



Accelerated Testing and Preventive Maintenance in Acquisition, Maintenance and Operation of Vehicle Systems using Time-Dependent Reliability / Durability Principles

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Report Documentation Page

Form Approved
OMB No. 0704-0188

Public reporting burden for the collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to a penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number.

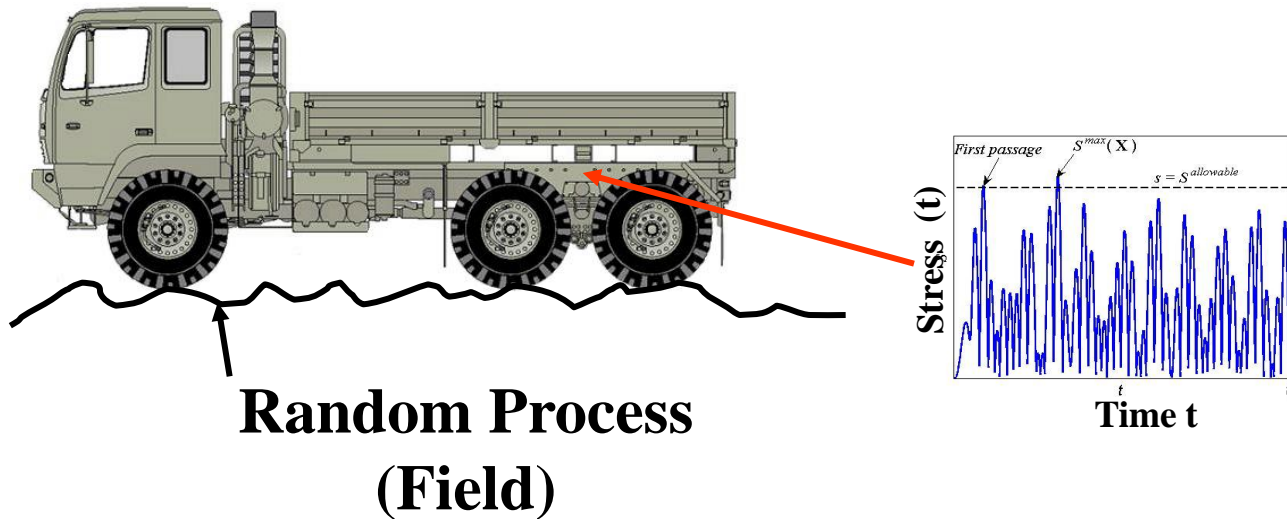
1. REPORT DATE 24 MAY 2011		2. REPORT TYPE Briefing Charts		3. DATES COVERED 24-05-2011 to 24-05-2011	
4. TITLE AND SUBTITLE ACCELERATED TESTING AND PREVENTIVE MAINTENANCE IN ACQUISITION, MAINTENANCE AND OPERATION OF VEHICLE SYSTEMS USING TIME-DEPENDENT RELIABILITY/DURABILITY PRINCIPLES				5a. CONTRACT NUMBER	
				5b. GRANT NUMBER	
				5c. PROGRAM ELEMENT NUMBER	
6. AUTHOR(S) Amandeep Singh; Igor Baseski; Zissimos Mourelatos; Jing Li				5d. PROJECT NUMBER	
				5e. TASK NUMBER	
				5f. WORK UNIT NUMBER	
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) Oakland University, Mechanical Engineering Department, Rochester, MI, 48309				8. PERFORMING ORGANIZATION REPORT NUMBER ; #22500	
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) U.S. Army TARDEC, 6501 E.11 Mile Rd, Warren, MI, 48397-5000				10. SPONSOR/MONITOR'S ACRONYM(S) TARDEC	
				11. SPONSOR/MONITOR'S REPORT NUMBER(S) #22500	
12. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release; distribution unlimited					
13. SUPPLEMENTARY NOTES Automotive Research Center (ARC) Conference briefing					
14. ABSTRACT N/A					
15. SUBJECT TERMS					
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT	18. NUMBER OF PAGES	19a. NAME OF RESPONSIBLE PERSON
a. REPORT unclassified	b. ABSTRACT unclassified	c. THIS PAGE unclassified			



Army Needs in Reliability, Maintenance and Logistics



- Reduce operations and **maintenance** costs
- Increase effectiveness of **fleet logistics**
- Control **lifecycle cost** and also use it in design and procurement
- Improve **availability**; **schedule maintenance**
- Use both analytical and experimental / field data to estimate reliability



Input
Random
Process



Output
Random
Process

Random Process leads to Time-Dependent Reliability



Research Statement



Develop methodologies to obtain a preventive maintenance schedule and to assess and improve the reliability / durability of vehicle systems using

- **Experimental (field) data**
- **“Expert” opinion**

Previously and currently at TARDEC

- **Predictive tools (physics-of-failure data)**

Current research



Part 1:

**Optimal preventive maintenance schedule
using time-dependent reliability and lifecycle cost**

Part 2:

**Accelerated testing method based on
importance sampling using few tests which run for
only a short time**



Part 1: Optimal Preventive Maintenance Schedule



What is Reliability?

Cumulative Probability of Failure



Reliability at time t is the probability that the system **has not failed before time t.**

$$F_T^c(t_L) = P(\exists t \in [0, t_L], \text{ such that } g(\mathbf{X}(t), t) \leq 0)$$

Cumulative Prob. of Failure

$$F_T^i(t_L) = P(g(\mathbf{X}(t_L), t_L) \leq 0)$$

Instantaneous Prob. of Failure

Calculation Methods for $F_T^c(t)$

- Maximum Response Method
- Niching GA & Lazy Learning Local Metamodeling
- MCS / Importance sampling

} **Analytical**

$$F_T^c(t) = 1 - \exp\left[-\int_0^t \lambda(t) dt\right]$$

} **Simulation-based**

Lifecycle Cost = Production Cost

+ Inspection Cost

+ Expected Variable Cost

Quality

Time-Dependent System Reliability

$$C_L(\mathbf{d}, \mathbf{X}, t_f, r) = C_P(\mathbf{d}, \mathbf{X}) + C_I(\mathbf{d}, \mathbf{X}, t_0) + C_V^E(\mathbf{d}, \mathbf{X}, t_f, r)$$

Lifecycle Cost Production Cost Inspection Cost Expected Variable Cost

$$C_V^E(\mathbf{d}, \mathbf{X}, t_f, r) = \int_0^{t_f} c_F(t) e^{-rt} f_T^c(t) dt$$

Final time t_f Interest rate r
 Cost of failure at time t $c_F(t)$ PDF of time to failure time $f_T^c(t)$

$$F_T^c(t_L) = P(\exists t \in [0, t_L], \text{ such that } g(\mathbf{X}(t), t) \leq 0)$$

Estimation of Time for Preventive Maintenance

$$\max_{\mathbf{d}, \mu_{\mathbf{X}}, \sigma_{\mathbf{X}}, t_M} t_M$$

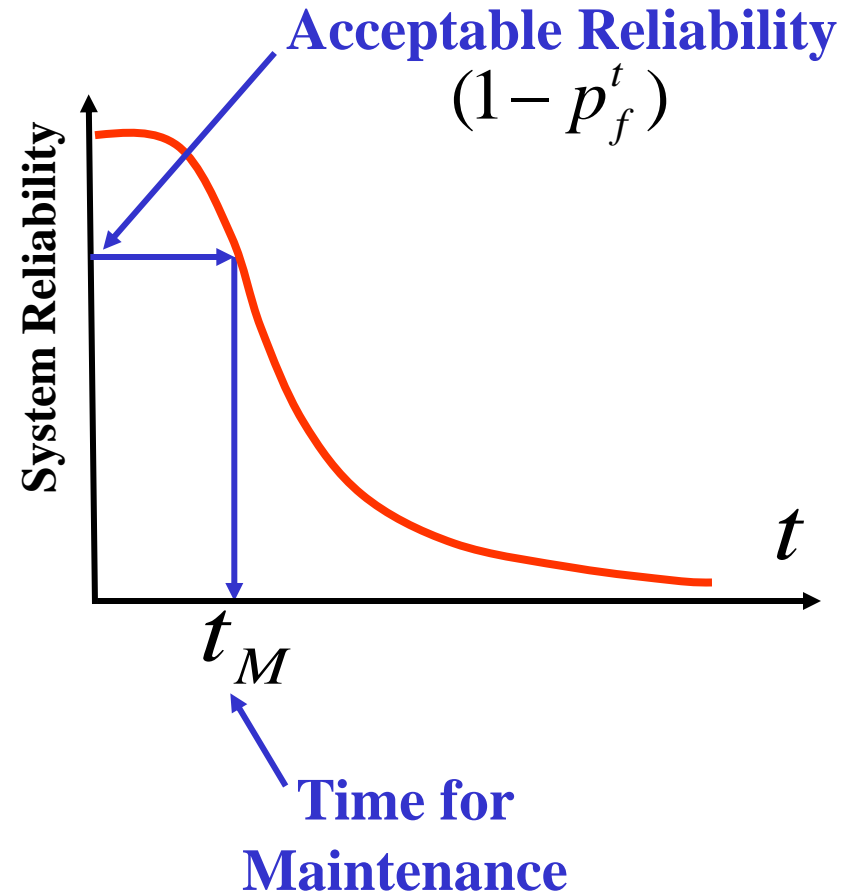
$$\text{s. t. } C_L(\mathbf{d}, \mu_{\mathbf{X}}, \sigma_{\mathbf{X}}, t_M, r) \leq C_L^t$$

