	4.84	4.84	4.88	4.85	4.84
2	4.87	4.84	4.83	4.87	4.84	4.83
3	4.88	4.85	4.84	4.88	4.85	4.84
4	4.88	4.86	4.85	4.89	4.85	4.85
5	4.88	4.85	4.85	4.88	4.86	4.85
6	4.89	4.86	4.85	4.89	4.85	4.85
Avg	4.88	4.85	4.84	4.88	4.85	4.84
	Compre M2 - N	ession M3 ave:	set averag rage Wear:	ge wea: 0.00	r: 0. 7	031





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Test name: A-86-I 11/21/07 Test date: Test description: I MACHINE AL-27876-L Oil type: Viscosity: Miscellaneous: Software version: 1.40 I0706127 - AL-27876-L Run name & desc: 11/27/07 Run date: Oil temperature: 82 degrees C Oil flow rate: 3.78 liter/minute Operator: HC Remarks: "I" MACHINE OIL TEST AL-27876-L / LO-224037 Sequence name: SE01223 Use 1Y0712 Disc and 1Y0726 Plate Remarks: Number of cycles run: 1054 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0712 - Transmission Paper Material: Raybestos 7901-2 Paper 2 - 37 Multiple Parallel Groove pattern: Use with 1Y0726 Steel Plate Miscellaneous: Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius 128.21 (mm) : Batch number: 27MR9-00001 Remarks: TRANSMISSION PAPER Plate name & desc: 1Y0726 - Steel Plate Surface: 0.30 micron Maximum Roughness Miscellaneous: Install the side marked with the average roughness Batch number: 27MR9-00001 0.25 SURFACE FINISH Remarks: LIM1223 - Reference run: I0706006 Report limit name: Limit file generated: 07/26/06 REP1223 - TRANSMISSION PAPER Report format name:



1Y0712 DISC THICKNESS

	Outer Diameter			Inner Diameter				
Loc	Ml	M2	M3	Ml	M2	MЗ		
1	5.00	4.98	4.95	5.00	4.98	4.96		
2	5.00	4.98	4.97	5.00	4.98	4.96		
3	5.00	4.98	4.97	5.00	4.98	4.97		
4	5.01	4.98	4.97	5.01	4.98	4.97		
5	5.00	4.98	4.97	5.00	4.98	4.97		
6	5.00	4.98	4.96	5.00	4.98	4.96		
Avg	5.00	4.98	4.97	5.00	4.98	4.97		
	Compression set average wear: 0.022 M2 - M3 average Wear: 0.015							





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Test name: A-86-I 11/21/07 Test date: I MACHINE AL-27876-L Test description: Oil type: Viscosity: Miscellaneous: Software version: 1.40 I0706128 - AL-27876-L Run name & desc: Run date: 11/28/07 82 degrees C Oil temperature: Oil flow rate: 3.78 liter/minute HC Operator: "I" MACHINE OIL TEST AL-27876-L / LO-224037 Remarks: Sequence name: SEQ1224 Use 1Y0713 Disc and 8E4095 Plate Remarks: Number of cycles run: 1109 Machine: Ι Coast down check run: 07/19/02 151.76 seconds Result: 07/19/02 Inertia check run: 1.0288 N-m-s² Result: 1Y0713 - Elastomeric Disc Disc name & desc: Caterpillar F37 Material: Groove pattern: Single Lead Spiral - 12 Radial Miscellaneous: Use with 8E4095 Steel Plate 285.80 Outer diameter (mm): Inner diameter (mm): 223.20 (mm): 128.21 Mean radius Batch number: C63007FE1 ELASTOMERIC Remarks: Plate name & desc: 8E4095 - Steel Plate Surface: 0.70 to 1.00 micron Roughness Install the side marked with the average roughness Miscellaneous: Batch number: C63007FE1 0.82 SURFACE FINISH Remarks: Report limit name: LIM1224 - Reference run: I0706007 Limit file generated: 07/26/06 REP1224 - ELASTOMERIC, F37 Report format name:



1Y0713 DISC THICKNESS

	Outer Diameter			Inner Diameter				
Loc	M1	M2	M3	M1	M2	МЗ		
1	5.05	5.04	5.03	5.05	5.04	5.03		
2	5.05	5.03	5.03	5.04	5.03	5.03		
3	5.05	5.04	5.03	5.04	5.04	5.03		
4	5.05	5.04	5.03	5.04	5.04	5.03		
5	5.05	5.04	5.03	5.04	5.04	5.03		
6	5.04	5.03	5.03	5.04	5.03	5.02		
Avg	5.05	5.04	5.03	5.04	5.04	5.03		
	Compression set average wear: 0.008 M2 - M3 average Wear: 0.008							




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SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

Fuels and Lubricants Research Division

Report on

John Deere JDQ-96 Performed using 1400 Series Axle

Conducted for

ARMY LAB

AL-27876-L

Test Number 07498

October 17, 2007

Submitted by:

Michael Source

Michael D. Lochte Manager Specialty & Driveline Fluids Evaluations



The results of this report relate only to the items tested. This report shall not be reproduced, except in full, without the written approval of Southwest Research Institute®.



John Deere JDQ-96 Performed using 1400 Series Axle

General Information

Oil Codo: AL 27976 I	EOT Deter October 17 2007
OII COde. AL-27070-L	E.O.T. Date: October 17, 2007

Purpose

The purpose of this test was to evaluate the anti-chatter properties of this oil on the brakes of a 1400 series John Deere Inboard Planetary Axle.

Test Procedure

The test was performed as specified by John Deere Product Engineering. The only changes made to the Deere procedure were those necessary to compensate for a different spiral bevel gear ratio. This procedure is proprietary to Deere and Company.

Data Interpretation

The capacity for each engagement is the average torque during the middle of the engagement. The torque variation is the greatest difference between the maximum and minimum torque recorded during any 0.2-second portion of the engagement. The SwRI variation is the sum of all differences between the maximum torque and minimum torque for each engagement. It is obtained by summing all torque variations of each 0.2-second time block of all engagements.

Test Number

The run number listed on this report is a random number and is not sequential. Only SwRI® can link this run number to JDQ-96, AL-27876-L, October 17, 2007.



John Deere JDQ-96 Performed using 1400 Series Axle

Results

Oil Code: AL-27876-L	E.O.T. Date: October 17, 2007

The candidate results can be compared to the baseline reference average. Pass or fail decisions are only made by John Deere Product Engineering. The current reference baseline average is the average of the five most recent tests.

	Current Reference Baseline Average (N · m)										
	1,000 Cycles	10,000 Cycles	20,000 Cycles	30,000 Cycles	TOTAL						
Relative Capacity	338,535	338,534	341,629	343,274	1,361,972						
Torque Variation	79,214	84,272	79,152	74,708	317,346						

	Results From Test Candidate AL-27876-L										
-	1,000 Cycles	10,000 Cycles	20,000 Cycles	30,000 Cycles	TOTAL						
Relative Capacity	330,895										
Torque Variation	200,980										

Tables 1 of the Appendix contains chatter test results from 1,000cycles. Table 2 contains results of the five current baseline reference tests. Figures 1 through 4 are graphic presentations of candidate oil performance compared to baseline reference data.

Figure 5 is a graphic presentation of 1000-cycle reference results and AL-27876-L. Table 3 contains the history of reference tests.

Oil Code: AL-27876-L

E.O.T. Date: October 17, 2007

Appendix

Tables

- 1. Table 1 Durability results 1,000 cycles Candidate Oil
- 2. Table 2 Reference Data Compared to Candidate Data
- 3. Figure 1 & Figure 2 Torque Variation Chart
- 4. Figure 3 & Figure 4 Relative Capacity & Average Disk Thickness Chart
- 5. Figure 5 Graphic presentation of 1000 cycle reference results & Candidate
- 6. Table 3 History of reference tests

October 17, 2007

TABLE 1: JDQ-96 DURABILITY TEST RESULTS 1,000 CYCLES

SwRI Oil Code

LO-224037

Sponsor Oil Code AL-27876-L

	0	Temp.	72	72	71	71	71	71	71	71	71	71	71	72	70	69	70	70	70	70	70	70
	il Temp. 71°(Variation	3720	3890	3210	3860	5030	1700	1520	1490	1500	1450	1440	1510	880	1110	2790	3080	3480	3610	4620	7140
	0	Torque	4282	4233	3954	3882	3779	3947	3862	3852	3750	3773	3897	3838	1659	2472	3126	4004	5050	5972	6964	7915
TION in Nm	0	Temp.	61	60	59	58	59	59	60	60	61	61	61	61	59	58	58	59	59	59	59	59
E and VARIA	il Temp. 60°(Variation	3780	4060	3080	3590	4230	1320	1190	1260	1190	1190	1170	1170	880	1050	2860	3020	3490	3460	5650	6270
S (TORQUE	ō	Torque	4165	4112	3867	3832	3808	3906	3823	3821	3739	3695	3811	3632	1641	2408	3086	4058	4791	5743	6638	7678
ST RESULT	0	Temp.	51	50	49	49	49	50	50	50	51	51	48	49	49	48	48	48	48	48	48	48
RIATION TE	il Temp. 49°(Variation	2510	2470	3000	3570	4140	1030	1010	1040	1000	980	910	1020	750	2440	3000	3070	3440	3500	5730	5960
TORQUE VA	0	Torque	4155	4060	3892	3926	3798	3918	3849	3851	3759	3732	3650	3630	1667	2334	3089	3910	4762	5638	6444	7456
•	o	Temp.	29	29	29	29	29	30	32	33	33	35	33	34	32	32	32	32	32	32	33	33
	Jil Temp. 32°	Variation	4150	2610	3160	200	680	770	730	770	780	760	720	770	210	640	2830	3280	3380	3350	3520	5660
		Torque	3924	3947	3761	4006	4001	4014	3992	4041	3983	3943	3730	3730	1554	2315	3185	3932	4774	5727	6738	7613
Brake	Press.	(kPa)	3831	3831	3831	3831	3831	3831	3831	3831	3831	3831	3831	3831	1532	2300	3065	3831	4598	5364	6130	7050
Axle	Speed	(rpm)	ω	10	15	20	25	30	35	40	45	50	55	60	15	15	15	15	15	15	15	15

	Relative	Torque	SwRI
Temp	Capacity	Variation	Variation
(°C)	(MM)	(MM)	(MM)
32	82,912	39,470	539,920
49	81,518	50,570	661,660
60	82,254	53,910	637,060
71	84,211	57,030	679,650
TOTAL	330,895	200,980	2,518,290

TABLE 2: JDQ-96 REFERENCE DATA COMPARED TO CANDIDATE DATA

EOT Date: October 17, 2007 Oil Code : AL-27876-L

Reference Oil Coded : 69	9X31111i			-	Average Facing
	Cycles	Relative Capacity	Torque Variation	SwRI Variation	Thickness
First Reference Run					(millimeters)
	1,000	326,304	57,420	730,050	7.60
	10,000	331,809	64,900	804,030	7.50
	20,000	345,325	69,500	899,880	7.44
	30,000	341,770	66,210	810,190	7.39
	Total	1,345,208	258,030	3,244,150	
Second Reference Run					
	1,000	337,791	66,660	848,580	7.60
	10,000	338,055	92,240	1,129,330	7.55
	20,000	343,166	77,010	1,001,920	7.49
	30,000	350,470	73,280	863,980	7.44
	Total	1,369,482	309,190	3,843,810	
Third Reference Run					
	1,000	339,375	100,390	1,204,240	7.56
	10,000	335,754	106,780	1,079,450	7.52
	20,000	334,120	84,770	1,030,270	7.49
	30,000	335,614	79,620	1,021,190	7.47
	Total	1,344,863	371,560	4,335,150	
Fourth Reference Run					
Run on new backing pla	1,000	343,906	79,990	1,020,120	7.48
and piston	10,000	343,056	72,520	893,570	7.30
	20,000	342,668	69,920	885,870	7.07
	30,000	345,315	70,360	833,920	6.90
	Total	1,374,945	292,790	3,633,480	
Invalid test run on same	1,000	348,860	132,110	1,721,010	
backing plate and pistor	10,000	323,093	153,860	1,919,720	
as test above was run on					
Fifth Reference Run	******				
most recent run	1,000	345,296	91,610	1,125,260	7.50
Run on new backing	10,000	343,999	84,920	1,019,400	7.33
plate and piston	20,000	342,864	94,560	1,264,070	7.22
	30,000	343,201	84,070	1,052,400	7.11
	Total	1,375,360	355,160	4,461,130	
AL-27876-L		Candidate	Oil Test Results		
	1,000	330,895	200,980	2,518,290	
	10,000				
	20,000				
	30,000				
	Total	330,895	200,980	2,518,290	









Figure 3

AL-27876-L

History of 1000 cycle reference tests.

