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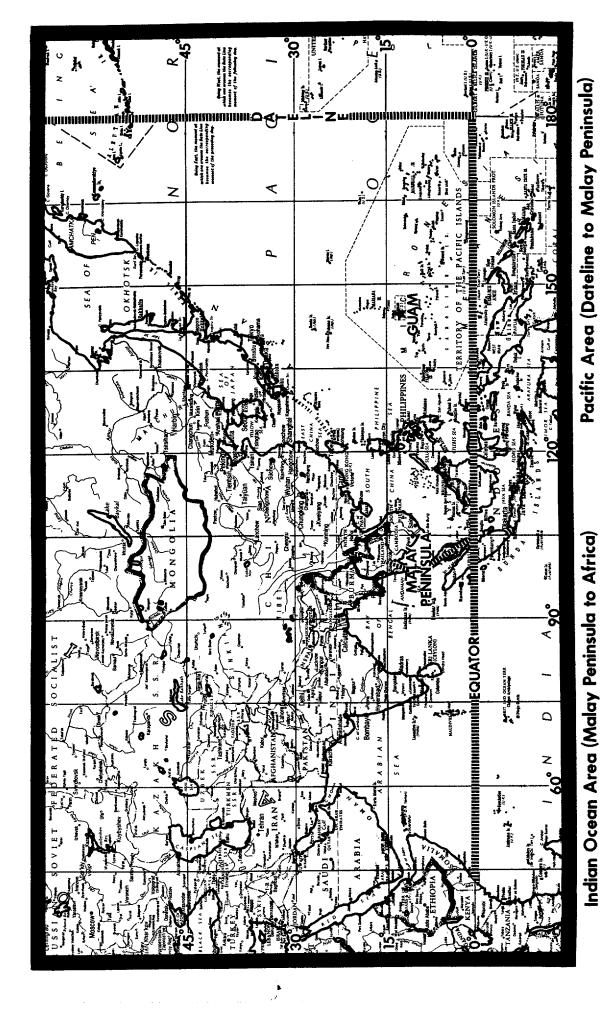


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JOINT TYPHOON WARNING CENTER GUAM, MARIANA ISLANDS

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AREA OF RESPONSIBILITY - JOINT TYPHOON WARNING CENTER, GUAM

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FRONT COVER: Super Typhoon Tip near maximum intensity of 160 kt (82 m/sec), 11 October 1979, 21272. The minimum sea-level pressure was 870 mb and the associated circulation pattern was 1200 nm (2222 km) in diameter at that time. Details on Tip can be found on page 72. (DMSP imagery)

#### **FOREWORD**

The Annual Typhoon Report is prepared by the staff of the Joint Typhoon Warning Center (JTWC). JTWC is a combined USAF/USN entity operating under the command of the U. S. Naval Oceanography Command Center, Guam. The senior Air Force Officer assigned is designated as Director, JTWC and is responsible to the Commanding Officer, U. S. Naval Oceanography Command Center, Guam for the operation of the JTWC. The senior Naval Officer of the JTWC is designated as the Deputy Director/Operations Officer. The JTWC was established by CINCPACFIT message 2802082 April 1959 when directed by CINCPAC message 230233Z April 1959. Its operation is guided by the CINCPACINST 3140.1 (series).

The Naval Oceanography Command Center/ Joint Typhoon Warning Center, Guam has the responsibility to:

- 1. Provide continuous meteorological watch of all tropical activity north of the equator, west of the Date Line, and east of the African coast (JTWC area of responsibility) for potential tropical cyclone development.
- 2. Provide warnings for all significant tropical cyclones in the assigned area of responsibility.
- 3. Determine tropical cyclone reconnaissance requirements and assign priorities.

- 4. Conduct an annual postanalysis of all tropical cyclones occurring within the JTWC area of responsibility and prepare an Annual Typhoon Report for issuance to interested agencies.
- 5. Conduct tropical cyclone forecasting and detection research as practicable.

In the event of incapacitation of the JTWC, the alternate (AJTWC) assumes the responsibility for issuing warnings. The U. S. Naval Western Oceanography Center, Pearl Harbor, Hawaii is designated as the AJTWC. Assistance in determining tropical cyclone reconnaissance requirements and in obtaining reconnaissance data is provided by Detachment 4, 1st Weather Wing, Hickam AFB, Hawaii.

The meteorological services of the United States are planning to implement the metric system of measurement over the next few years. Some civilian and military agencies have started the education program by showing the metric equivalents to current units of measure. This Annual Typhoon Report includes metric equivalents to most measures.

Unless otherwise stated, all satellite data used in this ATR are Air Force Air Weather Service DMSP Data as acquired by OL-C, 27CS personnel and analyzed by Det 1, 1WW personnel colocated with the JTWC at Nimitz Hill, Guam.

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# CHAPTER I - OPERATIONAL PROCEDURES

# 1. GENERAL

Routine services provided by the Joint Typhoon Warning Center (JTWC) include the following: (1) Significant Tropical Weather Advisories issued daily describing all tropical disturbances and their potential for further development; (2) Tropical Cyclone Formation Alerts issued whenever interpretation of satellite and synoptic data indicates likely formation of a significant tropical cyclone; (3) Tropical Cyclone Warnings issued four times daily for significant tropical cyclones; and (4) Prognostic Reasoning messages issued twice daily for tropical storms and typhoons in the Pacific area.

JTWC responds to changing requirements of activities serviced. Therefore, contents of routine services are subject to change from year to year usually as a result of deliberations at the Tropical Cyclone Conference.

#### 2. DATA SOURCES

#### a. COMPUTER PRODUCTS:

The Naval Oceanography Command Center (NAVOCEANCOMCEN) Guam provides computerized meteorological/oceanographic products for JTWC. In addition, the standard array of synoptic-scale computer analyses and prognostic charts are available from the Fleet Numerical Oceanography Center (FLENUMOCEANCEN) at Monterey, California. With the installation of the Naval Environmental Display Stations (NEDS) during 1978, JTWC now has very timely access to necessary FLENUMOCEANCEN products and is thereby able to more efficiently and effectively use this information.

#### b. CONVENTIONAL DATA:

Conventional meteorological data are defined as surface and upper-air observations from island, ship and land stations plus weather observations from commercial and military aircraft (AIREPS). Conventional data charts are prepared daily at 0000Z and 1200Z for the surface, 700 mb, and 500 mb levels. A chart of upper-air data is prepared which utilizes 200 mb rawinsonde data and AIREPS above 29,000 ft within 6 hours of the 0000Z and 1200Z synoptic times.

#### c. AIRCRAFT RECONNAISSANCE:

Aircraft weather reconnaissance data are invaluable in the positioning of centers of developing systems and essential for the accurate determination of the eye/center, maximum intensity, minimum sea-level pressure and radius of significant winds exhibited by tropical cyclones. Winds and pressure-height data at the 500 and/or 400 mb level, provided by reconnaissance aircraft while enroute to, or returning from, fix missions, are also used to supplement the sparse data in the tropics and subtropics. These data are plotted on large-scale sectional charts for each mission flown. A comprehensive discussion of aircraft weather reconnaissance is presented in Chapter II.

#### d. SATELLITE RECONNAISSANCE:

Meteorological satellite data from the Defense Meteorological Satellite Program (DMSP) and the National Oceanic and Atmospheric Administration played a major role in the early detection and tracking of tropical cyclones in 1979. A discussion of this role is presented in Chapter II.

#### e. RADAR RECONNAISSANCE:

During 1979, as in recent years, land radar coverage was utilized extensively when available. Once a storm moved within the range of a land radar site, reports were usually received hourly. Use of radar during 1979 is discussed in Chapter II.

#### 3. COMMUNICATIONS

- a. JTWC currently has access to three primary communications circuits:
- (1) The Automated Digital Network (AUTODIN) is used for dissemination of warnings and other related bulletins to Department of Defense installations. These messages are relayed for further transmission over U. S. Navy Fleet Broadcasts, U. S. Coast Guard CW (continuous wave morse code) and voice communications. Inbound message traffic for JTWC is received via AUTODIN addressed to NAVOCEANCOMCEN GUAM.
- (2) The Air Force Automated Weather Network (AWN) provides weather data to JTWC through a dedicated circuit from the automated digital weather switch (ADWS) at Clark AB, R.P. The ADWS selects and routes the large volume of meteorological reports necessary to satisfy JTWC requirements for the right data at the right time. Weather bulletins prepared by JTWC are inserted into the AWN circuit by the Nimitz Hill Naval Telecommunications Center (NTCC) of the Naval Communications Area Master Station Western Pacific.
- (3) The Naval Environmental Data Network (NEDN) provides the communications link with the computers at FLENUMOCEANCEN. JTWC is able to both receive environmental data from FLENUMOCEANCEN and access the computers directly to run various programs.
- b. Besides providing forecasters with the ability to rapidly access computer products, the NEDS has recently become the backbone of the JTWC communications system. AUTODIN and AWN message tapes can now be prepared by JTWC personnel for insertion into the AUTODIN and AWN circuits by the NTCC. The NEDS is also used by the TDO to request forecast aids which are processed by the computers at Monterey and transmitted back to the TDO over the NEDN circuit.

# 4. ANALYSES

A composite surface/gradient level (3000 ft) manual analysis is accomplished on the 0000Z and 1200Z conventional data. Analysis of the wind field using streamlines is stressed for tropical and subtropical

regions. Analysis of the pressure field is stressed for higher latitudes and in the vicinity of tropical cyclones.

Manual analysis of the 500 mb level is accomplished on the 0000Z and 1200Z data. Although the analysis of the 500 mb height field is stressed, knowledge of the wind field to more clearly delineate steering currents is equally important.

A composite upper-tropospheric manual analysis, utilizing rawinsonde data from 300 mb through 100 mb, wind directions extracted from satellite data by Det 1, 1WW and AIREPS (plus or minus 6 hours) at or above 29,000 feet is accomplished on 0000Z and 1200Z data daily. Wind and height data are used to arrive at a representative analysis of tropical cyclone outflow patterns, of steering currents and of areas that may indicate tropical cyclone intensity change. All charts are hand plotted over areas of tropical cyclone activity to provide all available data as soon as possible to the TDO. These charts are augmented by the computer-plotted charts for the final analyses.

Additional sectional charts at intermediate synoptic times and auxiliary charts such as checkerboard diagrams and pressure-change charts are also analyzed during periods of significant tropical cyclone activity.

#### 5. FORECAST AIDS

# a. CLIMATOLOGY:

Climatological publications utilized during the 1979 typhoon season include previous JTWC Annual Typhoon Reports and climatic publications from local sources, Naval Environmental Prediction Research Facility, Naval Postgraduate School, Air Weather Service, First Weather Wing and Chanute Technical Training Center. Publications from other Air Force and Navy activities, various universities and foreign countries are also used by the JTWC.

# b. OBJECTIVE TECHNIQUES:

The following objective techniques were employed in tropical cyclone forecasting during 1979. A description of these techniques is presented in Chapter IV.

- (1) TYFN75 (Analog)
- (2) MOHATT (Steering)
- (3) 12 HR EXTRAPOLATION
- (4) CLIMATOLOGY
- (5) HPAC (Combined extrapolation and climatology)
- (6) TROPICAL CYCLONE MODEL (Dynamic)
- (7) INJAH74 (Analog)
- (8) CYCLOPS (Steering)
- (9) TYAN78 (Analog)

#### 6. FORECASTING PROCEDURES

#### a. INITIALIZATION:

In the preparation of each warning, the actual surface location (fix) of the tropical cyclone eye/center just prior to (within three hours of) warning time is of prime importance. JTWC uses the Selective Reconnaissance Program (SRP) to levy an optimum mix of aircraft, satellite and radar resources to obtain fix information. When tropical cyclones are either poorly defined or the actual surface location cannot be determined, or when conflicting fix information is received, the "best estimate" of the surface location is subjectively determined from the analysis of all available data. If fix data are not available due to reconnaissance platform malfunctions or communication problems, synoptic data or extrapolation from previous fixes are used. The initial forecast (warning time) position is then obtained by extrapolation using the current fix and a "best track" of the cyclone movement to date.

#### b. TRACK FORECASTING:

An initial forecast track is developed based on the previous forecast and the objective techniques. This initial track is subjectively modified based on the following:

- (1) The prospects for recurvature are evaluated. This evaluation is based primarily on present and forecast position and amplitude of middle tropospheric midlatitude troughs from the latest 500 mb analysis and numerical prognoses.
- (2) Determination of steering level is partly influenced by maturity and vertical extent of the system. For mature cyclones located south of the 500 mb subtropical ridge, forecast changes in speed of movement are closely correlated with forecast changes in the intensity of the ridge. When steering currents are very weak, the tendency for cyclones to move northward due to their internal forces is an important consideration.
- (3) The proximity of the tropical cyclone to other tropical cyclones is evaluated to determine if there is a possibility of Fujiwhara interaction.
- (4) Over the 12- to 72-hr forecast spectrum, speed of movement during the early time frame is biased toward persistence (12-hr extrapolation) while that near the end of the time frame is biased towards objective techniques and climatology.
- (5) A final check is made against climatology to determine the likelihood of the forecast track. If the forecast deviates greatly from climatology, the forecast rationale is reappraised and the track adjusted as necessary.

#### c. INTENSITY FORECASTING:

In forecasting intensity, heavy reliance is placed on aircraft reconnaissance reports, the Dvorak satellite interpretation model, wind and pressure data from ships and land stations in the vicinity of the cyclone, and the objective techniques. Additional considerations are the position and intensity of the tropical upper-tropospheric trough (TUTT), extent and intensity of upper-level outflow, sea-surface temperature, terrain influences, speed of movement and proximity to an extratropical environment.

#### 7. WARNINGS

Tropical cyclone warnings are issued when a definite closed circulation is evident and maximum sustained wind speeds are forecast to increase to 34 or more knots within 48 hours, or the cyclone is in such a position that life or property may be endangered within 72 Warnings are also issued in other situations if it is determined that there is a need to alert military and civil interests to conditions which may become hazardous in a short period of time. Each tropical cyclone warning is numbered sequentially and includes the initial warning time, eye/center position, intensity, the radial extent of 30, 50 and 100 knot surface winds (when applicable), the levied reconnaissance platform used, the instantaneous speed and direction of movement of the cyclone's surface center at warning time and the forecast information. The forecast intervals for all tropical cyclones, regardless of intensity, are 12-, 24-, 48- and 72-hr. Warnings within the JTWC Pacific area are issued within two hours of 0000Z, 0600Z, 1200Z and 1800Z with the constraint that two consecutive warnings may not be more than seven hours apart. Warnings in the JTWC Indian Ocean area are issued within two hours of 02002, 08002, 14002 and 20002 with the constraint that two consecutive warnings may not be more than seven hours apart. These variable warning times allow for maximum use of all available reconnaissance platforms and more effectively distribute the workload in multiple cyclone situations. If warnings are discontinued and a cyclone reintensifies, warnings are numbered consecutively from the last warning issued. Warning forecast positions are verified against the corresponding postanalysis "best track" positions. A summary of the verification results for 1979 is presented in Chapter IV.

#### 8. PROGNOSTIC REASONING MESSAGE

In the Pacific Area, prognostic reasoning messages are transmitted based on the 0000Z and 1200Z warnings or whenever the previous reasoning is no longer valid. This plain language message is intended to provide users with the reasoning behind the latest JTWC forecast. Prognostic reasoning messages are not prepared for tropical depressions nor for cyclones in the Indian Ocean area.

For the 1979 season, JTWC included confidence statements for the 24 and 48-hour forecasts. The confidence values were percentage probabilities that the 24-hour forecast position error would be less than 100 nm and less than 150 nm, respectively, and that the 48-hour error would be less than 200 nm and less than 300 nm, respectively. These probabilities were based on objective data from error analysis studies of past cyclones and were a function of latitude, longitude, storm intensity, organization and the number of western Pacific storms in existence.

Prognostic reasoning information applicable to all customers is provided in the remarks section of warnings when significant forecast changes are made or when deemed appropriate by the TDO.

#### 9. SIGNIFICANT TROPICAL WEATHER ADVISORY

This plain language message, summarizing significant weather in the entire JTWC area of responsibility, is issued by 0600Z daily. It contains a detailed, non-technical description of all significant tropical disturbances and the JTWC evaluation of potential for significant tropical cyclone development within the 24-hour forecast period.

#### 10. TROPICAL CYCLONE FORMATION ALERT

Alerts are issued whenever interpretation of satellite and other meteorological data indicates significant tropical cyclone formation is likely. These alerts will specify a valid period not to exceed 24 hours and must either be cancelled, reissued or superseded by a warning prior to expiration of the valid period.

# CHAPTER II RECONNAISSANCE AND FIXES

#### 1. GENERAL

The Joint Typhoon Warning Center depends on reconnaissance to provide necessary, accurate and timely meteorological information in support of each warning. JTWC relies primarily on three sources of reconnaissance: aircraft, satellite and radar. Optimum utilization of all available reconnaissance resources is obtained through use of the Selective Reconnaissance Program (SRP) whereby various factors are considered in selecting a specific reconnaissance platform for each warning. These factors include: cyclone location and intensity, reconnaissance platform capabilities and limitations, and the cyclone's threat to life/property afloat and ashore. A summary of reconnaissance fixes received during 1979 is included in Section 6.

#### 2. RECONNAISSANCE AVAILABILITY

#### a. Aircraft:

Aircraft weather reconnaissance is performed in the JTWC area of responsibility by the 54th Weather Reconnaissance Squadron (54 WRS). The squadron, presently equipped with six WC-130 aircraft, is located at Andersen Air Force Base, Guam. From July through October, augmentation by the 53rd WRS at Keesler Air Force Base, Mississippi brings the total number of available aircraft to nine. The JTWC reconnaissance requirements are provided daily throughout the year to the Tropical Cyclone Aircraft Reconnaissance Coordinator (TCARC). These requirements include area(s) to be investigated, tropical cyclone(s) to be fixed, fix times and forecast positions of fixes. The following priorities are utilized in acquiring meteorological data from aircraft, satellite and land-based radar in accordance with CINCPACINST 3140.1N:

- "(1) Investigative flights and vortex or center fixes for each scheduled warning in the Pacific area of responsibility.

  One aircraft fix per day of each cyclone of tropical storm or typhoon intensity is desirable.
- (2) Center or vortex fixes for each scheduled warning of tropical cyclones in the Indian Ocean Area of responsibility.
  - (3) Supplementary fixes.
  - (4) Synoptic data acquisition."

As in previous years, aircraft reconnaissance provided direct measurements of height, temperature, flight-level winds, sea level pressure, estimated surface winds (when observable) and numerous additional parameters. The meteorological data are gathered by the Aerial Reconnaissance Weather Officers

(ARWO) and dropsonde operators of Detachment 4, Hq AWS who flew with the 54th. These data provide the Typhoon Duty Officer (TDO) indications of changing cyclone characteristics, radius of cyclone associated winds, and present cyclone position and intensity. Another important aspect of this data is its availability for research in tropical cyclone analysis and forecasting. Aircraft reconnaissance will become even more important in years to come when high-resolution tropical cyclone dynamic steering programs will require a dense input of wind and temperature data.

#### b. Satellite

Satellite fixes from USAF ground sites and USN ships provide day and night coverage in the JTWC area of responsibility. Interpretation of this satellite imagery provides cyclone positions and estimates of storm intensities through the Dvorak technique (for daytime passes).

Detachment 1, 1st Weather Wing, which receives and processes DMSP data, is the primary fix site for the northwestern Pacific. DMSP fix positions received at JTWC from the Air Force Global Weather Central (AFGWC), Offutt Air Force Base, Nebraska were the major source of satellite data for the Indian Ocean. GOES fixes were also provided by the National Environmental Satellite Service, Honolulu, Hawaii for tropical cyclones near the dateline.

#### c. Radar

Land radar provides positioning data on well developed cyclones when in proximity (usually within 175 nm of the radar site) of the Republic of the Philippines, Taiwan, Hong Kong, Japan, the Republic of Korea, Kwajalein, and Guam.

#### d. Synoptic

In 1979, the JTWC also determined tropical cyclone positions based on the analysis of the surface/gradient level synoptic data. These positions were helpful in situations where the vertical structure of the tropical cyclone was weak or accurate surface positions from aircraft were not available due to flight restrictions.

# 3. AIRCRAFT RECONNAISSANCE SUMMARY

During the 1979 tropical season, the JTWC levied 289 six-hourly vortex fixes and 52 investigative missions. In addition to the levied vortex fixes, 150 supplemental fixes were also obtained. The number of levied investigative missions has increased steadily over the past four years in response to JTWC's increased efforts to detect initial tropical cyclone development.

Of 1979's 28 tropical cyclones, investigative missions were not flown on four. The average vector error for all aircraft fixes received at the JTWC during 1979 was 13.0 nm (24.1 km).

Reconnaissance effectiveness is summarized in Table 2-1 using the criteria as set forth in CINCPACINST 3140.1N.

TABLE 2-1. AIRCRAF	T RECONNAIS	SANCE EFFE	CTIVENESS		
EFFECTIVENESS		ER OF D FIXES	PERCENT		
COMPLETED ON TIME EARLY LATE MISSED		58 2 15 1 <u>4</u> 39	89.3 0.7 5.2 4.8 100.0		
LEVIE	VS. MISSED	FIXES			
	LEVIED	MISSED	PERCENT		
AVERAGE 1965-1970 1971 1972 1973 1974 1975 1976 1977 1978 1979	507 802 624 227 358 217 317 203 290 289	10 61 126 13 30 7 11 3 2	2.0 7.6 20.2 5.7 8.4 3.2 3.5 1.5 0.7		

#### 4. SATELLITE RECONNAISSANCE SUMMARY

The Air Force provides satellite reconnaissance support to JTWC using imagery data from DMSP polar orbiting spacecraft. Data from similar NOAA spacecraft (TIROS-N/NOAA-6) were not available to the tactical sites of the network but could be processed on a backup basis by the Air Force Global Weather Central (AFGWC).

The DMSP network consists of both tactical and centralized facilities. Tactical DMSP sites are located at Nimitz Hill, Guam; Clark AB, Philippines; Kadena AB, Japan; Osan AB, Korea; and Hickam AFB, Hawaii. These sites provide a combined coverage that blankets the JTWC area of responsibility in the western Pacific from near the dateline westward to the Malay Peninsula.

The centralized member of the DMSP network is the Air Force Global Weather Central located at Offutt AFB, Nebraska. AFGWC receives worldwide satellite imagery coverage four times daily from two DMSP spacecraft. In addition, AFGWC has the capability to process either TIROS-N or NOAA-6 should one of the primary DMSP spacecraft fail. Imagery taken over the JTWC area of responsibility is recorded on board

the spacecraft and later downlinked to AFGWC via command/readout sites and communications satellites. With their coverage, AFGWC is able to fix a storm anywhere within the JTWC area of responsibility. As the only site in the network that receives coverage over the entire Indian Ocean, AFGWC has the primary responsibility for satellite reconnaissance in this area as well as a small portion of the central Pacific near the dateline. On occasion, AFGWC is tasked to provide storm positions in the western Pacific as backup to the tactical sites.

The thread that ties the network together is Det 1, lww colocated with JTWC atop Nimitz Hill, Guam. Based on available satellite coverage, Det 1 coordinates satellite reconnaissance requirements with JTWC and tasks the individual DMSP sites to provide the necessary storm fixes. The tasking concept is to fix every storm or tropical disturbance (alert area) once from each satellite pass over the area of the storm. When a satellite position is required as the basis for a warning (levy), a dual-site tasking concept is applied. Under this concept, two sites are tasked to fix the storm off the same satellite pass. This provides the necessary redundancy to virtually guarantee JTWC a successful satellite fix of the storm. Using the dual-site tasking concept, the satellite reconnaissance network was able to meet 98 percent of JTWC's satellite fix requirements. Dual-site tasking is not available over the Indian Ocean since only AFGWC receives the satellite coverage for most of that area.

The network provides JTWC with several products and services. The main service is one of surveillance. With the exception of Osan, each site reviews its daily coverage for any indications of development. If an area shows indications of development, JTWC is notified. Once JTWC issues either an alert or warning, the network is tasked to provide three products: storm positions, storm intensity estimates, and 24-hour storm intensity forecasts. Satellite storm positions are assigned position code numbers (PCN) depending on the availability of geography for precise gridding and the degree of organization of the storm's circulation center (Table 2-2). During 1979, the network provided JTWC with 1970 satellite fixes of tropical cyclones in warning status. A comparison of those fixes made on numbered tropical cyclones with their corresponding JTWC best track positions is shown in Table

#### TABLE 2-2. POSITION CODE NUMBERS

PCN METHOD OF CENTER DETERMINATION/GRIDDING

- 1 EYE/GEOGRAPHY
- 2 EYE/EPHEMERIS
- WELL DEFINED CC/GEOGRAPHY
- WELL DEFINED CC/EPHEMERIS
- 5 POORLY DEFINED CC/GEOGRAPHY
- 6 POORLY DEFINED CC/EPHEMERIS

CC=Circulation Center

TABLE 2-3. MEAN DEVIATIONS (NM) OF DMSP DERIVED TROPICAL CYCLONE POSITIONS FROM JTWC BEST TRACK POSITIONS.

NUMBER OF CASES SHOWN IN PARENTHESIS.

PCN	WESTPAC	WESTPAC	INDIAN OCEAN
	1974-1978 AVERAGE	1979	1979
	(ALL SITES)	(ALL SITES)	(ALL SITES)
1 2 3 4 5	13.3 (178) 18.5 (68) 21.2 (270) 25.6 (101) 37.1 (368) 47.2 (190)	14.4 (268) 17.9 (61) 18.6 (341) 20.5 (70) 37.8 (605) 43.3 (232)	13.5 (7) 23.1 (7) 23.4 (16) 18.0 (8) 34.1 (22) 42.2 (66)
1&2	14.8 (246)	15.0 (329)	18.3 (14)
3&4	22.0 (371)	18.9 (411)	21.6 (24)
5&6	40.6 (558)	39.4 (837)	40.2 (88)

2-3. Estimates of the storm's current and 24-hour forecast intensity are made once each day by applying the Dvorak technique (NOAA Technical Memorandum NESS 45 as revised) to daylight visual data. Satellite derived storm positions, intensity estimates, and forecasts constitute the satellite portion of the JTWC forecast data base.

The availability of satellite data varied during the year. At the start, the network had access to three DMSP spacecraft: F-1 (late-morning), F-2 (mid-morning), and F-3 (sunrise). In June, a fourth DMSP spacecraft, F-4, was launched into a late morning orbit. The network had access to these four spacecraft until mid-September when F-1 failed. Three months later, in early December, F-3 failed reducing the active DMSP fleet to only two spacecraft with similar mid- to late-morning coverages. The network was able to partially compensate for this loss by depending on AFGWC to provide fixes for the entire network based on its unique ability to process TIROS-N as a replacement for F-3. Therefore, the 1979 season ended with available satellite coverage at its lowest point for the entire year.

Besides the network provided fixes, JTWC also receives satellite-derived storm positions from several secondary sources. These include: U.S. Navy ships equipped for satellite direct readout; the National Environmental Satellite Service using NOAA and GOES data; and the Naval Polar Oceanography Center, Suitland, Maryland using stored DMSP and NOAA data. Fixes from these secondary sources are not included in the network statistics.

#### 5. RADAR RECONNAISSANCE SUMMARY

Sixteen of the 28 significant tropical cyclones occurring over the western North Pacific during 1979 passed within range of land based radars with sufficient cloud pattern organization to be fixed. The hourly and oftentimes, half-hourly land radar fixes that were obtained and transmitted to JTWC totaled 1143.

The WMO radar code defines three categories of accuracy: good (within 10 km (5.4 nm)), fair (within 10-30 km (5.4-16.2 nm)) and poor (within 30-50 km (16.2-27 nm)).

This year, 1139 radar fixes were coded in this manner; 25% were good, 29% fair and 46% poor. Compared to the JTWC best track, the mean vector deviation for land radar sites was 15 nm (28 km).

Of the 16 tropical cyclones which were monitored with land radar, ll were typhoons: Alice, Cecil, Ellis, Hope, Irving, Judy, Mac, Owen, Sarah, Tip and Vera. These ll typhoons accounted for 89% of all radar fixes received for this season. Excellent support through timely and accurate radar fix positioning allowed JTWC to track and forecast tropical cyclone movement through even the most difficult and erratic tracks.

The 54 WRS made four radar center fixes from their WC-130 aircraft when actual penetration was restricted. One ship radar center fix was received on Typhoon Bess. No radar fixes were received on Indian Ocean tropical cyclones.

#### 6. TROPICAL CYCLONE FIX DATA

A total of 3318 fixes on 28 northwest Pacific tropical cylones and 166 fixes on 7 northern Indian Ocean tropical cyclones were received at JTWC. Table 2-4, Fix Platform Summary, delineates the number of fixes per platform for each individual tropical cyclone. Season totals and percentages are also indicated.

Annex B lists individual fixes sequentially for each tropical cyclone. Fix data is divided into four categories: Satellite, Aircraft, Radar and Synoptic. Those fixes labeled with an asterisk (\*) were determined to be unrepresentative of the surface center and were not used in determining the best tracks. Within each category, the first three columns are as follows:

FIX NO. - Sequential fix number

TIME (Z) - GMT time in day, hours and minutes

FIX POSITION - Latitude and longitude to the nearest tenth of a degree

Depending upon the category, the remainder of the format varies as follows:

TABLE 2-4. FIX S	SUMMARY FOR 19	979						
	•			FIX SUMMARY	<u></u>			
	AIRCRAFT	<u>DMSP</u>	TIROS-N	GOES3	RADAR	SYNOPTIC	TOTAL	
WESTERN PACIFIC								
TY ALICE TY BESS TY CECIL TS DOT TD 05 TY ELLIS TS FAYE TD 08 ST HOPE TS GORDON TD 11 TY IRVING ST JUDY TD 14 TS KEN TY LOLA TY MAC TS NANCY TY OWEN TS PAMELA TS ROGER TY SARAH ST TIP ST VERA TS WAYNE TD 26 TY ABBY TS BEN	43 17 29 7 12 14 1 22 8 6 25 26 3 5 17 14 - 34 5 6 13 59 14 11 2 40 4	80 47 87 71 20 66 48 29 78 40 33 124 140 23 41 63 86 33 87 9 32 112 99 54 44 11 66 20	- - - - - - - - - - - - - - - - - - -	5	42 1* 51 12 11 14 - 44 25 - 148** 177 73 - 312 - 55*** 312 - 5 109 60*** - 7	- - 3 2 7 5 7 1 - 2 2 2 - - - - - - - - - - - - - - -	170 65 167 93 33 99 67 37 145 73 41 297 345 28 119 80 155 48 441 14 44 134 267 137 56 116 33	
TOTAL	437	1643	9	5	1146	78	3318	
% OF TOTAL NO. OF FIXES	13.1	49.5	.3	.2	34.6	2,3	100	
		DMSP	TIROS-N			SYNOPTIC	TOTAL	
INDIAN OCEAN								
TC 17-79 TC 18-79 TC 22-79 TC 23-79 TC 24-79 TC 25-79 TC 26-79		28 16 8 30 19 17 20	5 4 2 6 3 -			5 2 1 -	33 25 12 37 22 17 20	
TOTAL		138	20			8	166	

% OF TOTAL NO. OF FIXES

83 13

4

100

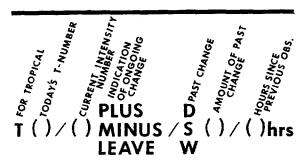
<sup>\*</sup> SHIP RADAR FIX
\*\* INCLUDES TWO ACFT RADAR FIXES
\*\*\* INCLUDES ONE ACFT RADAR FIX

#### a. Satellite

(1) ACCRY - Position Code Number (PCN) (see Sec. 5) or Confidence (CONF) number (see table 2-5) is listed depending on method used to determine the fix position.

	DENCE (CONF) DRAK T NUMBER BILITY AREA (	AND RADIUS	
TROPICAL CYCLONE INTENSITY	CONF (1)	CONF (2)	CONF (3)
T1.5	60	120	170
T2.0	60	120	170
T2.5	60	120	170
T3.0	50	100	150
T3.5	45	90	140
T4.0	45	90	140
T4.5	45	90	140
T5.0	40	90	130
T5.5	40	80	130
T6.0	40	80	130
T6.5	30	70	120
T7.0	30	70	120
T7.5	30	60	100
T8.0	30	60	100

(2) DVORAK CODE - Intensity evaluation and trend utilizing DMSP visual satellite data. (For specifics refer to NOAA TM; NESS-45)



EXAMPLE: T5/6 MINUS/W1.5/24hrs.

- (3) SAT Specific satellite used for fix position (DMSP 35, 36, 37 or 39, TIROS-N or Geostationary Operational Environmental Satellite (GOES, 135W)).
- (4) COMMENTS For explanation of abbreviations see Appendix.
- (5) SITE ICAO call sign of the specific satellite tracking station.

#### b. Aircraft

(1) FLT LVL - The constant pressure surface level, in mb, maintained during the penetration. 700 mb is the normal level flown in developed cyclones due to turbulence factors with low-level missions flown at 1500 ft.

- (2) 700 MB HGT Minimum height of the 700 mb pressure surface within the vortex recorded in meters.
- (3) OBS MSLP If the surface center can be visually detected (e.g., in the eye), the minimum sea level pressure is obtained by a dropsonde released above the surface vortex center. If the fix is made at the 1500-foot level, the sea level pressure is extrapolated from that level.
- (4) MAX-SFC-WND The maximum surface wind (knots) is an estimate made by the ARWO based on sea state. This observation is limited to the region of the flight path, and may not be representative of the entire cyclone. Availability of data is also dependent upon the absence of undercast conditions and the presence of adequate illumination. The positions of the maximum flight level wind and the maximum observed surface wind do not necessarily coincide.
- (5) MAX-FLT-LVL-WND Wind speed (knots) at flight level is measured by the AN/APN 147 doppler radar system aboard the WC-130 aircraft. Values entered in this category represent the maximum wind measured prior to obtaining a scheduled fix. This measurement may not represent the maximum flight level wind associated with the tropical cyclone because the aircraft only samples those portions of the tropical cyclone along the flight path. In many instances the flight path may be through the weak sector of the cyclone. In areas of heavy rainfall, the doppler radar may track energy reflected from precipitation rather than from the sea surface; thus preventing accurate wind speed measurement. In obvious cases, such erroneous wind data will not be reported. In addition, the doppler radar system on the WC-130 restricts wind measurements to drift angles less than or equal to 27 degrees if the wind is normal to the aircraft heading.
- (6) ACCRY Fix position accuracy. Both navigational (OMEGA and LORAN) and meteorological (by the ARWO) estimates are given in nautical miles.
- (7) EYE SHAPE Geometrical representation of the eye based on the aircraft radar presentation. Reported only if center is 50% or more surrounded by wall cloud.
- (8) EYE DIAM/ORIENTATION Diameter of the eye in nautical miles. In case of an elliptical eye, the lengths of the major and minor axes and the orientation of the major axis are respectively listed.

#### c. Radar

- (1) RADAR Specific type of platform utilized for fix (land radar site, aircraft or ship).
- (2) ACCRY Accuracy of fix position (good, fair or poor) as given in the WMO ground radar weather observation code (FM20-V).
- (3) EYE SHAPE Geometrical representation of the eye given in plain language (circular, elliptical, etc.).

- (4) EYE DIAM Diameter of eye given in nautical miles.
- (5) RADOB CODE Taken directly from WMO ground weather radar observation code FM20-V. First group specifies the vortex parameters, while the second group describes the movement of the vortex center.
- (6) RADAR POSITION Latitude and longitude of tracking station given in tenths of a degree.

 $(x_1, x_2, \dots, x_n) = (x_1, x_2, \dots, x_n) + (x_1, x_2, \dots, x_n)$ 

 $\ensuremath{\text{(7)}}$  SITE - WMO station number of the specific tracking station.

#### d. Synoptic

- (1) INTENSITY ESTIMATE TDO's analysis of low-level synoptic data to determine a cyclone's maximum sustained surface wind (knots).
- (2) NEAREST DATA Accuracy of fix based on distance (nautical miles) from the fix position to the nearest synoptic report or to the average distance of reports in data sparse cases.

# CHAPTER III SUMMARY OF TROPICAL CYCLONES

# WESTERN NORTH PACIFIC TROPICAL CYCLONES

27

28

ΤY

ABBY

BEN

\*OVERLAPPING DAYS INCLUDED ONLY ONCE IN SUM.

