

REPORT DOCUMENTATION PAGE				Form Approved OMB No. 0704-0188	
Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing this collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden to Department of Defense, Washington Headquarters Services, Directorate for Information Operations and Reports (0704-0188), 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to any penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number. PLEASE DO NOT RETURN YOUR FORM TO THE ABOVE ADDRESS.					
1. REPORT DATE (DD-MM-YYYY) 09/09/2013		2. REPORT TYPE Interim Research Performance Report (Monthly)		3. DATES COVERED (From - To) October 1 - October 31, 2013	
4. TITLE AND SUBTITLE Expeditionary Light Armor Seeding Development				5a. CONTRACT NUMBER	
				5b. GRANT NUMBER N00014-13-1-0219	
				5c. PROGRAM ELEMENT NUMBER	
6. AUTHOR(S) Nichole Cicchetti, Bazle Haque, Shridhar Yarlagadda				5d. PROJECT NUMBER	
				5e. TASK NUMBER	
				5f. WORK UNIT NUMBER	
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) UNIVERSITY OF DELAWARE OFFICE OF THE VICE PROVOST FOR RESEARCH 220 HULLIHEN HALL NEWARK, DE 19716-0099				8. PERFORMING ORGANIZATION REPORT NUMBER MONTHLY-7	
9. SPONSORING / MONITORING AGENCY NAME(S) AND ADDRESS(ES) Office of Naval Research 875 North Randolph Street Arlington, VA 22203-1995				10. SPONSOR/MONITOR'S ACRONYM(S) ONR	
				11. SPONSOR/MONITOR'S REPORT NUMBER(S)	
12. DISTRIBUTION / AVAILABILITY STATEMENT Approved for Public Release; distribution is Unlimited.					
13. SUPPLEMENTARY NOTES					
14. ABSTRACT Half-symmetric model is used in AutoDyn to simulate Depth of Penetration (DoP) experiments on SiC tile with and without a gap supported by solid aluminum. Impacts of a .30cal AP M2 projectile over an impact velocity range 700 m/s to 1000 m/s are modeled using SPH elements. Model validation runs with monolithic SiC tiles are conducted based on the DoP experiments described in reference - ARL-TR-2219, 2000 Tile gap is found to increase the DoP as compared to monolithic tiles The next step will be run simulations on narrower and wider gap sizes and different geometries of tile configurations. Determinations need to be made on what the manufacturers tolerances on tile gaps are and possible filling materials for gaps. DOP is the main measurement to determine which geometry and configuration yield the best results.					
15. SUBJECT TERMS .30cal AP M2 Projectile, 762x39 PS Projectile, SPH, Aluminum 5083, SiC, DoP Expeminets, AutoDyn Simulations, Tile Gap					
16. SECURITY CLASSIFICATION OF: UU			17. LIMITATION OF ABSTRACT UU	18. NUMBER OF PAGES 39	19a. NAME OF RESPONSIBLE PERSON Shridhar Yarlagadda
a. REPORT	b. ABSTRACT	c. THIS PAGE			19b. TELEPHONE NUMBER (include area code) 302-831-4941

20131114798



MONTHLY REPORT
OCTOBER 2013

Nicole A. Cicchetti, Bazle Z. (Gama) Haque,
Shridhar Yarlagadda

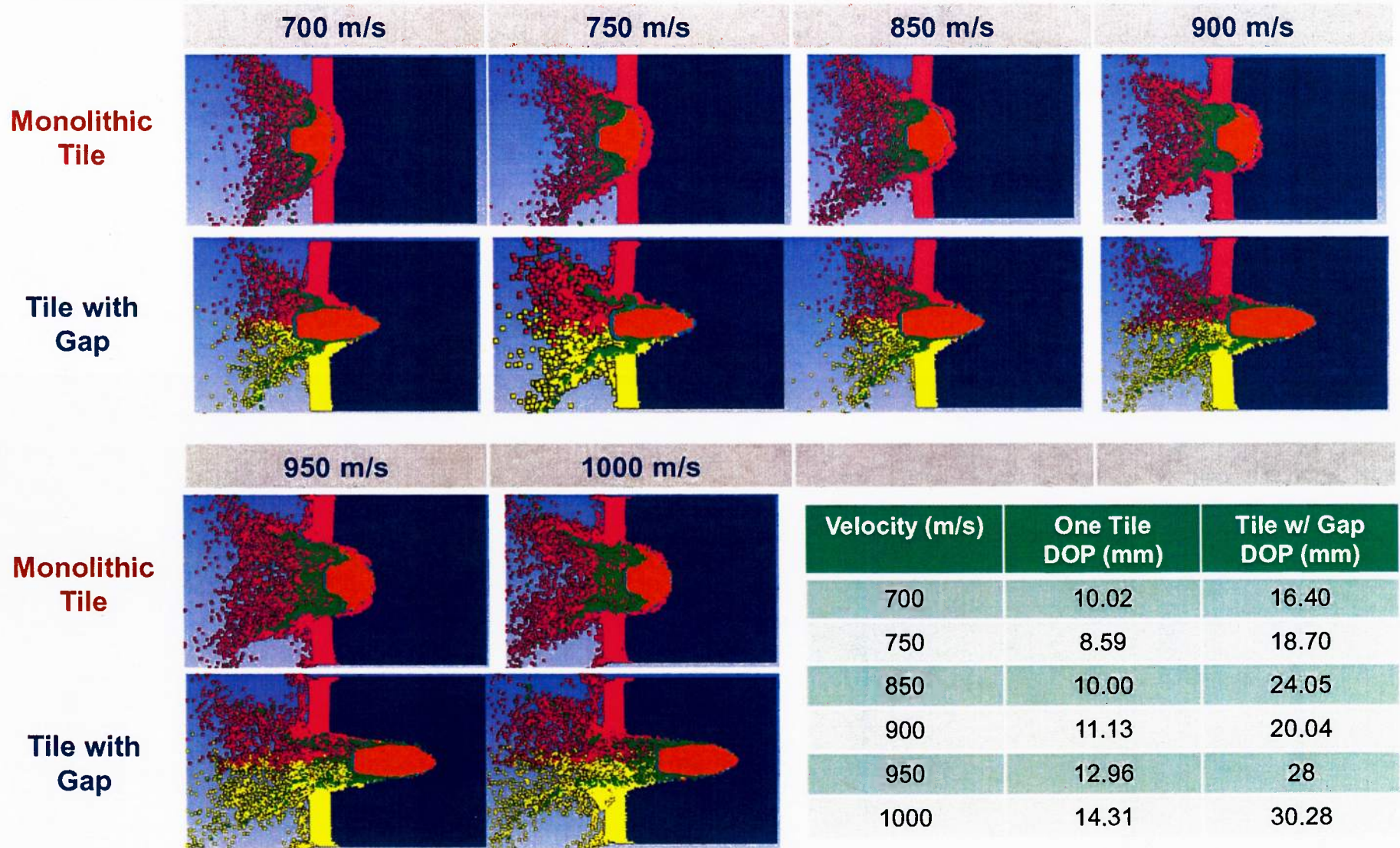
MODELING AND SIMULATION OF CERAMIC ARRAYS TO IMPROVE BALLAISTIC PERFORMANCE

MONTHLY REPORT FOR OCTOBER 2013



- ☐ Half-symmetric model is used in AutoDyn to simulate Depth of Penetration (DoP) experiments on SiC tile with and without a gap supported by solid aluminum.
- ☐ Impacts of a .30cal AP M2 projectile over an impact velocity range 700 m/s to 1000 m/s are modeled using SPH elements.
- ☐ Model validation runs with monolithic SiC tiles are conducted based on the DoP experiments described in reference - ARL-TR-2219, 2000
- ☐ Tile gap is found to increase the DoP as compared to monolithic tiles
- ☐ The next step will be run simulations on narrower and wider gap sizes and different geometries of tile configurations.
- ☐ Determinations need to be made on what the manufacturers tolerances on tile gaps are and possible filling materials for gaps.
- ☐ DOP is the main measurement to determine which geometry and configuration yield the best results.

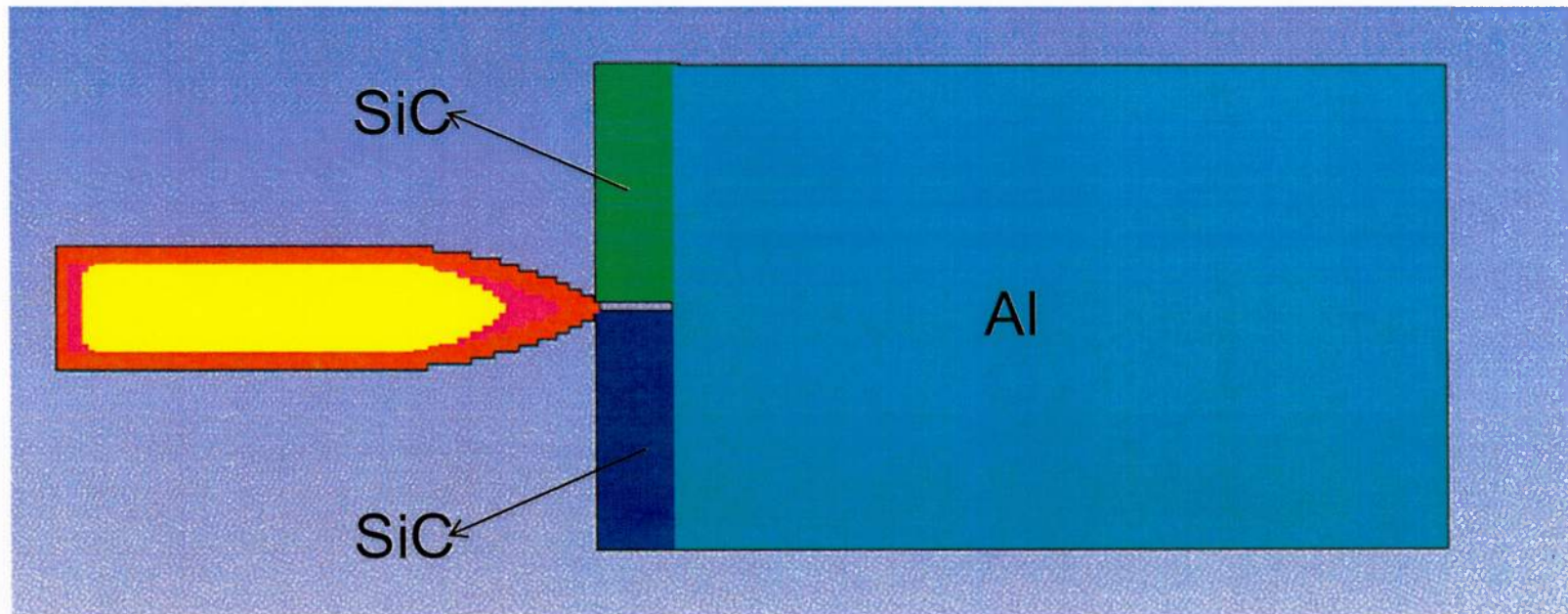
EFFECT OF TILE GAP ON DOP





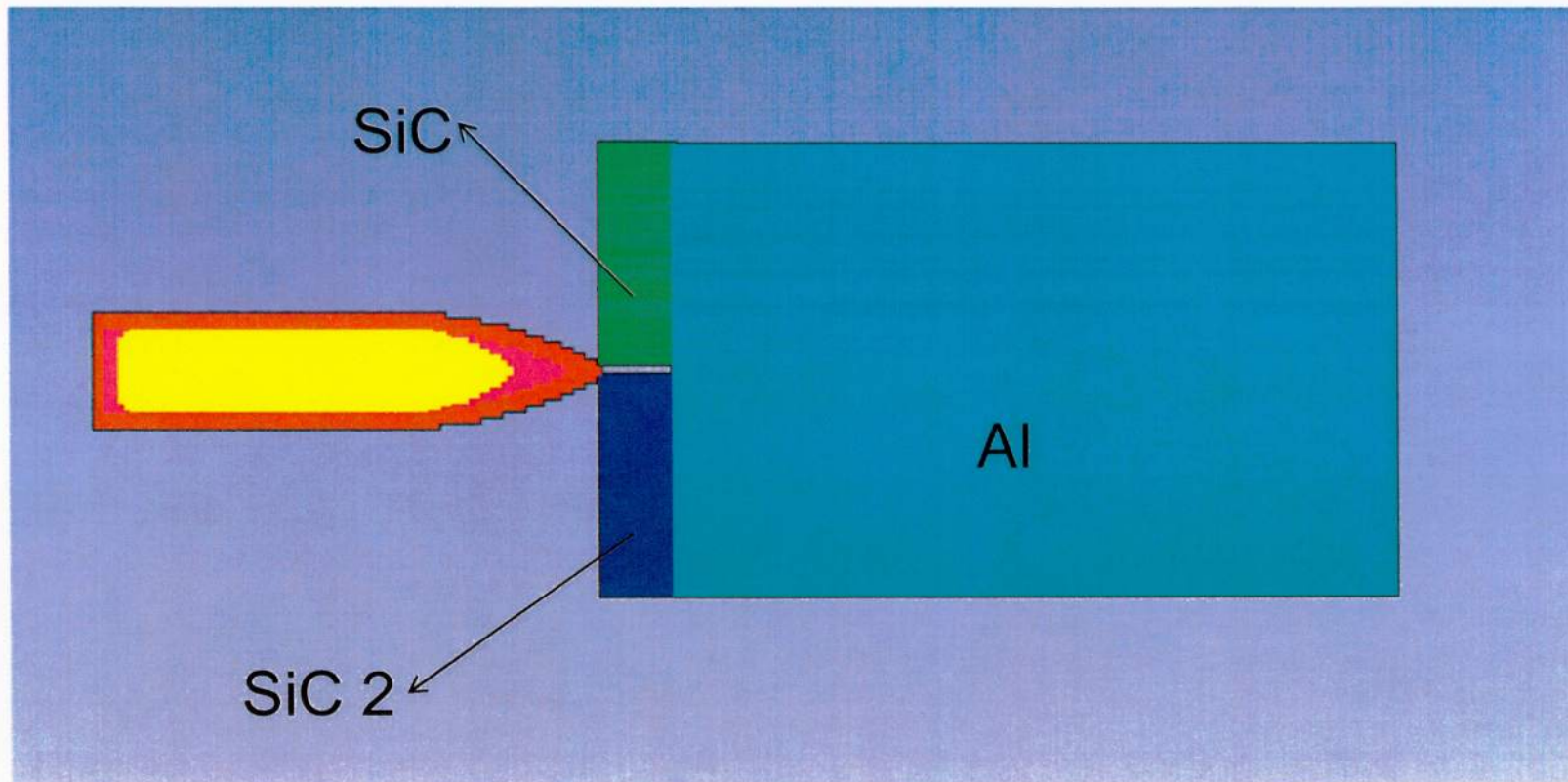
DOP SIMULATION DETAILS

HALF SYMMETRIC MODEL WITH GAP IN AUTODYN



- ☐ Smoothed-particle hydrodynamics (SPH) used for all parts
- ☐ SPH size = 0.40-mm, totaling 278k elements
- ☐ Clamp boundary condition used

