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MODELING AND SIMULATION, TESTING AND VALIDATION



INVESTIGATION OF STRESS AND FAILURE IN GRANULAR SOILS FOR LIGHTWEIGHT ROBOTIC VEHICLE APPLICATIONS

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Motivation

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- Gain deeper understanding of fundamental mechanics governing traction generation under small, lightweight vehicles.
- Improve modeling accuracy and predictive power.
- This will allow small robots to be more effective performers and operate more reliably.



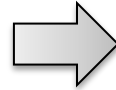
Methodology

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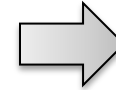
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**Soil
Characterization**



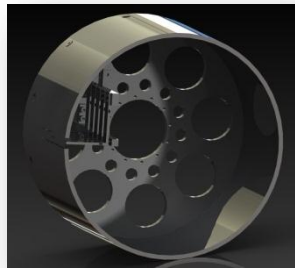
**Single Wheel
Experiments**



**Terramechanics
Modeling**

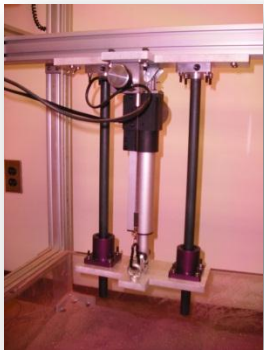
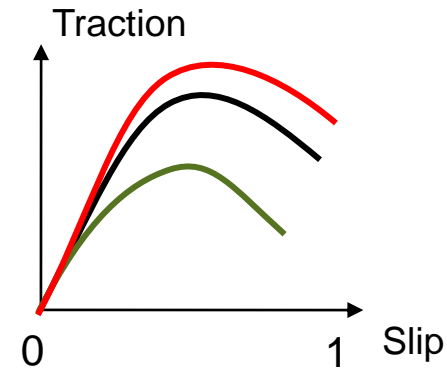


Direct Shear Tests

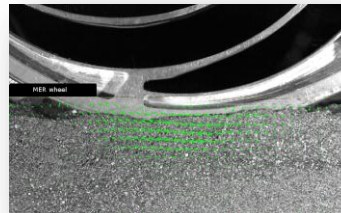
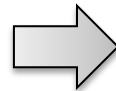


Radius = 13 cm
Width = 16 cm

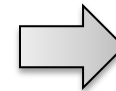
*Interfacial Stress
Measurement*



Penetration Tests



*Soil Motion
Measurement (PIV)*



Presentation Outline

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- State-of-the-art model for wheeled vehicles mobility.
- Soil characterization (i.e., how to obtain the parameters for the aforementioned model).
- Single wheel experimental methodologies
 - Particle Image Velocimetry
 - Force sensors
- Comparison between State-of-the-art modeling and measurements
- Conclusions and future work

Bekker-Wong Model

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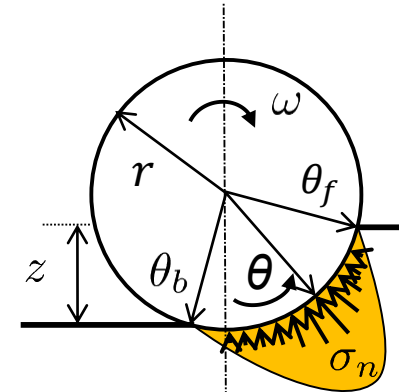
MODELING AND SIMULATION, TESTING AND VALIDATION

- Terramechanics models are based on:
 - **Bekker-Wong** equations for normal stress calculations

$$\sigma_n = \begin{cases} \sigma_1 = \left(\frac{k_c}{b} + k_\phi\right) r^n (\cos \theta - \cos \theta_f)^n \\ \sigma_2 = \left(\frac{k_c}{b} + k_\phi\right) r^n \left(\cos \left(\theta_f - \frac{\theta - \theta_b}{\theta_m - \theta_b} (\theta_f - \theta_m)\right) - \cos \theta_f\right)^n \end{cases}$$

$$\theta_m < \theta < \theta_f$$

$$\theta_b < \theta < \theta_m$$



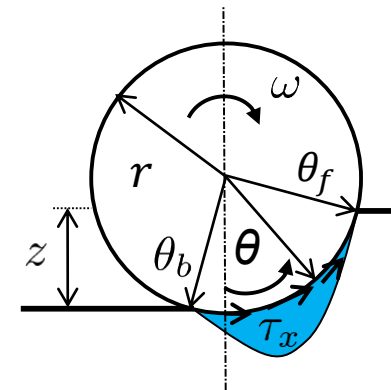
θ_m is the angle where normal stress reaches a peak

- **Janosi-Hanamoto** equation for tangential stress calculation

$$\tau_x(\theta) = \tau_{max} \left(1 - e^{\frac{-jx}{k_x}}\right)$$

$$\tau_{max} = c + \sigma_n(\theta) \tan \phi$$

Mohr-Coulomb criterion



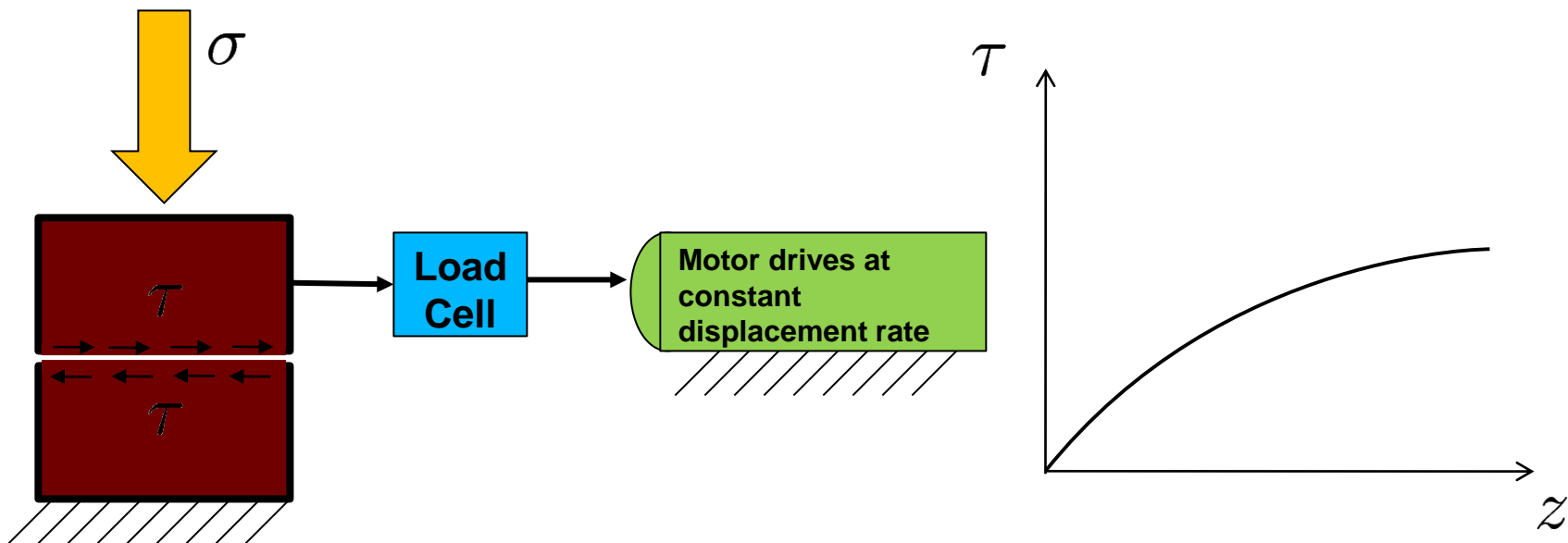
Soil Characterization

Direct Shear Test

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- Direct shear tests are used to characterize shearing properties of soils
- Direct shear tests are standard tests in the geotechnical practice