01 DEC-14 DEC

21 DEC-23 DEC

1979 TOTALS

During 1979, the western North Pacific experienced a below normal year of tropical cyclone activity with a total of 28 cyclones (Table 3-1). By comparison, 1978 was a near normal year with 32 cyclones and 1977 was a near record low year with a total of 21 cyclones. Five significant tropical cyclones never developed beyond tropical depression (TD) stage, and nine developed into tropical storms (TS). Of the 14 cyclones that devel-

oped to typhoon (TY) stage, only 4 reached the 130 kt (67 m/sec) intensity necessary to be classified as a super typhoon (ST). This season, beginning with Typhoon Bess, tropical cyclones attaining tropical storm strength or greater were assigned names on an alternating male/female basis. This change was a result of the 1979 Tropical Cyclone Conference, and the list of names can be found in CINCPACINST 3140.1N CH-1. A similar but different series of cyclone names is used for eastern North Pacific and North Atlantic cyclones. Each tropical cyclone's

TABLE 3-1.	•		WESTER	RN NORTH PACI	FIC			
1979 SIGNI	IFICANT T	ROPICAL CYC	LONES					
CYCLONE	TYPE	NAME	PERIOD OF WARNING	CALENDAR DAYS OF WARNING	MAX SFC WIND	MIN OBS SLP	NUMBER OF WARNINGS	DISTANCE TRAVELLED
01	TY	ALICE	01 JAN-14 JAN	14	110	930	51	2597
02	TY	BESS	20 MAR-25 MAR	6	90	958	21	1804
03	TY	CECIL	11 APR-20 APR	10	80	965	40	2535
04	TS	DOT	10 MAY-16 MAY	7	40	984	24	2876
05	TD	TD-05	23 MAY-24 MAY	2	30	998	6	2170
06	TY	ELLIS	01 JUL-06 JUL	6	85	955	22	1612
07	TS	FAYE	01 JUL-06 JUL	6	40	998	20	1837
08	TD	TD-08	24 JUL-25 JUL	2	20	1004	5	1264
09	ST	HOPE	27 JUL-03 AUG	10	130	898	33	3928
10	TS	GORDON	26 JUL-29 JUL	4	60 .	980	13	1058
11	TD	TD-11	03 AUG-06 AUG	4	25	997	14	1088
12	TY	IRVING	09 AUG-18 AUG	10	90	954	38	2732
13	ST	JUDY	16 AUG-26 AUG	11	135	887	39	2502
14	TD	TD-14	18 AUG-20 AUG	3	20	1006	9	605
15	TS	KEN	01 SEP-04 SEP	5	60	985	13	1418
16	ΤY	LOLA	02 SEP-08 SEP	7	90	950	23	1298
17	TY	MAC	15 SEP-24 SEP	10	70	984	35	1831
18	TS	NANCY	19 SEP-22 SEP	4	45	993	14	528
19	TY	OWEN	22 SEP-01 OCT	10	110	918	37	2151
20	TS	PAMELA	25 SEP-26 SEP	3	45	1002	.6	984
21	TS	ROGER	03 OCT-07 OCT	6	45	985	16	1920
22	TY	SARAH	04 OCT-15 OCT	12	110	929	43	1194
23	ST	TIP	05 OCT-19 OCT	16	165	870	60	3972
24	ST	VERA	02 NOV-07 NOV	6	140	915	23	1868
25 26	TS	WAYNE	08 NOV-13 NOV	6	50	990	22	1559
26	TD	TD-26	01 DEC-02 DEC	2	30	998	6	1070

110

951

990

52

10

695

4044

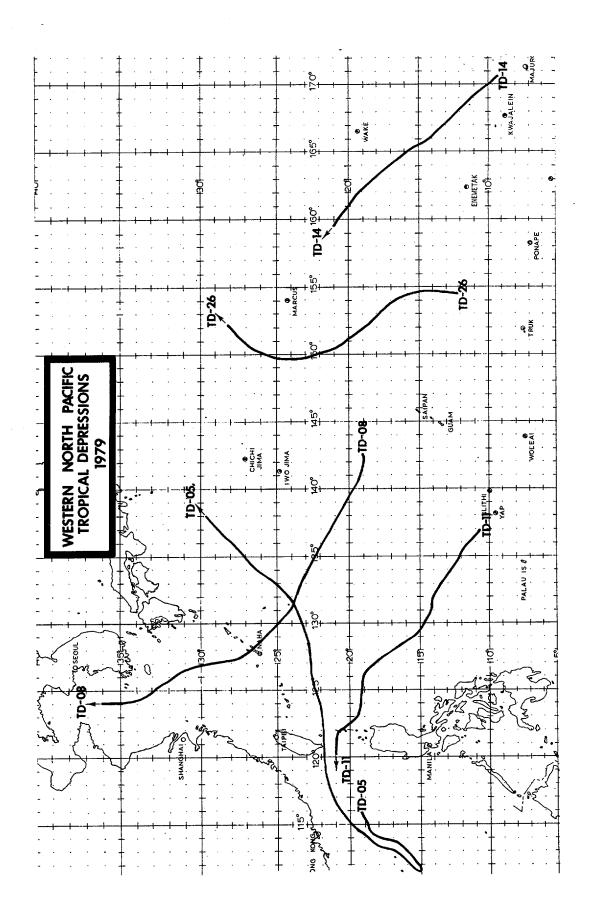
2245

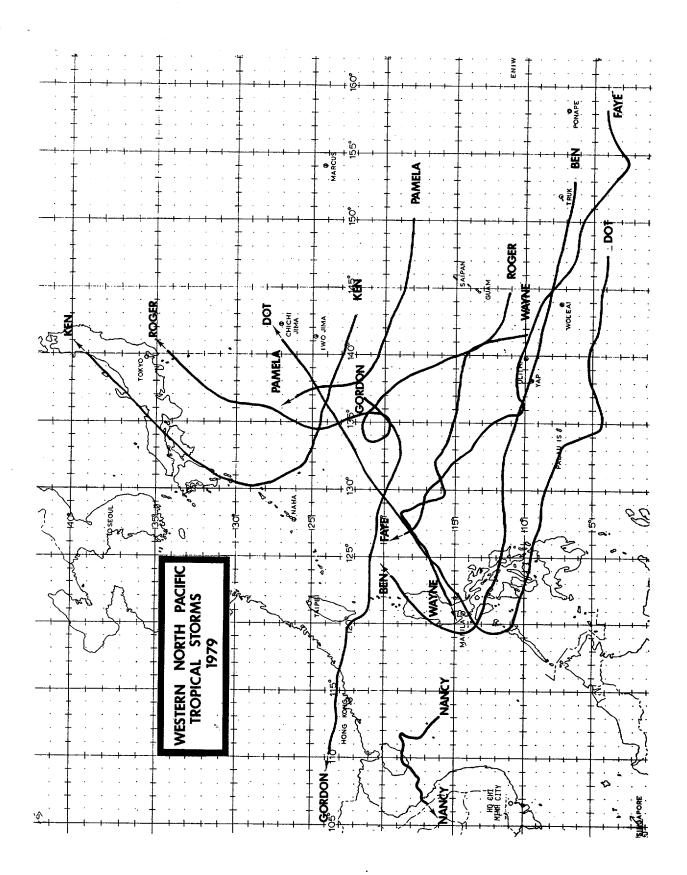
149\*

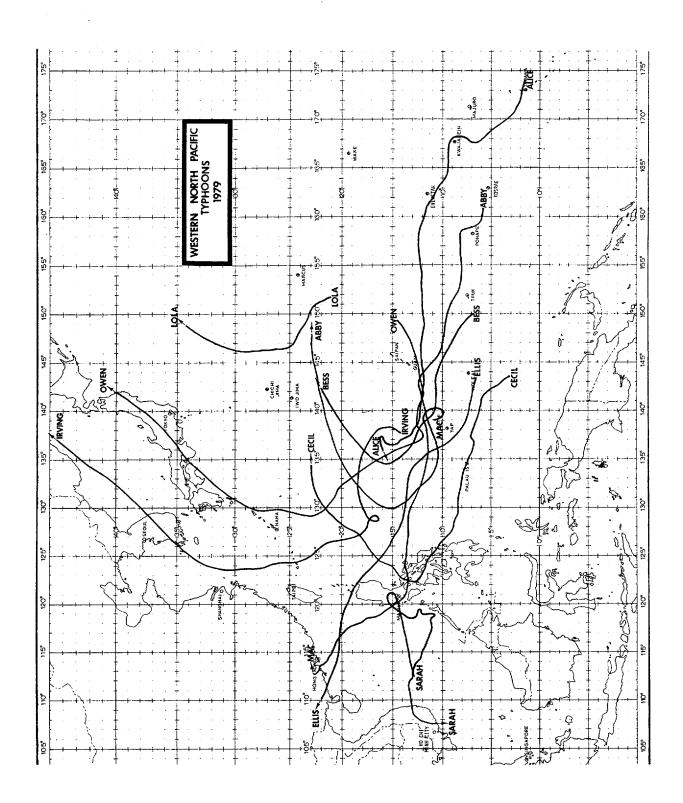
maximum surface wind (MAX SFC WND), in knots, and minimum observed sea-level pressure (MIN OBS SLP), in millibars, were obtained from best estimates of all available data. The distance travelled, in nautical miles, was calculated from the JTWC official best track (see Annex A).

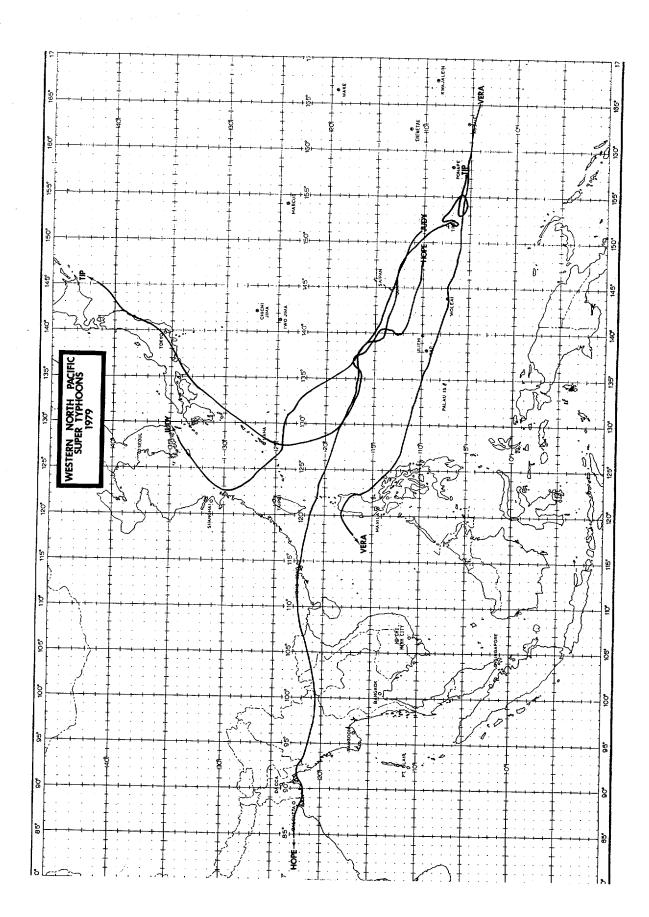
Table 3-2 provides further information on the monthly distribution of tropical cyclones and statistics on Tropical Cyclone Formation Alerts and Warnings. Even though there were 4 fewer cyclones this season compared to last season, there were 18 more warning days.

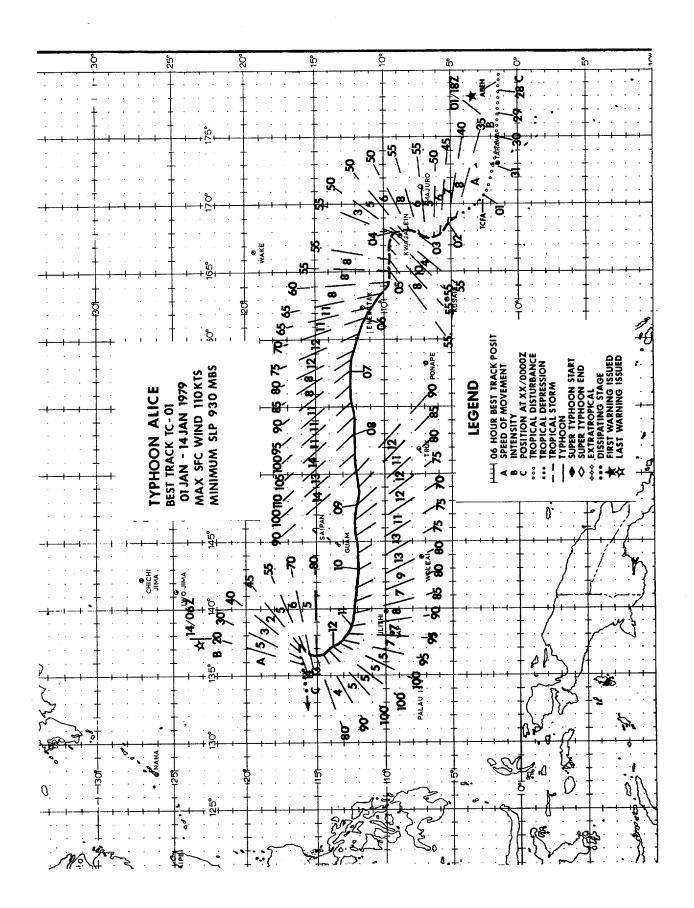
			197	9 SIGN	IFICAN	T TROP	ICAL C	YCLONE	STATI	STICS				
WESTERN NORTH PACIFIC	NAL	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	ОСТ	NOV	DEC	TOTAL	(1959-78) AVERAGE
TROPICAL DEPRESSIONS	0	0	0	0	1	0	1	2	0	0	0	1	5	4.8
TROPICAL STORMS	0	0	0	0	1	0	2	0	4	1	1	1	10	10.0
TYPHOONS	1	0	1	1	0	0	2	2	2	2	1	1	13	18.0
ALL CYCLONES	1	0	1	1	2	0	5	4	6	3	2	3	28	32.8
(1959-78) AVERAGE	0.6	0.4	0.6	0.9	1.4	2.1	5.2	6.8	6.0	4.8	2.7	1.3	32.8	
FORMATION ALERTS			27 (85 28 (183	•							•	al cyclo ert.	nes.	
WARNINGS	Numb	er of	warnir	ng day:	s: 149	)								
	Numb	er of	warnir	ng day:	with	2 cyc	ones:	38						











Typhoon Alice, the first tropical cyclone of the 1979 season, was actually first sighted as a tropical disturbance on the 27th of December 1978. Being over the Gilbert Islands quite close to the equator, the potential for development was considered poor. A tropical cyclone formation alert was issued at 03002 1 January 1979 when satellite data showed the disturbance progressively increasing in organization. Soon after, the suspect area accelerated northwest to higher latitudes where development conditions were more favorable, and by 0118002, tropical storm Alice was named. Post-analysis showed that the tropical depression stage began near 010000Z at low latitudes, contrary to the general rule that cyclones do not form close to the equator.

Although a climatologically unfavored period for western North Pacific tropical cyclone development, the fact that Alice did form supports the non-existence of a definitive "typhoon season" for WESTPAC; tropical cyclones are possible anytime of the year. The greatest forecasting difficulties and concomitant large forecast errors occurred during Alice's formative and dissipating stages. Double intensification also contributed to Alice's notoriety.

Early in her lifetime, Alice meandered through the Marshall Islands as if determined to visit each island. One week later, on 12 January 1979, President Carter declared the Marshall Islands a major disaster area.

A satellite reconnaissance fix at 022133Z showed Alice had moved northeastward when forecast to continue northwestward. Being a fix on a poorly defined satellite image (PCN 6), it was not taken verbatim; northwest movement continued to be forecast. An aircraft reconnaissance fix at 030053Z confirmed the earlier satellite fix as did a follow-on 0303102 aircraft fix. Postanalysis revealed that a mid-latitude, shortwave trough passed north of Alice during this time period. The trough extended deep enough into the tropics to weaken the midtropospheric ridge. This weakness permitted a southward intrusion of mid-latitude westerlies into Alice's vicinity, temporarily steering her northeastward. As the shortwave trough continued eastward, the subtropical ridge quickly reestablished itself north of Alice producing strong easterly steering flow, temporarily accelerating her from 4 to 10 kt (8 to 19 km/hr) toward the northwest when continued northeast movement was forecast. During this time, decision makers on Enewetak (also within the Marshall Islands), noting the low forecast confidence stated on prognostic reasoning messages, kept a condition of readiness which paid off.

From the 6th to the 11th, Alice traveled due west. On the 8th, Alice attained 110 kt (57m/sec) intensity and simultaneously accelerated to a speed of 14 kt (26 km/hr) (the fastest observed along track), whereupon she began weakening slowly.

During the 9th, Alice began an unexpected northward movement trend and showed further weakening. Post-analysis of low-level synop-

tic data and satellite imagery (Fig. 3-01-1) indicated that an approaching frontal shear-line was the responsible agent. The shear-line began interacting with Alice while she was southeast of Guam. As Alice neared Guam, radar data from Andersen AFB and aircraft data indicated that Alice's previously well-defined wall cloud became larger and somewhat less organized. Cooler, drier air north of the shear-line was likely responsible for this weakening trend. A weakness in the subtropical ridge vertically above the shear-line apparently allowed for Alice's northward deviation.

The most unusual portion of Alice's track occurred during the final 3 days of Alice's life. Based on interpretation of PE progs, the subtropical ridge was expected to persist and maintain Alice in the easterlies. As a result, the JTWC forecasts (supported by the majority of objective forecast aids) indicated westward movement until 120000Z, 18 hours after Alice had actually begun tracking northwestward. The subtropical ridge weakened in response to a long-wave trough deepening over eastern Asia. Easterly steering currents in Alice's vicinity diminished and veered in direction, permitting a more northward track. Alice reached a secondary intensity maximum of 100 kt (51 m/sec) during this period due to her slowing in speed of movement, the increased absolute vorticity of higher latitudes and good outflow aloft.

By the 13th, Alice turned northeastward and began weakening rapidly. The subtropical ridge was now completely severed and upperair westerlies were shearing Alice significantly in the vertical. Close proximity of yet another frontal shear-line contributed to further weakening. The biggest surprise, however, came when Alice's low-level circulation turned almost 180 degrees back toward the west at about 1312002 under the influence of strong, low-level easterlies and weakened rapidly in the strong, vertical-shear environment. As a result of vertical decoupling, Alice as a shallow depression, dissipated during the following 12-hour period.

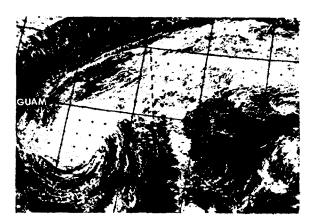
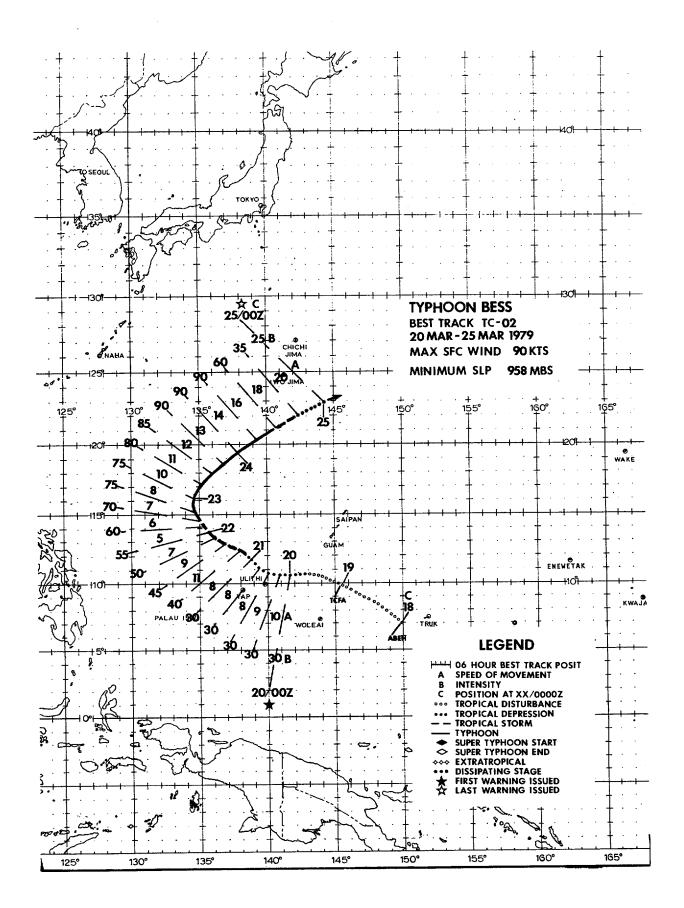


FIGURE 3-01-1. Typhoon Alice merging with the trailing end of a frontal shear-line, 9 January 1979, 00542. [DMSP imagery]



Since 1959, only three typhoons have developed over the Western Pacific in March. Of these three, only Bess developed in the last decade with Typhoon Tess developing in 1961 and Typhoon Sally in 1967. Tropical cyclone development in March is usually inhibited by a southward adjustment in the subtropical ridge axis. Although not recognized in advance, Typhoon Bess' development paralleled Typhoon Tess, which developed in the eastern Caroline Islands and reached tropical depression strength near Woleai Atoll. Continuing northwestward between Guam and Yap, both recurved northward near 135E (Fig. 3-02-1) before dissipating north of 20N under the influence of a strong vertical shear.



FIGURE 3-02-1. Typhoon Bess tracking northwestward between Guam and Yap at 8 kt (15 km/hr), 21 March 1979, 01032. Satellite imagery captured increased organization in the convective banding just prior to Bess reaching tropical storm intensity. (DMSP imagery)

Synoptic data at 1600002 suggested the existence of a weak surface circulation near 3.0N 152.5E at the base of a wave in the easterly flow. Satellite imagery at 1601192 indicated that an ill-defined area of convection existed near the surface circulation. By 1611092, however, increased upper-level organization suggested development of a weak 200 mb anticyclone (Fig. 3-02-2). Increased curvature in the mid-level convective cloud pattern hinted at the possibility of tropical cyclone formation. As often observed in weak

developing systems, 162207Z satellite imagery showed a significant decrease in the mid- to upper-level convective organization, while the synoptic analysis continued to support a weak circulation southeast of Guam. Continuing to pulsate, the suspect area presented a curious, but intensified upper-level convective pattern on 172151Z and 172333Z satellite imagery. Synoptic analysis at 180000Z indicated that, in addition to the circulation near 3.5N 147.5E, a secondary low had developed on the slow moving wave axis near 7.1N 150.0E and that the earlier ill-defined convection had been associated with these two circulations. As this secondary low tracked northward up the wave axis, increased cyclon-



FIGURE 3-02-2. Infrared imagery of very early development stage of Bess, 16 March 1979, 11092. Streamline pattern indicates an upper-level anticyclone. A surface circulation had not yet developed. (DMSP imagery)

ic shear between strong easterly flow north of the wave and weak equatorial westerlies south of the wave caused the northern circulation to become the dominant center as the initial low weakened. Simultaneously, the upper-level anticyclone intensified, producing an excellent outflow signature on 182315Z satellite imagery (Fig. 3-02-3). Although a formation alert was issued based on 182315Z satellite imagery, continued rapid development did not occur as expected. Aircraft data at 200259Z found strong enhanced easterly flow of 20-30 kt (10-15 m/sec) to the northeast, but only weak cyclonic flow to the south and east. Aircraft reports finally confirmed tropical storm strength early on the 21st (Fig. 3-02-4), five days after Bess was initially observed.

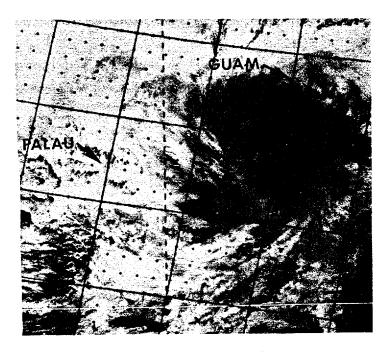


FIGURE 3-02-3. Infrared imagery of Typhoon Bess developing under good upper-level outflow which is visible from the southeast through the northwest, 18 March 1979, 23152. (DMSP imagery)

Sea Surface Temperature (SST) plays a vital role in the development and maintenance of tropical cyclones. A study by Charles P. Guard (1979) indicates that tropical cyclones which move over water cooler than 26C are less likely to intensify due to a reduction in latent heat. The study further states that tropical cyclones which develop prior to June intensify up to 10 kt (5 m/sec) after recurvature. This intensification, if experienced, will occur within the 12-24 hour period following recurvature. Typhoon Bess followed this recurvature pattern. The axis of recurvature was crossed at 230000Z. Slow intensification occurred over the next 18 hours with Bess reaching her maximum intensity of 90 kt (46 m/sec) at 231800Z. Bess maintained 90 kt (46 m/sec) for 18 hours and then rapidly weakened, dissipating by 250000Z. SST analyses during 24-27 March (Fig. 3-02-5) indicate that the area in which Bess weakened from 90-60 kt (46-31 m/sec) in a six-hour period corresponds closely to the location of water cooler than 26C. The reduction of latent heat input, coupled with increased vertical shear produced by strong westerlies aloft, literally sheared Bess apart during the final 12-18 hours.



FIGURE 3-02-4. Typhoon Bess just prior to reaching her maximum intensity of 90 kt (46 m/sec), 23 March 1979, 02357. Bess displays a large elliptical eye with strong radial cirrus outflow in all directions. (DMSP imagery)

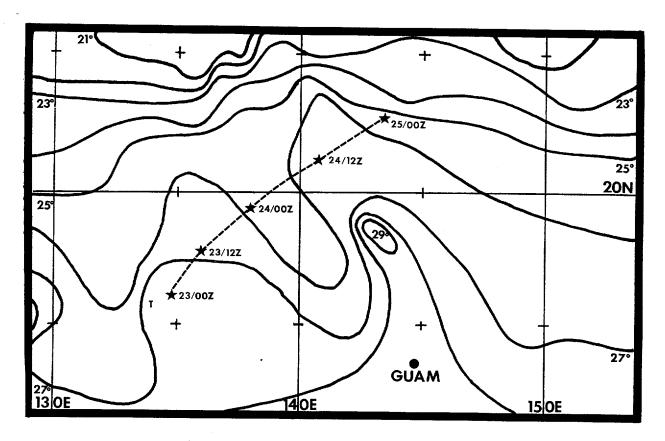
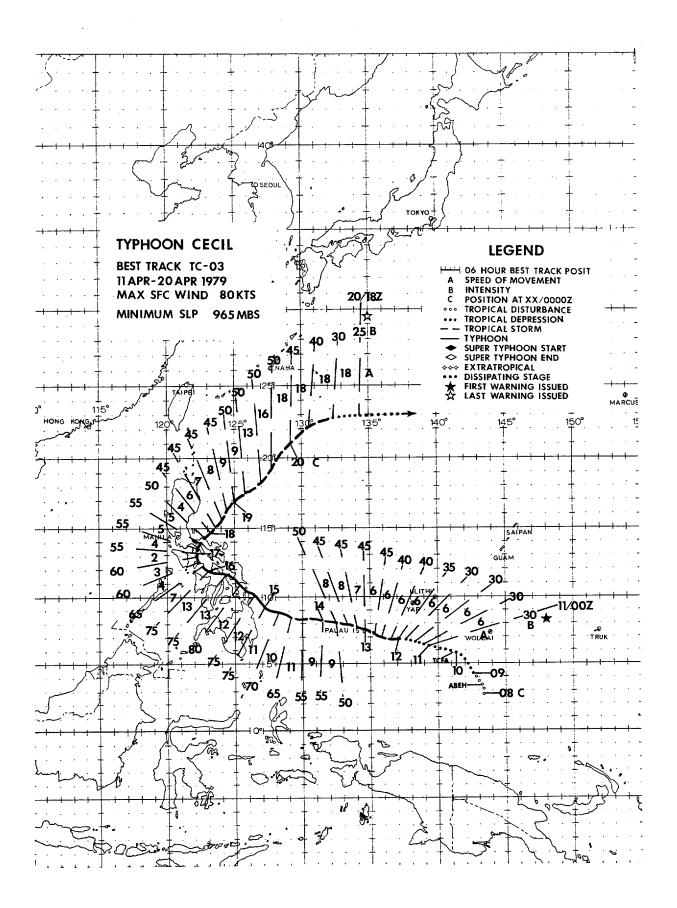


FIGURE 3-02-5. Composite of sea surface temperature analyses from 24-27 March 1979. Northeastward track of Typhoon Bess during dissipation stage is indicated by a dashed line with 12-hour positions.



Typhoon Cecil, the first tropical cyclone of 1979 in the Northwest Pacific given a male name, generated in mid-April from an easterly wave over the Philippine Sea. Cecil was forecast very well while on a climatological west-northwest track toward the central Philippines. Overall, post-analysis statistics showed that mean forecast errors were better than long-term averages. Nevertheless, JTWC warnings failed to forecast the crucial recurvature point in Cecil's track. Was there sufficient evidence to forecast this recurvature 24-48 hours in advance?

Post-analysis showed that recurvature occurred 36 hours after the 1512002 best track position. Satellite imagery (Fig. 3-03-1) located Cecil just south of Samar. At this time, the 500 mb subtropical ridge axis was at 17N with a small high pressure cell located over Northern Luzon. The 500 mb 36-hour PE prog maintained the ridge. Steering techniques based on this synoptic situation indicated westward movement for 72 hours. Analog techniques indicated west-northwest-ward movement. As a matter of fact, no objective forecast technique indicated recurvature prior to entrance into the South China Sea. The climatological average location of the 500 mb ridge axis is along 15N for April over the Philippines and the climatological recurvature point is 15-17N. Both

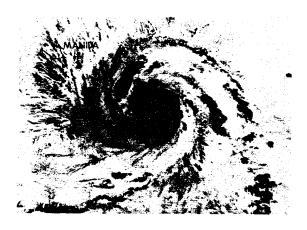
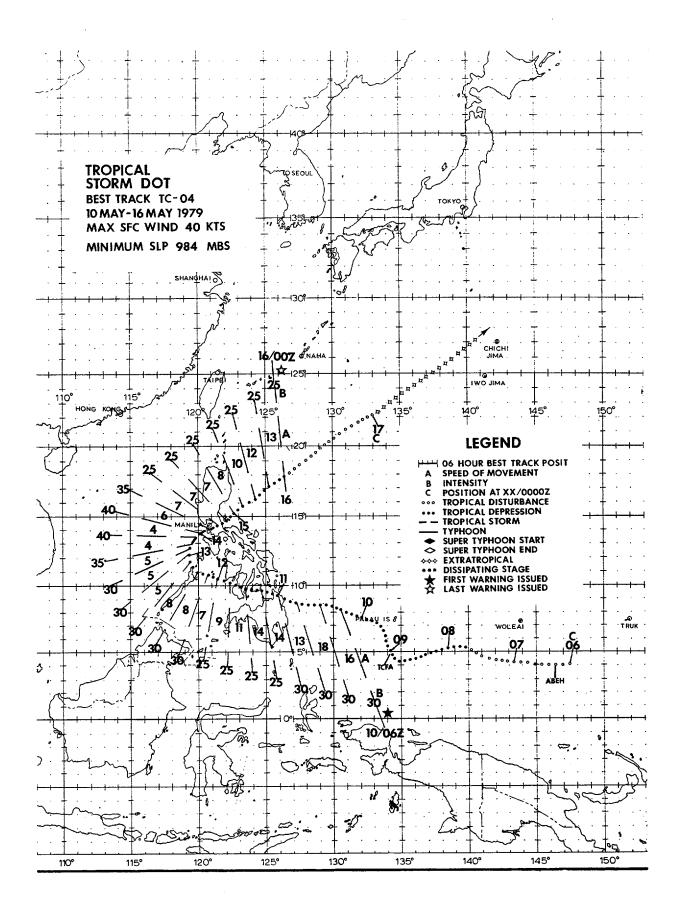


Figure 3-03-1. Infrared imagery of Typhoon Cecil 36 hours prior to recurvature with maximum sustained winds of 80 kt (41 m/sec), 15 April 1979, 1225Z. (DMSP imagery)

synoptic and climatological data indicated a west-northwestward track over the Philippines with recurvature late in the forecast period in the South China Sea as Cecil tracked to the vicinity of 15N. Post-analysis, however, revealed that the ridge axis east of the Philippines abruptly shifted south between 161200Z and 170000Z with westerly winds intruding far to the south over the South China Sea. This pattern shift caused Cecil to recurve much earlier than anticipated. in 48 hours, Cecil was well east of Luzon (Fig. 3-03-2). The ridge axis shift was the vital piece of information not present in any of the available prognostic tools. it appears even in post-analysis that forecasting of Cecil's recurvature 36 hours in advance was beyond state-of-the-art capabilities.



FIGURE 3-03-2. Cecil after recurvature with maximum sustained winds of 50 kt {26 m/sec}, 19 April 1979, 0014Z. (DMSP imagery)



Tropical Storm Dot did not reach tropical storm strength prior to landfall on the Philippine Islands (Fig. 3-04-1). Once Dot crossed the islands, tropical storm strength was attained lasting, however, less than 24 hours (Fig. 3-04-2). Dot's development was cut short by the eventual frictional effects of Luzon and increasing vertical wind shear aloft.

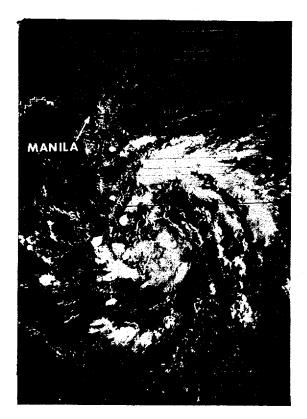


FIGURE 3-04-1. Tropical Storm Dot at 30 kt (15 m/sec) intensity while over northern Mindanao, 11 May 1979, 00292. (DMSP imagery)

TS Dot slowly formed in an area of broad, low-level easterlies, high surface pressures, and strong upper-level shear. The conditions for significant tropical cyclone development were poor while the system existed east of the Philippine Islands. After crossing the Philippines, however, Dot reached tropical storm strength while over the South China Sea.

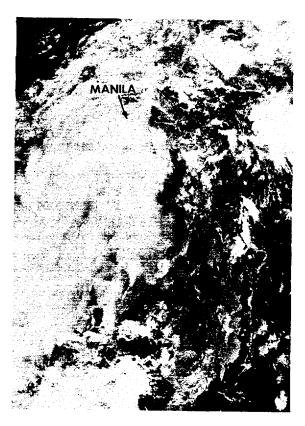
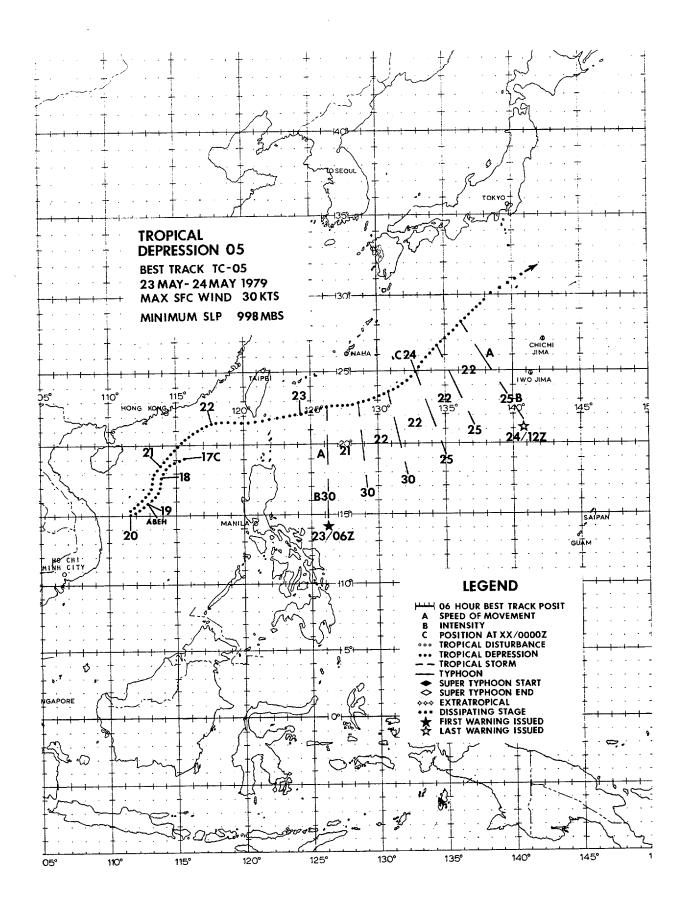


FIGURE 3-04-2. Tropical Storm Dot while recurving toward Manila, 12 May 1979, 23537. (DMSP imagery)



Early season disturbances in the South China Sea, as discussed by Ramage (1971), may develop as a result of active monsoon troughs which extend eastward across Southeast Asia into the South China Sea (SCS). During late May, increased convergence in the enhanced southwest monsoon flow produced a significant increase in convection across the SCS, and several weak surface circulations were noted along the monsoon trough between Hainan Island and northern Luzon. Surface/gradient level synoptic analysis at 170000Z confirmed the existence of an elongated pressure trough with several 1005 mb centers. The main circulation, located northeast of the Paracel Islands, was actually north of the main convective area which covered most of the SCS south of the trough. Characteristics of SCS monsoon depressions include: strong enhanced southwesterly flow with light winds near the depression center; large areas of convection associated with convergence in the southwesterly flow with little curvature in towards the center; a relatively flat surface pressure regime of large areal extent; and, a mid-tropospheric cyclonic circulation over the area (Ramage, 1971). These conditions were observed in this area.

Initially, TD 05 drifted southwestward east of the Paracel Islands. By 2000002 a slow, eastward-tracking 500 mb short-wave over central China caused TD 05 to accelerate northeastward. As TD 05 accelerated, increased cyclonic shear at the surface southeast of Taiwan caused the system to transition from a monsoon depression to a tropical depression with a small anticyclonic outflow center evident aloft. (Many SCS mon-soon depressions never make this transition, usually dissipating after 3-4 days.) Totally divorced from the monsoon trough, TD 05 tracked eastward through the Bashi Channel and then along the remnants of a weak frontal boundary. TD 05 was not forecast to intensify significantly, but it merged with an extratropical frontal boundary near 22.0N 124.8E and produced an improved satellite signature at 230018Z (Fig. 3-05-1) which included a banding-type eye. (Banding-type eyes are usually characteristic of more intense tropical cyclones.) Synoptic analyses during the life of TD 05 never indicated an intensity above 30 kt (15 m/sec). The lowest pressure recorded was 998 mb measured by a ship close to the circulation center. This pressure equates to approximately 32 kt (17 m/sec) (Atkinson and Holliday, 1975).

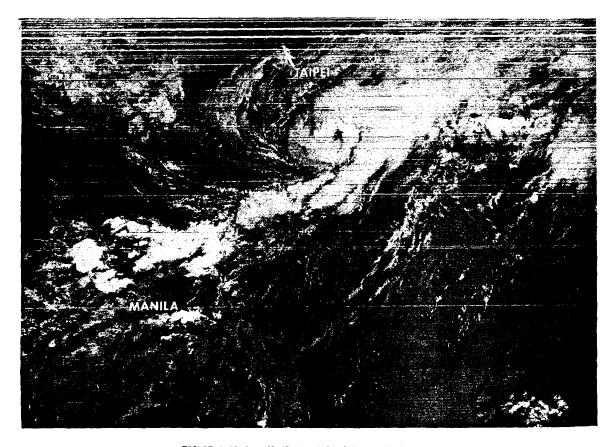
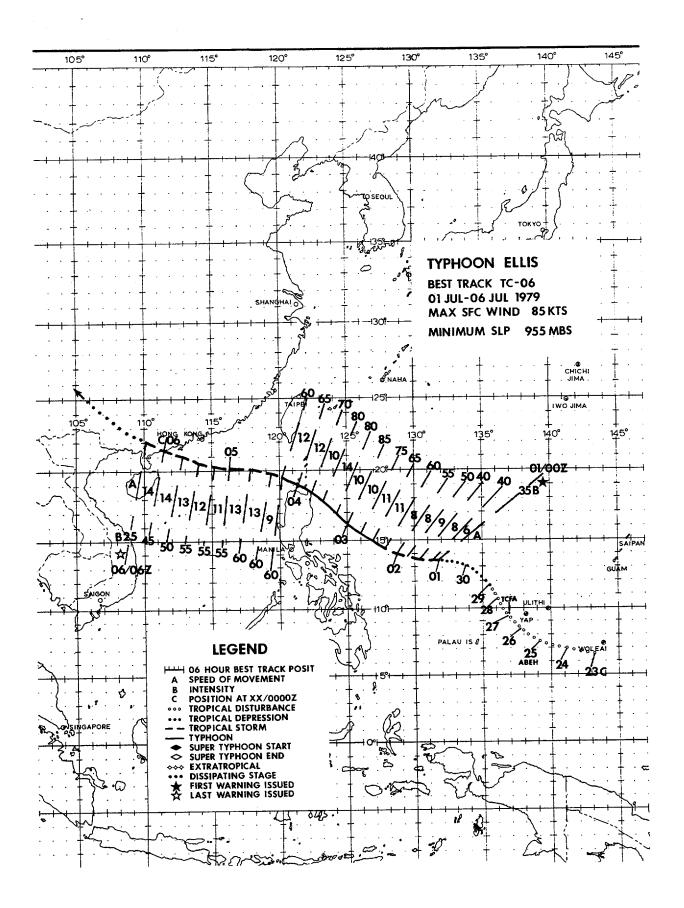


FIGURE 3-05-1. TO 05 at 30 kt [15 m/sec] intensity with banding-type eye moving east-northeastward at 20 kt [37 km/hr], 23 May 1979, 0018Z. (DMSP imagery)



The tropical disturbance, which later became Typhoon Ellis, was first noted on satellite and synoptic data on 25 June 1979. The surface/gradient-level analysis showed that a broad monsoon trough had developed between Guam and the Philippine Islands. upper-levels, a Tropical Upper Tropospheric Trough (TUTT) was oriented northeastsouthwest between the Volcano Islands and the central Philippine Islands. This TUTT allowed excellent upper-level outflow to the northeast and was expected to induce intensification of the tropical disturbance southeast of the TUTT axis. Therefore, a Tropical Cyclone Formation Alert (TCFA) was issued for the area valid at 270000Z. However, significant development did not occur. Reconnaissance aircraft could find only a very broad surface circulation with relatively high surface pressures. surface circulation drifted under the TUTT and the associated convection was suppressed; development was thereby thwarted. Based on the superposition of the TUTT and the surface circulation and the fact that the overall satellite signature had not improved, the TCFA was cancelled at 282000Z.

The area was closely monitored, and when satellite imagery showed increased convective development and surface data showed decreasing pressures and increasing winds, a second TCFA was issued valid at 300600Z. Subsequent aircraft investigation revealed a minimum sea-level pressure of 1000 mb and surface winds in excess of 35 kt (18 m/sec). Based on this new information, the first warning on TS Ellis was issued at 010000Z July. Ellis was in a favorable position at that time and steady intensification occurred over the next 2 days.

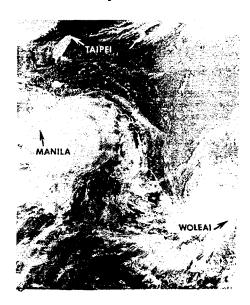


FIGURE 3-06-1. Typhoon Ellis (left) at maximum intensity of 85 kt (44 m/sec), 2 July 1979, 2356Z. TS Faye (right) is developing north of Woleai. (DMSP imagery)

For his entire lifetime, Ellis followed an uncomplicated, classic west-northwest track at near climatological speeds ranging from 9-14 kt (17-26 km/hr). Post-analysis indicates that Ellis was moving under the influence of the east-southeasterly steering flow on the southern edge of the subtropical mid-tropospheric ridge. Ellis' nearly straight track is due primarily to the fact that this ridge did not change in intensity or orientation during the period.

Ellis reached typhoon strength at 0212002 and a maximum intensity of 85 kt (44 m/sec) at 0300002 (Fig. 3-06-1). Continued intensification was anticipated, but a slow weakening trend was actually observed. As with Tropical Storm Faye, this weakening was associated with a drastic change in the upper-level flow pattern.

During Ellis' developing stage, the TUTT was located to the north-northwest and was providing the necessary outflow channel to the northeast. By 020000Z, however, an upper-level anticyclone over central China began to ridge eastward, forcing the TUTT to the northeast. Strong upper-level northeasterly winds associated with this anticyclone began to exert pressure on Ellis, shearing the convective activity to the southwest. Continuing west-northwest in this shearing environment, Ellis weakened steadily. By the time he was in the South China Sea, Ellis had weakened to tropical storm strength and was a completely exposed low-level circulation (Fig. 3-06-2).