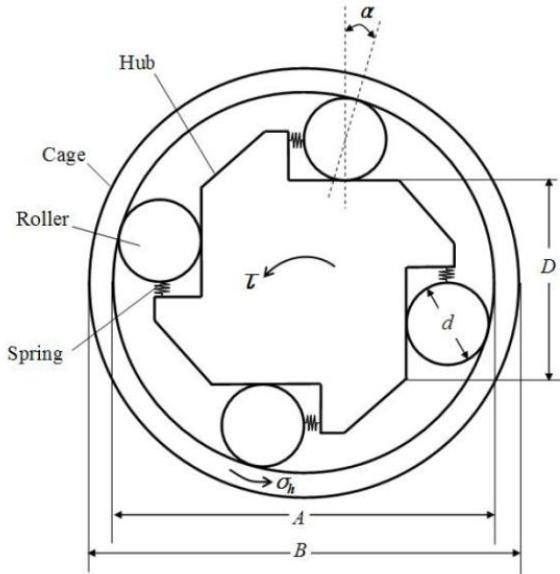
$$F_T^c(\mathbf{d}, \mathbf{X}, t_M) \leq 1 - R^t(t_M)$$

$$\mathbf{d}_L \leq \mathbf{d} \leq \mathbf{d}_U$$

$$\mu_{\mathbf{X}_L} \leq \mu_{\mathbf{X}} \leq \mu_{\mathbf{X}_U}$$

$$\sigma_{\mathbf{X}_L} \leq \sigma_{\mathbf{X}} \leq \sigma_{\mathbf{X}_U}$$





Constraints:

→ **Contact angle** $\alpha = 0.11 \pm 0.06$ rad

→ **Torque** $\tau \geq 3000$ Nm

→ **Hoop stress** $\sigma_h \leq 400$ MPa

Random Variables: D, d, A

Due to degradation:

$$\mathbf{D} \rightarrow \mathbf{D}(1 - kt)$$

$$\mathbf{d} \rightarrow \mathbf{d}(1 - kt)$$

$$\mathbf{A} \rightarrow \mathbf{A}(1 + kt)$$

with: $k = 2.5E - 04$ mm/year

$$g_1(D, d, A) = 0.05 - \cos^{-1}\left(\frac{D-d}{A-d}\right) \leq 0$$

$$g_2(D, d, A) = \cos^{-1}\left(\frac{D-d}{A-d}\right) - 0.17 \leq 0$$

$$g_3(D, d, A) = 3000 - NL \left(\frac{\sigma_c}{c_1}\right)^2 \frac{D^2 d}{4(D+d)} \sqrt{1 - S^2} \leq 0$$

$$g_4(D, d, A) = \frac{N}{2\pi} \left(\frac{\sigma_c}{c_1}\right)^2 \left(\frac{Dd}{(D+d)}\right) \frac{S}{A} \left(\frac{B^2 + A^2}{B^2 - A^2}\right) - 400E06 \leq 0$$

$$C_L = C_P + C_I + C_V^E$$

where:

$$C_P = \left(3.5 + \frac{0.75}{3\sigma_D} \right) + \left(3.0 + \frac{0.65}{3\sigma_d} \right) + \left(0.5 + \frac{0.88}{3\sigma_A} \right)$$

$$C_I = 20F_T^i(\mathbf{X}, t_0)$$

Scrap cost/unit

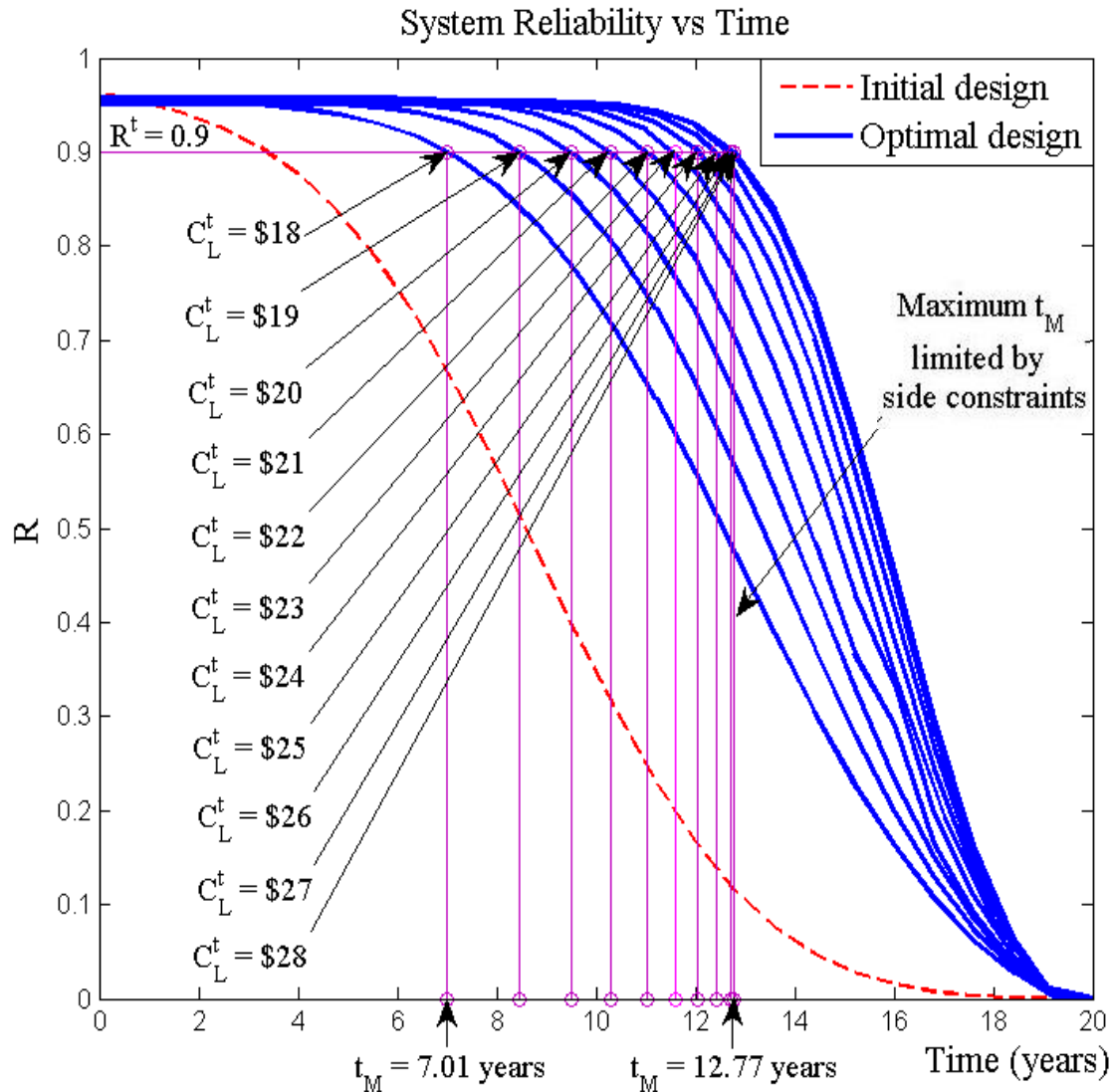
$$C_V^E = \int_0^{t_f} 20e^{-rt} f_T^c(t) dt$$

Failure cost/unit (warranty cost)