Table 3

	Torq	ue variation at 1000 cycle	es
69X31111k	1999 brake disk	103,360	
69X31111k	1997 brake disk	129,540	
69X31111k	2000 brake disk	121,120	
69X31111K	2000 brake disk	129,620	
69X31111k	2000 brake disk	135,700	
69X31111k	2000 brake disk 2000GDD brake di	130,700	
69X31111k	2000GDD brake ui	144 820	
69X31111k	2000GDD brake	124 310	
69X31111k	2000 GDD brake	131.860	
69X31111k	2000 GDD brake	105,010	
69X31111k	2000 GDD brake	109,220	
69X31111k	2000 GDD brake	142,510	
69X31111k	2000 GDD brake	128,080	
69X31111k	2000 GDD brake	109,100	
69X31111k	2000 GDD brake	111,800	
69X31111k	2000 GDD brake	90,070	
69X31111k	2000 GDD brake	90,810	
69X31111K	2000 GDD brake	79,930	
69X31111K	2000 GDD brake	79,930	
60X21111K	2000 GDD brake	83,190	
60V21111k	2000 GDD brake	01,220	
68¥31111k	2000 GDD brake	64,170	
60X31111k	2000 GDD brake	67 300	
69X31111k	2000 GDD brake	82 / 10	
69X31111k	2000 GDD brake	96,730	
69X31111k	2000 GDD brake	90,390	
69X31111k	2000 GDD brake	99,960	
69X31111k	2000 GDD brake	87,380	
69X31111k	2000 GDD brake	74,720	
69X31111k	2000 GDD brake	74,940	
69X31111k	2000 GDD brake	85,980	
69X31111k	2000 GDD brake	94,410	
69X31111k	2000 GDD brake	74,300	
69X31111k	2000 GDD brake	90,950	
69X31111k	2000 GDD brake	83,190	
69X31111k	2000 GDD brake	105,210	
69X31111k	2000 GDD brake	91,960	
69X31111K	2000 GDD brake	97,320	
69X31111K	2000 GDD brake	75,040	
60V21111k	2000 brake disk	86,060	
60Y31111k	2000 brake disk	68,590 57,400	
60Y31111k	2003 brake disk	57,420	
60X31111k	2003 brake disk	76.260	
69X31111k	2003 brake disk	86 210	
69X31111k	2003 brake disk	84 550	
69X31111k	2000 brake disk	66 660	
69X31111k	2003 brake disk	84 760	
69X31111k	2003 brake disk	87.800	
69X31111k	2003 brake disk	100.390	
69X31111k	2003 brake disk	96,620	
69X31111k	2003 brake disk	106,710	
69X31111k	2003 brake disk	123,110	
69X31111k	NEW BACKING PI	79,990	
69X31111k		98,440	
69X31111k		106,370	
69X31111k		110,040	
69X31111k		127,550	
69X31111k		111,280	
69X31111k	invalid run	132,110	
	NEW BACKING		
69X31111k	Plate and piston	91,610	
	NEW BACKING		
69X31111k	Plate and piston	92,230	
	plate used for 1		
69X31111k	test	89,200	
	same brake plate		
AL 070701	and piston as	000.000	
AL-27876-L	above	200,980	

October 17, 2007



Figure 5

SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

Fuels And Lubricants Research Division

Report on

ALLISON HYDRAULIC TRANSMISSION FLUID, TYPE C-4 GRAPHITE CLUTCH FRICTION TEST

Conducted For

SWRI ARMY LAB

Oil Code: AL-27877-L

Test Number: C4-2-1189

September 11, 2007

Submitted by:

Matthew Jackson Principal Engineer Specialty & Driveline Fluids Evaluation



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	smission					Allison Tra Genei	nsmission Division al Motors
		VIII. Graphite C	lutch Fric	tion Test			
Test Laboratory: Test Number: Friction Plate Batch: Steel Plate Batch:	SWRI C4-2-1189 LOT 43 9/11/2005)		Lab Flu Sponsor Flu Completi	id Code: id Code: on Date:	ATF-2237(AL-27877- 09/11/07	03 L
Clutch Wear Dat	a		······				
		Steel Plates Clutch Plate	Maximum 0.0010 0.0820	Average 0.0002 0.0735			
		Pack Clearance	Before 0.4064	After 0.6350			
Reference Tests				m, un <u>t e terressen et terresse</u>		. <u></u>	
Test Number	Test Date	Test Fluid]			Now	FOT
C4-0-1163	01/19/07	PASS REF-L-06-04		Viscosity at 4	0°C_cSt	58.17	42.61
C4-0-1176	05/05/07	PASS REF-L-06-04		Viscosity at 1	00°C cSt	10.62	8.06
C4-0-1187	8/30/2007	PASS REF-L-06-04]	Iron Content,	ppm	2	71
Γ	D5185	New Fluid (ppm)	1				
F	Ba	<1 <1					
-	B	1					
F	Ca	3595					
	Ma	10					
F	P	1302					
F	Si	4					
	Na	<5					

ALLISON C- 4 GRAPH FRICTION TEST SUMMARY



(Torque in Ft-Lbs)

Sponsor Fluid Code: AL-27877-L	Test Number: C4-2-1189
Lab Fluid Code: ATF-223703	Fric. Plate Batch: LOT 43
Completion Date: 9/11/2007	Steel Plate Batch: 9/11/2005

PHASE A

	SLIP	TORQUE	TORQUE	TORQUE	STATIC PEAK	LOW SPEED	LOWSPEED
CYCLE	TIME	(MIDPOINT)	STATIC PEAK	(.2 Second)	- 0.2 TORQUE	STATIC PEAK	STATIC TORQUE
500	1.11	55	62	52	10	68	60
1000	1.10	56	64	51	13	67	61

PHASE B

	SLIP	TORQUE	TORQUE	TORQUE	STATIC PEAK	LOW SPEED	LOWSPEED
CYCLE	TIME	(MIDPOINT)	STATIC PEAK	(0.2 Second)	- 0.2 TORQUE	STATIC PEAK	STATIC TORQUE
1500	0.73	108	130	104	26	145	129
2000	0.75	106	129	100	29	142	129
2500	0.75	106	128	100	28	141	127
3500	0.76	104	123	95	28	135	128
4000	0.76	105	123	96	27	138	125
4500	0.78	103	120	95	25	141	126
5000	0.77	104	118	96	22	136	126
5500	0.78	103	117	96	21	135	125

	L	Limits		Results		
	Max	Max Change	1,500 N	5,500 N	% Change	P/F
Slip Time Max.	0.81	N/A	0.73	0.78	6.85	Ρ
0.2 Second Dynamic Coeff.	N/A	N/A	0.097	0.090	-7.216	
Mid-Point Fric. Coeff. Min.	0.093	N/A	0.101	0.097	-3.960	Ρ
Static Friction Coeff.	N/A	N/A	0.122	0.110	-9.836	
Low Speed Peak Fric. Coeff.	N/A	N/A	0.136	0.126	-7.353	
0.25 Second Low Speed Coeff.	N/A	N/A	0.121	0.117	-3.306	

SOUTHWEST RESEARCH INSTITUTE®

ALLISON C4-GRAPHITE FRICTION TEST



Candidate Fluid: AT-27877-L Lab Fluid Code : ATF-223703		'7-L	Test Number	: C4-2-1189		Completion	Date : 9/11/2	2007
		703	Steel Plate Batch: 09/11/2005			Fric Plate Batch : LOT 43		
Plates	Location of Tooth	Near Inner Diameter		Near Outer Diameter		Inner Diameter	Average Overall	Outer Diameter
	(Clockwise)	Before	After	Before	After	Change	Change	Change
-	1.1.5		FRIC	TION MATERIAL			ŶI	<u>y</u>
1.1.1.1.1.1	Top	2.2200	2.1510	2.2200	2.1540	0.0690		0.0660
2	120	2.2260	2.1440	2.2280	2.1540	0.0820		0.0740
1	240	2.2230	2.1420	2.2190	2.1500	0.0810		0.0690
5	Average					0.0773	0.0735	0.0697
			STEE	L SEPARATORS	-			
	Тор	1.7520	1.7510	1.7520	1.7520	0.0010		0.0000
1	120	1.7520	1.7520	1.7520	1.7520	0.0000		0.0000
	240	1.7500	1.7500	1.7500	1.7490	0.0000	1	0.0010
	Average					0.0003	0.0003	0.0003
1	Тор	1.7480	1.7480	1.7480	1.7480	0.0000		0,0000
3	120	1.7500	1.7500	1.7500	1,7500	0.0000		0,0000
1	240	1.7500	1.7500	1.7500	1.7500	0.0000		0.0000
1.000	Average					0.0000	0.0000	0.0000

PLATE CONDITION AT E.O.T .: PLATES IN GOOD CONDITION WITH NO UNUSUAL DISCOLORATION

(Anything Unusual)

Test Date:

9/11/2007

Operator's Name:

RAUL VALDEZ

Reviewed By (Signature and Date)

9/14/07

Pack ID#: 4068





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SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

Fuels And Lubricants Research Division

Report on

ALLISON HYDRAULIC TRANSMISSION FLUID, TYPE C-4 PAPER CLUTCH FRICTION TEST

Conducted For

SWRI ARMY LAB

Oil Code: AL-27877-L

Test Number: C2-2-1484

September 12, 2007

Submitted by:

Matthew Jackson Principal Engineer Specialty & Driveline Fluids Evaluation



The results of this report relate only to the fluid tested. This report shall not be reproduced except in full without the written approval of Southwest Research Institute®