With winds of 54 kt (26 m/sec), Ellis made landfall on the Chinese coast at 060000Z, 164 nm (296 km) southwest of Hong Kong and dissipated rapidly over land thereafter.

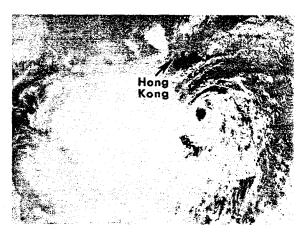
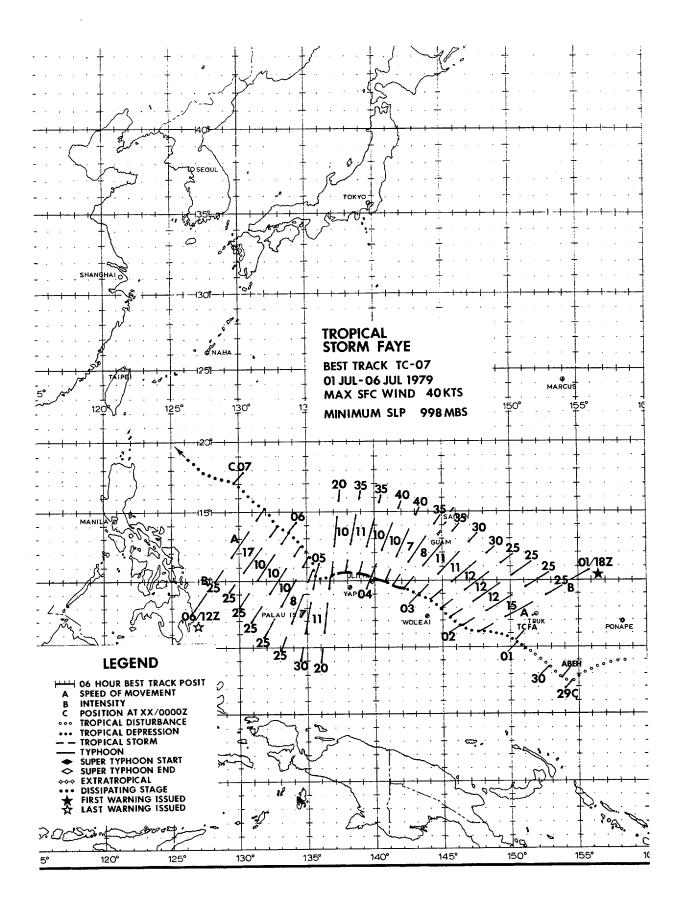


FIGURE 3-06-2. Tropical Storm Ellis as an exposed low-level circulation in the South China Sea, 5 July 1979, 0101Z. (DMSP imagery from Det 5, 1WW, Clark AB, RP)



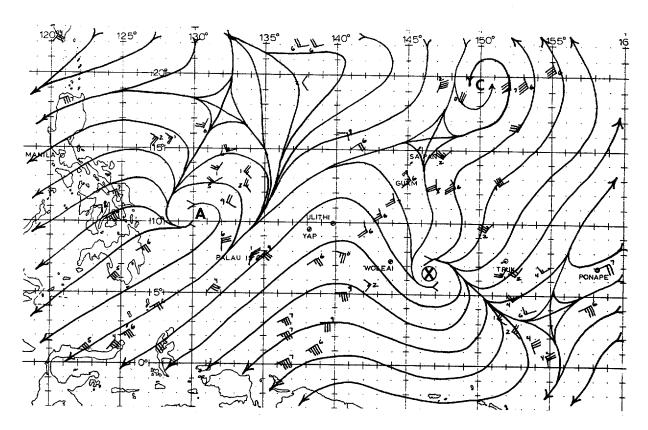


FIGURE 3-07-1. Upper-level streamline analysis ot 020000Z July 1979.

Tropical Storm Faye proved a most interesting case study, not because it developed into an intense tropical cyclone, but because typhoon intensity was not attained as forecast.

TD 07 was first analyzed as a closed surface circulation about 800 nm (1482 km) southeast of Guam on the 28th of June. The associated convective activity remained disorganized until 011200Z July. At that time a TUTT cell developed north of the system; thereby providing an excellent upper-level outflow channel to the northeast (Fig. 3-07-1). The wind data plotted in figures 3-07-1, -3 and -5 are a combination of RAOBS, AIREPS and satellite-derived winds for the 250 mb to 150 mb levels.

Diffluence over TD 07 was extensive and well-defined. The satellite signature also showed improved outflow (Fig. 3-07-2), and further intensification was expected.

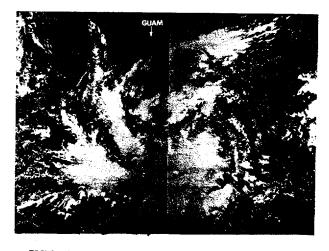


FIGURE 3-07-2. The tropical depression that was to become TS Faye, 02 July 1979, 00222. [DMSP imagery]

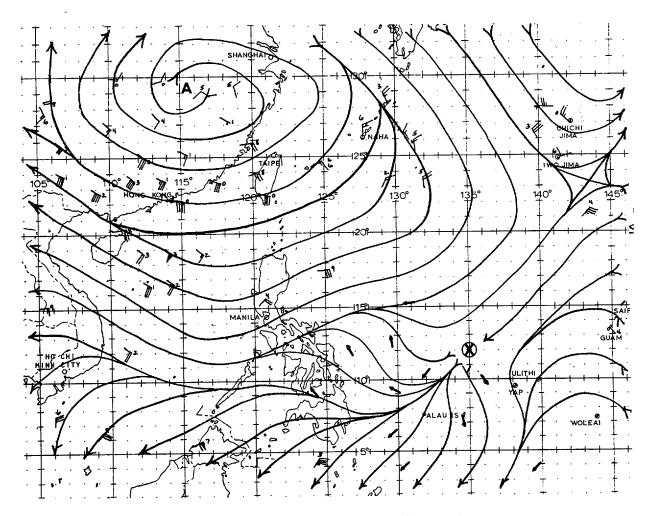


FIGURE 3-07-3. Upper-level streamline analysis at 051200Z July 1979.

The flow pattern over the depression (TD 07) remained favorable for development for the next two days and tropical storm intensity was reached by 031800Z. Continued intensification was still anticipated with typhoon strength forecast within 18 hours.

Instead of intensification, however, Faye weakened. Post-analysis shows that Faye's weakening, and subsequent dissipation, was linked to a radical change in the upper-level flow pattern. Whereas figure 3-07-1 shows a tropical cyclone in excellent position for intensification, figure 3-07-3 shows just the opposite. By 051200Z, a large upper-level anticyclone over China was beginning to build southeastward into the western Pacific toward Faye. Faye's outflow channel to the north became restricted and her low-level circulation center became exposed (Fig. 3-07-4). The mid- to upper-level centers and the associated convection were sheared off to the southwest by increased northeasterly winds at the upper-levels.



FIGURE 3-07-4. TD 07 (FAYE), 05 July 1979, 12027. Strong upper-level northeasterlies have begun to shear off the convection to the southwest. (DMSP imagery, Moonlight Visual)

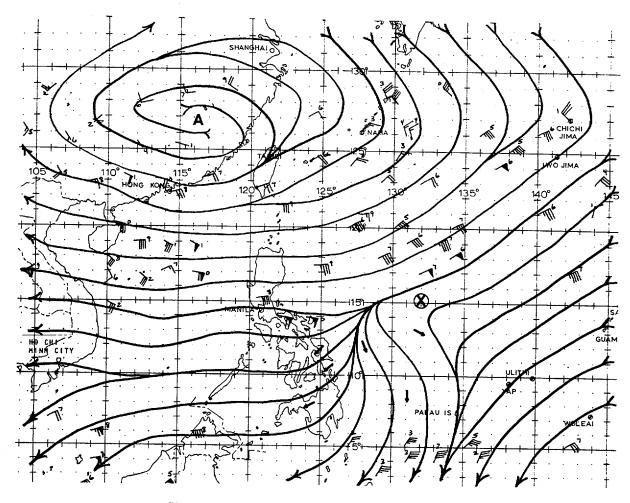


FIGURE 3-07-5. Upper-level streamline analysis at 0612002 July 1979.

Displacement between surface and upper-level centers was observed often during the 1979 season (e.g., see discussions on Hope, Irving, Ellis). Development is usually arrested in this situation, until the system becomes aligned in the vertical. In the case of TS Faye, the upper-level pattern failed to improve. Figure 3-07-5 shows that by 061200Z the upper-level ridge had intruded as far east as Guam and that northeast winds aloft had increased to 50 kt (26 m/sec). At that time, Faye's low-level circulation was fully exposed (Fig. 3-07-6).

This exposed low-level circulation meandered northwestward for two days and eventually dissipated northeast of Luzon.

The short history of Tropical Storm Faye is an excellent example of premature dissipation induced by strong vertical wind shear.

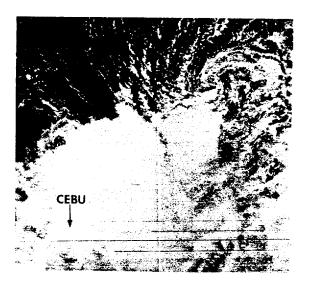
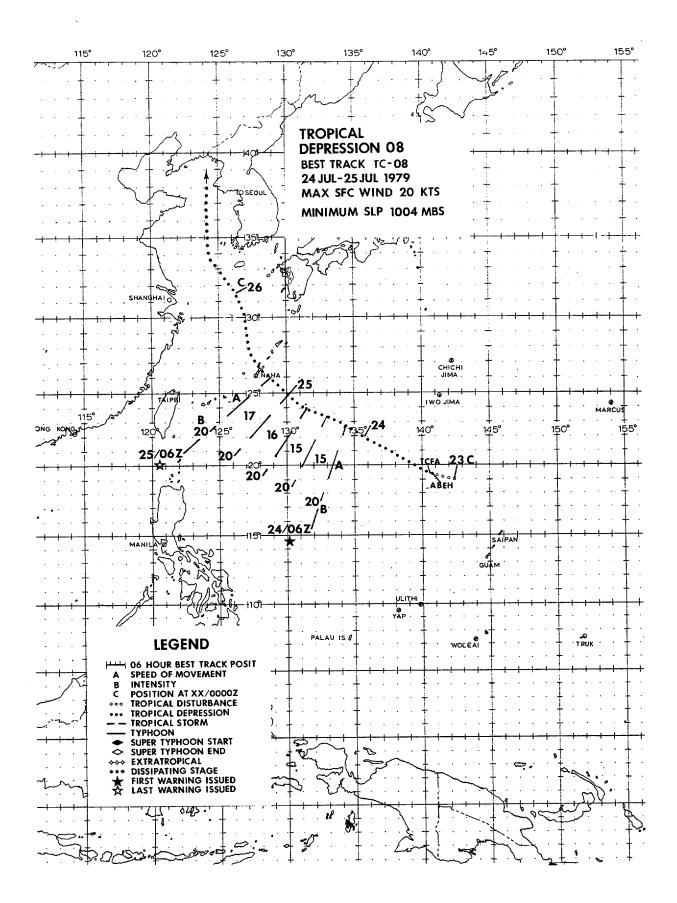


FIGURE 3-07-6. TD 07 (FAVE) is now a fully exposed low-level circulation, 06 July 1979, 1518Z. (DMSP imagery, Moonlight Visual)



## TROPICAL DEPRESSION 08

For the greater part of its life, TD 08 was an exposed low-level circulation with the major convective activity detached to the north of the surface center (Fig. 3-08-1). Aircraft reconnaissance confirmed an exposed surface circulation approximately 100 nm (185 km) south of the convective center at 2410162.

TD 08 was not expected to intensify to

tropical storm strength as a result of tropical storm strength as a result or strong vertical shear which began on 2312002. However, initial warnings were issued based on the forecast track which indicated passage directly over Okinawa.

Post-analysis indicated that the calmwind center did indeed track over Okinawa with most of the convective activity track-

with most of the convective activity track-ing well north of the island.

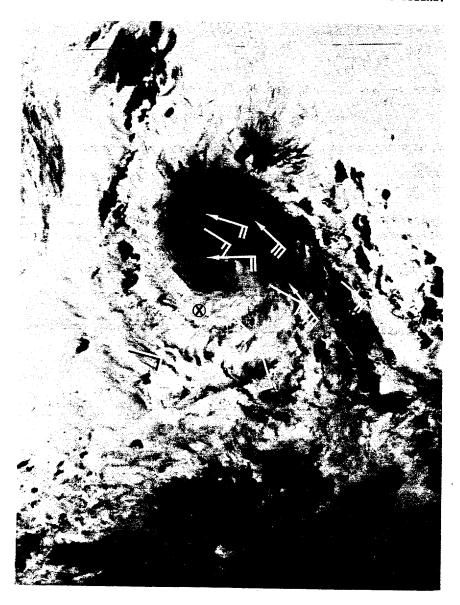
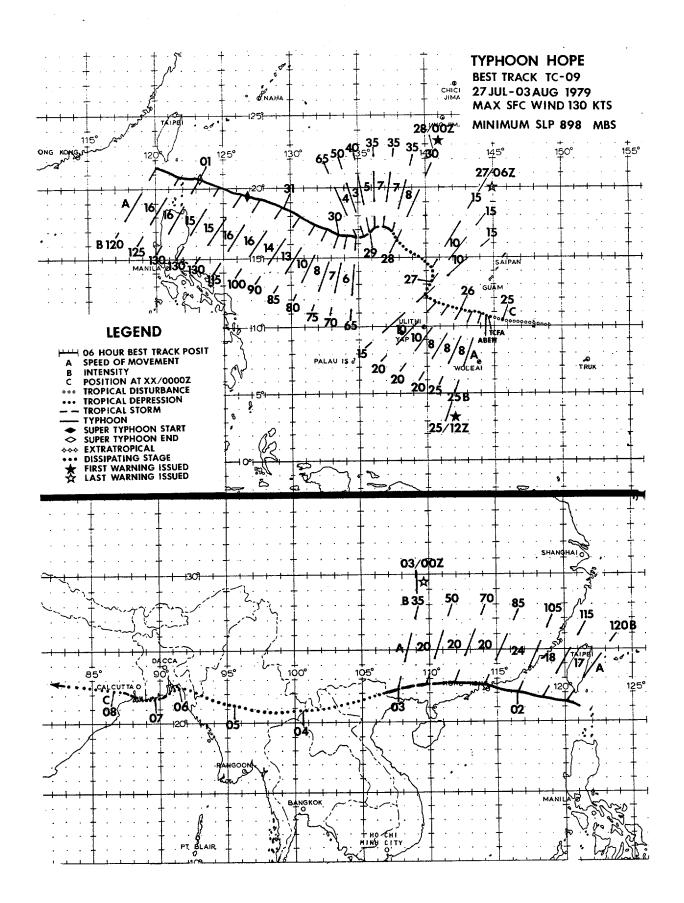


FIGURE 3-08-1. Infrared imagery of TD 08 at maximum intensity of 20 kt [37 m/sec], 24 July 1979, 12447. TD 08's 2412007 surface center [3] is depicted relative to surface ship reports [ ) and 700 mb aircraft reports [ ). (DMSP imagery)



The disturbance which eventually developed into the first super typhoon of 1979 became evident on satellite imagery at 2500002 July as a focal point of cumulus banding. Future intensification was indi cated as the disturbance was situated within an area of strong upper-level diffluence associated with the southern periphery of an east-west oriented TUTT. This outflow mechanism aloft, combined with an improved satellite signature, dictated issuance of a Tropical Cyclone Formation Alert at 2507512; the alert box described an area southwest of Guam. Subsequent aircraft reconnaissance at 2509002 described a cyclonic circulation with wind speeds of 15-25 kt (8-10 m/sec) and a central pressure of 1004 mb centered near 11.1N 144.5E. Based on this aircraft data and the proximity to Guam, the first warning on TD 09 (Hope) was issued at 251200Z.

From the 25th through the 26th of July, while TD 09 (Hope) tracked to the west-northwest, the TUTT axis shifted northward and strong upper-level northeast flow dominated the area. The resultant shear produced by this uni-directional upper-level flow displaced the convective activity to the southwest of the surface circulation, indicating a loss of vertical alignment and subsequent weakening. By 270600Z, the center of the convective activity was displaced 120 nm (222 km) southwest of the low-level circulation center. Surface analyses, at this time, indicated the southwest monsoonal flow was being channeled principally into Tropical Storm Gordon located 750 nm (1389 km) to the northwest of TD 09 (Hope). With further weakening of Hope expected, a final warning was issued at 270451Z advising that the area would be closely monitored for possible

, carrier and a second

regeneration. Post-analysis showed that from £71200Z through 280000Z, the TUTT weakened with resultant reduced shear over TD 09 (Hope). Conditions for development being improved, reorganization took place and TD 09 began to develop. Unfortunately, the improvement in the surface circulation went unnoticed as it occurred during the night when only infrared satellite imagery, on which low-level clouds are difficult to distinguish, was available. An aircraft investigation on the morning of the 28th reported a surface pressure of 999 mb with 45-50 kt (23-27 m/sec) winds in the heavy convective activity to the southwest of the surface center. A warning was issued at 280221Z indicating the regeneration of TD 09 (Hope).

By 280000Z, Tropical Storm Gordon had moved into the Luzon Straits. Due to the orographic blocking of the Philippine land mass, the majority of the strong southwest monsoonal flow was diverted into Hope. This increased low-level inflow coupled with decreasing upper-level shear resulted in a much improved vertical structure with feederband activity developing in the south; 282052Z aircraft reconnaissance supported this improved organization trend. Post-analysis indicates that TD 09 (Hope) could have been upgraded to tropical storm intensihave been upgraded to tropical Scotm Intensity 12-24 hours prior to the warning upgrade at 2900002, as 35-45 kt (18-23 m/sec) winds were reported in feederband activity as much as 24 hours earlier (Fig. 3-09-1). By as 24 hours earlier (Fig. 3-09-1). By 290920Z, a well-defined eye with a central surface pressure of 972 mb and 65-70 kt (33-36 m/sec) surface winds were reported by aircraft data; the 291200Z warning upgraded Hope to a typhoon.

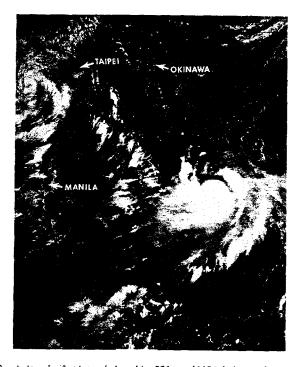


FIGURE 3-09-1. Hope (right) at tropical storm intensity 570 nm (1056 km) northeast of Guam, 29 July 1979, 02192. Tropical Storm Gordon (left) is 100 nm (185 km) east of Hong Kong. (DMSP imagery)

The 291200Z 200 mb analysis indicated the TUTT had again established itself north of Hope. Due to the east-west orientation of the TUTT, strong westerly flow along its southern periphery enhanced Hope's upper-level anticyclonic outflow. Aircraft recon-naissance at 292031Z indicated a sharp decrease in surface pressure to 961 mb with the temperature/dewpoint data correlating to an equivalent potential temperature  $(\theta_e)$  of 359K. An empirically derived forecast aid that relates pressure and  $\theta_{\rm e}$  indicates that once the traces intersect, rapid intensification can be expected within 18-30 hours (Fig. 3-09-2). The intensification equates to a possible mean pressure decrease of 44 mb and a mean wind speed increase of 50-60 kt (26-30 m/sec). Typhoon Hope verified this study 36 hours after the intersection occurred; reconnaissance aircraft reported a surface pressure of 898 mb and wind speeds of 100-120 kt (51-62 m/sec). By 311200Z, Rope attained super typhoon intensity of 130 kt (67 m/sec) (Fig. 3-09-3).

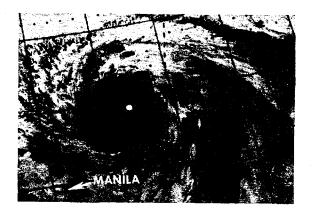


FIGURE 3-09-3. Infrared imagery of Hope just after attaining super typhoon intensity of 130 kt (67 m/sec), 31 July 1979, 12442. (DMSP imagery)

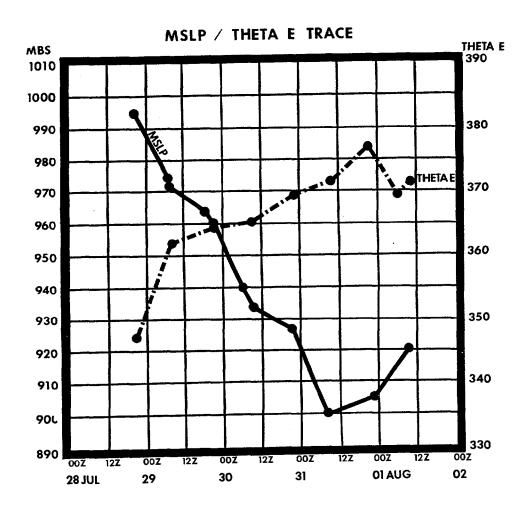


FIGURE 3-09-2. Time cross-section of Hope's minimum sea-level pressure versus equivalent potential temperature (THETA E  $(\theta_e)$ ) derived from aircraft reconnaissance.

Hope entered the Luzon Straits approximately 4 days after Tropical Storm Gordon. Hope's compact wind structure and a slight weakening trend were noted as Heng Chun (WMO 46752) on the southern tip of Taiwan reported sustained winds of 40 kt (21 m/sec) with gusts to 86 kt (44 m/sec) at 011000Z as Hope passed 45 nm (83 km) south of the station. Two persons on the Batanes Islands and one person on Taiwan were killed as a result of the torrential rainfall experienced as Hope tracked through the Luzon Straits.

Typhoon Hope made landfall less than 10 nm (19 km) north of Hong Kong at 0205302 (Fig. 3-09-4) with maximum sustained winds of 70 kt (36 m/sec) and gusts to 110 kt (57 m/sec) reported. Figure 3-09-5 is a time sequence of the surface observations received from the Royal Observatory of Hong Kong during Hope's passage. Extensive wind and rain damage, 3 deaths and over 258 injuries were reported. Damage to shipping within Hong Kong harbor was heavy as 17 ships broke their moorings and 8 ships collided.

Subsequent to passage over Hong Kong, Hope moved into southern China and weakened. The final warning was issued at 030111Z downgrading Hope to tropical storm intensity. Hope's uncomplicated northwest track after development into a typhoon resulted in minimal right-angle track errors with her unexpected acceleration accounting for the majority of the discrepancy.

Although weakening considerably during passage over southeast Asia, Hope did maintain a satellite signature and exited into the northern Bay of Bengal 110 nm (204 km) southeast of Dacca, Pakistan at 0605002.

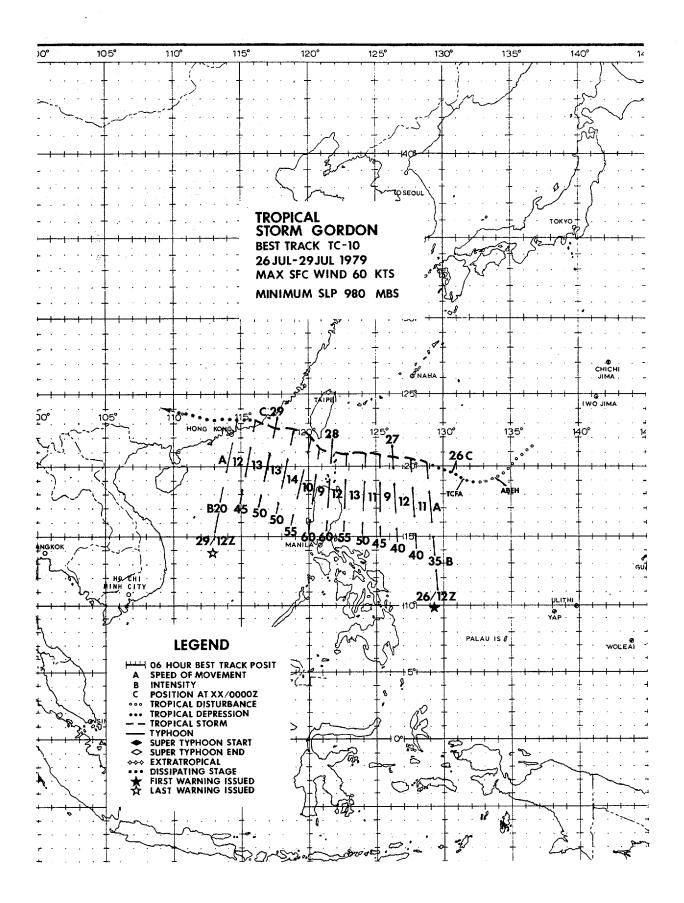


FIGURE 3-09-4. Typhoon Hope at 100 kt {51 m/sec} intensity, 3 hours prior to closest point of approach to Hong Kong, 2 August 1979, 02472. [DMSP imagery]

Strengthened once again by pre-existing strong southwest monsoonal flow, Hope reintensified from 0700002 through 0718002 with maximum sustained winds of 35 kt (18 m/sec) reported on 0712002 surface analysis. A tropical cyclone warning was not issued due to Hope's proximity to land and her expected movement into northeastern India within 12 hours. Hope, however, was discussed at length in the Significant Tropical Weather Advisory (ABEH PGTW).

45005 - HONG KONG OBSERVATORY				ST	HOPE	DATE: 02 JULY 1979 / TIMES: 01-10Z			
02/01z	02/02z	02/03z	02/04z	02/05z	02/06z	02/07z	02/08z	02/09z	02/10z
G39 991	y <u>→</u> 989	984 G49]	978	965 ©79:	960 G83	976 □ G57	: 9 <sup>983</sup>	.:• 988 G54	÷ <b>3</b> 992 ₅

FIGURE 3-09-5. Hourly surface synoptic observations from the Royal Observatory of Hong Kong  $\{ROHK\}$  during passage of Typhoon Hope.



Gordon, the 10th significant tropical cyclone of 1979, developed in late July in the monsoon trough near 20N-135E and eventually made landfall east-northeast of Hong Kong. A stronger sister, Hope (TD 09), followed Gordon several days later on a similar track into Hong Kong. Note that TD 09 (Hope) and TD 10 (Gordon) are alphabetically out of sequence because TD 10 was upgraded to tropical storm stage before TD 09.

Post-analysis revealed that Gordon reached tropical storm intensity at the time of the first warning. CINCPACINST 3140.1N, section 2.5.1., paragraph b states that warnings will be issued when "maximum sustained wind speeds are forecast to increase to 34 or more knots within 48 hours." In this case, there was no lead time between the first warning and tropical storm stage. Figures 3-10-1 and 3-10-2 illustrate why this occurred. TD 10 developed rapidly within the 22-hour time period between these figures. Synoptic data indicated increasing southwest monsoon flow into the area during this period; yet no definitive surface circulation could be located. The most significant finding of the post-analysis was that Gordon could not be traced back 48 hours prior to the first warning from available synoptic and satellite data, and, therefore, falls into the category of a rapid developing system.

Gordon's track took an unexpected jog northwestward while passing south of Taiwan (Fig. 3-10-3). (Typhoon Hope took a similar, but less pronounced, jog.) This northward adjustment is historically evident from tropical cyclones that pass south of Taiwan. The influence of Taiwan's high mountain range is thought to be responsible. As tropical cyclones pass south of Taiwan, they induce lee-side troughing west of the mountains over the Formosa Strait and track northwestward in response.

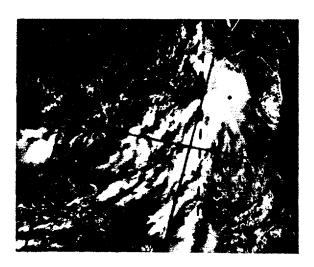


FIGURE 3-10-1. Tropical Storm Gordon in its infancy 4 hours prior to being discussed on the Significant Tropical Weather Advisory (ABEH PGTW), 25 July 1979, 01512. [DMSP imagery]

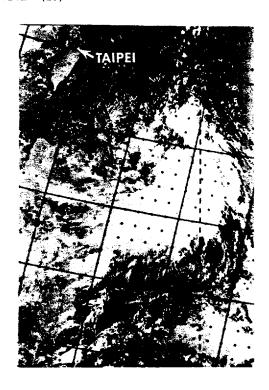
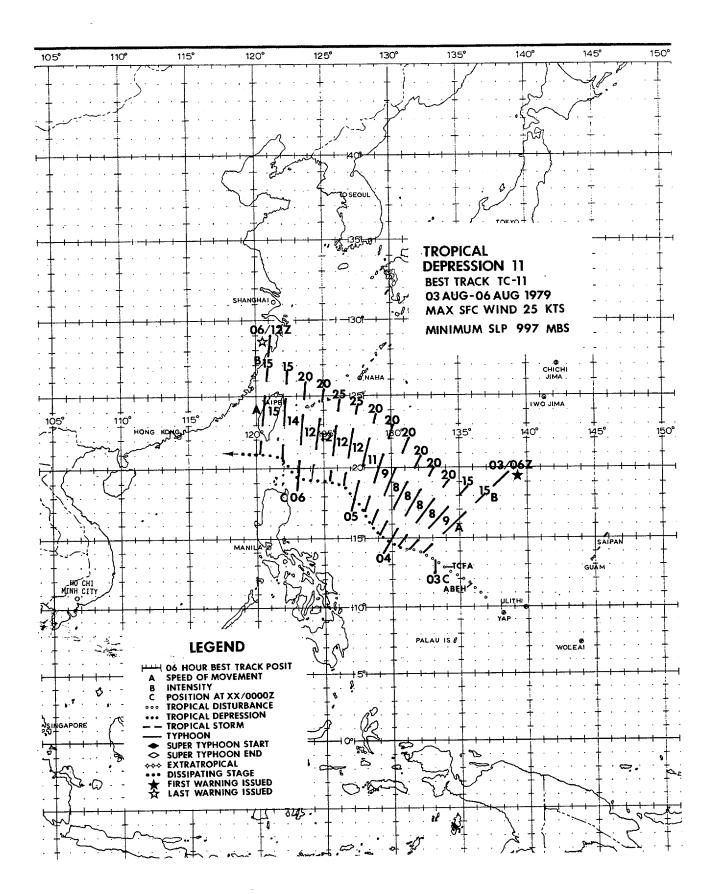


FIGURE 3-10-2. Tropical Storm Gordon 22 hours after Figure 3-10-1 showing increased development, 25 July 1979, 23502. A Tropical Cyclone Formation Alert was issued 6 hours prior to this time. (DMSP imagery)



FIGURE 3-10-3. Kaohsiung radar presentation of Gordon at 2821037 after passing south of Taiwan. (Photograph courtesy of the Central Weather Bureau, Taipei, Taiwan.)



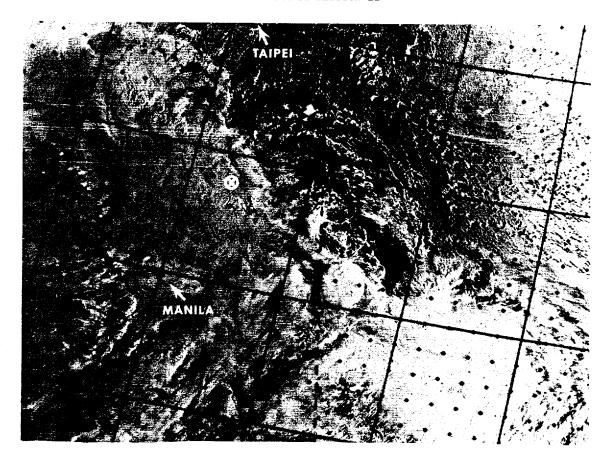
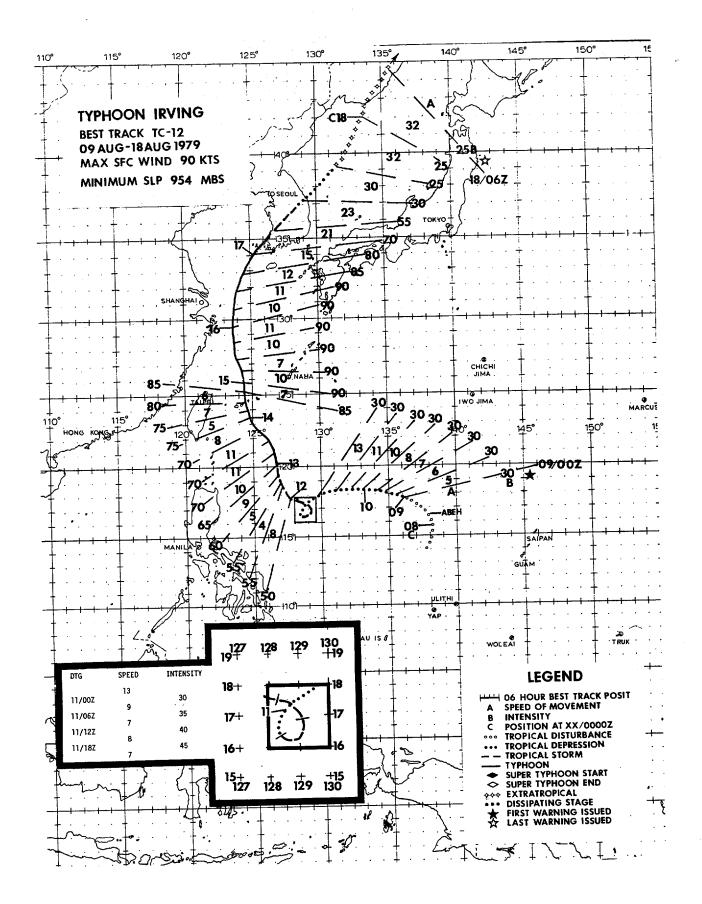


FIGURE 3-11-1. Tropical Depression 11 at 20 kt  $\{10 \text{ m/sec}\}$  intensity, 5 August 1979, 21532. The TD symbol  $\{ \odot \}$  is superimposed at location of surface circulation center as determined by aircraft reconnaissance at 0522222. Considerable vertical shear existed over the system and was the reason that it did not develop into tropical storm strength.  $\{DMSP \text{ imagery}\}$ 



Surges in the southwest monsoon frequent the western North Pacific during the early tropical cyclone season and produce widespread convection from the Malay Peninsula to as far east as Guam. During the same period, the 500 mb monsoon trough fluctuates eastward across the South China Sea (SCS) and occasionally into the Philippine Sea. By late July 1979, an eastward extension of the midlevel monsoon trough was the main synoptic feature west of Guam. The 500 mb trough axis extended along 15N from northern Vietnam through the central SCS and then eastward into a quasi-stationary low pressure center over the Philippine Sea.

On 7 August at 1200Z, a developing surface circulation was observed at the eastern end of the monsoon trough near 14.1N 137.7E. This weak circulation tracked cyclonically around the eastern periphery of the broad 500 mb low pressure center in the Philippine Sea. Taking on the characteristics of a monsoon depression (Ramage, 1971), Irving was described in aircraft reconnaissance data received from 9-11 August as a weak depression with poor vertical alignment and maximum surface winds located 150 to 180 nm (278 to 333 km) west of the surface center. At this stage, Irving displayed an

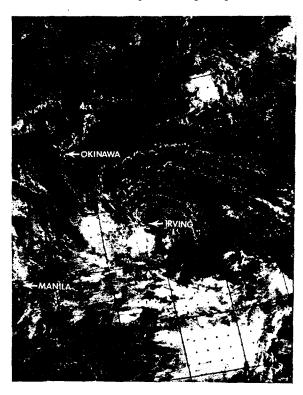


FIGURE 3-12-1. Typhoon Irving as a weak tropical depression with an exposed low-level circulation, 10 August 1979, 01262. Prior to intensification, aircraft reconnaissance consistently observed the maximum convection to the west of the surface center. [DMSP imagery]

exposed low-level circulation in satellite imagery with maximum convection located to the west of the surface center (Fig. 3-12-1). Ship synoptic data during the same period indicated that 25-35 kt (13-18 m/sec) winds extended outward 120 nm (222 km) south of the surface center.

By the llth, the monsoon surge had weakened and receded westward, leaving a cut-off 500 mb low over the Philippine Sea in the vicinity of Irving's surface circulation. Irving executed a small, tight cyclonic loop on the llth. During the loop, vertical alignment between the surface and the 500 mb center improved, and Irving intensified to tropical storm intensity Simultaneously, a break developed in the 500 mb subtropical ridge to the north, and Irving tracked north-northwestward towards the Ryukyu Islands while intensifying further to typhoon strength. Although originally forecast to recurve south of Japan, strengthening of the 500 mb ridge southeast of Japan caused Typhoon Irving to track over the western East China Sea and accelerate northnortheastward across Korea before merging with an extratropical frontal boundary north of Japan.

Although not a spectacular typhoon, Irving's apparent sinusoidal motion, unusually large wind radii, failure to rapidly deepen and damage to southern Korea are noteworthy. Sinusoidal motion of tropical cyclones has been observed for many years, especially when short-term movements are observed by accurate fix platforms such as land radar (Fig. 3-12-2) and reconnaissance aircraft. Sinusoidal motion was observed from 131600Z to 151800Z as Irving tracked north-northwestward through the East China Sea. Radar reports from the Ryukyu Islands

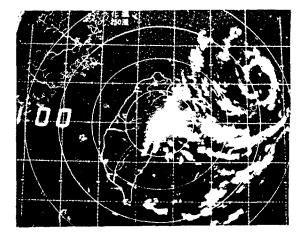


FIGURE 3-12-2. Typhoon Irving as seen by the radar at Haulien, Taiwan. Irving tracked north-northwestward across the southern Ryukyu Islands and was accurately tracked by eight radar sites, 14 August 1979, 1700Z. (Photograph courtesy of the Central Weather Bureau, Taipei, Taiwan)

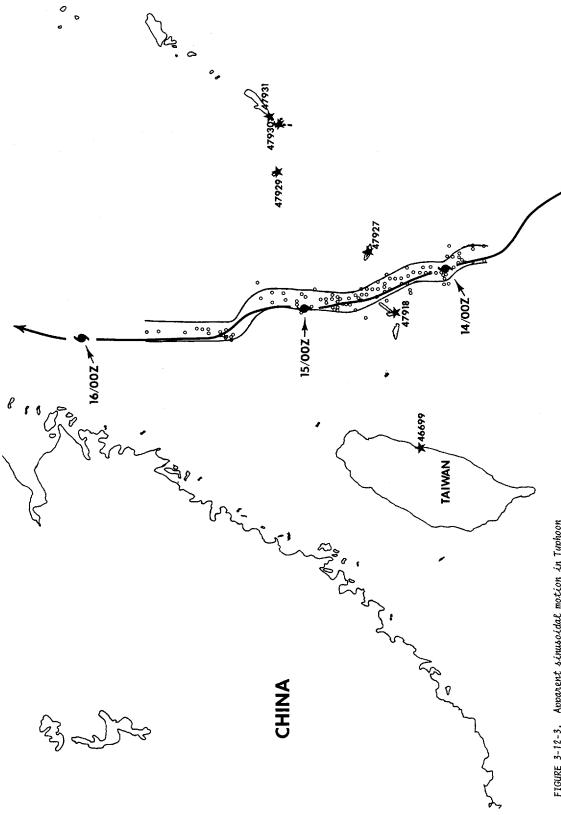


FIGURE 3-12-3. Apparent simusoidal motion in Typhoon Inving's north-northwest track from 1316002 to 1518002 August as observed by land radar stations in the Ryukyu Islands.

clearly indicate that Irving oscillated about an overall north-northwest track (Fig. 3-12-3).