HALF-SYMMETRIC MODEL WITH GAP IN AUTODYN



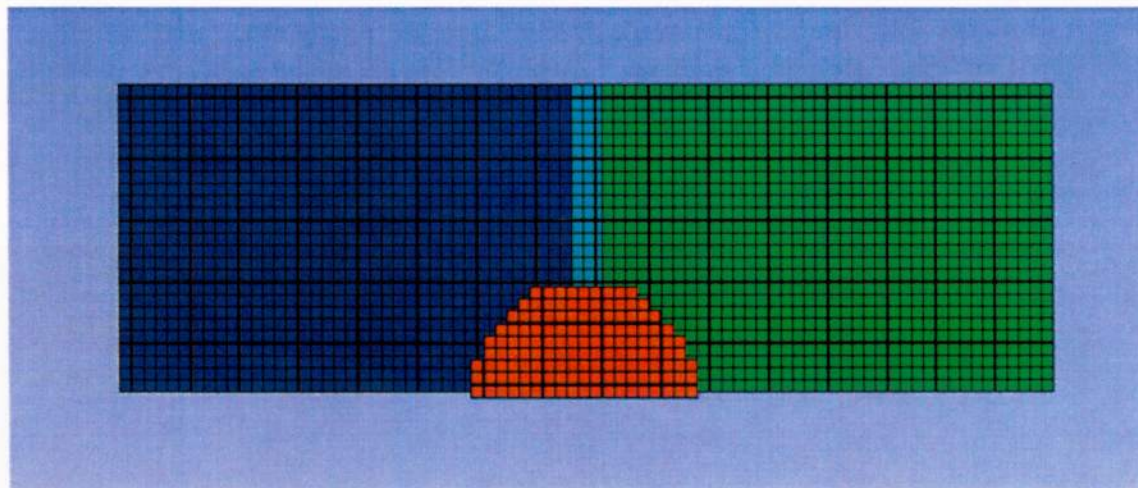
- ☐ SiC and SiC 2 have the same properties. They have been saved as separate materials to differentiate between the two ceramic tiles
- ☐ There is a gap size of 1.2 mm in-between the two ceramic tiles to simulate a impact on a seam

Target Dimensions

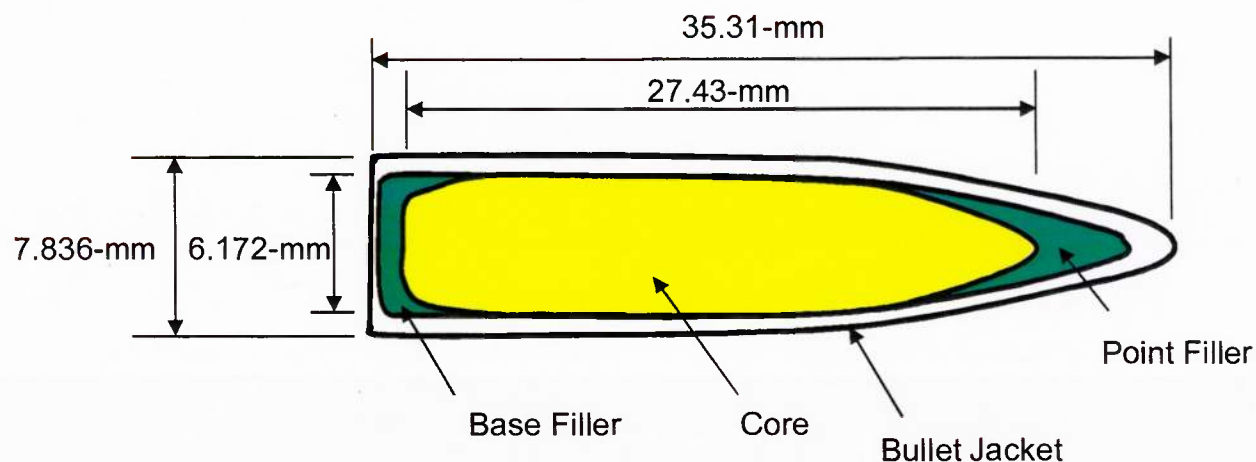


- ❑ **Aluminum Backing**
 - ❑ **Length = 35.08 mm**
- ❑ **Ceramic Plate(s)**
 - ❑ **Length (t_c) = 5.08 mm**
 - ❑ **Gap size = 1.2 mm**
- ❑ **Total Length = 40.08 mm**

FRONT VIEW OF MODEL AND PROJECTILE WITH GAP

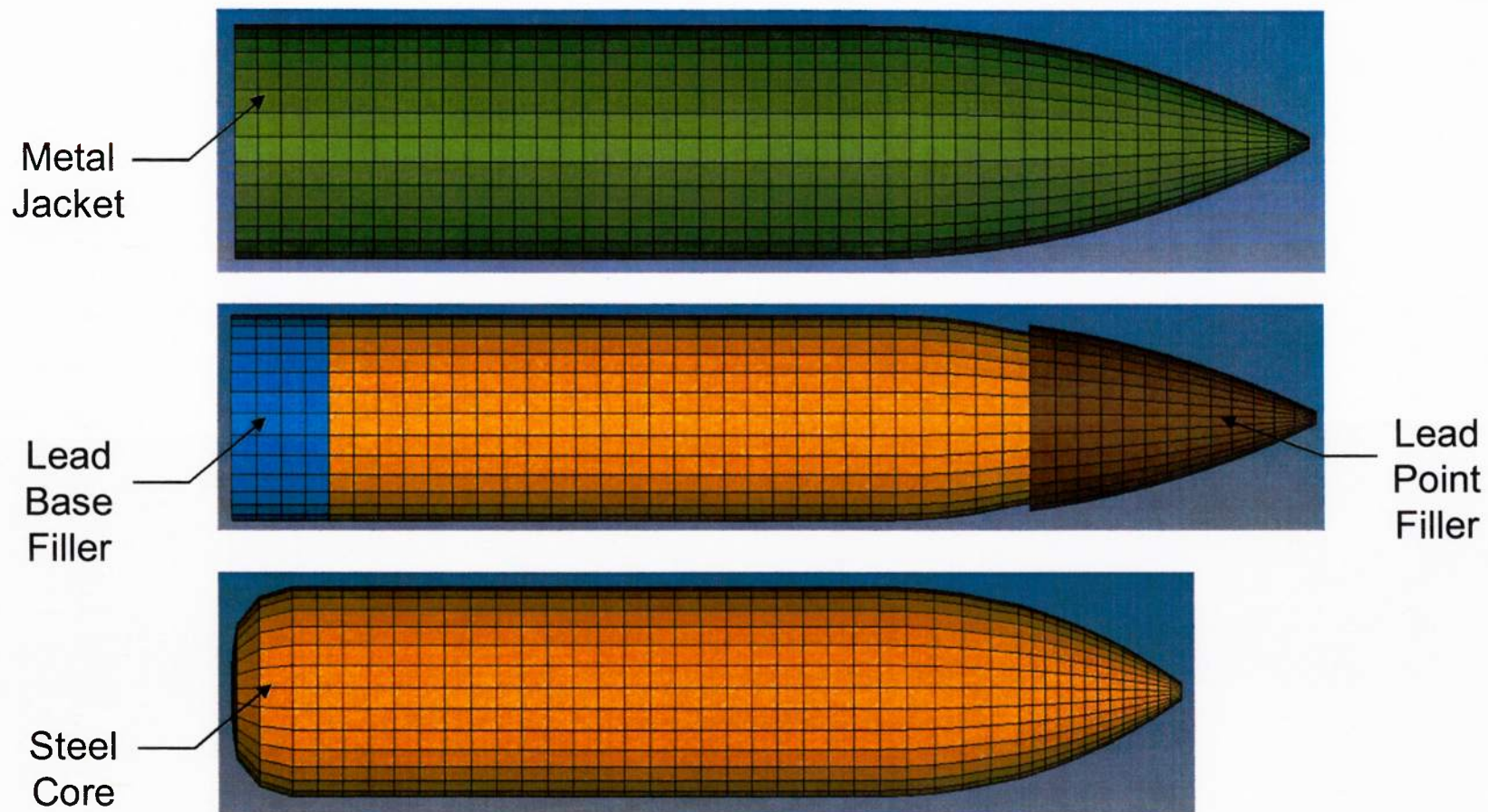


.30cal AP-M2 PROJECTILE MASS PROPERTIES



Component	Material	Weight (g)
Jacket	Gilding Metal	4.2
Core	Hardened Steel - RC 63	5.3
Point Filler	Lead	0.8
Base Filler	Lead	0.5
Total Weight		10.8

SOLID MODEL OF .30cal AP M2 PROJECTILE



MATERIAL PROPERTIES – AI 5083



Experimental AI 5083

	AI 5083
Density (g/cm ³)	2.65
Tensile Strength (MPa)	377.1
Yield Strength (MPa)	318.5
Elongation (%)	9.3

Ref:

MTL TR-86-14, 1986.

ARL-TR-2219, 2000.

AutoDyn AI 5083

Equation of State	Linear
Reference density	2.70000E+00 (g/cm ³)
Bulk Modulus	5.83300E+11 (ubar)
Reference Temperature	2.93000E+02 (K)
Specific Heat	9.10000E+06 (erg/gK)
Thermal Conductivity	0.00000E+00 ()
Strength	Johnson Cook
Shear Modulus	2.69200E+11 (ubar)
Yield Stress	1.67000E+09 (ubar)
Hardening Constant	5.96000E+09 (ubar)
Hardening Exponent	5.51000E-01 (none)
Strain Rate Constant	1.00000E-03 (none)
Thermal Softening Exponent	8.59000E-01 (none)
Melting Temperature	8.93000E+02 (K)
Ref. Strain Rate (/s)	1.00000E+00 (none)
Strain Rate Correction	1st Order
Failure	None
Erosion	None
Material Cutoffs	-
Maximum Expansion	1.00000E-01 (none)
Minimum Density Factor	1.00000E-05 (none)
Minimum Density Factor (SPH)	2.00000E-01 (none)
Maximum Density Factor (SPH)	3.00000E+00 (none)
Minimum Soundspeed	1.00000E-04 (cm/s)
Maximum Soundspeed (SPH)	1.01000E+20 (cm/s)
Maximum Temperature	1.00000E+16 (K)

MATERIAL PROPERTIES - SiC



Experimental SiC

	SiC
Density (g/cm ³)	3.20
Elastic Modulus (GPa)	455
Shear Modulus (GPa)	195
Longitudinal Wave Velocity (km/s)	12.3
Poisson's Ratio	0.14
Hardness (kg/mm ²)	2700
Compressive Strength (MPa)	3410

Ref:
ARL-TR-2219, 2000.

AutoDyn SiC

Equation of State	Polynomial
Reference density	3.21500E+00 (g/cm3)
Bulk Modulus A1	2.20000E+12 (ubar)
Parameter A2	3.61000E+12 (ubar)
Parameter A3	0.00000E+00 (ubar)
Parameter B0	0.00000E+00 (none)
Parameter B1	0.00000E+00 (none)
Parameter T1	2.20000E+12 (ubar)
Parameter T2	0.00000E+00 (ubar)
Reference Temperature	2.93000E+02 (K)
Specific Heat	0.00000E+00 (erg/gK)
Thermal Conductivity	0.00000E+00 ()
Strength	Johnson-Holmquist
Shear Modulus	1.93500E+12 (ubar)
Model Type	Segmented (JH1)
Hugoniot Elastic Limit, HEL	1.17000E+11 (ubar)
Intact Strength Constant, S1	7.10000E+10 (ubar)
Intact Strength Constant, P1	2.50000E+10 (ubar)
Intact Strength Constant, S2	1.22000E+11 (ubar)
Intact Strength Constant, P2	1.00000E+11 (ubar)
Strain Rate Constant, C	9.00000E-03 (none)
Max. Fracture Strength, SFMAX	1.30000E+10 (ubar)
Failed Strength Constant, ALPHA	4.00000E-01 (none)
Failure	Johnson Holmquist
Hydro Tensile Limit	-7.50000E+09 (ubar)
Model Type	Segmented (JH1)
Damage Constant, EFMAX	1.20000E+00 (none)
Damage Constant, P3	9.97500E+11 (ubar)
Bulking Constant, Beta	1.00000E+00 (none)
Damage Type	Instantaneous (JH1)
Tensile Failure	Hydro (Pmin)

CALCULATING DEPTH OF PENETRATION

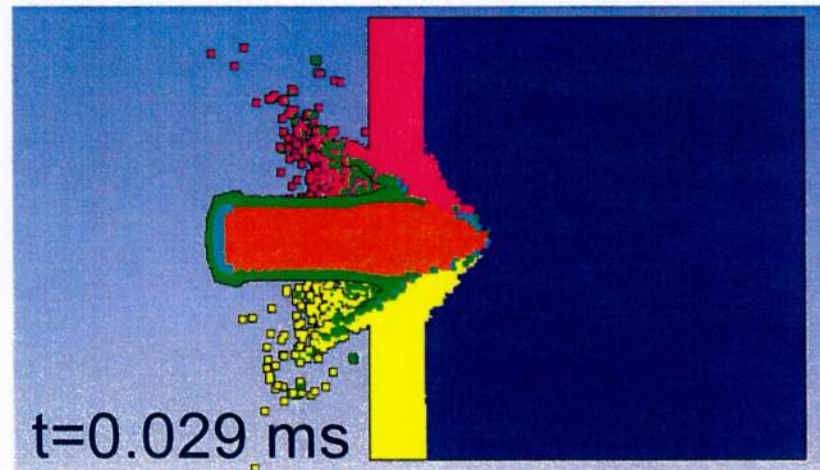
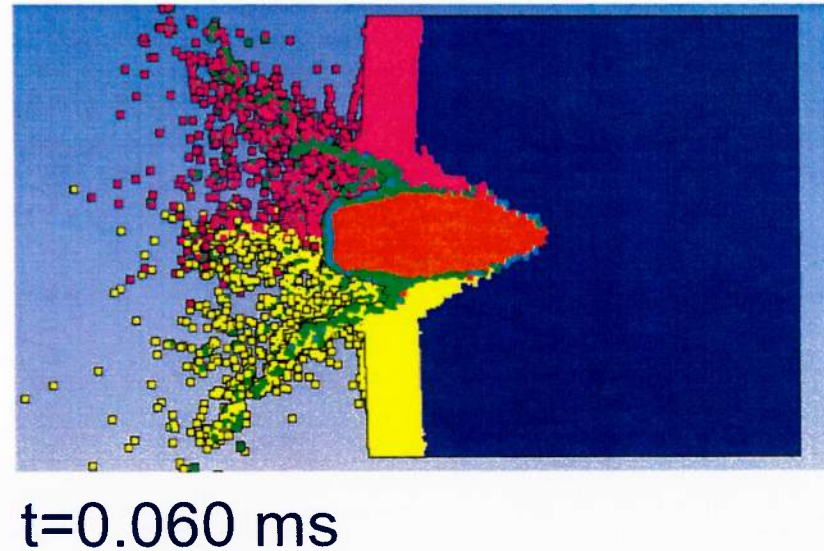
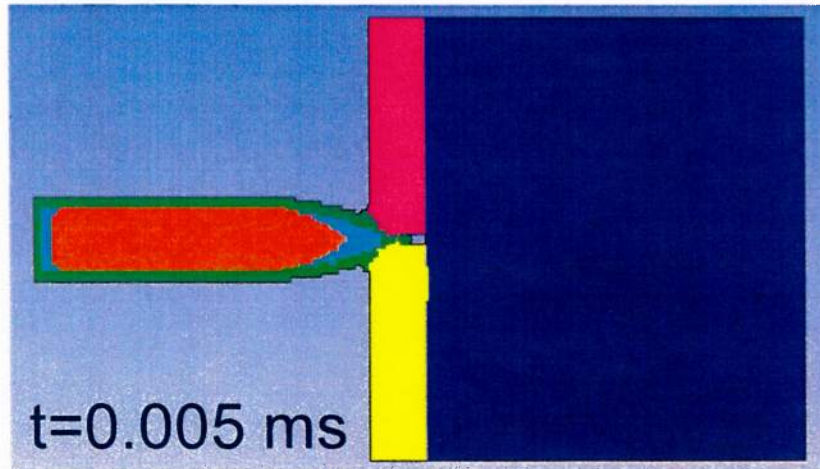


