U.S. Army Corrosion Summit 2009

Clearwater Beach, FL

Chemically accelerated vibratory surface finishing (CAVSF)

Juergen Fischer, Dustin Umland, Brian Trenbeath, Jennifer Vein, Jennie Jorgenson, Jessica Messer, Matthew Cavalli, Douglas Larson, Bryce Mitton
(Engineered Surfaces Center of the University of North Dakota, Grand Forks)

Ranko Tudorovic, Damian Wilmot, Jarrod Schell, Ben Hoiland, John Rindt
(Alion Science and Technology, Grand Forks)

Report Documentation Page

Form Approved
OMB No. 0704-0188

1. REPORT DATE **FEB 2009**	2. REPORT TYPE	3. DATES COVERED **00-00-2009 to 00-00-2009**
4. TITLE AND SUBTITLE **Chemically accelerated vibratory surface finishing (CAVSF)**		5a. CONTRACT NUMBER
		5b. GRANT NUMBER
		5c. PROGRAM ELEMENT NUMBER
6. AUTHOR(S)		5d. PROJECT NUMBER
		5e. TASK NUMBER
		5f. WORK UNIT NUMBER
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) **University of North Dakota,Engineered Surfaces Center,4201 James Ray Drive,Grand Forks,ND,58202**		8. PERFORMING ORGANIZATION REPORT NUMBER
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)		10. SPONSOR/MONITOR'S ACRONYM(S)
		11. SPONSOR/MONITOR'S REPORT NUMBER(S)

12. DISTRIBUTION/AVAILABILITY STATEMENT
Approved for public release; distribution unlimited

13. SUPPLEMENTARY NOTES
2009 U.S. Army Corrosion Summit, 3-5 Feb, Clearwater Beach, FL

14. ABSTRACT

15. SUBJECT TERMS

16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT	18. NUMBER OF PAGES	19a. NAME OF RESPONSIBLE PERSON
a. REPORT **unclassified**	b. ABSTRACT **unclassified**	c. THIS PAGE **unclassified**	**Same as Report (SAR)**	**51**	

Background

University of North Dakota - UND
* Founded in 1883 - 6 years before statehood.
* 13,000 students in 193 fields of study.

School of Engineering and Mines - SEM
* 1889 made the Engineering College at UND.
* Programs include: Chemical, Civil, Electrical, Geological, and Mechanical Engineering.

Engineered Surfaces Center - ESC
* About 3 years.
* Director, 3 FT Engineers and expanding.
* 2 PT Faculty.
* 1 PT Technician & OA.
* 6 PT Students

Content

- Introduction (Equipment – General – Test samples)
- Basics (Material removal – Roughness changes – Shear stress removal – Temperature increase – Sample distribution – Different media)
- End-roughness and micro structure of different C-steels
- Material removal and roughness changes versus the amount of treatment solution in the bowl
- Material removal and roughness changes versus pH
- Comparing the performance of a commercially available acid treatment solution with 0.5 M Ammonium bioxalate solution

Large vibratory bowl with 1.16 m inner diameter and a dosing station in the background for continuous flow of chemicals through the bowl

Small vibratory bowl with 0.28 m inner diameter filled with 4 kg of large ceramic media.

Chemically accelerated vibratory surface finishing (CAVSF)

Typical Process:

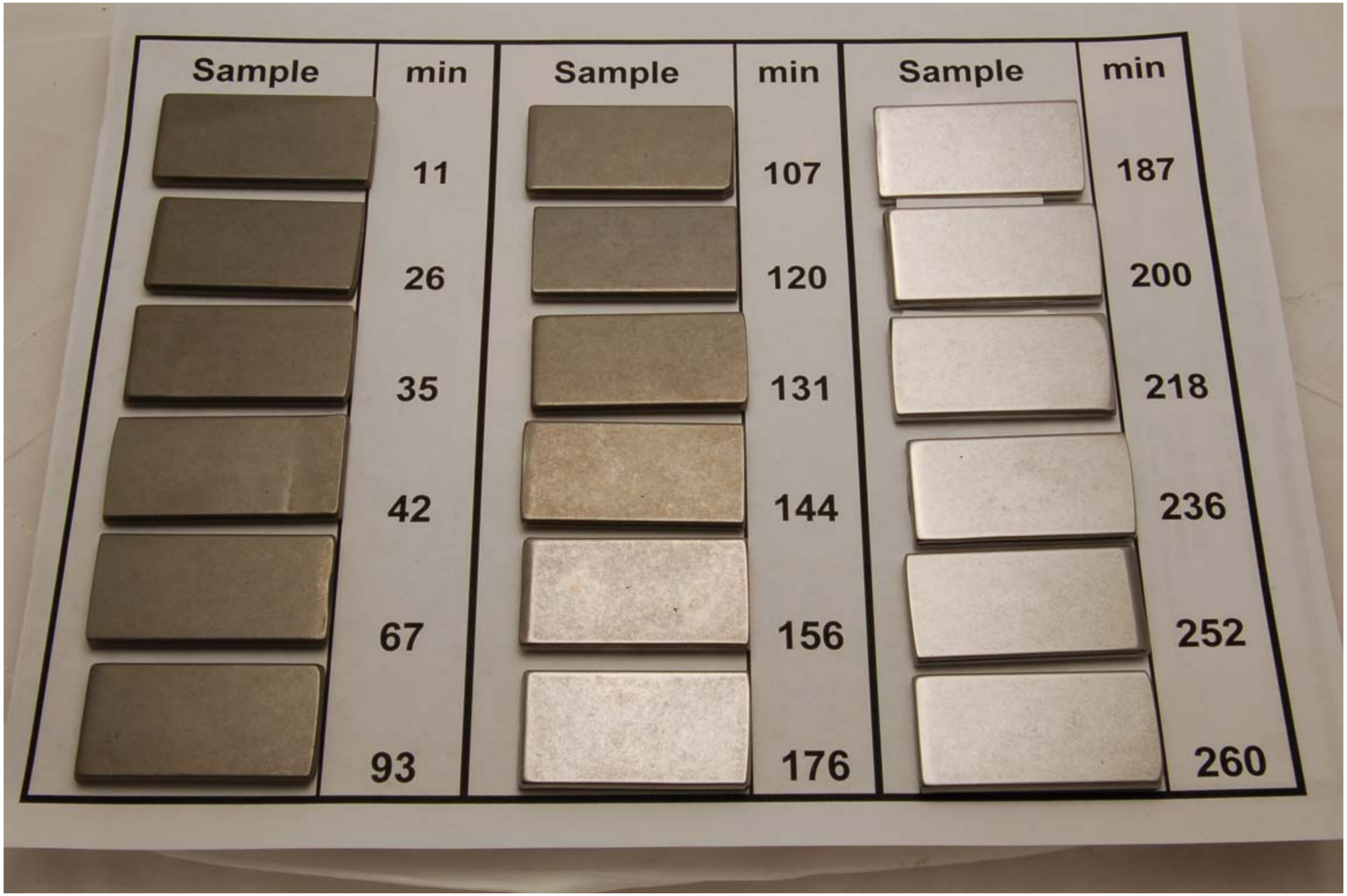
- 2 hours acid treatment
- 15 minutes water rinse
- 2 hours burnishing

Typical Result:

- The average surface roughness of for example helicopter gear teeth goes down from 16 to 2 micro-inches without impairing the geometry – less than 200 micro-inches removed.

Benefits: Less friction and stress at the mating surfaces resulting in

- No run-in time
- Lower operation temperature
- 300 to 400 % longer fatigue lifetime
- Reduced downtime
- Less noise, less vibration
- Higher energy efficiency
- Lower weight in new designs
- Overall lower costs

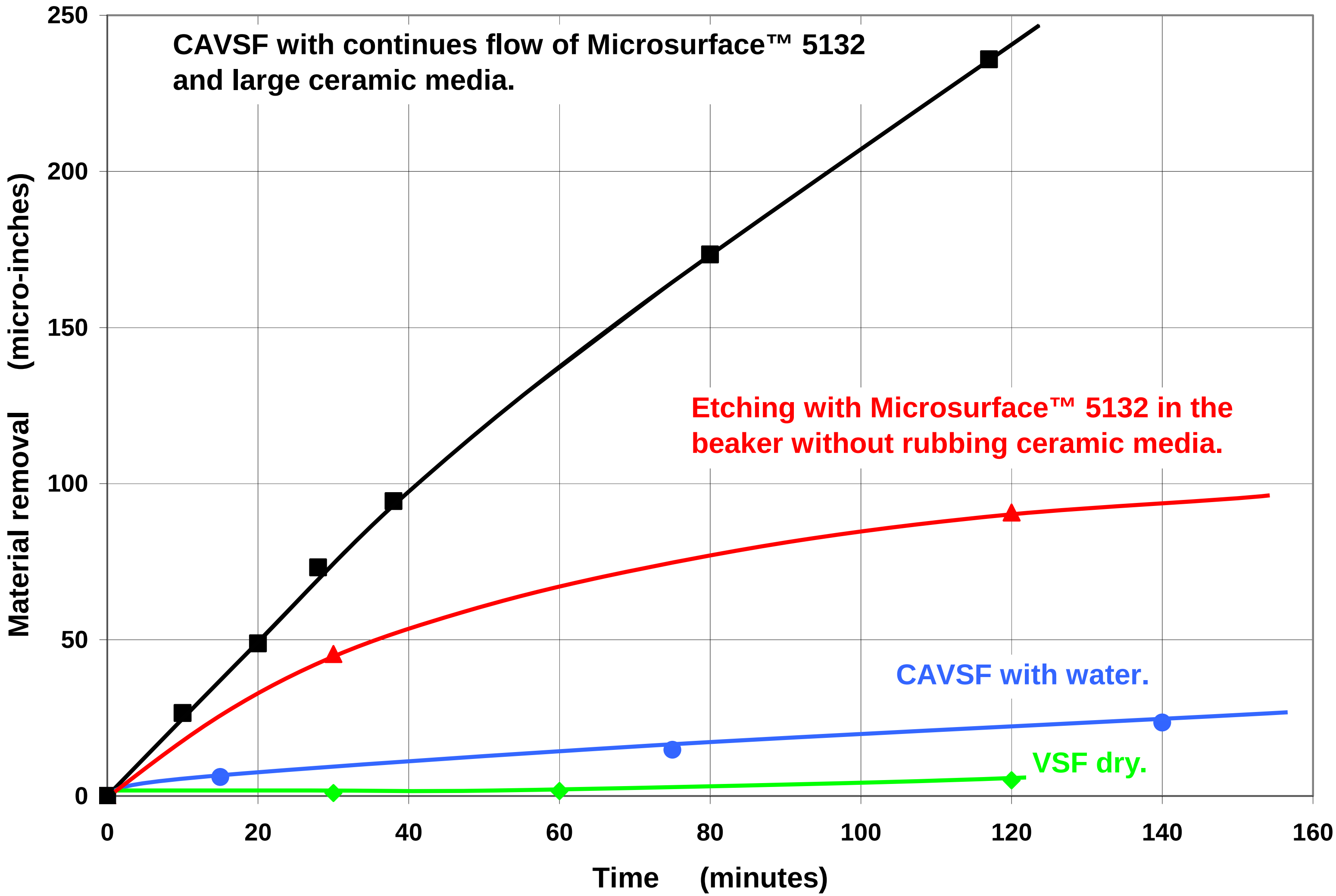


Visual appearance of strip steel test pieces during the CAVSF process.

0-120 minutes = acid treatment

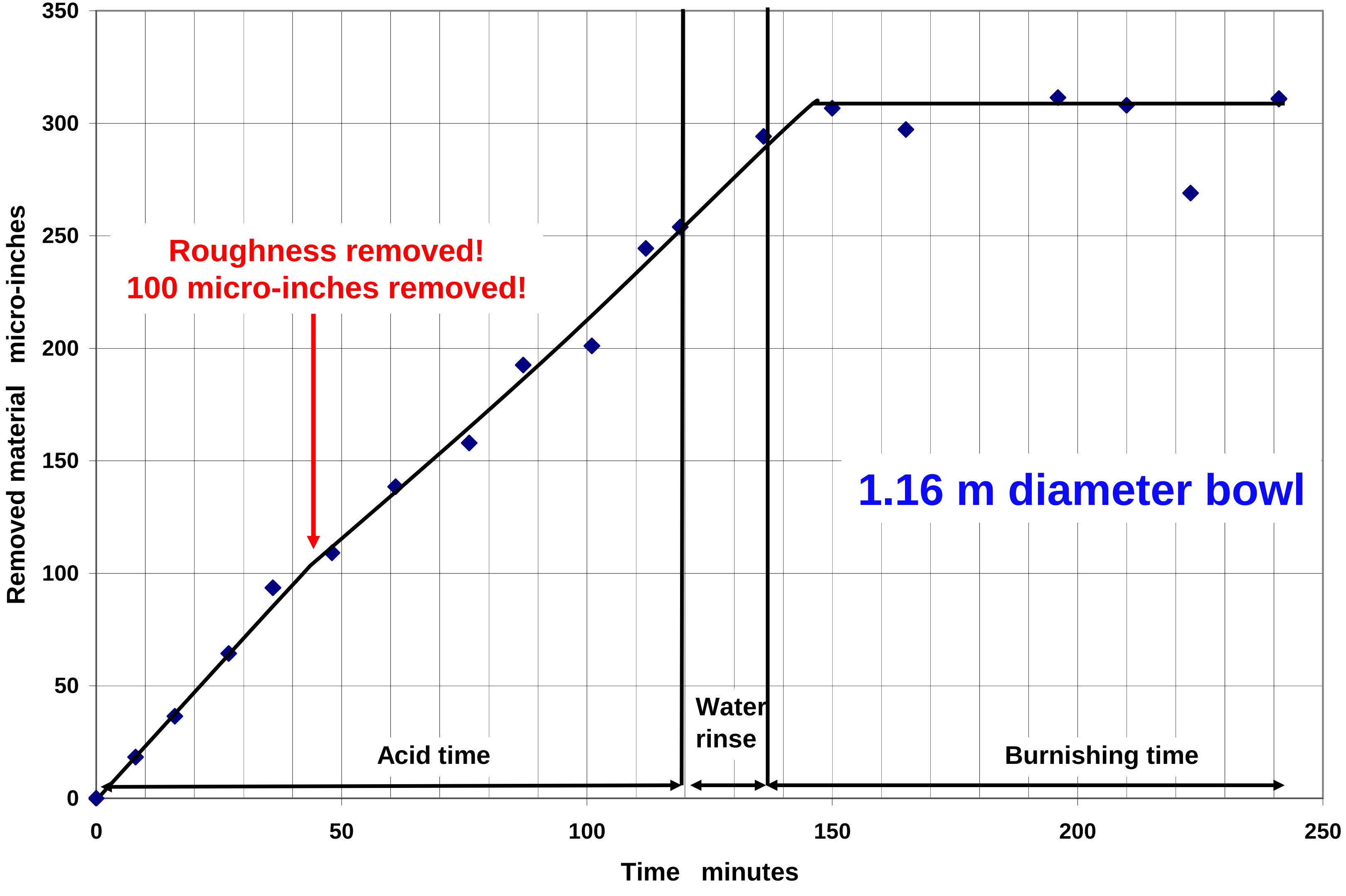
120-135 minutes = water rinse

135-260 minutes = burnishing

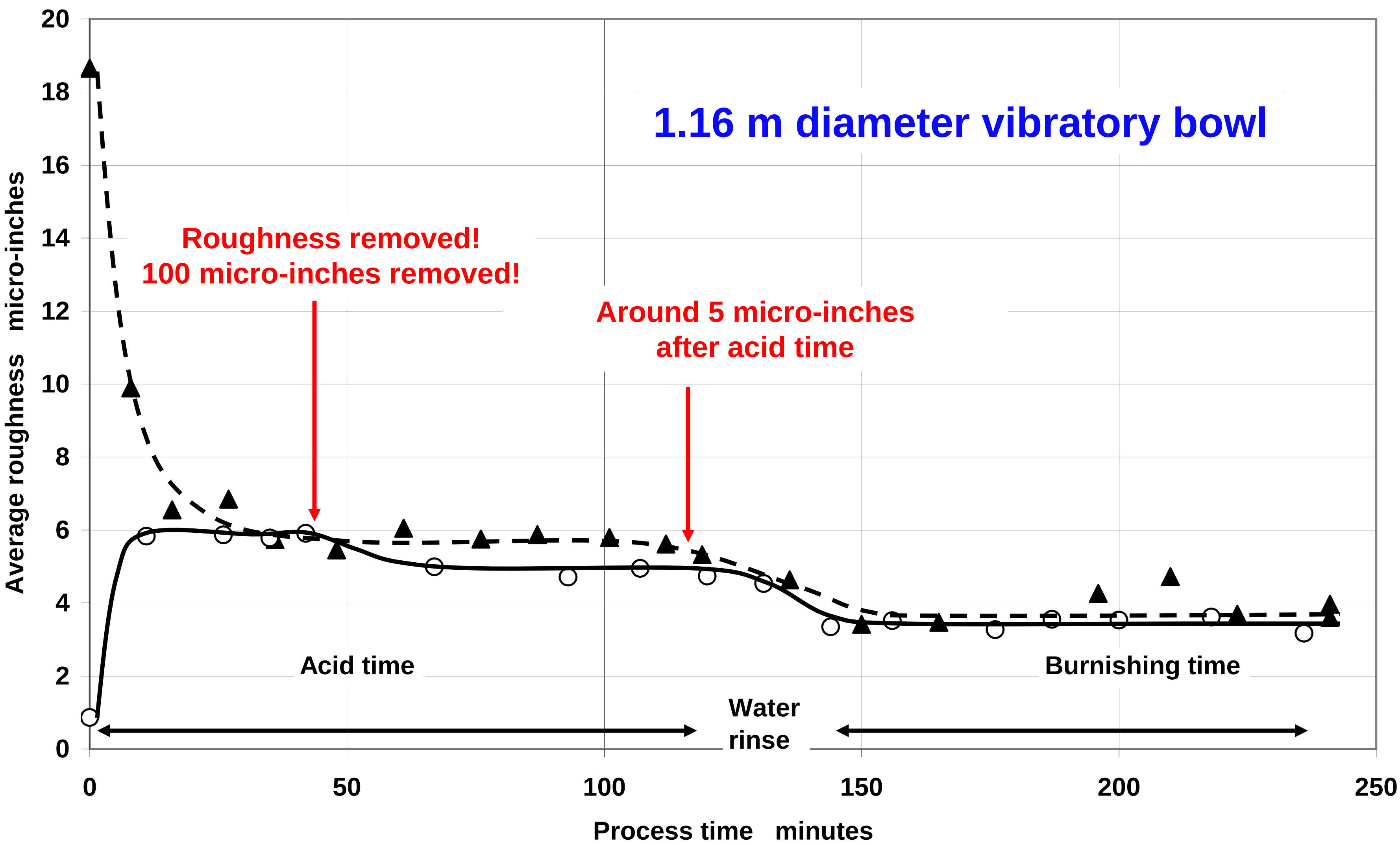


Material removal on Pyrowear 53™ during different processes versus time.