Direct Shear Test Results

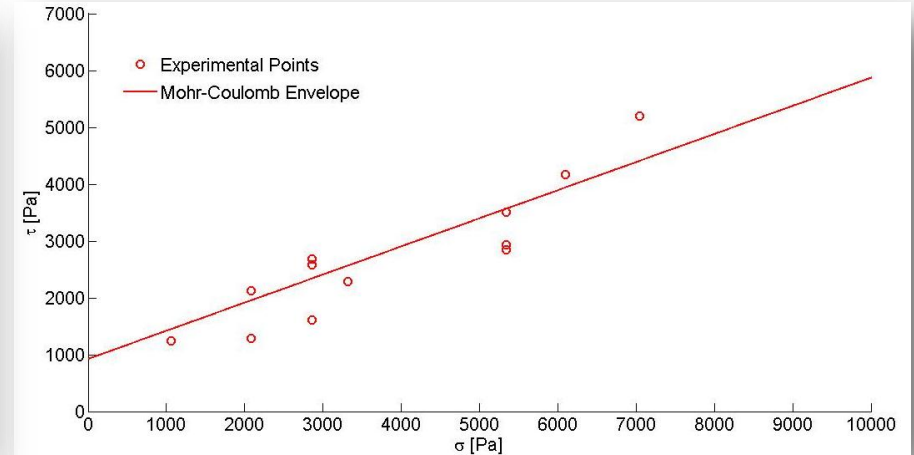
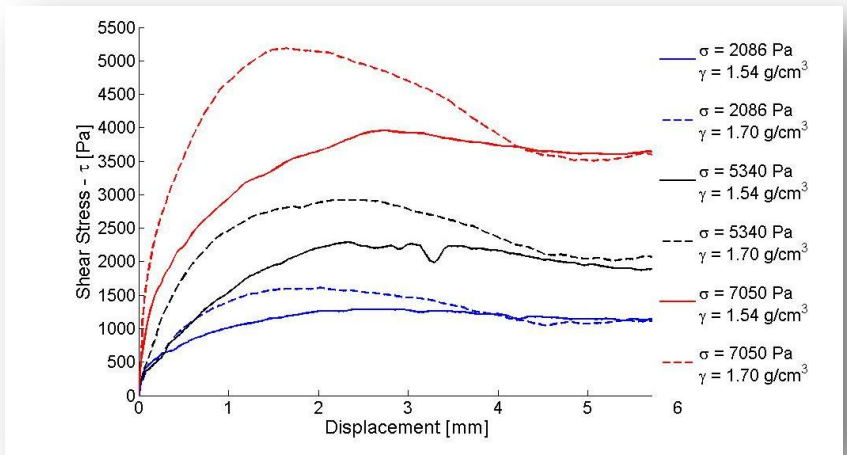


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- Direct shear tests provide shearing properties of the soil:

$$\left\{ \begin{array}{l} \tau_x(\theta) = \tau_{max} \left(1 - e^{\frac{-jx}{k_x}} \right) \leftarrow \text{Shear Modulus} \\ \tau_{max} = c + \sigma_n(\theta) \tan \phi \leftarrow \text{Cohesion} \\ \phantom{\tau_{max}} \leftarrow \text{Angle of Internal Friction} \end{array} \right.$$



$$\tau_x(\theta) = \tau_{max} \left(1 - e^{\frac{-jx}{k_x}} \right)$$

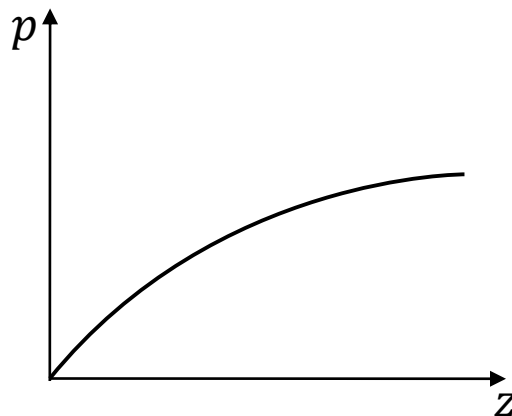
$$\tau = c + \sigma \tan(\phi)$$

Soil Characterization Penetration Tests

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- Plate penetration tests were performed to characterize soil response to normal loading
- According to Bekker-Wong theory, plates dimension have to be comparable with the wheel contact patch under investigation.