☐ DoP is calculated:

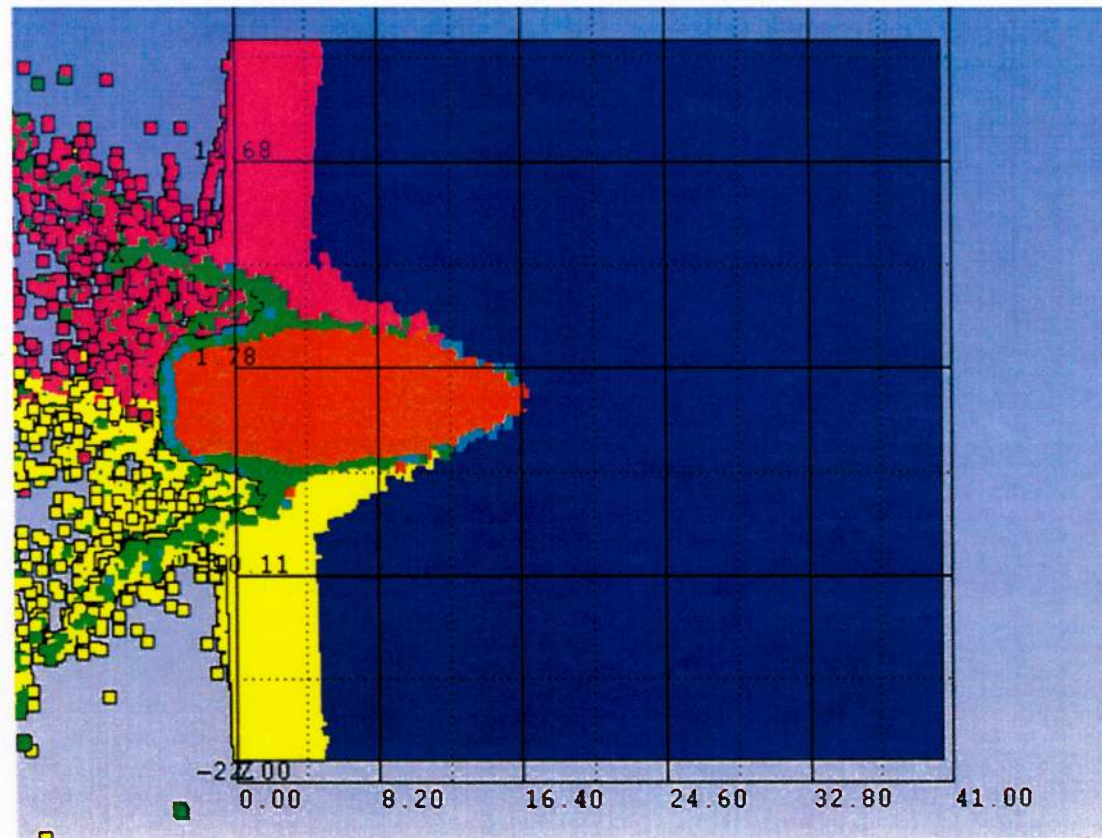
$$DOP = L - L_{NP}$$

- ☐ Where L is the length of the entire target ceramic tiles and aluminum backing
- ☐ L_{NP} is the length of the target left not penetrated when the velocity and kinetic energy of the projectile have reached zero

$V_0 = 700 \text{ m/s}$ $t_c = 5.08 \text{ mm}$ particle size
 $= 0.4$, Gap = 1.2 mm

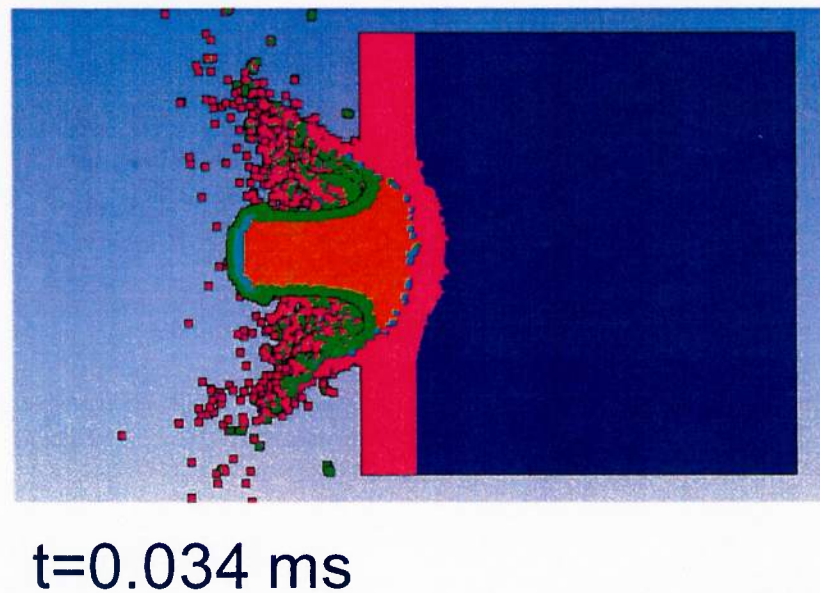
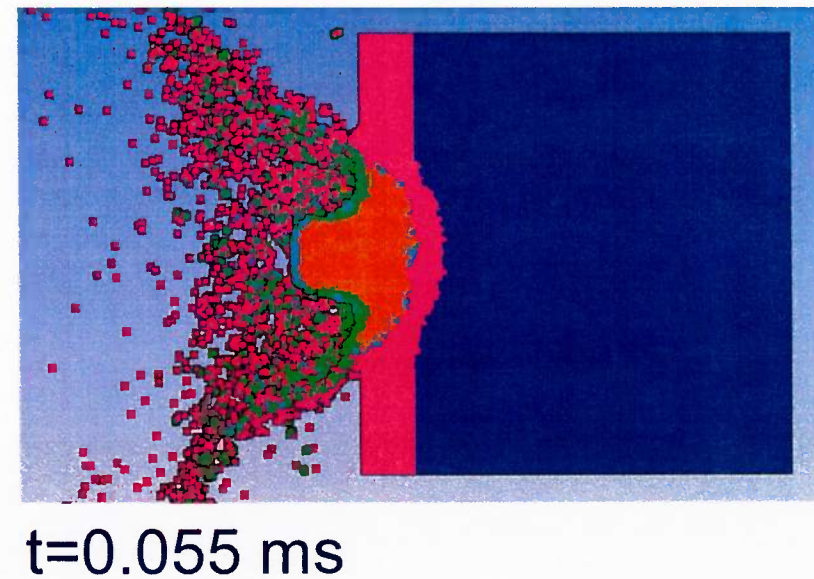
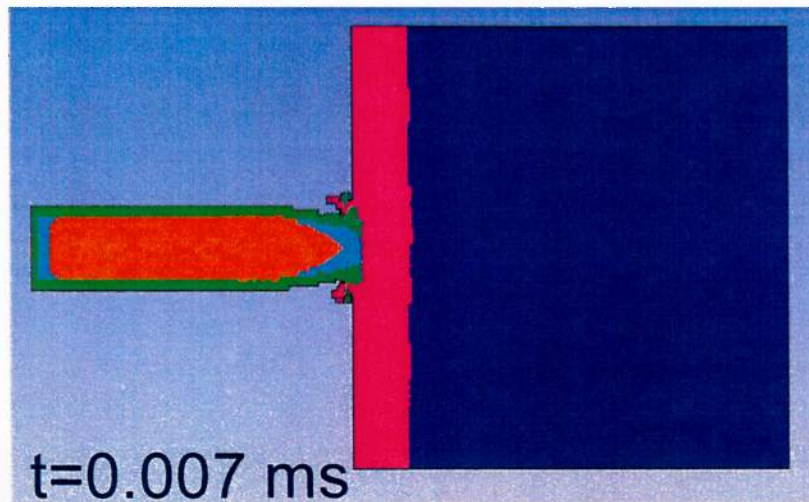


DEPTH OF PENETRATION $V_0 = 700$ m/s $t_c = 5.08$ mm particle size = 0.4, Gap = 1.2 mm

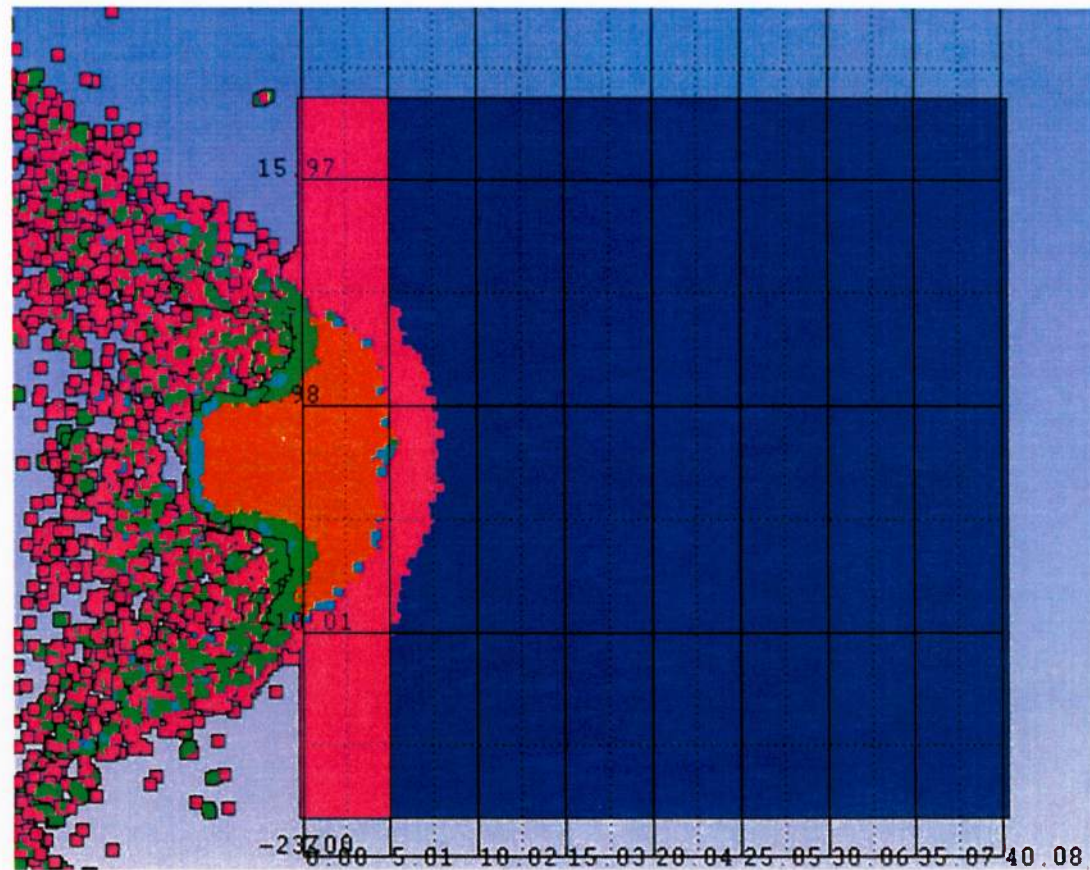


$$\text{DOP} = L - L_{np} = 40.08 - 23.68 = 16.40 \text{ mm}$$

$V_o = 700 \text{ m/s}$ $t_c = 5.08 \text{ mm}$ particle size
 $= 0.4$, No Gap

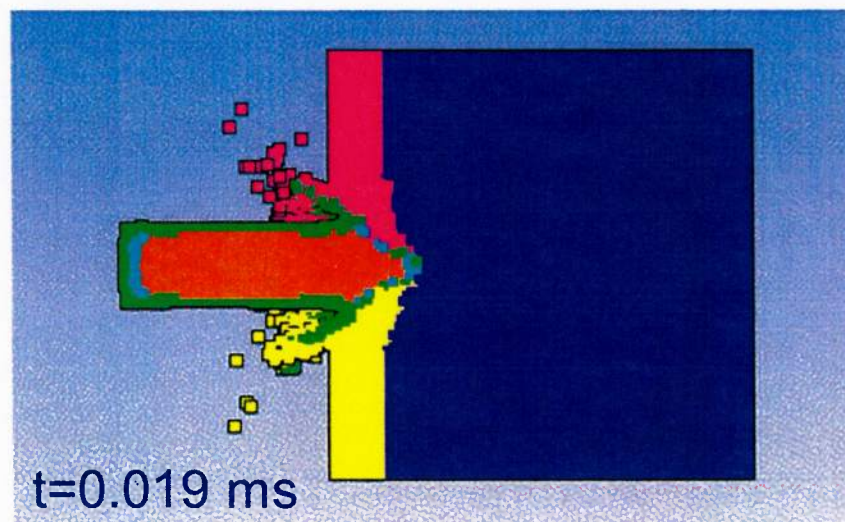
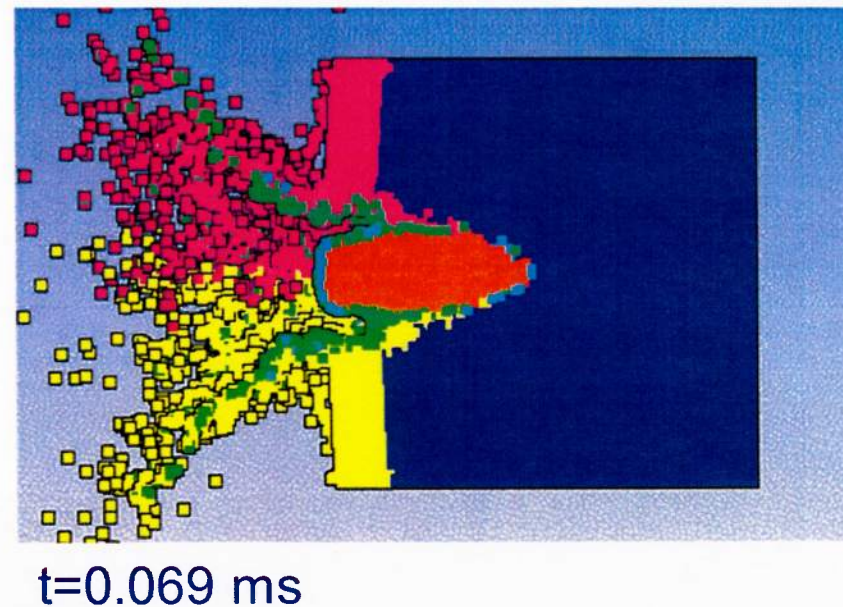
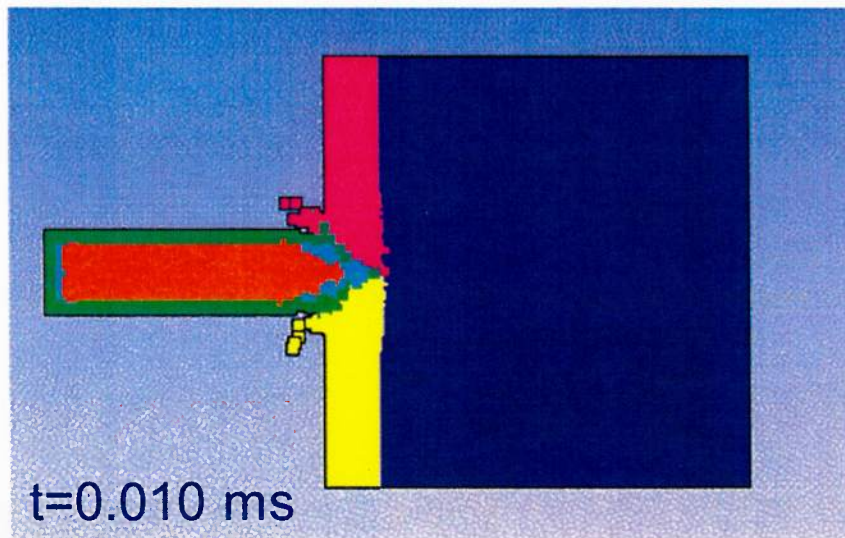