Material removal of strip steel pieces versus CAVSF time



Average roughness of strip steel pieces versus CAVSF time

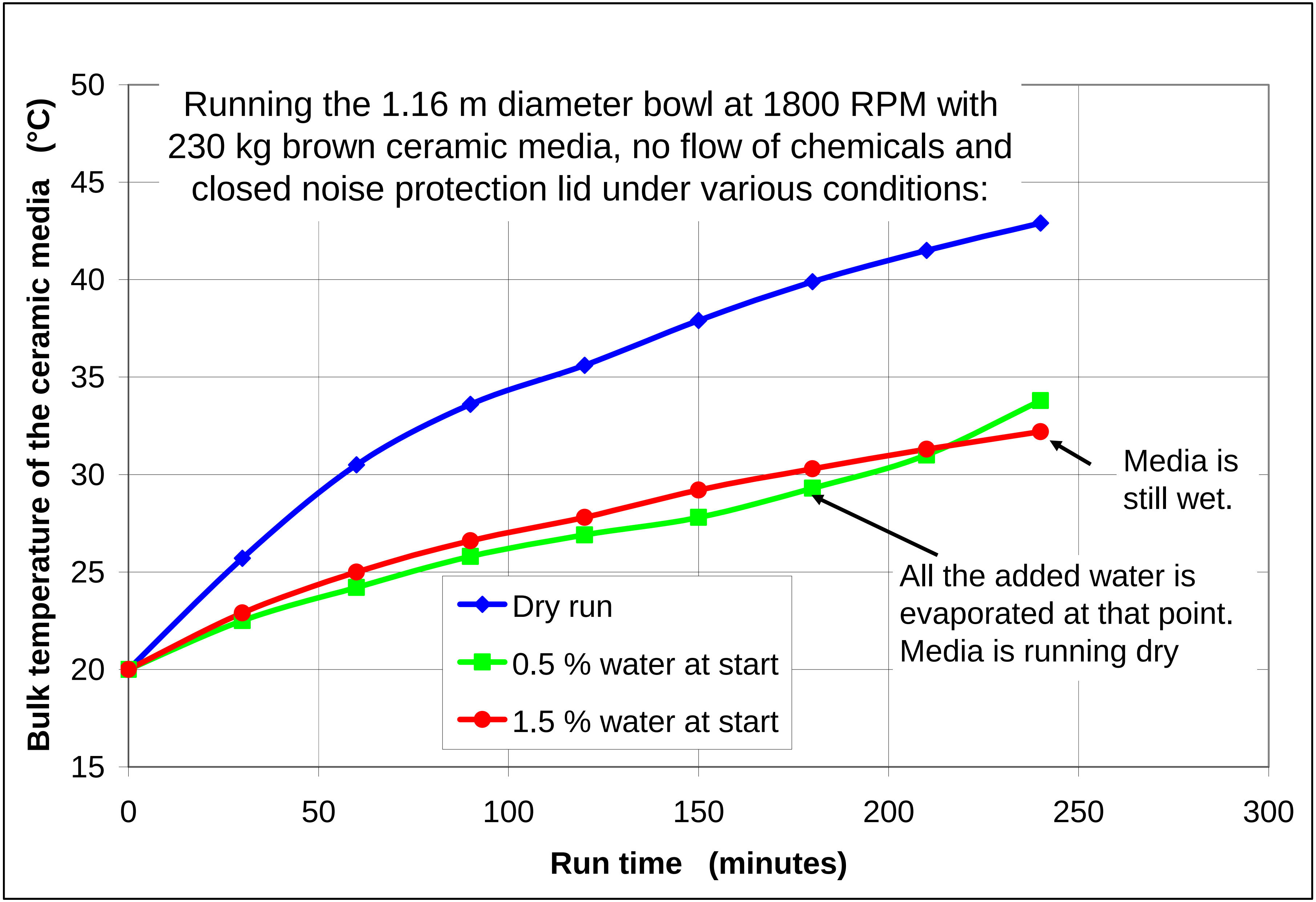


Results of surface stress analysis by Bruker

	Sample	σ_{11}	σ_{22}	σ_{12}	σ_{I}	σ_{II}
As ground	11	-499±80	-211±82	-184±199	-588	-121
After acid treatment	5	-441±82	-375±79	-110±193	-523	-292
After CAVSF	10	-412±87	-427±85	-7±199	-440	-400

The stress unit is MPa

- **σ_I and σ_{II} are the transformed stress values with all shear stress vanished.**
- **The σ_I and σ_{II} indicates the distribution of the stress. The closer values means the stress is more equally distributed along each direction.**
- **With the CAVSF, the shear stress was removed and the distribution of compressive stress becomes much more uniform.**

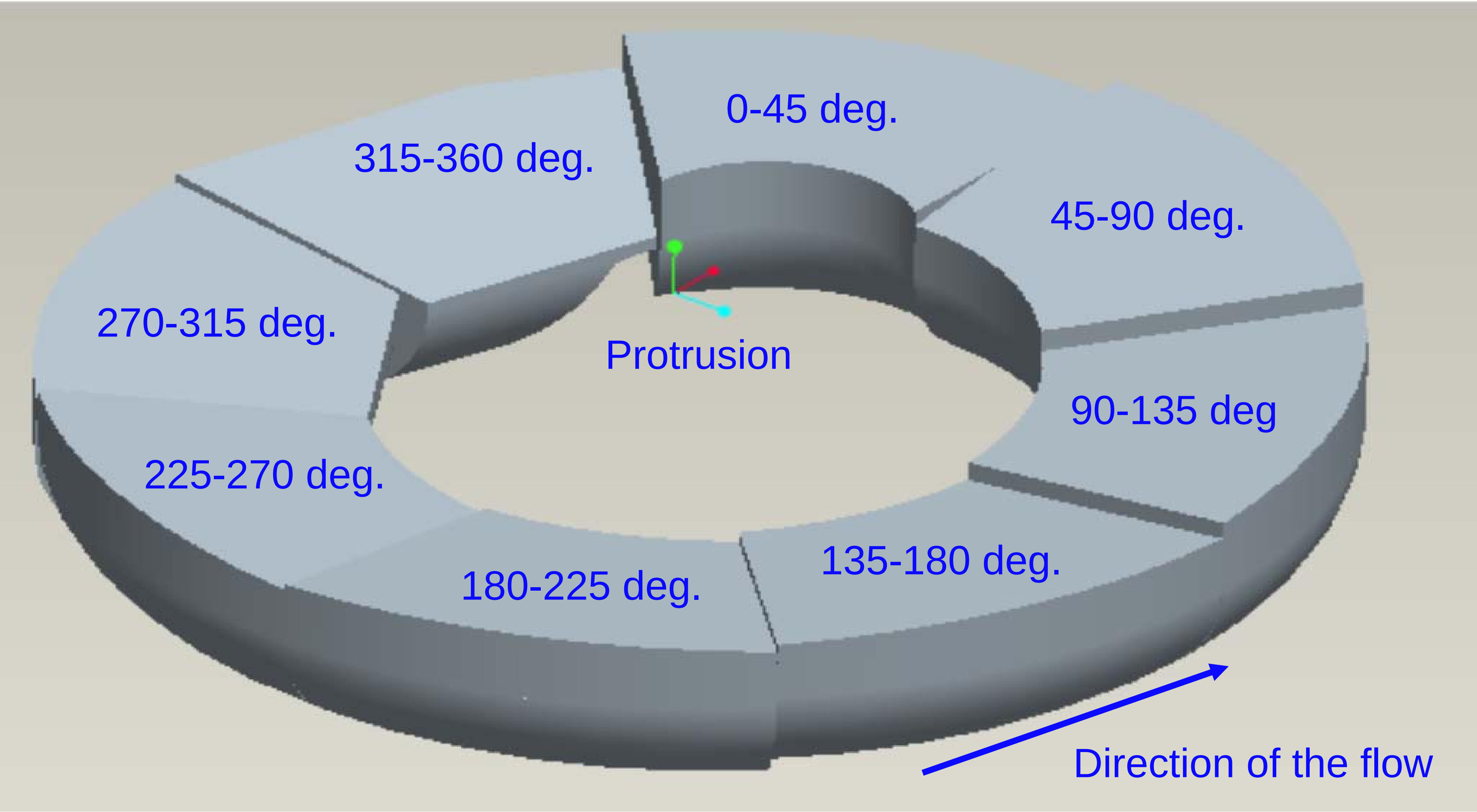

Running the 1.16 m diameter bowl at 1800 RPM with
230 kg brown ceramic media, no flow of chemicals and
closed noise protection lid under various conditions:
Bulk temperature of the ceramic media (°C)
50
45
40
35
30
25
20
15
0
50
100
150
200
250
300
Run time (minutes)
Dry run
0.5 % water at start
1.5 % water at start
Media is still wet.
All the added water is evaporated at that point. Media is running dry

100 strip steel samples arranged for the distribution test

Starting the distribution test

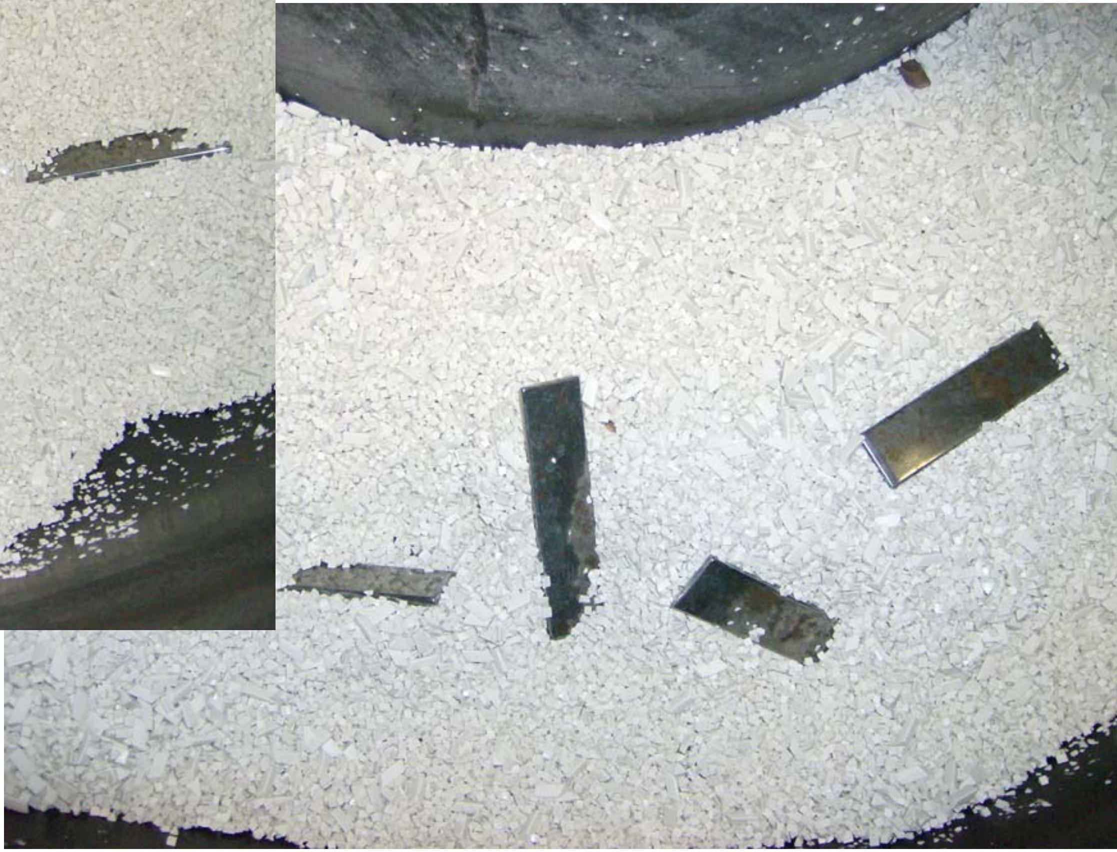
Running the distribution test

Drawing of the media bulk in the 1.16 m bowl

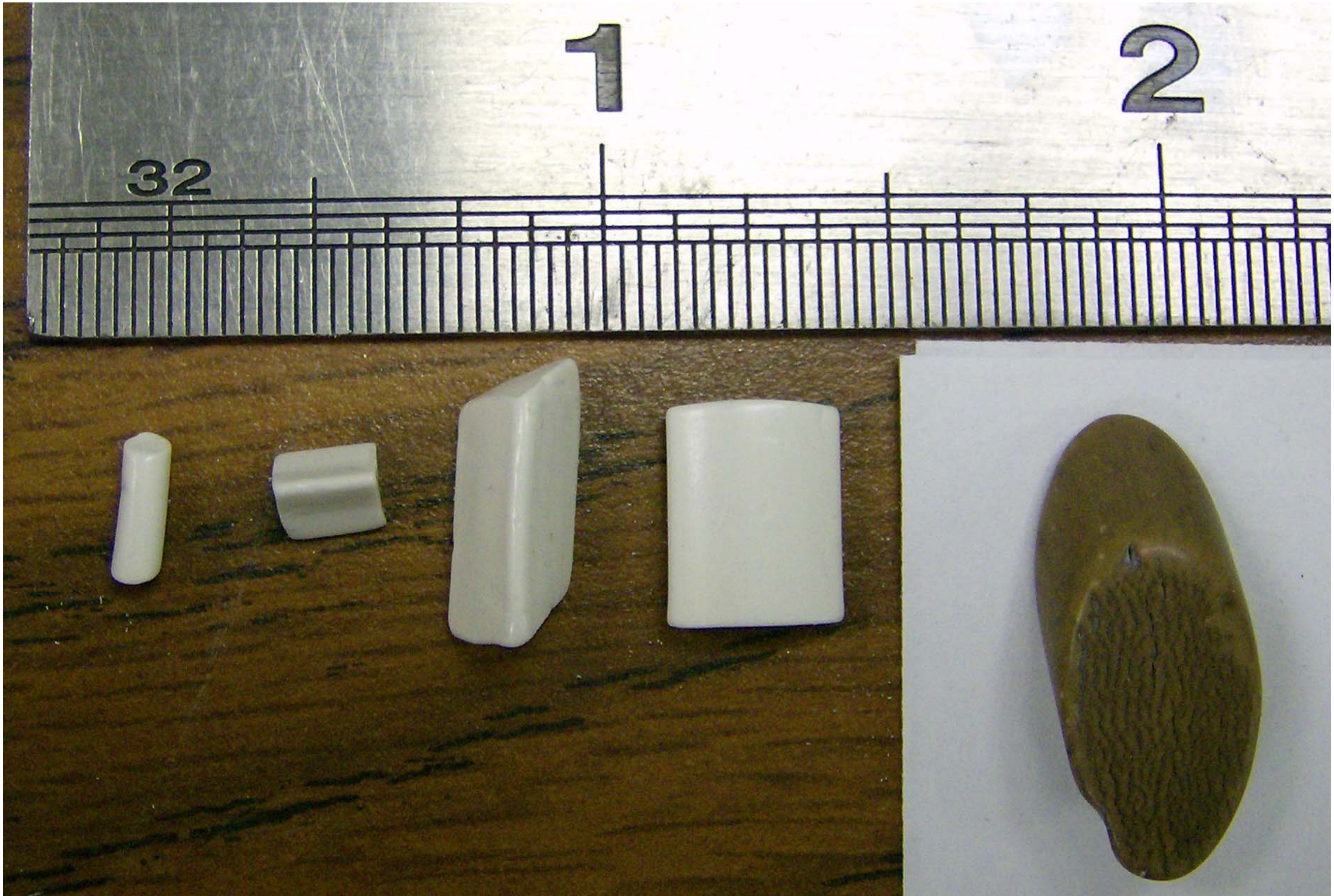


ENGINEERED SURFACES CENTER

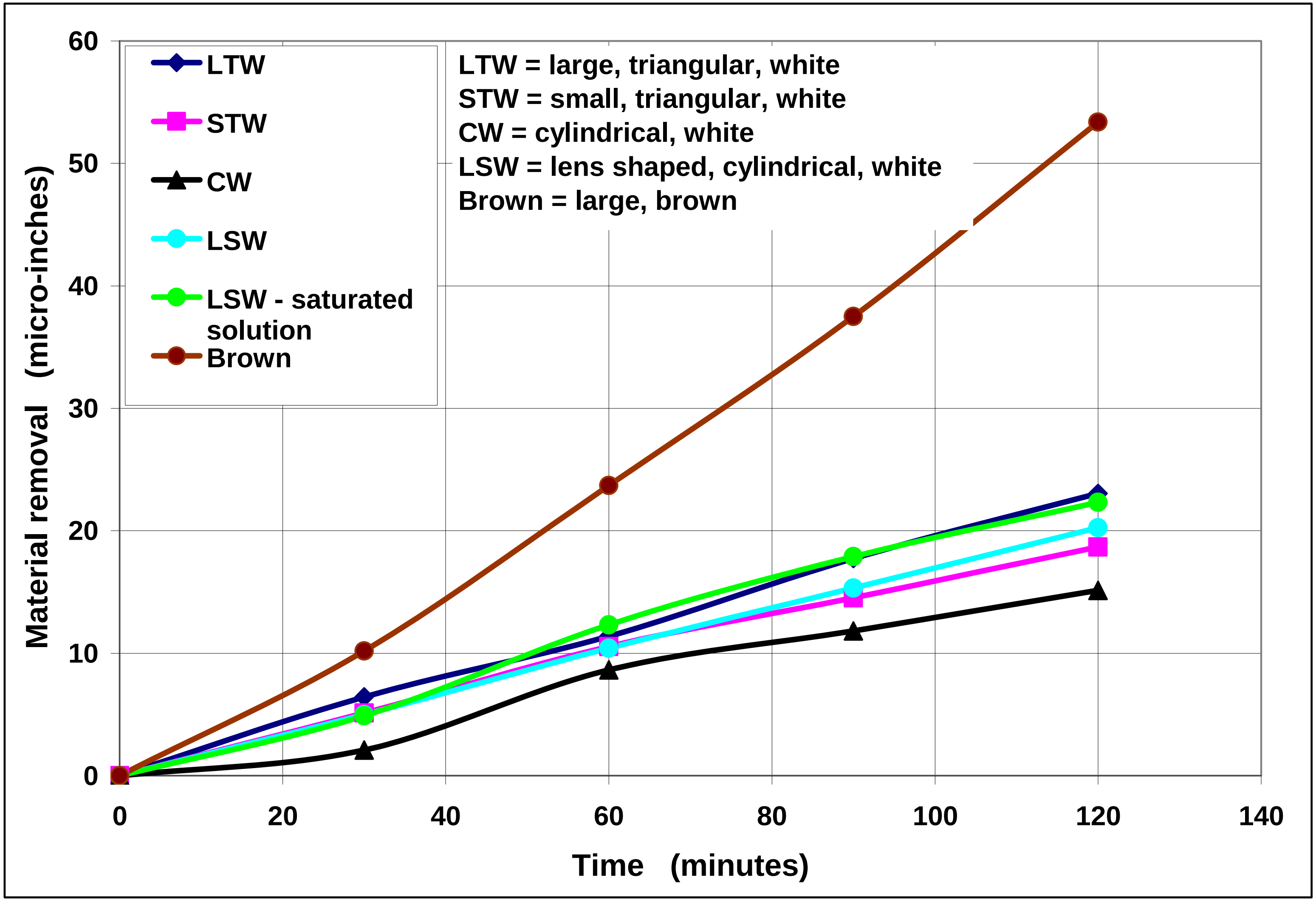
Digging out the samples and measuring the location and orientation



