Thermo-Kinetic Model of Burning for Polymeric Materials

<u>Stanislav I. Stoliarov</u>^a, Sean Crowley^b, Richard Lyon^b ^aUniversity of Maryland, Fire Protection Engineering, College Park, MD 20742

^bFAA W. J. Hughes Technical Center, Egg Harbor Twp., NJ 08405

Report Documentation Page				Form Approved OMB No. 0704-0188		
Public reporting burden for the collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to a penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number.						
1. REPORT DATE JUL 2010				3. DATES COVERED		
4. TITLE AND SUBTITLE				5a. CONTRACT NUMBER		
Thermo-Kinetic Model of Burning for Polymeric Materials				5b. GRANT NUMBER		
				5c. PROGRAM ELEMENT NUMBER		
6. AUTHOR(S)				5d. PROJECT NUMBER		
				5e. TASK NUMBER		
				5f. WORK UNIT NUMBER		
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) University of Maryland, Fire Protection Engineering, College Park, MD 20742				8. PERFORMING ORGANIZATION REPORT NUMBER		
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)				10. SPONSOR/MONITOR'S ACRONYM(S)		
				11. SPONSOR/MONITOR'S REPORT NUMBER(S)		
12. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release, distribution unlimited						
^{13. SUPPLEMENTARY NOTES} See also ADM002313. Department of Defense Explosives Safety Board Seminar (34th) held in Portland, Oregon on 13-15 July 2010, The original document contains color images.						
14. ABSTRACT						
15. SUBJECT TERMS						
16. SECURITY CLASSIFIC	17. LIMITATION OF	18. NUMBER	19a. NAME OF			
a. REPORT unclassified	b. ABSTRACT unclassified	c. THIS PAGE unclassified	- ABSTRACT SAR	OF PAGES 19	RESPONSIBLE PERSON	

Standard Form 298 (Rev. 8-98) Prescribed by ANSI Std Z39-18 Develop a versatile model for simulation of bench-scale flammability tests.

□ Parameterize this model for various types of polymeric materials.

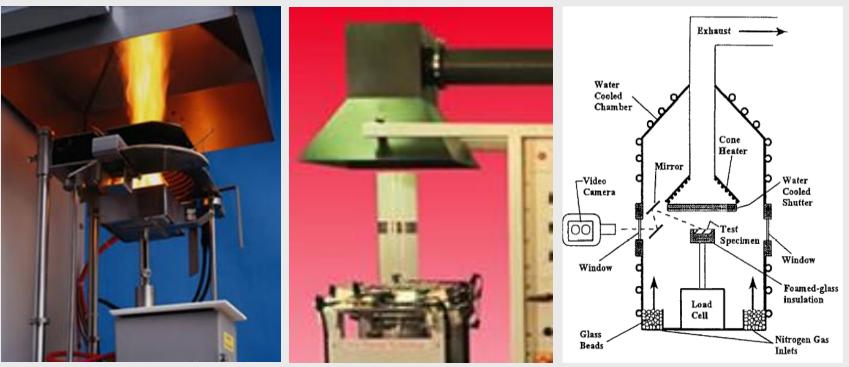
□ Relate parameters (properties) used in the model to molecular structure.

Flammability Measurement Techniques

Cone Calorimetry (heat release measurement)

Fire Propagation Apparatus (heat release measurement)

Gasification Apparatus (mass loss measurement)