DEPTH OF PENETRATION $V_o = 700$ m/s $t_c = 5.08$ mm particle size = 0.4, No Gap

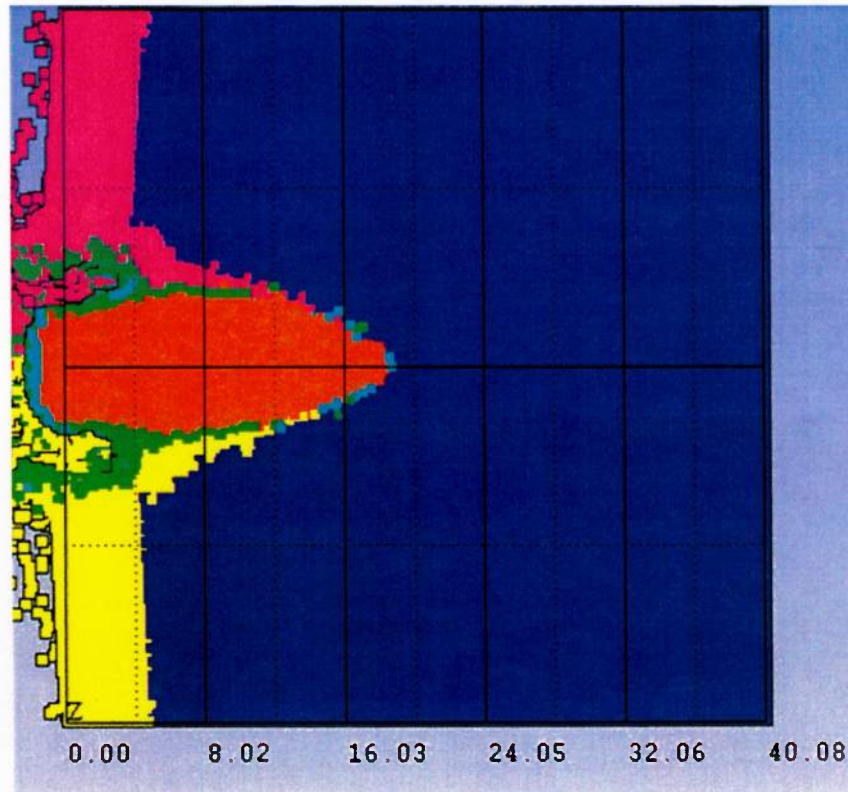


$$\text{DOP} = L - L_{np} = 40.08 - 30.06 = 10.02 \text{ mm}$$

**$V_o = 750 \text{ m/s}$ $t_c = 5.08 \text{ mm}$ particle size
 $= 0.4$, Gap $= 1.2 \text{ mm}$**

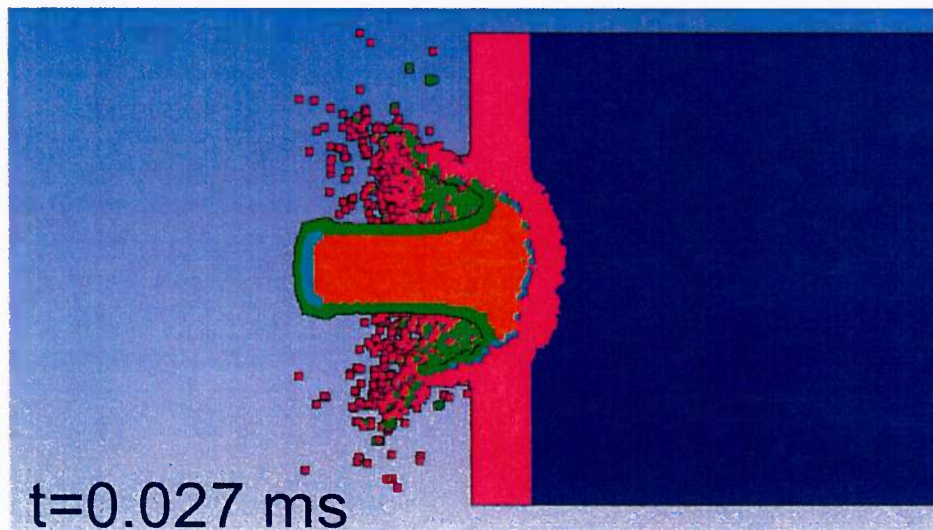
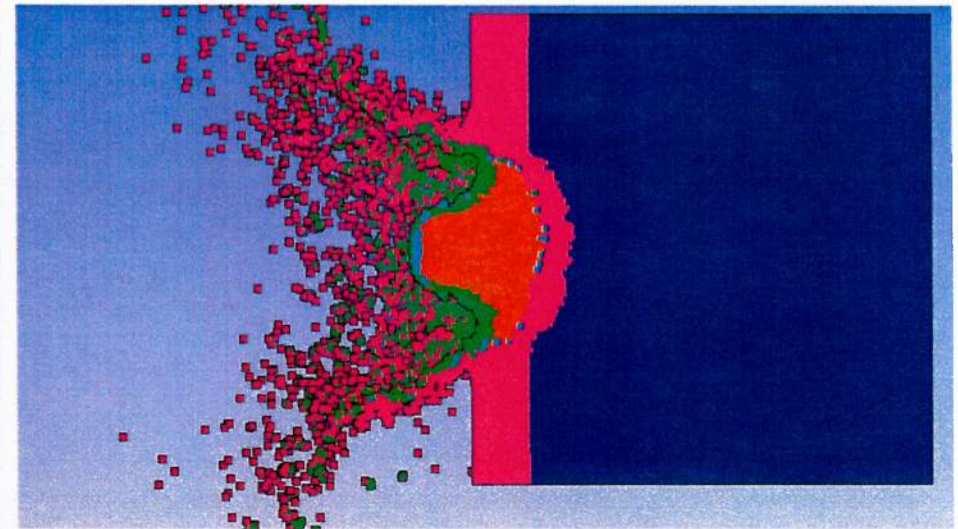
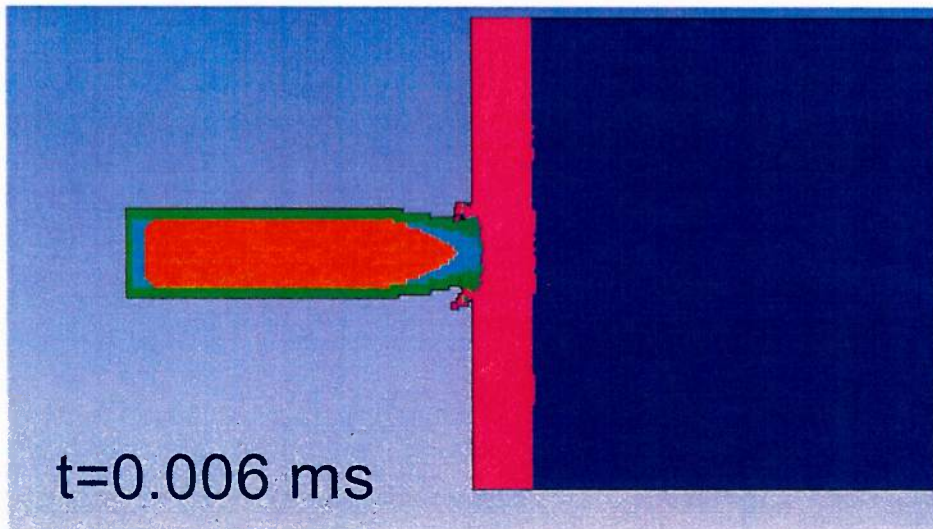


DEPTH OF PENETRATION $V_o = 750$ m/s $t_c = 5.08$ mm particle size = 0.4, Gap = 1.2 mm