$$t_f = 10 \text{ years}$$

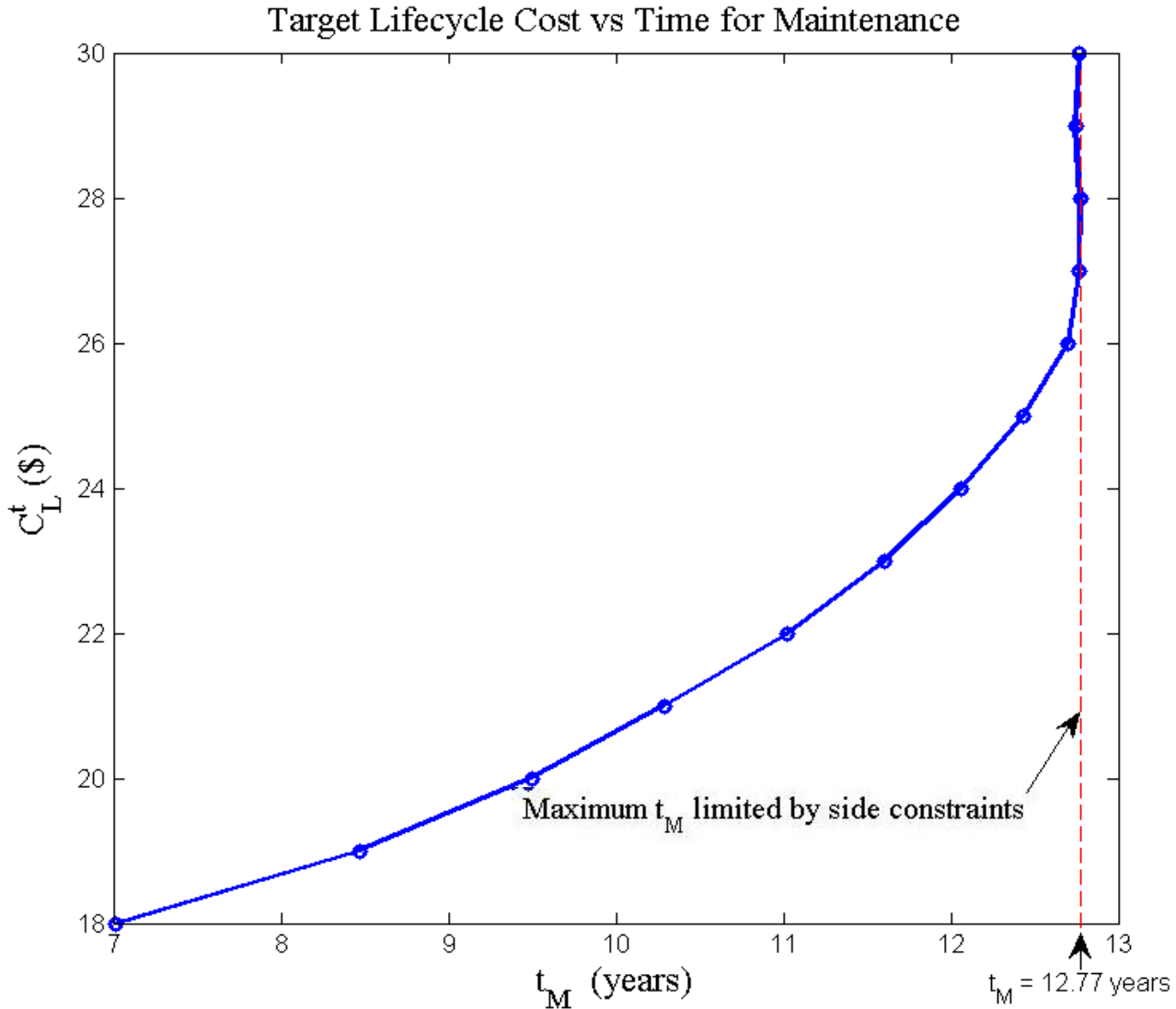
$$r = 3\%$$

Roller Clutch: Reliability vs Time-to-Maintenance





Roller Clutch: Pareto Optimality between Time-to-Maintenance and Cost





Roller Clutch: Pareto Optimality between Time-to-Maintenance and Cost



Design Variables:

$$\boldsymbol{\mu}_X = \{\mu_D, \mu_d, \mu_A\} \quad \boldsymbol{\sigma}_X = \{\sigma_D, \sigma_d, \sigma_A\}$$

Side Constraints:

$$55.0973 \leq \mu_D \leq 55.4973 \quad 22.66 \leq \mu_D \leq 23.06 \quad 101.49 \leq \mu_A \leq 101.89$$

$$0.04 \leq \sigma_D \leq 0.08 \quad 0.03 \leq \sigma_d \leq 0.1 \quad 0.07 \leq \sigma_A \leq 0.113$$

C_L^t	18	19	20	21	22	23	24	25	26	27	28
μ_D	55.4946	55.4973	55.4973	55.3822	55.4973	55.4973	55.4973	55.4973	55.4973	55.4973	55.4973
μ_d	22.7562	22.7735	22.7867	22.8535	22.8071	22.8146	22.8208	22.8259	22.8296	22.8315	22.8316
μ_A	101.49	101.49	101.49	101.49	101.49	101.49	101.49	101.49	101.49	101.49	101.49
σ_D	0.08	0.08	0.0771	0.0693	0.0661	0.0593	0.054	0.0496	0.0423	0.04	0.04
σ_d	0.0639	0.0543	0.0481	0.0449	0.0407	0.0368	0.0334	0.0306	0.03	0.03	0.03
σ_A	0.1107	0.0946	0.084	0.0763	0.0701	0.07	0.07	0.07	0.07	0.07	0.07

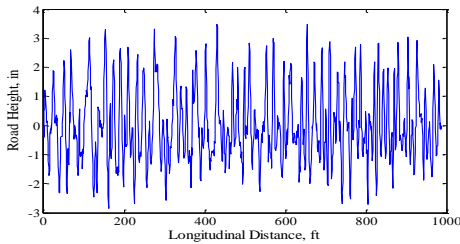


Part 2: Accelerated Testing using Importance Sampling

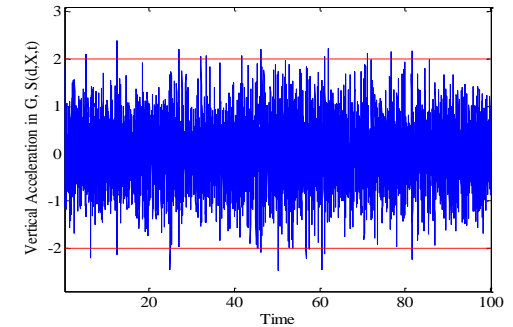
Random Variables



Vertical Accel. (G)



Terrain



Vehicle speed : 20 mph; Mission distance : 100 miles

Simulation can be practically performed for a short-duration time

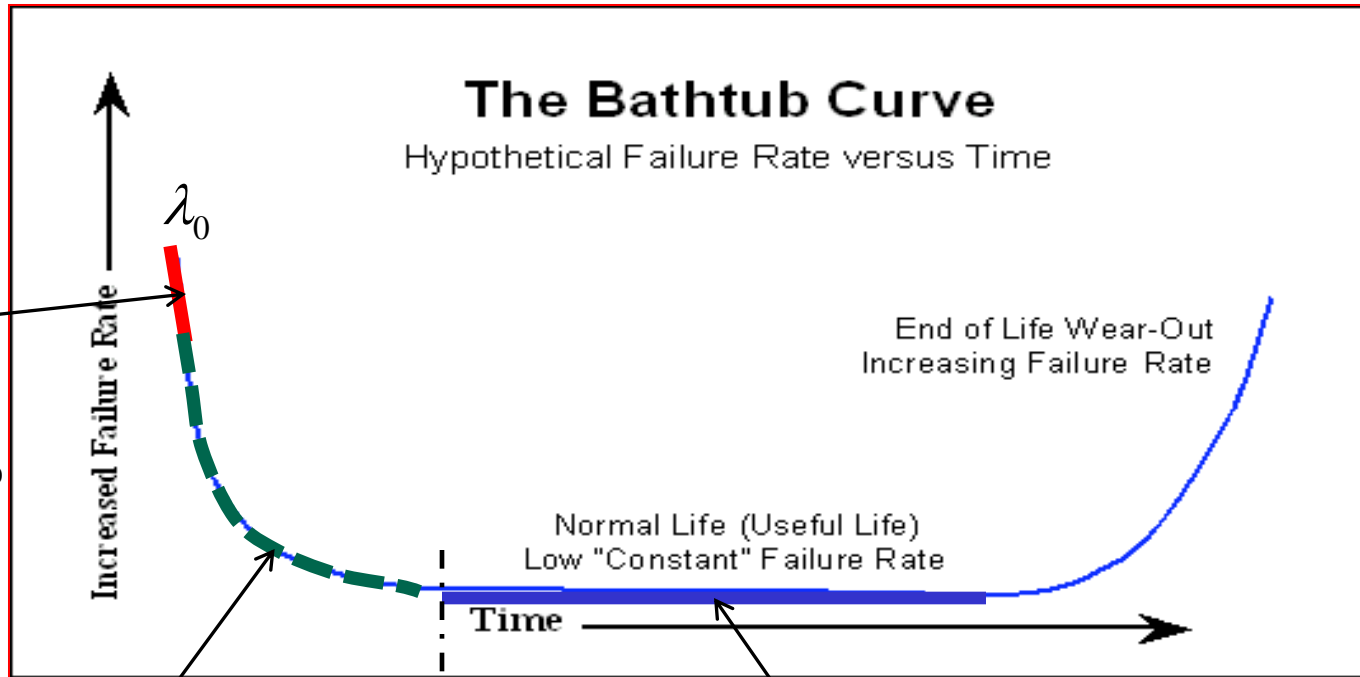


Our Approach



A novel MC-based method to calculate the time-dependent reliability (cumulative probability of failure) based on :

- **short-duration data and an exponential extrapolation using MCS or Importance Sampling (Infant Mortality)**
- **Poisson's assumption (Useful Life)**



MCS

$$b = -\frac{1}{\lambda_0} \left(\frac{d\hat{\lambda}}{dt} \right)_{t=0}$$

**Exponential
Extrapolation**

$$\hat{\lambda}(t) \approx \lambda_0 e^{-bt}$$

Poisson's Assumption

$$F_T^c(t) = \begin{cases} 1 - e^{-\int_0^t \hat{\lambda}(t) dt} & , t \in [0, t_{int}] \\ 1 - (1 - F_T^c(t_{int})) e^{-v_m(t-t_{int})} & , t \in [t_{int}, t_f] \end{cases}$$

$$F_T^c(t_{\min}, t) = 1 - (1 - F^i(t_{\min}))e^{-m_1}$$

where :

$$m_1 = E[N^+(t_{\min}, t)] = \int_{t_{\min}}^t v^+(t) dt = v_m(t - t_{\min})$$

Number of out-crossings

$$v^+(t) = \lim_{\Delta\tau \rightarrow 0, \Delta\tau > 0} \frac{P[g(\mathbf{d}, \mathbf{X}, t) > 0 \cap g(\mathbf{d}, \mathbf{X}, t + \Delta\tau) \leq 0]}{\Delta\tau}$$