Different media pieces

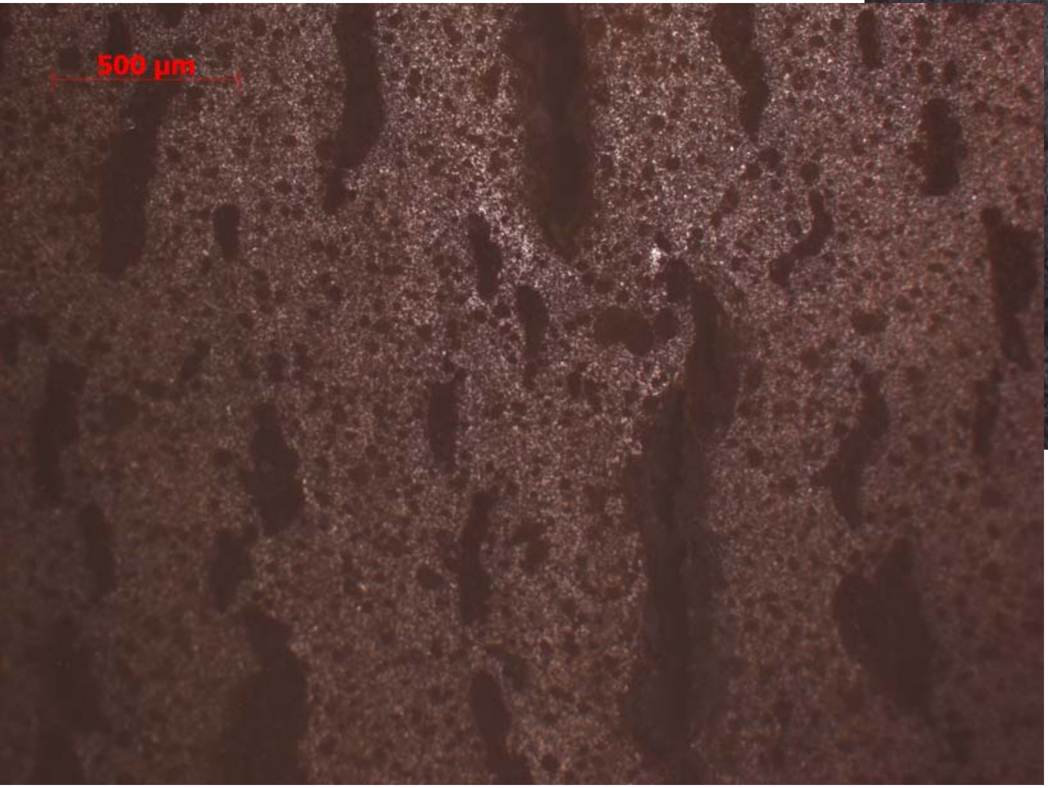


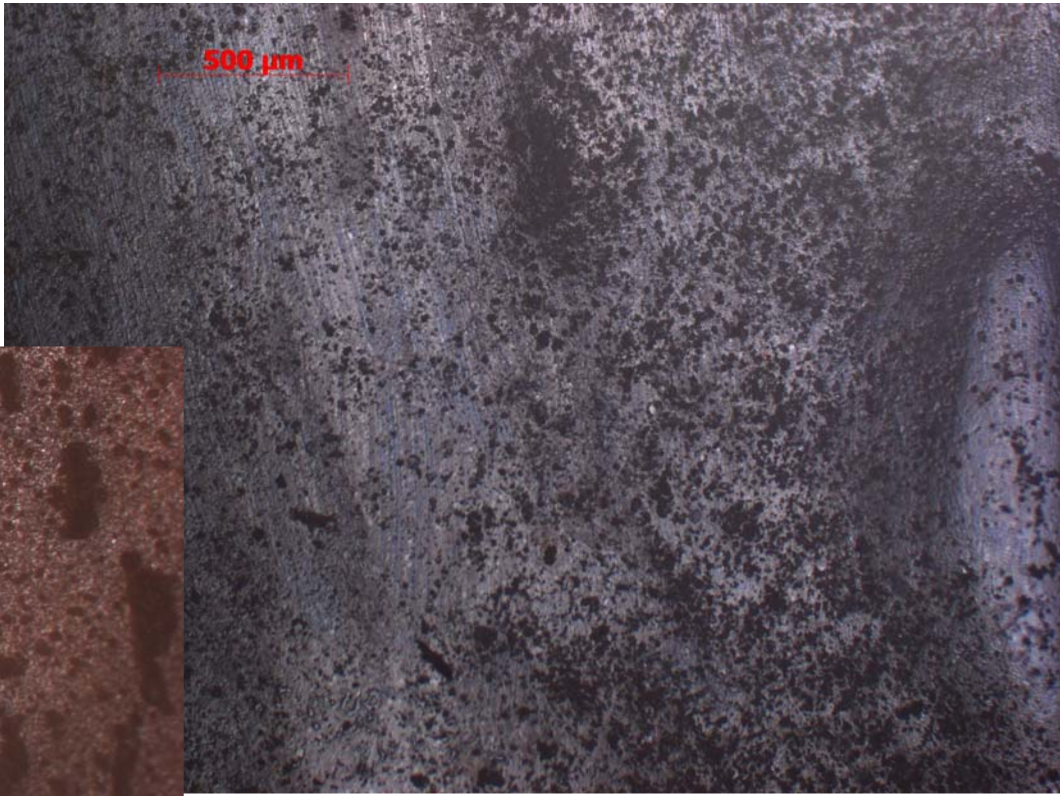
Material removal versus acid time with 0.27 M oxalic acid, 0.17 M ammonium oxalate and with different media.



ENGINEERED SURFACES CENTER

Brown media (top side)

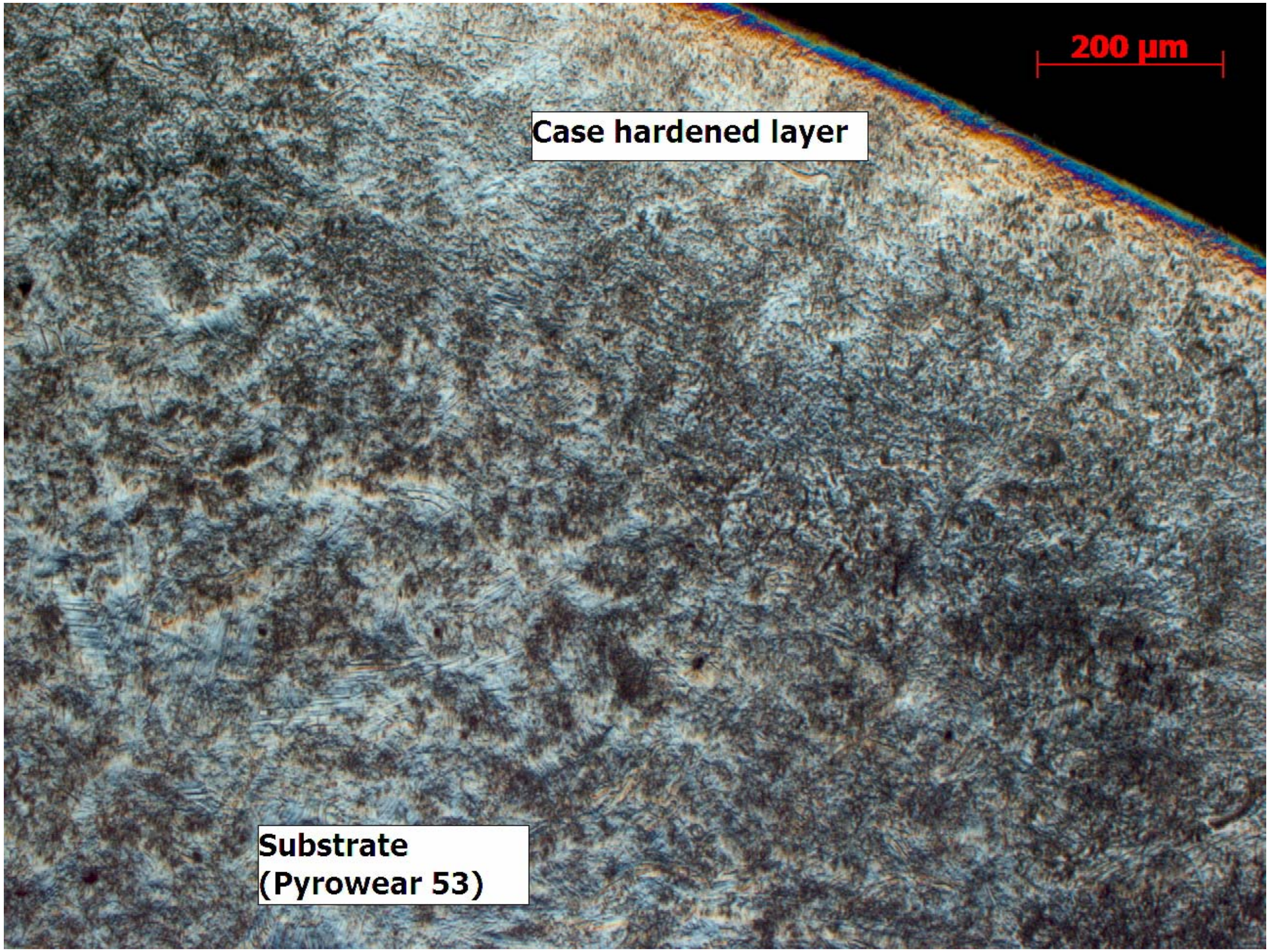




White media

Media characteristics

Media	Bulk density	Max. liquid per load (2.2 L)	2/3 Max	Area per load (2.2 L)	Water thickness
Brown	1808 g/L	60 mL	40 mL	967877 mm^2	41.3 µm
White Large Triangle	1746 g/L	53 mL	35 mL	1403172 mm^2	24.9 µm
White Small Triangle	1622 g/L	100 mL	67 mL	2545960 mm^2	26.3 µm
White Circular Cylinder	1584 g/L	104 mL	69 mL	2906367 mm^2	23.7 µm
White Lens Cylinder	1726 g/L	72 mL	48 mL	1742464 mm^2	27.5 µm



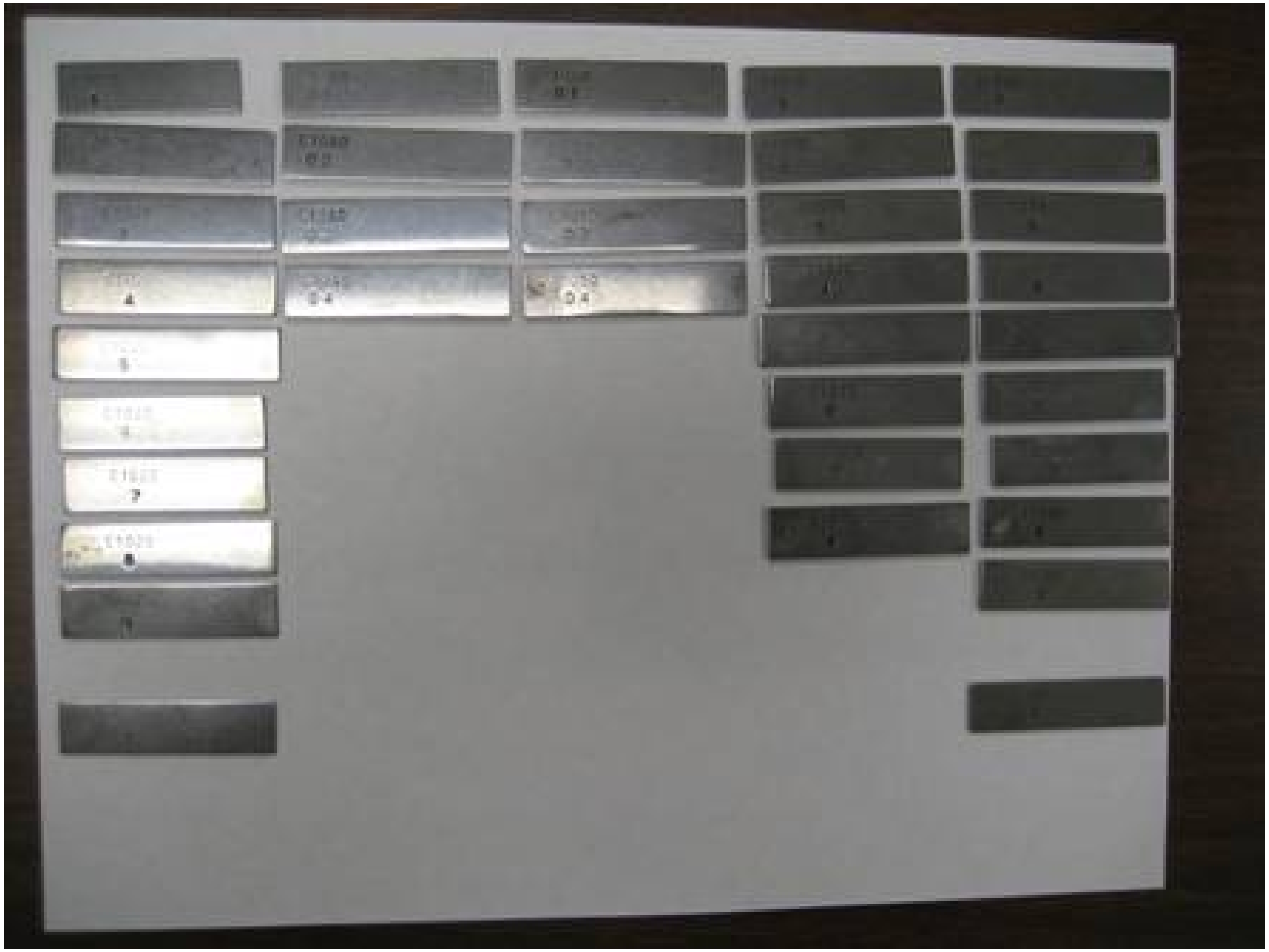
Cut Pyrowear 53™ sample with super-finished surface. The case hardened layer is smoother (Ra = 3 micro-inches (0.076 µm)) than the substrate (Ra = 7 micro-inches (0.18 µm)). CAVSF reveals the microstructure of the surface through etching.

Reasons for thermodynamic differences in the local etching rates

- Components are unevenly distributed
- Crystal size may differ
- Grain boundaries are different than the grain itself
- Failure in the crystal structure leads to tension in the lattice
- Crystal structure (martensite has a 1.7 kJ per mol higher free energy than ferrite)
- Grains are often randomly oriented. Different lattice planes are exposed during cutting which creates atoms surrounded by 6 atoms or 4 atoms or …
- Atoms in tips and edges of a crystal are only loosely connected.