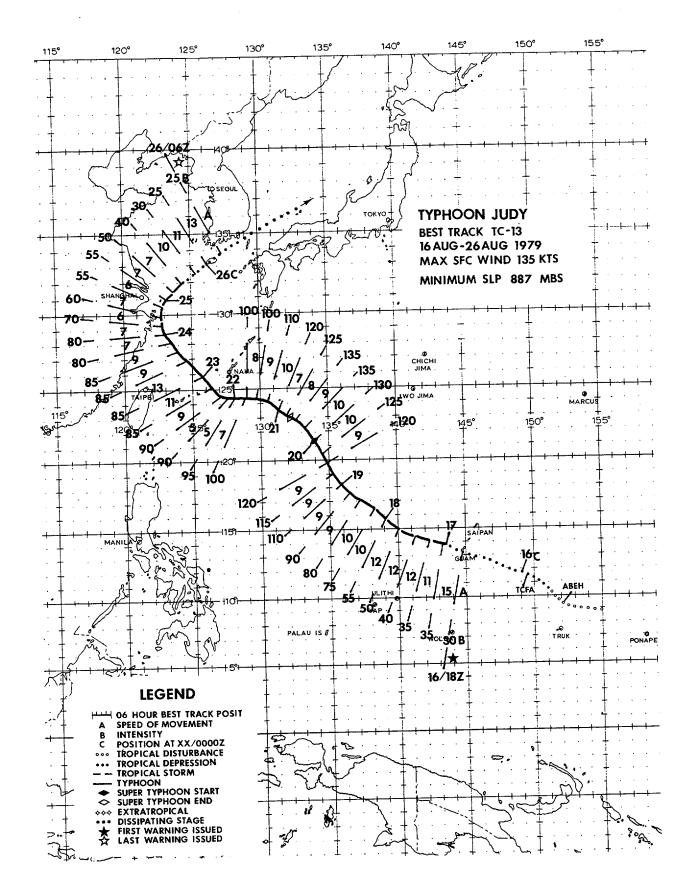
The relationship between Irving's surface and 500 mb centers during the earlier stages of development produced unusually large surface wind radii. Synoptic and aircraft data between 092002 and 1200002 indicate that Irving's maximum wind band actually existed 150-200 nm (278-370 km) west of the large, calm-wind surface center. Although the maximum wind hands did eventually migrate towards the surface center, the wind radii remained large for the duration of Irving. The large wind radii may be related to Irving's developmental interaction with the 500 mb monsoon low and its large areal extent. Irving never became a tight, well-developed tropical cyclone. Aircraft reconnaissance during the period of eyewall development indicated that Irving had a large 30 nm (56 km) diameter eye with the radius of over 30 kt (15 m/sec) winds extending outward 400 nm (741 km) in the eastern semi-circle.

Unlike Super Typhoon Hope, Typhoon Irving (Fig. 3-12-4) did not follow the intensification pattern suggested by JTWC's Equivalent Potential Temperature  $(\theta_e)$ /Minimum Sea-level Pressure Study. This study indicates that sea-level pressure should fall about 44 mb and maximum surface winds should intensify an average of 55 kt from the point where the  $\theta_e$  and pressure curves intersect (see Super Typhoon Hope, Figure 3-09-2). The reason why Irving failed to intensify further is not known.

Typhoon Irving was the first tropical cyclone to strike Korea in 1979. Rapidly weakening as he made landfall, Irving spared southern Korea from the destructive typhoon force winds he had maintained through most of the East China Sea. Korea did, however, receive torrential rains which produced widespread flooding. The hardest hit area was the island of Cheju Do where 4.3 inches (109.7mm) of rain were reported at Cheju. Official estimates reported 150 dead or missing, 1000-2000 homeless and approximately 10-20 million US dollars damage to food and agriculture.



FIGURE 3-12-4. Although Typhoon Irving did not develop according to intensification studies, Irving did possess good feederband activity and cirrus outflow, 14 August 1979, 02282. (DMSP imagery)



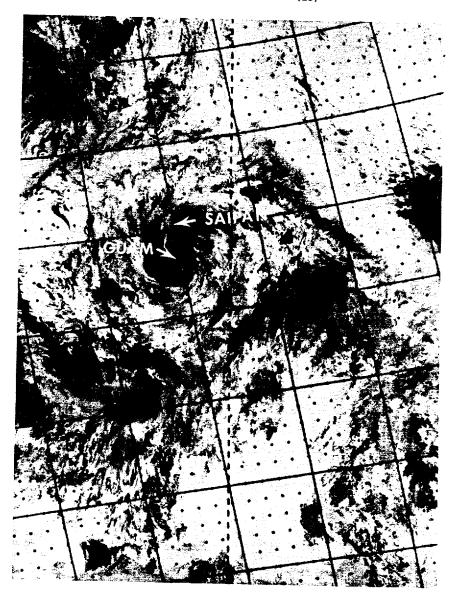


FIGURE 3-13-1. Infrared imagery of tropical disturbance (Judy) while southeast of Guam, 16 August 1979, 11202. The star denotes the approximate location of a weak surface center discovered by a reconnaissance aircraft about 4 hours earlier. [DMSP imagery)

Of all the typhoons of 1979, Judy's significance was only surpassed by Super Typhoon Tip. Judy eventually developed into the year's second super typhoon, but more importantly, she served as a reminder of how rapidly a minor tropical disturbance can develop into a dangerous tropical cyclone.

Surface synoptic data from the beginning to the middle of August showed that the area south and east of Guam was fairly inactive. Good cross-equatorial flow was present, but only a few flare-ups of convective activity were noted. Surface circulations were broad, ill-defined and transient. By 15 August, however, synoptic and satellite data revealed a tropical disturbance, about 120 nm (222 km) east-northeast of Truk, which was to eventually become Typhoon Judy.

This area was closely monitored by JTWC, and when the satellite signature began to improve, a Tropical Cyclone Formation Alert was issued at 1521002.

No significant pressure falls were observed over the area as the disturbance drifted slowly west-northwestward. A reconnaissance aircraft at 160700Z was able to define only a weak surface circulation with a MSLP of approximately 1006 mb and observed surface winds in the south semicircle of 10 kt (5 m/sec) or less (Fig. 3-13-1).

Rapid intensification was not expected at that time, but at 161635Z, less than 10 hours after the aircraft investigation, weather radar at Andersen Air Force Base, Guam, located a well-defined circulation center moving west-northwest toward Guam at 15 kt (28 km/hr). Gradient-level wind reports from Guam, Truk, Palau and Ulithi at 161200Z also showed that the low-level inflow pattern associated with the disturbance had increased in areal extent. The disturbance continued tracking toward Guam and at 161800Z the center passed over the Naval Oceanography Command Center (NAVOCEANCOMCEN), Guam building on Nimitz Hill (Fig. 3-13-2). NAVOCEANCOMCEN reported a MSLP of 1001.0 mb and a wind gust to 51 kt (26 m/sec) at that time. Based on this "first-hand" information, JTWC issued the first warning on Tropical Storm Judy at 161900Z. Post-analysis revealed, however, that Judy did not reach tropical storm strength until 170000Z.

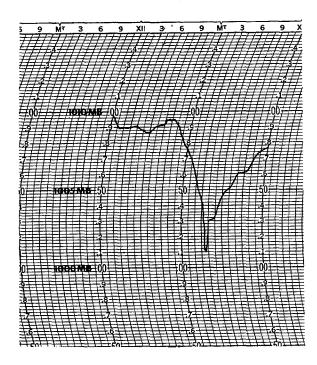


FIGURE 3-13-2. Microbarograph trace recorded at NAVOCEANCOMCEN, Guam during the passage of TD 13 (Judy) at about 1618002, August 1979.

Judy intensified steadily while following a nearly climatological west-northwest track at 10-12 kt (19-22 km/hr) for the next 24 hours. She reached typhoon strength at approximately 1803002. After that, a longwave trough in the mid-level westerlies, moving over Japan toward the Pacific, fractured the subtropical mid-tropospheric ridge north of Judy, allowing her to track more to the northwest.

During the next 36-hour period, after reaching typhoon strength, Judy's central pressure dropped 69 mb and she attained super typhoon strength at 200000Z. Her lowest central pressure, 887 mb, was measured by a reconnaissance aircraft at 192145Z. Three distinct, concentric wall clouds were also noted at that time (Fig. 3-13-3). Super typhoon intensity was maintained until 201500Z, with gradual weakening thereafter.

Forecast aids indicated that Judy would pass to the south of Okinawa, but based on her persistence track and the deep trough that existed over Japan at 500 mb, Judy was forecast to recurve east of Okinawa. The steering aids were reacting to the mid-level PE Forecast series which built the ridge back between Japan and Judy. The numerical forecasts had not been verifying well up to that point, and, thus, the well-entrenched trough was forecast to persist. The numerical forecasts proved to be correct, however, and Judy did pass south of Okinawa before beginning to recurve into the East China Sea.

The rapidly intensifying ridge was expected to drive Judy into the Asian main-land south of Shanghai. The 500 mb analysis at 241200Z provided the first indication that Judy was not going to make landfall. At that time, she was just off the Chinese coast, but north of the mid-level ridge axis. Three-hourly synoptic reports from Sheng-Szu were watched closely and when the winds backed from east at 40 kt (21 m/sec) to north at 35 kt (18 m/sec), there was little doubt that Judy had, in fact, recurved to the northeast.

As Judy recurved, she was downgraded to tropical storm strength based on land synoptic data. Transition to an extratropical system occurred at 261200Z while Judy passed through the Korea Strait.

Due to being still relatively weak while passing over Guam, damage there was insignificant. Damage to Okinawa was also minimal, even though sustained winds of 40 kt (21 m/sec) were experienced for a 28-hour period. Southern Korea did not fare as well, however. One hundred eleven people were killed, over 8,000 houses were inundated, 57 vessels were destroyed and many thousands of acres of crops were ruined by Judy's torrential rains and strong winds.

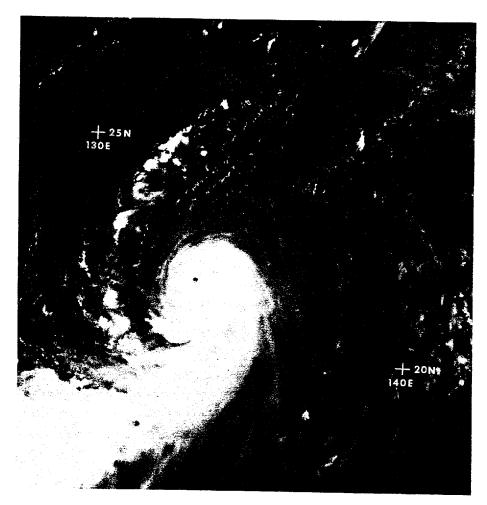
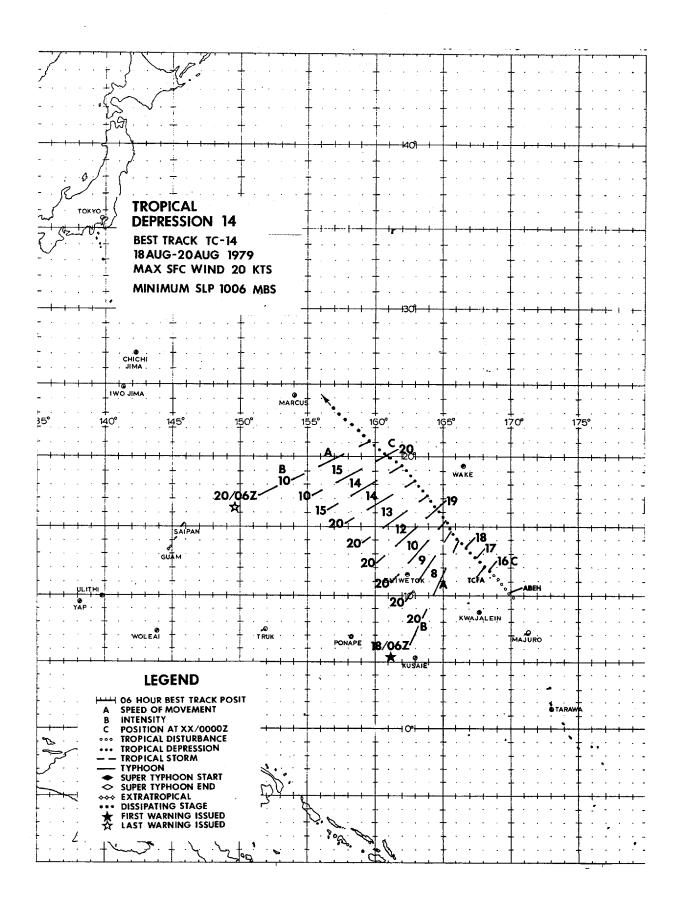
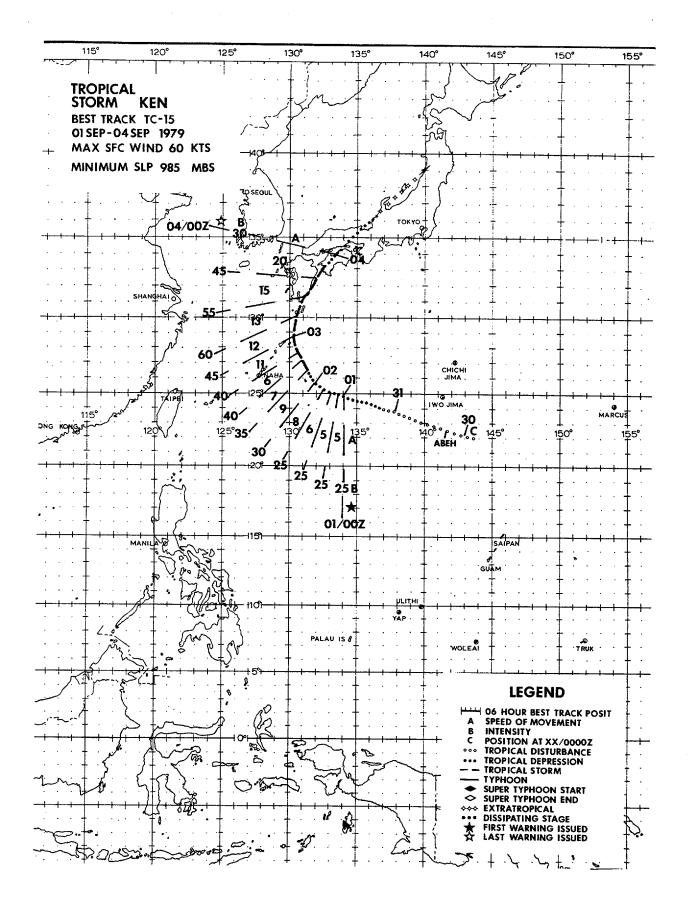
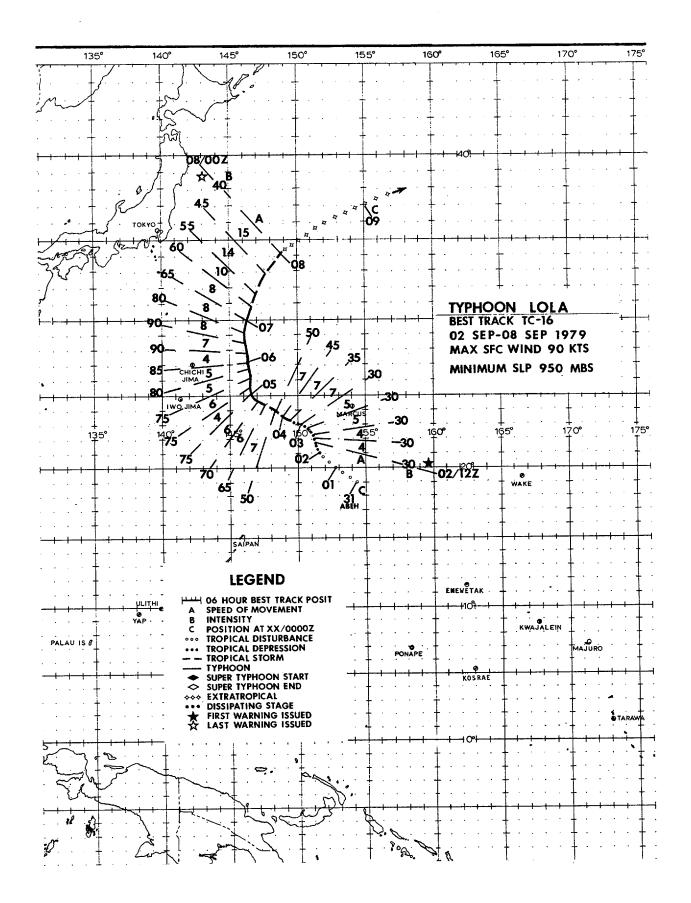


FIGURE 3-13-3. Judy as a super typhoon, 20 August 1979, 02197. (DMSP imagery)







## TROPICAL STORM KEN (15) AND TYPHOON LOLA (16)

Ken and Lola developed almost concurrently along the periphery of an upper-level TUTT. Satellite imagery on 1 September 1979 (Fig. 3-16-1) shows a number of disturbances organized into a line of convection ringing the TUTT in question from north of Kadena to south of Marcus. Ken developed from the disturbance just east of Kadena. At this same time, the disturbance which developed into Lola is south of Marcus and appears quite weak. The largest and most menacing middle disturbance northwest of Guam (Fig. 3-16-1) did not develop.

During the next 48 hours, the TUTT

deepened southwestward over the middle disturbance and suppressed its convection. At the same time, it divided the convective line into the two distinct systems, Ken and Lola (Fig. 3-16-2).

After forming, Ken and Lola began to move in similar recurvature tracks. Ken tracked northward into the Sea of Japan reaching a maximum intensity of 60 kt (31 m/sec). Lola intensified into a typhoon and eventually transitioned into an extratropical system over the cooler waters east of Japan.

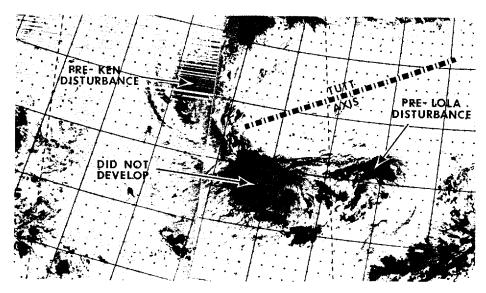


FIGURE 3-16-1. Line of tropical disturbances from which TS Ken and TY Lola eventually developed, 3122572 Aug - 0100392 Sep 1979. (DMSP imagery)

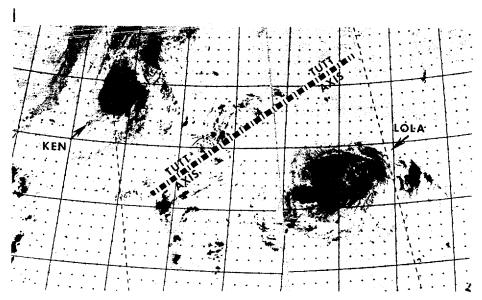
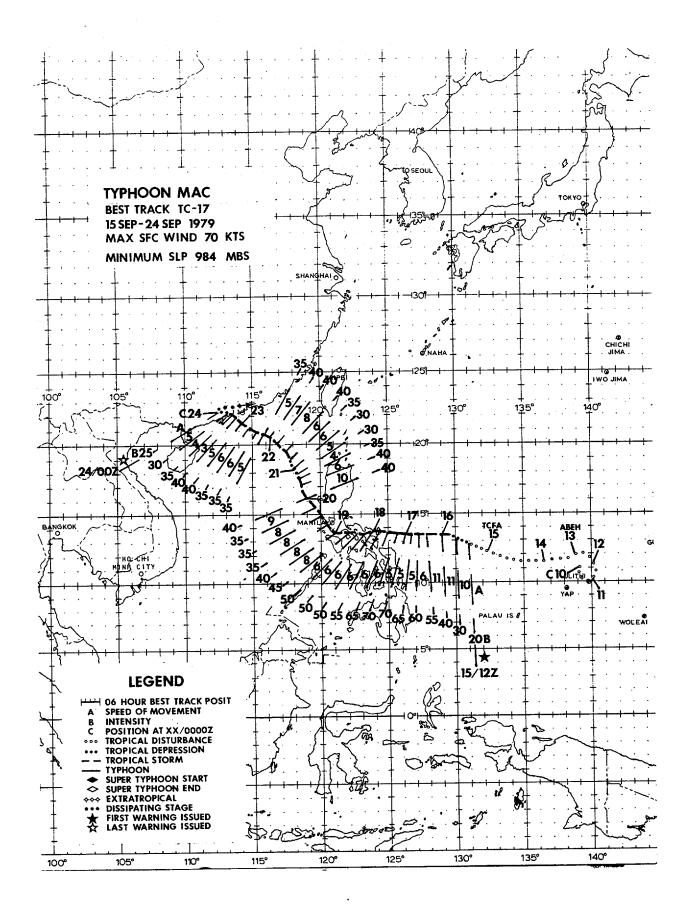


FIGURE 3-16-2. Ken at 45 kt  $\{23 \text{ m/sec}\}$  intensity and Lola at 36 kt  $\{15 \text{ m/sec}\}$  intensity, 022221Z - 030003Z Sep 1979. (DMSP imagery)



Typhoon Mac developed from a weak surface circulation northeast of Yap in September 1979. This circulation tracked westward, reaching tropical storm intensity by 1600002. Mac followed the climatological intensification rate for tropical cyclones approaching the Philippines and reached typhoon intensity prior to making landfall. Frictional effects caused Mac to weaken slowly as he tracked across southern Luzon towards the South China Sea. The unexpected development of Tropical Storm Nancy east of Hai-nan Island influenced Mac's track in the South China Sea.

JTWC's real-time forecasts do not always reflect the actual intensity of a tropical cyclone. Rapid intensification or weakening, peripheral data unavailable due to geographical restrictions, and tight maximum wind bands, which are not initially detected, all reduce the accuracy of intensity estimates provided in tropical cyclone warnings. These intensity discrepancies often go unrecognized until discovered during post-analysis, as in the case of Typhoon Mac.

Reanalysis of aircraft reconnaissance data from 16-18 September indicates that Mac most probably intensified to typhoon intensity by 161800Z. During the period 16-18 September, aircraft reconnaissance at 160503Z reported 68 kt (35 m/sec) at 1500 ft (457 m) and 60 kt (31 m/sec) on the surface prior to encountering moderate turbulence which forced the aircraft to climb through the overcast stratocumulus cloud layer above. Subsequent reconnaissance data at 170810Z confirmed typhoon intensity by locating 80-90 kt (41-46 m/sec) surface winds in a 10-nm (19 km) wide band tucked under the strong eastern feederband. Mac made landfall prior to the next scheduled aircraft fix with geographical constraints severely reducing peripheral data collection.

Although real-time data were available which indicated Mac had possibly reached typhoon intensity, the isolated reports of strong winds were dismissed as gusts associated with lower velocity sustained winds. (Aircraft data are occasionally not used verbatum when they fall outside reasonable limits after being analyzed with available surface reports, satellite data intensity estimates and the JTWC Maximum-Wind Minimum-Pressure Relationship (Atkinson and Holliday, 1977).) During post-analysis, the reconnaissance data were re-examined using an intensity study of tropical cyclones crossing the Philippines (Sikora, 1976). For typhoons with maximum sustained winds of less than 80 kt (41 m/sec), the study shows that an average intensification of 30 kt (15 m/sec) can be expected for tropical cyclones which follow a track similar to Mac's. Reanalysis of the period between 151800Z and 180000Z shows, in fact, that Mac intensified to typhoon intensity before weakening from frictional effects over Catanduanes Island on 18 September (Fig. 3-17-1).

The unexpected development of a second tropical cyclone in the South China Sea (SCS) produced a series of track and intensity modifications in Typhoon Mac. Upon exiting the Philippines, Mac, which was originally forecast to track west-northwest into the SCS, began a Fujiwhara interaction (Fig. 3-18-2) with the rapidly developing Tropical Storm Nancy located near Hai-nan Island. Instead of tracking west-northwest, Mac tracked north-northwest, skirting Cubi Point Naval Air Station, Philippines, on his new track toward Hong Kong. Strong anticyclonic outflow from Nancy sheared Mac's convection towards the southwest with aircraft reconnaissance reporting an exposed low-level circulation of 30-35 kt (15-18 m/sec) intensity on the 20th.

Weak steering currents allowed Nancy to take a cyclonic track across southern Hai-nan Island before heading southwestward into Vietnam. Nancy's southwestward track towards landfall forced Mac further north than originally forecast. Mac eventually passed just south of Hong Kong. Ironically, Nancy's development, which caused Mac to track towards Hong Kong, also helped to spare Hong Kong from potential typhoon force winds. Nancy's upper-level outflow, which dominated the SCS from 19-23 September, produced strong vertical shear over Mac and slowed his rate of reintensification. Typhoon Mac only reached minimal tropical storm intensity prior to making landfall west of Hong Kong.

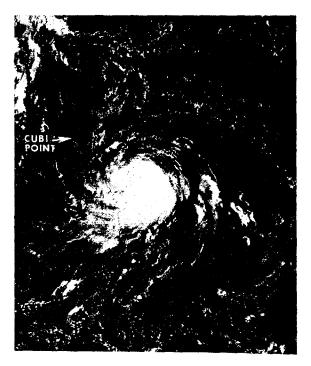
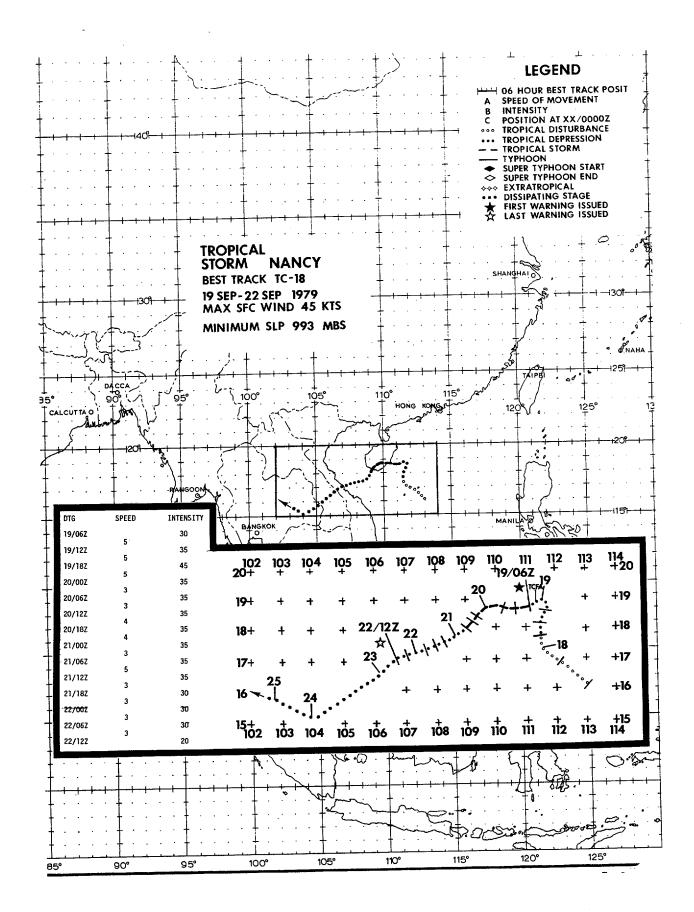


FIGURE 3-17-1. Typhoon Mac after crossing Catanduanes Island, Philippines, 18 September 1979, 00382. (DMSP imagery)



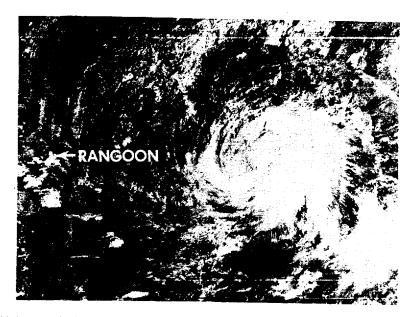


FIGURE 3-18-1. Tropical Storm Nancy at 35 kt [18 m/sec] intensity just after landfall on the southern end of Hai-nan Island, 20 September 1979, 01432. (DMSP imagery from Det 8, 10W, Kadena AB, Okinawa)

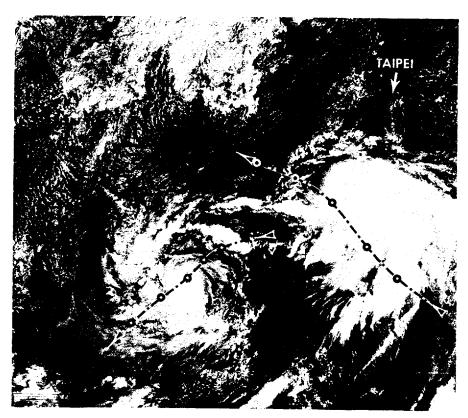
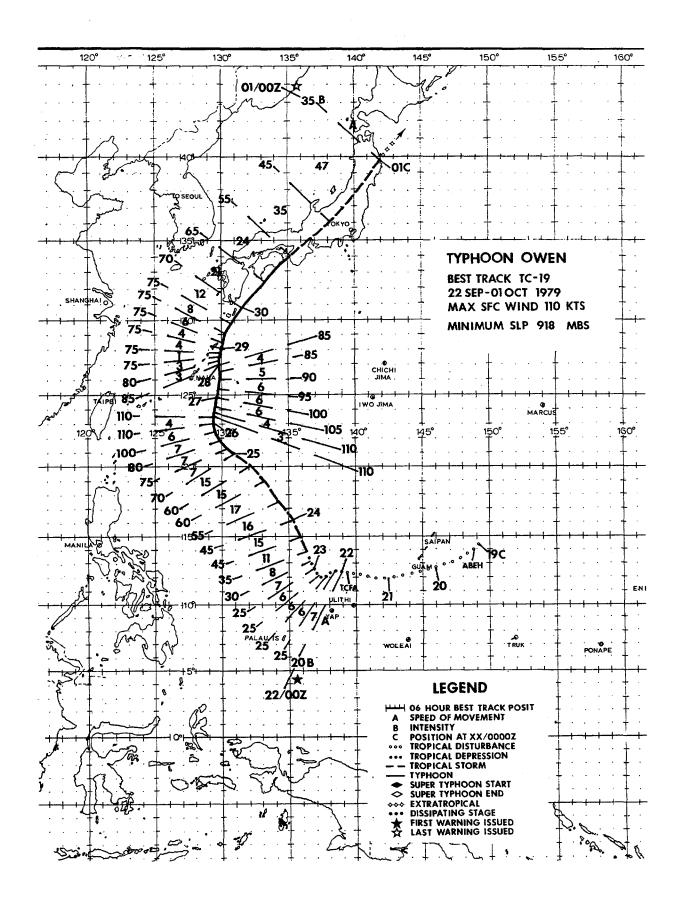


FIGURE 3-18-2. Typhoon Mac and Tropical Storm Nancy undergoing Fujiwhara interaction over the South China Sea, 22 September 1979, 0302Z. The 48-hour tracks before and after picture time are superimposed (Dots bracket 24-hour intervals). (DMSP imagery from Det 5, 1WW, Clark AB, RP)



## TYPHOON OWEN (19)

Typhoon Owen developed from a disturbance which tracked south of Guam during 20 September 1979. Two days later, satellite imagery (Fig. 3-19-1) showed that the system was organizing at the same time that aircraft reconnaissance data indicated a definite surface circulation with a 1000 mb central pressure. This prompted JTWC to issue a tropical depression warning on the system at 220000Z.

During the 2 days prior to and 1 day after 22 September, the system moved on a generally westward track at 5 to 8 kt (9 to 15 km/hr). This speed and direction was in good agreement with climatological tracks. Also, the 500 mb analysis showed a strong subtropical ridge which indicated westward steering. Based on this information, JTWC forecast westward movement for the first 8 warnings. However, Owen unexpectedly turned sharply to the north and began moving at speeds of 15 kt (28 km/hr).

Post-analysis revealed a possible reason for this movement. Figure 3-19-2 shows

the 221200Z analyses at 500 mb and 200 mb superimposed. An upper-level trough is evident on the 200 mb analysis just west of the cyclone. Southerly winds of 50 kt (26 m/sec) were observed on the eastern periphery of the trough. Considerable vertical shear existed in the layer from 500 mb to 200 mb. It appears that the steering and depth of this upper-level trough rather than 500 mb steering was the dominant feature in Owen's movement. Under its influence, Owen tracked generally northward throughout his lifetime, although undergoing major changes in speed. He slowed to a barely perceptible 1-kt (2 km/hr) movement just northeast of Okinawa (at the latitude of the subtropical ridge axis) and then dramatically accelerated to 24 kt (44 km/hr) 36 hours later under vertically consistent westerly steering. At this time, Owen made landfall near Osaka, Japan and began weakening in intensity while still accelerating to 47 kt (87 km/hr). Eventually, he transitioned into an extratropical system but not before reaching a maximum intensity of 110 kt (57 m/sec) (Fig. 3-19-3) on 26 September.

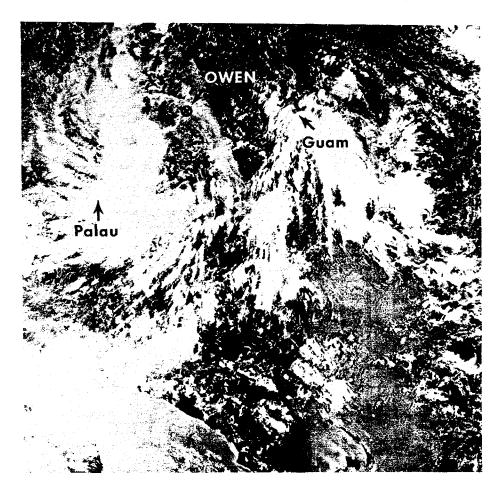
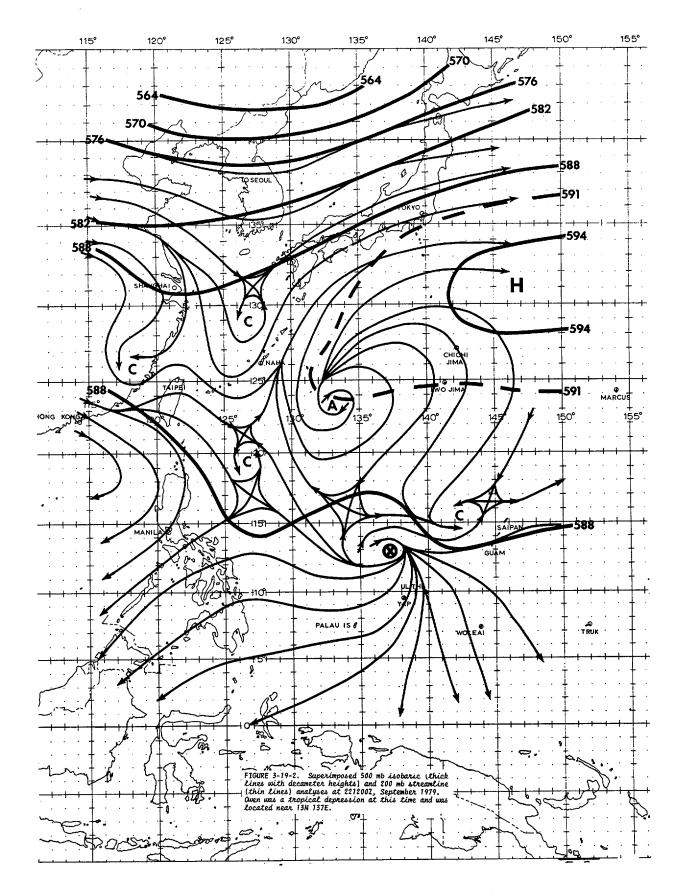


FIGURE 3-19-1. Typhoon Owen as a tropical disturbance, 21 September 1979, 23262. (DMSP imagery)



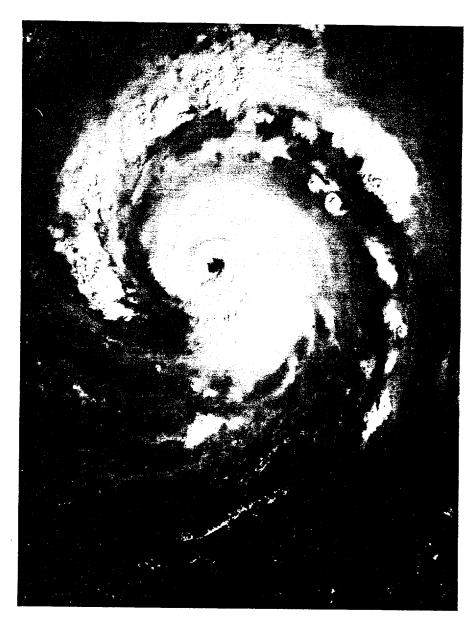
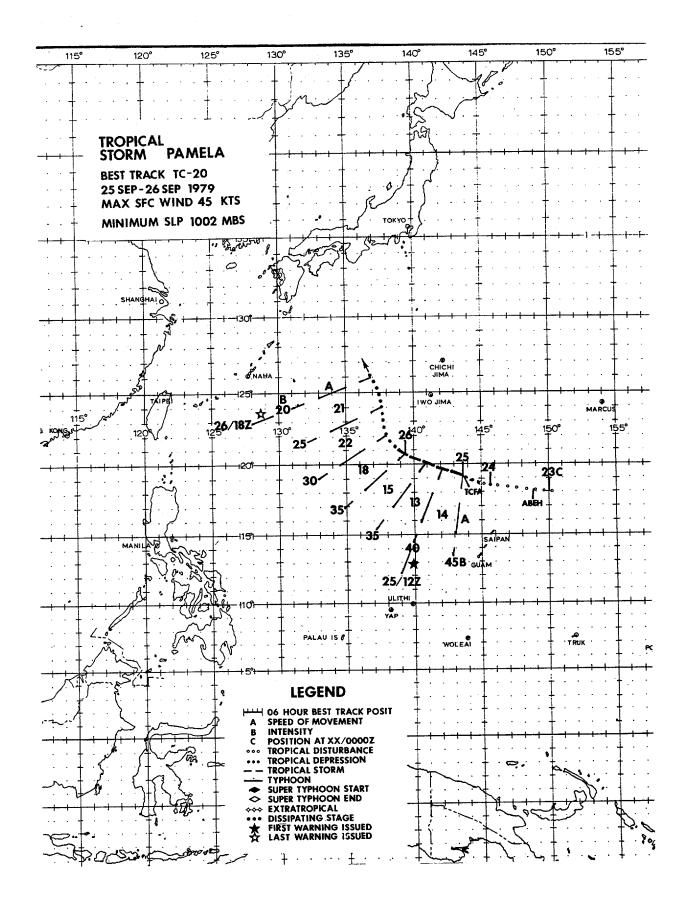


FIGURE 3-19-3. Typhoon Owen at maximum intensity of 110 kt [57 m/sec], 26 September 1979, 01452. (DMSP imagery)



#### TROPICAL STORM PAMELA (20)

Developing at the apex of a wave in the easterly flow in late September 1979, Tropical Storm Pamela tracked westward, north of the Mariana Islands, and dissipated in Typhoon Owen's eastern feeder band under strong vertical shear (Fig. 3-20-1).

A JTWC pressure-wind relationship study (Atkinson and Holliday, 1977) suggested TS Pamela's maximum intensity should have ranged between 25-30 kt (13-15 m/sec) for the concomitant 1002-1003 mb minimum sealevel pressure reported. Instead, aircraft data at 250827Z reported a very narrow,

transient wind band of 60 kt (31 m/sec) north and east of the surface center. The ARWO on this mission indicated that surface winds may have been even higher than the reported 60 kt (31 m/sec). Subsequent aircraft investigations were not able to locate winds greater than 25 kt (13 m/sec). The occurrence of maximum winds which exceed the range of the JTWC tropical cyclone pressure-wind relationship is encountered several times each season. Although several explanations have been offered for these anomalies, none have been substantiated.