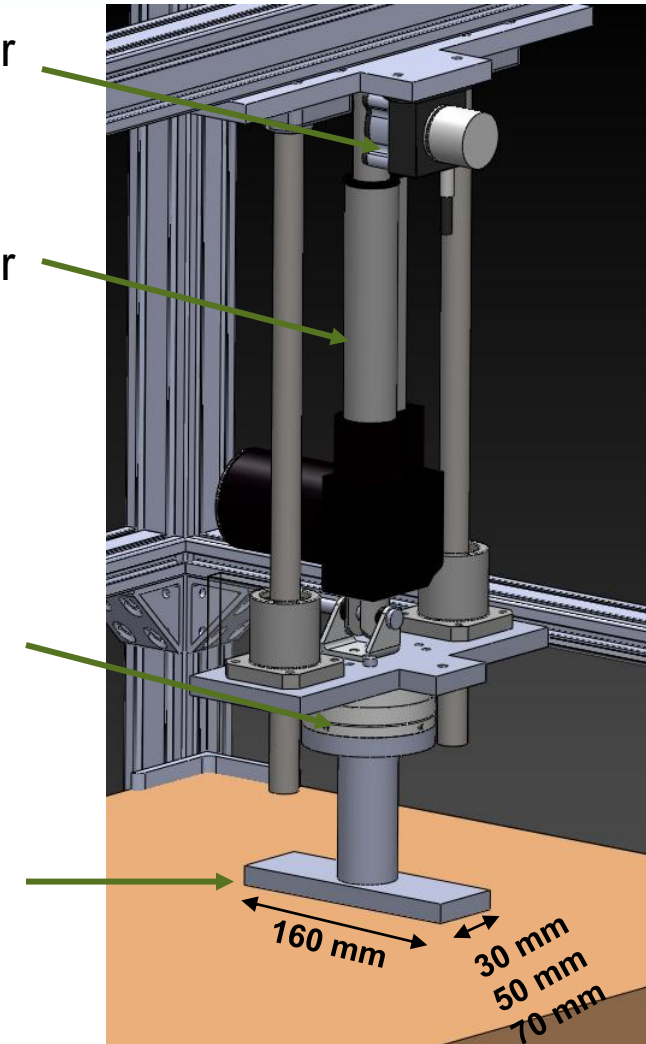


Encoder

Actuator

Force
Sensor

Penetration
Plate



Penetration Tests

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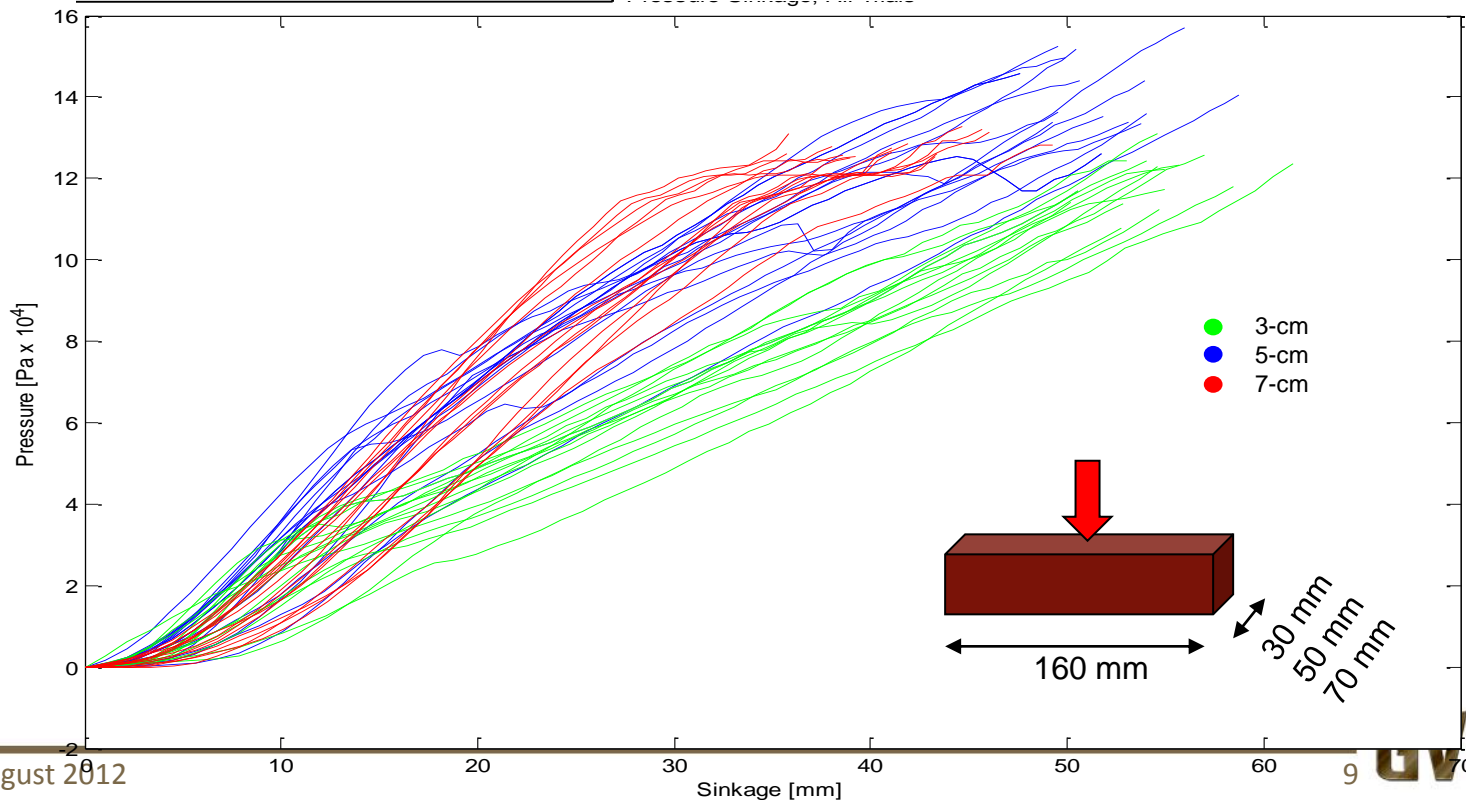
- Penetration tests provide information about soil normal loading response

Cohesion dependent soil coefficient

Frictional dependent soil coefficient

$$\sigma_n = \left(\frac{k_c}{b} + k_\phi \right) z^n$$

Plate width b Sinkage exponent n



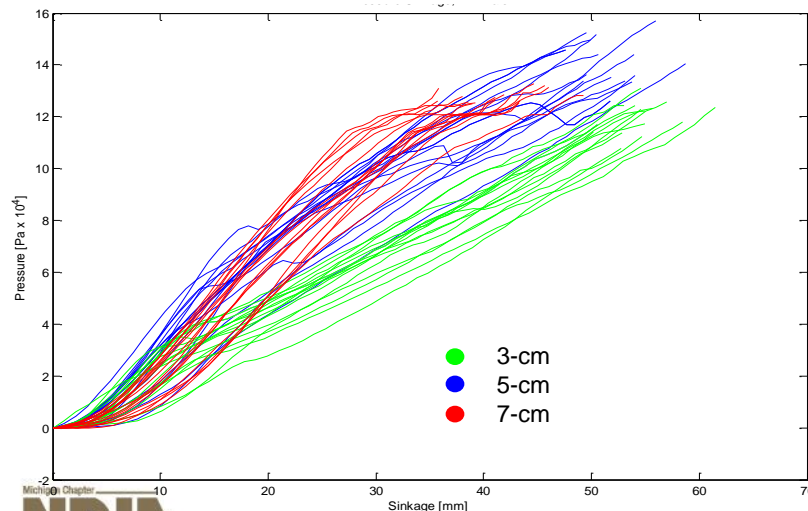
Penetration Tests Variability

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- Penetration tests showed how variable, even under carefully controlled laboratory conditions, soil response can be.
- An initial attempt to statistically characterize soil response was made but further investigations are under way.
- Aspect ratio influence was not investigated because plate width is constrained by wheel geometry (wheel width is fixed while contact patch length depends on sinkage).
- Using the (deterministic) approach suggested by Wong*, two sets of parameters were calculated. **57** is obtained truncating the data at 50kPa.



Set	n	k_c [kN/m ⁿ⁺¹]	k_ϕ [kN/m ⁿ⁺²]
357	0.99	-55	4584
57	1.4	846	6708

Single Wheel Testbed

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Draw-wire encoder for sinkage measurement

A motor drives the horizontal carriage.