ENGINEERED SURFACES CENTER

C 1020 C 1040 C 1050 C 1075 C 1095

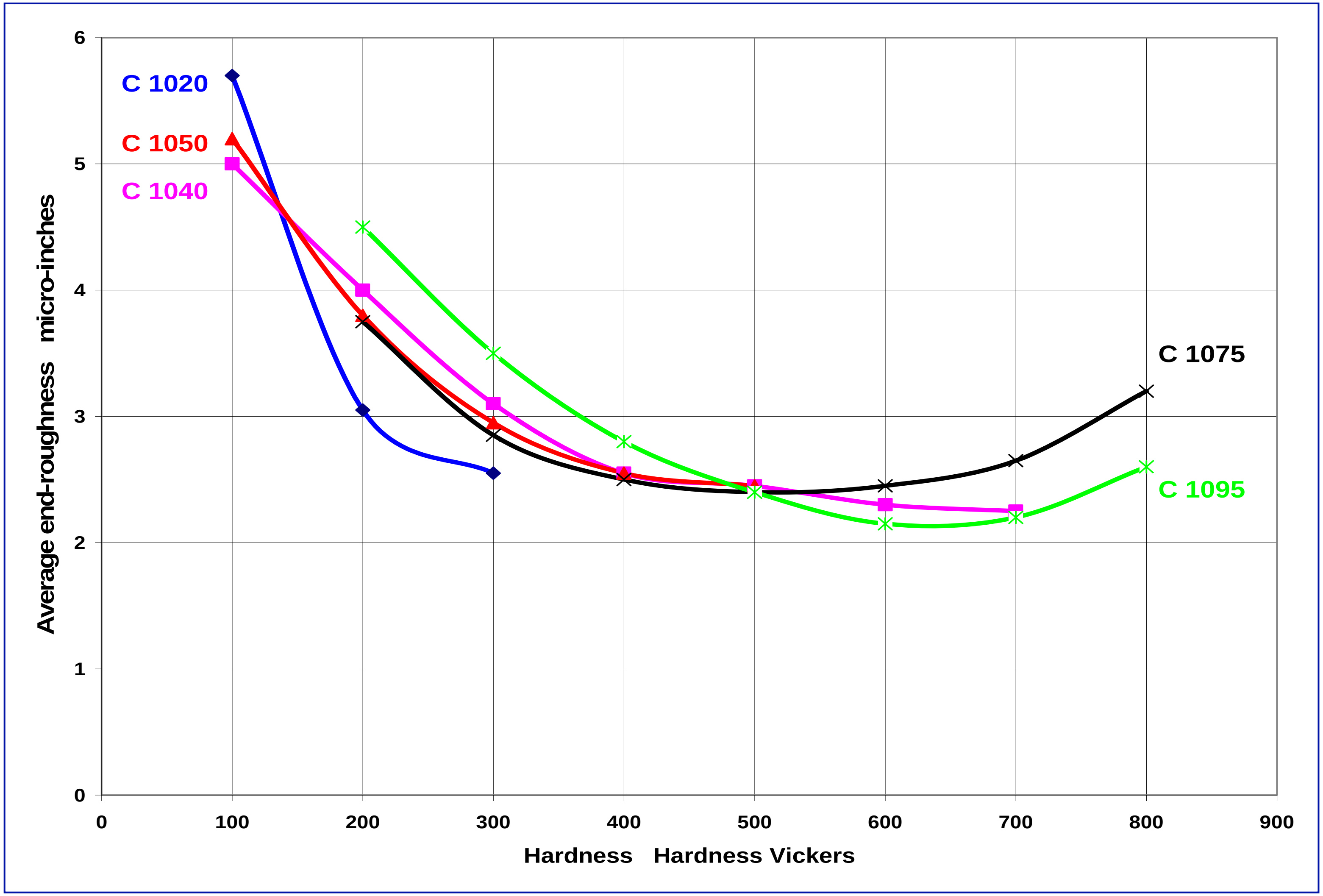


Tested carbon steels

Used heat treatments:

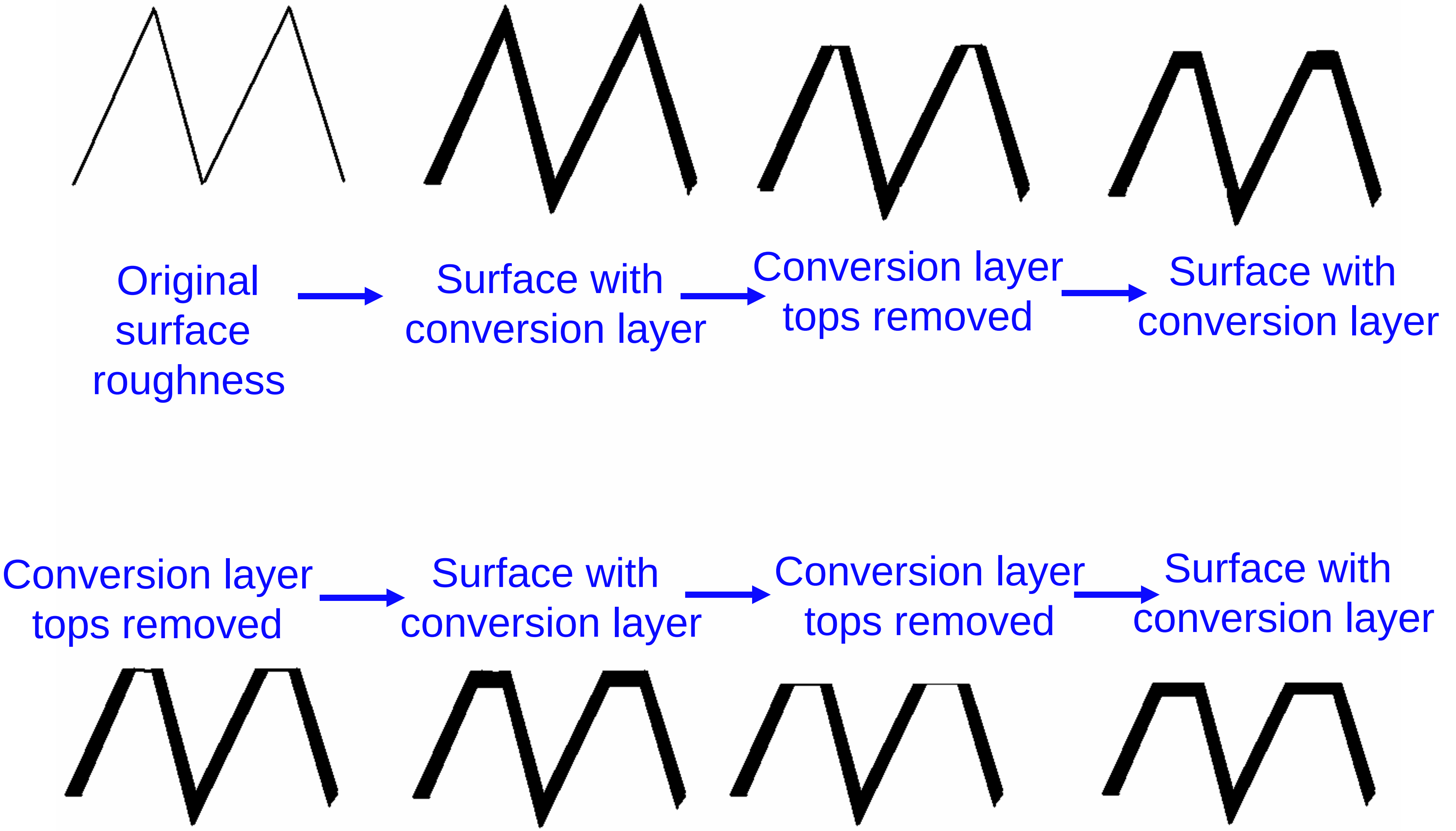
As received (annealed)
Air cooled
Cooled between plates
Cooled with wet towels
Water quenched (Wq)
Wq + heat treatm. 1
Wq + heat treatm. 2
Wq + heat treatm. 3
Annealed
Annealed (diff. temp.)
Heat treatment not defined

Carbon steel test samples with different carbon contents and different heat treatments to create different hardnesses and a variety of grains (ferrite, cementite, pearlite, bainite, martensite, retained austenite …)



Average end-roughness versus hardness for C-steels with different carbon contents and heat treatments.

Mechanism of the CAVSF



Possible chemical reactions during acid treatment

(1) $2\ H^{+}_{(aq)} + Fe_{(s)} \rightarrow Fe^{++}_{(aq)} + H_{2(g)}$

(2) $Fe^{++}_{(aq)} + 2\ H_2O \rightarrow Fe(OH)_{2(s)} + 2\ H^{+}_{(aq)}$

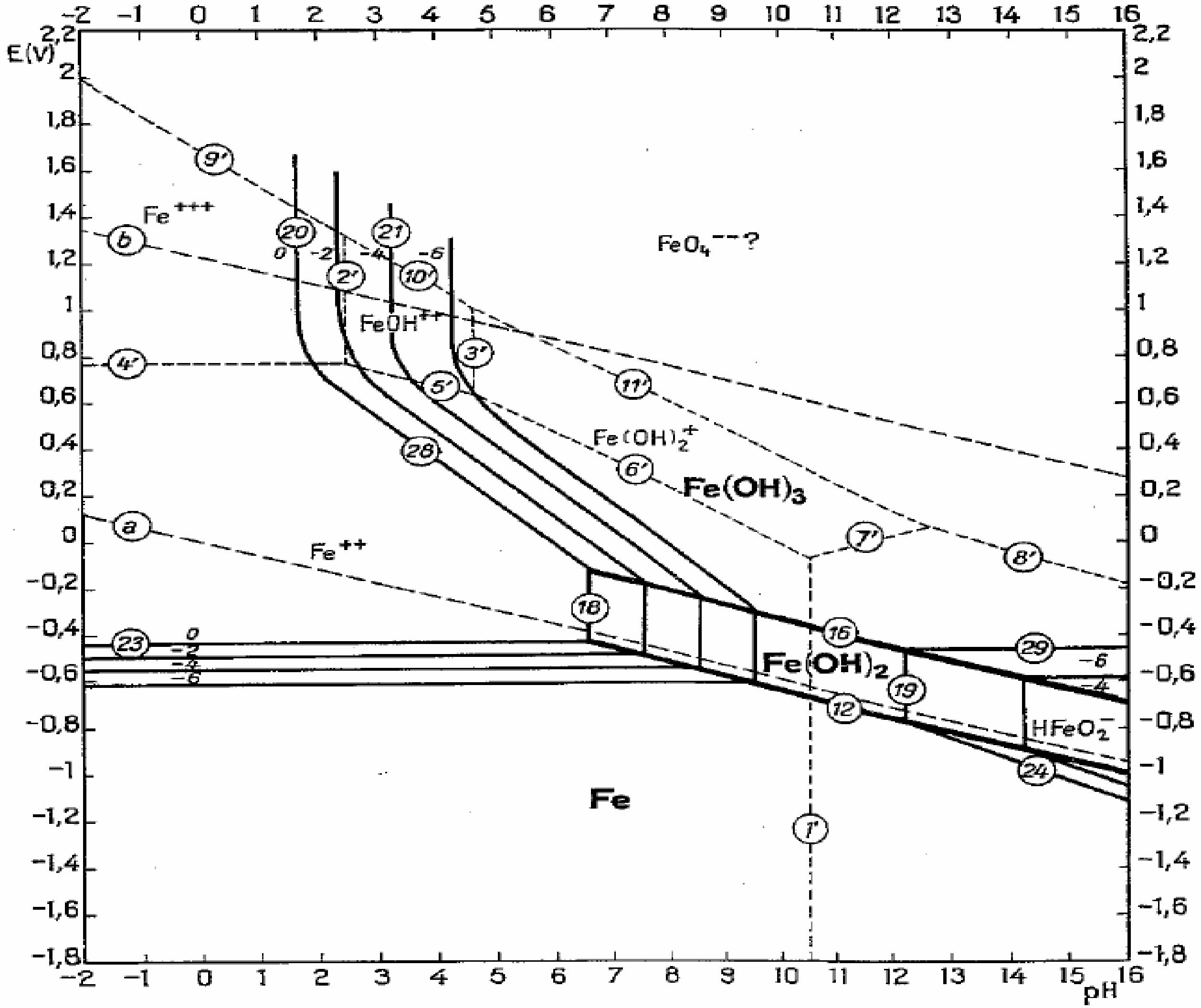
(3) $4\ Fe^{++}_{(aq)} + O_2 + 2\ H_2O \rightarrow 4\ Fe^{+++}_{(aq)} + 4\ OH^{-}$

(4) $3\ Fe^{++}_{(aq)} + 3\ (COOH)_{2(aq)} \rightarrow 3\ Fe(COO)_{2(s)} + 6\ H^{+}_{(aq)}$

(5) $2\ Fe^{+++}_{(aq)} + Fe_{(s)} \rightarrow 3\ Fe^{++}_{(aq)}$

(4+5) $2\ Fe^{+++}_{(aq)} + Fe_{(s)} + 3\ (COOH)_{2(aq)} \rightarrow 3\ Fe(COO)_{2(s)} + 6\ H^{+}_{(aq)}$

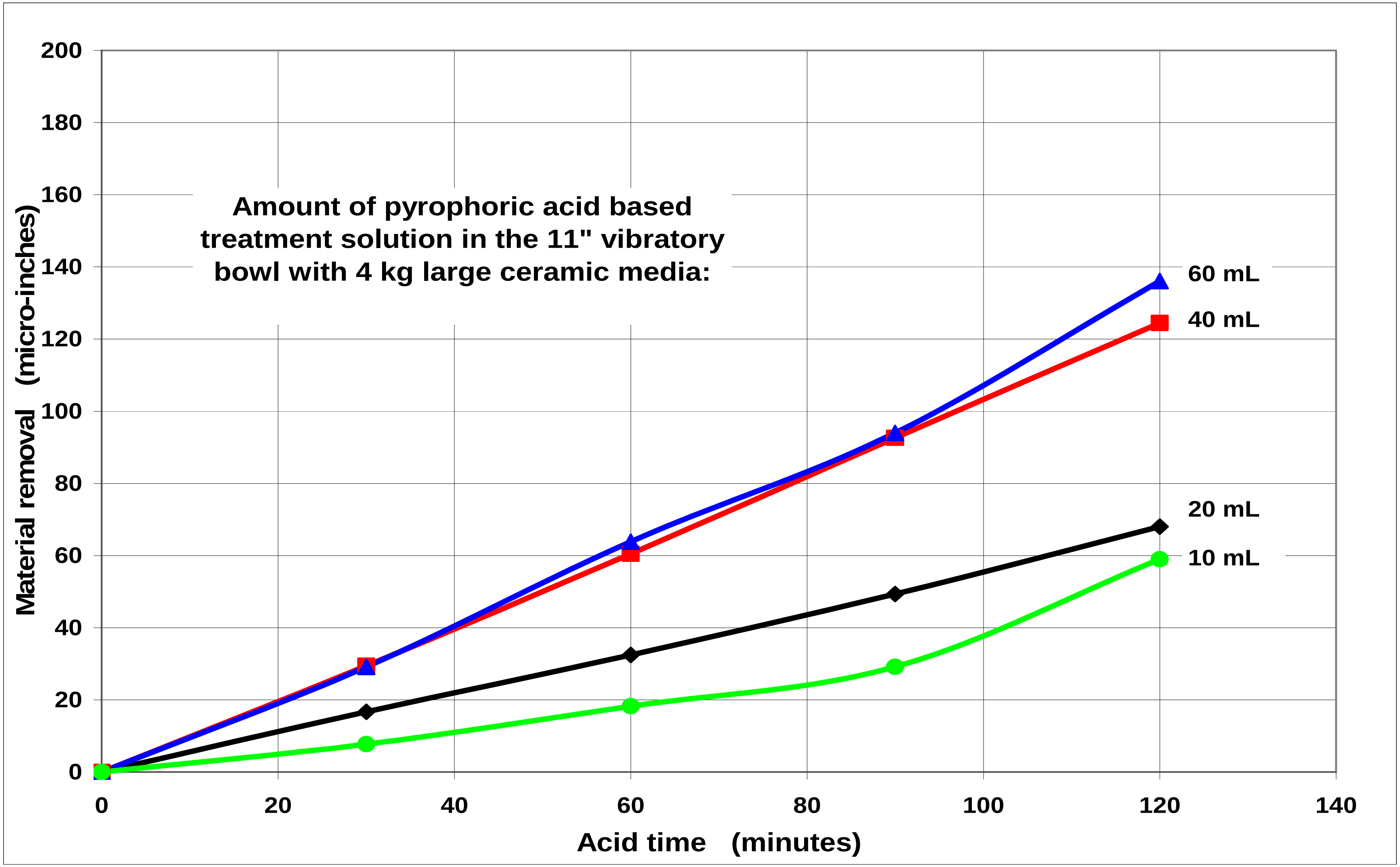
Potential – pH equilibrium diagram



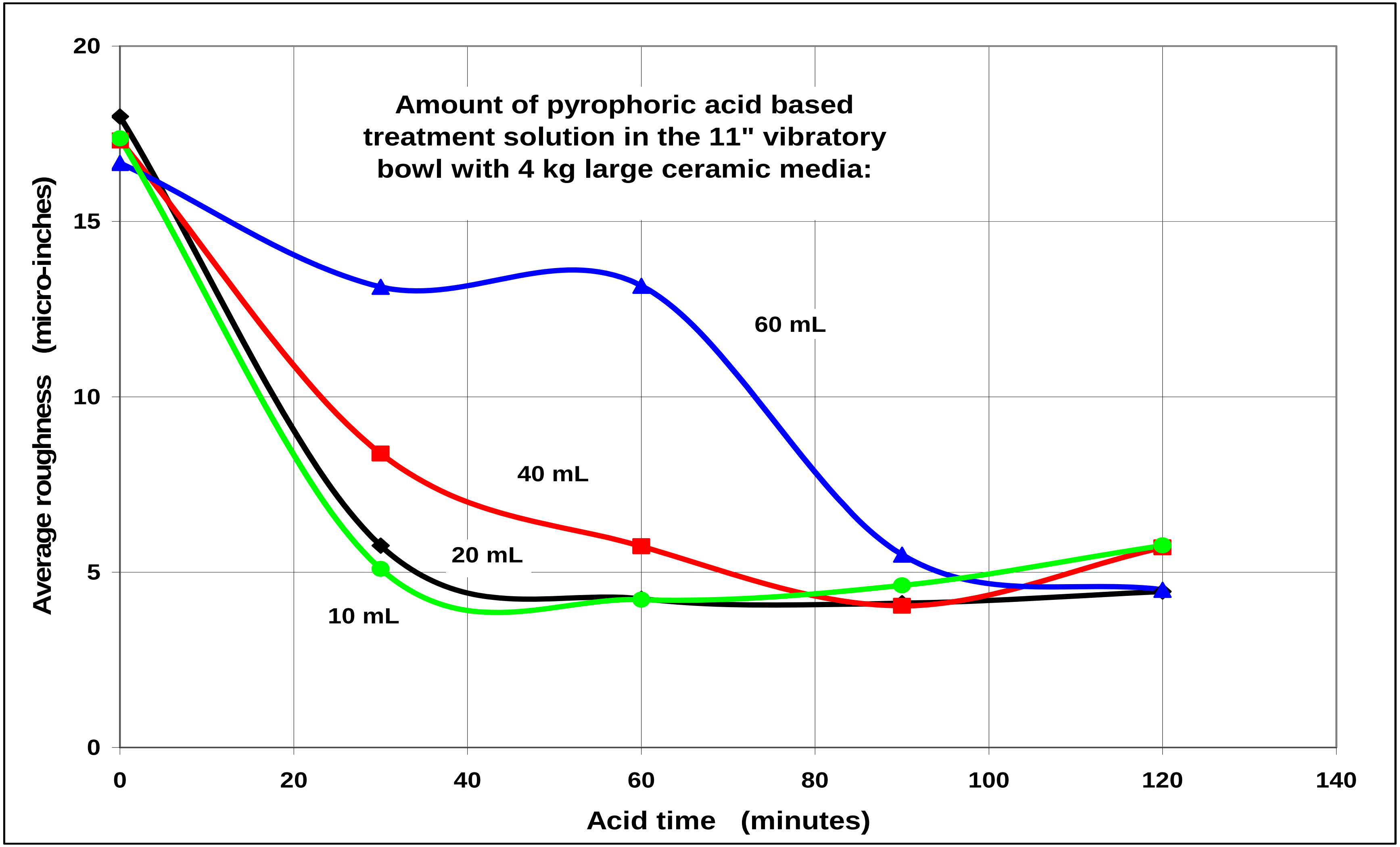
System:
Iron – Water
at 25 deg. C
(considering
as solid
substances only
Fe, $Fe(OH)_2$,
and $Fe(OH)_3$)