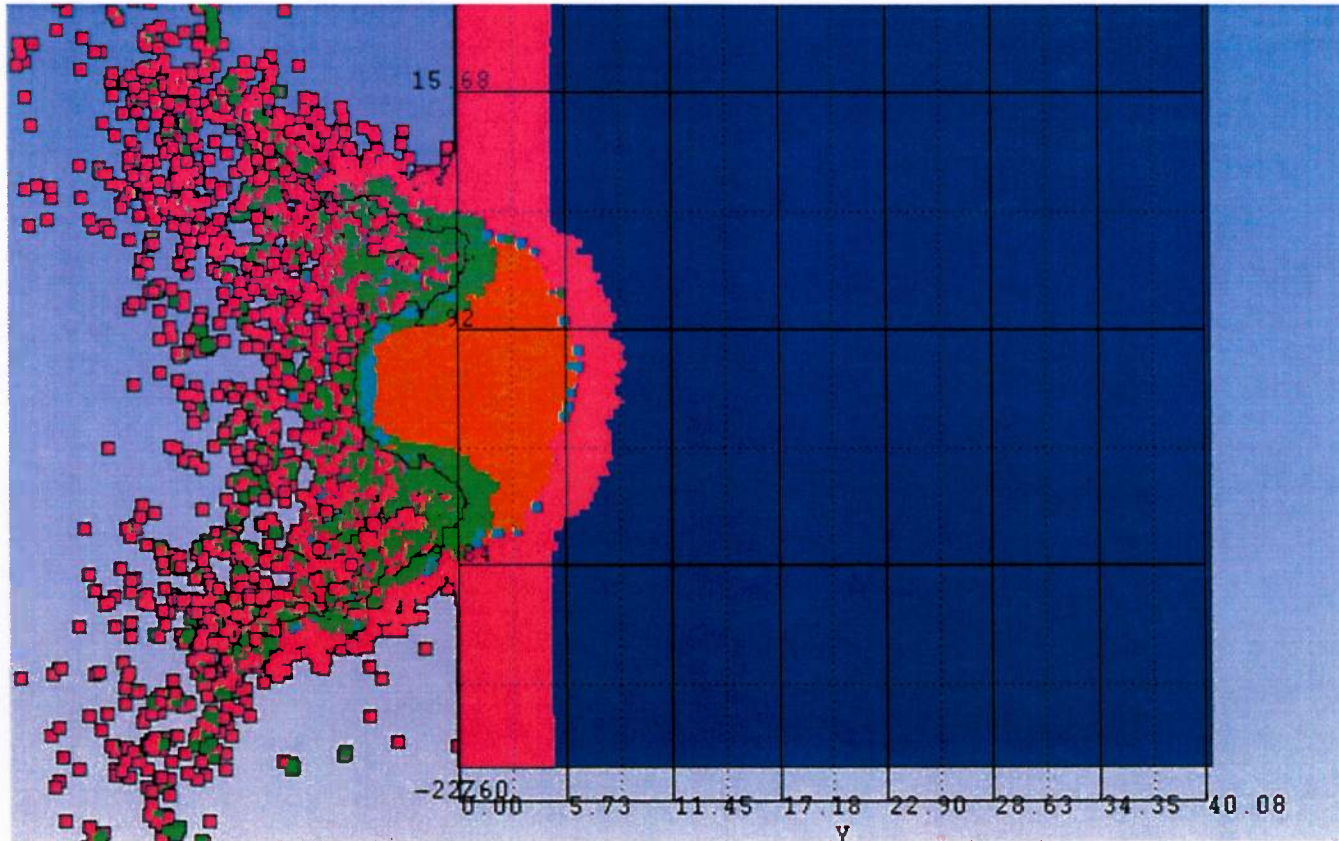


$$\text{DOP} = L - L_{np} = 40.08 - 21.38 = 18.70 \text{ mm}$$

$V_o = 750 \text{ m/s}$ $t_c = 5.08 \text{ mm}$ particle size
 $= 0.4$, No Gap

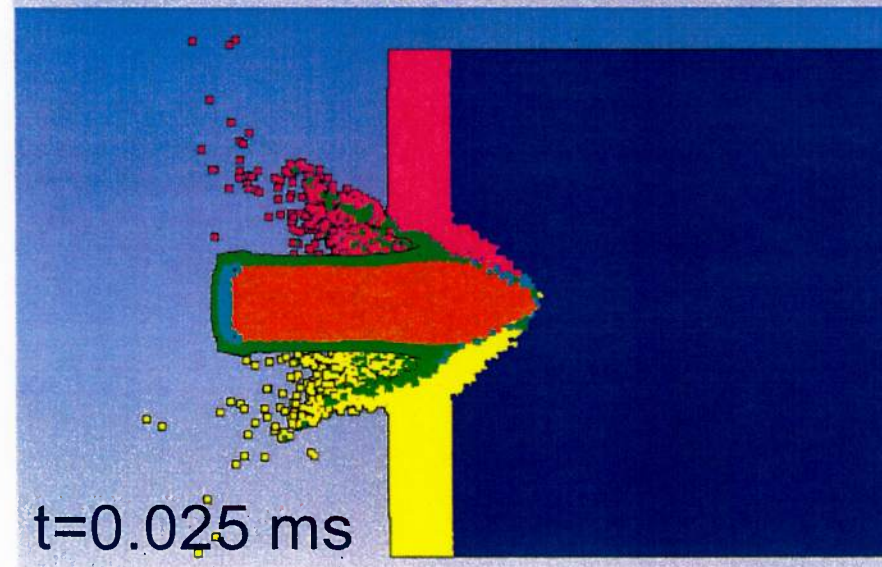
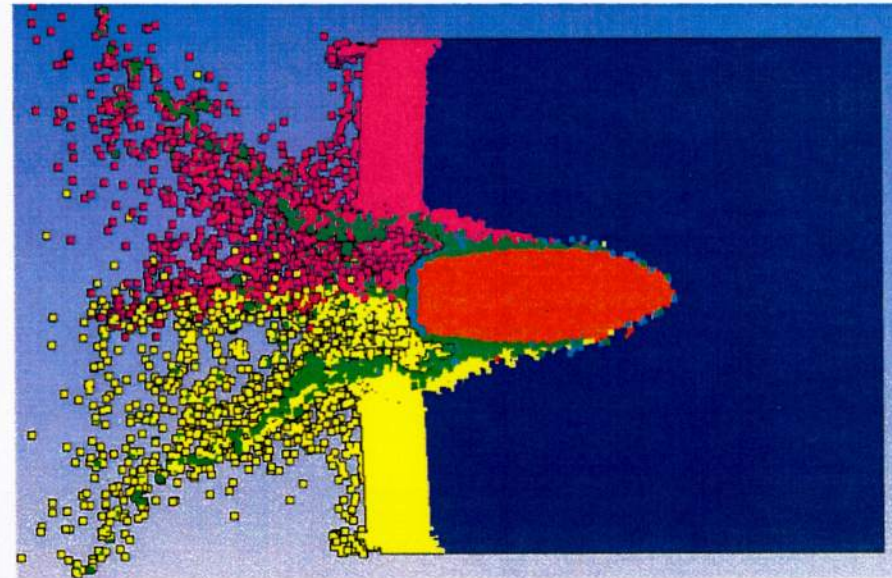
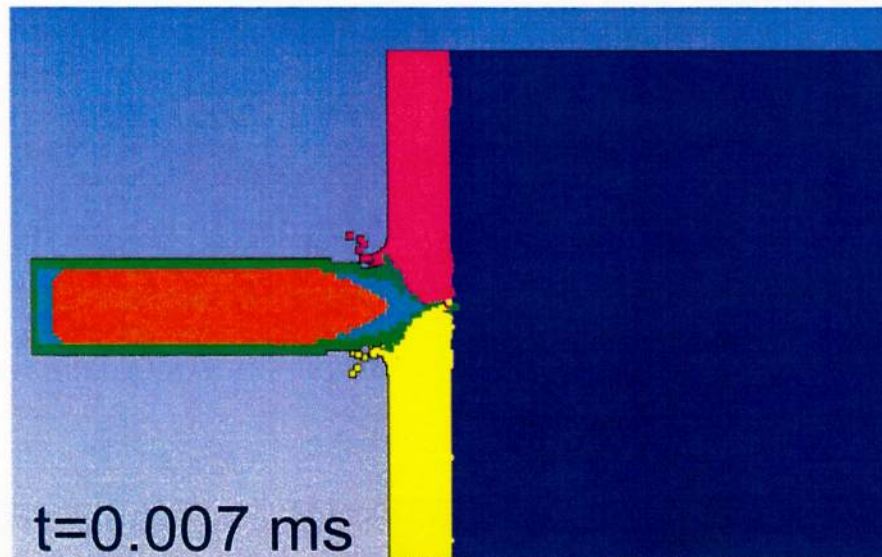


DEPTH OF PENETRATION $V_o = 750$ m/s $t_c = 5.08$ mm particle size = 0.4, No Gap

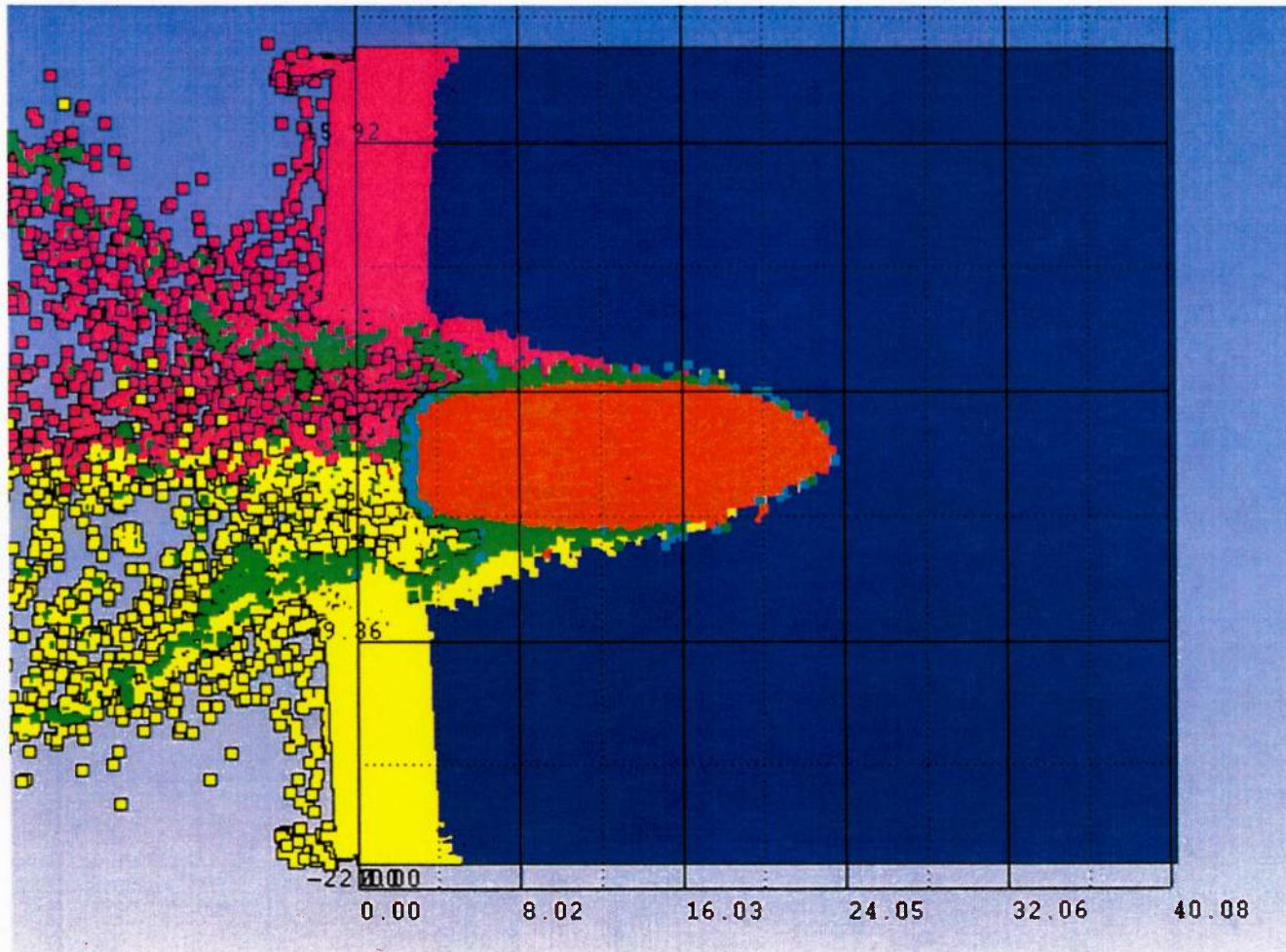


$$\text{DOP} = L - L_{np} = 40.08 - 31.49 = 8.59 \text{ mm}$$

$V_o = 850 \text{ m/s}$ $t_c = 5.08 \text{ mm}$ particle size
 $= 0.4$, Gap = 1.2 mm

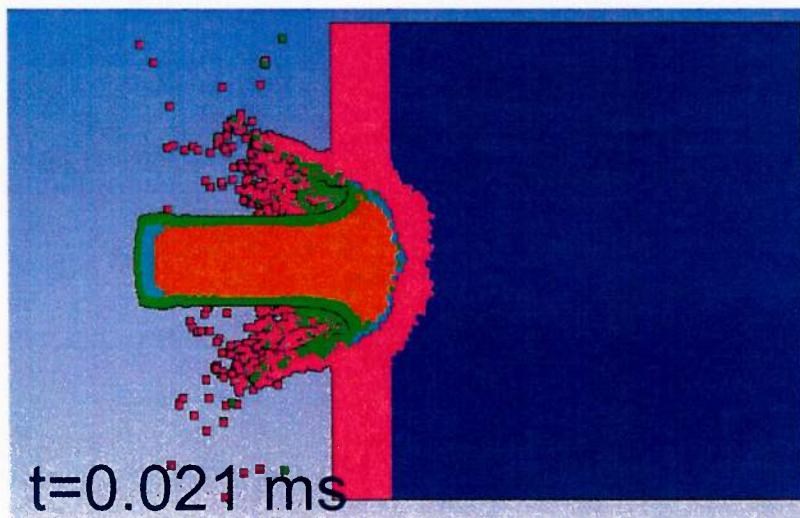
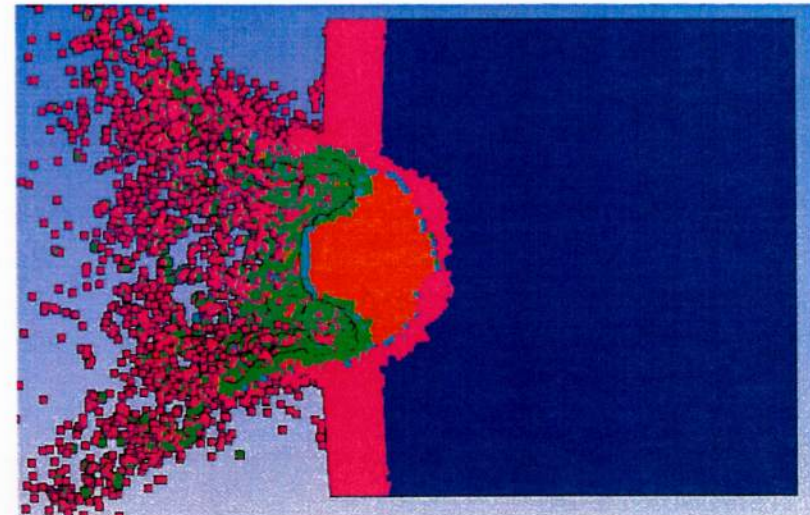
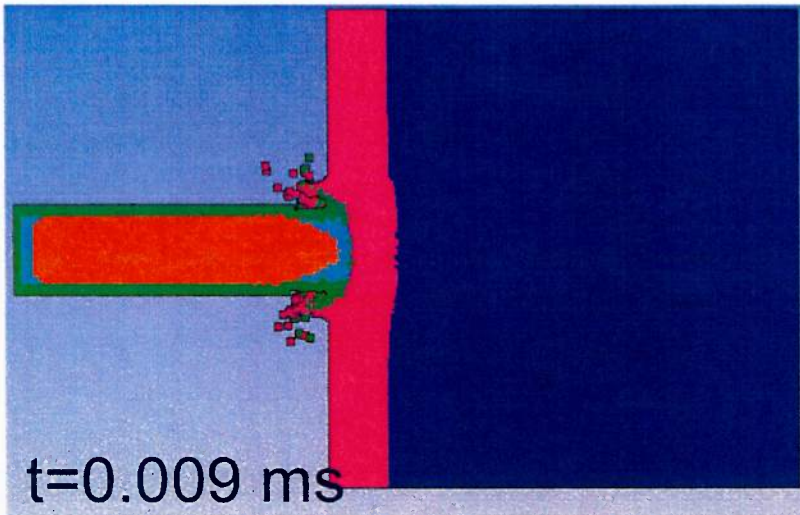