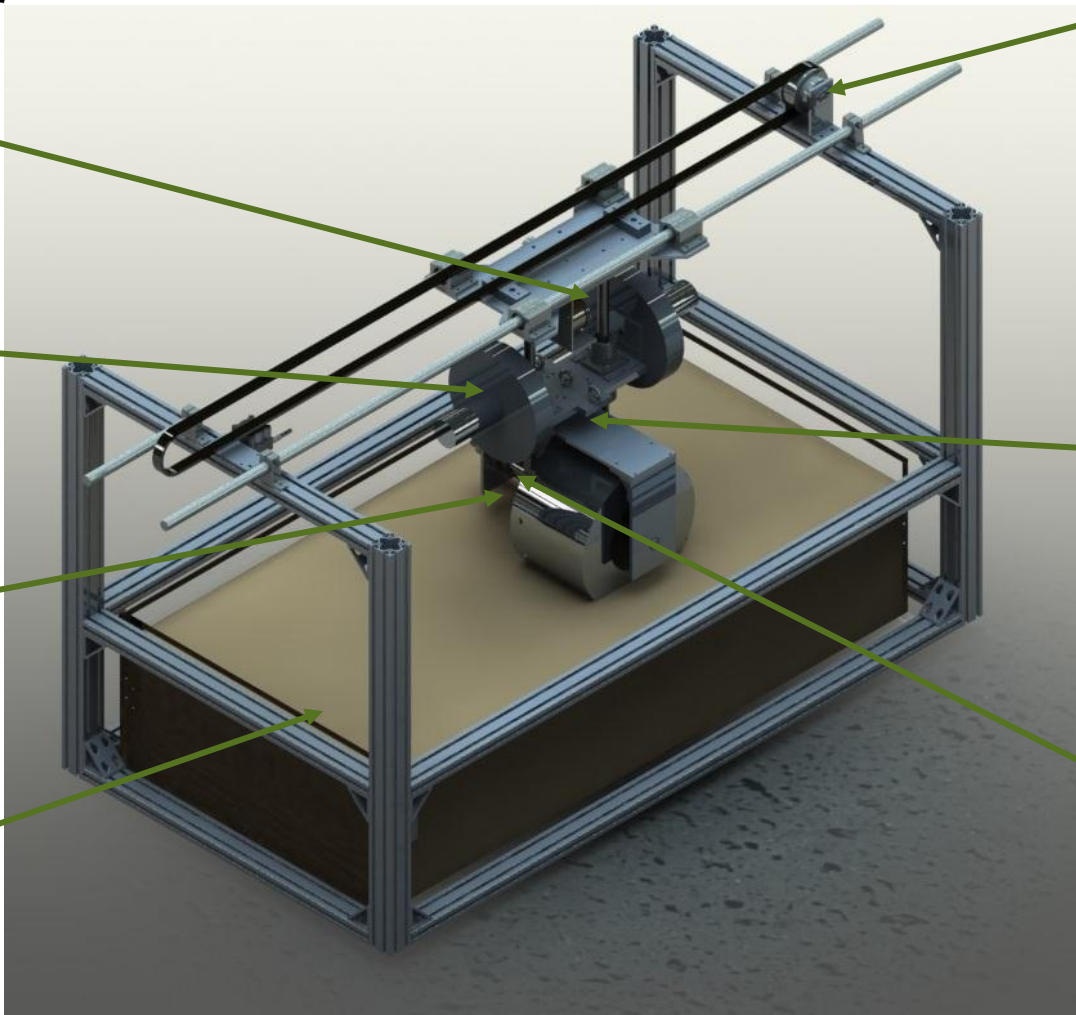
Vertical load control

6-axis F/T Sensor

A motor drives the wheel

Torque sensor

Mars Soil Simulant*



PIV Setup

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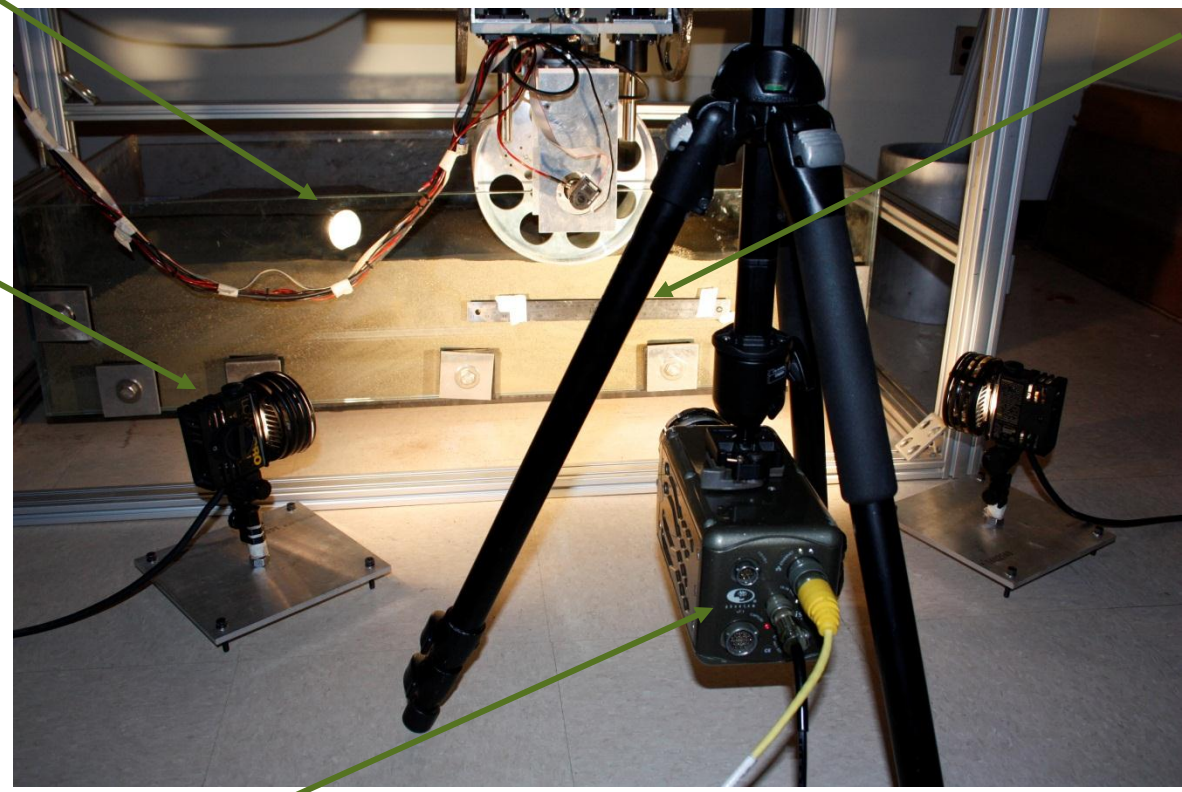
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Tempered 1" Thick Glass