C-4 Heavy Duty Tr Fluid Specification	ansmission	······································				Allison Tra Genera	nsmission Division al Motors
		IX. Paper Clu	Itch Frictic	n Test			
Test Laboratory: SWRI Test Number: C2-2-1484 Friction Plate Batch: LOT 4D Steel Plate Batch: 9/11/2005				Lab Sponsor Comp	Fluid Code: Fluid Code: letion Date:	ATF-22370 AL-27877-L 09/12/07	3 -
Clutch Wear D	Data						······································
		Steel Plates Clutch Plate Pack Clearance	Maximum 0.0010 0.1110 Before 1.0922	Average 0.0001 0.1060 After 1.3462			
Reference Tes	its						
Test Number	Test Date	Test Fluid	7			New	FOT
C2-0-1460	11/19/06	RDL-2746 08-05	1	Viscositv a	t 40°C, cSt	58 24	44 16
C2-0-1471	03/17/07	RDL-2746 08-05]	Viscosity a	t 100°C, cSt	10.6	8.37
C2-0-1482	08/31/07	RDL-2746 07-06]	Iron Conte	ent, ppm	2	227
	D5185 Ba B Ca Mg P Si Si Na Zn	New Fluid (ppm) <1 2 3593 12 1298 5 <5 <5 1441					
Name: Title:	Matthew Ja	ckson gineer	S	Signature: Date:	9/21/07		

ALLISON C- 4 PAPER FRICTION TEST

(Torque in N*m)



Sponsor Fluid Code: AL-27877-L

Lab Fluid Code: ATF-223703

Completion Date: 09/12/2007

Test Number: C2-2-1484

Fric. Plate Batch: LOT 4D

Steel Plate Batch: 9/11/2005

CYCLE	SLIP TIME	TORQUE (MIDPOINT)	TORQUE STATIC PEAK	STATIC PEAK - MIDPOINT	LOW SPEED STATIC PEAK	LOWSPEED STATIC TORQUE
100	0.53	195	232	37	259	243
500	0.55	181	302	121	321	295
1000	0.51	196	318	122	340	316
2500	0.49	207	308	101	348	315
5000	0.47	220	298	78	325	307
7500	0.46	224	287	63	314	302
10000	0.46	225	274	49	309	289

TORQUE

COEFFICIENT OF FRICTION

	SLIP	TORQUE	TORQUE TORQUE STATIC PEAK		LOW SPEED	LOWSPEED	
CYCLE	TIME	(MIDPOINT)	STATIC PEAK	- MIDPOINT	STATIC PEAK	STATIC TORQUE	
100	0.53	0.095	0.113	0.018	0.126	0.118	
500	0.55	0.088	0.147	0.059	0.156	0.144	
1000	0.51	0.095	0.155	0.060	0.166	0.154	
2500	0.49	0.101	0.150	0.049	0.169	0.153	
5000	0.47	0.107	0.145	0.038	0.158	0.150	
7500	0.46	0.109	0.140	0.031	0.153	0.147	
10000	0.46	0.110	0.133	0.023	0.150	0.141	

ſ	Liı	mits	Results			1	
	Value	% Change	100 N	10,000 N	% Change	P/F	
Slip Time Max.	0.600	N/A	0.530	0.460	-13.21	Р	
Mid-Point Fric. Coeff. Min.	0.085	N/A	0.095	0.110	15.79	Р	
Static Friction Coeff.	N/A	N/A	0.113	0.133	17.70		
Low Speed Peak Fric. Coeff.	N/A	N/A	0.126	0.150	19.05	1	
0.25 Second Low Speed Coeff.	N/A	N/A	0.118	0.141	19.49]	

SOUTHWEST RESEARCH INSTITUTE®

ALLISON C4-PAPER FRICTION TEST

Candidate Fluid: AL-27877-L		L	Test Number	: C2-2-148	34	Completion Date : 9/12/2007			
Lab Fluid Co	de : ATF-22370	3	Steel Plate Batch: 09/11/2005				Fric Plate Batch : LOT 4D		
	Location					Inner	Average	Outer	
Plates	of Tooth	Near Inner Diameter		Near Outer Diameter		Diameter	Overall	Diameter	
	(Clockwise)	Before	After	Before	After	Change	Change	Change	
			FRICT	ION MATERIAL					
1	Тор	1.7670	1.6600	1.7670	1.6640	0.1070		0.1030	
2	120	1.7670	1.6650	1,7660	1.6630	0.1020		0.1030	
	240	1.7670	1.6560	1.7650	1.6550	0.1110		0.1100	
	Average					0.1067	0.1060	0.1053	
	Тор	1.7670	1.6570	1.7670	1.6650	0.1100		0.1020	
5	120	1.7630	1.6550	1.7670	1.6620	0.1080		0.1050	
	240	1.7660	1.6580	1.7670	1.6640	0.1080		0.1030	
	Average					0.1087	0.1060	0.1033	
			STEELS	SEPARATOR	RS				
	Тор	1.7540	1.7540	1.7530	1.7530	0.0000		0.0000	
1	120	1.7520	1.7520	1.7540	1.7540	0.0000		0.0000	
	240	1.7550	1.7550	1.7550	1.7550	0.0000		0.0000	
	Average					0.0000	0.0000	0.0000	
	Тор	1.7440	1.7440	1.7440	1.7430	0.0000		0.0010	
3	120	1.7450	1.7440	1.7430	1.7430	0.0010		0.0000	
	240	1.7440	1.7440	1.7440	1.7440	0.0000		0.0000	
	Average					0.0003	0.0003	0.0003	
4	Top	1.7470	1.7470	1.7470	1.7470	0.0000		0.0000	
	120	1.7480	1,7480	1.7480	1.7480	0.0000		0.0000	
	240	1.7430	1.7420	1.7420	1.7420	0.0010		0.0000	
	Average					0.0003	0.0002	0.0000	
	Тор	1.7510	1.7510	1.7510	1.7510	0.0000		0.0000	
6	120	1.7510	1.7510	1.7500	1.7500	0.0000		0.0000	
	240	1.7490	1.7490	1.7480	1.7480	0.0000		0.0000	
	Average	_				0.0000	0.0000	0.0000	
								and the second se	

(Anything Unusual)

PLATE CONDITION AT E.O.T.: PLATES IN GOOD CONDITION WITH LIGHT DISCOLORATION ON INNER STEEL PLATES

Test Date and Operator's Name: 9/12/2007

EDWARD TIJERINA

Pack ID#: 4072

Reviewed By (Signature and Date)

14/07






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SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

FUELS AND LUBRICANTS RESEARCH DIVISION

Report on

CATERPILLAR TO-4 FRICTION PROPERTIES, VC-70

Conducted for

ARMY LAB

Oil Code: AL-27877-L

Test Number: VC70-A-75-I

October 2, 2007

Submitted by:

Brian Koehler

Principal Engineer Specialty & Driveline Fluids Evaluations



R
CATERPILLAR TO-4 FRICTION PROPERTIES, VC-70



Summary Sheet

Company:	ARMY	' LAB					
Test start date: End of test date: Oil Code:	Septer Octob AL-27	mber 28, 2 er 2, 2007 877-l	007				
Sequence Number	1219	N/A	1221	1222	1223	1224	Friction Retention
Dynamic Coefficien Vs. Cycle:	t F	N/A	P	P	F	F	N/A
Dynamic Coefficient Vs. Load:	t F	N/A	P	P	F	F	
Dynamic Coefficient Vs. Speed:	t F	N/A	F	F	F	F	
Energy Limit:	P	N/A	P	P	Р	 Р	
Static Coefficient Vs. Cycle:							N/A
Static Coefficient							
Vs. Load:	P	N/A	F	F	F	P	
Static Coefficient Vs. Speed:	P	N/A	F	F	F	F	
Energy Limit:	P	<u>N/A</u>	P	Р	P	 P	
Total Wear:	0.007	N/A	0.040	0.033	0.033	0.000	
Wear Limit:	0.030	N/A	0.070	0.070	0.070	0.040	
Comments: Acceptance bands sho	wn are for	the last tim	e each seo		eferenced	aing the TO	
reference oil.				uchec was I		sing the TO-4	+ CAT. Category

F = Fail P = Pass N/A = Not Applicable

Test name: A-75-I Test date: 09/28/07 Test description: AL-27877-L Oil type: AL-27877-L / LO-223703 Viscosity: OW-30 Miscellaneous: Software version: 1.40 Run name & desc: I0706091 - AL-27877-L Run date: 09/25/07 Oil temperature: 82 degrees C Oil flow rate: 3.78 liter/minute Operator: HC Remarks: "I" machine oil test AL-27877-L / LO-223703 Sequence name: SE01219 Remarks: Use 1Y0708 Disc and 1Y3610 Plate Number of cycles run: 1155 Machine: Т Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0708 - Elastomeric Disc Material: Raybestos 6475-4 Rayflex Groove pattern: Single Lead Spiral - 12 Radial Miscellaneous: Use with 1Y3610 Steel Plate Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm) : 128.21 Batch number: 26NO0-00004 Remarks: Elastomeric Plate name & desc: 1Y3610 - Steel Plate Surface: 0.70 to 1.30 micron Roughness Miscellaneous: Install the side marked with the average roughness Batch number: 26NO0-00004 Remarks: 0.99 Surface Finish Report limit name: LIM1219 - Reference run: I0706090 Limit file generated: 09/24/07 Report format name: REP1219 - ELASTOMERIC, RAYFLEX



1Y0708 DISC THICKNESS

_	Oute	r Diam	eter	Inne	r Diam	neter
Loc	Ml	M2	M3	Ml	M2	MЗ
1	4.95	4.95	4.95	4.94	4.93	4.93
2	4.96	4.96	4.95	4.95	4.94	4.94
3	4.95	4.94	4.94	4.95	4.94	4.94
4	4.95	4.95	4.95	4.95	4.94	4.94
5	4.95	4.94	4.94	4.93	4.93	4.93
6	4.95	4.95	4.94	4.94	4.94	4.94
Avg	4.95	4.95	4.94	4.94	4.94	4.94
	Compre M2 - I	ession M3 ave:	set aver rage Wear	age wear : 0.002	r: 0. 2	005
	_					

Total Wear (all measurements in mm): 0.007





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Southwest Research Institute "I"machine oil test AL-27877-L / LO-223703

Test name: A-75-I Test date: 09/28/07 Test description: AL-27877-L Oil type: AL-27877-L / LO-223703 Viscosity: OW-30 Miscellaneous: Software version: 1.40 Run name & desc: I0706092 - AL-27877-L / LO-223703 Run date: 09/29/07 82 degrees C Oil temperature: Oil flow rate: 3.78 liter/minute Operator: mtd Remarks: I machine oil test AL-27877-L / LO-223703 Sequence name: SEQ1221 Remarks: Use 1Y0710 Disc and 1Y3610 Plate. Number of cycles run: 1087 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0710 - Steering Brake Paper Material: Raybestos 7894-4 Paper Groove pattern: 2 - 37 Multiple Parallel Use with 1Y3610 Steel Plate Miscellaneous: Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm): 128.21 Batch number: 23MR9-00001 Remarks: Steering brake paper Plate name & desc: 1Y3610 - Steel Plate Surface: 0.70 to 1.30 micron Roughness Miscellaneous: Install the side marked with the average roughness Batch number: 23MR9-00001 Remarks: 0.72 surface finish Report limit name: LIM1221 - Reference run: 10706003 Limit file generated: 07/26/06 Report format name: REP1221 - STEERING BRAKE PAPER