From M. Pourbaix
and N. de Zoubov

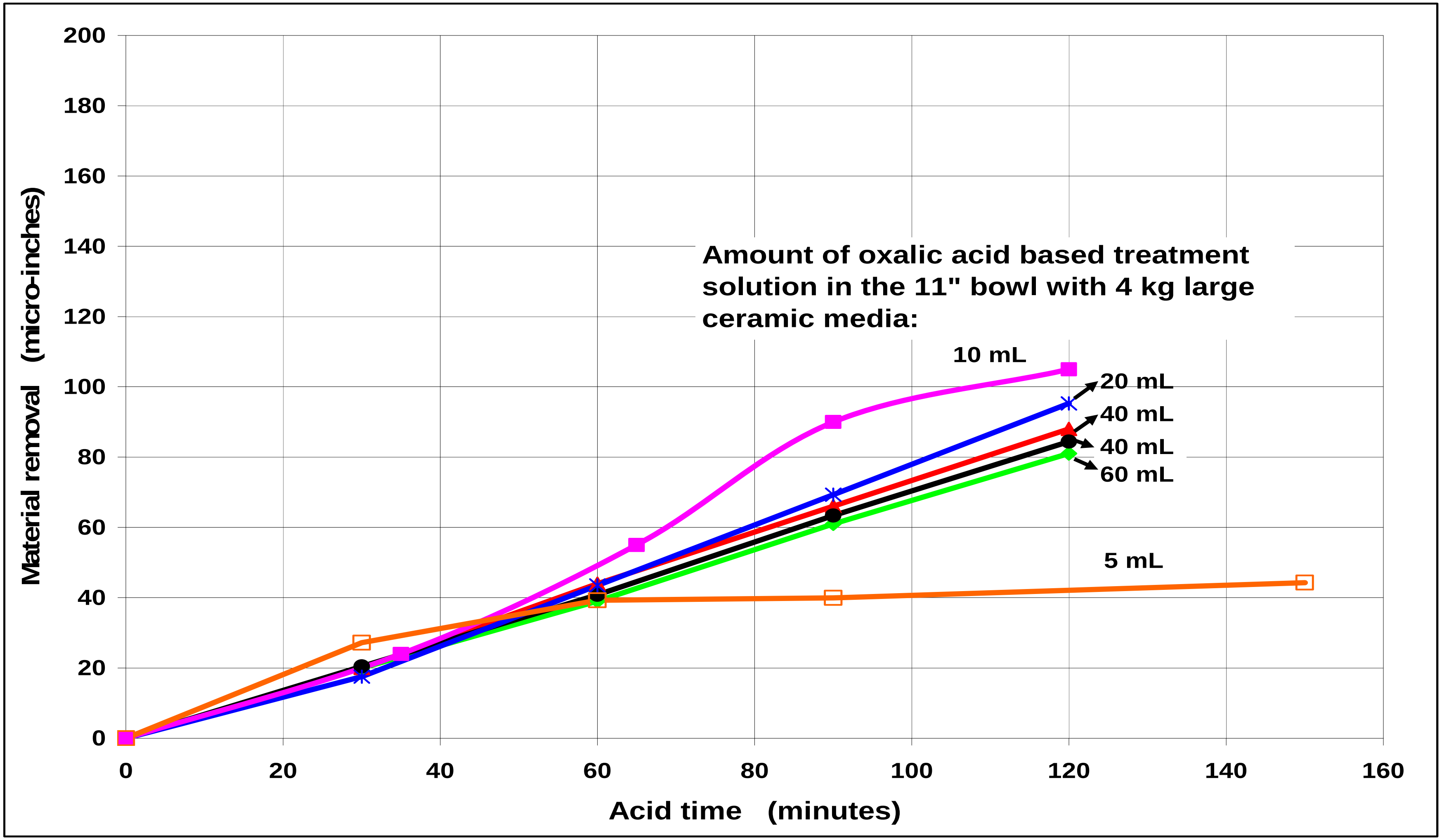
Material removal versus acid time for different amounts of pyrophosphoric acid.



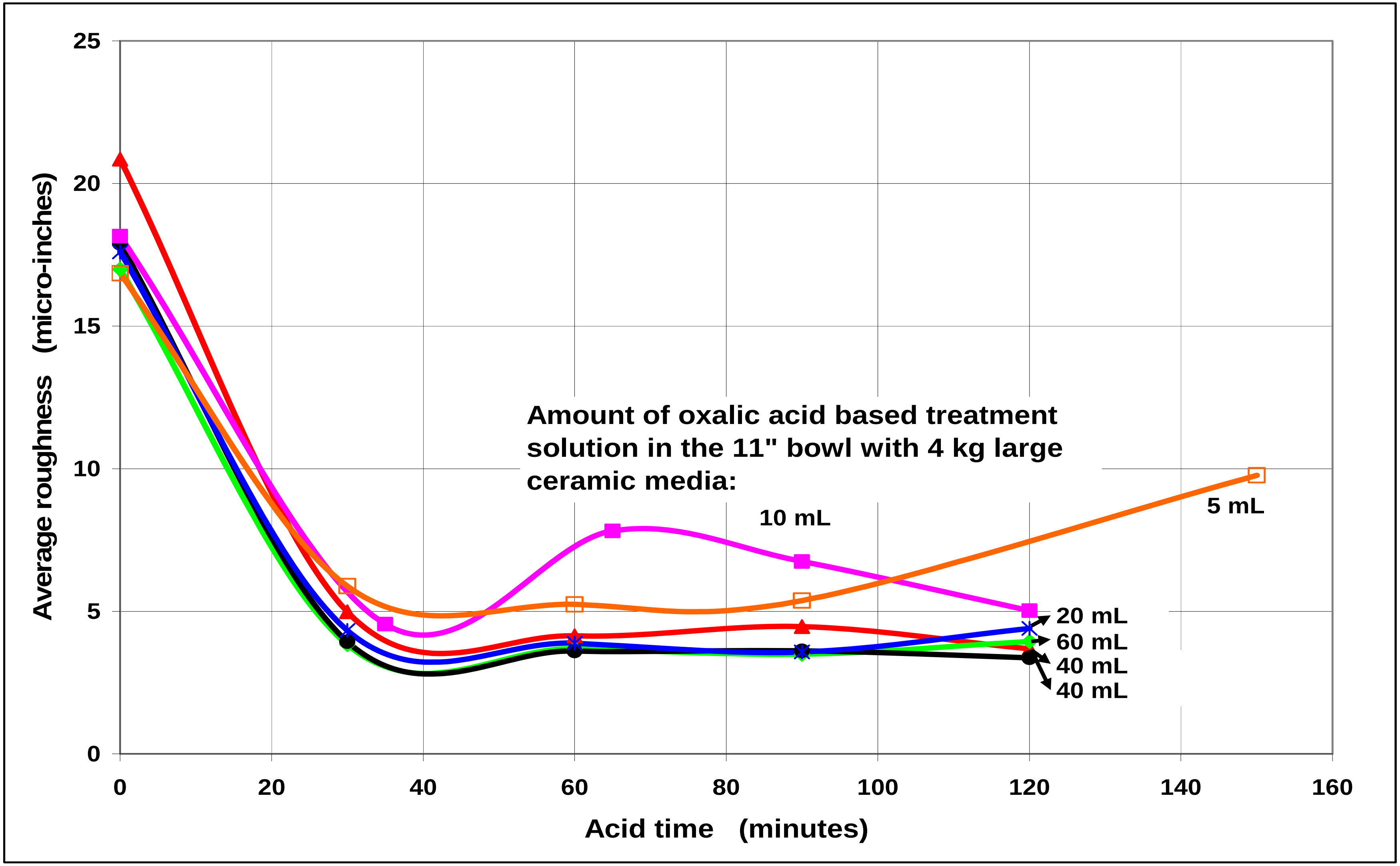
Average roughness versus acid time for different amounts of pyrophosphoric acid.



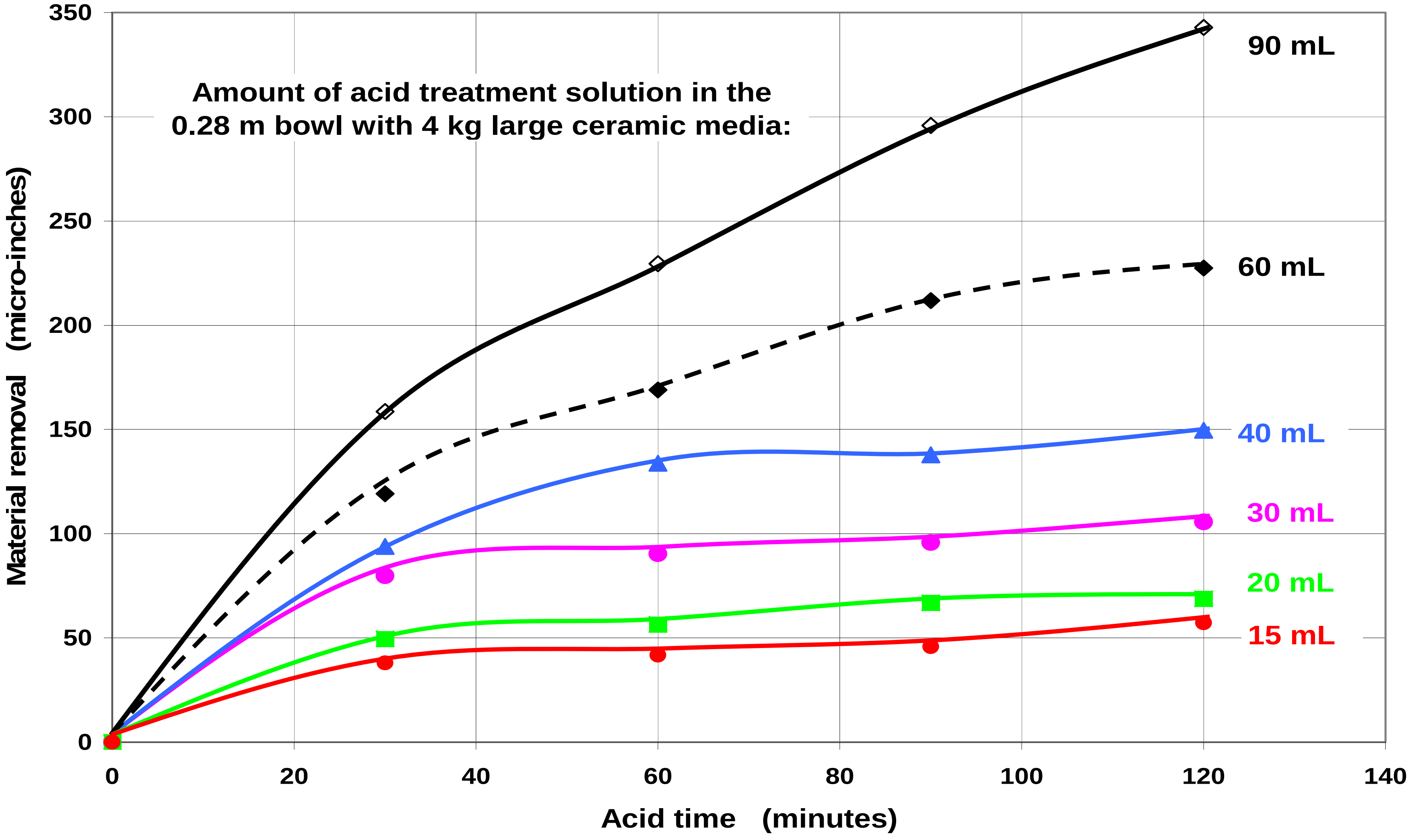
Material removal versus acid time for different amounts of oxalic acid.



Average roughness versus acid time for different amounts of oxalic acid.

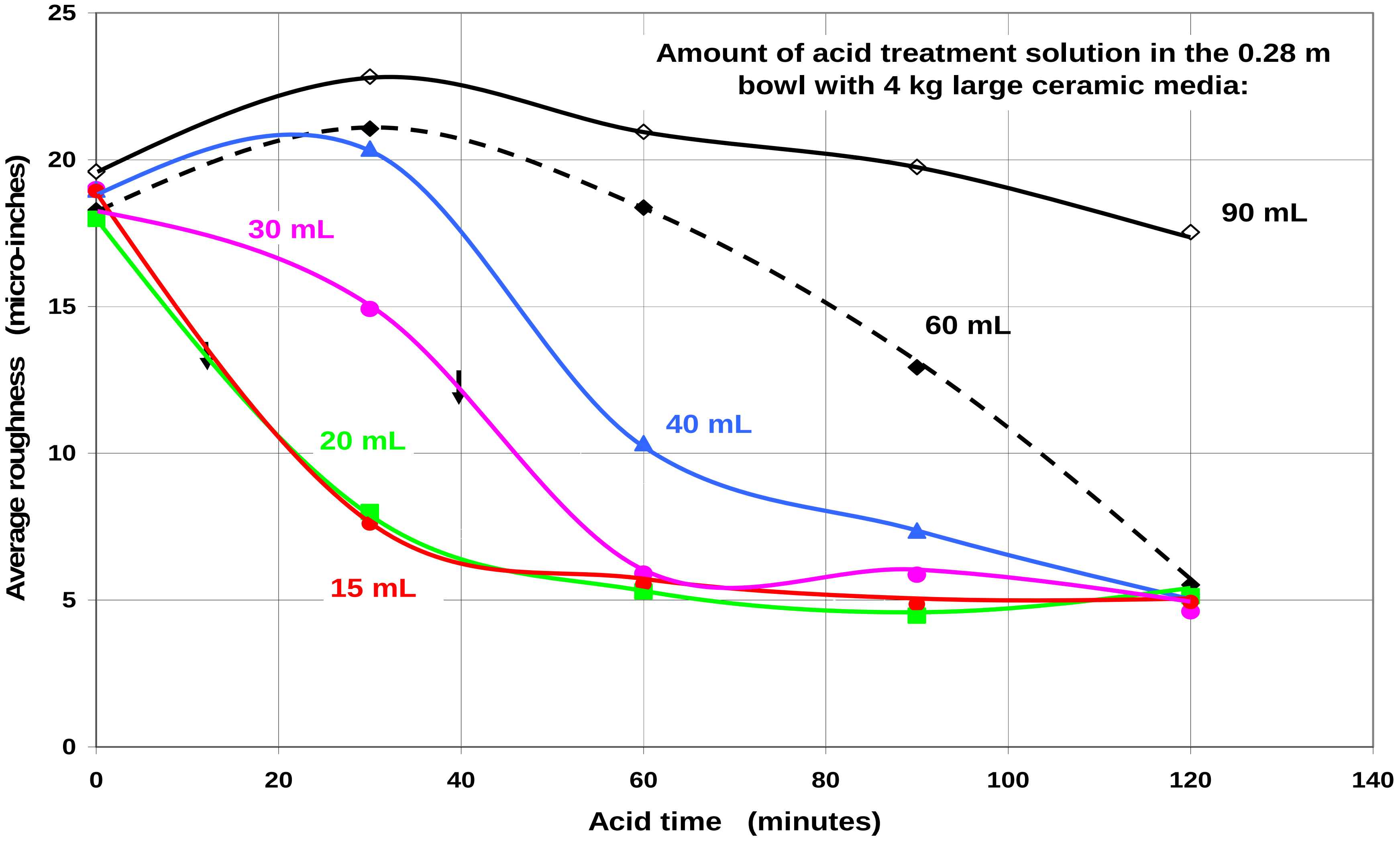


Material removal versus acid time for 0.2 M sodium bisulfate, 0.2 M iron (II), 0.2 M iron (III) (sulfate based).