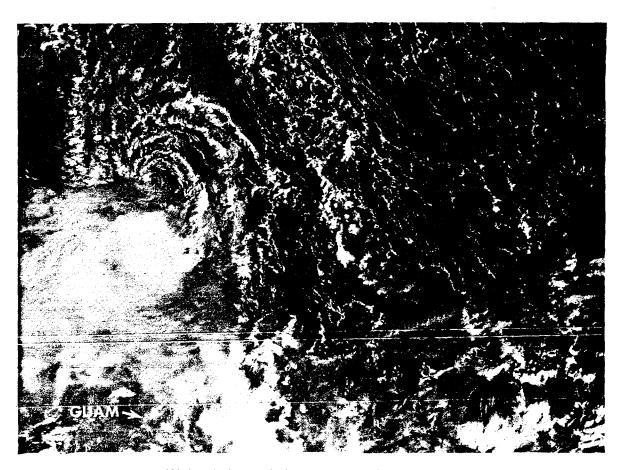
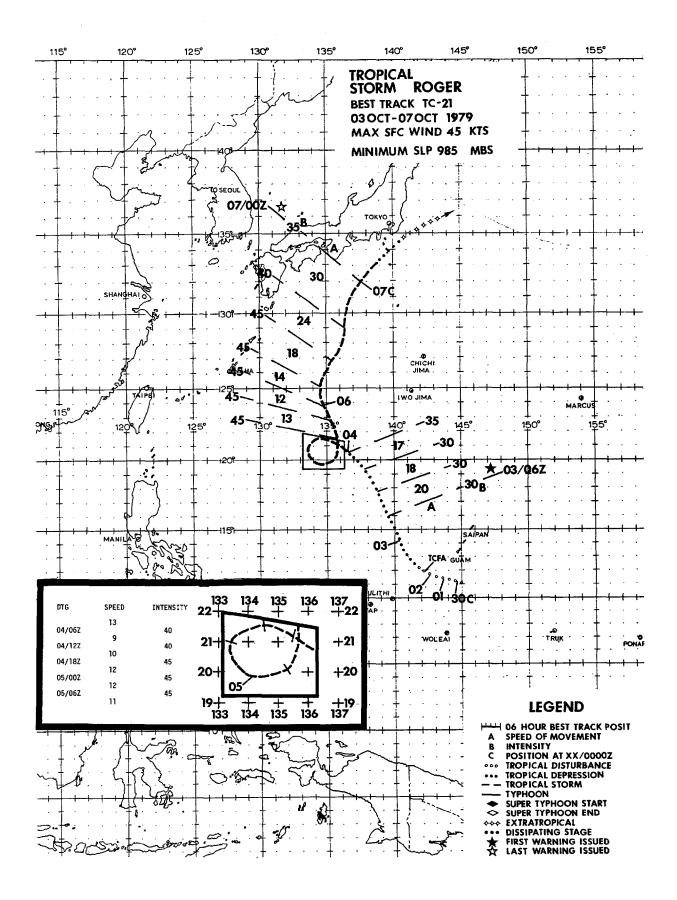


FIGURE 3-20-1. Tropical Storm Pamela with maximum sustained winds of 45 kt (23 m/sec), 24 September 1979, 22327. The exposed low-level circulation was a result of strong vertical shear produced by Typhoon Owen. (DMSP imagery)



As Typhoon Owen began recurving toward Japan, activity increased in the monsoon trough that extended over the Caroline Islands. The increased activity was noted in the Significant Tropical Weather Advisory (ABEH PGTW) on 28 September. For the next 5 days, 2 weak surface circulations and associated cloud clusters within the broad trough, one southwest of Guam and the other southeast of Guam, were closely monitored. As Owen began weakening over Japan, the southwest monsoon flow into the trough oriented NW-SE increased on 30 September, and a line of strong convective activity developed from the southern Philippines to a position south of Guam.

Post-analysis indicated the existence of a weak circulation southwest of Guam which was to become Tropical Storm Roger. During the entire time preceding the issuance of the first warning on Roger, JTWC's attention was focused on another area of major convective activity 5° west of the circulation center which was associated with strong low-level convergence and cyclonic shear. Gradient-level winds at Yap of 56 kt (29 m/sec), Palau 52 kt (27 m/sec) and Guam 28 kt (14 m/sec) are indicative of the strong low-level winds around the periphery of the trough. Thus, the initial and the reissued formation alerts (0206002 Oct and 0222002 Oct) covered the area of heavy convective activity rather than the actual surface circulation center.

Numbered warnings began at 0600Z on 3 October when a reconnaissance aircraft at

030220Z reported a surface pressure of 998 mb and estimated surface winds of 40 kt (21 m/sec) in a band of strong southwesterly flow 60 nm (111 km) south of the surface center. The aircraft also observed a calm wind center at the surface of 30 nm (56 km) in diameter with clear skies over the area.

Synoptic and satellite data at 0312002 indicated that TD 21 was beginning to separate from the broad trough as convective activity was becoming more directly associated with the circulation center (Fig. 3-21-1). TD 21 was upgraded to a tropical storm at 0600Z on 4 October based on 35 kt (18 m/sec) surface winds and a 982 mb sealevel pressure reported by aircraft reconnaissance at 040308Z. Post-analysis indicates tropical storm intensity was attained 6 hours earlier.

A break in the mid-tropospheric subtropical ridge north of Roger existed as Owen recurved over Japan. The strong mid-level southeasterly steering current along the southwestern periphery of the ridge was responsible for Roger's 15 to 20 kt (8 to 10 m/sec) northwestward movement. The ridge retreated eastward between 0000Z and 1200Z on 4 October as a mid-level trough deepened over Korea. The loss of definitive steering flow permitted Roger to execute a cyclonic loop. After emerging from the loop, Roger continued on a northwestward track until north of the ridge axis, after which he accelerated north-northeastward. Extratropical transition was complete by 070600Z as Roger merged with a cold front south of Japan.

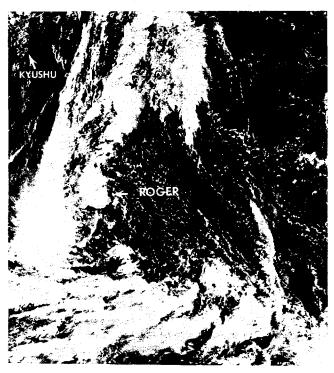
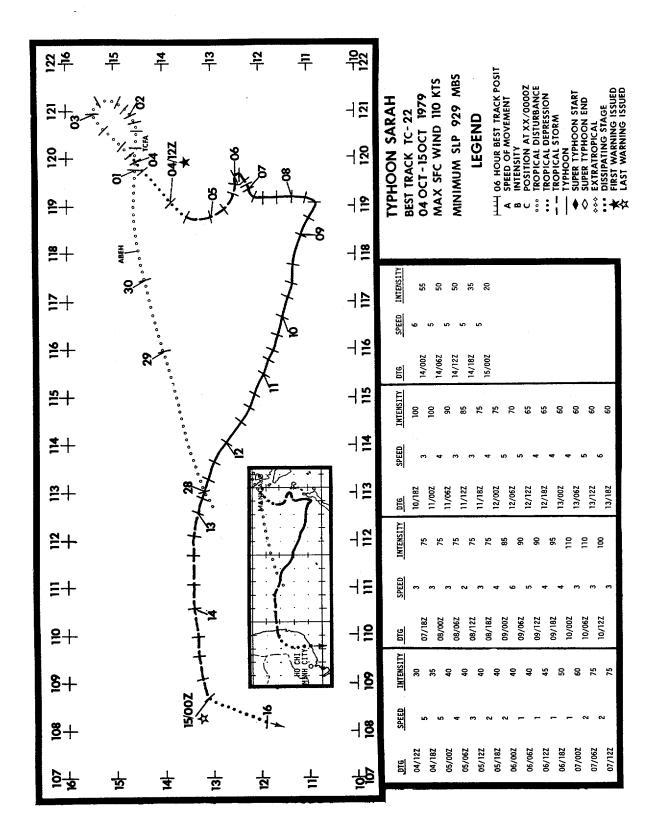


FIGURE 3-21-1. Tropical Storm Roger at 35 kt [18 m/sec] intensity 04 October 1979, 0054Z. (DMSP imagery)



Typhoon Sarah spawned in the monsoonal trough during late September 1979. This trough extended from the southwestern portion of the South China Sea toward Luzon. A northeast monsoon surge existed north of the trough, while the southwest monsoon dominated the area south of the trough. circulation was steered initially by the southwest monsoon and then later by the first northeast surge of the fall from the Asian During the last few days of September, the circulation meandered slowly toward Luzon under the influence of the southwest monsoon, and then looped over Luzon during the first three days of October as a mid-tropospheric short-wave trough moved eastward north of Luzon. Once the short-wave trough had moved east of the circulation, the northeast surge intensified and became more of an influence as the circulation finished its loop and began its south-southwest track.

On 5 and 6 October, Sarah, now a tropical storm, apparently was again influenced by another mid-tropospheric short-wave trough which moved across Sarah's longitudinal position and induced the brief eastward movement in her track. At this time, the southwest monsoon also increased in intensity and may have been another factor in steering Sarah eastward. For almost the entire period that Sarah was tracking southward, there was a weakness in the mid-tropospheric ridge between the Philippines and the Asian mainland, enabling Sarah's track to be influenced by short-wave troughs. This weakness in the ridge resulted in midtropospheric flow that was too weak to significantly affect the steering of Sarah. This weakness allowed the surface winds to dictate Sarah's direction of motion through the first 8 days of October. Figures 3-22-1 and 3-22-2 illustrate the surface and midlevel flow patterns which influenced Sarah during this phase of her track.

During Sarah's depression stage, strong easterlies in the upper-troposphere restricted Sarah's outflow to the northeast, thus inhibiting development into a tropical storm. As Sarah proceeded southward, the easterlies decreased in strength, outflow increased, and Sarah intensified to tropical storm and then typhoon strength. It is very interesting to note that Sarah intensified to typhoon strength while tracking southward which is quite unusual for a tropical cyclone. Several aircraft reconnaissance flights reported that Sarah had attained typhoon strength even though her cloud structure was not well organized.

During the first several days of October when Sarah was slowly developing to typhoon strength and moving south, Palawan Island and the central Philippines were battered by high winds and rain. These areas were inundated by flooding and landslides which caused massive crop damage and death. Many villages were cut off from any

source of food, fresh water, and other necessities for survival. Four deaths were attributed to Sarah. On 8 October, Sarah finally began to track westward and the weather finally cleared over Palawan Island and the central Philippines. Sarah's change in track was due to the strengthening of the mid-tropospheric ridge north of Sarah from Luzon across the South China Sea into Asia. Aircraft reconnaissance early on the 9th reported that Sarah's structure had become better organized. Earlier aircraft reported that Sarah was not vertically aligned; but on the 9th, the mid-level center had become vertically aligned with the surface center. With vertical alignment and improved upperlevel outflow, Sarah's intensity increased to 110 kt (57 m/sec) as she became a most impressive storm. This is in contrast to her unusual origin.

After Sarah reached peak intensity early on 10 October, she began to slowly weaken as



FIGURE 3-22-3. Sarah with 60 kt [31 m/sec] intensity one day prior to landfall over Vietnam, 13 October 1979, 0136Z. (DMSP imagery)

she tracked west-northwestward (Fig. 3-22-3). Sarah continued on a west-northwest track until dissipation over Vietnam on 17 October. After 20 days, she dissipated within 300 nm (556 km) of her origin as a monsoon depression on 28 September.

FIGURES 3-22-1 and 3-22-2 are on following pages.

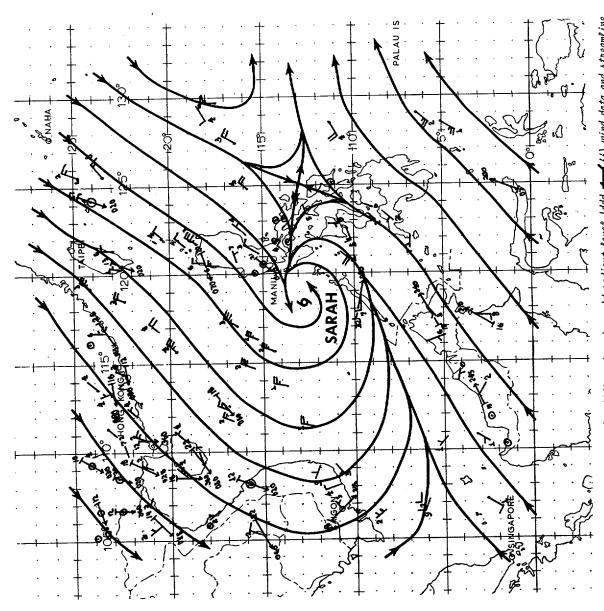
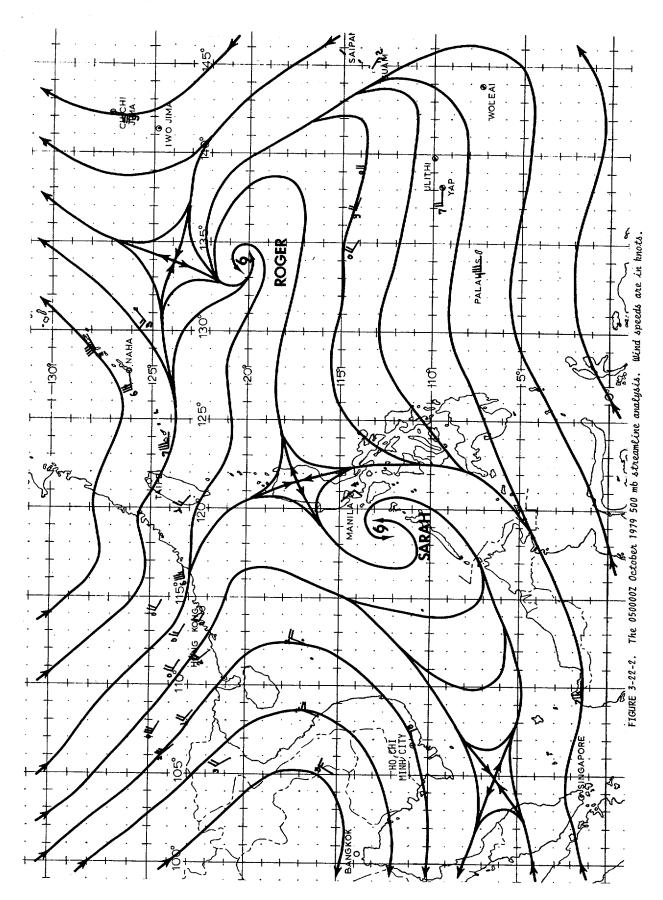
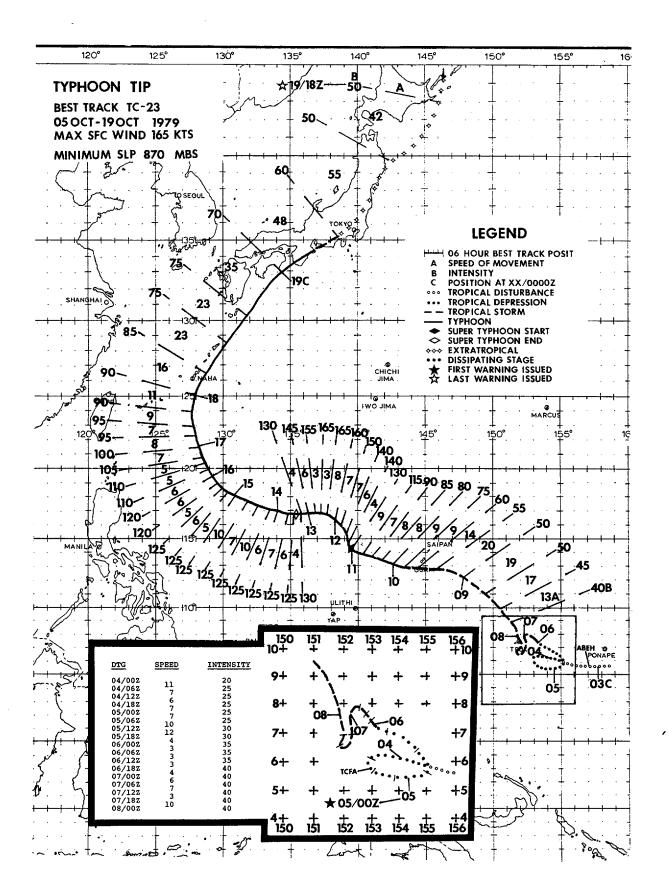


FIGURE 3-22-1. The 0500001 October 1979 surface ( $-\eta$ )/gradient-level (ddd -(56) wind data and streamline analysis. Wind speeds are in knots.





Super Typhoon Tip was the most significant typhoon of the 1979 season, and possibly the most significant tropical cyclone this century. Forty aircraft reconnaissance missions were flown on Tip, which produced 60 fixes, and thus made it one of the most closely watched cyclones in recent memory. Aircraft and synoptic data showed that Tip achieved the lowest sea-level pressure ever observed in a tropical cyclone (870 mb) and also had the largest circulation pattern on record (nearly 1200 nm (2222 km) in diameter).

Satellite and synoptic data during the early part of October revealed an active monsoon trough that extended from the Marshall Islands through the Caroline Islands to Luzon. Three distinct circulations developed in this trough: One near Manila, which would become Typhoon Sarah; another southwest of Guam, which would become Tropical Storm Roger; and the last between Truk and Ponape, which was destined to become Super Typhoon Tip.

It is not possible to discuss the development of Tip without, at the same time, examining the development of TS Roger. The surface analysis for 030000Z showed the three circulations in the monsoon trough with strong cross-equatorial flow, most of which was feeding into TS Roger. This situation was enhanced, in part, by an extratropical trough north of Roger over Southern Japan. The split in the surface flow pattern near Guam tended to keep Tip from developing rapidly while southeast of Guam. The upperlevel analysis at the same time showed a large anticyclone north of Guam in close association with TS Roger and a developing TUTT cell about 300 nm (556 km) east of Marcus Island. The TUTT cell was moving slowly westward. Only strong upper-level northeasterlies existed over Truk and Ponape.

The satellite signature of the tropical disturbance near Truk continued to show improvement despite the initially unfavorable upper-air pattern. A Tropical Cyclone Formation Alert was issued at 040900Z, when a reconnaissance aircraft found a closed surface circulation about 120 nm (222 km) southeast of Truk with a MSLP of 1003.9 mb and a maximum observed surface wind of 25 kt (13 m/sec).

A reconnaissance aircraft fixed the disturbance the following day about 100 nm (185 km) southeast of the previous position. Based on indications of continual development, the first warning on TD 23 was issued at 050000Z. Although the surface pressure did not drop significantly, the observed surface winds did increase, and as a result, TD 23 was upgraded to Tropical Storm Tip at 060000Z.

During the period from 050000Z to 071800Z, TS Tip gave the JTWC forecasters a striking example of what the term "erratic movement" really means. TS Tip first executed a cyclonic loop southeast of Truk, then accelerated to the northwest, only to stall and meander to a position south of Truk. It was difficult to keep track of

The second second second

TS Tip's surface position during this period. The best track is based almost entirely on aircraft surface positions, because the satellite fixes were based on upper-level outflow centers, and even the 700 mb center, as observed by aircraft reconnaissance, was considerably displaced from the surface center. Changes in the surface wind direction reported by Truk assisted JTWC in monitoring TS Tip during this period of erratic behavior.

Post-analysis shows that Tip's slow development and early erratic behavior are related to the weak, yet extensive circulation patterns that were associated with TS Roger. While near Truk, TS Tip was still competing with TS Roger for strong southerly surface inflow and, until the 8th, was coming out second best. During the period of erratic movement, JTWC continued to forecast a northwestward track with passage south of Guam. These forecasts were based primarily on the mid-level steering winds observed at Guam and obtained by the reconnaissance aircraft. These fairly strong winds were from the southeast and were expected to steer Tip toward Guam. However, at this stage of development, Tip was evidently too far south of this wind band and the steering in the immediate vicinity of Tip remained weak.

On 8 October, the expected northwest movement began. Roger was far to the north becoming extratropical, and the southerly winds that had been flowing north began to veer toward Tip. The TUTT cell earlier near Marcus Island migrated to a position northwest of Guam, affording Tip an excellent outflow channel to the north. Synoptic and subsequent aircraft data revealed that the southeasterly mid-level winds finally began to influence TS Tip, and the 0802082 aircraft fix confirmed that Tip was heading toward Guam at approximately 13 kt (24 km/hr). The minimum sea level pressure dropped to 995 mb and surface winds were 40 kt (21 m/sec).

Tropical Storm Tip continued to intensify and accelerate, eventually to 20 kt (37 km/hr) as he headed toward Guam. Until 6 hours before reaching Guam, Tip's persistence track and JTWC's forecasts indicated that he would pass directly over the center of the island. Six hours before expected landfall, however, reconnaissance aircraft and radar positions from Andersen AFB showed that TS Tip had turned to the west. Tip actually passed south of Guam, reaching CPA at about 25 nm (46 km) south of the southern end of the island at 091015Z. Maximum winds of 48 kt (25 m/sec) with gusts to 64 kt (33 m/sec) were recorded at the Naval Oceanography Command Center on Nimitz Hill. Andersen AFB recorded 6.5 inches of rain between 081800Z and 091800Z, and an additional 2.61 inches between 091800Z and 091900Z.

Shortly after passing Guam, Tip reached typhoon strength and continued on a basic west-northwest track. The analyses over the next few days showed that Typhoon Tip was moving into an area of strong upper-level divergence which appeared to cover most of

the western Pacific. Rapid intensification was forecast based upon the favorable upper-level pattern and the continued drop in surface pressure as observed by the reconnaissance aircraft. Intensification was much more rapid than expected, however, as the pressure between the 9th and the 11th dropped 98 mb to 898 mb. Tip reached super typhoon strength at that time with maximum winds of 130 kt (67 m/sec) reported by aircraft reconnaissance. The surface analyses revealed that the circulation pattern associated with Typhoon Tip had increased to a diameter of 1200 nm (2222 km) which broke the previous record of 720 nm (1333 km) set by Typhoon Marge in August 1951.

Super Typhoon Tip intensified still further, and at 120353Z, a reconnaissance aircraft recorded the lowest sea-level pressure ever observed in a tropical cyclone: 870 mb. This was 6 mb lower than the previous record set by Super Typhoon June in November 1975. The 700 mb height was 1944 meters and the 700 mb temperature within the eye was an exceptionally high 30° C (Fig. 3-23-1). The Aerial Reconnaissance Weather Officer (ARWO) on that particular mission remarked that "...one unusual feature was the spiral striations on the wall cloud. It looked like a double helix spiraling from the base of the wall cloud to the top, making about two revolutions in

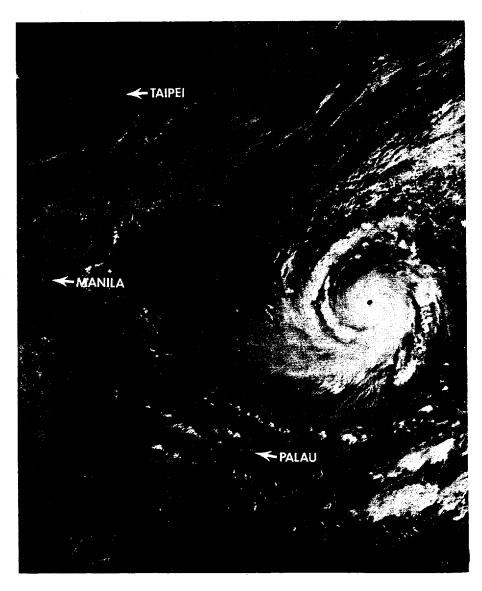


FIGURE 3-23-1. Super Typhoon Tip shortly before the record MSLP of 870 mb was observed by reconnaissance aircra(t, 12 October 1979, 0012Z. [DMSP imagery].

climbing."1 Tip maintained super typhoon strength for the next 54 hours while moving to the northwest at between 3 and 7 kt (6 and 13 km/hr). Estimated maximum wind intensity of 165 kt (85 m/sec) was reached at 120600Z.

The immense circulation pattern associated with Typhoon Tip extended from the surface through 500 mb (and probably higher) and essentially split the subtropical midtropospheric ridge south of Japan. This would have allowed an average typhoon to recurve sharply to the north, but Tip was an atypical system and the northwestward movement persisted for the next three days.

Steering forecast aids were useless during this period because they merely steered Tip in his own large storm-induced flow. Persistence and climatology became the primary forecast aids during this stage in Tip's life.

From the 13th to the 17th, the radius of surface and gradient-level 30 kt (15 m/sec) or greater winds extended over 600 nm (1111 km) from Typhoon Tip's center. The radius of over 50 kt (26 m/sec) winds was over 150 nm (278 km) (Fig. 3-23-2). The aircraft reconnaissance data likewise showed that 700 mb winds of 105 kt (54 m/sec) existed more than 120 nm (222 km) from Tip's center during this period (Fig. 3-23-3).

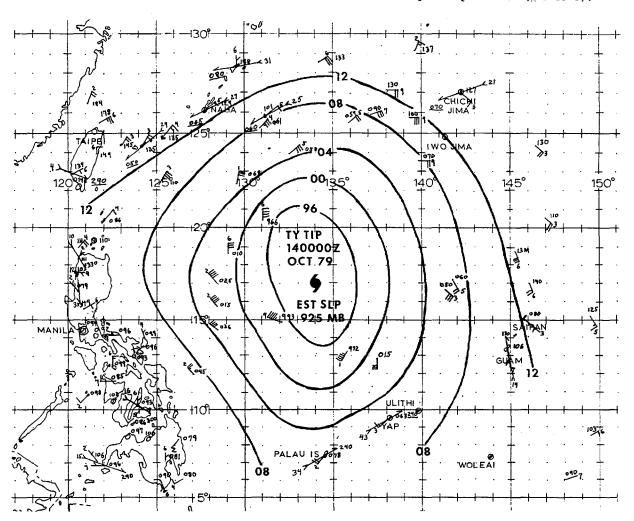


FIGURE 3-23-2. The 1400007 October 1979 surface ( )/gradient-level (ddd / (ff) wind data and pressure analysis in the vicinity of Super Typhoon Tip. Wind speeds are in knots.

lpatrick w. GIESE, Capt, USAF: Mission ARWO.

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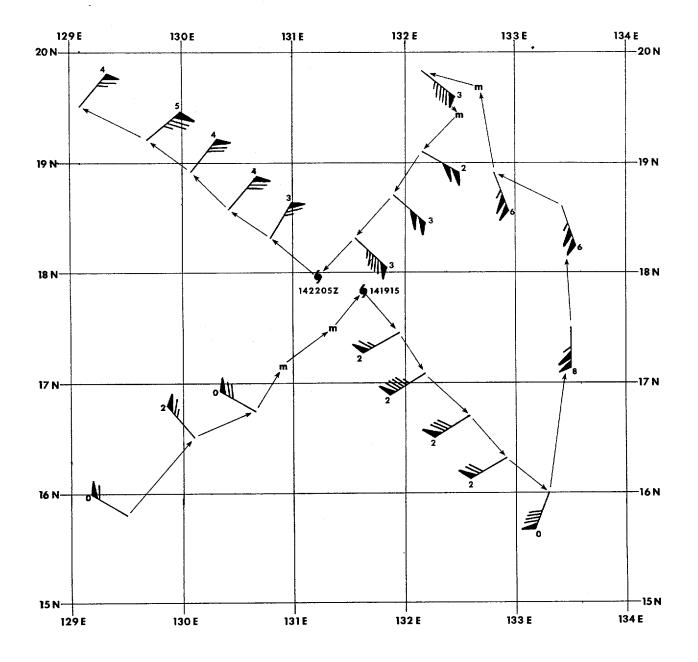


FIGURE 3-23-3. Plot of aircraft reconnaissance data from the 26th mission into Super Typhoon Tip on 15 October 1979. Tip's positions were fixed at 1419157 and 1422052. Wind barbs are the measured 700 mb winds. The tens digit of the wind direction is also plotted with the wind barbs. An "m" indicates no 700 mb wind data available.

After the 17th, Tip began to weaken as the large circulation pattern began to shrink. This, together with the effects of a mid-level trough moving toward Japan from China, caused Tip to begin tracking northward. By the 18th, he was accelerating to the northeast under the influence of the increased mid-level southwesterlies.

During recurvature, Tip passed within 35 nm (65 km) of Kadena AB on Okinawa, which reported maximum sustained winds of 38 kt (20 m/sec) with gusts to 61 kt (31 m/sec).

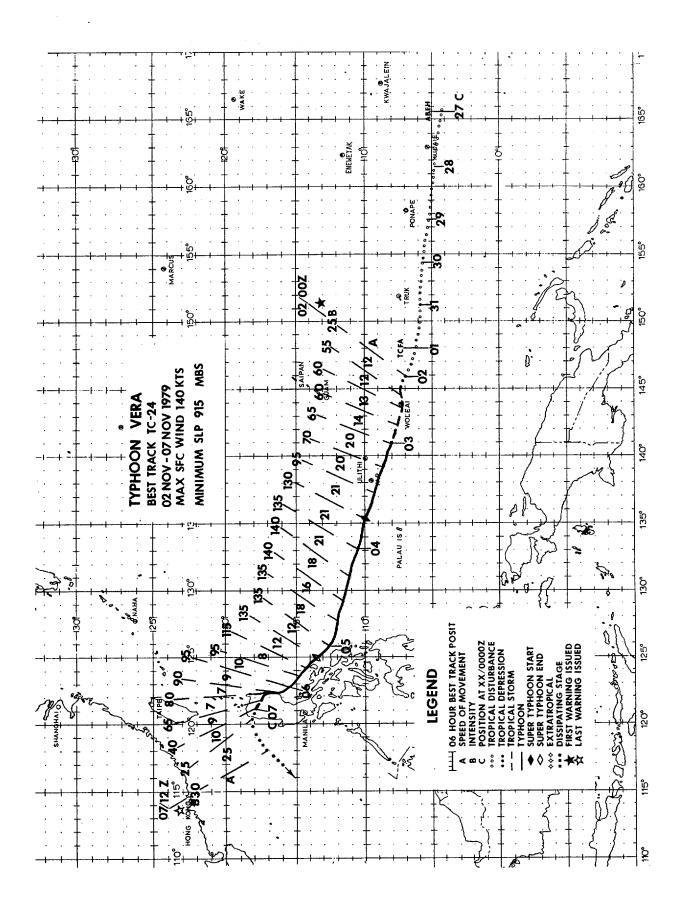
At approximately 190100Z, after reaching a forward speed of between 35 and 45 kt (65 and 83 km/hr), Typhoon Tip, with maximum winds of 70 kt (36 m/sec), made landfall on the Japanese island of Honshu, about 60 nm (111 km) south of Osaka. Synoptic and radar data from stations on the island showed that Tip maintained a speed in excess of 45 kt (83 km/hr) as he passed to the north of Tokyo and eastward into the Pacific Ocean. According to satellite imagery, Tip completed extratropical transition over Honshu.

The extratropical low pressure center (the remnants of Tip) maintained winds of storm force, 48 kt (25 m/sec), until the 21st when it moved to a position east of Kamchatka and finally began to fill rapidly.

The majority of the severe damage occurred in Japan where the agricultural and fishing industries sustained losses into the millions of dollars. Flooding from Tip's rains also breached a fuel retaining wall at Camp Fuji, west-northwest of Yokosuka. The fuel caught fire causing 68 casualties, including 11 deaths, among the U.S. Marines stationed there.

Considering the size and strength of Super Typhoon Tip, the Western Pacific faired well. Luckily, the maximum intensity was reached while the system was still far from any inhabited areas. The potential for mass destruction was always there, but from a strictly meteorological standpoint, Tip was also a thing of great beauty. One of the Aerial Reconnaissance Weather Officers stated, shortly after she returned from a mission, that "...the second penetration was beyond description. This is unquestionably the most awe-inspiring storm I have ever observed. In the 2½ hours that transpired between the first and second fixes, the moon had risen sufficiently to shine into the eye through an 8 nm clear area at the top of the eyewall. To say it was spectacular is totally inadequate...'awesome' is a little closer."

<sup>1</sup>CAROL L. BELT, 1LT, USAF: Mission ARWO.



Vera, the fourth and final super typhoon of 1979, originated in an active near-equatorial trough (NET) which extended through the Caroline and Marshall Islands. Vera was first analyzed as a weak surface circulation 100 nm (185 km) southeast of Ponape on 27 October and was included on JTWC's Significant Tropical Weather Advisory (ABEH PGTW) for the next 4 days as it remained in the NET. Low-level inflow during this period was split between several weak eddies

By 300000Z, synoptic data indicated that the low-level inflow was now concentrated into the developing cyclone. Meanwhile, the convective activity increased rapidly over a 24-hour period from 310000Z to 010000Z. A Tropical Cyclone Formation Alert was issued at 010000Z November based on increased upper-level outflow and a continued decrease in surface pressure.

Aircraft reconnaissance at 0121002 found an ill-defined circulation center with a central pressure of 1004 mb and estimated surface winds of 15 kt (8 m/sec). Numbered warnings began at 0200002 based on an improved satellite signature. Rapid intensification occurred, and TD 24 was upgraded to Tropical Storm Vera 6 hours later. Vera continued to intensify, reaching typhoon strength by 00002 on 3 November while 190 nm (352 km) south-southeast of Yap. At this time, the 200 mb analysis revealed that a large upper-level anticyclone, previously located northwest of Vera at 0100002, was weakening and was no longer restricting Vera's outflow to the north. By 0200002, the anticyclone situated over Vera had become the dominant upper-level synoptic feature over the western Pacific.

From the time of the first warning until her approach to the Philippines northeast of Samar, Vera moved on a virtually straight west-northwest track. The major influence on her movement was the unusually strong mid-tropospheric subtropical ridge over the western Pacific. The strength of the easterly current south of the ridge steered Vera at forward speeds of 20 to 22 kt (37 to 41 km/hr)--almost twice the climatological average--as she passed 35 nm (65 km) south of Yap. As a result, although JTWC's forecast tracks were consistent and accurate, forecast forward speeds lagged behind Vera's actual speeds. The underestimates were considerable during the early stages of acceleration.

Vera continued to intensify during her west-northwestward acceleration and reached super typhoon intensity only 18 hours after being upgraded to a typhoon. Reconnaissance aircraft reports indicated Vera maintained super typhoon strength for over 24 hours before weakening as she approached Catanduanes Island. The peak wind reported on Catanduanes Island was 50 kt (26 m/sec) at 051200Z as Vera passed just off the coast.

The island chain began restricting low-level inflow as Vera continued northwestward toward northern Luzon. Vera made landfall north of Tarigtig Point packing winds of 90 kt (46 m/sec).

After landfall, the onset of enhanced low-level northeasterly flow over the Taiwan Straits coupled with strong upper-level southwesterlies over the Philippines resulted in vertical disorganization and rapid weakening of Vera. Radar and aircraft reports indicated the low-level circulation continued to track northwestward over the Cagayan River valley and exit into the South China Sea near Culili Point south of Laoag. The upper-level circulation sheared off near Tuguegarao and was tracked using satellite imagery northward over Aparri then east-northeastward into the Philippine Sea. Surface synoptic and ship reports at 070000Z indicated that a secondary surface center existed near Baguio. At the same time, the primary center was crossing the Cordillera Central Mountain range 95 nm (176 km) to the north (Fig. 3-24-1).

After exiting into the South China Sea, the strong northeast monsoon flow accelerated Vera southwestward, and the final warning was issued at 12002 on the 7th downgrading Vera to a tropical depression.

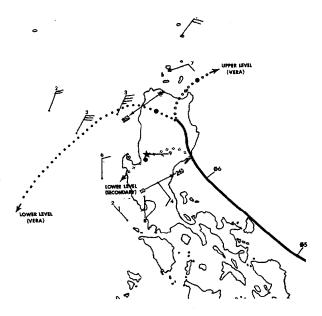
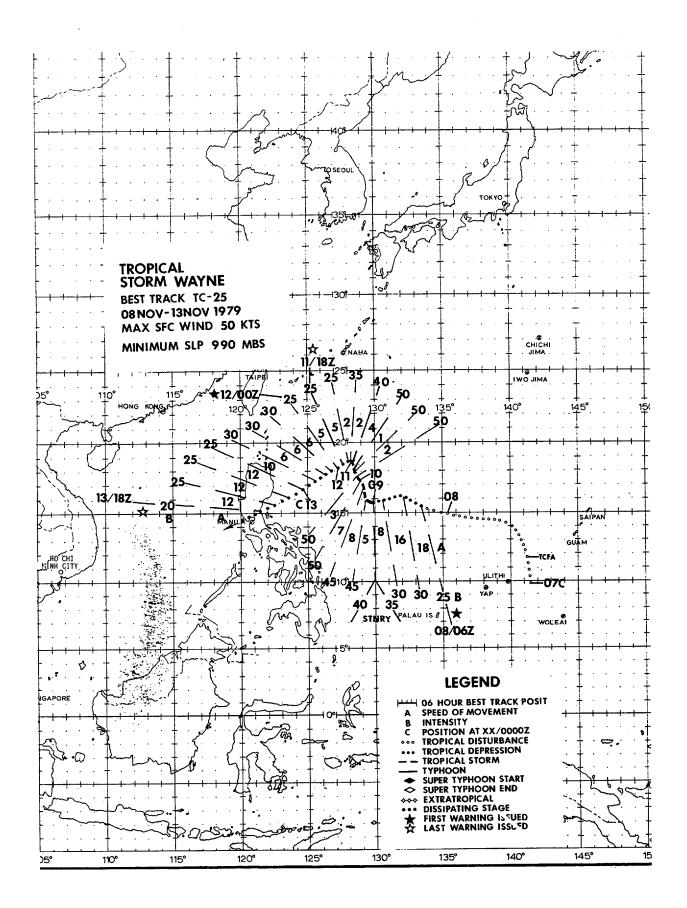


FIGURE 3-24-1. Tracks of low-level and upper-level centers after the upper-level sheared off over northern luzon. Synoptic and ship reports at 0700002 November indicate secondary low-level center near Baguio (WMO 98328) (indicated by a star). The 0700002 center positions are indicated by solid dots. Wind speeds are in knots.



#### TROPICAL STORM WAYNE

Tropical Strom Wayne was first detected as a mid-level circulation on satellite imagery in early November. Figure 3-25-1 shows the broad cloud structure associated with the system. Aircraft reconnaissance around this period showed that the disturbance was most developed at mid-levels. Wayne moved northward initially and began developing a more definitive surface circulation which became evident in synoptic data on 7 November. Wayne lasted only a relatively short time, but he still proved to be one of the more difficult storms to forecast for 1979.

JTWC's first forecasts called for recurvature. They were based on the 0800002 November 500 mb synoptic situation which showed a weakness in the subtropical ridge with westerlies extending south to 23°N latitude. Steering flow at all levels, however, was not consistent and strong lowlevel easterlies prevented Wayne from recurving toward the east. On 9 November, an extratropical system with accompanying surface frontogenesis developed north of Wayne. This caused a break in the otherwise persistent easterly flow and Wayne began to track northward. JTWC forecasts again reflected recurvature and called for early dissipation due to the strong shear from low-level easterlies and upper-level westerlies. The extratropical system moved rapidly eastward bypassing Wayne. By 11 November, strong northeasterlies had once again been established, and Wayne turned back to the west, ultimately, tracking west-southwest toward the central

Thilippines. At the same time, strong shear did weaken Wayne as it tracked toward the Philippines (Figure 3-25-2) and dissipation occurred as he made landfall over Luzon.