500W Spot Lights

Ruler, needed to calibrate pixel/mm ratio



Phantom 7.1 High Speed Camera

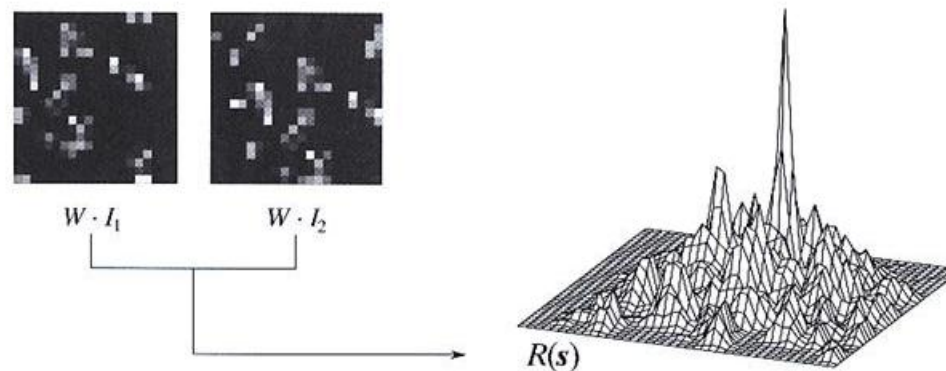
PIV Description

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- PIV is a methodology for extracting instantaneous velocity fields from a series of images
- Probable displacement is determined by using the cross correlation function

$$R_u(x, y) = \sum_{i=-K}^K \sum_{j=-L}^L I_1(i, j) I_2(i + x, j + y)$$

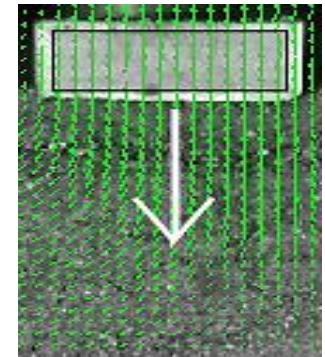
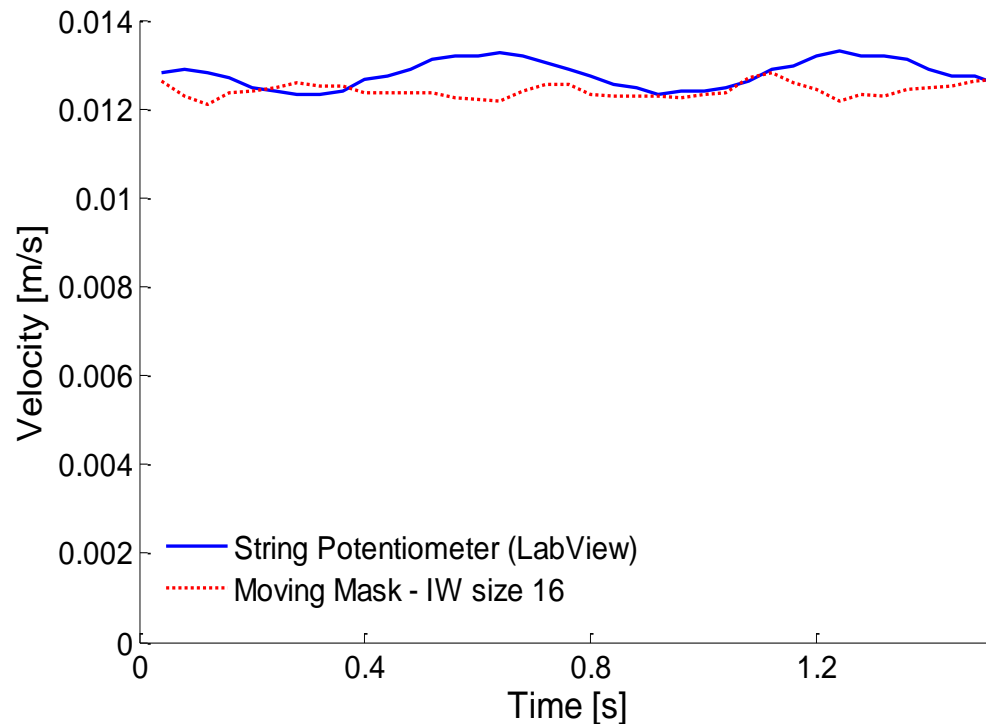


PIV Validation

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- Since a ground truth for soil motion was not available, the velocity of a plate (precisely measured through a draw-wire encoder) was compared with PIV measurements.



PIV Results

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- Wong Experiments
 - Average Ground Pressure = 30-90 kPa

- MIT Experiments
 - Average Ground Pressure = 7-13 kPa

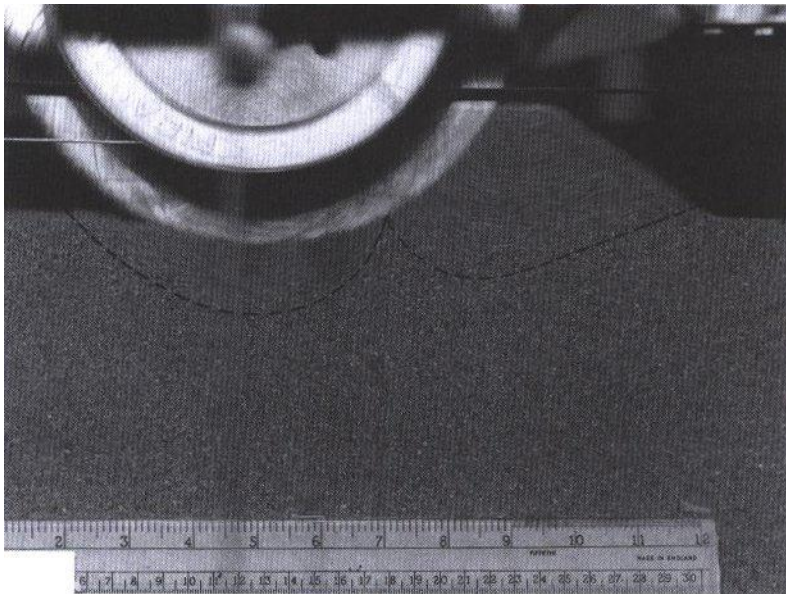
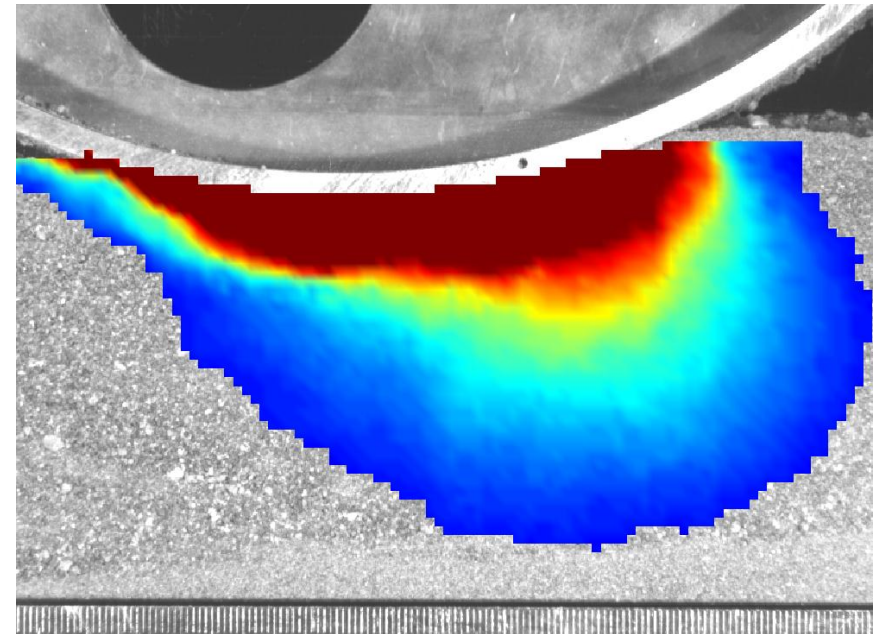