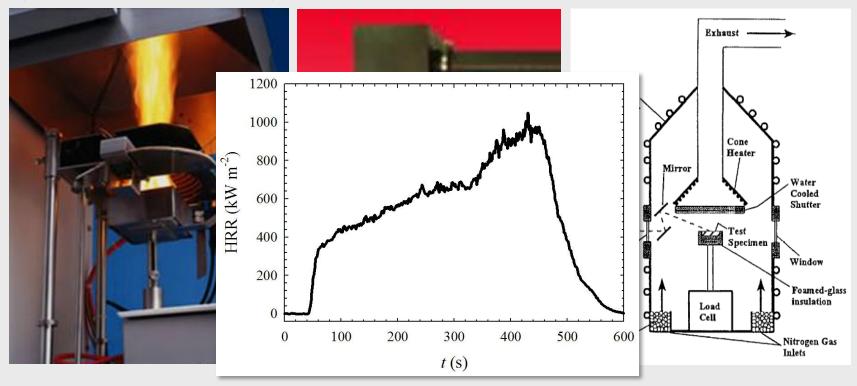


Flammability Measurement Techniques

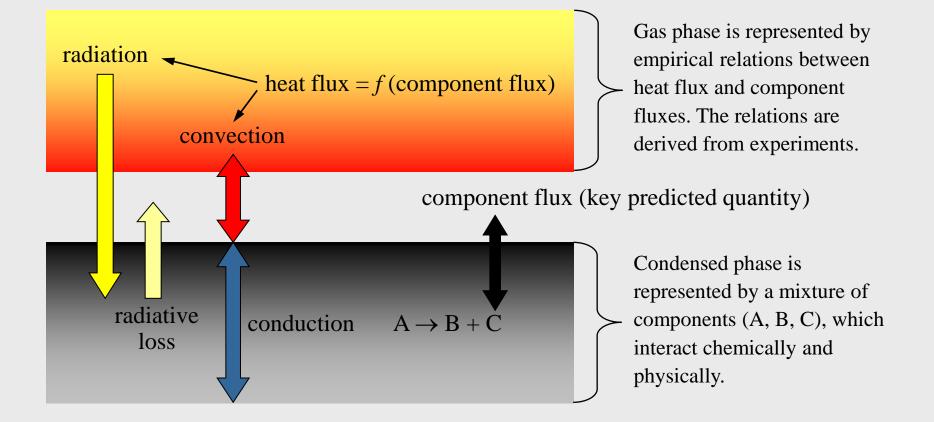
Cone Calorimetry (heat release measurement)

Fire Propagation Apparatus (heat release measurement)

Gasification Apparatus (mass loss measurement)



ThermaKin Model Overview

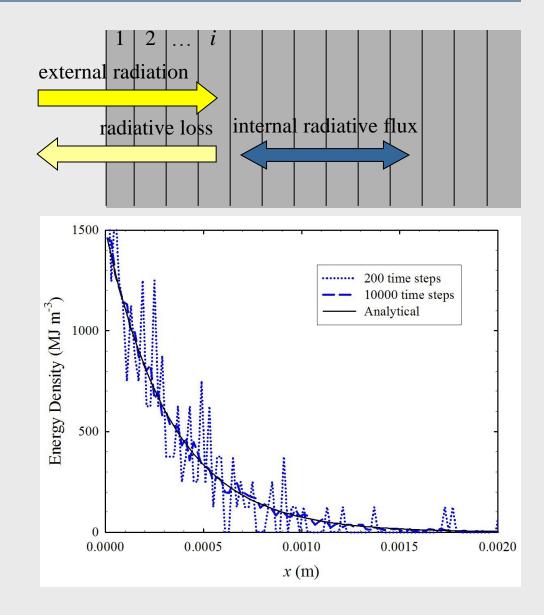


Radiative Energy Transfer

During any given time step, the external radiation is absorbed by a single element chosen at random.

probability of absorption = $\frac{I_i \alpha_i \Delta x_i}{I_1}$ radiative loss = $\varepsilon_i \sigma T_i^4$

internal radiative flux
$$= -k_r \sigma T^3 \frac{\Delta T}{\Delta x}$$



Mass Transfer

Components are categorized as solids, liquids, or gases.

mass flux of gas
$$= -\lambda \rho_g \frac{\Delta \left(\frac{m_g/\rho_g}{V}\right)}{\Delta x}$$

Swelling factor γ defines volumetric reaction of the condensed phase to the presence of gases.