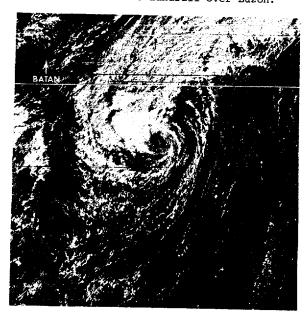


FIGURE 3-25-2. Tropical Storm Wayne weakening due to strong shear as it approached the Philippines, 12 November 1979, C100Z. (DMSP imagery)

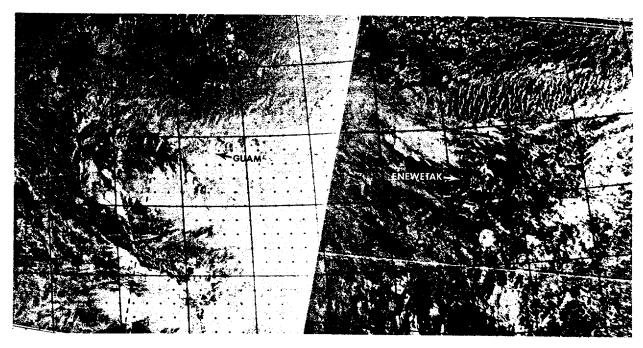
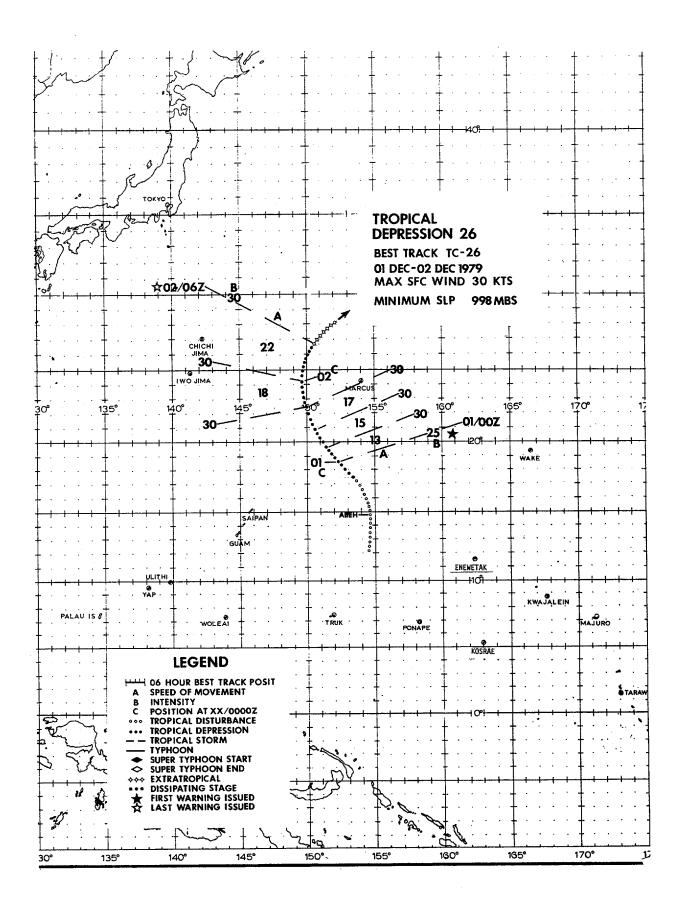


FIGURE 3-25-1. Disturbance stage of Tropical Storm Wayne when the system was mainly a mid-level circulation, 6 November 1979, 12082. (DMSP imagery)



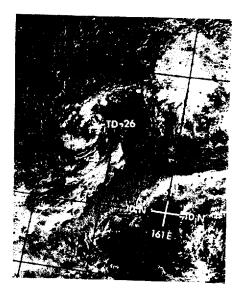


FIGURE 3-26-1. Tropical Depression 26 developed north-northeast of the Truk Islands and appeared to be the surface reflection of a mid-level circulation. Surface data suggest the existence of a weak circulation 400 nm (741 km) northeast of Tropical Depression 26 and a broad circulation (Typhoon Abby) to the southeast, 29 November 1979, 22552. (DMSP imagery)

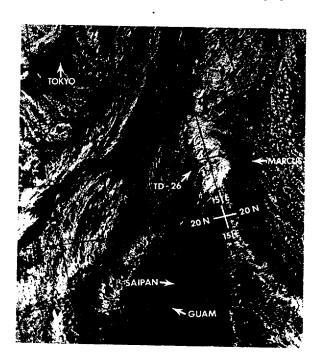


FIGURE 3-26-3. Tropical Depression 26 passed west of Marcus Island and merged with an extratropical frontal boundary. Tropical Depression 26 sheared in the vertical with the low-level exposed surface circulation remaining on the western edge of the convection, 2 December 1979, 00362. [DMSP imagery]

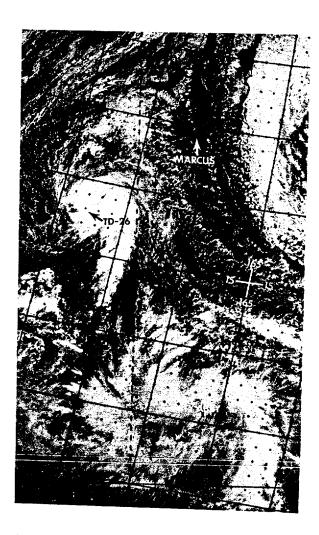
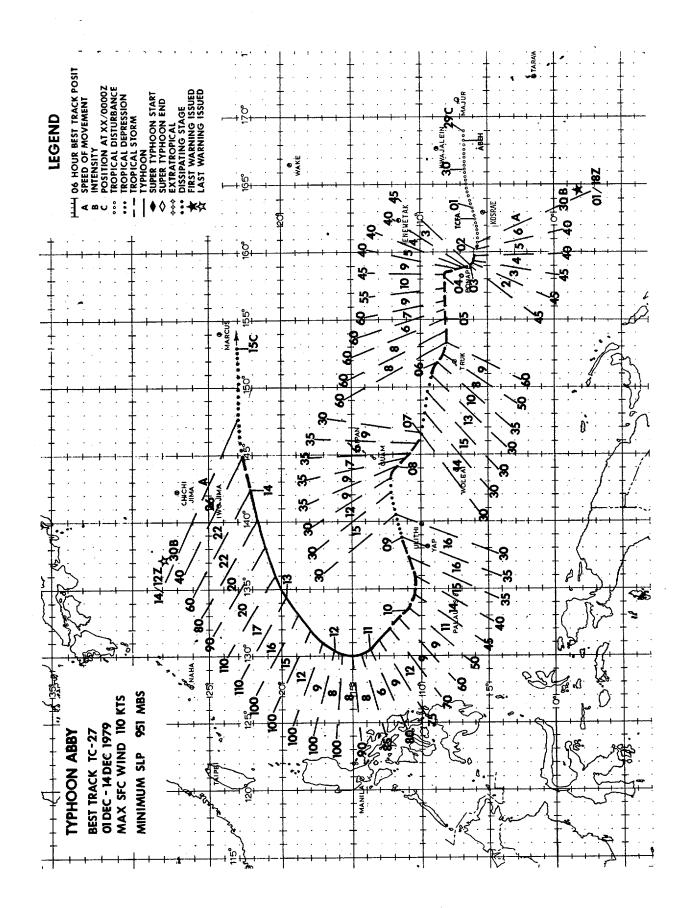


FIGURE 3-26-2. Tropical Depression 26 developed an identifiable surface circulation and intensified as it tracked north-northwestward. A ship, transiting the area, passed through the storm center and reported 35 kt [18 m/sec] winds in heavy showers. Based on synoptic data, the first warning was issued on Tropical Depression 26, but 35 kt-or-greater winds were never reported again. This photo shows Tropical Depression 26 at its maximum convective intensity, 30 November 1979, 22372. (DMSP imagery)



Abby, the last typhoon of the 1979 season, developed over the Marshall Islands during early December. Abby proved to be an unusual cyclone in several ways. Throughout much of Typhoon Abby's existence, Abby was not vertically aligned. Aircraft reconnaissance located the mid-level circulation center displaced as much as 55 nm (102 km) from the surface center. At one point, two centers were identified; a point to be discussed later. In addition, Abby fluctuated between tropical depression and tropical storm strength several times before reaching typhoon strength 10 days after

Within 24 hours of the first warning, aircraft reconnaissance observed surface winds of 45 kt (23 m/sec) and a sea-level pressure of 996 mb. The surface and 700-mb centers were displaced by 12 nm (22 km). Abby continued to intensify to 60 kt (31 m/sec) on 4 October while increasing the displacement between the surface and 700-mb centers.

Abby deviated from a westward track to a north-northwestward track on 3 December with a reduced forward speed of movement. The temporary northward movement was associated with a deepening mid-tropospheric trough which moved rapidly northeastward away from Japan on 1 December. Abby resumed a westward track with increased forward speed after the trough axis passed east of Abby late on the 3rd.

All available information (climatology, analog aids, analyses and numerical fore-casts) indicated continued intensification as Abby tracked towards Guam. This expected intensification was reflected in JTWC warnopposite occurred. As Abby moved west of Truk, she weakened to less than tropical storm strength. An upper tropospheric anticyclone north of Abby restricted Abby's outflow and resulted in the observed weakening (Fig. 3-27-1). By 7 December, Abby reintensified to minimum tropical storm strength as she moved westward and away from the influence of the restricting anticyclone. Abby then tracked west-northwestward under the influence of a mid-tropospheric long-wave trough oriented along 142E. As the trough moved east of Abby, the subtropical mid-tropospheric ridge again built eastward, providing a mechanism which steered Abby towards the west-southwest. During the 8th, Abby once again weakened to less than tropical storm strength and increased her forward speed of movement.

Abby was not vertically aligned from the issuance of the first warning through the 9th. On the 9th, aircraft reconnaissance making a supplemental fix at 06172 observed that Abby possessed multiple 700 mb centers. By the time of entry into Abby for a levied 0830Z fix, only one well organized, intensifying center was found. The following is a storm mission summary by the Aerial Reconnaissance Weather Officer (ARWO), who made the double penetration into Abby: "This mission started out as a normal fix but ended

FIGURE 3-27-1 is on following page.

up being unusual. On our way inbound for the supplemental fix, there was no problem reading winds at flight level or on the surface. Winds were 20-25 kt the entire way. An area of thunderstorm activity became visible ahead of us. As we neared it, the doppler indicated that the 700 mb center was in the middle of the thunderstorm. Not eager to go find this out, we went back not eager to go that this out, we went back to find the surface center. Enroute, we saw surface winds in excess of 35 kt which led us to a fairly disorganized surface center just east of the main thunderstorm. Over it was a fairly small light and variable wind center. Radar showed little curvature in the shower pattern, but the surface winds did indicate a weak circulation existed at this first position. No weather existed to the east of our first fix, and this position was right on the JTWC forecast track. On the second fix, things had changed. As we came in the second time, we encountered considerable precipitation. Doppler and search radar indicated a center with a possible wall cloud forming considerably west of our first fix. Winds were stronger at flight level and we penetrated a wall cloud of about 80% coverage. When we broke through, we encountered our strongest winds at flight level. The surface center was under the eastern wall cloud with a small light and variable wind center at 700 mb centered in the eye. Lightning started in the eastern wall cloud and spread around the

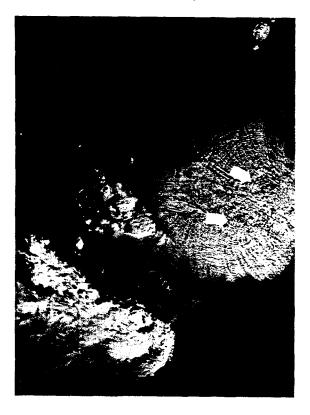
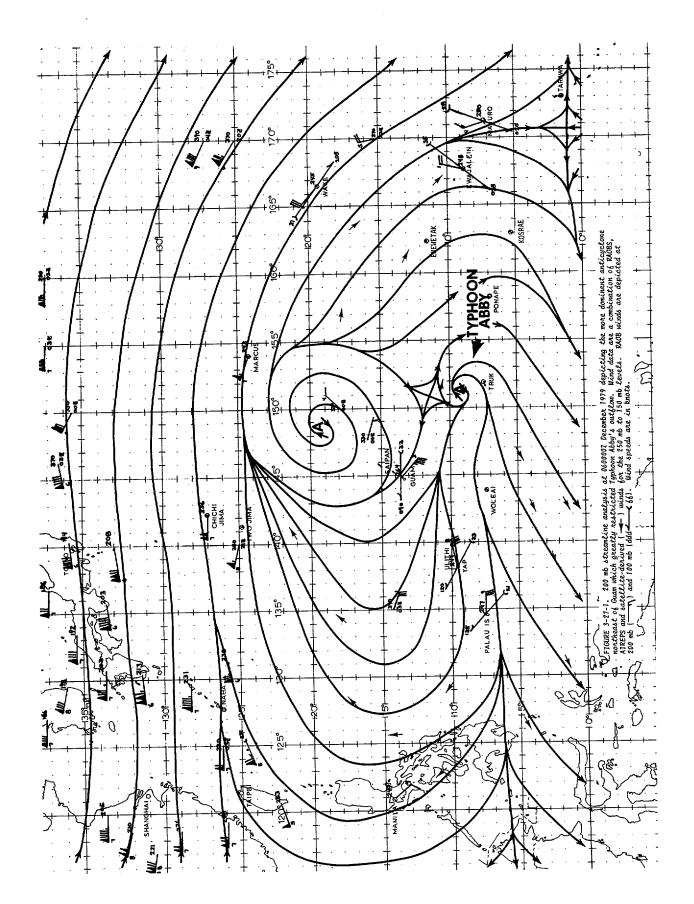


FIGURE 3-27-2. Typhoon Abby's two outflow centers are indicated by arrows, 9 December 1979, 01442. (DMSP imagery) Figure 3-27-1 is on next page.



eye. Our drop was made as close to the surface center as was possible and indicated a good 988 mb sea-level pressure. The 700 mb height was down 72 meters from the first fix. The positions were 85 miles apart causing me to believe that two centers existed for a short time with the latter becoming the predominate one. The pressure profile seems to indicate this theory...."1 Satellite imagery at 0901442 also indicated the possible existence of multiple outflow centers (Fig. 3-27-2). While Abby was reorganizing into a single center, she began to reintensify to tropical storm strength. By the 10th, Abby had attained typhoon strength which made her the last typhoon of the decade.

A mid-tropospheric short-wave trough moved from mainland China into the Sea of Japan and deepened on the 10th. In response to the short-wave trough, the subtropical mid-tropospheric ridge again receded eastward north of Abby. The interaction of these two synoptic features allowed Abby to again track northwest. On the 11th, Typhoon Abby recurved in response to another mid-tropospheric short-wave trough, which extended further south than the trough on the 10th. This last trough in the series moved into the northern part of the South China Sea and deepened, causing Abby to finally follow a recurvature track.

Typically, recurving typhoons have their maximum intensities either less than 12 hours after recurvature or prior to recurvature (Riehl, 1971). Abby, however, did not reach maximum intensity until 36 hours after recurvature. By 13 December, Typhoon Abby reached maximum intensity of 110 kt (57 m/sec) with a minimum sea-level pressure of 951 mb (Fig. 3-27-3). As Abby continued toward the east-northeast, she approached a regime of very strong westerlies in the middle-and upper-troposphere. The strong westerlies induced Abby's acceleration

and rapid weakening. Abby dissipated on the 14th due to strong vertical shear between the surface and middle levels.

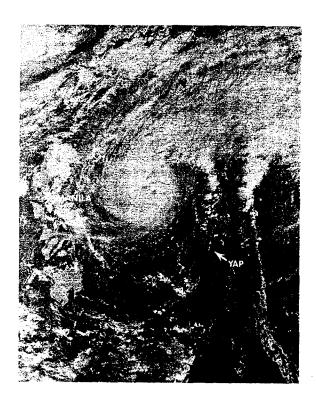
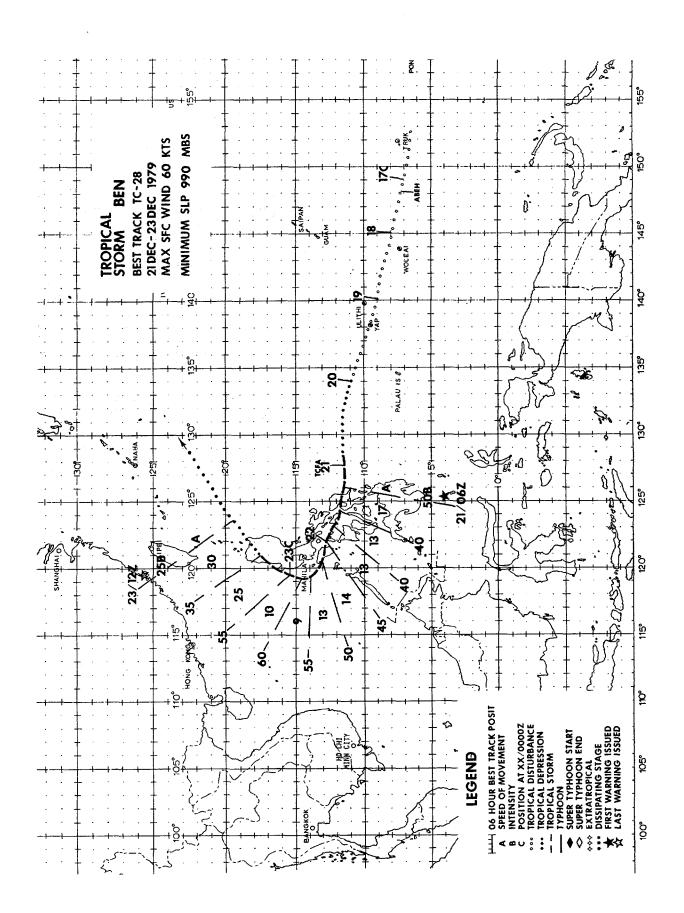


FIGURE 3-27-3. Typhoon Abby just after recurvature, 12 December 1979, 00212. [DMSP imagery]

<sup>&</sup>lt;sup>1</sup>CHARLES B. STANFIELD, Capt, USAF: Mission ARWO.



# TROPICAL STORM BEN (28)

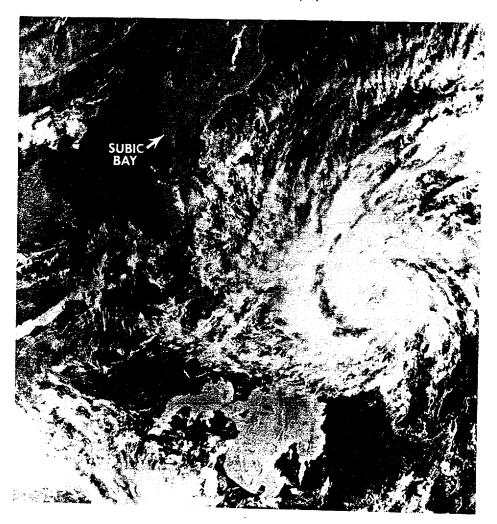


FIGURE 3-28-1. Tropical Storm Ben at 40 kt [21 m/sec] intensity, 21 October 1979, 00597. Ben was the last tropical cyclone in the western North Pacific during 1979. [DMSP imagery]

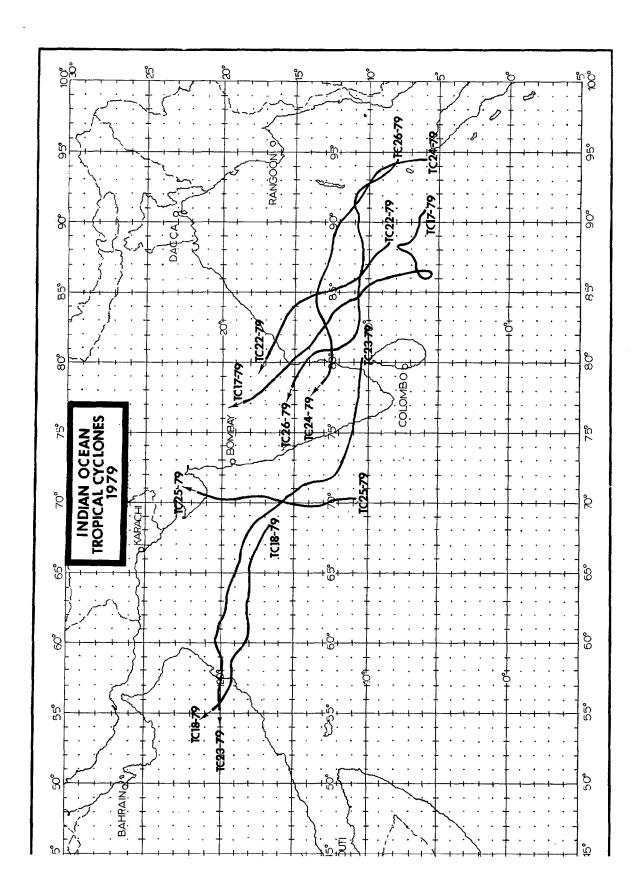
## 2. NORTH INDIAN OCEAN TROPICAL CYCLONES

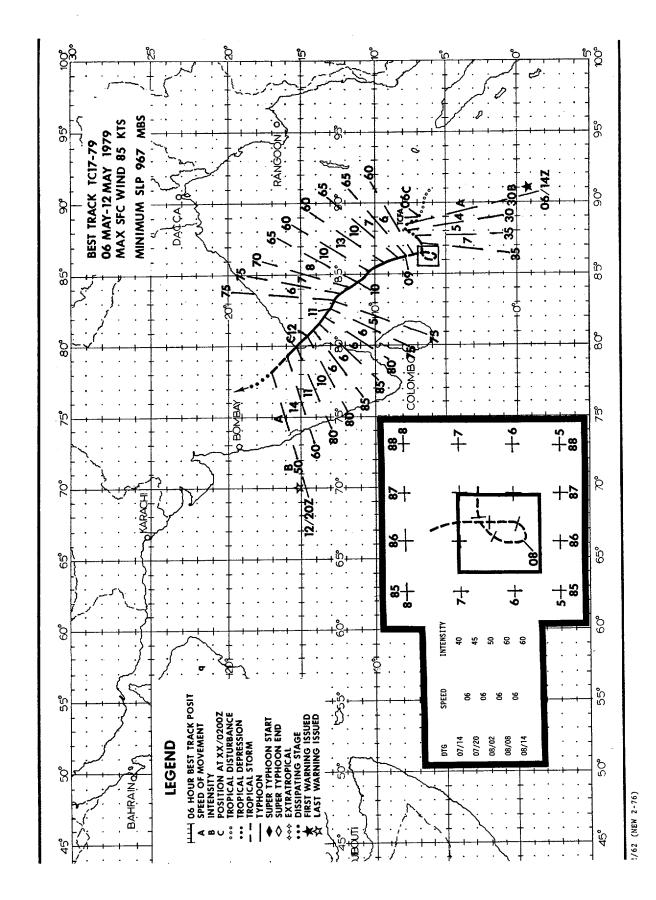
During 1979, 7 significant tropical cyclones occurred in the North Indian Ocean area (Table 3-3). As usual, the transition

seasons between the northeast and southwest monsoon periods were the favored "cyclone seasons" (Table 3-4). This was an above normal season with most activity occurring during the fall transition period.

TABLE 3-3		NORTH INDI	AN OCEAN								
1979 SIGNIFICANT TROPICAL CYCLONES											
CYCLONE	PERIOD OF WARNING	CALENDAR DAYS OF WARNING	MAX SFC WIND	EST MIN SLP	NUMBER OF WARNINGS	DISTANCE TRAVELLED					
TC 17-79 TC 18-79 TC 22-79 TC 23-79 TC 24-79 TC 25-79 TC 26-79	06 MAY-12 MAY 18 JUN-20 JUN 21 SEP-23 SEP 21 SEP-25 SEP 29 OCT-01 NOV 16 NOV-17 NOV 23 NOV-25 NOV	7 3 5 4 2 3	85 50 25 55 35 40 30	967 985 1000 980 995 994 995	26 12 10 14 13 8	1267 581 694 1108 720 547					
	1979 TOTALS	24*			93						

TABLE 3-4.													
NORTH			1979 5	IGNIFIC	ANT TRO	PICAL C	CLONE	STATIST	ICS				
INDIAN OCEAN	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
ALL CYCLONES	0	0	0	0	1	1	0	0	2	1	2	0	7
(1971-78) AVERAGE*	0.1	0	0	0.3	0.5	0.3	0	0	0.4	0.8	1.4	0.3	4
FORMATION ALERTS	7 of	the 8	(87%) F	ormatio	n Alert	Events	develo	ped int	o numbe	red cyc	lones.		
WARNINGS	Numb	er of w	varning	days:	25								
	Numb	er of v	warning	days wi	th 2 cy	clones:	3						
	Numb	er of v	varning	days wi	th 3 or	more c	yclones	s: 0					
			······································			*		· · · · · · · · · · · · · · · · · · ·			<del></del>		
*From 1971 through extended in 1975 1	1974, to incl	only Ba ude Ara	ay of Be abian Se	engal cy ea cyclo	clones nes.	were co	nsidere	ed; the	JTWC ar	ea of r	esponsi	bility w	as





TC 17-79 was the only significant tropical cyclone in the Bay of Bengal during the 1979 spring transition season. Attaining typhoon intensity, TC 17-79 was the most destructive cyclone in India since TC 22-77 (Nov 1977) which, coincidentally, followed a similar track.

A Tropical Cyclone Formation Alert and the first warning were precipitated by synoptic reports received from ships participating in the First GARP Global Experiment (FGGE). At 1200Z on 6 May, these ships' observations defined a cyclonic circulation near 07N-088E with reported surface pressures near 1003 mb and wind speeds of 20-25 kt (10-12 m/sec). The first warning on TC 17-79 was issued at 061507Z.

From 060000Z through 061200Z, a strong mid-tropospheric ridge extended westward along 15N with southeast steering flow dominating TC 17-79's movement. During the same time period, a short-wave trough, evident at both middle and upper levels, was deepening over India. Interaction between this ridging and troughing resulted in a loss of definitive steering flow in the vicinity of TC 17-79, producing an erratic north and then south track. Also during this time, TC 16-79 located in the southern Indian Ocean about 750-800 nm (1389-1481 km) to the southwest,



FIGURE 3-29. TC 17-79 with well-defined satellite signature during the erratic cyclonic loop, 8 May 1979, 05282. (DMSP imagery from AFGWC, Offutt AFB, Nebraska)

began tracking slowly to the southeast possibly initiating a Fujiwhara type interaction.

By 080000Z, a mid-level anticyclone had formed in the northern Bay of Bengal with east-northeasterly steering flow over TC 17-79 resulting in a west-southwest forecast track. From 080000Z through 090000Z, while TC 17-79 intensified (Fig. 3-29), the dominant steering flow shifted to the south then southeast as the mid-level ridge was replaced by a trough and the upper-level trough dug southward over India. As a result of this shift in steering flow, TC 17-79 executed a tight cyclonic loop from 080000Z to 081800Z. From 7 through 9 May, though satellite fix position accuracies improved due to the formation of a well-defined eye, forecast errors increased appreciably due to the erratic movement.

By 0912002, southeast steering flow became dominant with TC 17-79 oscillating about a northwest track until making landfall over India (Fig. 3-30). TC 17-79 struck the east central coast of India at 1208002, 45 nm (83 km) north of Nellore with maximum sustained winds of 80 kt (41 m/sec). Twenty-one deaths occurred and over 800,000 persons were left homeless as a result of TC 17-79's passage over the Nellore district.

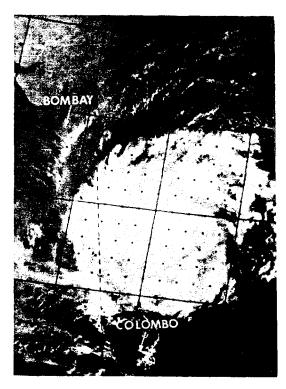
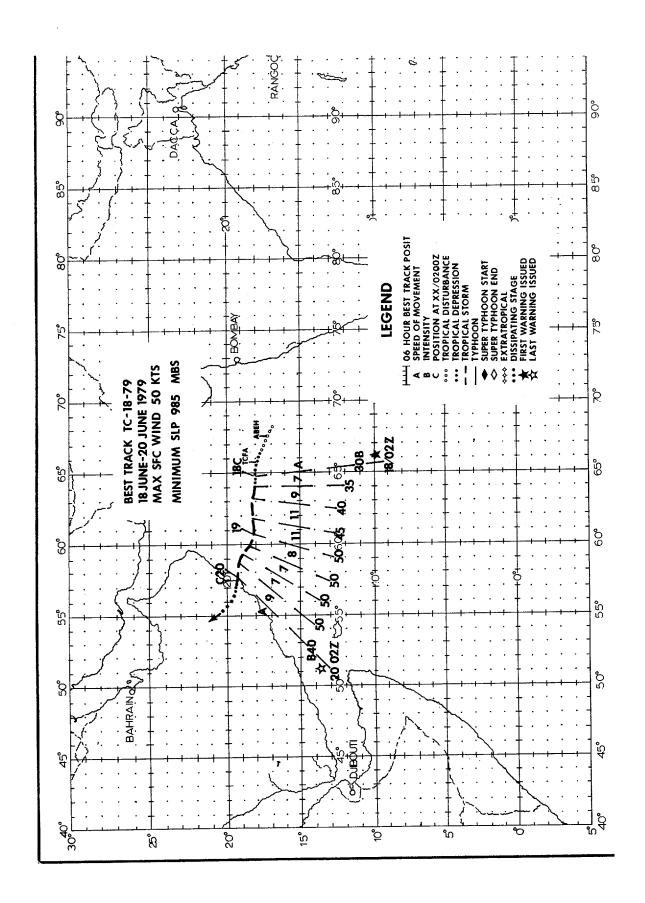


FIGURE 3-30. TC 17-79 just prior to making landfall over east central India with 80 kt [41 m/sec] intensity, 12 May 1979, 05567. (DMSP imagery from AFGWC, Offutt AFB, Nebraska)



TC 18-79 began 1714002 June 1979 as a monsoon depression in the Arabian Sea and tracked virtually westward throughout its life, finally dissipating over the Oman coast (Fig. 3-31). Although TC 18-79's movement was confined to a narrow 2-degree latitudinal band, the extent of the meteorological hazard from gale force winds encompassed roughly half of the Arabian Sea. These gale force winds were produced by the interaction of TC 18-79 with the normal southwest monsoonal flow over the Arabian Sea.

During this season, a climatological low-level wind maximum develops off the coast of Somali. Normal wind speeds can reach 35-40 kt (18-21 m/sec), but the gale area is generally localized near the coast. However, beginning 2 days prior to TC 18-79's forma-

tion, a surge in the monsoonal flow occurred and a low-level jet could be traced from the Somali coast extending eastward across the entire Arabian Sea. The strength and persistence of this feature aided the formation of TC 18-79 in the cyclonic shear side of the wind maximum. As TC 18-79 intensified and moved westward, the southwesterly flow strengthened to a point where 65 kt (33 m/sec) surface winds were observed 600 nm (1111 km) away from TC 18-79's center. Examination of the visual data of Figure 3-31 shows cloud streets indicative of this strong low-level flow from 05N to 12N between 55E to 62E. The gale area persisted during TC 18-79's dissipation over land, weakening gradually with time. Interestingly, post-analysis reveals the maximum winds in the gale area exceeded the maximum sustained winds estimated in TC 18-79's center.

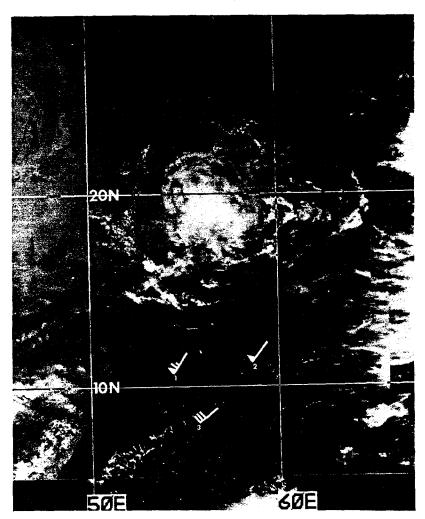
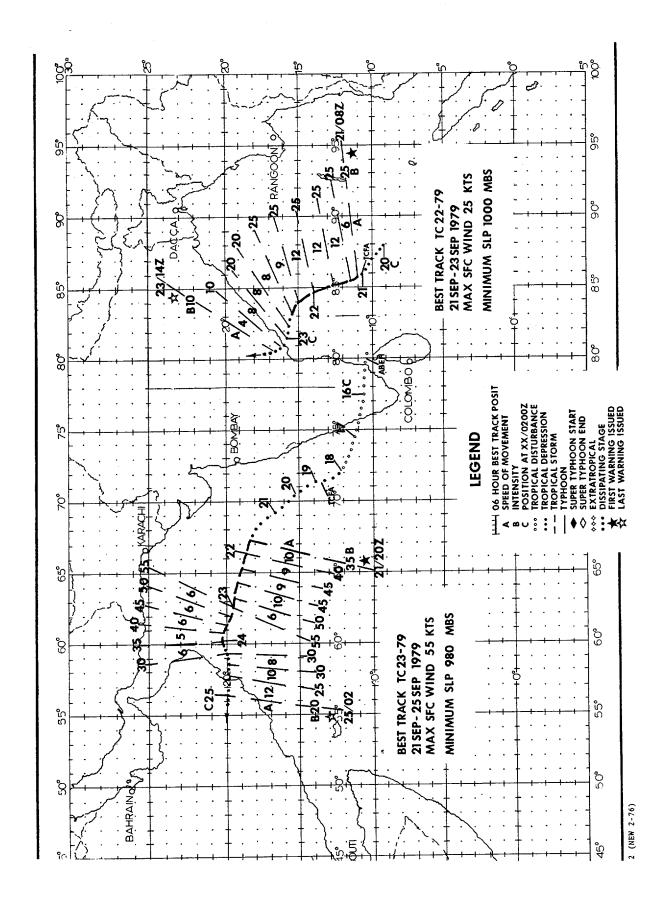
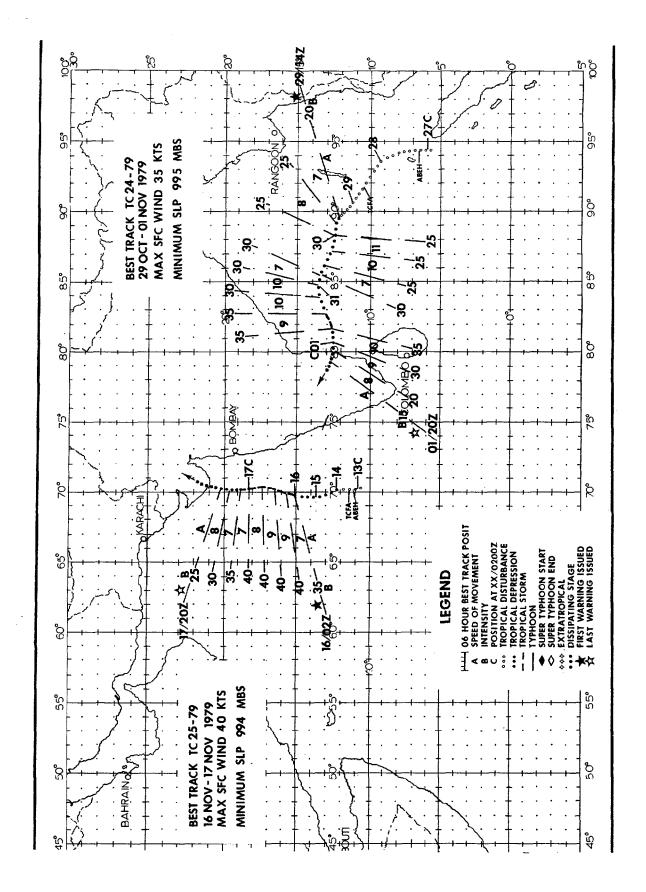
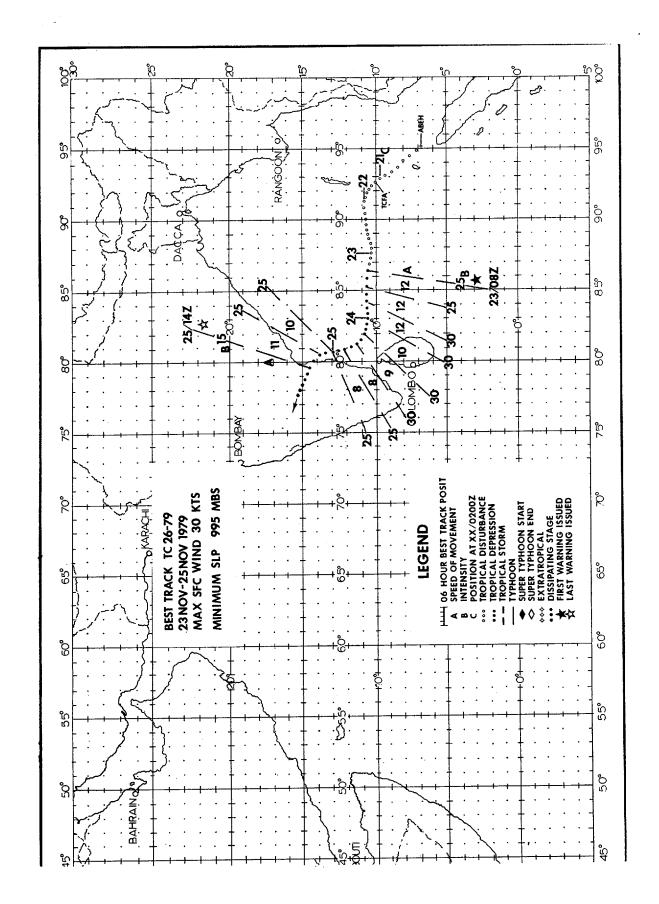


FIGURE 3-31. TC 18-79 located just off the Oman coast with gale force winds to the south, 20 June 1979, 07312. Superimposed are ship observations at 2006002. (DMSP imagery from AFGUC, Offutt AFB, Nebrask4)







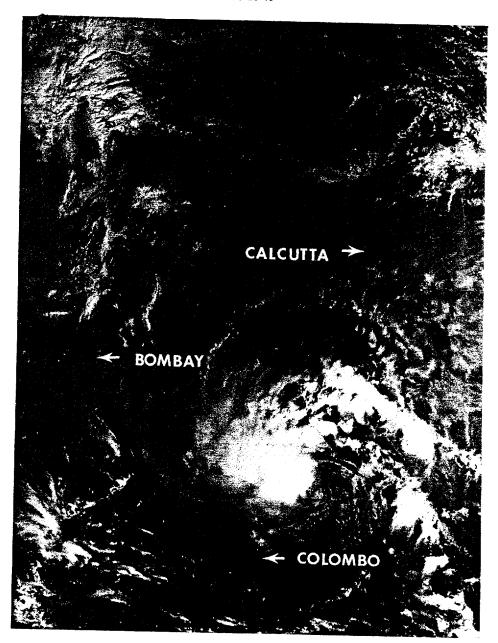


FIGURE 3-32. TC 26-79 as an exposed low-level circulation, 24 November 1979, 0455Z. [DMSP imagery from AFGWC, Offutt AFB, Nebraska]

## CHAPTER IX SUMMARY OF FORECAST VERIFICATION

### 1. ANNUAL FORECAST VERIFICATION

a. Western North Pacific Area

Forecast positions at warning times and 24-, 48-, and 72-hour valid times were verified against corresponding best tracks. Vector errors and right angle errors for individual tropical cyclones were calculated

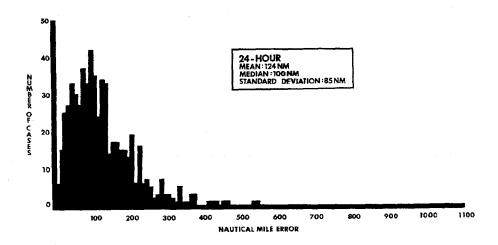
and are displayed in Table 4-1. Annual mean errors for all tropical cyclones are listed in Table 4-2 for comparison. Frequency distributions of the vector errors for 24-, 48-, and 72-hour forecasts on all 1979 tropical cyclones are shown in Figure 4-1. Annual mean vector errors are graphed in Figure 4-2.

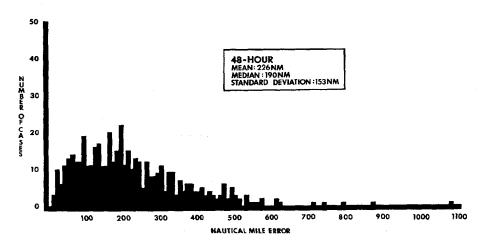
TABLE 4-1. FORECAST ERROR SUMMARY FOR THE 1979 WESTERN NORTH PACIFIC SIGNIFICANT TROPICAL CYCLONES.