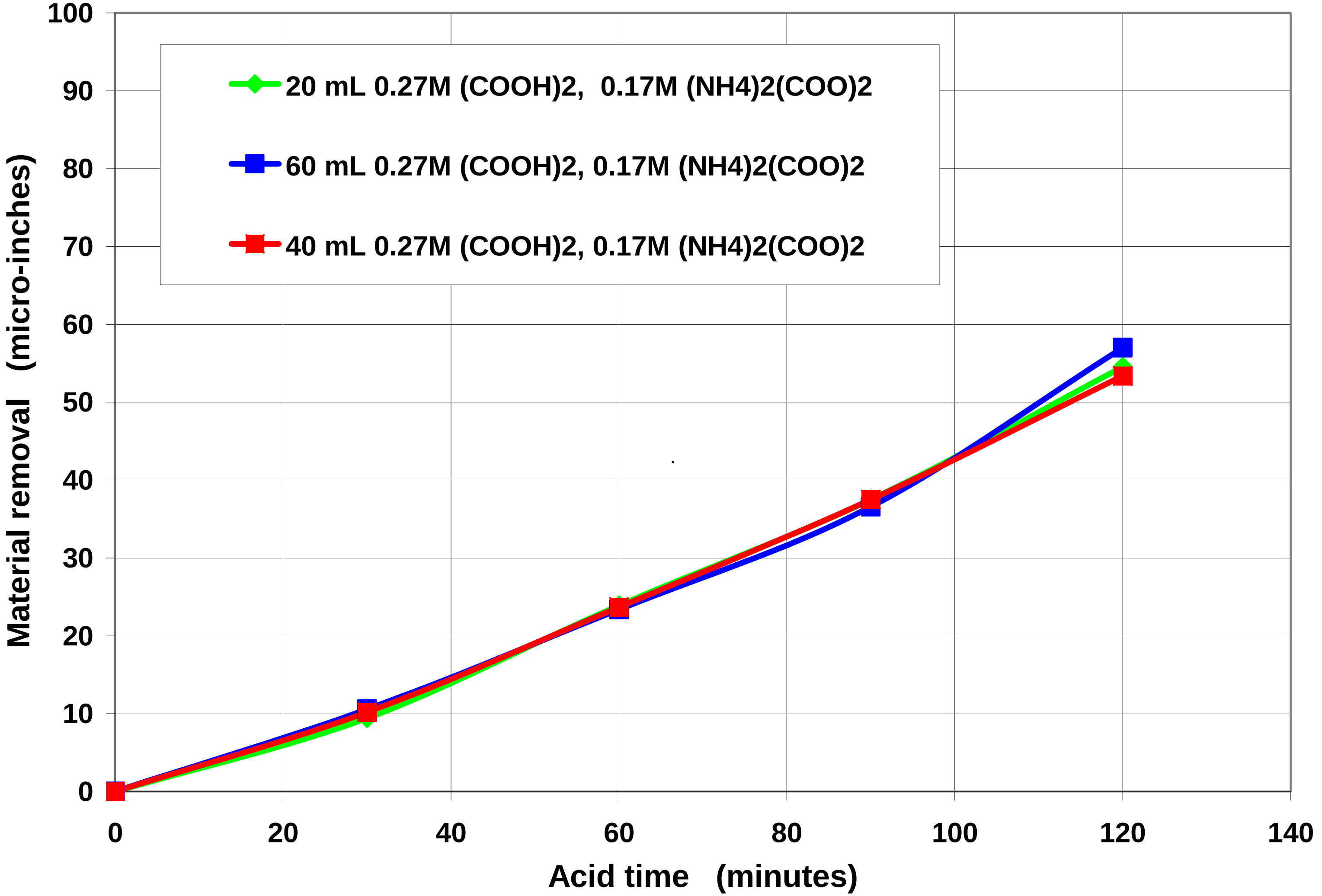


ENGINEERED SURFACES CENTER

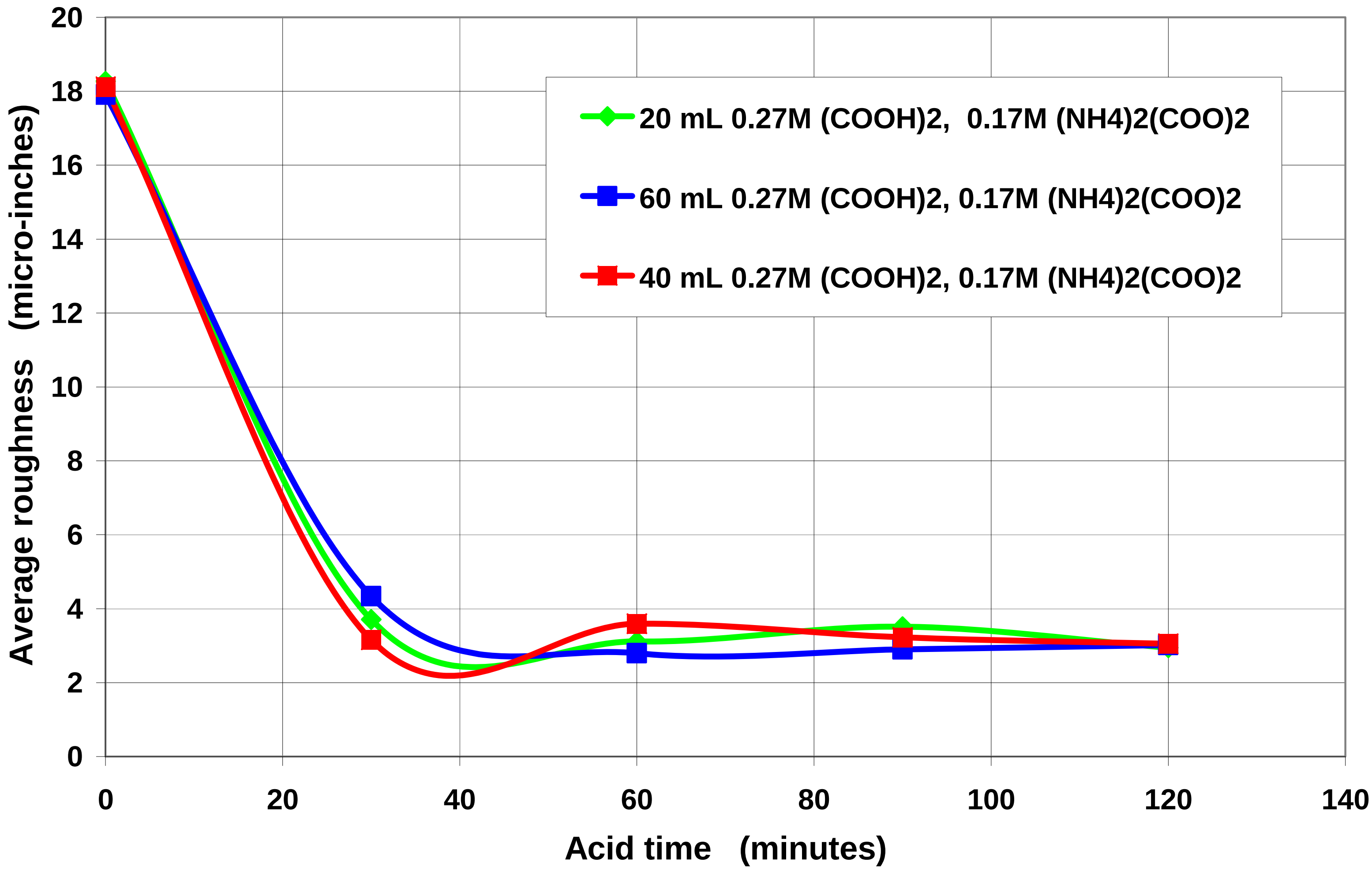
Average roughness versus acid time for 0.2 M sodium bisulfate, 0.2 M iron (II), 0.2 M iron (III) (sulfate based).



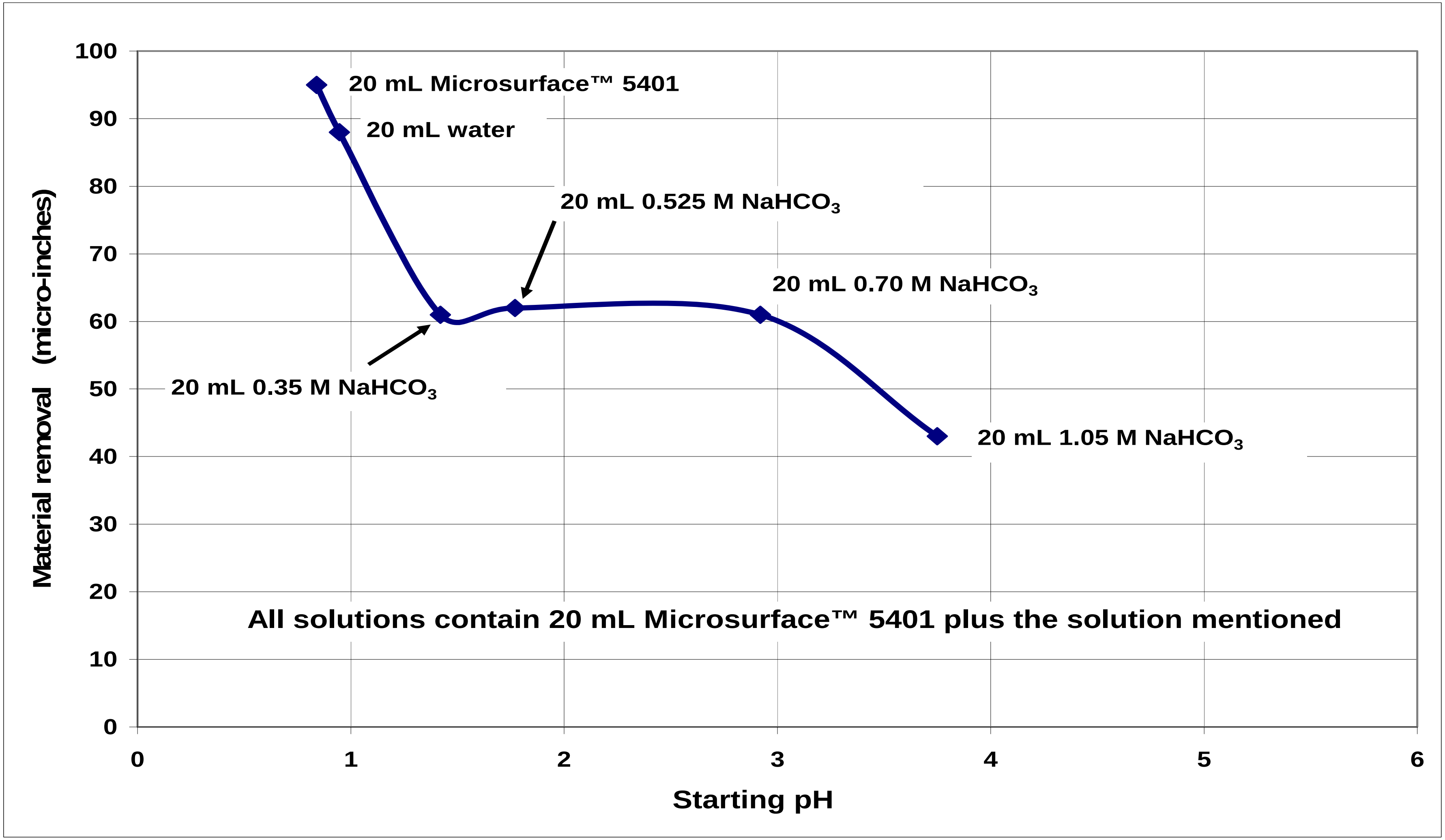
Material removal versus acid time for various amounts of a solution containing 0.27 M oxalic acid, 0.17 M ammonium oxalate



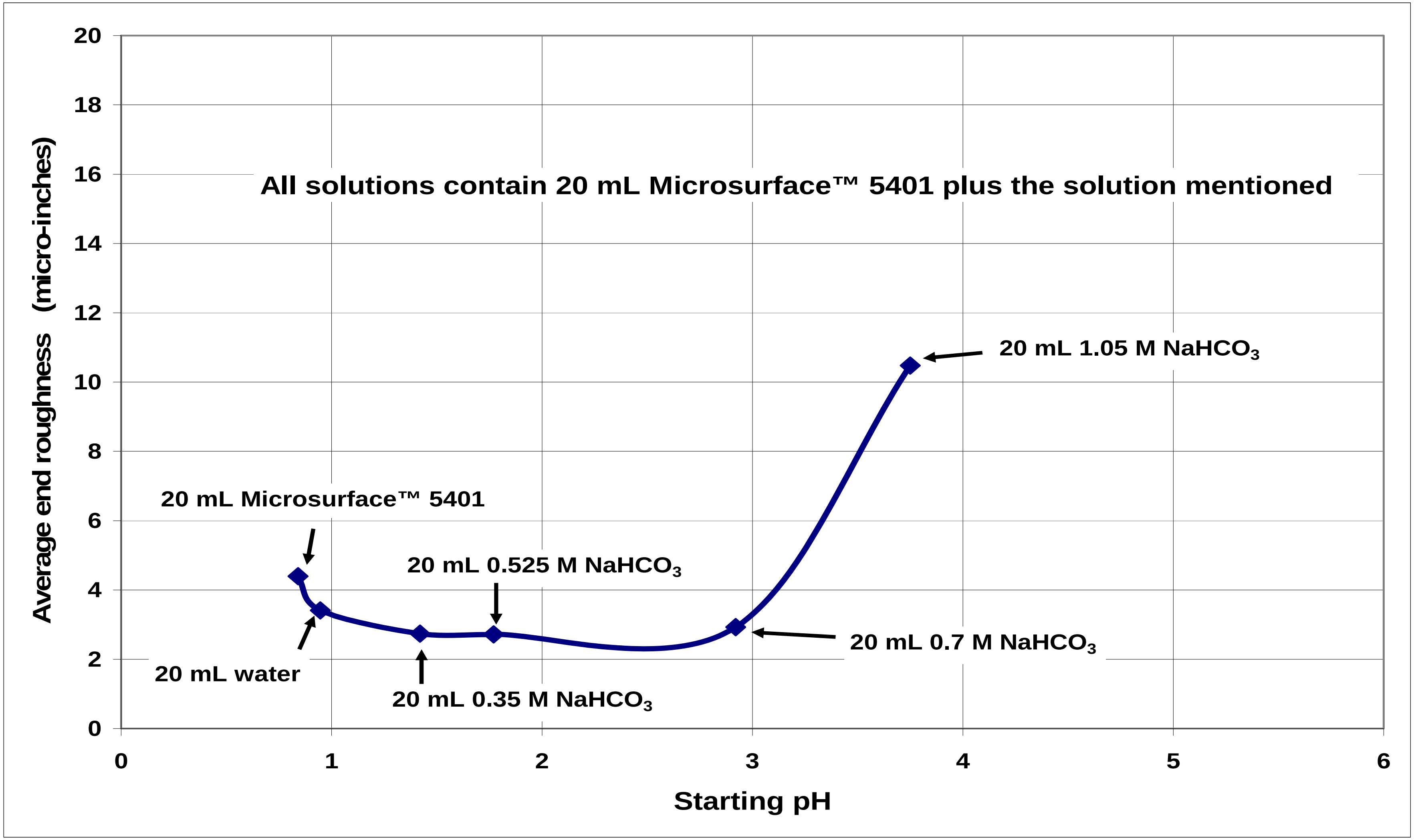
Average roughness versus acid time for various amounts of a solution containing 0.27 M oxalic acid, 0.17 M ammonium oxalate



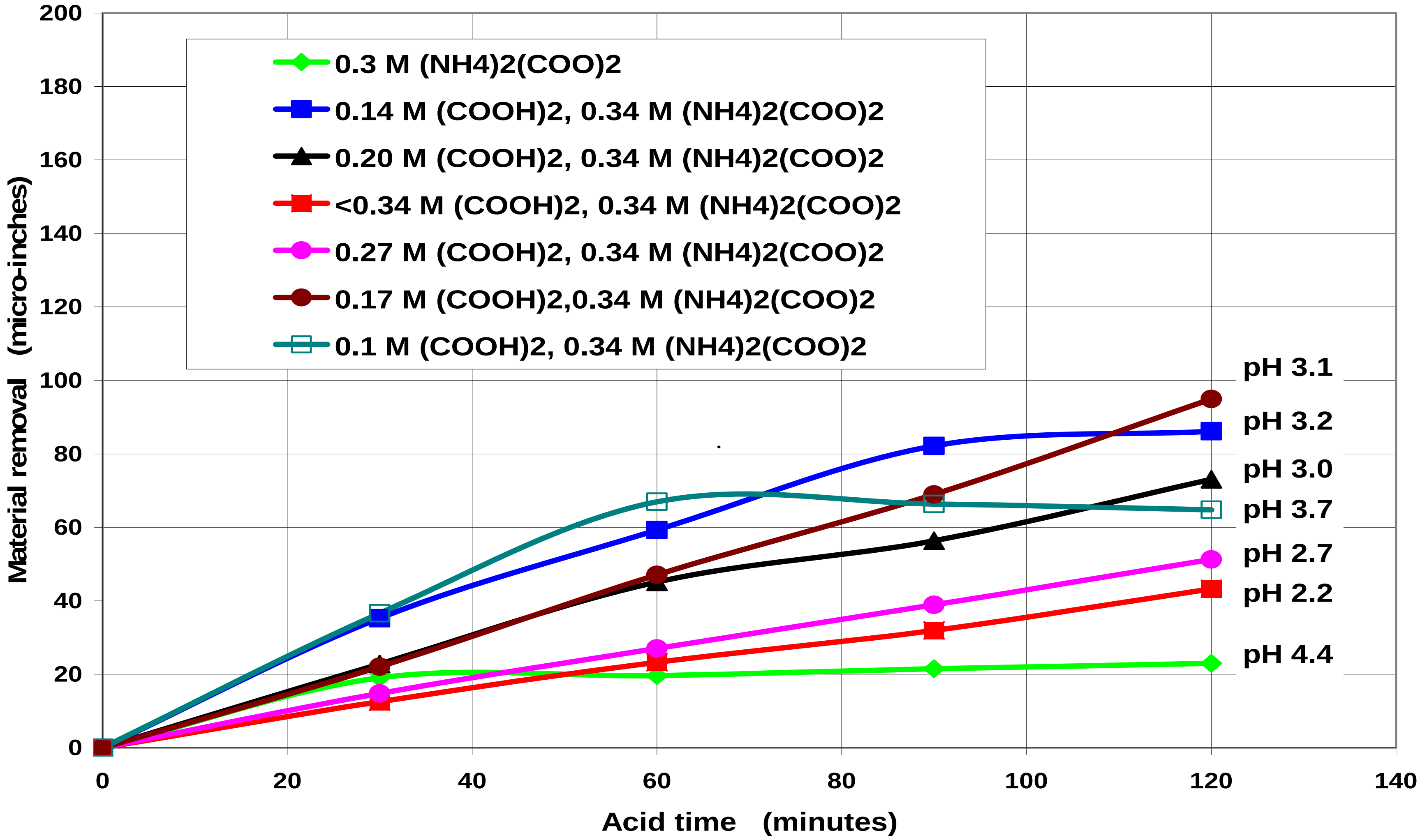
Material removal versus starting pH for different mixtures of oxalic acid based treatment solutions.



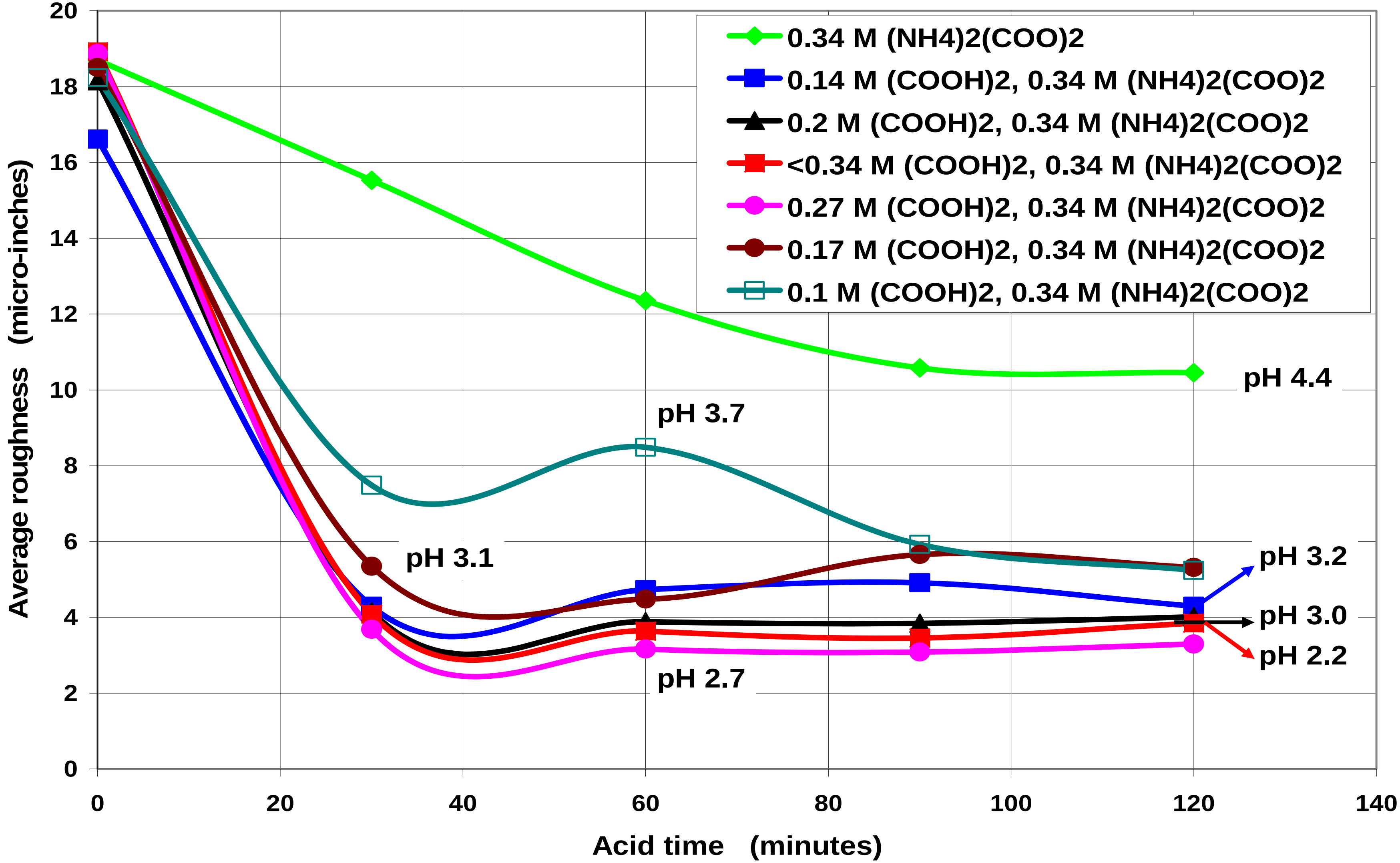
Average roughness versus starting pH for different mixtures of oxalic acid based treatment solutions.