Out-crossing rate

Constant design parameters:

$$m_s = 1000 \text{ kg}$$

$$m_u = 100 \text{ kg}$$

Vehicle speed = 20 mph

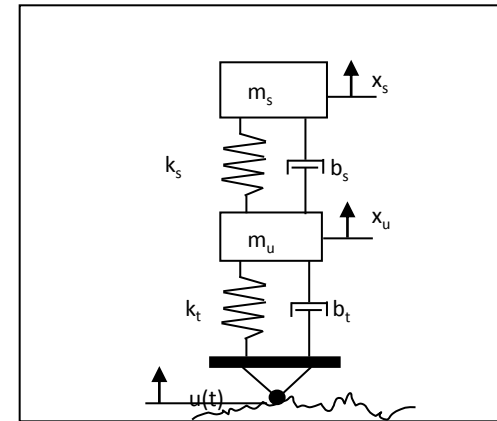
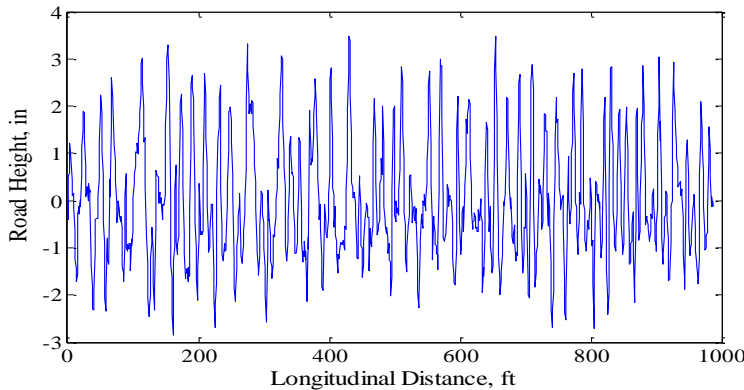


Random Input variables

Damping, $b_s \sim N(7000, 1400^2)$

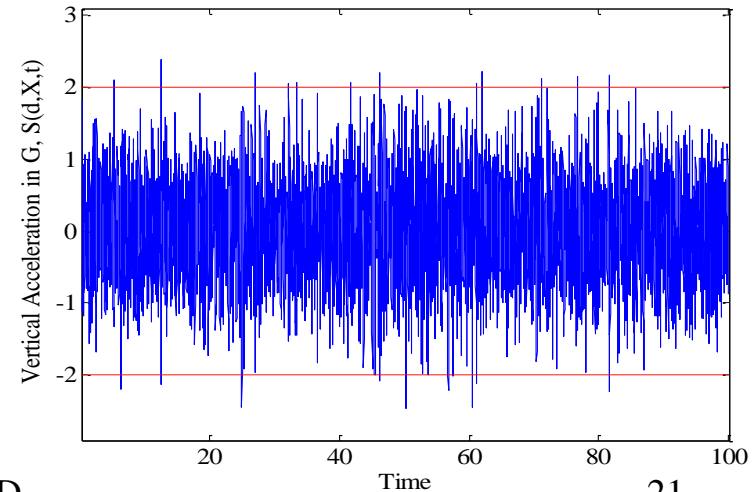
Stiffness, $k_s \sim N(40 \times 10^3, (4 \times 10^3)^2)$

Random Input Process: Experimental Stochastic Terrain from Yuma Proving Grounds.



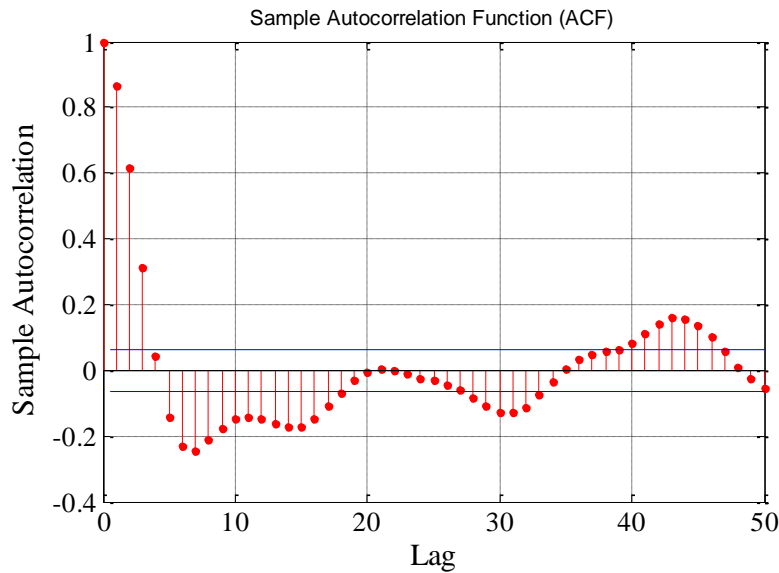
Random Output Process
(Vertical Acceleration, G')

Threshold = 2G

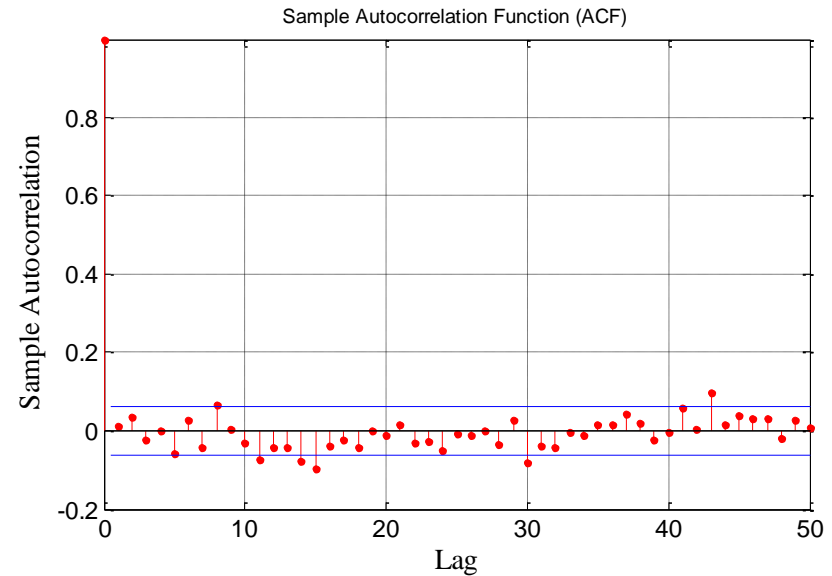


AR(3) model was identified based on:

Autocorrelation Function



Autocorrelation of Residual process



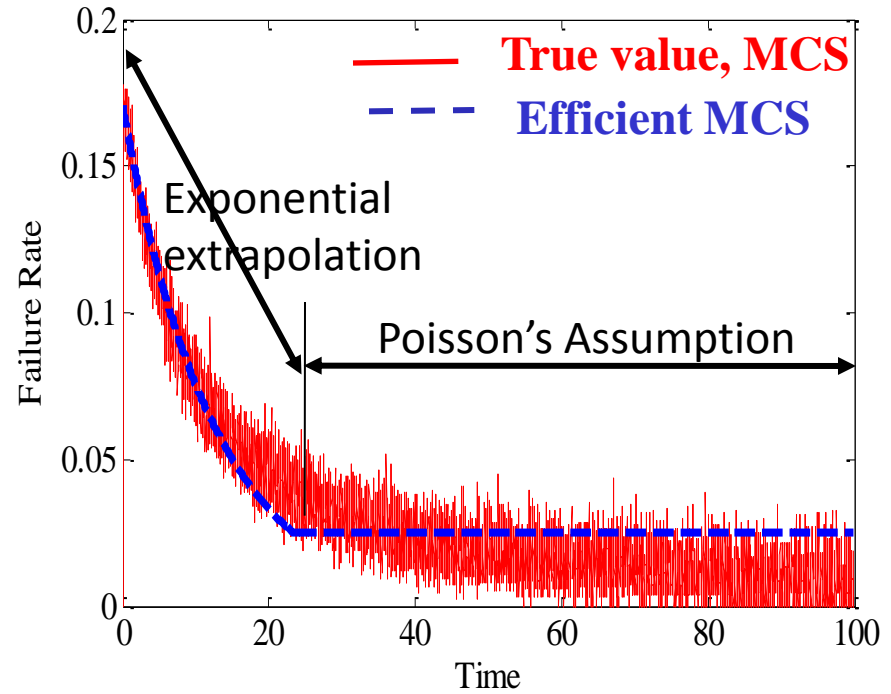
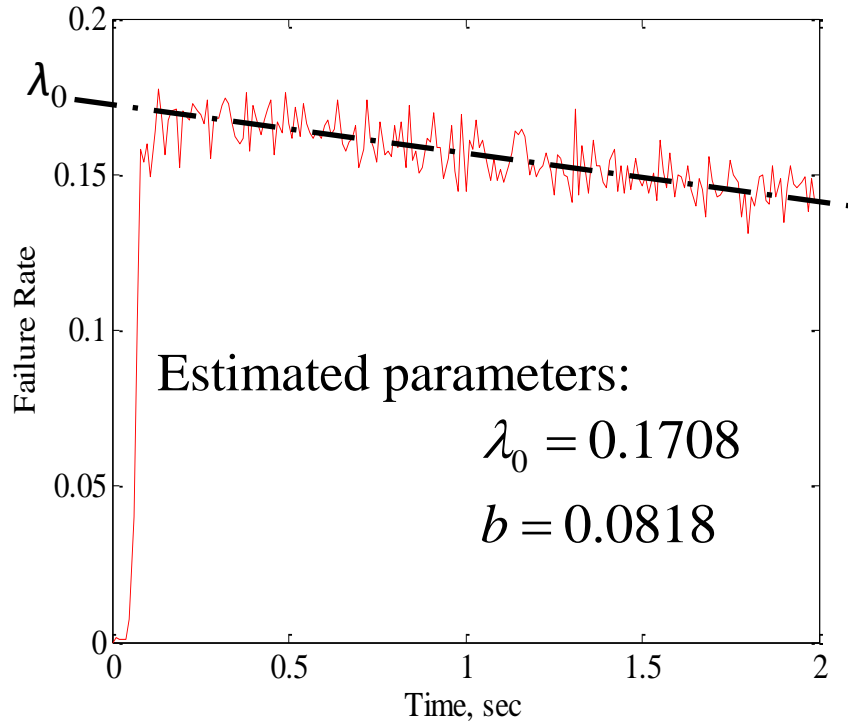
$$u_i = 1.2456 u_{i-1} - 0.2976 u_{i-2} - 0.1954 u_{i-3} + \varepsilon_i(0, 0.5132^2)$$