1Y0710 DISC THICKNESS

	Oute	er Diam	neter	Inne	r Dian	leter	
Loc	M1	M2	M3	Ml	M2	M3	
1	5.03	5.00	4.99	5.02	5.00	4.99	
2	5.04	5.02	5.00	5.03	5.01	4.99	
3	5.05	5.02	5.00	5.05	5.02	5.01	
4	5.04	5.02	5.00	5.04	5.01	4.99	
5	5.03	5.01	5.00	5.03	5.01	5.00	
6	5.03	5.00	4.99	5.03	5.00	4.98	
Avg	5.04	5.01	5.00	5.03	5.01	4.99	
	Compr M2 -	ession M3 ave	set ave rage Wea	erage wea: ar: 0.01	r: 0. 5	025	
	Total We	ar (al	l measur	rements in	n mm):	0.040	С







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Southwest Research Institute "I"machine oil test AL-27877-L / LO-223703

Test name: A-75-I Test date: 09/28/07 Test description: AL-27877-L Oil type: AL-27877-L / LO-223703 Viscosity: OW-30 Miscellaneous: Software version: 1.40 Run name & desc: I0706093 - AL-27877-L Run date: 09/30/07 Oil temperature: 82 degrees C Oil flow rate: 3.78 liter/minute Operator: mtd Remarks: I machine oil test AL-27877-L / LO-223703 Sequence name: SE01222 Remarks: Use 1Y0711 Disc and 1Y0726 Plate Number of cycles run: 1164 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0711 - Wheel Brake Paper Material: Raybestos 7902-1 Paper 2 - 37 Multiple Parallel Use with 1Y0726 Steel Plate Groove pattern: Miscellaneous: Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm): 128.21 Batch number: 24FE9-00001 Remarks: wheel brake paper Plate name & desc: 1Y0726 - Steel Plate Surface: 0.30 micron Maximum Roughness Install the side marked with the average roughness Miscellaneous: Batch number: 24FE9-00001 Remarks: 0.21 surface finish Report limit name: LIM1222 - Reference run: I0706004 Limit file generated: 07/26/06 Report format name: REP1222 - WHEEL BRAKE PAPER



1Y0711 DISC THICKNESS

	Oute	r Diam	eter	Inne	r Diam	leter
Loc	Ml	M2	M3	Ml	M2	МЗ
1	5.00	4.98	4.96	4.99	4.97	4.96
2	4.98	4.96	4.95	4.97	4.96	4.95
3	4.98	4.96	4.95	4.98	4.96	4.95
4	4.99	4.97	4.95	4.99	4.96	4.95
5	4.98	4.96	4.95	4.98	4.96	4.95
6	4.99	4.97	4.96	4.99	4.96	4.95
Avg	4.99	4.97	4.95	4.98	4.96	4.95
	Compre	ession	set avera	ge wea	r: 0.	021

Total Wear (all measurements in mm): 0.033







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Southwest Research Institute "I"machine oil test AL-27877-L / LO-223703

Test name: A-75-I Test date: 09/28/07 Test description: AL-27877-L Oil type: AL-27877-L / LO-223703 Viscosity: OW-30 Miscellaneous: Software version: 1.40 Run name & desc: I0706094 - AL-27877-L Run date: 10/01/07 82 degrees C Oil temperature: Oil flow rate: 3.78 liter/minute Operator: HC Remarks: "I" machine oil test AL-27877-L / LO-223703 Sequence name: SE01223 Remarks: Use 1Y0712 Disc and 1Y0726 Plate Number of cycles run: 1033 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0712 - Transmission Paper Material: Raybestos 7901-2 Paper 2 - 37 Multiple Parallel Use with 1Y0726 Steel Plate Groove pattern: Miscellaneous: Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm): 128.21 Batch number: 27MR9-00001 Remarks: Transmission Paper Plate name & desc: 1Y0726 - Steel Plate Surface: 0.30 micron Maximum Roughness Install the side marked with the average roughness Miscellaneous: Batch number: 27MR9-00001 Remarks: 0.18 Surface Finish Report limit name: LIM1223 - Reference run: I0706006 Limit file generated: 07/26/06 Report format name: REP1223 - TRANSMISSION PAPER



1Y0712 DISC THICKNESS

	Oute	er Diam	leter	Inne	r Diam	neter	
Loc	Ml	M2	M3	Ml	M2	MЗ	
1	4.99	4.97	4.96	4.98	4.97	4.95	
2	4.98	4.96	4.95	4.98	4.96	4.95	
3	4.98	4.95	4.95	4.98	4.96	4.95	
4	4.99	4.96	4.95	4.98	4.96	4.95	
5	5.00	4.97	4.96	5.00	4.97	4.96	
6	5.00	4.97	4.96	4.99	4.97	4.96	
Avg	4.99	4.96	4.95	4.99	4.97	4.95	
	Compr M2 -	ession M3 ave	set ave rage Wea	erage wear er: 0.010	r: 0.	023	
	Total We	ar (al	l measur	ements in	n mm):	0.033	3



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Southwest Research Institute "I"machine oil test AL-27877-L / LO-223703

Test name: A-75-I Test date: 09/28/07 Test description: AL-27877-L Oil type: AL-27877-L / LO-223703 Viscosity: OW-30 Miscellaneous: Software version: 1.40 Run name & desc: I0706095 - AL-27877-L Run date: 10/02/07 82 degrees C 3.78 liter/minute Oil temperature: Oil flow rate: Operator: HC Remarks: "I" machine oil test AL-27877-L / LO-223703 Sequence name: SEQ1224 Remarks: Use 1Y0713 Disc and 8E4095 Plate Number of cycles run: 1096 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0713 - Elastomeric Disc Material: Caterpillar F37 Groove pattern: Single Lead Spiral - 12 Radial Miscellaneous: Use with 8E4095 Steel Plate Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm): 128.21 Batch number: C63007FE1 Remarks: Elastomeric Plate name & desc: 8E4095 - Steel Plate Surface: 0.70 to 1.00 micron Roughness Miscellaneous: Install the side marked with the average roughness Batch number: C63007FE1 Remarks: 0.88 Surface Finish Report limit name: LIM1224 - Reference run: I0706007 Limit file generated: 07/26/06 Report format name: REP1224 - ELASTOMERIC, F37



1Y0713 DISC THICKNESS

	Out	er Diam	neter	Inne	r Diam	leter			
Loc	Ml	M2	M3	M1	M2	MЗ			
1	5.04	5.04	5.04	5.04	5.04	5.04			
2	5.04	5.04	5.04	5.04	5.04	5.04			
3	5.04	5.04	5.04	5.04	5.04	5.04			
4	5.04	5.04	5.04	5.04	5.04	5.04			
5	5.04	5.04	5.04	5.04	5.04	5.04			
6	5.04	5.04	5.04	5.04	5.04	5.04			
Avg	5.04	5.04	5.04	5.04	5.04	5.04			
	Compression set average wear: 0.000 M2 - M3 average Wear: 0.000								
	Total We	ear (al	l measu:	rements in	n mm):	0.000	0		







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SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

FUELS AND LUBRICANTS RESEARCH DIVISION

Report on

CATERPILLAR TO-4 FRICTION PROPERTIES, VC-70

Conducted for

SWRI - ARMY LAB

Oil Code: AT-27877-L

Test Number: VC70-A-73-I

September 20, 2007

Submitted by: 211 Brian Koehler

Principal Engineer Specialty & Driveline Fluids Evaluations



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CATERPILLAR TO-4 FRICTION PROPERTIES, VC-70



Summary Sheet

Company:	SWR	I – ARMY LA	В				
Test start date: End of test date: Oil Code:	Septe Septe AL-27	mber 13, 200 mber 20, 200 877-L	07 07			e	
Sequence Number	N/A	1220	N/A	N/A	N/A	N/A	Friction Retention
Dynamic Coefficient Vs. Cycle:	<u>N/A</u>	F	N/A	N/A	N/A	N/A	Ρ
Dynamic Coefficient Vs. Load:	N/A	F	N/A	_N/A	N/A	<u>N/A</u>	
Dynamic Coefficient Vs. Speed:	_N/A	F	N/A	<u>N/A</u>	<u>N/A</u>	_N/A	
Energy Limit:	N/A	P	N/A	N/A	N/A	N/A	
Static Coefficient Vs. Cycle:							N/A
Static Coefficient							
Vs. Load:	N/A	P	N/A	N/A	N/A	N/A	
Static Coefficient Vs. Speed:	N/A	P	N/A	N/A	N/A	N/A	
Energy Limit:	N/A	P	_N/A	<u>N/A</u>	N/A	N/A	
Total Wear:	N/A	0.030	<u>N/A</u>	N/A	N/A	N/A	
Wear Limit:	N/A	0.040	N/A	N/A	N/A	N/A	
Comments:	had a shu	tdown at at-					
oil temperature stabilize	nau a shu nd	luown at abc	out 3500 cyc	cies. The d	ynamic valu	les where s	hifted upward while the

F = Fail P = Pass N/A = Not Applicable southwest Research Institute "I" machine AL-27877-L / LO-223703

Test name: A-73-I Test date: 09/13/07 Test description: I machine AL27877-L Oil type: AL-27877-L /LO223703 Viscosity: OW-30 Miscellaneous: Software version: 1.40 Run name & desc: I0706087 - AL-27877-L Run date: 09/14/07 Oil temperature: 115 degrees C Oil flow rate: 3.78 liter/minute Operator: HC Remarks: "I" machine oil test AL-27877-L / LO-223703 Sequence name: SEOFRRET Remarks: USE 1Y0709 DISC AND 1Y0726 PLATE (8E7351 GROUP) Number of cycles run: 25100 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² 1Y0709 - Sintered Bronze Disc name & desc: Material: Raybestos 1349-ET Bronze Groove pattern: Single Lead Spiral - 12 Radial Miscellaneous: Use with 8E4095 Steel Plate for performance run Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm): 128.21 Batch number: 12FE1-00008 Remarks: Sintered Bronze Plate name & desc: 1Y0726 - Steel Plate Surface: 0.30 micron Maximum Roughness Miscellaneous: Install the side marked with the average roughness Batch number: 12FE1-00008 Remarks: 0.16 Surface Finish Report limit name: LIMFRRET - Reference run: 10706005 Limit file generated: 07/26/06 Report format name: **REPFRRET - FRICTION RETENTION**



Coefficient

southwest Research Institute "I" machine AL-27877-L / LO-223703

Test name: A-73-I Test date: 09/13/07 Test description: I machine AL27877-L AL-27877-L /LO223703 Oil type: Viscosity: OW-30 Miscellaneous: Software version: 1.40 Run name & desc: I0706088 - AT-27877-L Run date: 09/20/07 Oil temperature: 82 degrees C Oil flow rate: 3.78 liter/minute Operator: HC Remarks: "I" machine oil test AT-27877-L / LO-223703 Sequence name: SE01220 Remarks: Use 1Y0709 Disc and 8E4095 Plate Number of cycles run: 974 Machine: Ι Coast down check run: 07/19/02 Result: 151.76 seconds Inertia check run: 07/19/02 Result: 1.0288 N-m-s² Disc name & desc: 1Y0709 - Sintered Bronze Material: Raybestos 1349-ET Bronze Groove pattern: Single Lead Spirar - 12 Radiar Use with 8E4095 Steel Plate for performance run Single Lead Spiral - 12 Radial Miscellaneous: Outer diameter (mm): 285.80 Inner diameter (mm): 223.20 Mean radius (mm): 128.21 Batch number: 12FE1-00009 Remarks: Sintered Bronze Plate name & desc: 8E4095 - Steel Plate 0.70 to 1.00 micron Roughness Surface: Miscellaneous: Install the side marked with the average roughness Batch number: 12FE1-00009 Remarks: 0.87 Surface Finish Report limit name: LIM1220 - Reference run: I0706002 Limit file generated: 07/26/06 Report format name: REP1220 - SINTERED BRONZE