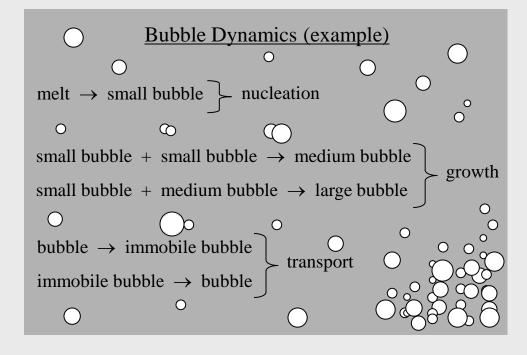
$$\gamma = 0$$

Chemical Reactions

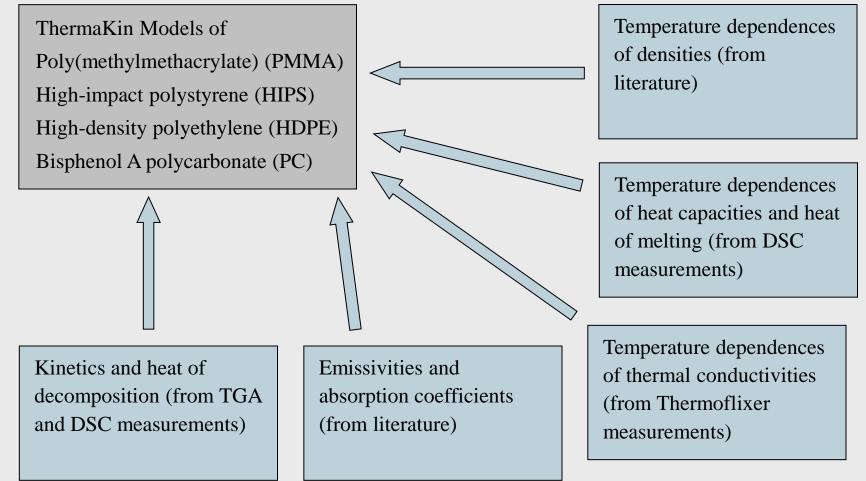
$$\theta_{A}A + \theta_{B}B \rightarrow \theta_{C}C + \theta_{D}D + heat$$

rate =
$$\begin{cases} A \exp\left(-\frac{E}{RT}\right) \left[\frac{m_{\rm A}}{V}\right] \\ \text{or} \\ A \exp\left(-\frac{E}{RT}\right) \left[\frac{m_{\rm A}}{V}\right] \left[\frac{m_{\rm B}}{V}\right] \end{cases}$$

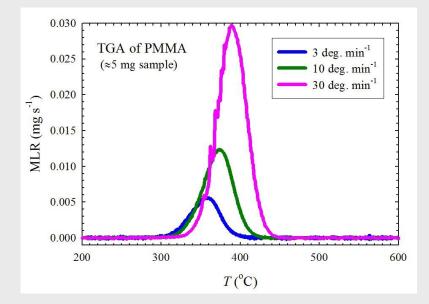
The reaction can be switched on or off at a specified temperature.



Parameterization



Kinetics of Decomposition

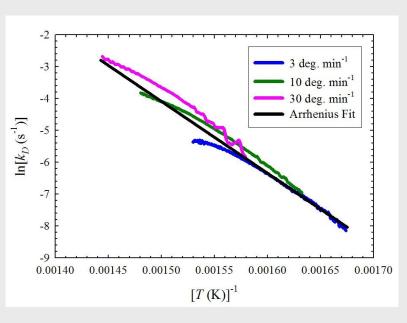


Assumptions:

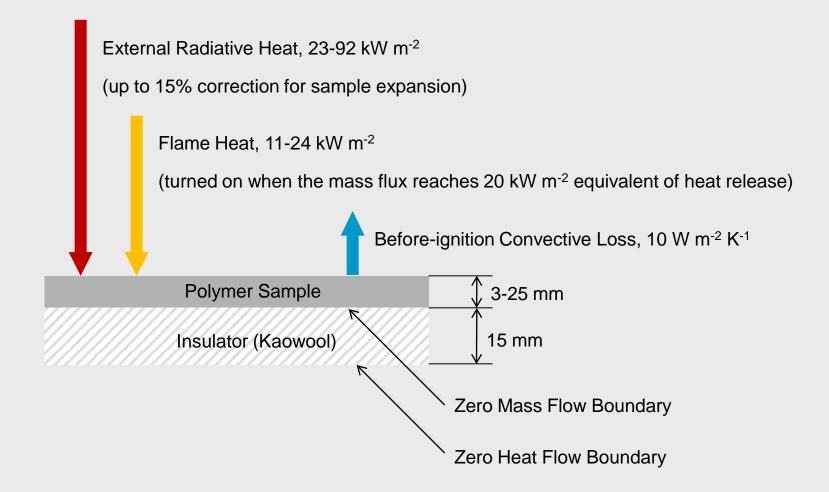
 $PMMA \rightarrow Gas + heat$

 $MLR = k_D m_{PMMA}$ (first order)

Gas leaves PMMA instantaneously.



Modeling of Fire Calorimetry Experiments

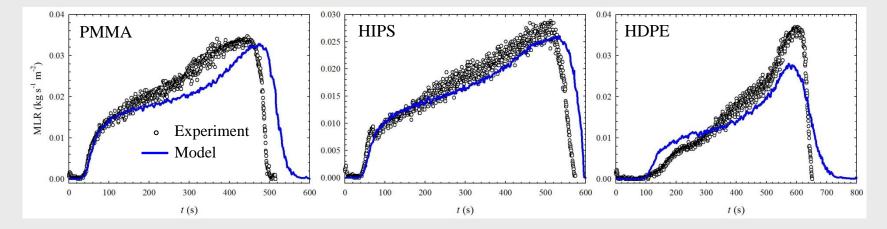


Gasification

Conditions:

external heat flux = 52 kW m^{-2}

```
initial sample thickness \approx 9 \text{ mm}
```