Figure 1.11: Soil flow patterns under a driven rigid wheel in sand

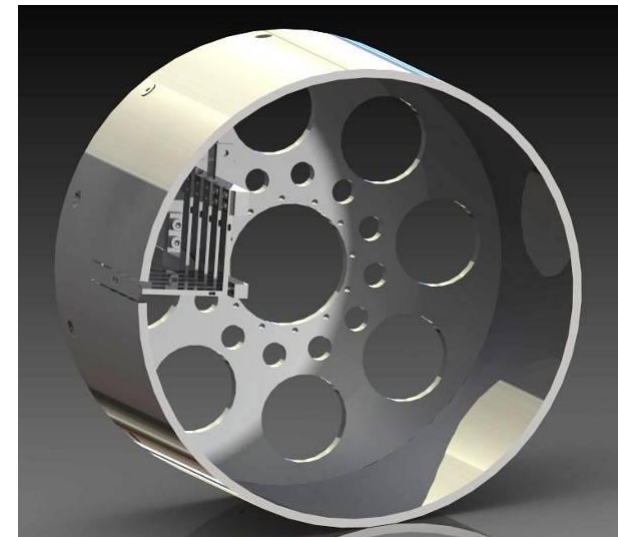
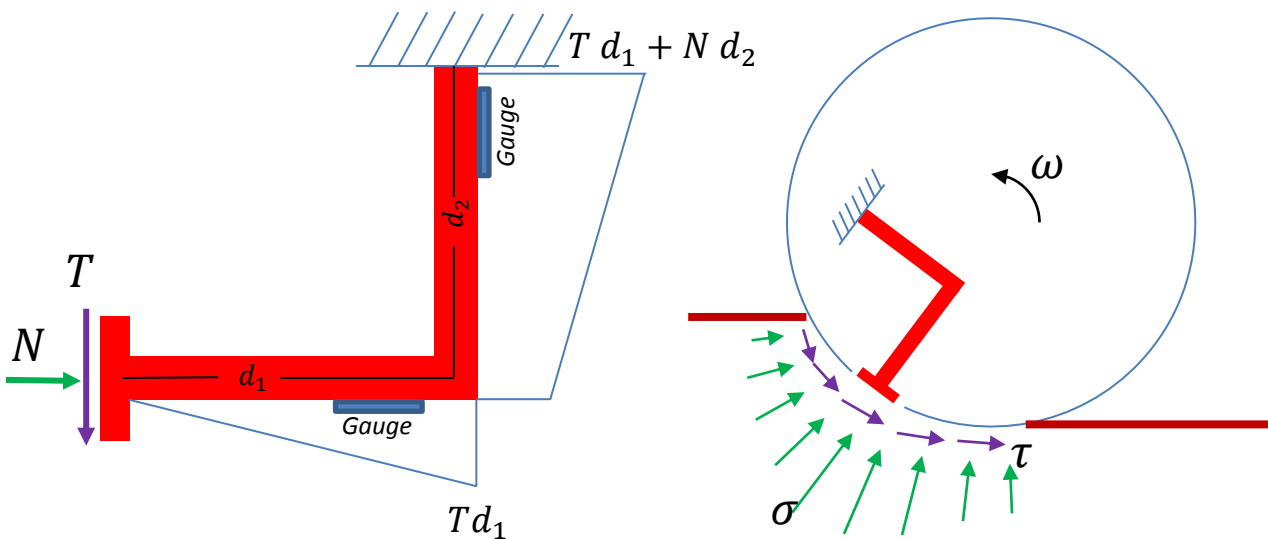


Force Sensors

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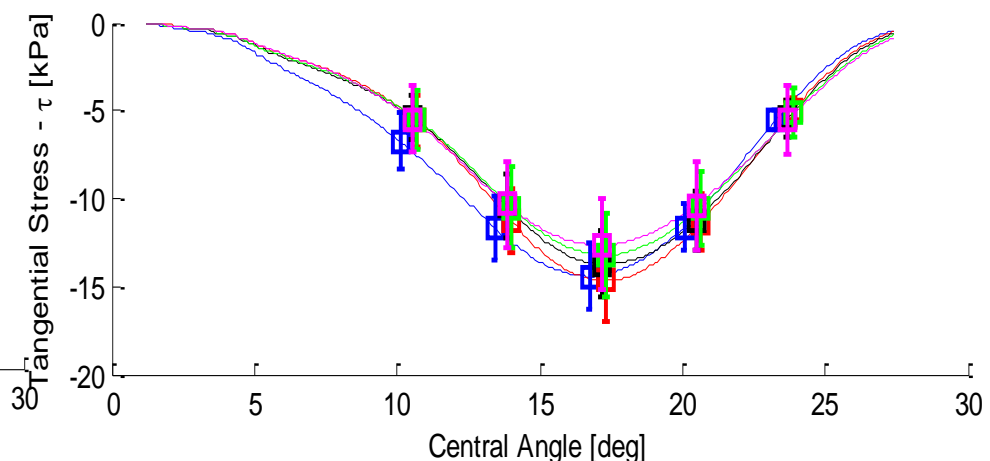
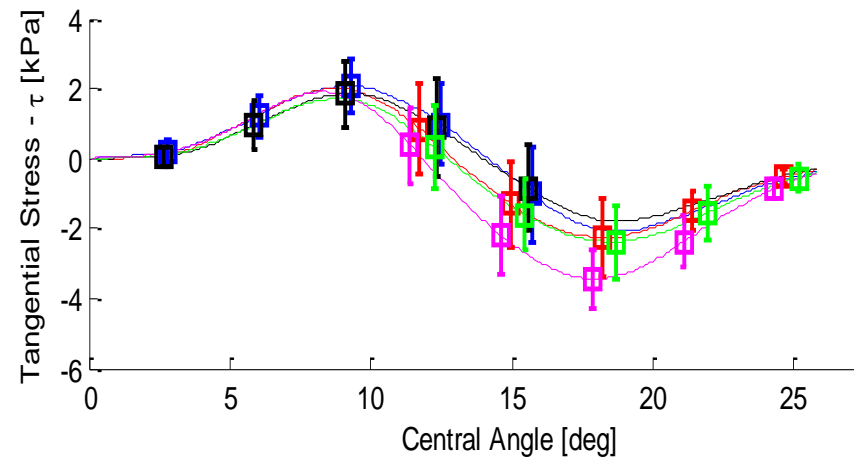
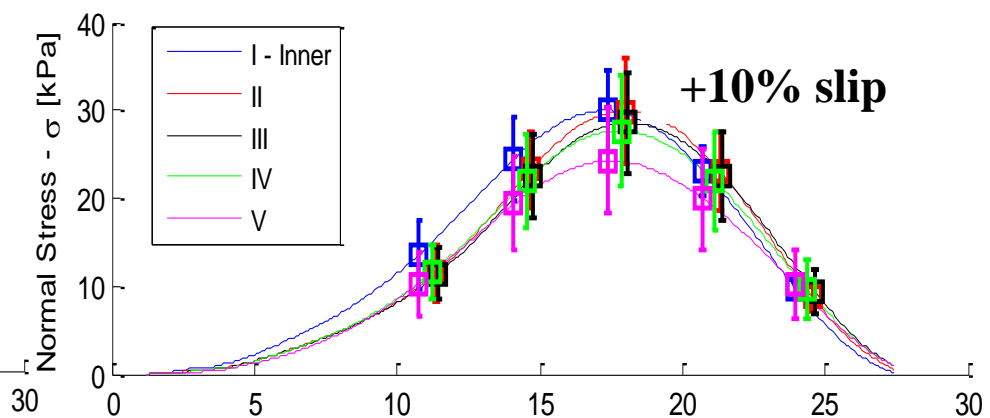
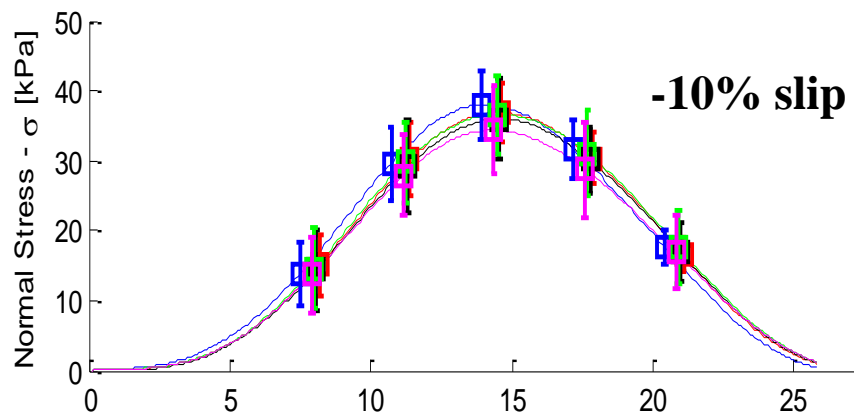
- Flexing beam instrumented with strain gauges
- Tangential and Normal forces applied to the tip can be reconstructed from gauges reading