Statistical tests were performed to verify the model



Quarter-Car Model: Results

(Failure Rate Estimation for Threshold = 2G)



Estimation requires short duration MCS

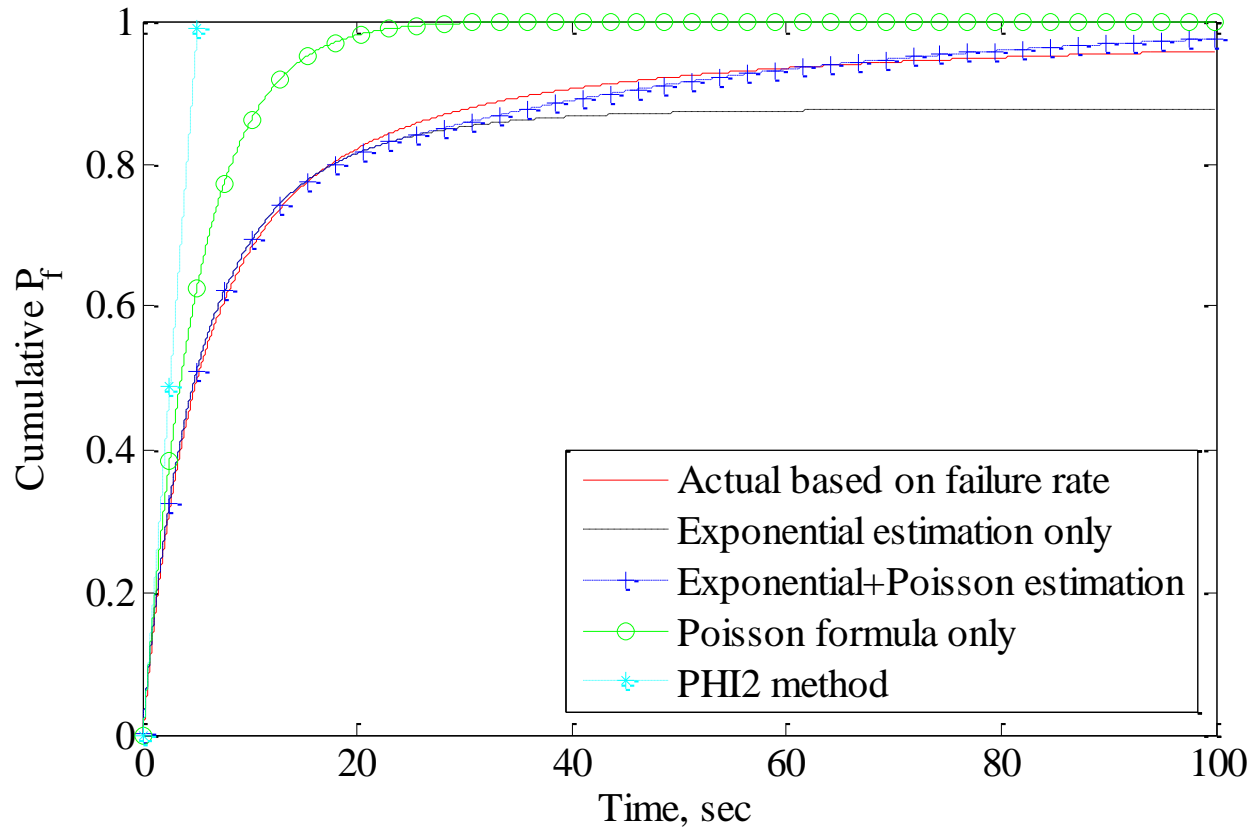
Exponential extrapolation

$$\hat{\lambda}(t) \approx \lambda_0 e^{-bt}$$

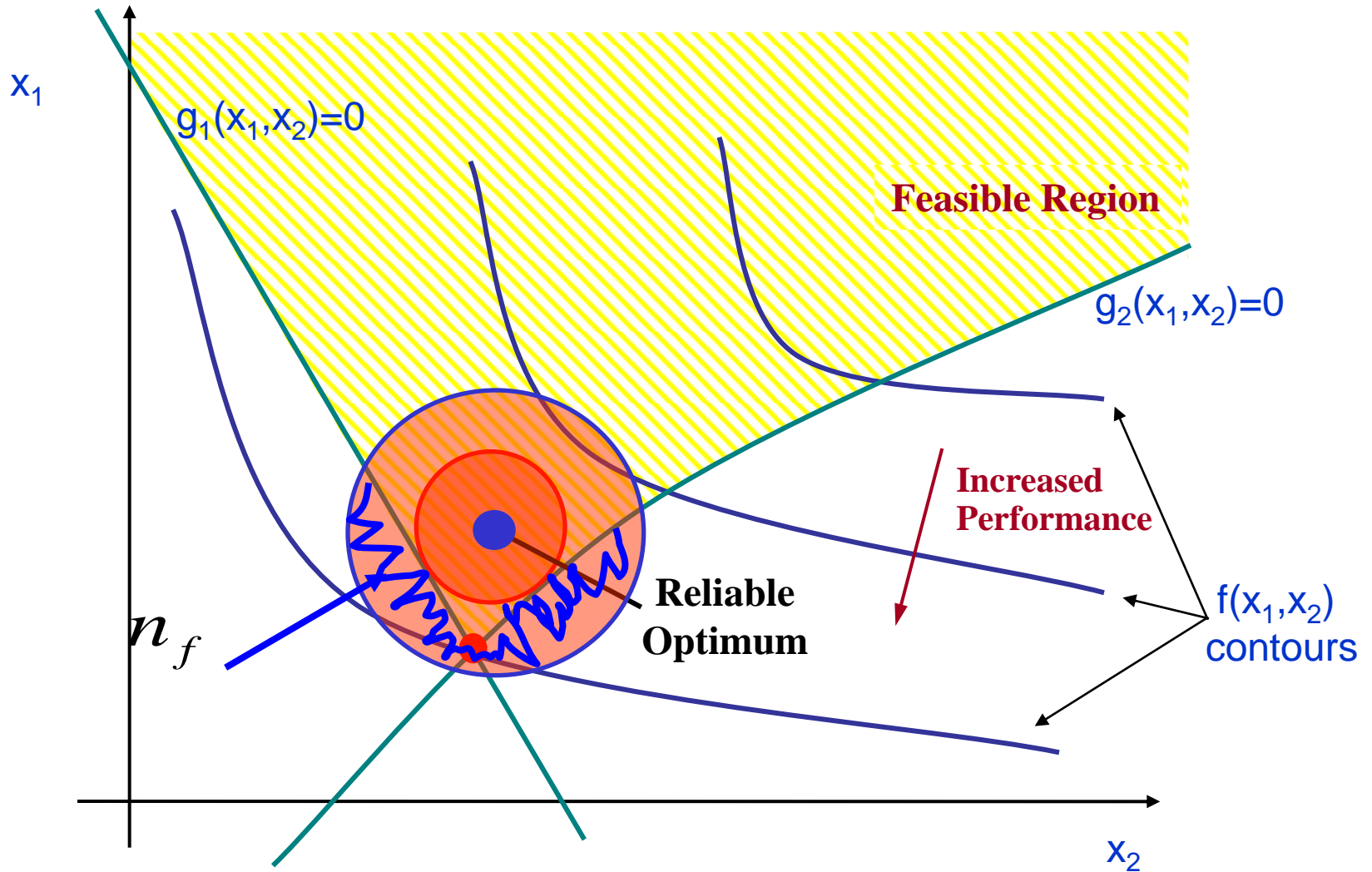


Quarter-Car Model: Results

Cumulative Probability of Failure for Threshold = 2G



Efficient MCS (blue) approach is close to true MCS results (red)