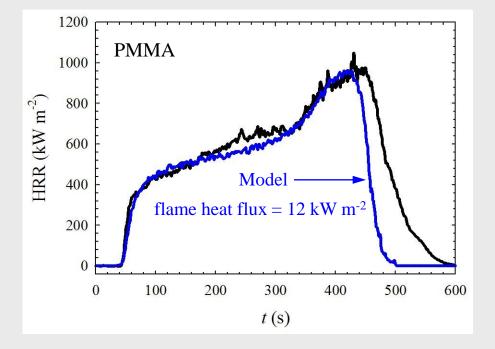


Cone Calorimetry

Conditions:

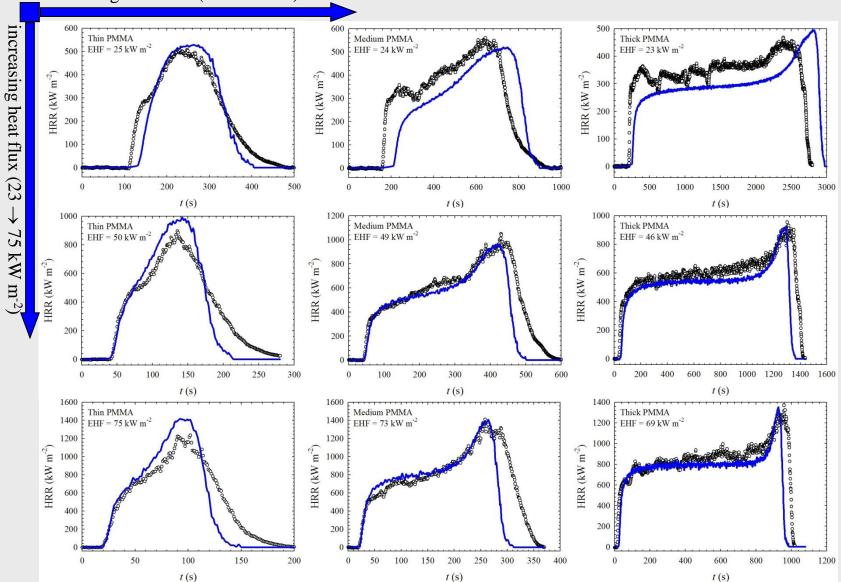
external heat flux = 49 kW m^{-2}

```
initial sample thickness \approx 9 \text{ mm}
```