Stress Profile at Wheel-Soil Interface for Low Slip



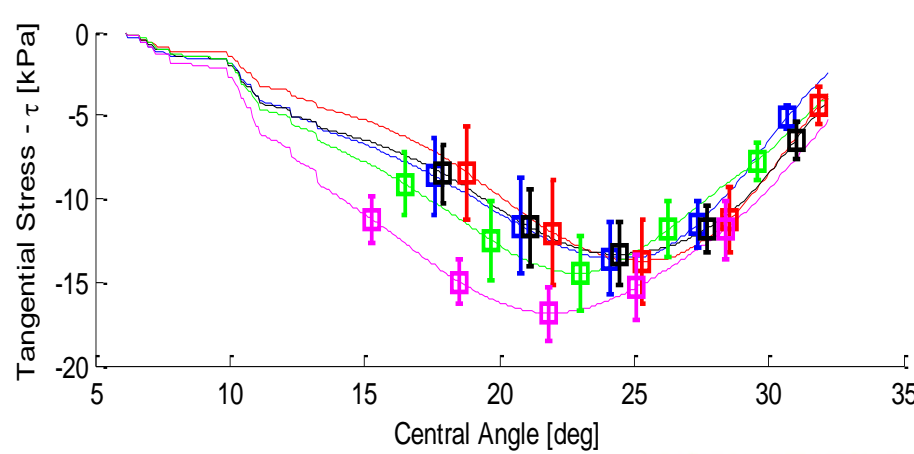
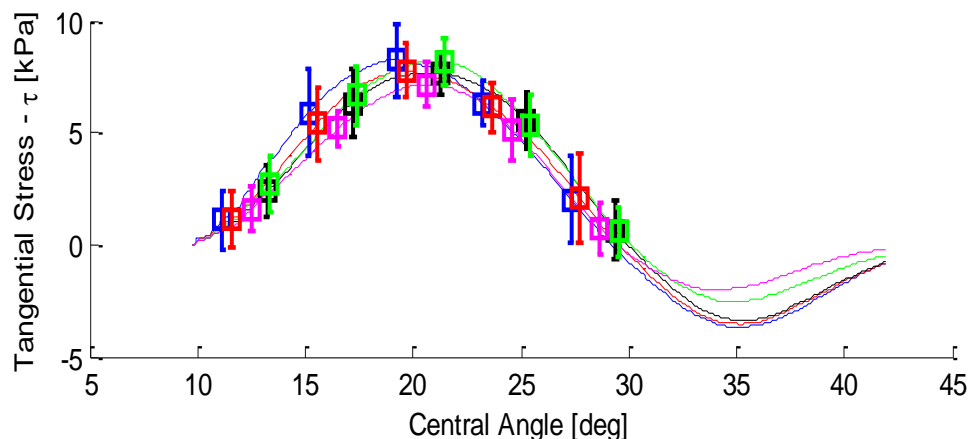
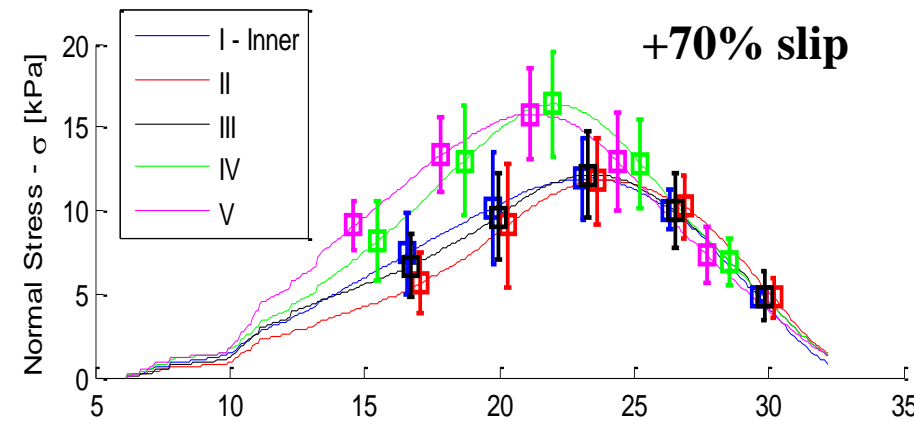
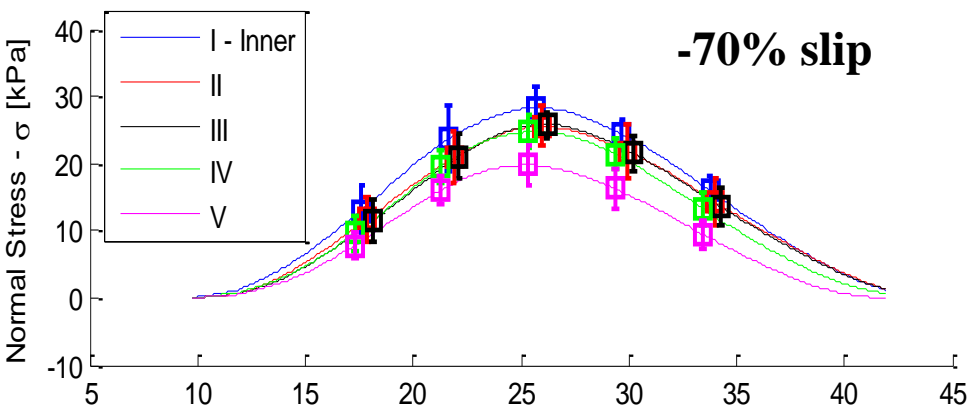
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Stress Profile at Wheel-Soil Interface for High Slip