Instantaneous **Conditional** Probability of Failure:

$$p_f^\lambda(t_i) = \int_{\Omega} \theta(\mathbf{x}; t_i) f_{\mathbf{X}}(\mathbf{x}; t_i) d\mathbf{x}$$

$\mathbf{x} = \{x_1, x_2, \dots, x_i\}$ where x_i is a realization of R.V. $X_i = X(t_i)$

$$p_f^\lambda(t_i) = \int_{\Omega} \theta(\mathbf{x}; t_i) \frac{f_{\mathbf{X}}(\mathbf{x}; t_i)}{f_{\mathbf{X}^S}(\mathbf{x}; t_i)} f_{\mathbf{X}^S}(\mathbf{x}; t_i) d\mathbf{x}$$

← **Sampling Joint PDF**

$$p_f^\lambda(t_i) = \frac{\sum_{n=1}^{N_s(t_{i-1})} \theta(\mathbf{x}; t_i) \omega(\mathbf{x}, t_i)}{N_s(t_{i-1})} = \frac{\sum_{n=1}^{N_f(t_i)} \omega(\mathbf{x}, t_i)}{N_s(t_{i-1})}$$

$$p_f^\lambda(t_i) = \frac{\sum_{n=1}^{N_S(t_{i-1})} \theta(\mathbf{x}; t_i) \omega(\mathbf{x}, t_i)}{N_S(t_{i-1})} = \frac{\sum_{n=1}^{N_f(t_i)} \omega(\mathbf{x}, t_i)}{N_S(t_{i-1})}$$

$$\lambda(t_i) = \lim_{\Delta t \rightarrow 0} \frac{p_f^\lambda(t_i)}{\Delta t} = \lim_{\Delta t \rightarrow 0} \frac{\sum_{n=1}^{N_f(t_i)} \omega(\mathbf{x}, t_i)}{\Delta t \cdot N_S(t_{i-1})}$$

$$\omega(\mathbf{x}, t_i) = \frac{f_{\mathbf{X}}(\mathbf{x}; t_i)}{f_{\mathbf{X}^S}(\mathbf{x}; t_i)} \quad : \text{Likelihood ratio at } t_i$$

$N_S(t_{i-1})$: Safe sample points at t_{i-1}

$N_f(t_i)$: Number of failures in $\Delta t = t_i - t_{i-1}$

Likelihood ratio:

$$\omega(\mathbf{x}; t_i) = \frac{f_{\mathbf{X}}(\mathbf{x}; t_i)}{f_{\mathbf{X}}^S(\mathbf{x}; t_i)} = \frac{f_{\mathbf{X}}(x_i, x_{i-1}, \dots, x_{i-d})}{f_{\mathbf{X}}^s(x_i, x_{i-1}, \dots, x_{i-d})}$$

Decorrelation length : Maximum number of lags over which realizations of x_i are significantly correlated

$$x_i - \mu = \phi_1(x_{i-1} - \mu) + \phi_2(x_{i-2} - \mu) + \dots + \phi_p(x_{i-p} - \mu) + \varepsilon_i(N(0, \sigma_s^2))$$

To generate sampling PDF

$$f_{\mathbf{X}}(\mathbf{x}) = \frac{1}{(2\pi)^{k/2} |\Sigma|^{1/2}} \exp\left(-\frac{1}{2}(\mathbf{x} - \boldsymbol{\mu})^T \Sigma^{-1}(\mathbf{x} - \boldsymbol{\mu})\right)$$

From Yule-Walker Eqs

Estimation of Safe Sample Functions

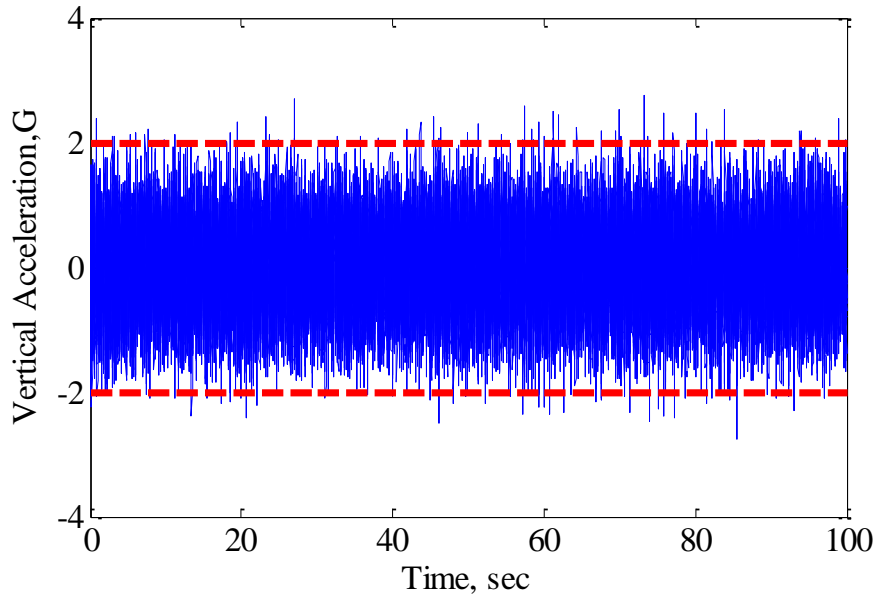
$$\lambda(t_i) = \lim_{\Delta t \rightarrow 0} \frac{\sum_{n=1}^{N_f(t_i)} \omega(\mathbf{x}, t_i)}{\Delta t \cdot N_S(t_{i-1})}$$

$$\frac{\sigma_e}{\sigma_S} x_f > S_{threshold}$$

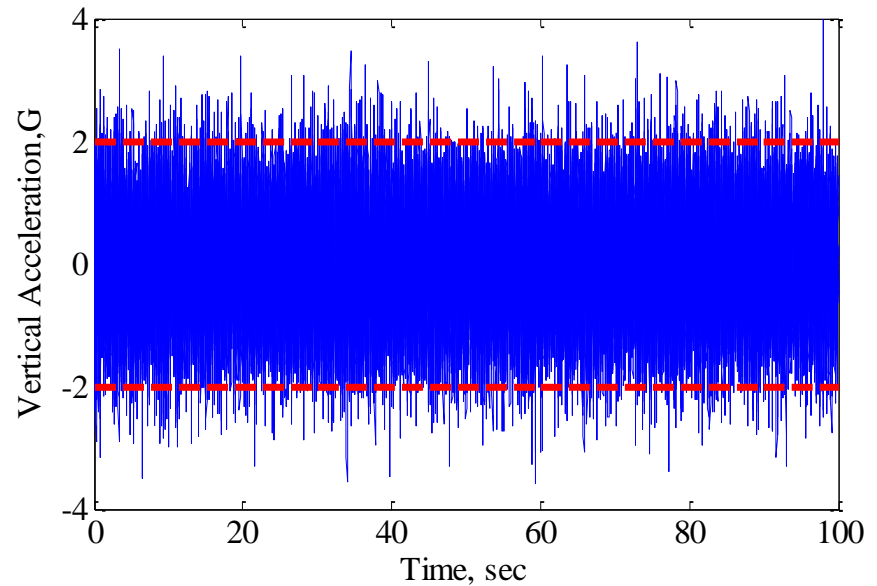
“Inflated” response

$$u_i = 1.2456u_{i-1} - 0.2976u_{i-2} - 0.1954u_{i-3} + \varepsilon_i(0,0.5132^2)$$