1Y0709 DISC THICKNESS

	Oute	r Diam	eter	Inne	r Diam	leter
Loc	Ml	M2	M3	M1	M2	MЗ
1	4.99	4.97	4.96	5.00	4.98	4.96
2	4.97	4.96	4.95	4.98	4.97	4.95
3	4.99	4.98	4.96	4.99	4.97	4.96
4	5.00	4.97	4.97	5.00	4.97	4.97
5	5.00	4.98	4.97	4.99	4.97	4.97
6	5.00	4.98	4.97	5.00	4.98	4.96
Avg	4.99	4.97	4.96	4.99	4.97	4.96
Compression set average wear: 0.019 M2 - M3 average Wear: 0.011						

Total Wear (all measurements in mm): 0.030









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SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

Fuels And Lubricants Research Division

Report on

DEXRON® VI BAND CLUTCH FRICTION TEST

Conducted For

SWRI ARMY LAB

Oil Code: AL-27877-L

Test Number: BH3-8-169

September 21, 2007

Submitted by:

Christopher Barker Research Engineer Specialty & Driveline Fluids Evaluation



The results of this report relate only to the fluid tested. This report shall not be reproduced except in full without the written approval of Southwest Research Institute®
DEXRON[®]-VI Band Friction - 150 HOURS

Program Code: AL-27877-L Status: * Test Cycles: 36,000 Test Performance: *

Start Date: 9/14/2007 EOT Date: 9/21/2007 Run Number: BH3-8-169 EOT Parts Condition: *

Band: 4L60 Drum

4L60	4L60
H	Ë

-	Stop	Time	Midpoin	It Torque	Max Torque	End T	orque	To	- Mid rque	Shift Energy
0	35 Is	0.55	180 IN	-m] 290	[N·m] Report	Ż.^	m] 200	Z v	[m]	[kJ] (15.7-16.3)
0	39		233		340	333		106		15.9
-	.41		230		313	309		83		15.8
1.2	0.42		218		331	315		113		15.8
	0.43	Three	218	Three	319	311	Three	101	Three	15.8
0.1	0.42	Point	215	Point	323	318	Point	108	Point	15.8
	0.43	Average	216	Average	315	310	Average	66	Average	15.8
	0.44	0.44	200	206	314	304	304	114	105	15.7
	0.45	0.45	202	202	303	299	296	101	102	15.8
- I.	0.45	0.45	204	204	294	286	290	06	91	15.8
	0.45	0.45	206	206	287	285	279	81	62	15.8
- 1	0.45	0.45	208	209	275	268	267	29	65	15.8
	0.44	0.44	212	211	257	249	247	46	49	15.8
	0.44	0.45	212	209	246	223	233	34	44	15.8
5.5	0.46	0.45	202	208	255	228	227	53	45	15.8
_	0.44	0.44	209	206	258	229	231	49	52	15.8
_	0.44	0.44	206	208	261	236	232	54	48	15.8
-	0.44	0.44	209	207	251	229	229	42	48	15.8
-	0.44	0.44	205	208	254	222	224	49	43	15.8
-	0.44	0.44	210	207	248	222	227	37	45	15.8
_	0.45	0.45	205	207	255	237	228	50	44	15.8
_	0.45	0.45	205	204	248	225	234	43	47	15.8
1.1	0.45	0.45	200	204	250	239	234	49	46	15.8
	0.45	0.45	205	203	251	238	238	46	47	15.8
	0.45	0.45	205	205	251	238	239	46	45	15.8
	0.45	0.45	206	206	249	242	238	43	42	15.8

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DEXRON[®]-VI Band Friction - 150 HOURS

Program Code: AL-27877-L Status: * Test Cycles: 36,000 Test Performance: *

Start Date: 9/14/2007 EOT Date: 9/21/2007 Run Number: BH3-8-169 EOT Parts Condition: *

d- /1 60 Banc

4L0U	4L60
and:	rum:

Shift Energy [kJ]	15.8	15.8	15.8	15.8	15.0	15.8	15.8	15.8	15.8	15.7
- Mid que 130	46	47	20	47	E C	50	53	54	53	52
Max Tor [N	38	58	45	46	50	53	54	53	55	50
orque m] 200	239	232	236	237	237	232	231	236	236	234
End T	233	240	222	244	243	225	227	242	238	229
Max Torque [N·m] Report	245	258	250	251	250	255	254	256	258	254
t Torque m] 290	204	204	203	204	203	201	202	202	203	204
Midpoin [N- 180	207	200	205	205	200	202	200	203	203	204
Time s] 0.55	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45
Stop [0.35	0.45	0.45	0.44	0.45	0.46	0.46	0.45	0.45	0.45	0.44
Cycles	25,200	26,400	27,600	28,800	30,000	31,200	32,400	33,600	34,800	36,000
Test Time [h]	105	110	115	120	125	130	135	140	145	150

	1				-		-	_	-	· · · · · · · · · · · · · · · · · · ·		-	-	_			-	_	_			_	_		-			_			
				Energy	(KJ)	(15.7-16.3)	15.9	15.8	15.8	15.8	15.8	15.8	15.7	15.8	15.8	15.8	15.8	15.8	15.8	15.8	15.8	15.8	15.8	15.8	15.8	15.8	15.8	15.8	15.8	15.8	15.8
				P	(MM)	00				Three	Point	Average	304	296	290	279	267	247	233	227	231	232	229	224	227	228	234	234	238	239	238
S. I.I.	9/14/2007	9/21/2007		ш	Torq.	>2	333	309	315	311	318	310	304	299	286	285	268	249	223	228	229	236	229	222	222	237	225	239	238	238	242
	Start of Test:	End of Test :		Maximum	Torq.(Nm)	(Report)	340	313	331	319	323	315	314	303	294	287	275	257	246	255	258	261	251	254	248	255	248	250	251	251	249
			c	d-Mid	(MM)	:120				Three	Point	Average	86	94	86	73	59	36	24	19	25	24	22	16	20	21	30	30	35	34	32
lte®	4L60	4L60	50 ml/mi	ш	Torc	v	100	79	67	93	103	94	103	67	82	79	60	37	÷	25	20	30	20	17	11	32	20	39	33	33	37
arch Institu	Band :	Drum :	Air Flow:	ax-Mid	q.(Nm)	<120				Three	Point	Average	105	102	91	79	65	49	44	45	52	48	48	43	45	44	47	46	47	45	42
st Rese	Ł	U	KPa	Ŵ	Tor		106	83	113	101	108	66	114	101	06	81	67	46	34	53	49	54	42	49	37	50	43	49	46	46	43
Southwes	15.80	135.1	304.2	oint	Nm)	290)				Three	Point	Average	206	202	204	206	209	211	209	208	206	208	207	208	207	207	204	204	203	205	206
0,	Energy:	Temp.:	Apply:	Midp	Torq.((180-2	233	230	218	218	215	216	200	202	204	206	208	212	212	202	209	206	209	205	210	205	205	200	205	205	206
				Jement	(Sec)	-0.55)				Three	Point	Average	0.44	0.45	0.45	0.45	0.45	0.44	0.45	0.45	0.44	0.44	0.44	0.44	0.44	0.45	0.45	0.45	0.45	0.45	0.45
	BH3-8-169	AL-27877-I		Engaç	Time	(0.35	0.39	0.41	0.42	0.43	0.42	0.43	0.44	0.45	0.45	0.45	0.45	0.44	0.44	0.46	0.44	0.44	0.44	0.44	0.44	0.45	0.45	0.45	0.45	0.45	0.45
	st Number:	Fluid Code: ,		Total	Cycles		10	240	480	720	096	1,200	2,400	3,600	4,800	6,000	7,200	8,400	9,600	10,800	12,000	13,200	14,400	15,600	16,800	18,000	19,200	20,400	21,600	22,800	24,000
	Te			Test	Hour		0	v -	2	σ	4	2	10	15	20	25	90	35	40	45	20	55	09	65	20	75	80	85	06	92	100

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<u> </u>	T			—			Т									
				Fnerav	(K1)	(15 7-16 3)	15.8	2 a 1 r 1 r	2. 4	0.01 8 m	0.01 8 21	15.8	15.8	15.8	5.5 8 T	15.7
				p	(MM)	00	239	232	236	237	237	232	231	236	236	234
S	9/14/2007	9/21/2007		Ē	Tora.	~ ~	233	240	222	244	243	225	227	242	238	229
	Start of Test:	End of Test :		Maximum	Torq.(Nm)	(Report)	245	258	250	251	250	255	254	256	258	254
			_	d-Mid	.(Nm)	120	34	28	32	33	35	31	29	34	33	30
ute®	4L60	4L60	50 ml/mir	Enc	Torq	· v	26	4	17	90 30	43	22	27	39	35	25
arch Instit	Band :	Drum :	Air Flow:	ax-Mid	ʻq.(Nm)	<120	46	47	50	47	50	52	53	54	53	52
st Rese	۲J ۲	с	KPa	Ÿ	Tor		38	58	45	46	50	53	54	53	55	50
Southwe	15.80	135.1	304.2	bint	Zm)	6 0)	204	204	203	204	203	201	202	202	203	204
(U	Energy:	Temp.:	Apply:	Midpo	Torq.((180-2	207	200	205	205	200	202	200	203	203	204
				jement	(Sec)	-0.55)	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45
	BH3-8-169	AL-27877-		Engaç	Time	(0.35	0.45	0.45	0.44	0.45	0.46	0.46	0.45	0.45	0.45	0.44
	st Number:	^c luid Code:		Total	Cycles		25,200	26,400	27,600	28,800	30,000	31,200	32,400	33,600	34,800	36,000
	Те			Test	Hour		105	110	115	120	125	130	135	140	145	150

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Southwest Research Institute ®

DEXRON® VI Band Friction Test Parts Rating

Sponsor Code: AL-27877-L Run Number: BH3-8-169 EOT Date: 09-21-07 Cycles: 36,000 Hours:150

Band: The fiber area is completely darkened with light/medium glazing and no stress cracks. One medium to heavy flake at one end of the band. Handling marks are also visible.

Drum: There are no cracks. Dark gray tracking marks and light debris denting and medium and heavy scratching is also visible.

SwRI Rating: Pass

Rater: Art Sanchez Date: 09-26-2007

Comments: This test was conducted using 4L60 Drum And 4L60 Band.