**DEPTH OF PENETRATION $V_o = 850$ m/s $t_c =$
5.08 mm particle size = 0.4, Gap = 1.2 mm**

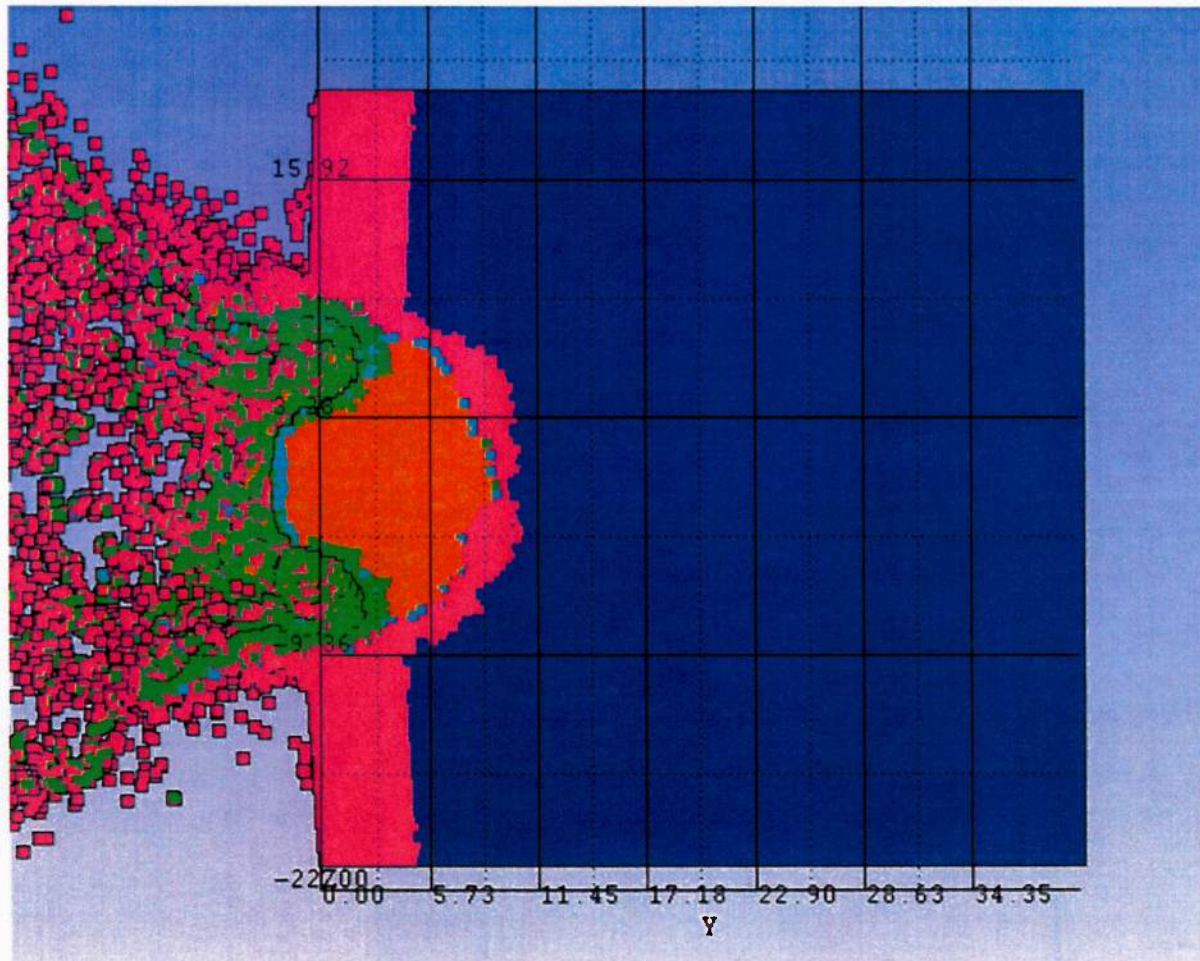


$$\text{DOP} = L - L_{np} = 40.08 - 16.03 = 24.05 \text{ mm}$$

**$V_o = 850 \text{ m/s}$ $t_c = 5.08 \text{ mm}$ particle size
 $= 0.4$, No Gap**

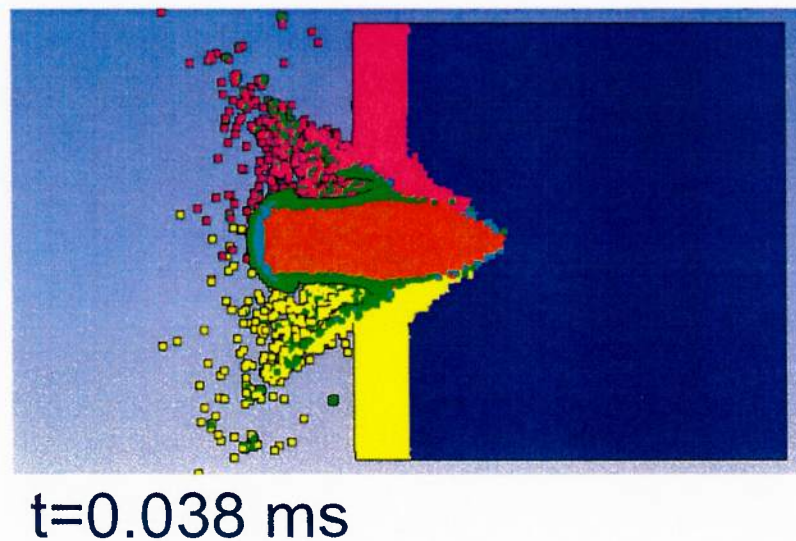
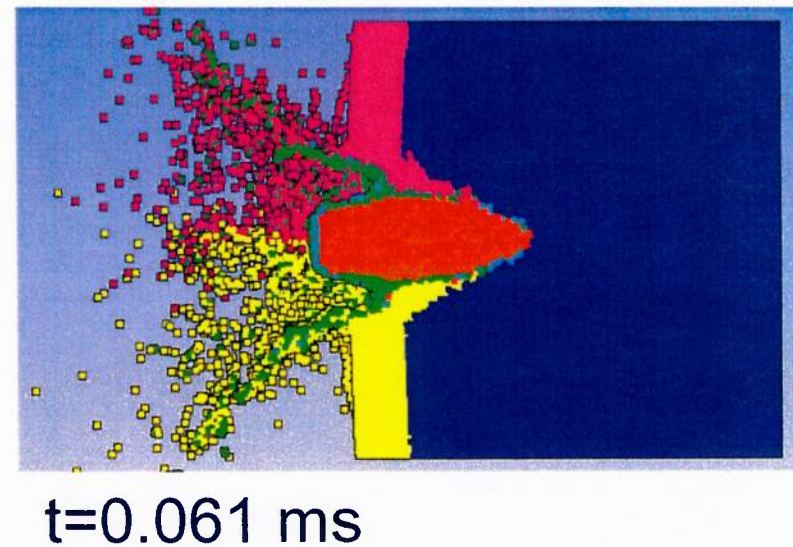
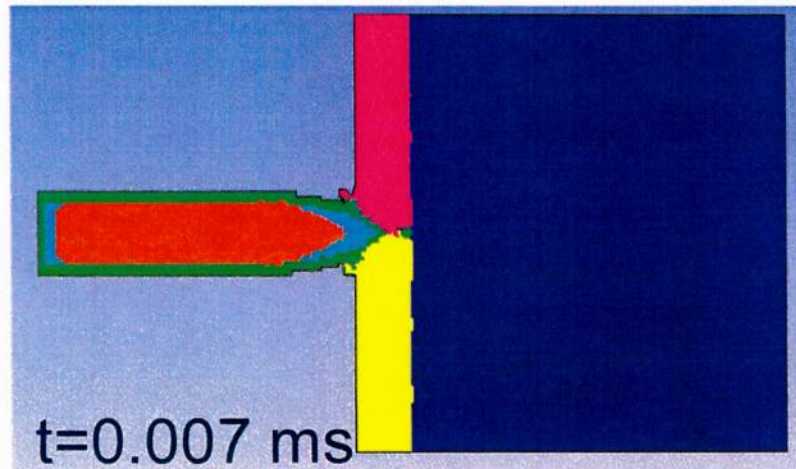


DEPTH OF PENETRATION $V_o = 850$ m/s $t_c = 5.08$ mm particle size = 0.4, No Gap

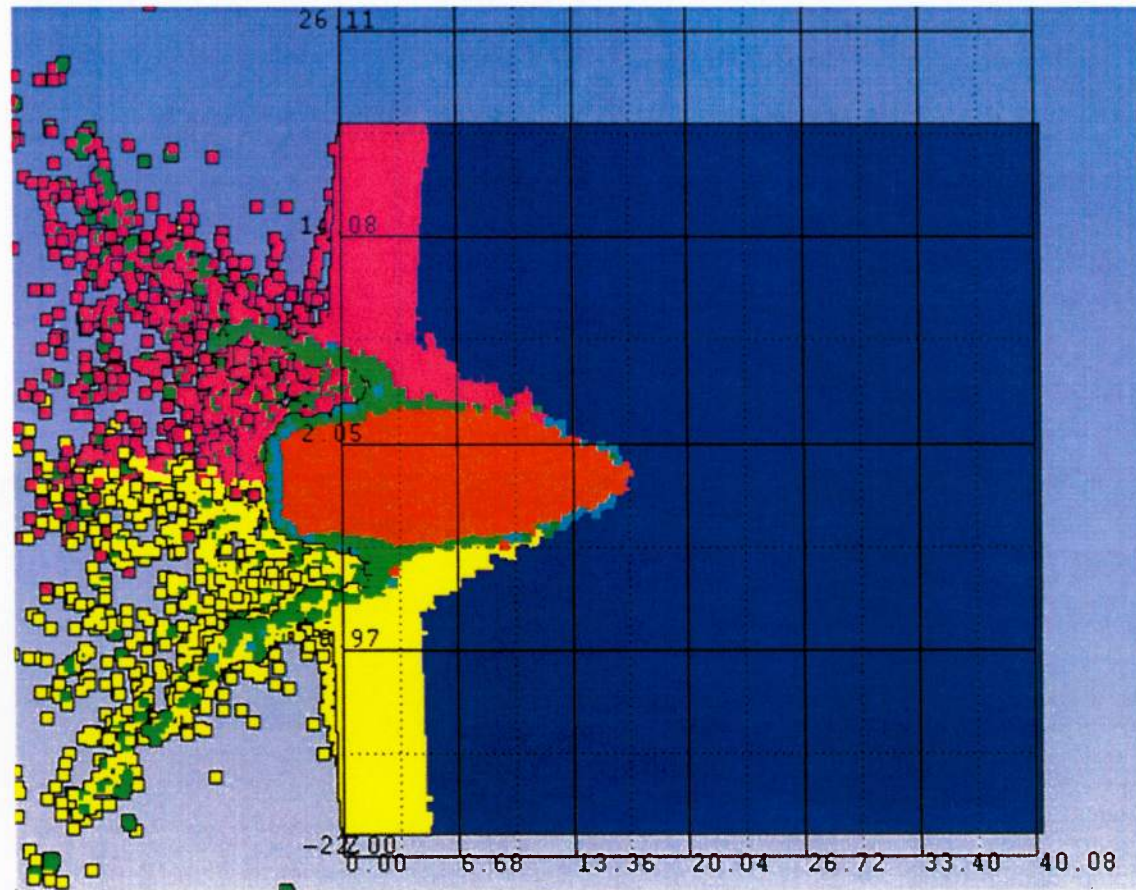


$$\text{DOP} = L - L_{np} = 40.08 - 30.08 = 10.00 \text{ mm}$$

**$V_0 = 900 \text{ m/s}$ $t_c = 5.08 \text{ mm}$ particle size
 $= 0.4$, Gap = 1.2 mm**

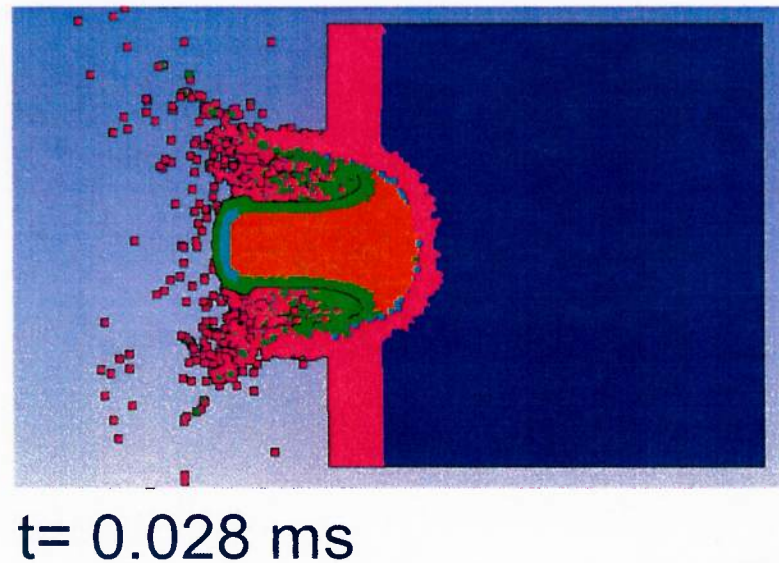
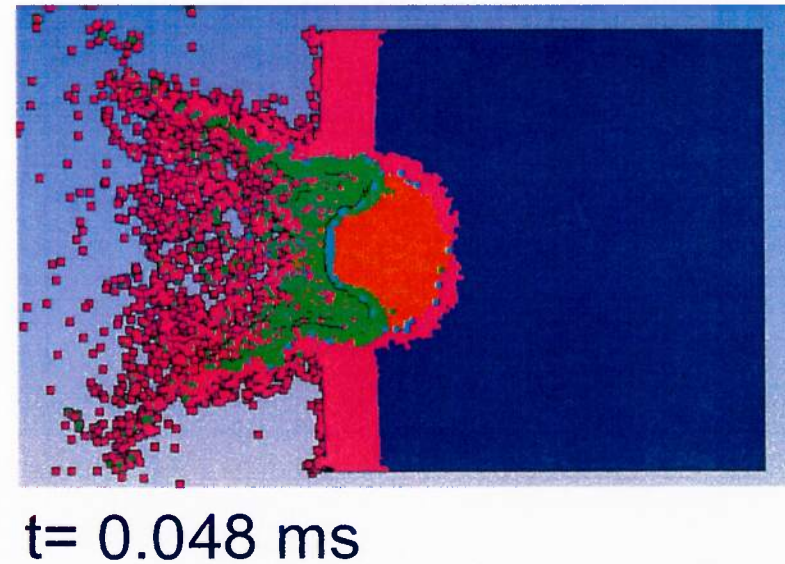
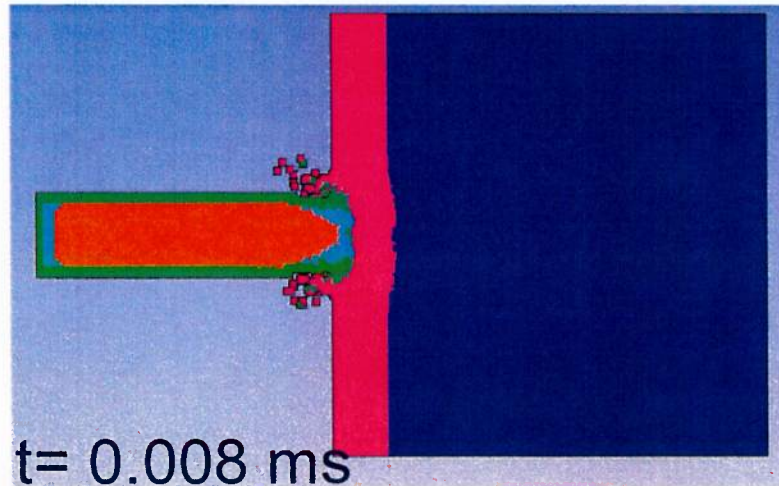


DEPTH OF PENETRATION $V_o = 900$ m/s $t_c = 5.08$ mm particle size = 0.4, Gap = 1.2 mm