CYCLONE   POSIT   RT ANGLE   POSIT   RT ANGLE   REROR   POSIT   RT ANGLE   REROR							24 HOUR			48 HOUR			72 HR	
CYCLONE   ERROR   ERROR   WRNGS   ERROR   ERROR   ERROR   ERROR   ERROR   ERROR   WRNGS   ERROR   ERROR   WRNGS   ERROR   ERROR   ERROR   WRNGS   ERROR   ER			****	WARNING		20022		- 1	55555			655 Tm		<del></del>
1. TY ALICE 18 11 51 105 83 47 222 175 43 338 271 39 2. TY BESS 19 15 21 114 73 17 265 164 13 348 240 9 3. TY CECIL 15 11 40 87 62 37 191 131 33 320 215 29 4. TS DOT 23 16 24 130 79 23 244 171 20 315 257 16 5. TD-05 12 12 22 6 158 150 3 6. TY ELLIS 25 21 22 71 57 18 145 103 14 185 113 10 7. TS FAYE 35 21 22 71 57 18 145 103 14 185 113 10 7. TS FAYE 35 21 20 138 86 17 167 93 14 180 99 10 8. TD-08 43 20 5 195 70 4 396 396 1 9. TS GORDON 23 12 13 129 90 9 173 121 5 449 278 1 10. TS HOPE 23 16 33 134 75 29 266 140 23 376 188 21 11. TD-11 47 30 14 144 94 10 138 89 6 171 129 2 12. TY IRVING 26 17 38 163 98 34 286 209 30 441 344 26 13. ST JUDY 18 12 39 105 81 36 173 138 27 277 213 23 14. TD-14 33 19 9 157 43 5 296 118 1 15. TS KEN 29 13 13 116 60 10 278 111 7 415 195 3 14. TD-14 33 19 9 157 43 5 296 118 1 15. TS KEN 29 13 13 116 60 10 278 111 7 415 195 3 16. TY LOLLA 16 10 23 88 64 21 172 148 19 207 236 14 17. TY MAC 23 16 35 93 66 27 196 152 19 279 227 19 18. TS NANCY 28 19 14 116 86 9 216 186 4 227 219 1 19. TY COWEN 25 15 37 146 78 33 250 158 29 327 256 25 20. TS PAMELA 28 22 6 254 15 2 21. TS ROGER 32 19 16 43 61 40 39 110 86 34 143 107 27 23. ST TIP 24 15 60 135 69 56 259 142 52 345 214 48 24. TY SARAH 26 16 43 61 40 39 110 86 34 143 107 27 23. ST TIP 24 15 60 135 69 56 259 142 52 345 214 48 24. TY SARAH 26 16 43 61 40 39 110 86 34 143 107 27 23. ST TIP 24 15 60 135 69 56 259 142 52 345 214 48 24. TY SARAH 26 16 43 61 40 39 110 86 34 143 107 27 23. ST TIP 24 15 60 135 69 56 259 142 52 345 214 48 24. TY SARAH 26 16 43 61 40 39 110 86 34 143 107 27 23. ST TIP 24 15 60 135 69 56 259 142 52 345 214 48 24. TY SARAH 26 16 6 55 28 3 28. TS BEN 34 18 10 81 89 6 287 16 28	<b>4</b> 00	rar ourn			MIDNOCO			MINICO						MDVC6
2. TY BESS 19 15 21 114 73 17 265 164 13 348 240 9 3. TY CECIL 15 11 40 87 62 37 191 131 33 320 215 29 4. TS DOT 23 16 24 130 79 23 244 171 20 315 257 16 5. TD-05 12 12 12 6 158 150 3 6. TY ELLIS 25 21 22 71 57 18 145 103 14 185 113 10 7. TS FAYE 35 21 20 138 86 17 167 93 14 180 99 10 8. TD-08 43 20 5 195 70 4 396 396 1 9. TS GORDON 23 12 13 129 90 9 173 121 5 449 278 1 10. TS HOPE 23 16 33 134 75 29 266 140 23 376 188 21 11. TD-11 47 30 14 14 49 10 138 89 6 171 129 2 12. TY IRVING 26 17 38 163 98 34 286 209 30 441 344 26 13. ST JUDY 18 12 39 105 81 36 173 138 27 277 213 23 14. TD-14 33 19 9 157 43 5 296 118 1 15. TS KEN 29 13 13 13 116 60 10 278 111 7 415 195 3 16. TY LOLA 16 10 23 88 64 21 172 148 19 287 236 14 17. TY MAC 23 16 35 93 66 27 196 152 19 279 227 19 18. TS NANCY 28 19 14 16 86 9 216 186 4 227 219 18. TS NANCY 28 19 14 16 78 33 250 158 29 327 256 25 20. TS PAMELA 28 22 6 254 15 2 21. TS ROGER 32 19 16 195 93 13 251 108 9 303 178 4 22. TY SARAH 26 16 43 61 40 39 110 86 34 143 107 27 23. ST TIP 24 15 60 135 69 56 259 142 52 345 214 48 24. ST VERA 43 20 23 148 69 19 249 111 15 385 247 11 25. TS WAYNE 27 14 22 170 115 16 362 295 12 443 413 47 26. TY ABBY 31 17 52 164 109 48 286 198 39 338 215 26 27. TD-26 21 16 6 55 28 3 28. TS BEN 34 18 10 81 89 6 287 16 2		CLONE	ERROR	LKKOK	MANGO	ERROR	ERROR	7714100	DAG N	Dittoit	marab	<u> </u>	- DIGITOR	MARIOD
2. TY BESS 19 15 21 114 73 17 265 164 13 348 240 9 3. TY CECIL 15 11 40 87 62 37 191 131 33 320 215 29 4. TS DOT 23 16 24 130 79 23 244 171 20 315 257 16 5. TD-05 12 12 6 158 150 3 6. TY ELLIS 25 21 22 71 57 18 145 103 14 185 113 10 7. TS FAYE 35 21 20 138 86 17 167 93 14 180 99 10 8. TD-08 43 20 5 195 70 4 396 396 1 9. TS GORDON 23 12 13 129 90 9 173 121 5 449 278 1 10. TS HOPE 23 16 33 134 75 29 266 140 23 376 188 21 11. TD-11 47 30 14 144 94 10 138 89 6 171 129 2 12. TY IRVING 26 17 38 163 98 34 286 209 30 441 344 26 13. ST JUDY 18 12 39 105 81 36 173 138 27 277 213 23 14. TD-14 33 19 9 157 43 5 296 118 1 15. TS KEN 29 13 13 116 60 10 278 111 7 415 195 3 16. TY LOLLA 16 10 23 88 64 21 172 148 19 287 236 14 17. TY MAC 23 16 35 93 66 27 196 152 19 279 227 19 18. TS NANCY 28 19 14 116 86 9 216 152 19 279 227 19 18. TS NANCY 28 19 14 116 86 9 216 152 19 279 227 19 18. TS NANCY 28 19 14 116 86 9 216 152 19 279 227 19 18. TS NANCY 28 19 14 116 86 9 216 188 29 327 256 25 20. TS PAMELA 28 22 6 254 15 2 21. TS ROGER 32 19 16 195 93 13 251 108 9 303 178 4 22. TY SARAH 26 16 43 61 40 39 110 86 34 143 107 27 23. ST TIP 24 15 60 135 69 56 259 142 52 345 214 48 24. ST VERA 43 20 23 148 69 19 249 111 15 385 247 11 25. TS WANNE 27 14 22 170 115 16 362 295 12 443 413 42 26. TY ABBY 31 17 52 164 108 48 286 198 39 338 215 26 27. TD-26 21 16 6 5 55 28 3 28. TS BEN 34 18 10 81 89 6 287 16 2	1.	TY ALICE	18	11	51	105								
3. TY CECIL 4. TS DOT 23 16 24 130 79 23 244 171 20 315 257 16 5. TD-05 12 12 2 6 158 150 3 6. TY ELLIS 25 21 22 71 57 18 145 103 14 185 113 10 8. TD-08 35 21 20 138 86 17 167 93 14 180 99 10 8. TD-08 43 20 5 195 70 4 396 396 1 9. TS GORDON 23 12 13 129 90 9 173 121 5 449 278 1 10. TS HOPE 23 16 33 134 75 29 266 140 23 376 188 21 11. TD-11 47 30 14 144 94 10 138 89 6 171 129 2 12. TY IRVING 26 17 38 163 98 34 286 209 30 441 344 26 13. ST JUDY 18 12 39 105 81 36 173 138 27 277 213 23 14. TD-14 33 19 9 157 43 5 296 118 1 15. TS KEN 29 13 13 13 116 60 10 278 111 7 415 195 3 16. TY LOLA 16 10 23 88 64 21 172 148 19 287 236 14 17. TY MAC 23 16 35 93 66 27 196 152 19 279 227 19 18. TS NANCY 28 19 14 116 86 9 216 186 4 227 219 1 18. TS NANCY 28 19 14 116 86 9 216 186 4 227 219 1 18. TS NANCY 28 19 14 116 86 9 216 186 4 227 219 1 18. TS NANCY 28 19 14 116 86 9 216 186 4 227 219 1 18. TS NANCY 28 19 14 116 86 9 216 186 4 227 219 1 18. TS NANCY 28 19 14 116 86 9 216 186 4 227 219 1 18. TS NANCY 28 19 14 116 86 9 216 186 4 227 219 1 18. TS NANCY 28 19 14 116 86 9 216 186 4 227 219 1 18. TS NANCY 28 19 14 116 86 9 216 186 4 227 219 1 18. TS NANCY 28 19 14 116 86 9 216 186 4 227 219 1 19. TY OWEN 25 15 37 146 78 33 250 158 29 327 256 25 20. TS PAHELA 28 22 6 254 15 2 21. TS ROGER 32 19 16 195 93 13 251 108 9 303 178 4 24. ST VERA 43 20 23 148 69 19 249 111 15 385 247 11 25. TS WENA 43 20 23 148 69 19 249 111 15 385 247 11 25. TS WANNE 27 14 22 170 115 16 362 295 12 443 413 4 26. TY JABBY 31 17 52 164 108 48 286 198 39 338 215 26 27. TD-26 21 16 6 55 28 3 28. TS BEN 34 18 10 81 89 6 287 16 2	2.				21	114	73	17	265	164	.13	348	240	9
4. TS DOT 23 16 24 130 79 23 244 171 20 315 257 16 5. TD-05 12 12 12 6 158 150 3 6. TY ELLIS 25 21 22 71 57 18 145 103 14 185 113 10 7. TS FAYE 35 21 20 138 86 17 167 93 14 180 99 10 8. TD-08 43 20 5 195 70 4 396 396 1 9. TS GORDON 23 12 13 129 90 9 173 121 5 449 278 1 10. TS HOPE 23 16 33 134 75 29 266 140 23 376 188 21 11. TD-11 47 30 14 144 94 10 138 89 6 171 129 2 12. TY IRVING 26 17 38 163 98 34 286 209 30 441 344 26 13. ST JUDY 18 12 2 39 105 81 36 173 138 27 277 213 23 14. TD-14 33 19 9 157 43 5 296 118 1 15. TS KEN 29 13 13 13 116 60 10 278 111 7 415 195 3 16. TY LOLLA 16 10 23 88 64 21 172 148 19 287 236 14 17. TY MAC 23 16 35 93 66 27 196 152 19 279 227 19 18. TS NANCY 28 19 14 116 86 9 216 186 4 227 219 1 19. TY OWEN 25 15 37 146 78 33 250 158 29 327 256 25 20. TS PAMELA 28 22 6 254 15 2 21. TS ROGER 32 19 16 43 61 40 39 110 86 34 143 107 27 23. ST TIP 24 15 60 135 69 56 259 142 52 345 214 48 24. ST VERA 43 20 23 148 69 19 249 111 15 385 247 11 25. TS WANNE 27 14 22 170 115 16 362 295 12 443 413 4 24. ST VERA 43 20 23 148 69 19 249 111 15 385 247 11 25. TS WANNE 27 14 22 170 115 16 362 295 12 443 413 4 26. TY ABBY 31 17 52 164 108 48 286 198 39 338 215 26 27. TD-26 21 16 6 55 28 3 28. TS BEN 34 18 10 81 89 6 287 16 2	3.	TY CECIL		11	46	87	62	37	191	131	33	320		
5. TD-05	4.				24	130	79	23	244	171	20	315	257	16
6. TY ELLIS 25 21 22 71 57 18 145 103 14 185 113 10 7. TS FAYE 35 21 20 138 86 17 167 93 14 180 99 10 8. TD-08 43 20 5 195 70 4 396 396 1   9. TS GORDON 23 12 13 129 90 9 173 121 5 449 278 1 1 10. TS HOPE 23 16 33 134 75 29 266 140 23 376 188 21 11. TD-11 47 30 14 144 94 10 138 89 6 171 129 2 12. TY IRVING 26 17 38 163 98 34 286 209 30 441 344 26 13. ST JUDY 18 12 39 105 81 36 173 138 27 277 213 23 14. TD-14 33 19 9 157 43 5 296 118 1 1 15. TS KEN 29 13 13 13 116 60 10 278 111 7 415 195 3 16. TY LOLA 16 10 23 88 64 21 172 148 19 287 236 14 17. TY MAC 23 16 35 93 66 27 196 152 19 279 227 19 18. TY DWEN 25 15 37 146 78 33 250 158 29 327 256 25 20. TS PAMELA 28 22 6 254 15 2 15 108 9 303 178 4 22. TY SARAH 26 16 43 61 40 39 110 86 34 143 107 27 27 27 28 23. ST TIP 24 15 60 135 69 56 259 142 52 345 247 11 25. TS WANNE 27 14 15 60 135 69 56 259 142 52 345 247 11 25. TS WANNE 27 14 22 170 115 16 362 295 12 443 413 4 26 23. TS BEN 34 18 17 75 26 64 10 88 88 64 21 175 115 15 385 247 11 25. TS WANNE 27 14 22 170 115 16 362 295 12 443 413 47 27 27 27 28 28. TS BEN 34 18 15 16 66 55 28 3					6	158	150	3						
7. TS FAYE 35 21 20 138 86 17 167 93 14 180 99 10 8. TD-08 43 20 5 195 70 4 396 396 1 9. TS GORDON 23 12 13 129 90 9 173 121 5 449 278 1 10. TS HOPE 23 16 33 134 75 29 266 140 23 376 188 21 11. TD-11 47 30 14 144 94 10 138 89 6 171 129 2 12. TY IRVING 26 17 38 163 98 34 286 209 30 441 344 26 13. ST JUDY 18 12 39 105 81 36 173 138 27 277 213 23 14. TD-14 33 19 9 157 43 5 296 118 1 1 15. TS KEN 29 13 13 16 60 10 278 111 7 415 195 3 14. TD-14 33 19 9 157 43 5 296 118 1 1 15. TS KEN 29 13 13 16 60 10 278 111 7 415 195 3 16. TY LOLLA 16 10 23 88 64 21 172 148 19 287 236 14 17. TY MAC 23 16 35 93 66 27 196 152 19 279 227 19 18. TS NANCY 28 19 19 14 116 86 9 216 186 4 227 219 1 18. TS NANCY 28 19 14 116 86 9 216 186 4 227 219 19. TY OWEN 25 15 37 146 78 33 250 158 29 327 256 25 20. TS PAMELA 28 22 6 254 15 2 2 2 2 6 254 15 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2					22	71	57	18	145	103	14	185		
8. TD-08					20	138	86	17	167			180	99	10
9. TS GORDON 23 12 13 129 90 9 173 121 5 449 278 1 10. TS HOPE 23 16 33 134 75 29 266 140 23 376 188 21 11. TD-11 47 30 14 144 94 10 138 89 6 171 129 2 12. TY IRVING 26 17 38 163 98 34 286 209 30 441 344 26 13. ST JUDY 18 12 39 105 81 36 173 138 27 277 213 23 14. TD-14 33 19 9 157 43 5 296 118 1 15. TS KEN 29 13 13 13 116 60 10 278 111 7 415 195 3 16. TY LOLA 16 10 23 88 64 21 172 148 19 287 236 14 17. TY MAC 23 16 35 93 66 27 196 152 19 279 227 19 18. TS NANCY 28 19 14 116 86 9 216 186 4 227 219 1 19. TY OWEN 25 15 37 146 78 33 250 158 29 327 256 25 20. TS PAMELA 28 22 6 254 15 2 21. TS ROGER 32 19 16 43 61 40 39 110 86 34 143 107 27 22. TY SARAH 26 16 43 61 40 39 110 86 34 143 107 27 23. ST TIP 24 15 60 135 69 56 259 142 52 345 214 48 24. ST VERA 43 20 23 148 69 19 249 111 15 385 247 11 25. TS WANNE 27 14 22 170 115 16 362 295 12 443 413 4 26. TY ABBY 31 17 52 164 108 48 286 198 39 338 215 26 27. TD-26 21 16 6 55 28 3 28. TS BEN 34 18 10 81 89 6 287 16 2	8.	TD-08		20	5	195	70	4	396	396	1 .			
10. TS HOPE  23	9.	TS GORDON		12	13	129	90	9	173	121	5	449	278	1
11. TD-11						134	75	29	266	140	23	376		
13. ST JUDY 18 12 39 105 81 36 173 138 27 277 213 23 14. TD-14 33 19 9 157 43 5 296 118 1 1 7 415 195 3 15. TS KEN 29 13 13 116 60 10 278 111 7 415 195 3 16. TY LOLLA 16 10 23 88 64 21 172 148 19 287 236 14 17. TY MAC 23 16 35 93 66 27 196 152 19 279 227 19 18. TS NANCY 28 19 14 116 86 9 216 186 4 227 219 1 19. TY OWEN 25 15 37 146 78 33 250 158 29 327 256 25 20. TS PAMELA 28 22 6 254 15 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	11.	TD-11			14	144	94							
13. ST JUDY 18 12 39 105 81 36 173 138 27 277 213 23 14. TD-14 33 19 9 157 43 5 296 118 1 1 7 415 195 3 15. TS KEN 29 13 13 116 60 10 278 111 7 415 195 3 16. TY LOLLA 16 10 23 88 64 21 172 148 19 207 236 14 17. TY MAC 23 16 35 93 66 27 196 152 19 279 227 19 18. TS NANCY 28 19 14 116 86 9 216 186 4 227 219 1 19. TY OWEN 25 15 37 146 78 33 250 158 29 327 256 25 20 20. TS PAMELA 28 22 6 254 15 2 2 21. TS ROGER 32 19 16 195 93 13 251 108 9 303 178 4 22. TY SARAH 26 16 43 61 40 39 110 86 34 113 107 27 23. ST TIP 24 15 60 135 69 56 259 142 52 345 214 48 24. ST VERA 43 20 23 148 69 19 249 111 15 385 247 11 25. TS WANNE 27 14 22 170 115 16 362 295 12 443 413 4 26. TY ABBY 31 17 52 164 108 48 286 198 39 338 215 26 27. TD-26 21 16 6 555 28 3 28. TS BEN 34 18 10 81 89 6 287 16 2	12.	TY IRVING	26	17	38	163	98	34	286	209		441		
14. TD-14 33 19 9 157 43 5 296 118 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1					39	105	81	36			27	277	213	23
15. TS KEN 29 13 13 116 60 10 278 111 7 415 195 3 16. TY LOLA 16 10 23 88 64 21 172 148 19 287 236 14 17. TY MAC 23 16 35 93 66 27 196 152 19 279 227 19 18. TS NANCY 28 19 14 116 86 9 216 186 4 227 219 1 19. TY OWEN 25 15 37 146 78 33 250 158 29 327 256 25 20. TS PAMELA 28 22 6 254 15 2 21. TS ROGER 32 19 16 195 93 13 251 108 9 303 178 4 22. TY SARAH 26 16 43 61 40 39 110 86 34 143 107 27 23. ST TIP 24 15 60 135 69 56 259 142 52 345 214 48 24. ST VERA 43 20 23 148 69 19 249 111 15 385 247 11 25. TS WAYNE 27 14 22 170 115 16 362 295 12 443 413 4 26. TY ABBY 31 17 52 164 108 48 286 198 39 338 215 26 27. TD-26 21 16 6 555 28 3 28. TS BEN 34 18 10 81 89 6 287 16 2	14.	TD-14		19	9	157	43	5						
16. TY LOLA 16 10 23 88 64 21 172 148 19 287 236 14 17. TY MAC 23 16 35 93 66 27 196 152 19 279 227 19 18. TS NANCY 28 19 14 116 86 9 216 186 4 227 219 1 19. TY OWEN 25 15 37 146 78 33 250 158 29 327 256 25 20. TS PAMELA 28 22 6 254 15 2 21. TS ROGER 32 19 16 195 93 13 251 108 9 303 178 4 22. TY SARAH 26 16 43 61 40 39 110 86 34 143 107 27 23. ST TIP 24 15 60 135 69 56 259 142 52 345 214 48 24. ST VERA 43 20 23 148 69 19 249 111 15 385 247 11 25. TS WANNE 27 14 22 170 115 16 362 295 12 443 413 4 26. TY ABBY 31 17 52 164 108 48 286 198 39 338 215 26 27. TD-26 21 16 6 555 28 3 28. TS BEN 34 18 10 81 89 6 287 16 2	15.	TS KEN	29		13	116	60							
17. TY MAC 23 16 35 93 66 27 196 152 19 279 227 19 18. TS NANCY 28 19 14 116 86 9 216 186 4 227 219 1 19. TY OWEN 25 15 37 146 78 33 250 158 29 327 256 25 20. TS PAMELA 28 22 6 254 15 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	16.	TY LOLA		10	23	88	64	21	172					
19. TY OWEN 25 15 37 146 78 33 250 158 29 327 256 25 20. TS PANELA 28 22 6 254 15 2 15 108 9 303 178 4 21. TS ROGER 32 19 16 195 93 13 251 108 9 303 178 4 22. TY SARAH 26 16 43 61 40 39 110 86 34 143 107 27 23. ST TIP 24 15 60 135 69 56 259 142 52 345 214 48 24. ST VERA 43 20 23 148 69 19 249 111 15 385 247 11 25. TS WAYNE 27 14 22 170 115 16 362 295 12 443 413 4 26. TY ABBY 31 17 52 164 108 48 286 198 39 338 215 26 27. TD-26 21 16 6 55 28 3 28. TS BEN 34 18 10 81 89 6 287 16 2	17.	TY MAC		16	35	93	66	27	196		19			
20. TS PAMELA 28 22 6 254 15 2 251 108 9 303 178 4 21. TS ROGER 32 19 16 195 93 13 251 108 9 303 178 4 22. TY SARAH 26 16 43 61 40 39 110 86 34 143 107 27 23. ST TIP 24 15 60 135 69 56 259 142 52 345 214 48 24. ST VERA 43 20 23 148 69 19 249 111 15 385 247 11 25. TS WAYNE 27 14 22 170 115 16 362 295 12 443 413 4 26. TY ABBY 31 17 52 164 108 48 286 198 39 338 215 26 27. TD-26 21 16 6 55 28 3 28. TS BEN 34 18 10 81 89 6 287 16 2	18.	TS NANCY	28	19	14	116	86							
20. TS PAMELA 28 22 6 254 15 2 21. TS ROGER 32 19 16 195 93 13 251 108 9 303 178 4 22. TY SARAH 26 16 43 61 40 39 110 86 34 143 107 27 23. ST TIP 24 15 60 135 69 56 259 142 52 345 214 48 24. ST VERA 43 20 23 148 69 19 249 111 15 385 247 11 25. TS WAXNE 27 14 22 170 115 16 362 295 12 443 413 4 26. TY ABBY 31 17 52 164 108 48 286 198 39 338 215 26 27. TD-26 21 16 6 55 28 3 28. TS BEN 34 18 10 81 89 6 287 16 2	19.	TY OWEN	25	15	37	146	78	33	250	158	29	327	256	25
22. TY SARAH 26 16 43 61 40 39 110 86 34 143 107 27 23. ST TIP 24 15 60 135 69 56 259 142 52 345 214 48 24. ST VERA 43 20 23 148 69 19 249 111 15 385 214 48 25. TS WAXNE 27 14 22 170 115 16 362 295 12 443 413 4 26. TY ABBY 31 17 52 164 108 48 286 198 39 338 215 26 27. TD-26 21 16 6 55 28 3 28. TS BEN 34 18 10 81 89 6 287 16 2	20.	TS PAMELA	28		6	254	15							
23. ST TIF 24 15 60 135 69 56 259 142 52 345 214 48 24. ST VERA 43 20 23 148 69 19 249 111 15 385 247 11 25. TS WAYNE 27 14 22 170 115 16 362 295 12 443 413 4 26. TY ABBY 31 17 52 164 108 48 286 198 39 338 215 26 27. TD-26 21 16 6 55 28 3 28. TS BEN 34 18 10 81 89 6 287 16 2	21.	TS ROGER	32	19	16	195	93		251	108				
24. ST VERA 43 20 23 148 69 19 249 111 15 385 247 11 25. TS WANNE 27 14 22 170 115 16 362 295 12 443 413 4 26. TY ABBY 31 17 52 164 108 48 286 198 39 338 215 26 27. TD-26 21 16 6 55 28 3 28. TS BEN 34 18 10 81 89 6 287 16 2	22.	TY SARAH	26	16	43	61								
25. TS WAYNE 27 14 22 170 115 16 362 295 12 443 413 4 26. TY ABBY 31 17 52 164 108 48 286 198 39 338 215 26 27. TD-26 21 16 6 55 28 3 28. TS BEN 34 18 10 81 89 6 287 16 2	23.	ST TIP	24	15	60	135	69	56	259	142				
26. TY ABBY 31 17 52 164 108 48 286 198 39 338 215 26 27. TD-26 21 16 6 55 28 3 28. TS BEN 34 18 10 81 89 6 287 16 2	24.	ST VERA	43	20	23	148	69	19	249					11
26. TY ABBY 31 17 52 164 108 48 286 198 39 338 215 26 27. TD-26 21 16 6 55 28 3 28. TS BEN 34 18 10 81 89 6 287 16 2	25.	TS WAYNE	27	14	22	170	115							
27. TD-26 21 16 6 55 28 3 28. TS BEN 34 18 10 81 89 6 287 16 2					52	164	108	48	286	198	39	338	215	26
28. TS BEN 34 18 10 81 89 6 287 16 2					6	55	28	3						
ALL FORECASTS 25 16 695 124 77 591 226 151 471 316 223 368					10		89	6	287	16	2			1
	ALL 1	FORECASTS	25	16	695	124	77	591	226	151	471	316	223	368

TABLE 4-2. ANNUAL MEAN FORECAST ERRORS FOR THE WESTERN NORTH PACIFIC.

		24-HR		48-HR	72-HR			
YEAR	VECTOR	RIGHT ANGLE	VECTOR	RIGHT ANGLE	VECTOR	RIGHT ANGLE		
1971	111	64	212	118	317	177		
1972	117	72	245	146	381	210		
1973	108	74	197	134	253	162		
1974	120	78	226	157	348	2 <b>4</b> 5		
1975	138	84	288	181	450	290		
1976	117	71	230	132	338	202		
1977	148	83	283	157	407	228		
1978	127	75	271	179	410	297		
1979	124	77	226	151	316	223		





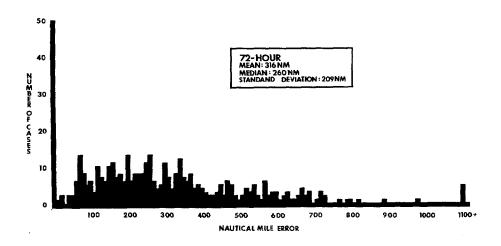


FIGURE 4-1. Frequency distribution of 1979 24-, 48-, and 72-hour forecast vector errors for all significant tropical cyclones in the western North Pacific.

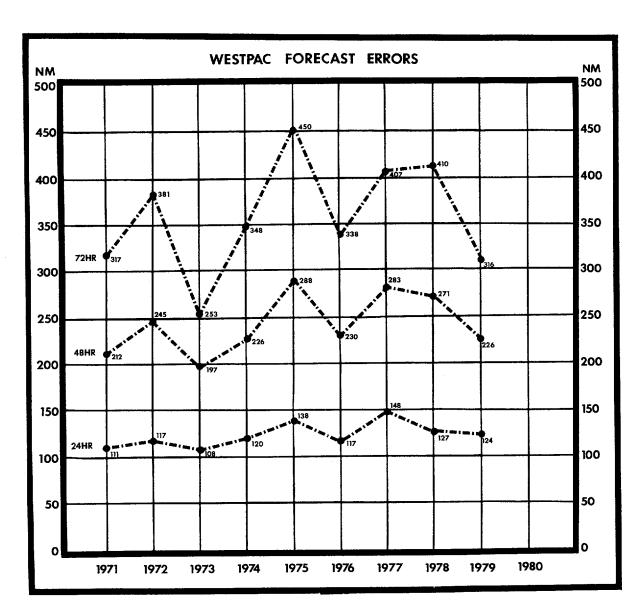
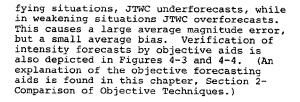


FIGURE 4-2. Annual vector errors (nm) for all cyclones in the western North Pacific.

Intensity verification statistics for all significant tropical cyclones in the western North Pacific area are depicted in Figures 4-3 and 4-4. The average absolute magnitude of the intensity error as well as the intensity bias (algebraic average) are graphically depicted. An analysis of the errors indicates that JTWC intensity forecasts often lag true intensity. In intensi-



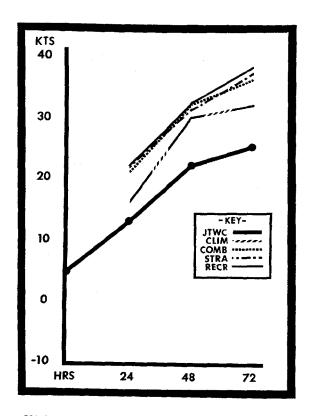


FIGURE 4-3. Comparison of average intensity errors (magnitude) for all cyclones in the western North Pacific.

and the second of the second

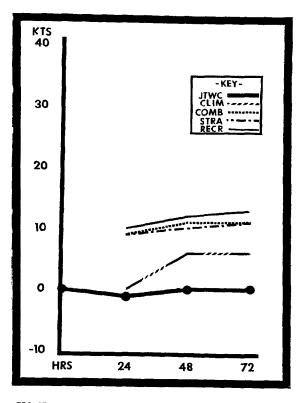


FIGURE 4-4. Comparison of average intensity errors (biases) for all cyclones in the western North Pacific.

## b. North Indian Ocean Area

Forecast positions at Warning times and 24-, 48-, and 72-hour valid times were verified by the same methods used for the western North Pacific area. Table 4-3 is the forecast error summary for the significant tropical cyclones in the North Indian

Ocean area. Table 4-4 contains the annual average of forecast errors back through 1971. Vector errors are plotted in Figure 4-5. Seventy-two hour forecast errors were evaluated for the first time in 1979.

Forecast intensities were not verified.

		TABLE			ERROR SUMMI T TROPICAL			NORTH IND	ian oceai	1		,			
	WARNING 24 HOUR 48 HOUR 72 HOUR  POSIT RT ANGLE POS														
CYCLONE															
<u> </u>								*****							
TC 17-79	36	17	26	139	95	22	233	192	18	346	296	14			
TC 18-79	48	24	12	137	78	7	363	284	4						
TC 22-79	54	34	10	122	90	7	170	122	3						
TC 23-79	48	21	14	160	97	9	253	184	5	773	629	2			
TC 24-79	48	26	13	190	142	9	482	332	5	1036	902	1			
TC 25-79	50	26	8	189	103	4	121	73	1						
TC 26-79	52	31	10	148	83	5	163	21	2						
ALL FORECASTS	46	24	93	151	99	63	270	202	38	437	371	17			

TABLE 4-4. ANNUAL MEAN FORECAST ERRORS FOR THE NORTH INDIAN OCEAN (the Arabian Sea was not included prior to 1975). 48-HR 72-HR 24-HR VECTOR RIGHT ANGLE VECTOR RIGHT ANGLE YEAR VECTOR RIGHT ANGLE 224 182 1973 151 1979 

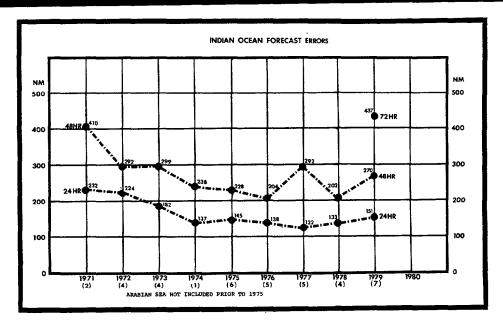


FIGURE 4-5. Annual mean vector errors (nm) for all cyclones in the North Indian Ocean.

#### 2. COMPARISON OF OBJECTIVE TECHNIQUES

#### a. General

Objective techniques used by JTWC are divided into four main categories:
(1) climatological and analog techniques;
(2) extrapolation; (3) steering techniques;
and (4) a dynamic model. The analog technique provides three movement forecasts:
one for straight moving cyclones, one for recurving cyclones and one which combines the tracks of straight, recurving and cyclones that do not meet the criteria of straight or recurving analogs. All techniques were executed using the operational data available at warning time.

#### b. Description of Objective Techniques

- (1) TYFN75 Analog program which scans history tapes for cyclones similar (within a specified acceptance envelope) to the current cyclone. Three 24-, 48-, and 72-hour position and intensity forecasts are provided (straight, recurve and combined).
- (2) MOHATT 700/500 Steering program which advects a point vortex on a preselected analysis and smoothed prognostic field at designated levels in 6-hour time steps through 72 hours. Utilizing the previous 12-hour history position, MOHATT computes the 12-hour forecast error and applies a bias correction to the forecast position.
- (3) TCM The Tropical Cyclone Forecast model is a coarse mesh (220 km) PE Model, with the digitized storm warning position bogused in the 850 mb wind and temperature fields of the FLENUMOCEANCEN Global Band Analysis. Hemispheric forecast data are used on the boundaries.
- (4) CLIM A climatological aid in the form of 24-, 48-, and 72-hour tropical

and a second

cyclone forecast positions and intensity changes for initial latitude/longitude positions. The data are arranged by months and are based on historical data which includes 1945 to 1973. This detailed climatology replaced the previous JTWC climatology on 1 September 1980.

- (5) 12-HR EXTRAPOLATION A track through the current warning position and the 12-hour old preliminary best track position is linearly extrapolated to 24 and 48 hours.
- (6) HPAC The 24- and 48-hour forecast positions are derived by averaging the 24- and 48-hour positions from the 12-hour EXTRAPOLATION track and the CLIM track.
- (7) INJAH74 Analog program for the North Indian Ocean similar to TYFN75, except tracks are not segregated.
- (8) TYAN An updated analog program which combines TYFN75 and INJAH74.
- (9) CYCLOPS An updated version of the MOHATT program which has the capability to select steering forecasts at the 1000, 850, 700, 500, 400, 300 and 200 mb levels.

#### c. Testing and Results

A comparison of selected techniques is included in Table 4-5 for all western North Pacific cyclones and in Table 4-6 for Indian Ocean cyclones. In Tables 4-5 and 4-6, "X-AXIS" refers to techniques listed horizontally across the top, while "Y-AXIS" refers to techniques listed vertically. The example in Table 4-5 compares COMB to MH70. In the 425 cases available for comparison, the average 24-hour vector error was 134 nm for COMB and 160 nm for MH70. The difference of 26 nm is shown in the lower right. (Differences are not always exact due to computational round off.)

## TABLE 4-5.

STATI	STICS	FOR 1	EAR		24 H	R FCS	TS													
	JT	HC_	ST	<u>ra</u>	RE	<u>CR</u>	<u>co</u>	MB.	MH	<u>70</u>	MH	<u>50</u>	<u>TC</u>	<u>M0</u>	CL	<u>IM</u>	XT	<u>RP</u>	HP.	<u>AC</u>
JTWC	591 124	12 <b>4</b> 0								1	NUMBER OF CASES		TEC	-AXIS HNIQUE						
STRA	525 153	122 31	533 153	153 0						•										
RECR	516 139	127 12	489 136	153 -16	524 139	139 0				TE	Y-AXIS CHNIQU ERROR	E	DIF	rror Ferenc Y-X						
COMB	543 135	124 10	514 133	153 -19	509 135	139 -3	551 135	135 0	/	*****	,,,,,,,, <del>,,,</del>			******						
<b>MH</b> 70	435 159	123 36	407 158	150 8	399 163	136 26	425 160	134.	445 158	158 0										
MH50	425 158	124 35	396 157	152 5	389 160	136 25	413 159	135 24	430 157	159 -1	434 157	157 0								
TCMO	121 132	122 10	111 134	152 -16	104 146	128 18	115 141	127 14	96 143	148 -4	96 1 <b>4</b> 2	138 4	124 136	136 0						
CLIM	305 150	129 20	282 142	165 -22	265 150	152 -1	291 149	145 3	245 149	170 <b>-</b> 20	245 150	162 -11	93 153	144 9	315 150	150 0				
XTRP	572 150	124 26	521 146	152 -5	511 153	138 15	538 150	133 17	439 145	159 -13	431 145	158 -12	124 142	136 6	309 168	150 18	584 149	149 0		
HPAC	559 134	124 10	514 129	152 -23	501 135	137 -2	527 134	133 1	434 133	158 -24	426 132	158 -25	124 129	136 -6	309 138	150 -11	571 134	150 -15	571 134	134 0

STATE	STICS	FOR Y	EAR		48 H	R FCST	\$													
	JT	<u>NC</u>	<u>\$T</u>	<u>RA</u>	RE	<u>CR</u>	<u>co</u>	<u>4B</u>	MH	70	Mil	<u> 0</u>	TO	<u>40</u>	₹ī.	<u>(M</u>	XTI	₹ <del>P</del>	<u>HP#</u>	<u>ic</u>
JTWC STRA RECR	471 226 437 309 415	0 224 85 232	462 306 422	306 0	440	252						JT ST RE CO MH	WC - C RA - S CR - I MB - C 70 - N	OFFICE STRAIG SECURV SOMBIN SCHATT SCHATT	AL JTN HT (T) E (TYI ED (T) 700-1 500-1	EC FOR FN 75 N 75) FN 75 B PRC B PRC	) () (G		WAY)	
COMB	247 440 244	15 225 20	248 449 243	-57 306 -62	252 430 243	251 -7	466 244	244 0				XI HP	RP - I		REXII	AND	TION CLIMAT			
<b>№</b> 170	330 313	222 91	340 308	307 1	323 318	249 69	347 310	243 <sup>-</sup> 67	359 308	308 0										
MH50	330 299	220 79	339 296	305 -8	320 297	247 50	345 297	242 55	345 292	310 -17	358 295	295 0								
TCMO	98 249	232 18	97 255	314 -57	86 273	246 27	96 264	254 10	76 264	357 -92	76 263	283 -20	102 257	257 0						
CLIM	244 246	235 11	249 243	330 -86	222 251	276 -25	247 252	265 -12	205 242	337 -94	206 242	294 -51	75 260	272 -11	263 250	250 0				
XTRP	457 291	224 67	450 290	304 -13	430 298	249 49	454 292	241 51	351 295	309 -13	353 291	296 -4	101 311	255 56	260 325	249 76	485 291	291 0		
HPAC	445 232	223	442 231	305 -74	418 235	246 -10	442 233	242 -7	345 231	308 -75	346 228	295 -66	101 245	255 -9	260 235	249 -13	471 233	291 -57	471 233	233 0

STATI	STICS	FOR '	YEAR		72 H	R FCS1	'S									
	JT	WC	ST	'RA	RE	CR	CO	MB	MH	170	MH	50	TCI	40	CL	IM
JTWC	368 316	316 0														
STRA	338 443	315 129	381 453	453 0												
RECR	319 327	331 -3		456 -107	360 349	349 0										
сомв	343 328	316 12		<b>452</b> -109	352 336	349 -12	385 340	340 0								
MH70	230 471	325 147	260 474	464 10	236 488	362 126	259 475	352 122	267 473	473 0						
MH50	227 482	329 153	258 481	467 14	234 488	364 124	257 482	355 127	259 479	469 10	265 486	486 0				
тсмо	73 347	314 33	78 376	445 -68	69 3 <b>9</b> 3	351 41	78 380	359 22	61 401		62 396	484 <del>-</del> 87	84 372	372 0		
CLIM	184 315	308 7	208 333	494 -160	179 338	357 -18	204 334	366 -31	161 329	506 -176	164 331		64 353	389 -34	218 332	332 0

STAT	ISTICS	S FOR	YEAR		24 1	HR FC	STS										
	J	TWC	11	NJA	Mi	170	M	H50	T	CMO	тх	RP	ня	PAC			
JTWC	63 151	151 0								:	NUMBEI	3		X-AXIS	3		
INJA	48 125	134 -7		127 0						ļ	OF CASES		1	CHNIQU ERROR	i		
MH70	28 173	159 14		132 44	30 180	180 0			aggerge	T	Y-AXIS ECHNIQU ERROR		DΠ	ERROR FFEREN	•		
MH50	27 167	158 9		132 32	29 173	175 -1	29 173	173 0		i	ERROR			Y-X	******		
TCMO	2 164	43 121		53 111	2 164	73 91	2	64		164 0							
XTRP	61 146	147 0		127 3		180 -32		173 -23	2 14	164 -150	65 148						
HPAC		148 -12		134 -5		179 -31		175 -26		164 -120		145 -9		135 0			
STATI	STICS	FOR	YEAR		48 H	IR FCS	STS										
	JT	WC	I	NJA	MH	170	Mł	150	TO	MO	хт	RP	HP	AC			
JTWC		270 0								JTW	C - OFF		JTWC				'
INJA		252 -24		227 0						INJA MH70 MH50	A - ANA O - MOH O - MOH	LOG ( IATT 7 IATT 5	INJAH7 00-MB 00-MB	74) PROG PROG		-	
MH70	14 360	332 28	9 365	273 91		340 0				HPAC	- 12- C - MEA	NOF	XTRP A	MD CT	OTAMI	LOGY	
MH50	13 407	338 69		298 149	14 388	331 57	14 388	388 0									
TCMO	0	0 0	0 0	0 0	1 343	61 282		141 202	1 343	343 0							
XTRP	36 259	272 -12	25 243	235 8	15 243	340 -96		388 ~135	1 110	343 -232	37 255	255 0					
НРАС		270 -38		235 -11		310 -76	7 249	424 -174	1 86		24 2 <b>2</b> 5		24 225	225 0			
STATI	STICS	FOR	YEAR		72 H	R FCS	TS										
	JT	WC	IN	JA	ŀ	<b>1</b> H70	ı	MH50									
JTWC	17 437																
AÇNI	12 262		12 292	292 0													
MH70	2 460	876 -415	1 263	361 -97	2 460												
MH50	2 838	876 -37	1 1033	361 672	2 838		2 838		_								

TABLE 4-6.