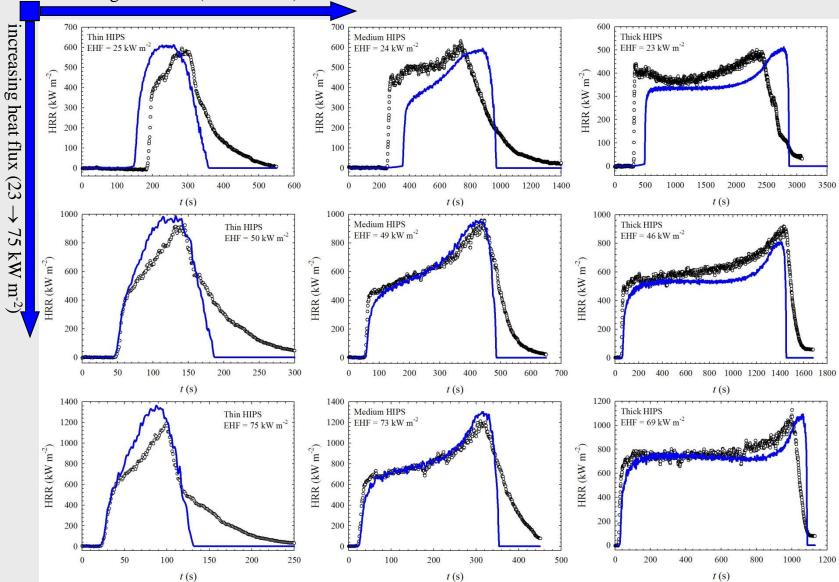
Cone Calorimetry of PMMA

increasing thickness $(3 \rightarrow 25 \text{ mm})$



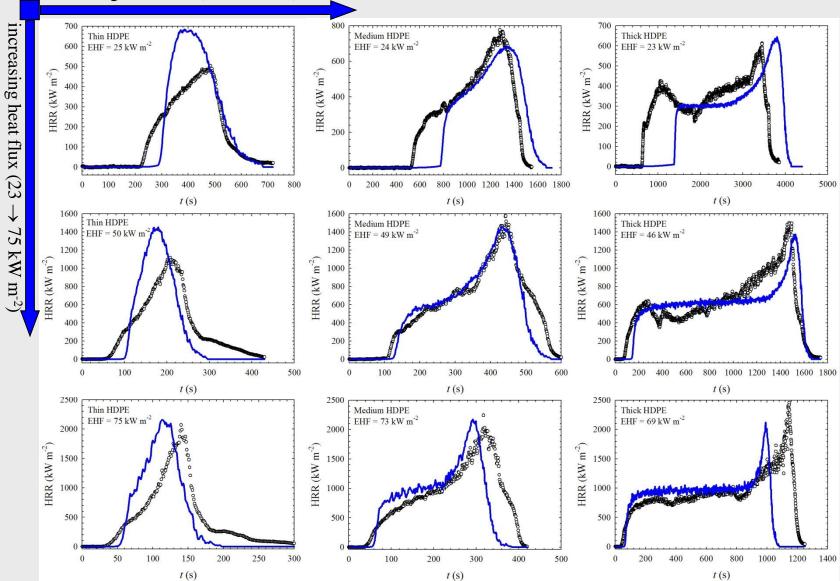
Cone Calorimetry of HIPS

increasing thickness $(3 \rightarrow 25 \text{ mm})$



Cone Calorimetry of HDPE

increasing thickness $(3 \rightarrow 25 \text{ mm})$



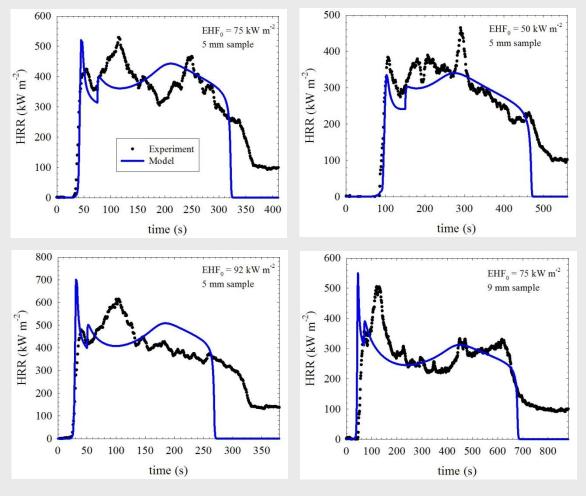
Cone Calorimetry of PC



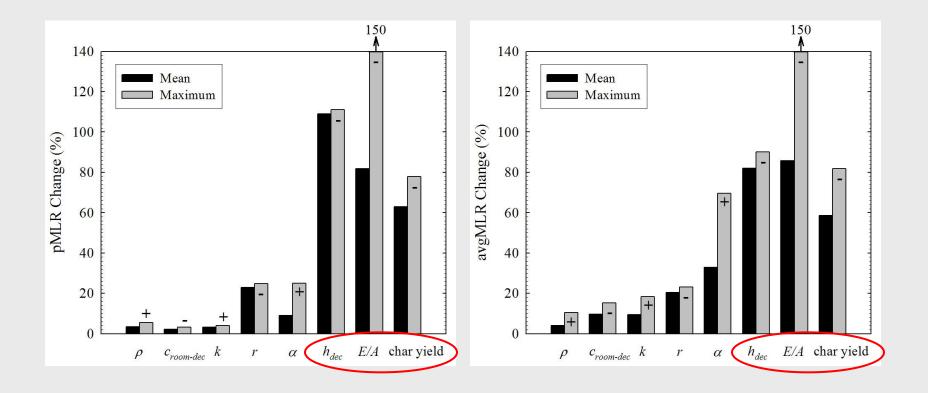
5 mm PC sample after 160 s at 75 kW m⁻².

Flame heat flux = 15 kW m^{-2} .

The main mode of heat transfer inside char is radiation. The rate of transfer is defined by a single adjustable parameter.



Sensitivity of Peak and Average Mass Loss Rates



Conclusions

□ A one-dimensional numerical pyrolysis model can be used to predict the outcome of fire calorimetry experiments performed on polymeric materials.

□ The predictions require the knowledge of chemical, thermal, and optical properties of the material. Measurement of these properties represents a challenging task.

□ The rate of decomposition (defined by *A* and *E*), heat of decomposition, char yield and heat of combustion are the key parameters required for prediction of the peak and average heat release rates.