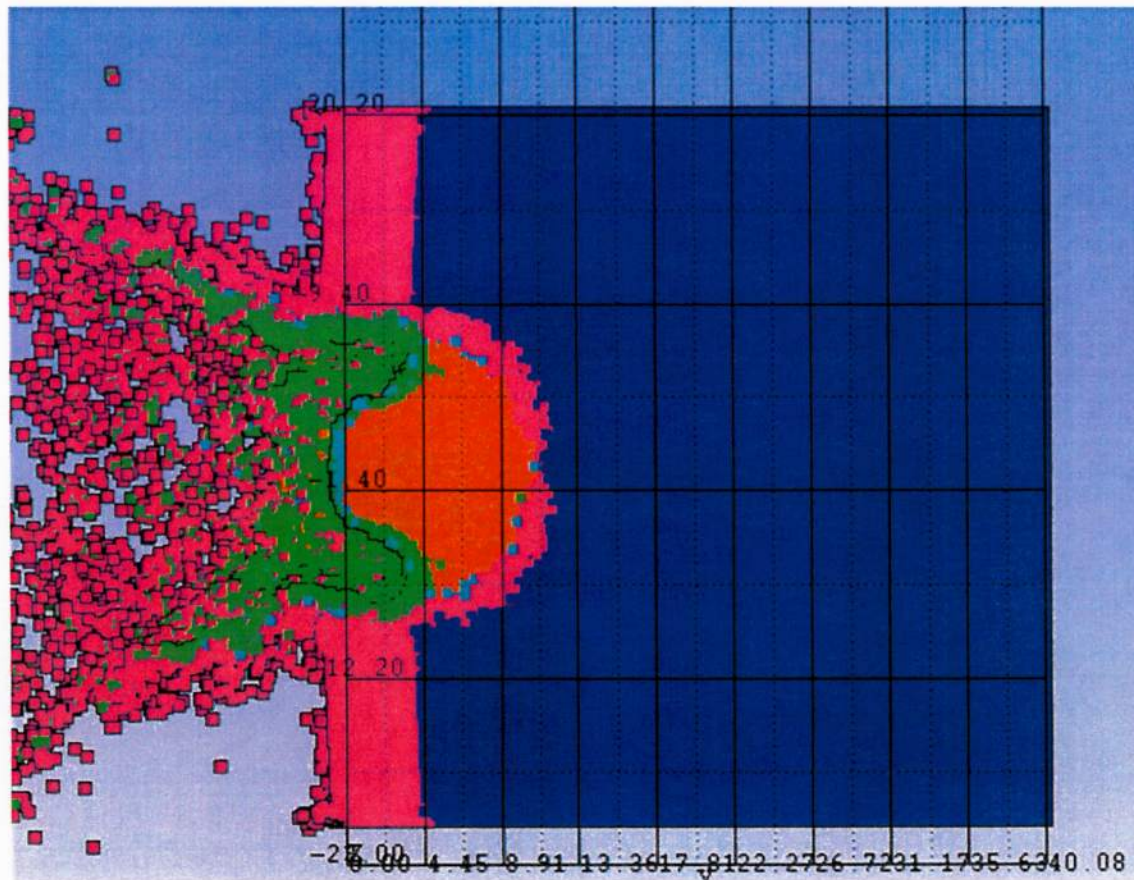


$$\text{DOP} = L - L_{np} = 40.08 - 20.04 = 20.04 \text{ mm}$$

$V_0 = 900 \text{ m/s}$ $t_c = 5.08 \text{ mm}$ particle size
 $= 0.4$, No Gap

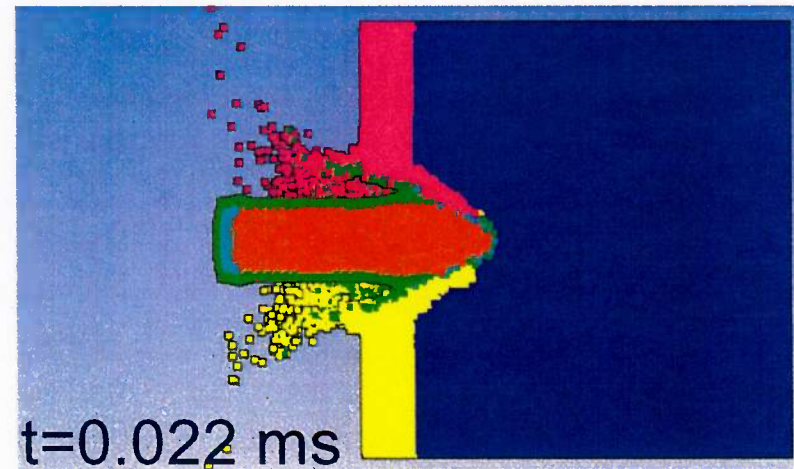
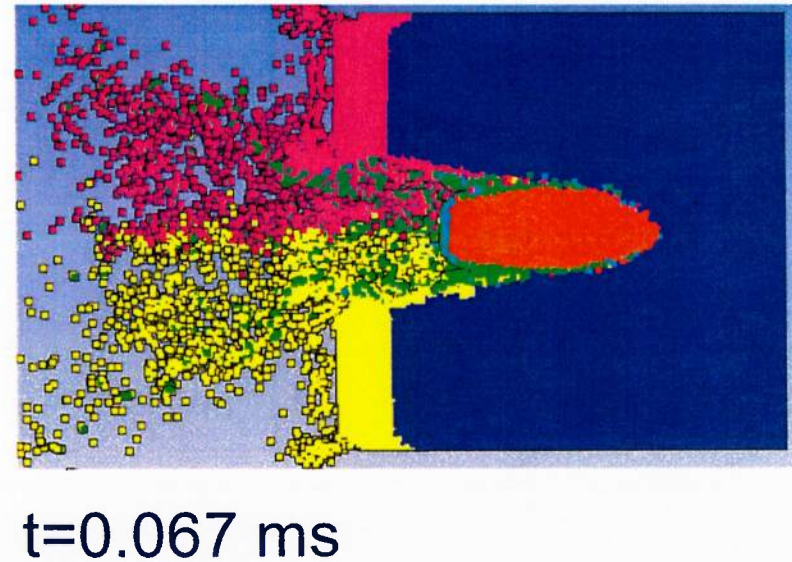
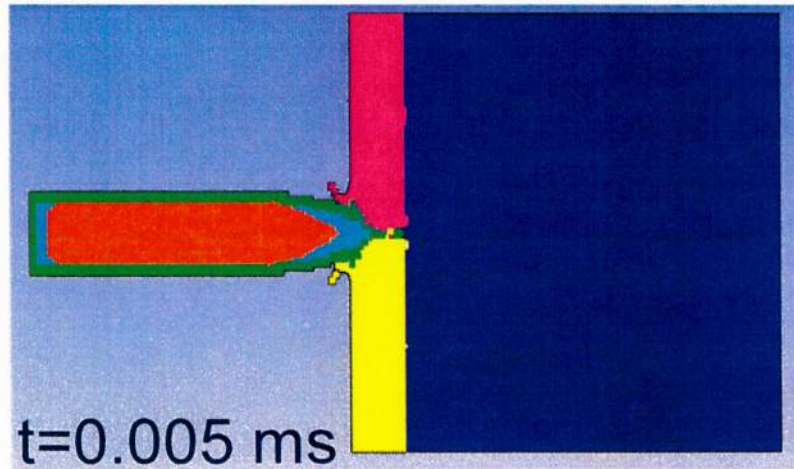


DEPTH OF PENETRATION $V_0 = 900$ m/s $t_c = 5.08$ mm particle size = 0.4, No Gap

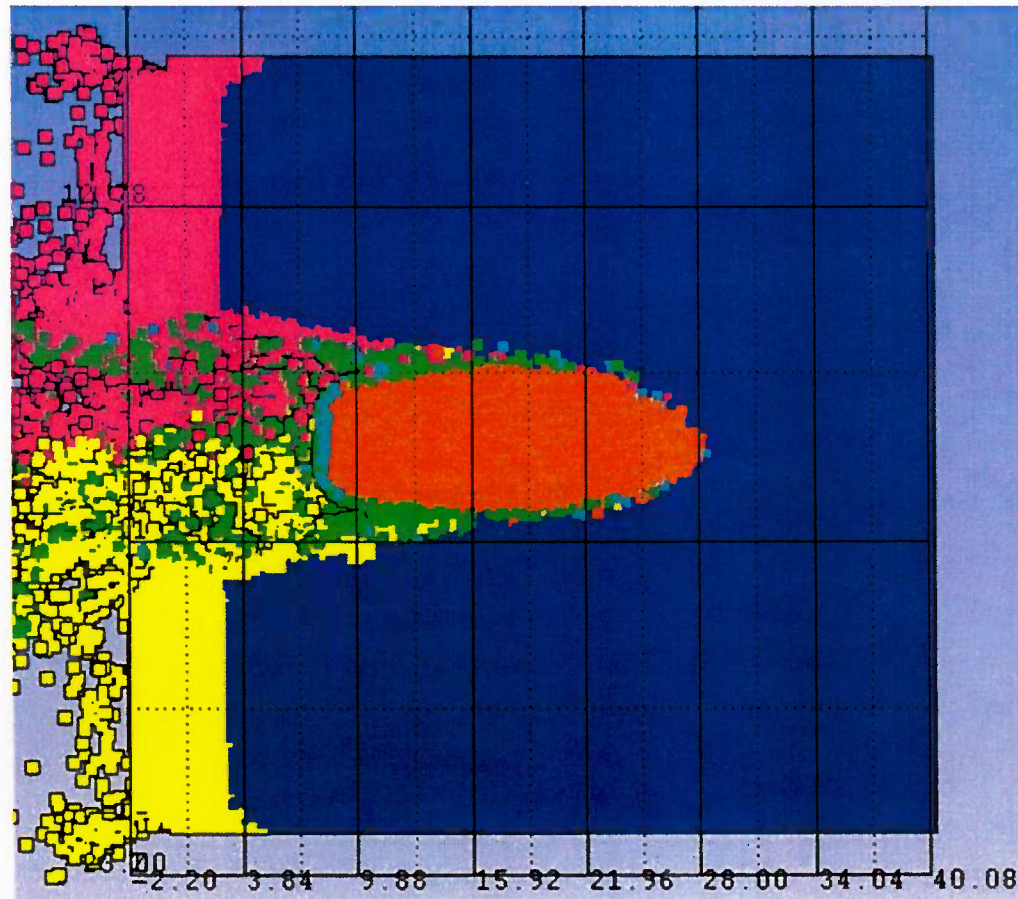


$$\text{DOP} = L - L_{np} = 40.08 - 28.95 = 11.13 \text{ mm}$$

$V_o = 950 \text{ m/s}$ $t_c = 5.08 \text{ mm}$ particle size
 $= 0.4$, Gap = 1.2 mm

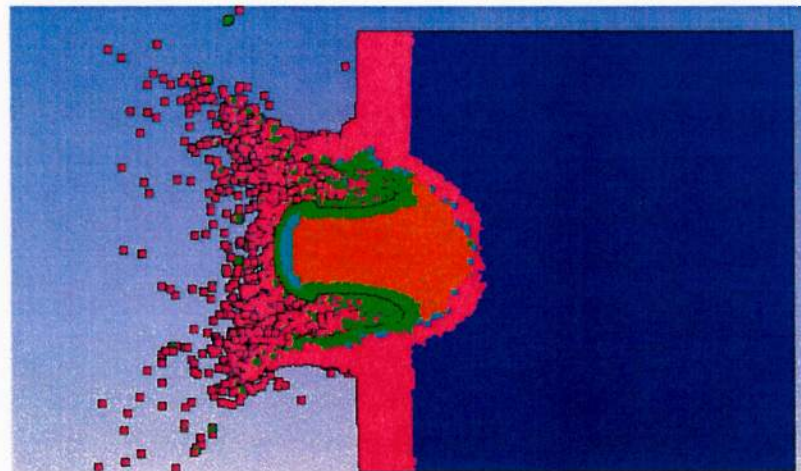
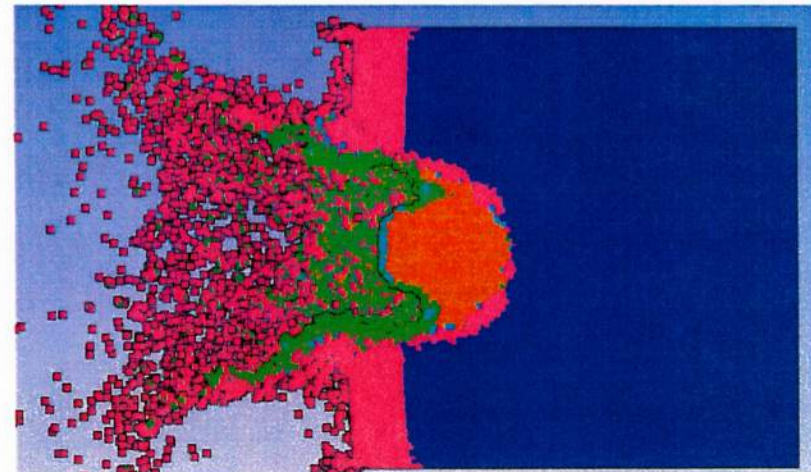
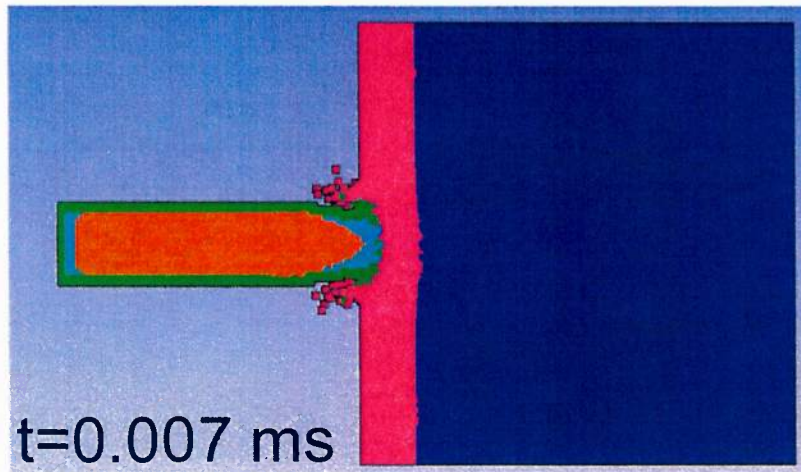


DEPTH OF PENETRATION $V_o = 950$ m/s $t_c = 5.08$ mm particle size = 0.4, Gap = 1.2 mm