*Pending GM ATF Committee approval



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SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

FUELS AND LUBRICANTS RESEARCH DIVISION

Report on DEXRON[®] VI LOW SPEED CLUTCH FRICTION AND TORQUE CAPACITY CHARACTERIZATION

Conducted for

ARMY LAB

Oil Code:

AL-27877-L

Test Numbers: LS12-5-0374

September 11, 2007

Submitted by:

Matthew Jackson Principal Engineer Specialty & Driveline Fluids Evaluation



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DEXRON[®] VI - LOW SPEED - NEW OIL

Program Code: AL-27877-L Status: EOT Test Cycles: 306 Test Performance:

Start Date: 9/10/2007 EOT Date: 9/11/2007 Run Number: LS12-5-0374 EOT Parts Condition:

	Sliding	40°	C Coefficie	ents	9	0°C Coefficien	ts	120	°C Coeffici	ents
Slip Speed	Speed	Appl	y Pressure	[kPa]	Ap	ply Pressure []	(Pa]	Appl	y Pressure	[kPa]
[r/min]	[m/s]	273	683	1044	273	683	1044	273	683	1044
1	0.007	0.134	0.134	0.131	0.119	0.118	0.117	0.112	0.109	0.111
2	0.014	0.136	0.136	0.134	0.123	0.121	0.119	0.116	0.113	0.112
4	0.028	0.140	0.138	0.136	0.127	0.125	0.122	0.120	0.116	0.115
8	0.056	0.140	0.139	0.137	0.130	0.128	0.124	0.123	0.119	0.118
16	0.112	0.141	0.139	0.136	0.133	0.129	0.126	0.127	0.122	0.120
24	0.168	0.143	0.138	0.136	0.133	0.130	0.127	0.127	0.123	0.121
30	0.210	0.141	0.138	0.136	0.134	0.130	0.126	0.128	0.124	0.120
40	0.280	0.141	0.137	0.135	0.134	0.129	0.126	0.128	0.124	0.121
70	0.490	0.140	0.134	0.132	0.133	0.128	0.125	0.128	0.123	0.120
80	0.560	0.140	0.134	0.131	0.133	0.127	0.125	0.127	0.123	0.120
100	0.700	0.140	0.133	0.130	0.133	0.126	0.123	0.128	0.122	0.120
135	0.946	0.139	0.131	0.128	0.132	0.125	0.121	0.128	0.121	0.118
170	1.191	0.139	0.130	0.126	0.132	0.124	0.119	0.127	0.120	0.116
235	1.646	0.137	0.127	0.123	0.130	0.121	0.117	0.126	0.118	0.114

DEXRON[®] VI - LOW SPEED - USED CYCLING TEST OIL

Program Code: Status: Test Cycles: Test Performance: Start Date: EOT Date: Run Number: EOT Parts Condition:

	Sliding	40°	C Coefficie	ents		90°C Coefficient	5	120	°C Coeffici	ents
Slip Speed	Speed	Appl	y Pressure	[kPa]	A	pply Pressure [kl	Pa]	Appl	y Pressure	[kPa]
[r/min]	[m/s]	273	683	1044	273	683	1044	273	683	1044
1	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
2	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
4	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
8	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
16	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
24	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
30	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
40	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
70	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
80	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
100	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
135	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
170	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
235	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000



Test Rig Overview

The GM Low Speed Clutch Friction Test Rig utilizes a 30 hp variable speed electric drive that provides input power to a Greening SAE No. 2 Universal Wet Friction Material Test Machine through a speed-reducing gearbox. Test fluid is drawn from the bottom of the test head, externally circulated using a small gear pump, and returned at the clutch centerline. This is done to more closely simulate fluid flow within a transmission.

Since the clutch cannot be slipped to achieve heating between engagements, an external heat source is employed to achieve the high fluid temperatures required by the test procedure. Silicon oil from an external bath is circulated through the test head "water jacket" chamber (in place of the normal cooling water). Temperature control of the silicon bath is achieved using immersion heaters and a shell-and-tube heat exchanger.

Procedure Overview

A clutch pack consists of one fiber plate installed between two steel plates. Both steel plates are instrumented with thermocouples to record plate interface temperatures during the clutch engagements. Once the test rig is assembled and filled with test fluid, the clutch is applied three times (at a rotational speed of 0 rpm) to ensure saturation of the friction plate.

Discrete Data

The clutch is slipped at fourteen discrete rotational speeds, repeated for nine different pressure and temperature combinations. The discrete conditions for SAE Standard clutch plates are listed below.

Rotational	Apply Pressure	Fluid
Speed (rpm)	(kPa)	Temperature (°C)
1		
2	273	
4		40
8		
16		
24		
30	683	
40		90
70		
80		
100		
135	1044	120
170		
235		

(Note: The use of different clutch plates will necessitate adjustment of the speed and pressure conditions to match the slip speeds and surface pressures encountered by the SAE Standard plates.)



At each discrete speed condition, the clutch is slipped for three seconds following stabilization of the apply force. Target times for data collection are 0.3, 1.0, and 2.9 seconds. The clutch pack is then rotated at 100 rpm (with the apply pressure released) until the separator plate temperatures are stabilized within 3 °C of the bulk fluid temperature.

Sweep Data

Once all speed data has been recorded for a given pressure and temperature combination, sweep data is collected. During a sweep, the clutch is applied and the rotational speed is ramped from 0 rpm to maximum in 20 seconds. The clutch is then held at maximum speed for 5 seconds, then ramped to 0 rpm in 20 seconds. One sweep is performed for every pressure and temperature combination.

Breakaway Data

At the conclusion of each sweep, two static breakaways are performed. In each breakaway, speed is set at 0 rpm and the clutch applied at the given pressure condition. The electric drive then increases power to the test head until the clutch "breaks away." Immediately following breakaway, the clutch is slipped for 3 seconds at 5 rpm. The first breakaway is performed immediately following the conclusion of the sweep, with the second following after the separator plate temperatures are stabilized within 3 °C of the bulk fluid temperature.

Friction Map

Completion of the 126 speed-pressure-temperature clutch slip combinations and their associated sweeps and breakaways constitutes a friction map.

Break-In

Following the initial friction map, a break-in procedure is performed. Break-in consists of continuously slipping the clutch for ten minutes at 120 °C, 683 kPa, and 100 rpm. (Note that break-in conditions must also be adjusted when using plates other than SAE standard.) The ten-minute engagement is performed three times with a one minute release period between each apply cycle.

Post Break-In

Upon completion of the break-in, a complete friction map is performed (as described above). This results in two complete sets of data – an initial "pre-break-in" friction map and a final "post-break-in" map.

New and Used Fluid

Two full tests are conducted on each fluid. The first test is conducted on new, unused fluid. The second test is conducted on identical fluid that was previously run in another test (typically the GM Cycling test).

Upon completion of the initial test on new fluid, the rig is allowed to drain for a minimum of 30 minutes. Since the used fluid test is conducted on the same clutch pack used to test the new fluid, the test head is not disassembled between runs. (For this reason, clutch pack measurements give an indication of overall wear only, as final measurements are not conducted until the completion of the second test.)



After the rig has been fully drained, the used fluid (which has been filtered to remove any debris from previous testing) is installed and the test repeated.

Data Interpretation

A friction coefficient is calculated for each discrete data combination. The coefficient is calculated according to the following equation:

$$\mu = \frac{T}{PARN}$$

where

T = Torque (Nm) P = Pressure (kPa) A = Apply Piston Area (m²) R = Mean Friction Radius (m) N = Active Friction Surfaces

Test Report

Per sponsor request, only the new fluid portion of the test was conducted. The test report consists of nine plots displaying the variation of coefficient with slip speed at each temperature and pressure combination, two charts summarizing friction map data from the new and used fluid tests (not run in this case), and clutch pack wear measurements.



Appendix

- 1. Coefficient vs. Slip Speed Plot: 40 °C / 273 kPa
- 2. Coefficient vs. Slip Speed Plot: 40 °C / 683 kPa
- 3. Coefficient vs. Slip Speed Plot: 40 °C / 1044 kPa
- 4. Coefficient vs. Slip Speed Plot: 90 °C / 273 kPa
- 5. Coefficient vs. Slip Speed Plot: 90 °C / 683 kPa
- 6. Coefficient vs. Slip Speed Plot: 90 °C / 1044 kPa
- 7. Coefficient vs. Slip Speed Plot: 120 °C / 273 kPa
- 8. Coefficient vs. Slip Speed Plot: 120 °C / 683 kPa
- 9. Coefficient vs. Slip Speed Plot: 120 °C / 1044 kPa
- 10. Clutch Pack Wear Measurements

New Fluid Test Number: LS12-5-0374







.

-New - - Used

AL-27877-L, 40°C, 683 kPa Apply Pressure



AL-27877-L, 40°C, 1044 kPa Apply Pressure

























SOUTHWEST RESEARCH INSTITUTE®

GM LOW SPEED CLUTCH FRICTION AND TORQUE CAPACITY CHARACTERIZATION



Candidate Lab Fluid C	Fluid: AL-2787 Code : ATF-223	7-L 703	Test Number Steel Plate Bat	: LS12-5-03 tch: 8-07 AXO	Completion Fric Plate Ba	Date : 9/11//	2007	
Plates	Location of Tooth	Near Inne	er Diameter	Near Outer I	Diameter	Inner Diameter	Average	Outer
_	(Clockwise)	Before	After	Before	After	Change	Change	Change
			FRIC	TION MATERIAL	1000			enange
	Тор	1.7720	1.6800	1.7740	1.7080	0.0920		0.0660
2	120	1.7600	1.6780	1.7590	1.7070	0.0820		0.0520
	240	1.7660	1.6690	1.7680	1.6970	0.0970		0.0320
	Average					0.0903	0.0767	0.0630
_			STEE	L SEPARATORS			0.0707	0.0000
	Тор	1.7450	1.7440	1.7460	1.7460	0.0010		0.0000
1	120	1.7460	1.7460	1.7460	1,7460	0,0000		0.0000
_	240	1.7460	1.7460	1.7450	1.7450	0.0000		0.0000
	Average					0.0003	0.0002	0.0000
	Тор	1.7330	1.7330	1.7330	1,7330	0,0000	0.0002	0.0000
3	120	1.7290	1,7290	1,7280	1 7280	0.0000		0.0000
	240	1.7270	1.7270	1.7280	1.7280	0.0000		0.0000
	Average					0.0000	0.0000	0.0000
						0.0000	0.0000	0.0000

PLATE CONDITION AT E.O.T.: PLATES IN GOOD CONDITION WITH NO UNUSUAL DISCOLORATION

(Anything Unusual)

Test Date:

9/11/2007

Operator's Name:

JOE MARTINEZ

Reviewed By (Signature and Date)

+/19/07

Pack ID#: 4088

SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

Fuels And Lubricants Research Division

Report on

DEXRON® VI PLATE CLUTCH FRICTION TEST

Conducted For

SWRI ARMY LAB

Oil Code: AL-27877-L

Test Number: HC11-1-82

September 19, 2007

Submitted by:

Christopher Barker Research Engineer Specialty & Driveline Fluids Evaluation



The results of this report relate only to the fluid tested. This report shall not be reproduced except in full without the written approval of Southwest Research Institute®

DEXRON[®]-VI Plate Friction - 200 HOURS

Program Code: AL-27877-L Status: * Test Cycles: 36,000 Test Performance: *

Start Date: 9/11/2007 EOT Date: 9/19/2007 Run Number: HC11-1-82 EOT Parts Condition: *