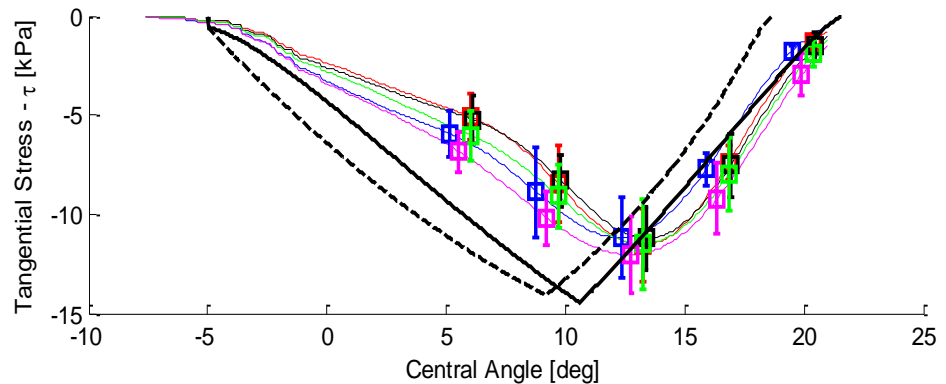
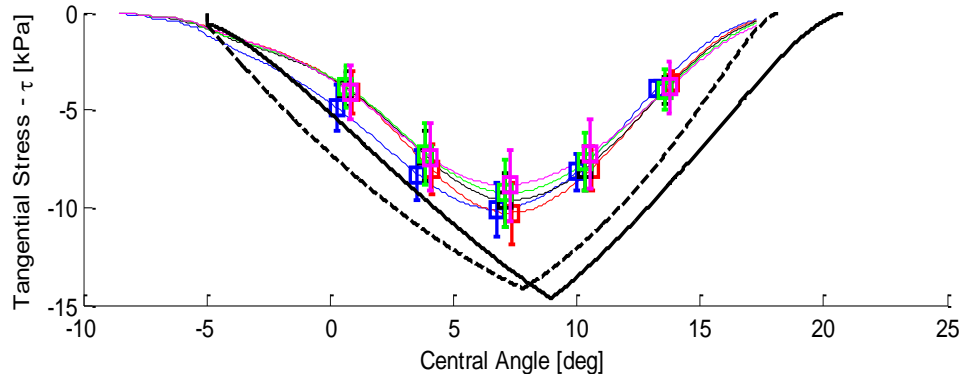
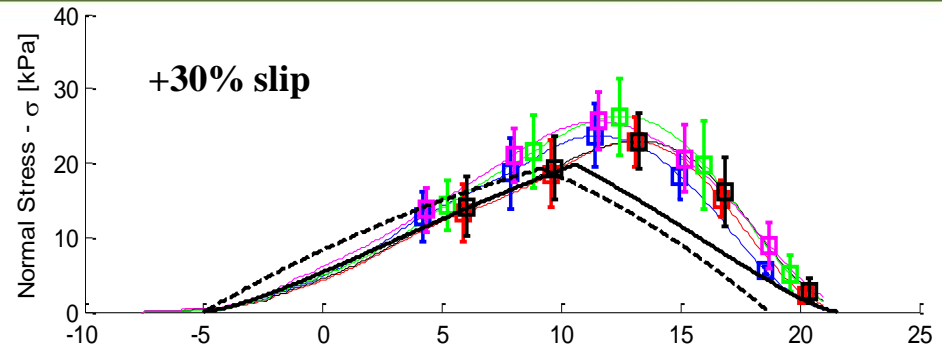
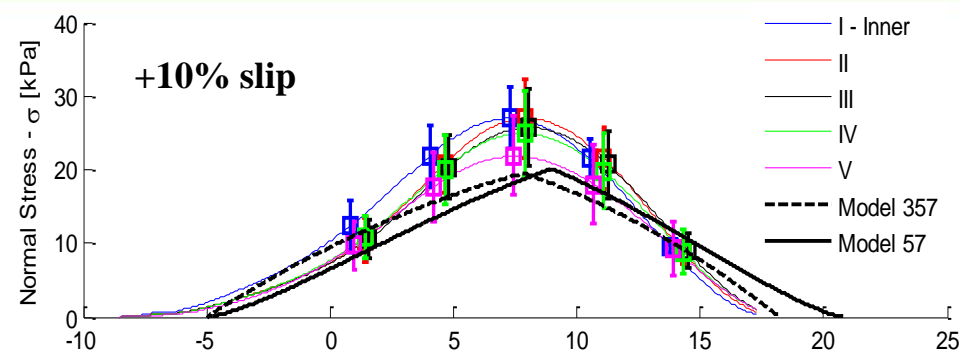
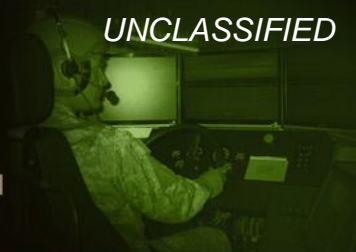
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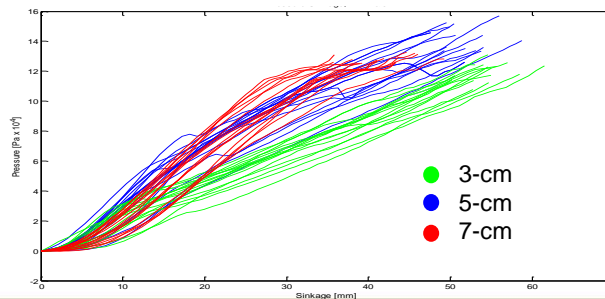


Comparison Between Bekker-Wong Model and Measured Stress

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Set	n	k_c [kN/m ⁿ⁺¹]	k_ϕ [kN/m ⁿ⁺²]
357	0.99	-55	4584
57	1.4	846	6708



Conclusions and Future Work

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- PIV shows phenomena that do not completely agree with assumptions behind classical models
 - Only one failure envelope develops (not two)
 - Soil failure is periodic
 - Soil is always attached to the wheel surface
- However, stress measurements show that Bekker-Wong model is still able to capture main trends (for low slip).
- Further efforts will be dedicated to characterize variability in soil response and how models are affected by it.
- The underlying complex mapping between soil displacement and stress (i.e., constitutive law) will be investigated in order to improve modeling capabilities.