Original PDF $\sigma_e = 0.51$

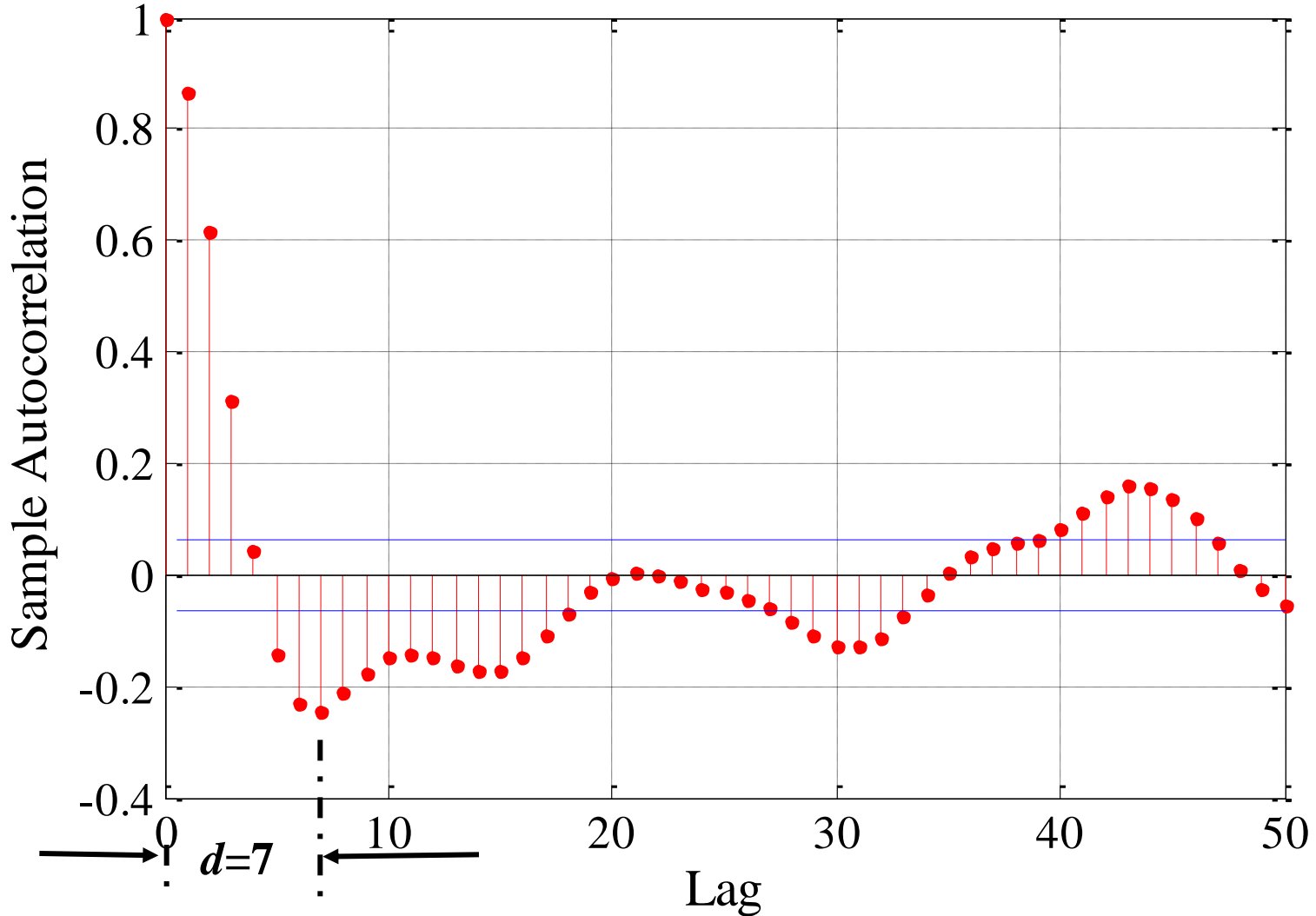


Sampling PDF $\sigma_s = 0.7$

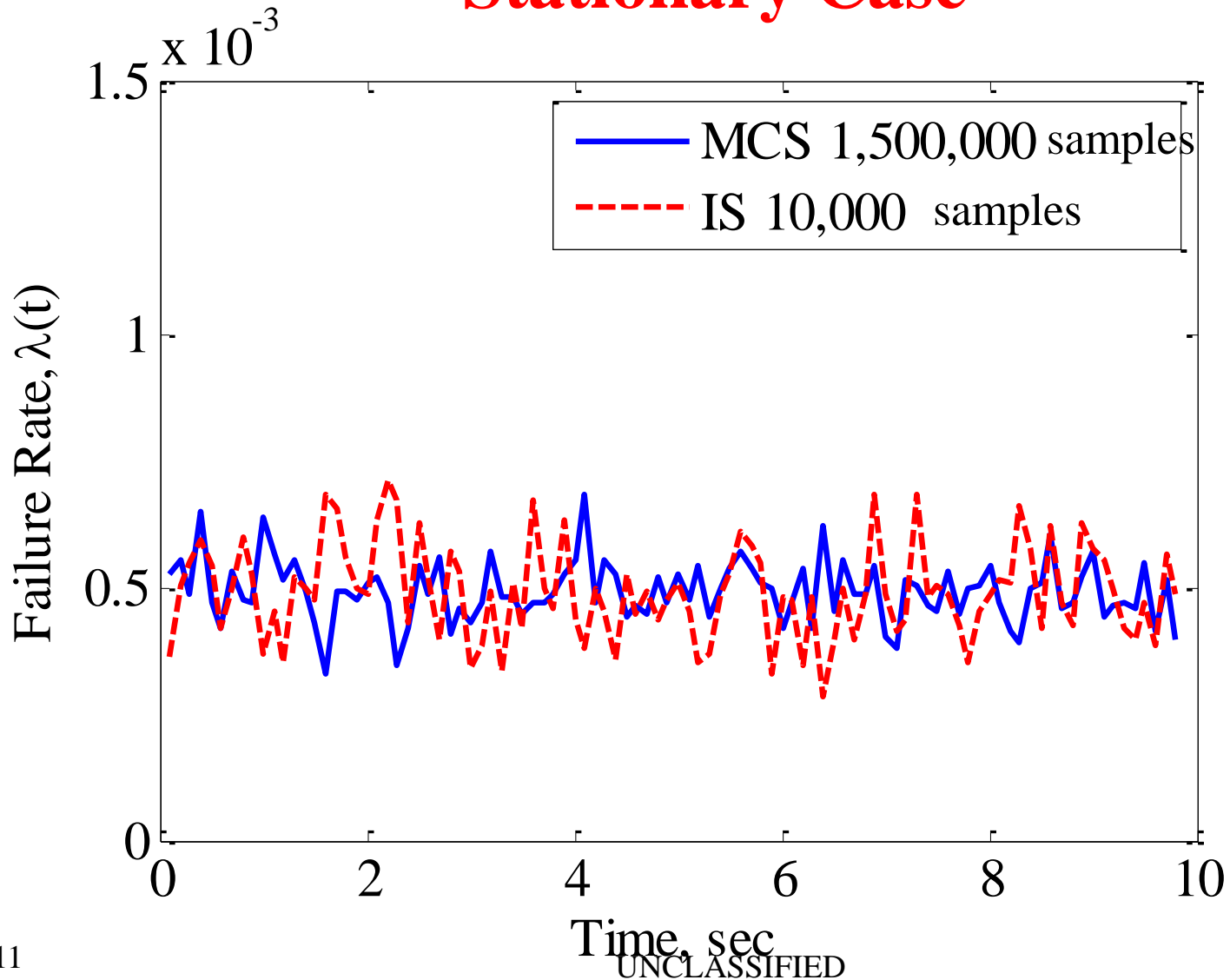


The sampling PDF results in more failures

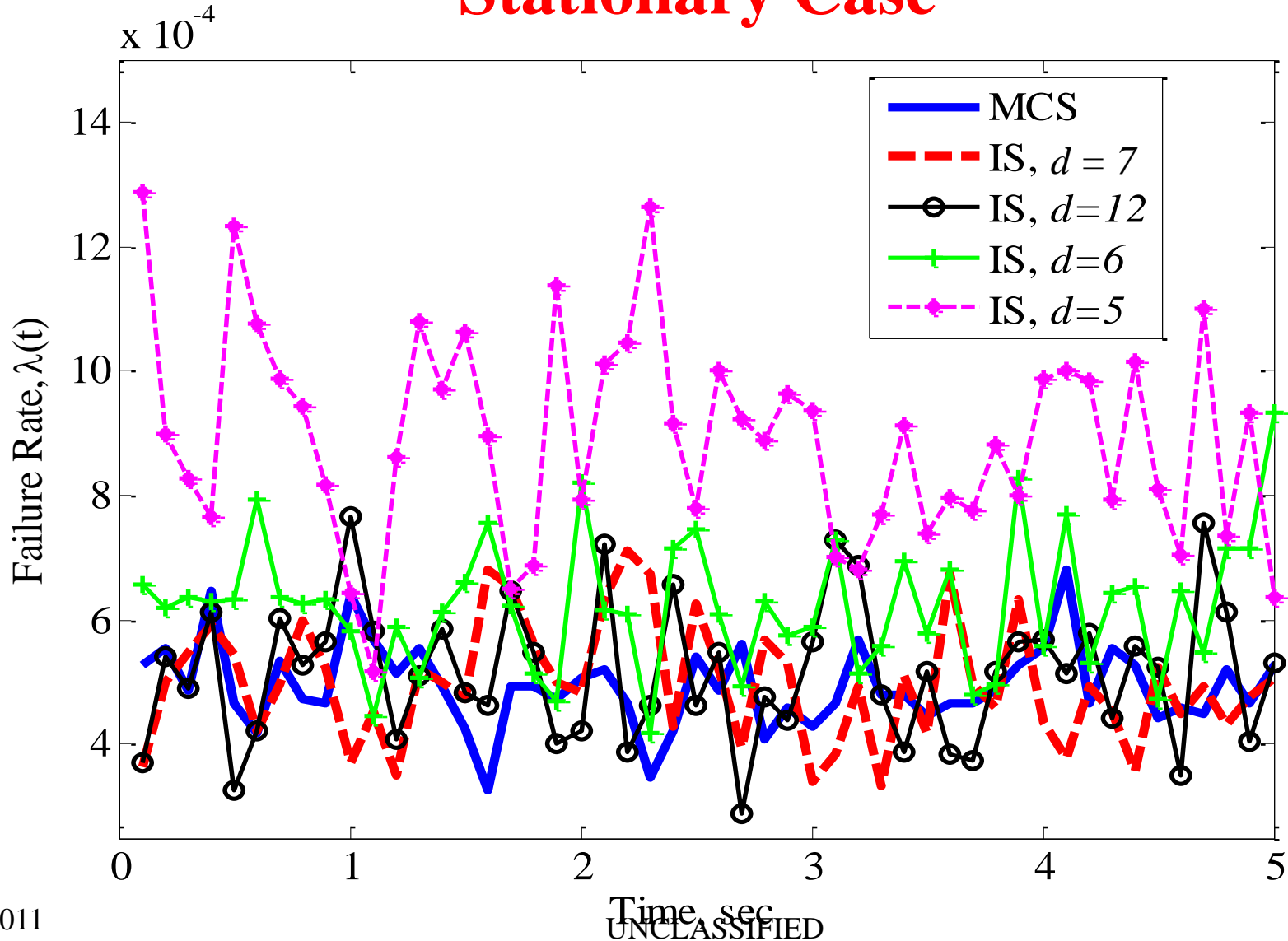
Sample Autocorrelation Function (ACF)