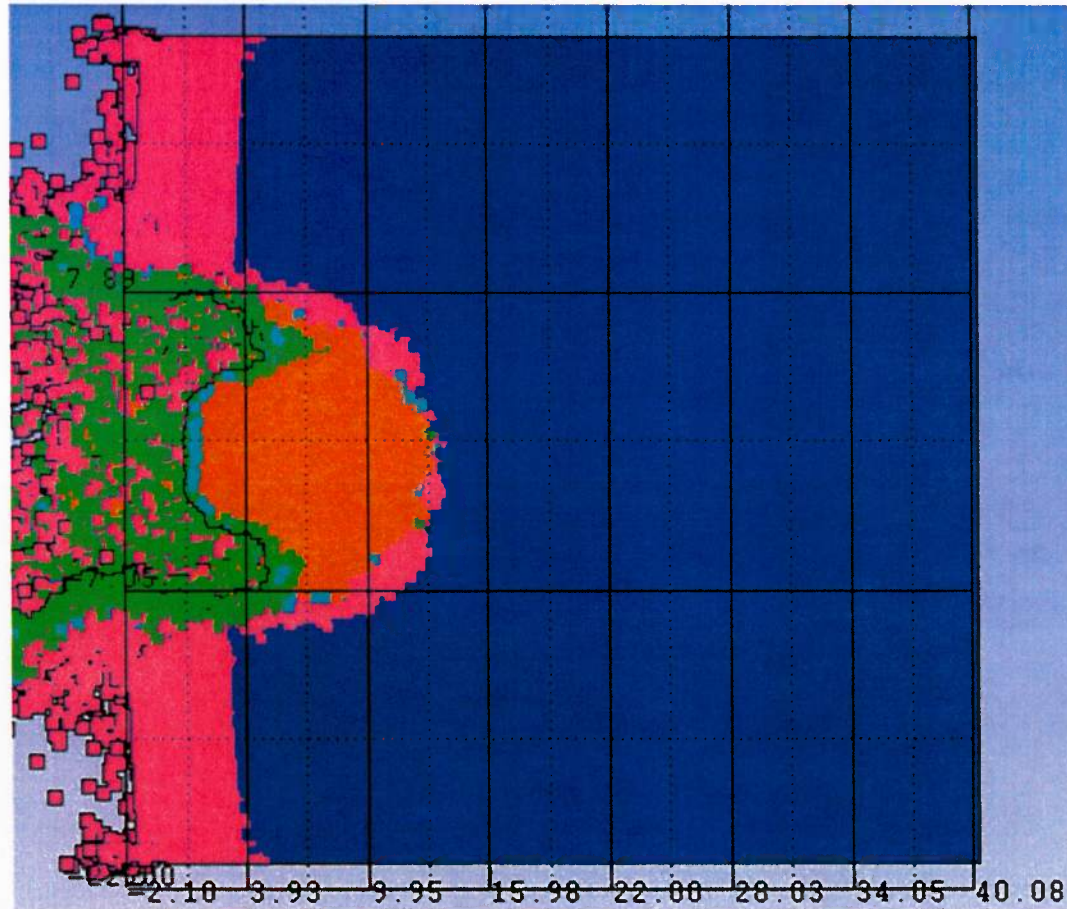


$$\text{DOP} = L - L_{np} = 40.08 - 12.08 = 28.00 \text{ mm}$$

$V_0 = 950 \text{ m/s}$ $t_c = 5.08 \text{ mm}$ particle size
 $= 0.4$, No Gap

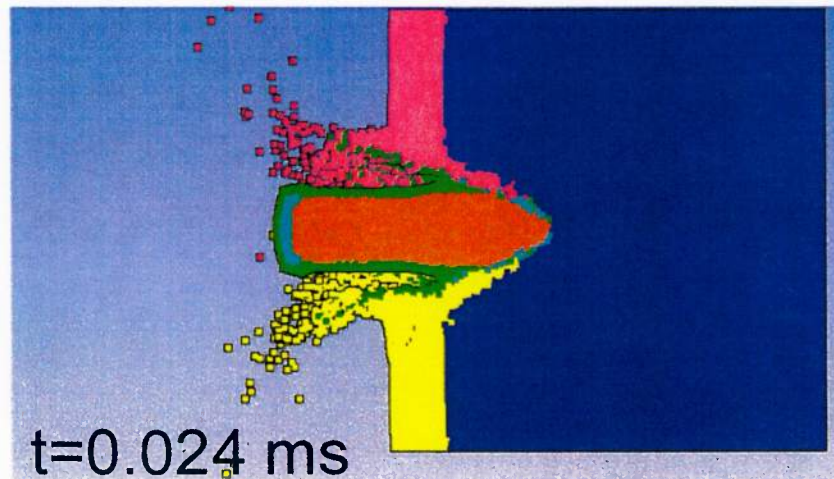
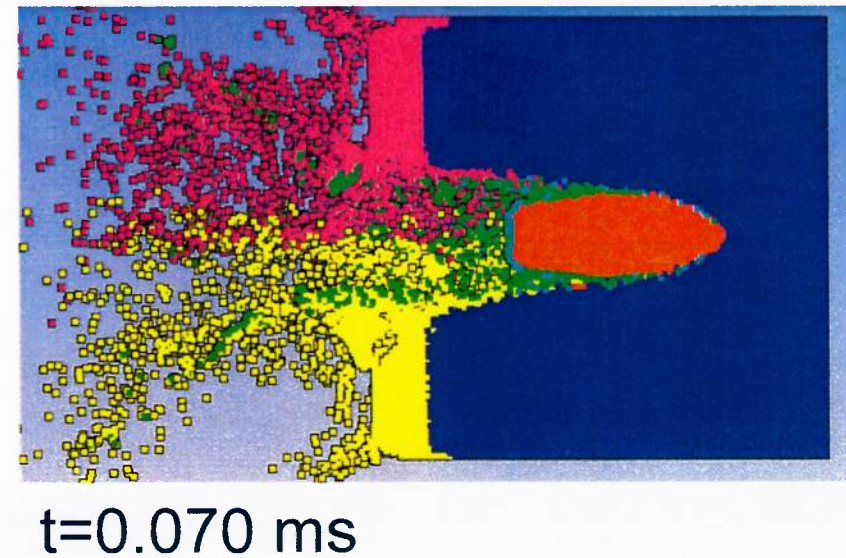
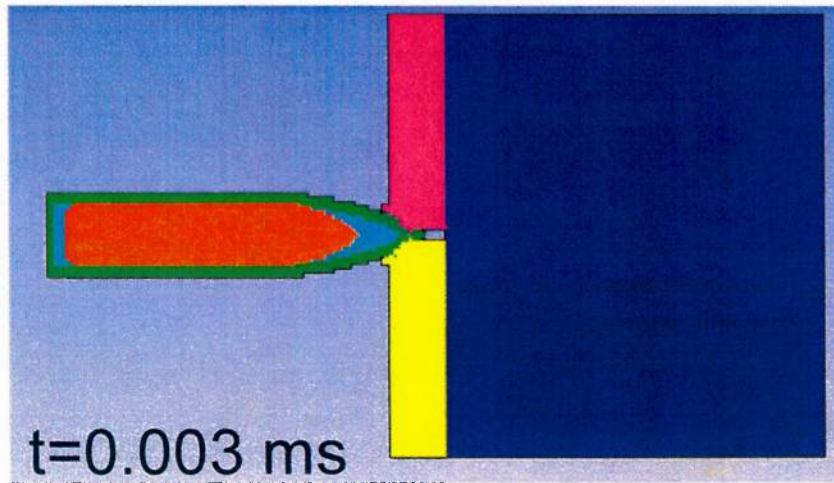


DEPTH OF PENETRATION $V_0 = 950$ m/s $t_c = 5.08$ mm particle size = 0.4, No Gap

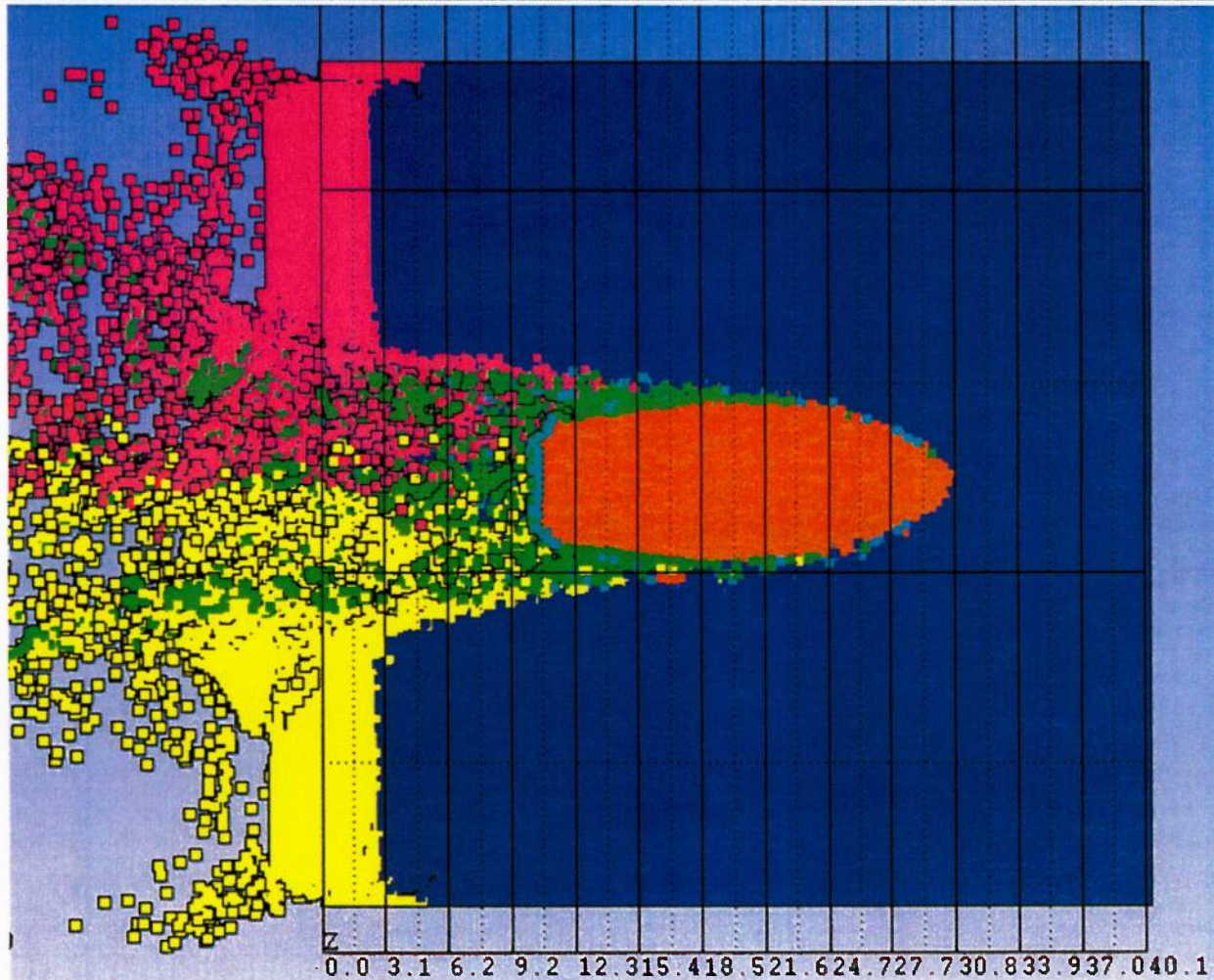


$$\text{DOP} = L - L_{np} = 40.08 - 27.12 = 12.96 \text{ mm}$$

**$V_o = 1000 \text{ m/s}$ $t_c = 5.08 \text{ mm}$ particle
size = 0.4, Gap = 1.2 mm**

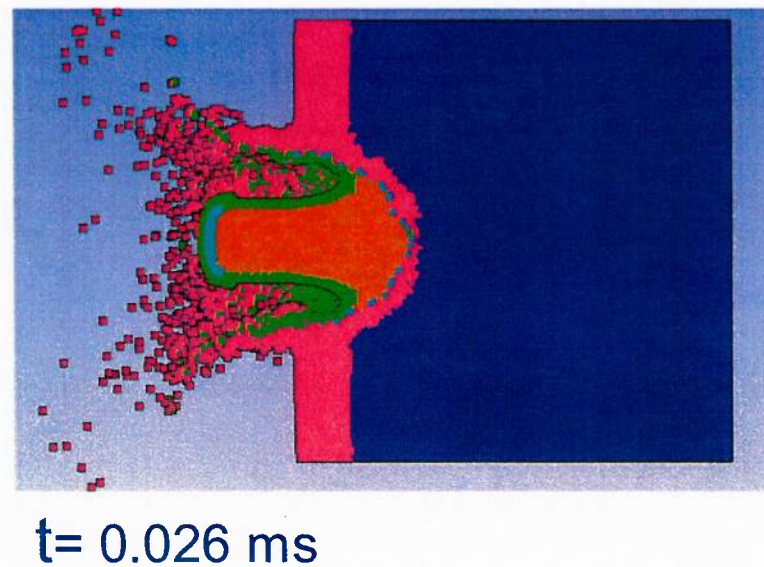
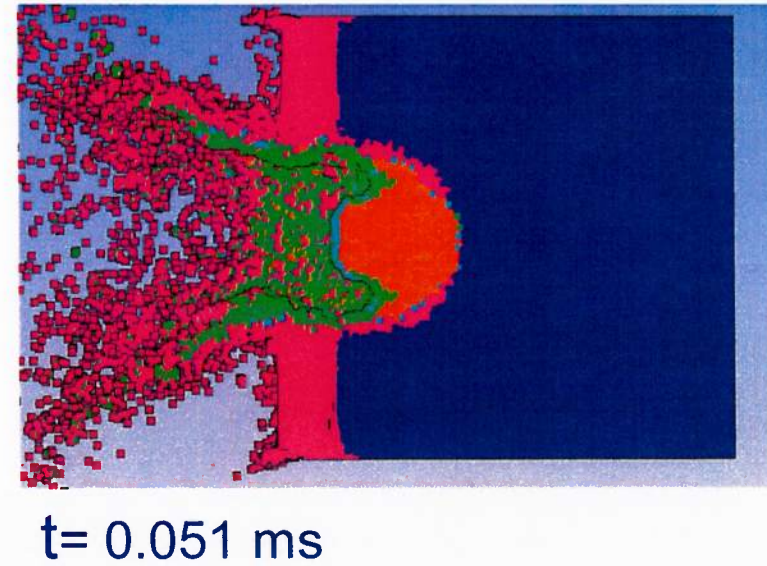
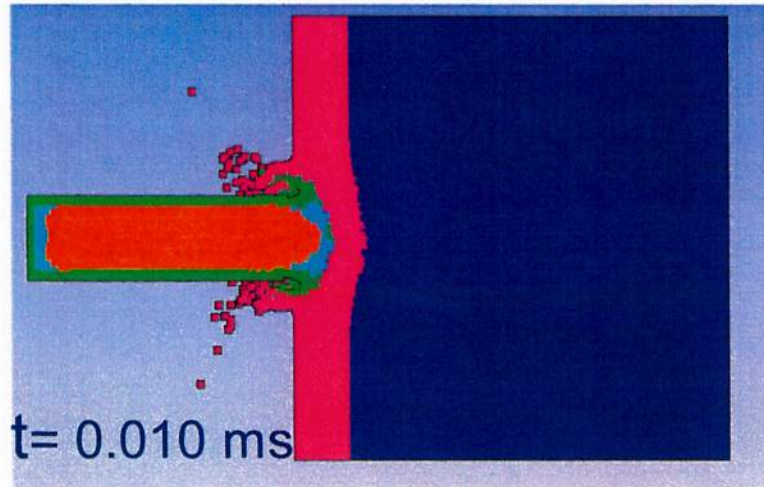


DEPTH OF PENETRATION $V_o = 1000$ m/s $t_c = 5.08$ mm particle size = 0.4, Gap = 1.2 mm

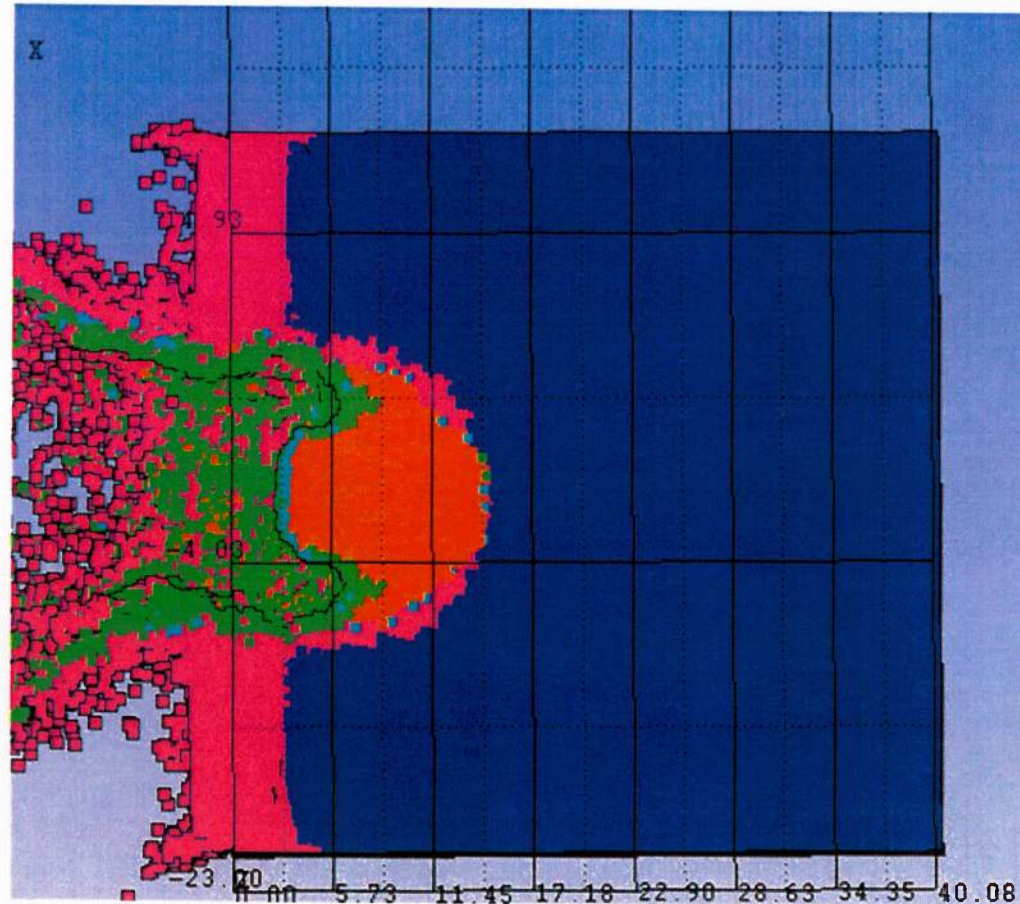


$$\text{DOP} = L - L_{np} = 40.08 - 9.28 = 30.28 \text{ mm}$$

$V_o = 1000 \text{ m/s}$ $t_c = 5.08 \text{ mm}$ particle
size = 0.4, No Gap



DEPTH OF PENETRATION $V_o = 1000$ m/s $t_c = 5.08$ mm particle size = 0.4, No Gap



$$\text{DOP} = L - L_{np} = 40.08 - 25.77 = 14.31 \text{ mm}$$

DEPTH OF PENETRATION



Velocity (m/s)	One Tile DOP (mm)	Gap DOP (mm)
700	10.02	16.40
750	8.59	18.70
850	10.00	24.05
900	11.13	20.04
950	12.96	28
1000	14.31	30.28