Material removal versus acid time for ammonium oxalate solutions with oxalic acid.

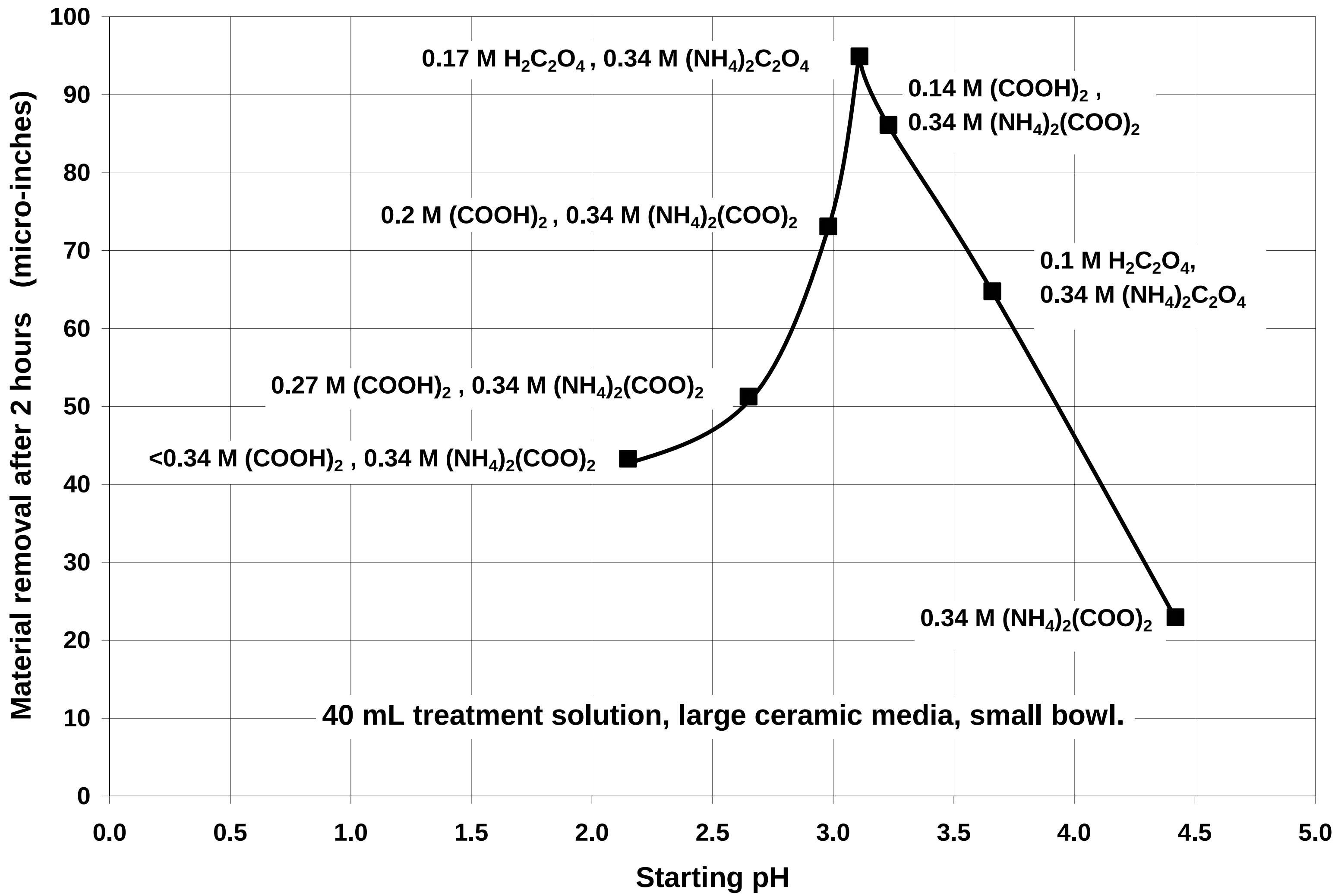


Average roughness versus acid time for ammonium oxalate solutions with oxalic acid.

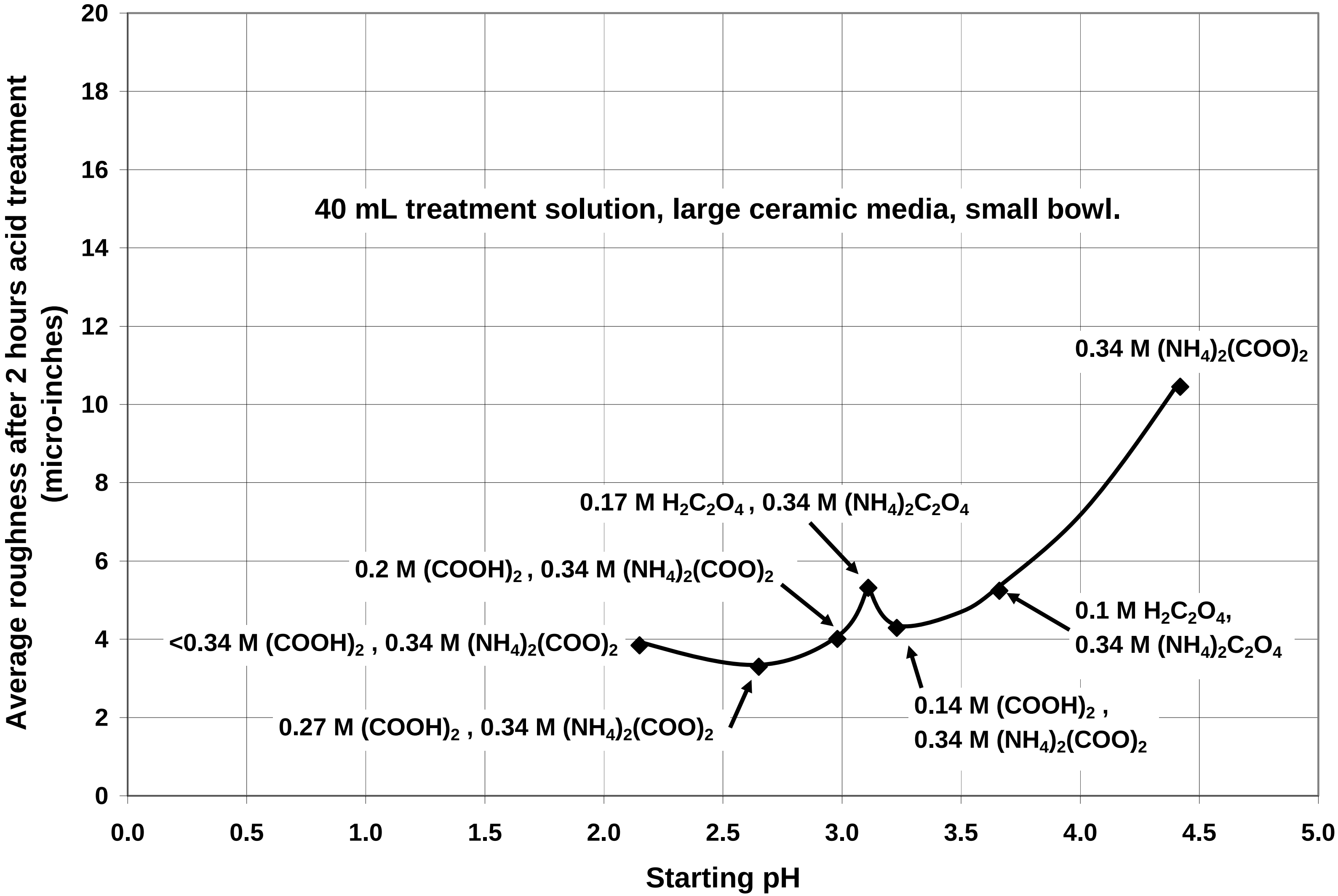


ENGINEERED SURFACES CENTER

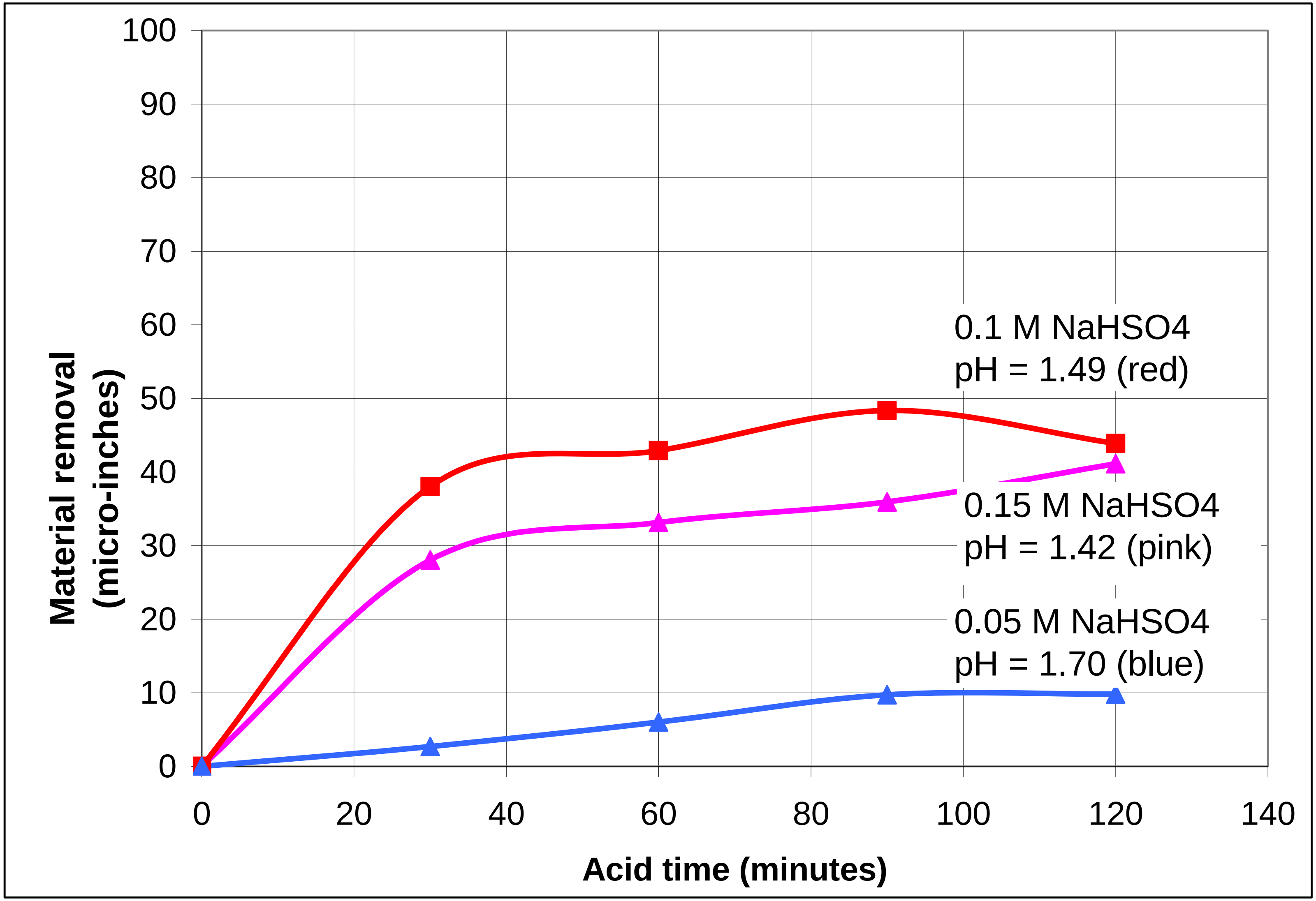
Material removal versus starting pH for 0.34 M ammonium oxalate solutions with oxalic acid.



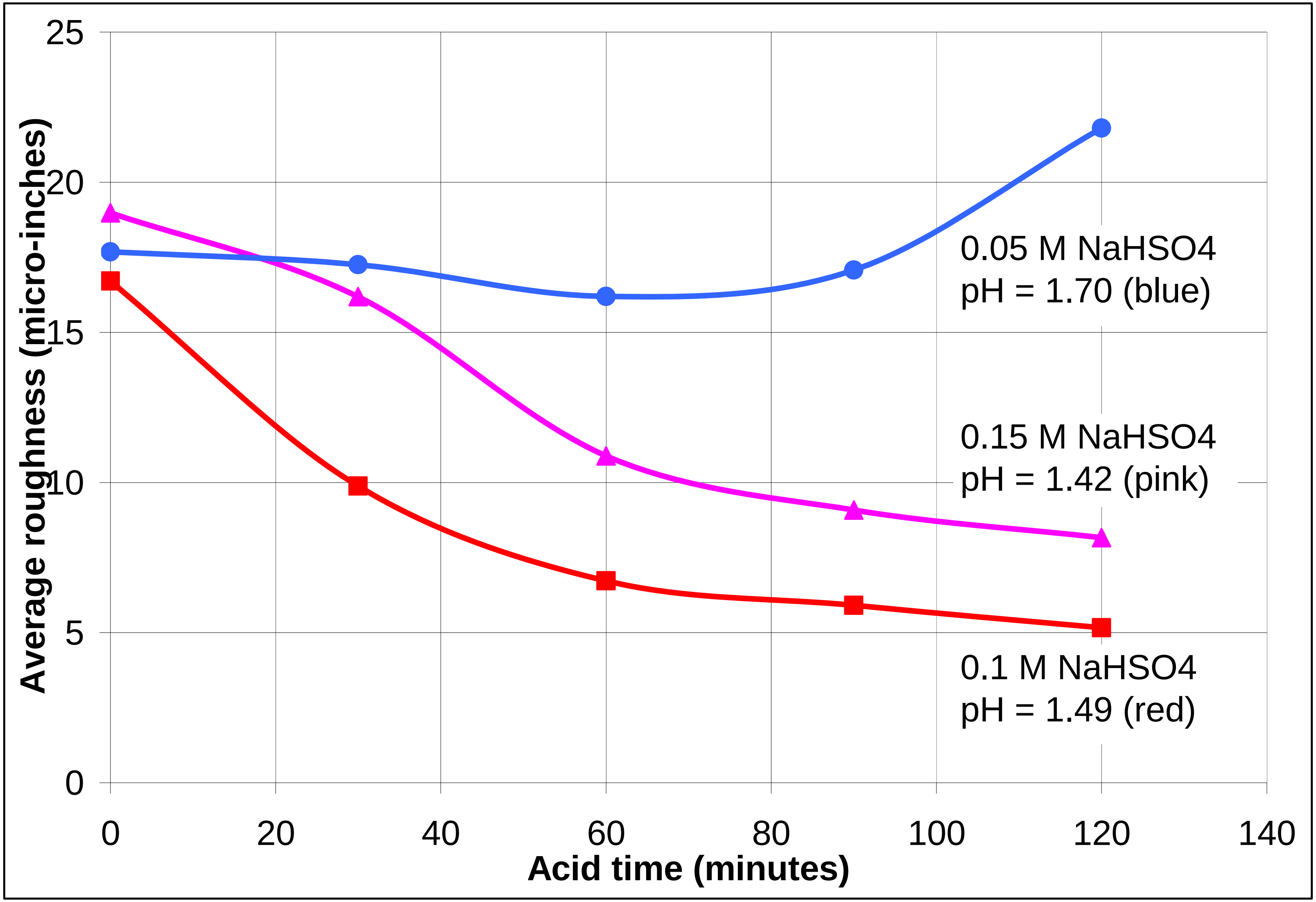
Average end roughness versus starting pH for 0.34 M ammonium oxalate solutions with oxalic acid.