Stationary Case



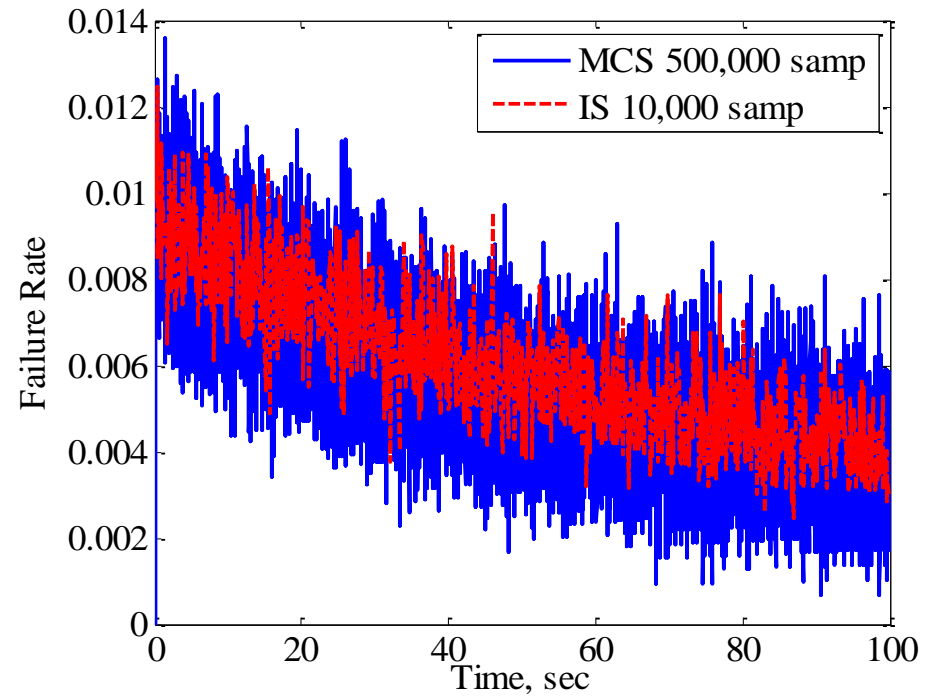
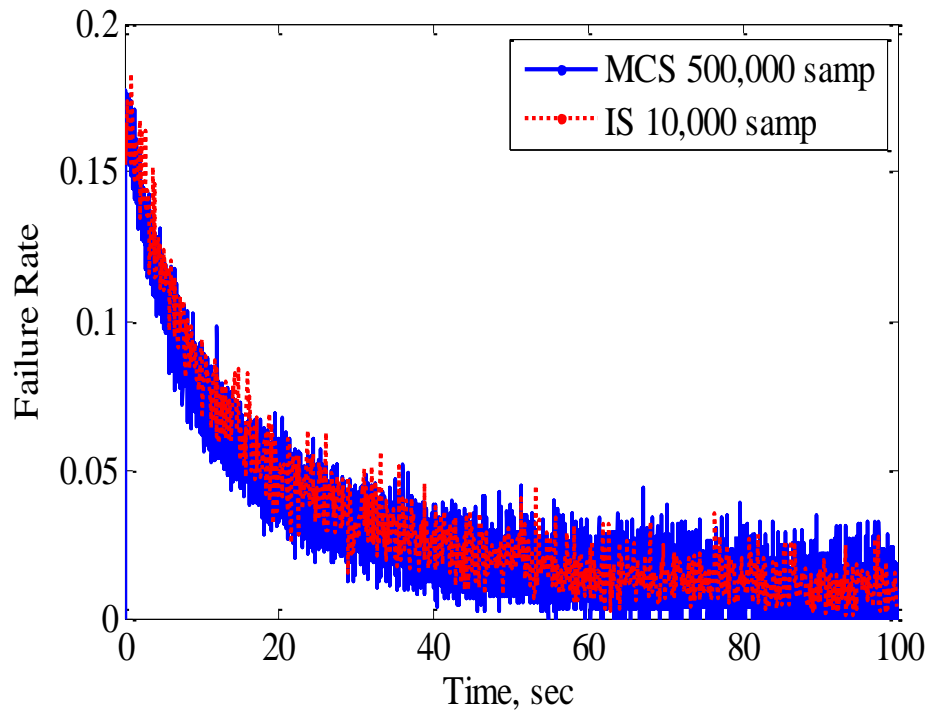
Stationary Case

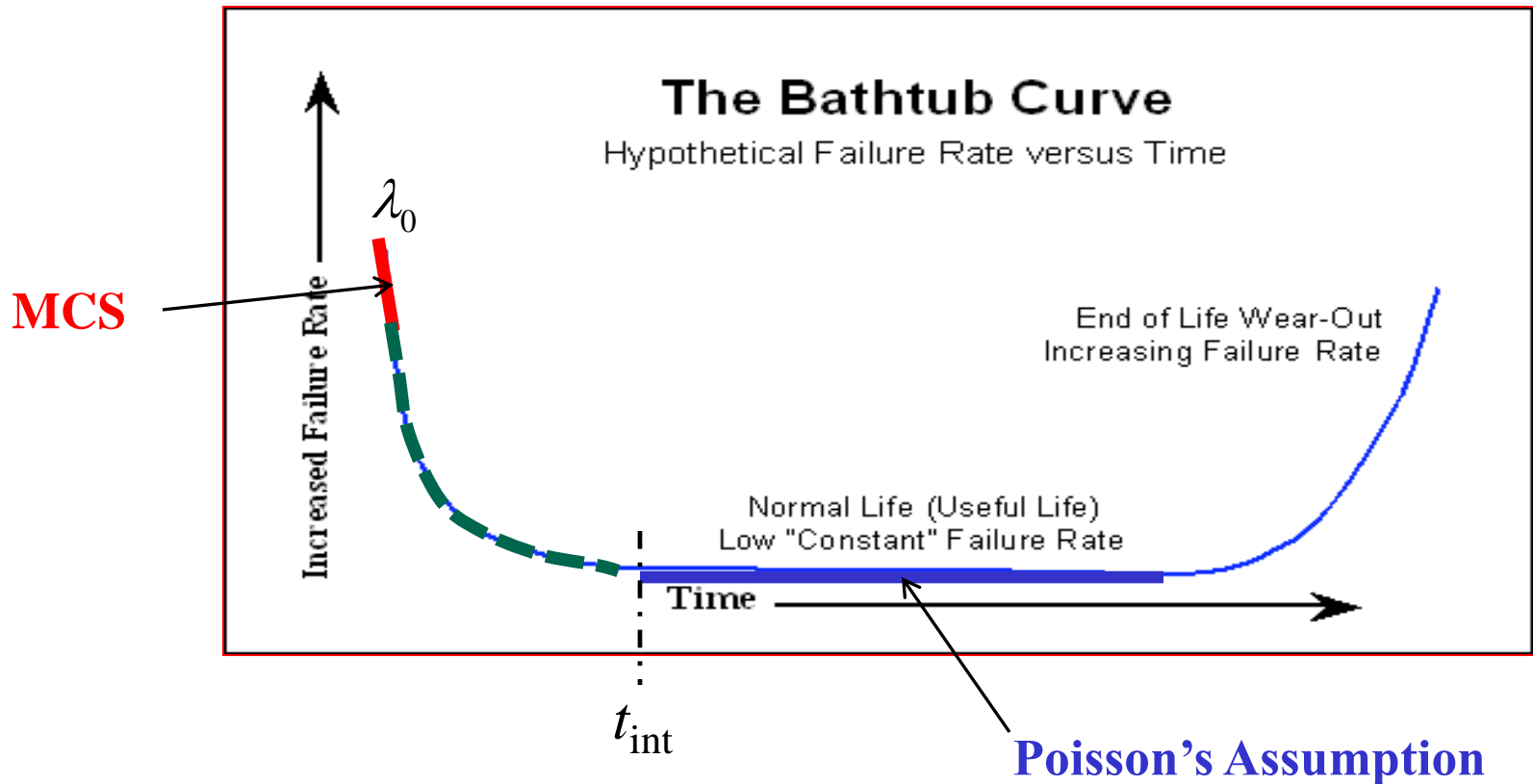


Non-Stationary Case

Threshold = 2 g

Threshold = 2.65 g





➤ Analytical methods can be used under the Poisson's assumption

➤ IS at initial time may need a few thousand output sample functions



Ongoing Work Plan



- **Improve the current accelerated testing method based on importance sampling so that **only 5-10 tests are needed** (Q3)**
 - ✓ **Characterize the “inflated” output random process in importance sampling using “generalized” Kriging and MLE and/or time series**

- **Demonstrate the accelerated testing methodology using the **N-post (or 4-post) Reconfigurable Road Simulator** of the Physical Simulation Laboratory at TARDEC (Q3 and Q4)**



TARDEC N-post Reconfigurable Road Simulator





Thanks for your attention !

Q & A

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