Fiber Plates: GMPT-0506 Steel Plates: GMPT-0506 Delta Travel [mm]: 0.069 mm

100			_	-	-				-	-	-	-	-	-	-	-	-	_	_	-	-	-	-	-	-	_	-
Shift Frierry	Tk.n	154-160	15.5	15.6	15.7	10.1	10.1	15.7	15.8	15.7	15.7	15.7	15.7	15.7	15.6	15.6	15.7	15.7	15.7	15.7	15.6	15.6	15.6	15.7	15.6	15.7	15.7
d ordine	Imi	30				Throo	Doint	Averade	13	8	4	0		-		0	0	0	0	0	C		-	-			
Max - M	Z		-	00	10	at	15	15	13	10	5	0	-	-	0	-	0		0	0	0	0	-	-	-	5	0
lorque	- Iu	06		T	-	Three	Doint	Average	104	100	95	91	88	87	87	87	87	86	86	86	86	85	85	85	85	85	86
Maximum	ŗ.N.J		82	112	114	112	110	109	104	101	95	06	87	86	87	87	88	86	86	86	85	85	86	85	85	85	86
End Lorque	[m·m]	Report	75	102	104	66	101	66	26	92	81	73	71	20	70	71	70	71	71	71	72	71	20	70	69	69	71
it lorque	[m·	105				Three	Point	Average	92	91	91	06	88	88	87	87	87	87	86	86	85	85	85	84	84	83	83
Midpoir	Z	80	81	60	95	95	95	94	91	91	93	60	88	87	87	88	87	87	86	86	85	85	85	84	83	84	83
1 ime	5	1.05				Three	Point	Average	0.94	0.95	0.96	0.98	1.00	1.01	1.01	1.01	1.01	1.01	1.01	1.02	1.02	1.02	1.02	1.03	1.04	1.04	1.04
stop	1	0.85	1.06	0.95	0.92	0.92	0.92	0.91	0.95	0.95	0.95	0.99	1.00	1.01	1.01	1.00	1.01	1.01	1.02	1.02	1.04	1.02	1.00	1.04	1.05	1.04	1.05
	Cycles		10	180	360	540	720	006	1,800	2,700	3,600	4,500	5,400	6,300	7,200	8,100	9,000	9,900	10,800	11,700	12,600	13,500	14,400	15,300	16,200	17,100	18,000
lest lime	Ξ		0.1		2	e	4	5	10	15	20	25	30	35	40	45	50	55	60 2	69	70	75	80	85	90	95	100

DEXRON[®]-VI Plate Friction - 200 HOURS

Program Code: AL-27877-L Status: * Test Cycles: 36,000 Test Performance: *

Start Date: 9/11/2007 EOT Date: 9/19/2007 Run Number: HC11-1-82 EOT Parts Condition: *

Fiber Plates: GMPT-0506 Steel Plates: GMPT-0506 Delta Travel [mm]: 0.069 mm

Shift Energy	[k.f]	15.4 - 16.0	15.7	15.7	15.7	15.6	15.6	15.7	15.7	15.7	15.6	15.7	15.6	15.6	15.6	15.7	15.7	15.7	15.7	15.7	15.7	15.7
X - Mid Lordue I	[N-m]	< 30	3 2	2 2	2 2	2 2	2 2	1 2	+	+	2 1	2 2	2 2	1 2	-	2 1	+					
I lorque Ma	- [E	06 4	86	86	85	85	86	85	85	86	86	86	86	86	86	86	86	86	86	86	86	86
Maximun	ż		86	86	85	86	86	85	85	86	86	86	86	86	86	86	86	86	86	86	86	86
End Jorque	[m·m]	Report	70	71	70	71	71	70	70	70	71	72	70	70	71	73	71	72	70	11	20	11
t lorque	[m	105	83	83	83	83	84	84	84	84	84	84	85	85	85	85	84	85	85	85	85	84
Midpoli	ż	80	83	83	83	83	84	84	84	85	84	84	84	85	85	84	85	84	85	85	84	84
Ime	-	1.05	1.05	1.04	1.05	1.05	1.06	1.05	1.04	1.04	1.04	1.05	1.04	1.04	1.03	1.03	1.04	1.04	1.03	1.03	1.03	1.03
Stop	3	0.85	1.04	1.05	1.04	1.06	1.07	1.05	1.05	1.03	1.05	1.05	1.05	1.03	1.04	1.01	1.05	1.05	1.03	1.02	1.03	1.04
	Cycles		18,900	19,800	20,700	21,600	22,500	23,400	24,300	25,200	26,100	27,000	27,900	28,800	29,700	30,600	31,500	32,400	33,300	34,200	35,100	36,000
lest lime	Ξ		105	110	115	120	125	130	135	140	145	150	155	160	165	170	175	180	185	190	195	200

															_																	
					Energy	(KJ)	(15.4 - 16.0)	15.5	15.6	15.7	15.7	15.7	15.7	15.8	15.7	15.7	15.7	15.7	15.7	15.6	15.6	15.7	15.7	15.7	15.7	15.6	15.6	15.6	15.7	15.6	15.7	15.7
G	¥				End	Torq.(Nm)	(Report)	75	102	104	66	101	66	67	92	81	73	71	70	20	71	70	71	71	71	72	71	20	20	69	69	71
		9/11/2007	9/19/2007	0.069 mm	mum	(Nm)	()				Three	Point	Average	104	100	95	91	88	87	87	87	87	86	86	86	86	85	85	85	85	85	86
		Start of Test:	End of Test:	Delta Travel:	Maxin	Torq.(6<)	82	112	114	112	110	109	104	101	95	06	87	86	87	87	88	86	86	86	85	85	86	85	85	85	86
Y		506	506	c	d-Mid	d.(Nm)					Three	Point	Average	4	-5	ဝု	-15	-17	-17	-17	-17	-17	-16	-15	-14	-14	-14	-14	-14	-14	-14	-13
ummar	ute®	GMPT-0	GMPT-0	50 ml/mi	Ē	Tor		Ģ	12	ი	4	9	5	9		-12	-17	-17	-17	-18	-17	-17	-16	-15	-15	-13	-14	-15	-14	-14	-14	-13
tion Test S	arch Institu	Fibers :	Steels :	Air Flow:	ax-Mid	'q.(Nm)	<30)				Three	Point	Average	13	8	4	0	,	4 -	-	0	0	0	0	0	0	0	~	~	-	7	2
tch Fric	st Rese	КJ К	U	KPa	Σ	Tol		~	22	19	18	15	15	13	10	2	0	Ţ	Ţ	0	7	0	<u>,</u>	0	0	0	0	-	~	-	7	2
late Clut	Southwe	15.7	140.1	349	oint	(HT)	<u>)5)</u>				Three	Point	Average	92	91	91	06	88	88	87	87	87	87	86	86	85	85	85	84	84	83	83
GM F		Energy:	Temp.:	Apply:	Midpo	Torq.(I	(80-1	81	06	95	95	95	94	91	91	93	06	88	87	87	88	87	87	86	86	85	85	85	84	83	84	83
			4		ement	(Sec)	0 1.05)			i	Three	Point	Average	0.94	0.95	0.96	0.98	1.00	1.01	1.01	1.01	1.01	1.01	1.01	1.02	1.02	1.02	1.02	1.03	1.04	1.04	1.04
		HC11-1-82	AL-27877-I		Engag	Time	(0.85 t	1.06	0.95	0.92	0.92	0.92	0.91	0.95	0.95	0.95	0.99	1.00	1.01	1.01	1.00	1.01	1.01	1.02	1.02	1.04	1.02	1.00	1.04	1.05	1.04	1.05
	1994 M	st Number:	Fluid Code:		Total	Cycles		10	180	360	540 700	1.20	006	1,800	2,700	3,600	4,500	5,400	6,300	7,200	8,100	9,000	9,900	10,800	11,700	12,600	13,500	14,400	15,300	16,200	17,100	18,000
		Te			Test	Hour		0 .	- (2 0	m •	4	2	10	15	50	25	30	35	40	45	20	55	00	65	0/	75	80	85	06	95	100

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		1											_					_						_		_	
					Enerav	(KJ)	(154-160)	15.7	15.7	15.7	15.6	15.6	15.7	15.7	15.7	15.6	15.7	15.6	15.6	15.6	15.7	15.7	15.7	15.7	15.7	15.7	15.7
S	x -				End	Torg.(Nm)	(Report)	20	71	20	71	71	20	20	70	71	72	202	20	71	73	71	72	70	71	70	71
		9/11/2007	9/19/2007	0.069 mm	mnu	Nm)		86	86	85	85	86	85	. 85	86	86	86	86	86	86	86	86	86	86	86	86	86
		Start of Test:	End of Test :	Delta Travel:	Maxim	Torq.(I)6<)	86	86	85	86	86	85	85	86	86	86	86	86	86	86	86	86	86	86	86	86
Z		506	506	c	d-Mid	q.(Nm)		-12	-13	-13	-13	-13	-14	-14	-14	-14	-13	-14	-15	-14	-13	-13	-14	-14	-14	-14	-14
ummar	ute®	GMPT-0	GMPT-0	50 ml/mir	ш	Toro		-13	-12	-13	-13	-13	-14	-14	-15	-13	-13	-15	-15	-14	-12	-14	-13	-15	-14	-14	-14
tion Test S	arch Institu	Fibers :	Steels :	Air Flow:	lax-Mid	rq.(Nm)	(<30)	2	7	2	5	7	7	~-	~	~~	7	2	5	~	~		~	~-	~	~	2
Itch Fric	st Rese	Ŗ	с U	KPa	Σ	To	<u> </u>	3	2	7	2	7	~	~	~	2	2	7	~		2	~	~		~	2	2
late Clu	outhwe	15.7	140.1	349	int	lm)	(2)	83	83	83	83	84	84	84	84	84	84	85	85	85	85	84	85	85	85	85	84
GMP	S	Energy:	Temp.:	Apply:	Midpo	Torq.(N	(80-10	83	83	83	83	84	84	84	85	84	84	84	85	85	84	85	84	85	85	84	84
					ement	(Sec)	0 1.05)	1.05	1.04	1.05	1.05	1.06	1.05	1.04	1.04	1.04	1.05	1.04	1.04	1.03	1.03	1.04	1.04	1.03	1.03	1.03	1.03
		HC11-1-82	AL-27877-I		Engag	Time	(0.85 to	1.04	1.05	1.04	1.06	1.07	1.05	1.05	1.03	1.05	1.05	1.05	1.03	1.04	1.01	1.05	1.05	1.03	1.02	1.03	1.04
		st Number:	Fluid Code: Al	Total	Cycles		18,900	19,800	20,700	21,600	22,500	23,400	24,300	25,200	26,100	27,000	27,900	28,800	29,700	30,600	31,500	32,400	33,300	34,200	35,100	36,000	
		Te			Test	Hour		105	110	115	120	125	130	135	140	145	150	155	160	165	1/0	G/L	180	C81	190	C S C	200

200 Hr. Extended Plate Test Ver. 1.0.0.0

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DEXRON®VI Plate Friction Test Parts Condition Rating

Sponsor Code: AL-27877-L Run Number: HC11-1-82 EOT Date: 09-19-2007 Cycles: 36,000 Hours: 200

Fiber Plates: The inner and outer facing areas are completely darkened with light/medium glazing and medium wear and heavy flaking.

Steel Plates: Outer steels show light/medium heat discoloration and trace/light scratching and no hot spots. Inner steels show medium heat discoloration and light scratching and light wear and not hot spots.

SwRI Rating: Fail

Rater: Art Sanchez Date: 09-20-2007

Comments: This test was conducted using GMPT 0506 steel plates and GMPT 0506 fibers.