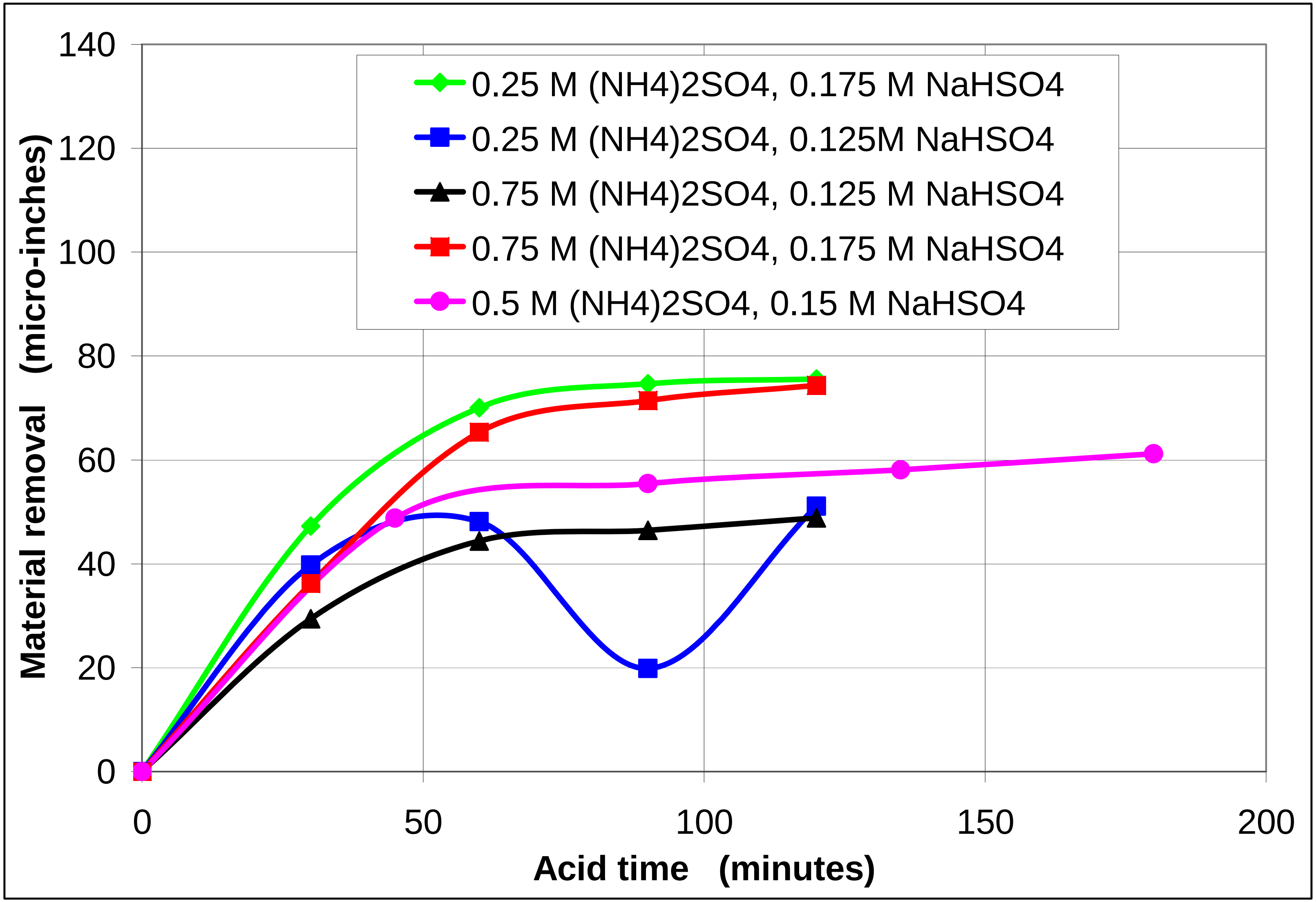
Material removed from strip steel samples vs. acid time for different sodium bisulfate solutions.



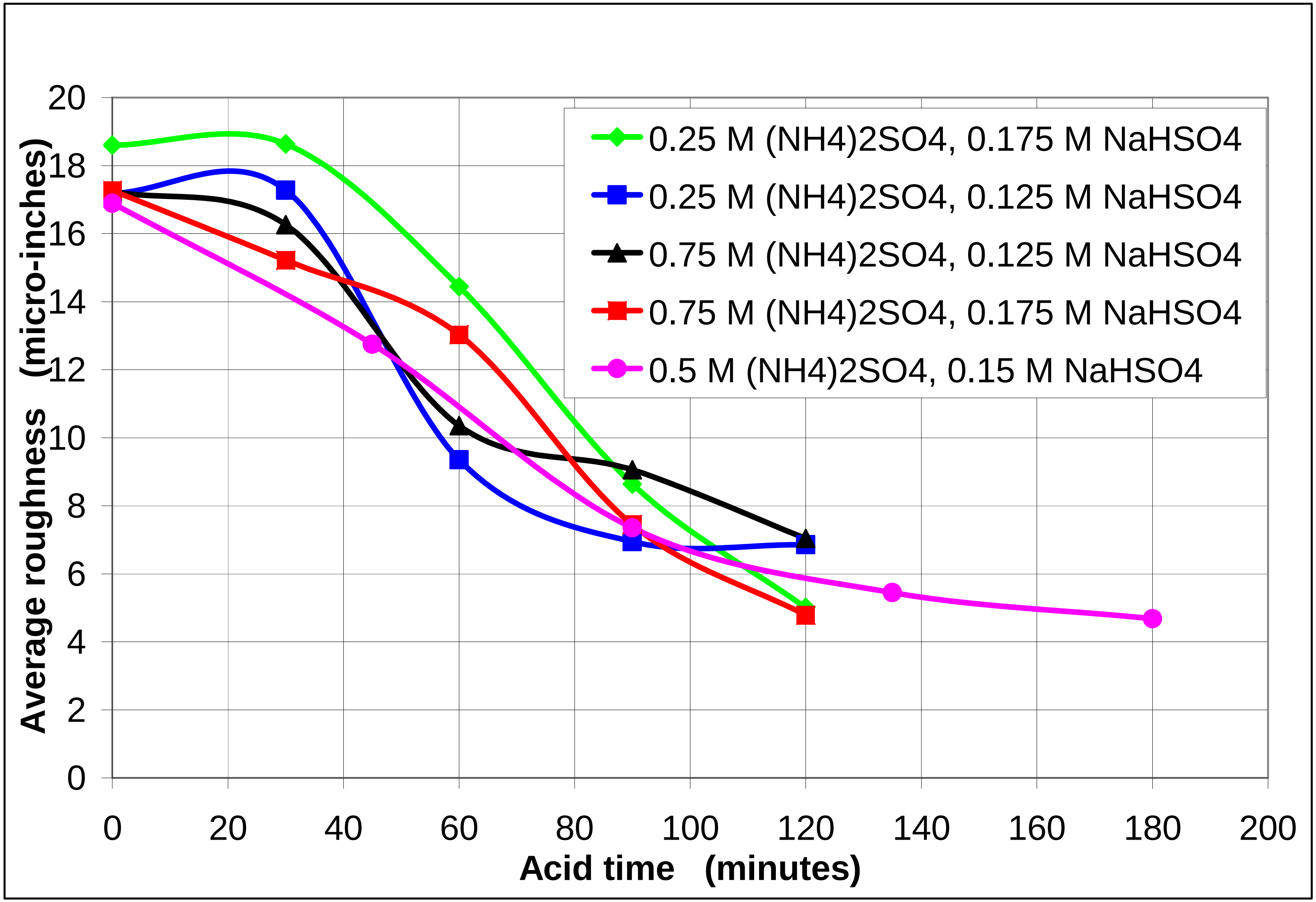
Average roughness of strip steel samples vs. acid time for different sodium bisulfate solutions.



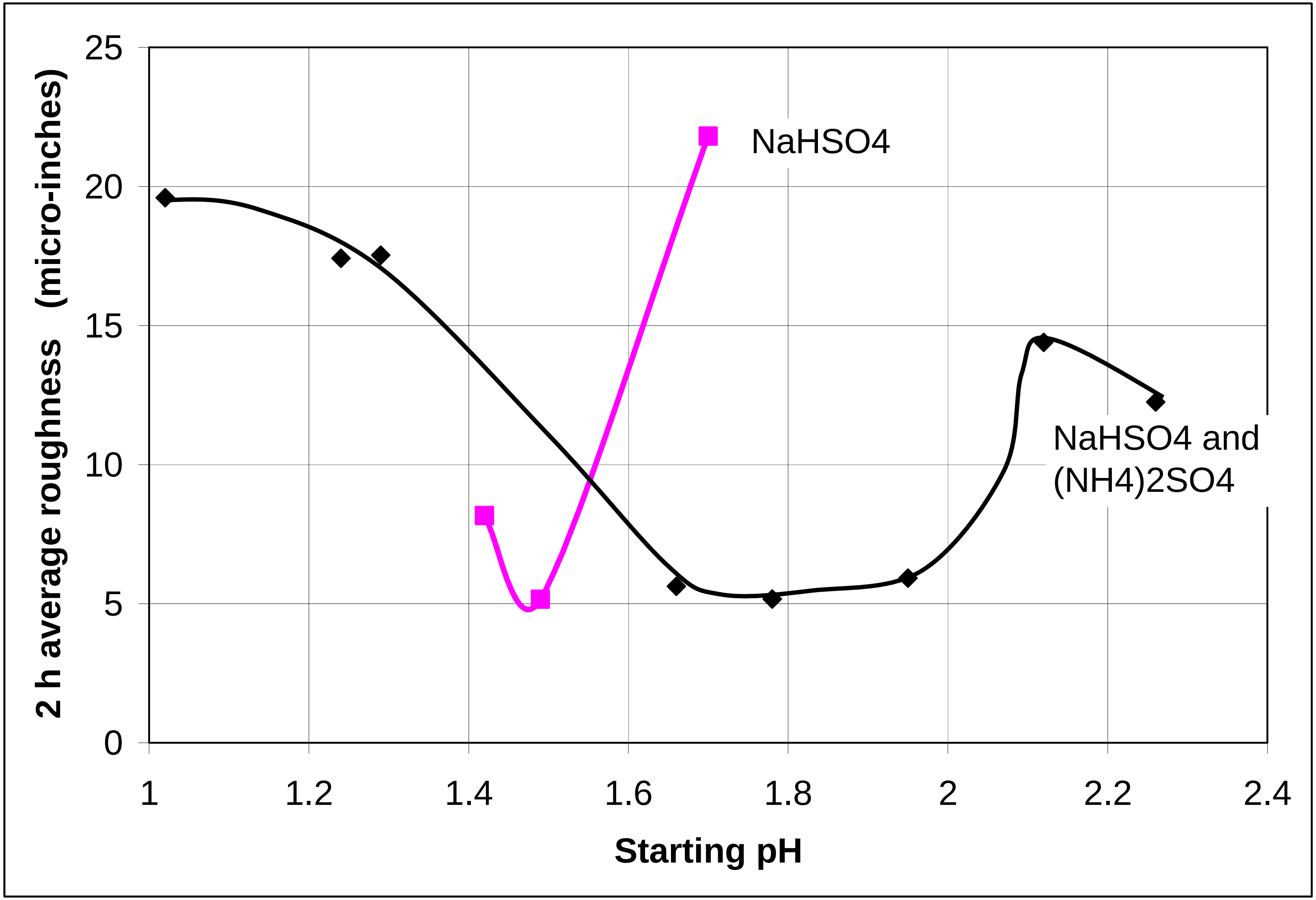
Material removed from strip steel samples vs. acid time for different buffered sodium bisulfate solutions.



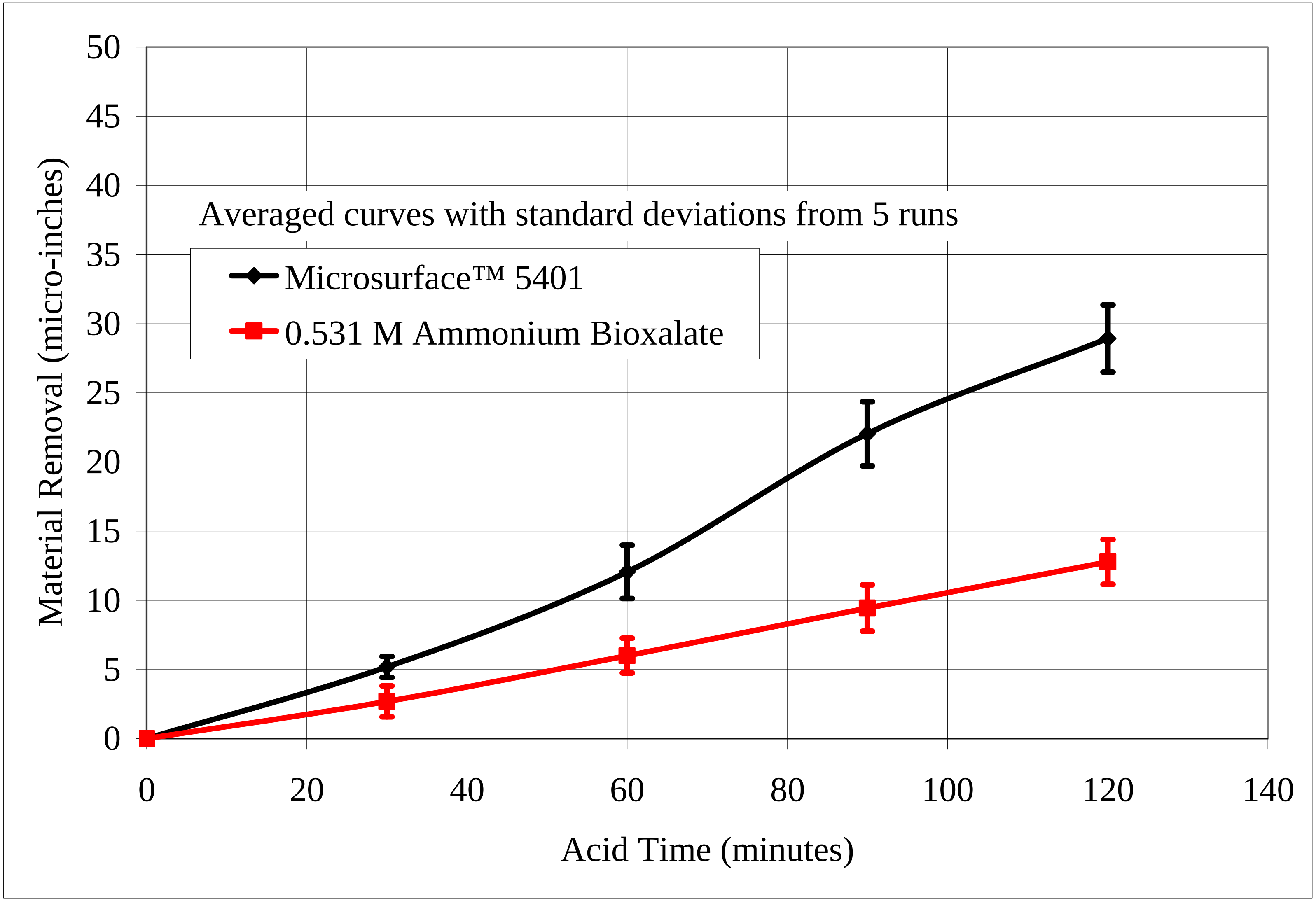
Average roughness of strip steel samples vs. acid time for different buffered sodium bisulfate solutions.



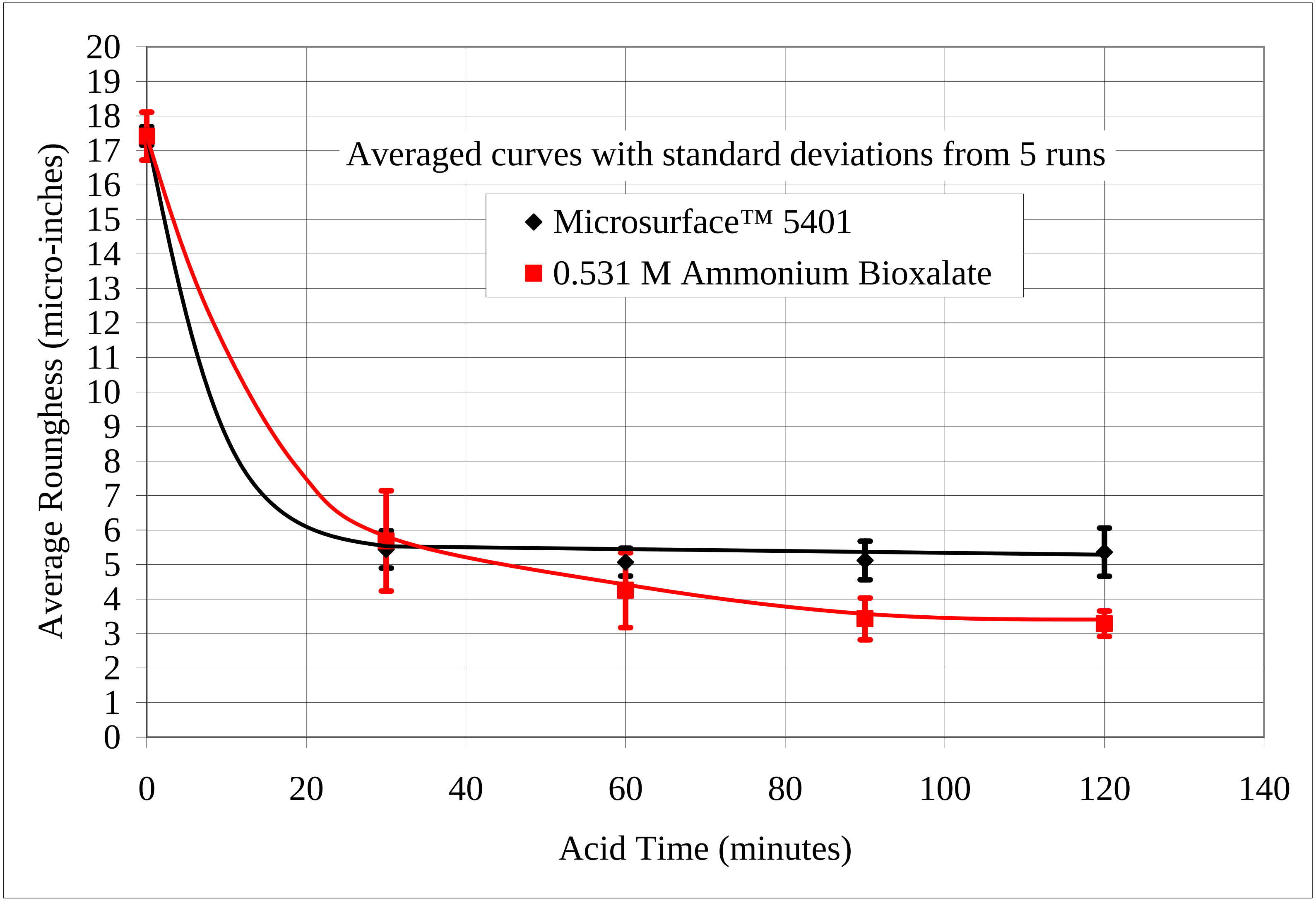
Average roughness after 2 h acid treatment vs. starting pH of the acid.



Material removal versus acid time in the 0.28 m vibrating bowl



Average roughness versus acid time in the 0.28 m vibrating bowl



US Army Benét Laboratories, Alion Science and Technology, and the Engineered Surfaces Center of the University of North Dakota are working together in improving life and performance of materials used for weapons systems.

Acknowledgements

This project is sponsored by the Defense Technical Information Center. The work was made possible by the contractual relationship between AMMTIAC and DoD to research and analysis of advanced materials. This includes US Army Benét Laboratories with US Army ARDEC (Armament Research, Development and Engineering Center).

Thank you for your attention!

Questions?

Email: JuergenFischer@mail.und.edu
Phone: 701-757-5144