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145.00 135.00 125.00 115.00 105.00 155.00 95.00 85.00 Test: HC11-1-82 Fluid: AL-27877-L 0000000 Pressure & Temperature for Do o o o o o o o o o o o 000000

360

355

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55.00

75.00

65.00



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SOUTHWEST RESEARCH INSTITUTE® San Antonio, Texas

Fuels and Lubricants Research Division

Report on

John Deere JDQ-96 Performed using 1400 Series Axle

Conducted for

ARMY LAB

AL-27877-L

Test Number 07793

October 10, 2007

Submitted by:

Michael D. Lochte Manager Specialty & Driveline Fluids Evaluations



The results of this report relate only to the items tested. This report shall not be reproduced, except in full, without the written approval of Southwest Research Institute®.



John Deere JDQ-96 Performed using 1400 Series Axle

General Information

Oil Code: AL-27877-L	E.O.T. Date: October 10, 2007

Purpose

The purpose of this test was to evaluate the anti-chatter properties of this oil on the brakes of a 1400 series John Deere Inboard Planetary Axle.

Test Procedure

The test was performed as specified by John Deere Product Engineering. The only changes made to the Deere procedure were those necessary to compensate for a different spiral bevel gear ratio. This procedure is proprietary to Deere and Company.

Data Interpretation

The capacity for each engagement is the average torque during the middle of the engagement. The torque variation is the greatest difference between the maximum and minimum torque recorded during any 0.2-second portion of the engagement. The SwRI variation is the sum of all differences between the maximum torque and minimum torque for each engagement. It is obtained by summing all torque variations of each 0.2-second time block of all engagements.

Test Number

The run number listed on this report is a random number and is not sequential. Only SwRI® can link this run number to test type, oil code, and end-of test date.



John Deere JDQ-96 Performed using 1400 Series Axle

Results

Oil Code: OR-97584	E.O.T. Date: October 10, 2007

The candidate results can be compared to the baseline reference average. Pass or fail decisions are only made by John Deere Product Engineering. The current reference baseline average is the average of the five most recent tests.

Current Reference Baseline Average (N · m)										
	1,000 Cycles	10,000 Cycles	20,000 Cycles	30,000 Cycles	TOTAL					
Relative Capacity	338,535	338,534	341,629	343,274	1,361,972					
Torque Variation	79,214	84,272	79,152	74,708	317,346					

Results From Test Candidate AL-27877-L										
	1,000 Cycles	10,000 Cycles	20,000 Cycles	30,000 Cycles	TOTAL					
Relative Capacity	345,338									
Torque Variation	154,990									

Tables 1 of the Appendix contains chatter test results from 1,000cycles. Table 2 contains results of the five current baseline reference tests. Figures 1 through 4 are graphic presentations of candidate oil performance compared to baseline reference data.

Figure 5 is a graphic presentation of 1000-cycle reference results and AL-27877-L. Table 3 contains the history of reference tests.

Oil Code: AL-27877-L

E.O.T. Date: October 10, 2007

Appendix

Tables

- Table 1 Durability results 1,000 cycles Candidate Oil
 Table 2 Reference Data Compared to Candidate Data
 Figure 1 & Figure 2 Torque Variation Chart
- 4. Figure 3 & Figure 4 Relative Capacity & Average Disk Thickness Chart
- 5. Figure 5 Graphic presentation of 1000 cycle reference results & Candidate
- 6. Table 3 History of reference tests

October 10, 2007

TABLE 1: JDQ-96 DURABILITY TEST RESULTS 1,000 CYCLES

SwRI Oil Code

LO-223703

Sponsor Oil Code AL-27877-L

		Temn	70	71	102	2.02	71	71	71	71	71	7					71		- +	- 7		71
	0il Temn 71°	Variation	1300	1670	1790	1770	1720	1790	1680	1720	1740	1670	1690	1620	890	1170	1410	1840	1070	0101	2750	2530
(Tornile	4341	4251	4190	4152	4064	4026	3960	3954	3872	3840	3966	3901	1832	2597	3381	4247	5080	5854	000 1 6835	7832
TION in Nn		Temp	61	60	59	59	60	60	61	61	61	61	62	28	58	58	58	85	2 X X	α Υ	20 G	09
F and VARIA	01 Temp. 60°	Variation	1610	1990	2130	1580	1640	1760	1670	1660	1710	1660	1560	1540	890	1120	2120	2770	2840	0102	2380	2350
TS (TOROU		Torque	4388	4278	4161	4223	4167	4120	4029	4059	3963	3899	4041	3841	1805	2641	3196	4165	5078	5925	6834	7778
ST RESUL	0	Temp.	50	49	48	48	49	50	50	50	50	51	52	48	49	48	48	48	48	48	48	49
ARIATION TE	il Temp. 49°(Variation	1670	1930	2420	2870	1410	1570	1410	1460	1570	1510	1390	1420	860	1060	2640	2920	3010	2980	2570	2510
TORQUE VI	0	Torque	4346	4288	4160	4073	4158	4113	4029	4065	3975	3926	4057	3855	1786	2599	3176	4098	5029	5926	6833	7799
	c	Temp.	29	29	29	29	29	30	31	32	33	34	32	29	31	31	31	31	31	31	31	32
	Dil Temp. 32°	Variation	4280	4430	3250	1310	1280	1330	1270	1340	1270	1290	1180	1090	680	830	2670	3040	3140	3470	3240	3210
		Torque	3995	4138	3943	4171	4140	4140	4115	4119	4085	4023	3977	3901	1701	2523	3290	4136	5049	5954	6922	7954
Brake	Press.	(kPa)	3831	3831	3831	3831	3831	3831	3831	3831	3831	3831	3831	3831	1532	2300	3065	3831	4598	5364	6130	7050
Axle	Speed	(rpm)	ω	10	15	20	25	30	35	40	45	50	55	60	15	15	15	15	15	15	15	15

	Relative	Torque	SwRI
Temp	Capacity	Variation	Variation
(°C)	(MM)	(MM)	(MM)
32	86,275	43,600	610,080
49	86,291	39,180	498,700
60	86,589	37,770	515,000
71	86,183	34,440	516,040
TOTAL	345,338	154,990	2,139,820

TABLE 2: JDQ-96 REFERENCE DATA COMPARED TO CANDIDATE DATA

EOT Date: October 10, 2007 Oil Code : AL-27877-L

Reference Oil Coded : 69	X31111i				Average Facing
	Cycles	Relative Capacity	Torque Variation	SwRI Variation	Thickness
First Reference Run					(millimeters)
	1,000	326,304	57,420	730,050	7.60
	10,000	331,809	64,900	804,030	7.50
	20,000	345,325	69,500	899,880	7.44
	30,000	341,770	66,210	810,190	7.39
	Total	1,345,208	258,030	3,244,150	
Second Reference Run					
	1,000	337,791	66,660	848,580	7.60
	10,000	338,055	92,240	1,129,330	7.55
	20,000	343,166	77,010	1,001,920	7.49
	30,000	350,470	73,280	863,980	7.44
	Total	1,369,482	309,190	3,843,810	
Third Reference Run					
	1,000	339,375	100,390	1,204,240	7.56
	10,000	335,754	106,780	1,079,450	7.52
	20,000	334,120	84,770	1,030,270	7.49
	30,000	335,614	79,620	1,021,190	7.47
	Total	1,344,863	371,560	4,335,150	
Fourth Reference Run					
Run on new backing pla	1,000	343,906	79,990	1,020,120	7.48
and piston	10,000	343,056	72,520	893,570	7.30
	20,000	342,668	69,920	885,870	7.07
	30,000	345,315	70,360	833,920	6.90
	Total	1,374,945	292,790	3,633,480	
Invalid test run on same	1,000	348,860	132,110	1,721,010	
backing plate and pistor	10,000	323,093	153,860	1,919,720	
as test above was run on					
Fifth Reference Run					
most recent run	1,000	345,296	91,610	1,125,260	7.50
Run on new backing	10,000	343,999	84,920	1,019,400	7.33
plate and piston	20,000	342,864	94,560	1,264,070	7.22
	30,000	343,201	84,070	1,052,400	7.11
AL 07077 L	Total	1,375,360	355,160	4,461,130	
AL-27877-L		Candidate Oi	I lest Results		
	1,000	345,338	154,990	2,139,820	
	10,000				
	20,000				
	30,000				
	Total	345,338	154,990	2,139,820	













October 10, 2007

AL-27877-L

History of 1000 cycle reference tests.

Table 3

		Torque variation at 1000 cycles
69X31111k	1999 brake disk	103,360
69X31111K	1997 brake disk	129,540
69X31111k	2000 brake disk	121,120
69X31111k	2000 brake disk	129,020
69X31111k	2000 brake disk	138,760
69X31111k	2000GDD brake	140,830
69X31111k	2000GDD brake	144.820
69X31111k	2000GDD brake	124,310
69X31111k	2000 GDD brak	131,860
69X31111k	2000 GDD brak	105,010
69X31111k	2000 GDD brak	109,220
69X31111k	2000 GDD brak	142,510
69X31111K	2000 GDD brak	128,080
60Y31111k	2000 GDD brak	109,100
69X31111k	2000 GDD brak	90.070
69X31111k	2000 GDD brak	90,810
69X31111k	2000 GDD brak	79.930
69X31111k	2000 GDD brak	79,930
69X31111k	2000 GDD brak	83,190
69X31111k	2000 GDD brak	81,220
69X31111k	2000 GDD brak	85,570
68X31111k	2000 GDD brak	64,170
69X31111K	2000 GDD brak	67,390
69X31111K 69X31111k	2000 GDD brak	82,410
69X31111k	2000 GDD brak	90,390
69X31111k	2000 GDD brak	99,960
69X31111k	2000 GDD brak	87,380
69X31111k	2000 GDD brak	74,720
69X31111k	2000 GDD brak	74,940
69X31111k	2000 GDD brak	85,980
69X31111k	2000 GDD brak	94,410
69X31111K	2000 GDD brak	74,300
60Y31111k	2000 GDD brak	90,950
69X31111k	2000 GDD brak	83,190
69X31111k	2000 GDD brak	01,060
69X31111k	2000 GDD brak	97,320
69X31111k	2000 GDD brak	75.040
69X31111k	2000 brake disk	86.060
69X31111k	2000 brake disk	68,590
69X31111k	2003 brake disk	57,420
69X31111k	2003 brake disk	60,330
69X31111k	2003 brake disk	76,260
69X31111K	2003 brake disk	86,210
60Y21111k	2003 brake disk	84,550
69X31111k	2003 brake disk	66,660 84,760
69X31111k	2003 brake disk	87 800
69X31111k	2003 brake disk	100.390
69X31111k	2003 brake disk	96.620
69X31111k	2003 brake disk	106,710
69X31111k	2003 brake disk	123,110
69X31111k	NEW BACKING	79,990
69X31111k		98,440
69X31111k		106,370
69X31111k		110,040
69X31111K		127,550
69X31111k	invalid run	111,280
03/01/11/	PACKING	132,110
69X31111k	Plate and	01 610
		31,010
69X31111k	Plate and	02.220
UUNUTTIK	nlate used for 1	92,230
69X31111k	test	89 200
	same brake	00,200
	plate and	
AL-27877-L	piston as	154,990