# CHAPTER Y APPLIED TROPICAL CYCLONE RESEARCH SUMMARY

#### 1. JTWC RESEARCH

Part of the mission of the Joint Typhoon Warning Center is to conduct applied tropical cyclone research as time and resources permit. The purpose of this research is to improve the timeliness and accuracy of operational forecasts. During 1979, there was continued effort to convert and update operational programs and to streamline operational procedures for compatibility with the Naval Environmental Display Station. The following abstracts summarize the year's applied research projects which were completed or are still in progress.

ESTABLISHMENT OF THE JTWC TROPICAL CYCLONE DATA BASE

(Curry, W. T. and Matsumoto, C. R., NAVOCEANCOMCEN/JTWC)

A data base of 6-hour best track positions (intensities, direction and speed of movement) and 24-, 48-, and 72-hour objective technique and official JTWC forecasts for each tropical cyclone in the western North Pacific, Arabian Sea and Bay of Bengal from 1966 through 1978 has been established on FLENUMOCEANCEN computer mass storage systems. Tropical cyclone fix data (position, intensities, platform, etc.) for each tropical cyclone from 1966 through 1977 remain to be added. This climatological data base will be maintained on disk and tape files at FLENUMOCEANCEN Monterey, California and updated annually.

NEDS/COMPUTER APPLICATIONS

(Staff, NAVOCEANCOMCEN/JTWC)

JTWC's objective techniques have been converted by contractors to execute on FLENUMOCEANCEN computers. A NEDS graphic capability is being developed to depict forecast tracks from objective techniques. Evaluation and monitoring of program conversion will continue in 1980.

TROPICAL CYCLONE MINIMUM SEA-LEVEL PRESSURE - MAXIMUM SUSTAINED WIND RELATIONSHIP

(Lubeck, O. M. and Shewchuk, J. D., NAVOCEANCOMCEN/JTWC)

The pressure-wind relationship developed by Atkinson and Holliday (1977), Tropical Cyclone Minimum Sea Level Pressure - Maximum Sustained Wind Relationship for Western North Pacific, is a primary tool used to determine tropical cyclone intensities for JTWC operations. This relationship was re-evaluated and tested with an independent data set. The study produced no significant differences or changes. Therefore, the current Atkinson and Holliday relationship will continue to be used at JTWC. Other regression equations using case-dependent latitude and environmental pressure (versus 1010 mb) as predictors were also tested. These predictors did not improve the maximum sustained windminimum sea-level pressure relationship.

OBJECTIVE TROFICAL CYCLONE INITIAL POSITIONING WITH A WEIGHTED LEAST SQUARES ALGORITHM

(Lubeck, O. M. and Shewchuk, J. D., NAVOCEANCOMCEN/JTWC)

Recent studies indicate tropical cyclone forecast errors through 72 hours can be reduced by more accurate initial warning positions. This study developed an objective and standardized method of determining initial position based on all available fix information. A least squares algorithm was used on available fix data with a weighting scheme which is inversely proportional to the stated fix accuracies. The results of this objective method showed no significant improvement over the current subjective method. Therefore, this method was not incorporated into operational procedures. This method, however, produces an improved tropical cyclone "best track" and was incorporated into JTWC's post-analysis procedures.

EQUIVALENT POTENTIAL TEMPERATURE/MINIMUM SEA-LEVEL PRESSURE RELATIONHIPS FOR FORE-CASTING TROPICAL CYCLONE INTENSIFICATION

(Dunnavan, G. M., NAVOCEANCOMCEN/JTWC)

The relationship between equivalent potential temperature at 700 mb in the center of developing tropical cyclones and associated intensity changes was explored by Sikora (ATR 1975), Milwer (ATR 1976), and Hassebrock (ATR 1977). The Sikora and Milwer studies produced conflicting results, but the Hassebrock study showed some skill in forecasting explosive and rapid deepening when 1977 and 1978 tropical cyclones were evaluated. Evaluation of 1979 tropical cyclones again showed that the Hassebrock technique has some skill. Unfortunately, dewpoint data from aircraft reconnaissance missions from earlier years are not readily available at JTWC, so it has been difficult to increase the data base. The Hassebrock study will be applied to 1980 tropical cyclones and any cyclones prior to 1976 for which data are available. The data base may then be large enough to draw some definite conclusions.

A related study of equivalent potential temperature was also started. A comparison was made of past 12- and 24-hour changes in equivalent potential temperature in the eye of a tropical cyclone with the subsequent 12- and 24-hour changes in 700 mb height. These correlations proved inconclusive, again due to the small initial data base. An attempt will be made to obtain more data for this study also.

BASIC STREAMLINE ANALYSIS AND TROPICAL CYCLONE FORECASTING TECHNIQUE GUIDE

(Guay, G. A., NAVOCEANCOMCEN/JTWC)

A case study, based on an active tropical cyclone period, is being developed. The study will be worked into a training guide for new forecasters and will include basic streamline analysis procedures as well as tropical cyclone forecasting techniques. The case study will also be integrated into STORMEX training (training scenario for DET 4 HQ AWS, 54 WRS, DET 1 1WW, JTWC, and AJTWC personnel).

IMPROVEMENT AND EXTENSION OF THE JTWC CLIMATOLOGY

(Shewchuk, J. D., NAVOCEANCOMCEN/JTWC)

Climatology is an important objective forecast aid for JTWC. A new climatology was developed for the western North Pacific which provides position and intensity forecast information for 24-, 48- and 72-hour intervals. Pertinent statistical information is produced by month for each latitude/longitude of available historical data, which includes 1945 to 1973.

Similar climatological information is being developed for the North and South Indian Oceans and the western South Pacific. The periods of available historical data are 1900-1970, 1900-1969 and 1900-1971, respectively.

#### 2. NEPRF RESEARCH

TROPICAL CYCLONE RESEARCH AT OR UNDER CONTRACT TO THE NAVAL ENVIRONMENTAL PREDICTION RESEARCH FACILITY (NEPRF), MONTEREY, CALIFORNIA

TROPICAL CYCLONE MODELING

(Hodur, R.M., NEPRF and Madala, R., NRL)

A one-way interactive Tropical Cyclone Model (TCM) is being evaluated operationally. This model differs from the original channeled TCM, that has been used for the past three years, in two ways. First, hemispheric forecast data are used on the boundaries as opposed to the channel boundaries used in the original TCM. Second, a new bogus is used to represent the storm based on the observed maximum wind. This latter change has cut the average initial position error by 59% to 15 nm. The one-way interactive TCM average forecast errors at 48, 60 and 72 hr are 8%, 14% and 21% less than the channel model, respectively, for Pacific cyclones through August 1979. Both TCMs have about the same average forecast errors at 12, 24 and 36 hr.

A more sophisticated TCM is being developed jointly by NEPRF and NRL and is expected to become operational in 1981. This TCM includes the effects of surface friction, cumulus clouds and latent and sensible heat transfer from the ocean. Preliminary tests indicate that these improvements may reduce forecast track errors by 15% to 20% when compared to the one-way interactive TCM.

TROPICAL CYCLONE WIND DISTRIBUTION

(Tsui, T., Brody, L.R., and Brand, S., NEPRF)

The wind distribution around tropical cyclones for the warnings issued by the JTWC from 1966 through 1977 have been compiled and edited into a unique data set. An analysis of the wind radii shows the asymmetrical nature of the radii of 30 kt and 50 kt winds around tropical cyclones as a function of the characteristics of the storm. A statistical forecast model to predict the asymmetric wind distribution has been developed.

TROPICAL CYCLONE STRIKE PROBABILITIES

(Brand, S., NEPRF and Jarrell, J.D., Science Applications Inc.)

Tropical cyclone strike probability is a method for determining probabilities up through 72 hours that a tropical cyclone will come within specified distances around geographic points of interest to the user. This program can be used as an aid for operational decisions associated with tropical cyclone evasion, evacuation and base preparedness. Strike probability output is presently being evaluated by a number of Navy and Air Force meteorologists and operational customers in WESTPAC. Other applications of strike probability that are presently being developed include geographic depictions, wind probabilities and strike probabilities for EASTPAC.

A STATISTICALLY DERIVED PREDICTION PROCEDURE FOR TROPICAL CYCLONE GENESIS

(Perrone, T., Lowe, P., Rabe, K., and Brand, S., NEPRF)

A statistical experiment using stepwise discriminant analysis was conducted to determine algorithms to be applied to daily, operationally-available meteorological analyses. Parameters identified as potential predictors of tropical cyclone formation were statistically examined to determine their tropical cyclone genesis prediction capability and were found to possess substantial promise to predict tropical storm formation 24, 48 and 72 hours prior to occurrence.

#### EXTREME SEA STATES WITHIN A TYPHOON

(Rabe, K., and Brand, S., NEPRF)

Extremely high sea states are known to occur to the right of the direction of movement in typhoons. A well-documented case of such extreme sea heights in the western North Pacific was examined and compared with results from a numerical spectral ocean wave model. The wind and sea state field of the numerical model compared favorably with the observed data. An examination was also made to determine how extreme sea states relate to tropical cyclone intensity, forward speed of movement, and circulation size or wind distribution. The results indicated that all three are important with the intensity being the primary factor, speed of movement being of secondary importance and circulation size or wind distribution being the least important factor.

TROPICAL CYCLONE ORIGIN, MOVEMENT AND INTENSITY CHARACTERISTICS BASED ON DATA COMPOSITING TECHNIQUES

(Gray, W.M., Colorado State University)

Observational studies using large amounts of composited rawinsonde, satellite and aircraft flight data have been performed to analyze global aspects of tropical cyclone occurrences. The data were used to study the physical processes of tropical cyclone genesis, tropical cyclone intensity changes, environmental factors influencing tropical cyclone turning motion 24-36 hours before the turn takes place, tropical cyclone intensity determination from upper-tropospheric reconnaissance, and the diurnal variations of vertical motion in tropical weather systems.

IMPROVED UPPER-LEVEL TROPICAL CYCLONE STEERING TECHNIQUES

(Hamilton, H., Systems and Applied Sciences Corporation)

Current automated objective steering forecast techniques incorporating HATRACK and MOHATT algorithms are operationally termed CYCLOPS and may be run in analysis or prognosis modes at seven different atmospheric levels including 1000 mb, 850 mb, 700 mb, 500 mb, 400 mb, 300 mb and 200 mb. Since tropical cyclones vary greatly in areal and vertical extent and may be representatively steered at varying atmospheric levels dependent on state of development/intensity, continuing research is ongoing which will attempt to identify, given certain tropical cyclone input parameters, a "best" steering level or a "weighted scheme" that takes into account several steering levels.

AIRBORNE EXPENDABLE BATHYTHERMOGRAPH OBSERVATIONS IMMEDIATELY BEFORE AND AFTER PASSAGE OF TYPHOON PHYLLIS (AUG 75)

(Schramm, W.G., NEPRF and NAVPGSCOL)

Ocean thermal response to an intense typhoon was analyzed on the basis of data collected during the passage of Typhoon Phyllis (Aug 75) in the Philippine Sea. A unique data set was collected using calibrated Airborne Expendable Bathythermographs dropped from a Navy P-3 aircraft. There were three flights: the first, 14 hours before storm passage, the second 10 hours after passage, and the third two days later. The results indicate a dramatic upward movement of isotherms, relative to the sea surface, in a narrow band under the storm path, with a reversal toward pre-typhoon conditions within three days.

MESOSCALE EFFECTS OF TOPOGRAPHY ON TROPICAL CYCLONE ASSOCIATED SURFACE WINDS

(Brand, S. and Chambers, R., NEPRF, Woo, H., Cermak, J., and Lou, I., Colorado State University, and Danard, M., University of Waterloo)

An analysis was made of the influence of topography on tropical cyclone associated strong surface wind conditions for Subic Bay, Republic of the Philippines by means of an environmental wind tunnel. Surface flow patterns were deduced by smoke and surface oil films, while isotach and gust values were obtained by hot wire anemometers. The laboratory results show the significant effects of the mountainous regions surrounding the Subic Bay harbor complex and indicate preferred sheltered locations. The results were compared with synoptic observations and a high resolution (0.19 nm) diagnostic, one-level, primitive equation model. Where direct comparison could be made, all techniques appeared to show qualitative agreement.

TYPHOON HAVEN STUDIES

(Stevenson, G.A. and Brand, S., NEPRF)

The Typhoon Havens Research Program, the results of which have been summarized in NEPRF Technical Paper 5-76, has been resumed. COMSEVENTHFLT has identified an additional 12 ports and harbors for evaluation as typhoon havens. Work has commenced on Palau, Saipan and Tinian.

# ANNEX A TROPICAL CYCLONE TRACK DATA

# WESTERN NORTH PACIFIC CYCLONE TRACK DATA

#### TYPHOON ALICE

	HEST THACK	#4HVING FARDAS	ZA HOUN FORECAST ENRUMS	48 HDHR FOMFCAST . +84045	72 HOUR FORECAST
MD/DA/Ha	POSIT WIND	POSTT WIND DET HIND	PARTT WIND DSE MIND	POSIT WIND OST WIND	UNIW TEN CHIM TIPOS
0101007	2.5 170.7 20	0.0 0.0 00. 0.	0.n n.n 0u. n.	0.0 0.0 00. 0.	n.0 0.0 00. 0.
0101067	3.1 170.1 25	0.0 0.n U0. U.	Q.o n.n Q0. n.	n.0 0.0 00. 0.	n.0 0.0 0 0.
0101127	3.9 159.4 30	0.0 0.0 00. 0.	0.0 0.0 0U. n.	n.o 0.0 00. 0.	n.D 0.0 DO. O.
0101187	4 6 149 2 35	4.4 168.7 25. 3210.	6.0 165.6 30. 120. *25.	7.7 161.3 35. 40815.	R.3 196.9 45. 54210.
0102007	5.2 168.7 40	5.3 168.5 45. 13. 5.	7.3 164.4 55. 21J. n.	7.9 159 7 50. 495. 5.	A.4 195.2 6D. SAB. 5.
0102067	5.7 168.2 45	5.8 167.8 50. 25. 5.	7.3 164.3 55. 240. 5.	7.4 159.5 60. 498. 5.	R.3 194.9 60. 567. 0.
0102127	6.2 147.8 5n	6.5 166.4 50. 85. 0.	7.7 161.9 60. 376. 10.	9.3 157.2 65. 571. 10.	9.2 192.3 65. 667. 0.
0102187	6.7 147.7 55	6.9 167.7 55. 12. 0.	9.2 165.4 65. 160. 15.	10.7 161.7 65. 263. 10.	11.6 197.0 70. 339. 5.
0103002	7.2 168.0 55	7.2 167.5 05. 30. 0.	9.3 165.7 65. 136. 10.	10.5 161.6 70. 214. 15.	11.6 196.5 70. 306. 0.
0103067	8.D 148.3 50	7.9 168.4 55. 8. 5.	10.6 169.5 65. 123. 1n.	14.1 169.9 65. 415. 5.	17.6 170.7 60. 69515.
0103127	8.5 148.2 50	8.7 168.9 55. 48. 5.	12.2 164.0 65. 201. 10.	15.7 169.0 55. 463. 0.	18.9 171.3 50. 79930.
0103187	8.9 148.1 50	9.6 168.0 55. 42. 5.	12.0 167.7 65. 226. 10.	14.3 169.5 65. 479. 0.	18.8 1/1.0 50. 81535.
0104002	9.2 168.0 55	9.3 167.8 =0. 135.	10.9 166.0 55. 99+ 0.	12.2 162.6 60. 8410.	13.0 158.6 60. 4330.
0104067	9.4 167.8 55	9.5 167.4 50. 175.	10.0 166.1 55. 1235.	12.3 162.7 60. 13015.	13.1 158.8 60. 13735.
0104127	9-5 146-8 55	9.7 167.0 50. 175.	10.0 164.7 55. 84. *1n.	12.3 160.9 60. R920.	13.4 197.1 60. 11440.
0104182	9.5 166.0 55	9.5 165.9 50. 65.	10.2 161.9 55. 53. 910.	10.8 158.0 60. 9125.	11.4 154.0 60. 5345.
0105U0Z	9.5 145.1 55	9.6 165.0 50. B5.	10.7 161.1 55. 59. 415.	11.5 157.2 60. 5930.	11.8 153.1 65. 1945.
0105067	9.7 154.4 60	9.7 164.1 55. 185.	10.5 160.1 60. 7215.	11.7 156.2 bo. 4335.	12.0 152.2 65. 4135.
0105122	10.0 153.6 65	10.1 163.2 55. 2410.	10.7 159.2 60. 7920.	11.6 155.3 60. 4340.	12.0 151.3 65. 6425.
0105182	10.6 162.7 65	10.6 152.7 55. 010.	11.7 154.7 65. 68. 420.	11.6 155.6 70. 7935.	11.9 151.6 70. 15215.
010600Z	11.1 161.7 70	11.2 161.7 55. 615.	12.7 158.0 65. 27. 425.	12.6 153.7 70. 5140.	12.0 149.0 77. 653.
0106062	11.6 150.6 75	11.8 160.4 70. 175.	13.6 156.7 85, 78. ₹1n.	13.0 152.8 95. 975.	17.0 148.6 105. 117. 30.
0106122	12.0 159.4 Bn	12.0 159.4 75. 05.	13.5 154.9 90, 80. 410.	13.6 150.4 100. 96. 10.	12.9 146.3 105. 71. 35.
0106182	12.2 158.4 HS	12.3 158.7 80. 195.	13.4 154.2 90. 73. 415.	13.2 149.8 100. 91. 15.	12.4 145.0 105. 52. 30.
010700Z	12.3 157.8 9n	12.3 157.4 85. 12. +5.	12.n 154.2 95. 70. 415.	11.6 150.1 105. 130. 25.	11.4 146.1 110. 183. 35.
U10706Z	12.3 156.6 95	12.3 156.7 90. 65.	11.8 152.9 105. 83. S.	11.5 148.9 110. 179. 35.	11.4 144.B 120. 186. 40.
010/122	12.3 155.5 100	12.2 155.9 95. 195.	11.R-151.8 110. 94. 20.	11.5 147.8 115. 145. 45.	11.5 143.8 120. 192. 40.
0107182	12.2 154.4 105	12.5 154.0 105. 29. 0.	12.2 149.3 115. 25. 30.	12.0 144-0 120- 12. 45.	13.5 139.1 120. RB- 35.
OTOROGZ	12.1 153.n 11n	12.2 153.1 1lu. B. O.	12.n 148.2 120. 19. 40.	12.0 143.1 120. 13. 45.	12.0 139.0 115. 58. 25.
0108062	12.0 151.5 100	12.0 151.7 115. 12. 15.	11.9 146.5 120. 13. 45.	11.9 141.0 115. 43. 35.	12.0 135.5 110. 169. 15.
0108122	12.0 150.2 90	12.0 150.5 115. 18. 25.	11.0 145.3 120. 19. 50.	11.9 140.0 115. 39. 35. 12.0 138.6 95. 71. 10.	13.5 133.6 95. 2325.
0108182	11.9.149.n B5	11.9 149-1 105. 6. 20.	11.8 143.9 100. 21. 25. 11.7 142.5 90. 30. 15.	11.9 137.3 85. 985.	12.0 131.9 80. 33020.
010900Z 010906Z	11.9 147.9 En	11.8 147.7 100. 13. 20. 11.8 146.5 95. 19. 20.	11.7 141.6 85. 25. 5.	11.9 136.4 80. 12115.	12.0 131.3 75. 35525.
010906Z	12.1 146.6 75	11.8 146.5 95. 19. 20. 12.0 145.2 90. 13. 20.	12.1 139.9 75. 415.	12.3 134.6 65. 19230.	12.4 179.3 60. 44230.
0109122	12.0 144.2 75	12.1 144.0 80. 13. 5.	12.2 138.7 70. 64. 415.	12.2 133.4 60. 25540.	12.4 128.1 55. 51225.
011000Z	11.8 143.n 75	11.9 143.0 BO. 6. 5.	11.9 137.9 70. 66. 20.	12.2 132.7 60. 28240.	12.5 127.4 55. 56115.
0110062	12.1 141.7 60	12.1 141.5 75. 125.	12.0 136.2 65. 129. #3n.	12.2 131.0 55. 36745.	12.7 125.9 50. 6635.
0110122	12.2 140.4 80	12.2 140.1 75. 295.	12.1 134.6 65. 196. *38.	12.5 129.4 55. 43535.	12.8 124.5 50. 766. 5.
0110182	12.2 139.8 B5	12.2 139.0 85. 47. 0.	12.2 133.8 85. 23315.	12.4 128.7 75. 4785.	12.9 123.9 60. 791. 20.
0111002	12.4 138.9 90	12.3 139.0 85. B5.	12.2 136.8 85. 94. 915.	12.1 132.8 75. 296. 5.	12.5 128.0 60. 577. 30.
0111062	12.7 138.3 95	12.5 137.9 90. 265.	12.2 134.2 BO. 1982n.	12.2 129.4 70. 485. 15.	12.2 124.8 45. 697. 25.
0111122	13.1 137.a 95	13.0 137.7 95. 8. 0.	13.5 135.7 BO. 791n.	12.8 132.2 80. 355. 35.	n.0 0.0 00. 0.
0111187	13.4 137.6 100	13.3 137.1 95. 305.	13.3 134.7 80. 146. n.	12.8 132.9 70. 308. 30.	n.0 0.0 00. 0.
0112002	13.7 137.3 100	13.8 137.2 90. B10.	15.8 137.4 BO. 52. 10.	TR.2 140.0 70. 236. 40.	n.0 0.0 00. 0.
0112062	14.1 137.0 100	14.2 136.9 90. B10.	16.2 137.2 70, 29. 15.	1R.5 140+0 60. 273. 40.	0.0 0.0 00. 0.
0115152	14.5 136.6 90	15.2 136.4 85. 435.	17.4 137.8 65. 83. 2n.	0.0 0.0 00. 0.	n.0 0.0 0 0.
0112187	15.0 136.5 9n	15.2 136.5 80. 12. 0.	17.4 137.9 60. 93. 20.	n.o 0.o oo. o.	0.0 0.0 00. D.
011300Z	15.4 136.6 70	15.5 136.5 80. 8. 10.	17.6 138.0 60. 124. 30.	n.o 0+0 D+ -0, 0+	0.0 0.0 00. 0.
011306Z	15.8 136.9 55	15.9 136.7 70. 13. 15.	18-1 138-6 55, 194- 35-	0.0 0.0 00. 0.	0.0 0.0 00. 0.
0113127	16.1 137.3 45	16.1 137.2 65. 6. 20.	0.0 0.0 0. +0. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
0113182	16.1 137.0 40	16.4 137.5 55. 34. 15.	0.n n.n 0. +0. n.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
011400Z	16.1 136.5 30	16.1 136.5 45. 0. 15.	0.0 0.0 00.	0.0 0.0 00. 0.	0.0 0.0 0
011406Z	16.0 136.0 20	16.0 136.0 30. 0. 10.	0.0 0.0 00. 0.	n.º 0.0 DO. O.	0.0 0.0 00. 0.

	AI'L	FORECAS	TS	
	WHNG	24-4R	48-H₹	72-4R
AVG FORECAST POSIT FRANK	18.	105.	222.	338.
AVG RIGHT ANGLE ERROR	11.	83.	175.	271.
AVG INTENSITY MAGNITUDE ERROR	8.	17.	23.	23,
AVG INTENSITY STAS	2.	2.	1.	-3,
NUMBER OF FORECASTS	51	47	43	39
		30	22	70

#### TYPHOON BESS

	BEST THA	СK	WARV	ING	24 +	INDH F	OHECA	s t	4 H	н0ы⊀ Е	OMECA	ST		43.	300 E	U0=C#	
M0/J4/H				= RK0 45			EKK	JAS			FRES			, c 4	JUN -	UNECH	<b>~</b> 1
			CNIM	05T 4140	Pasti	● I ND	Us I	# [ NI()	P0511	w1 NO			P3				
031800Z	7.1 150.n 1		∍n 0_	-0. 0.	0.0 0.0	0.	- 0 +	0.		.0 0.		0.	0.0	-	4143		
0318067	7.8 149.1 1		.n 0.	-0. 0.	0.0 0.0		-0.	0.		• 0 U		0.	H • D	0.0	0.	-0.	0.
031812Z	8.6 147.9 1		.n 0.	-0. U.	0.0 0.0	0.	-0.	٥.		•0 U.		0.		0.0	0.	-0.	0.
0318187	9.3 146.7 1	5 0.D 0	n 0.	-0. 0.	0.0 0.0		-0.	0.		.0 0.		-	0.0	0.0	0.	-0.	0.
031900Z	9.8 145.5 2		.0 0.	-0. 0.	0.0 0.0	- •	-0.	0.		•0 0•	••	0.	0.0	0.0	0.	-0.	-
0319062	10.2 144.6 2	0.0 0	0.	-0. 0.	0.0 0.0		-0.	0.		• U U •	-0.	0.	0.0	0.0	0.	-G.	1) -
0317127	10.4 143.7 2	0.0 0	0.	-0. 0.	0.0 0.0		-0.	0.			-0.	o.	0.0	0.0	v.	- 17 +	0.
0314182	10.6 142.7 2	5 0.0 0.		-0. 0.	0.0 0.0		-0.	0.			-0.	0.	0.0	0.0	0.	~O .	0.
0320002	10.5 141.7 3	0 10.9 141		275.	11.A 13H.H	30.	13.	0.	11.8 135		-0.	.0.	0.0	0 . v	0.	-0-	o.
032006/	10.6 140.7 3	0 10.5 140		12. 0	10.8 136.0		14/.	-5.	10.4 131		115.			1.11.7	50.	305.	-25.
032v12Z	10.7 139.9 3			13. 0.	10.9 135.9		128.		10.9 131		293.			177.8		443.	
0320182	11.0 139.2 3			12. 0.	11.7 135.5		102.				309.	-25.		177.0		444.	
0321002	11.7 138.4 3			35. 0.	11.9 135.3		107.		12.6 132		213.			1.40.4	45.	446.	-45.
0321062	12.3 138.0 4			125.			105.		12.5 132		250.			1.40.0	45·	492.	-45.
0321122	12.8 176.9 4			355.			110.		14.9 137		126.			1.59.1	30.	78.	-60.
0321182	13.3 136.1 5			195.	17.0 134.6				17.4 138		114.			1.0.9	35.	Al.	-25.
0325007	13.7 135.6 5			39. 0.	17.2 134.0		102.		19.3 138			<b>-45</b> .		142.3	35.	66.	0.
0322067	14.1 135.3 6			13. 0.	16.0 134.0		117.	٠.	20.0 134		193.		21.4	1.48.4	4Š.	338.	20.
0322122	14.7 135.0 7					75.		-5.	17.4 133		375.	-10.	0.0	0.0	U.	-0.	0.
0322187	15.3 134.8 7				16.5 133.3		173.	٠.	18.5 133		441.	30.	0.0	0.0	U.	-0-	0.
032300Z	16.1 134.7 7			17. 0.	A.FEI 0.61		216.	n.	19.3 134		495.	45.	0.0	0.0	D.	-0.	0.
0323067	17.0 135.2 B			19. 0.	18.0 134.7		202.	-5.	20.5 136		440.	50.	0 • D	0.0	0.	-0-	0.
0323127	17.8 136.n B			23. 0.	20.3 136.5			•]n•	n.0 0	0.	-0.	0.	0.0	0.0	٥.	-0.	o.
0323182	18.7 136.9 9			135.	20.6 140.7	60.	30+	n.	0.0 0	0 0.	-0.	0.	0.0	0.0	0.	-0-	Ö.
0324007				2510.	21.5 142.1	50.	32+	]5.	0.0 0.	0 0.	-0.	0.	0.0	0.0	0.	-0.	0.
032406Z				65.	22.4 142.6	50.	95.	25.	0.0	0 0.	-0.	0.	0.0	0.0	Ü.	-0.	0.
032412Z	20.3 179.2 9			615.	0.0 0.0	٥.	-0.	ο.	0.0 0	0 0.	-0.	o.	0.0	0.0	0.	-0.	Ö.
0324187	21.2 140.6 5			13. 15.	0.0	0.	-u.	٠.	0.0 0	0 0.	-0.	ō.	0.0	0.0	0.	-0.	ő.
0325007	22.0 142.3 3			23. 30.	0.0 0.0	0.	-u.	0.	0.0 0.	0 0.	-0.	ō.	0.0	0.0	ŏ.	-0.	0.
0353007	22.9 144.7 2	23,4 143.	A 30.	41. 5.	0.0 0.0	0.	-u.	6.	0.0 0.	0 0.	-0.	o.	0.0	0.0	0.	-0.	0.

	AI L	FORECAS	15	
AVG FORFCAST POSIT FRROR AVG RIGHT ANGLE EROOR AVG INTENSITY MAGNITHED ERROR AVG INTENSITY HIS NUMBER OF FORECASTS	WHNG 19. 15. 5. -0. 21	24-4R 114. 73. 10. -6.	48-HR 265. 164. 32. -13.	72-4R 34B. 24N. 31. -26.
•		5	5	3

#### TYPHOON CECIL

	HEST TRA	cK		<b>⊌AH</b> ЧT	NG			24 HO	HR FO	RECAS	11		48 HU	ud En				12 43	JR Fo	م ۽ ر ۵ د	: 1
		•			FRA	285				EHRJ	145				トカメント	5				_	
M0/J4/H2	POSIT WIN	m	POSTT	#INO	DST	WIND	Pos	ŢŢ	₩ [ND	งรเ	4 [ ND	POSI	T	UNIW	DST	<b>4 I N</b> ()	204		Chim	751	
040800Z	3.3 143.4 l		0.0 0.0	0.	-0.	0.	0.0	0.0	0.	- U -	۰.	0.0	0.0	0.	-0.	0.	. ∩ • 0	0.0	0.	-0.	U •
040806Z		5	0.0 0.0	o.	-0.	0.	0.0	0.0	0.	⇒ü•	ο.	0.11	0.0	0.	-0.	0.	0.0	0.0	0.	-0·	n.
0408127		5	0.0 0.0	Ö.	-0.	0.	0.0	0.0	0	-0.	ο.	0.0	0.0	0.	-0.	G.	0.0	0.0	0.	-17 -	0.
0408187		5	0.0 0.0	ō.	-0.	0.	0.0	0.0	0.	-U.	n.	0.0	0 • 0	Ú ◆	- U .	œ.	a = 0	0_0	υ.	-0.	0.
040900Z		5	0.0 0.0	o.	-0.	ō.	0.0	0.0	o.	-0.	n.	0.0	0.0	U.	-u.	0.	0.0	0.0	Ù.	-0.	0.
040706Z		5	0.0 0.0	ů.	-0.	0	0.0	0.0	o.	-0.	0.	0.0	0.0	ů.	-0.	0.	0.0	0.0	0.	-0.	0.
		5	0.0 0.0	Ů.	-0.	ŏ.	0.0	0.0	ō.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-t, -	0.
0409127		20	0.0 0.0	ŏ.	-0.	ŏ.	0.0	0.0	ō.	-0.	ο.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ο.
0409182			•	ŏ.	-0.	0.	0.0	0.0	ŏ.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-O.	0 .
041000Z		3.0		ő.	-0.	ő.	0.0	0.0	o.	-0.	٥.	0.0	0.0	0 -	-0-	0.	0.0	0.0	0.	-0.	0.
041006Z		30		ŏ.	-0.	ů.	0 • n	0.0	o.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0410122		25		0.	-0.	ů.	0.0	0.0	ō.	-0.	n.	0.0	0.0	v.	-0.	0.	0.0	0.0	0.	-0.	ο.
0410182		25,				0.		137.3	35.	U •	0.	P.1 1		40.	50.	-5.	4.2	1.41.2	50.	44.	-5.
0411002		3 n	6.3 139.7	30.	13.	0.		136.6	40.	30.	Λ.	R.4 I		45.	5.9	0.		140.6	55.	57.	(I •
041106Z		3 n	6.5 139.0		.0.			136.3	40.	25.	Λ.	A.2 1		45.	21.	9.		1 10 . 7	55.	45.	-10-
0411122		3 n	6.5 138+6		17.	0.		135.6	40.	8.	-5.	7.H 1		όų.	27.	0.	×.7	179.7	60.	78.	-10-
0411182		30	6.5 138 0		27.	0.		134.5	50.	45.	5.	9.2.1		60.	54	5.		1/3.5	70.	66.	-5.
0412002		35	7.2 137.2		13.	0.			55.	45.	10.	A 9 1		65.	30.	10.		177.4	75.	56.	0.
0412067	/ - / - /	4 N	7.2 136.5		27.	0.		133.5	55.	43.	10.	8.5 1		65.	124.	0.		123.4		190.	-5.
041212Z		4 ()	7.0 136+2		12.	0.		134.0	55.	51.	-	9.4			133.	-š.		1/7.5		228	0.
0412187		45	7.0 135.5		12.	0.		137.7	5ŝ.	50.	n.	9.6			178.			1/5.5	75.		5.
041300Z		45	7.2 134.9		19.	Ų.		137.4	55.	894	η.	9.2			169.			1/5.0		245.	10.
041306Z		45	7.5 134.4		13.	0.		131.9		103.		9.4 1			201.			125.2		238.	0.
0413122	8.0 133.4	45	8.0 133.5		5.	0.		131.0	55.			Q.H ]			174.			144.0			-10.
0413182	8.2 132.6	50	8.3 132.0		19.	-5.		130.0	55.	95+ 36+		10.7			105			100.9	50.	41.	-5.
0414002	8.3 131.6	55	8.3 131.4		0.	ú.		128.1	65.	30.		10.6			113.			119.3		205.	0.
0414062	8.4 130.4	55	B.3 130 -		13.	0.		126.7	65.		-	11.1			100.	0.		117.B		294.	15.
0414122	8.5 129.7	65	8.5 129.2		5.	0.		125.1	75.	62.	-5.	11.1			132.	0.		116.9		361.	15.
0414182	8.9 128.4	7 n	8.6 128.7		21.	0.		124.2	65.	108.		11.4			123.	10.		117.2		359.	25.
041500Z	9.4 127.5	75	9.1 127.5		19.	0.		124.3	70.	150.	٠.	13.0			160.	10.		115.6		44R.	25.
041506Z	10.1 126.5	75	10.0 126.4		9.	0.	11.9		60.	440	-5.	13.4			257	15.		114.7		536.	25.
041512Z	10.8 125.4	Βn	10.7 125.4		5.	0.		121.8	60	34.	٠.	13.9			360.	20.		114.9		546.	30.
041518Z	11.5 124.4	75	11.5 124.4		0.	0.		120.5	60.	93.	٠.	14.4			415.	25.		114.5		605.	25.
041600Z		7 n	11.9 123.2		6.	0.		119.7		163.	10.	15.1			473.	25.		115.4		593.	25.
0416062	12.4 122.6	65	15.5 155.4		17.	0.		114.6	65.	215.	10.				472.	25.		115.3		445.	25.
0416122	12.7 122.2	60	15.8 155.0		13.	٥.		118.6		550.	15.	15.6			494	25.		116.2		640.	25.
941618Z		60	13.0 151.0		35.	٥.		114.4			15.	15.4			379.	0.		140.5		514.	٠
#41700Z	13.1 122.1	55	15.0 155.0		13.	0.		150.0	50.	138+	5.	14.5			378.	0.		119.3		719.	
0417062		55	13.3 155.2		13.	o.		121.5		141.	5.	IA.L			136:	5.		127.7		339.	
0417122		50	13.9 155.4		5.	٥.		122.8	50.		5.	18.5			156;	5.		1/9.3		345.	35.
0417182		50	14.3 122.9		17.	٥.		123.0	50.	BU •	5.	10.2			167.	15.		133.7	60.	259.	
041800Z		45	14.6 123.		0.	0.		125.4	55.	48.		18.8			197	20.	0.0	0.0	0.	-0.	
041806Z	15.0 123.4	45	15.0 123-4		15.	0.		124.3		56.	5.	20.4			149	30.	0.0	0.0	0.	-0.	0.
041812Z	15.6 124.n	45	15.6 124.		5.	0.		127.1	55.	25.	٠.	20.1			195.	25.	0.0	0.0	ō.	-0.	
0418187		45	15.9 124.		33.	0.		127.9			5.				192.	25.	0.0	0.0	D.	-0.	
041 ±00Z		51	16.8 125.		8.			124.9		108.	10.	21.1			-0.	0.	n.0	0.0	0.	-0.	
041706Z	17.5 125.R	50	17.6 125.		₽.			130.3		132.	15.	n.n	0 • 0	0.	-0.	0.	n.0	0.0	0.	-0.	
B41912Z	18.2 127.0	50	17.9 126.		29.	5.		131.2				0.0	0+0	0.				0.0	0.	-0.	
0419187		50	19.6 127.		11.	0.		134.7		51.	15.	0.0	0 • 0	0.	-0.	0.	n.0	0.0	0.	-0.	
842000Z	21.0 129.1	45	21.1 129.		5	5.		136.8		96•	10.	0.0	0.0		-0.	٥.			0.	-0.	
Ø42006Z	22.1 130.4	40	21.8 130*	9 50.	24.	10.	0.0	0.0		-0.		0.0	0.0	-	-0.	٥.	0.0	0.0	0.	-0.	
042012Z	22.8 132.4	30	22.9 132.	n 45.	22.		0.0	0.0		-0.		0.0	0 • 0		-0.	٥.	0.0	0.0	٥.	-0.	
042018Z	23.0 134.4	25	24.0 134.		64.		0.0	0.0		-0.		0.0	0 • 0		-0.	٥.	0.0	0.0	0.	-0.	
8421007		25	0.0 0.	n U.	-0.	0.	0.0	0.0	٥.	-0-	n •	0.0	0.0	0.	-0.	٥.	0.0	0.0	٠.	-0.	

	ΔIL	FORECAS	15	
	<b>≠KN</b> G	24-4R	4B-H3	72-49
AVG FORFCAST POSIT FREOR	15.	87.	191.	320.
AVG HIGHT ANGLE ERROR	11.	62.	131.	215.
AVG INTENSITY MAGNITUDE ERROR	1.	7.	11.	74.
AVG INTENSITY BYAS	i.	3.	7.	11.
NUMBER OF FORECASTS	40	37	33	23
		24	24	16

## TROPICAL STORM DOT

	PEST THE	۸rK		24KV		Rnas		24 HI	DUK FE	RECA.			45 H	)ıı⊀ F	24FCA			\$5 H	OUR F	nerc 4	<b>&lt;</b> T
40/J4/H.	POSIT WIT	NO 1	11Sc	#INA		-	Pas								F 933						
0506007	4.0 147.4		0.0	0	.,,,				w [ Vii)		#1×10		SIT	WIAD	กรา	JIND	PO	5 ] †	#I NO	nst	WIND)
0506062		15 0.			-0.	0.	0.0	n • u	0.	-0.	n.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
U505127				٥.	-0.	0.	0.1	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	0.	0.0	0.0	Ö.	-0.	0.
0506182				v.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	Ů.	-0-	0.
0507007		15 0		u.	-0.	0.	0.0	0.0	0.	−ú.	Λ.	0.0	0.0	ů.	-0.	ō.	0.0	0.0	0.	-0.	0.
		15 0.		U.	-0.	0.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	ő.	0.0				
050/062		15 0.		0.	-0.	0.	0.0	0.0	0.	÷0.	0-	0.0	0.0	ŏ.	-0.	0.		0.0	0.	-0.	0.
0207127		15 0.	0 0.0	0.	-0.	0.	0 • n	0.0	o.	-0.	٥.	0.0	0.0	u.	-0.		0.0	0.0	υ.	-0-	0.
050718/		,0 n	0.0	υ.	-0.	0.	0.0	0.0	ō.	-0.	0.	0.0	0.0	0.		0.	u•0	0.0	0.	-0.	0.
0209005	5.2 138.4	۲n 0,	0.0	0_	-0-	o.	0.0	0.0	o.	-0.	0.	וו	0.0		-0.	0.	0.0	0.0	0.	-0.	0.
<b>050806</b> 2	4.8 136.8 Z	20 0.	0.0	0.	-0.	Ü.	0 • n	0.0	0.	-0.	n.			0.	-0.	0.	0.0	0.0	0.	-0.	ο.
0508127	4.4 135.6	20 0.	0.0	U.	-0.	ő.	0.0	0.0	0.	-0.		1.11	0.0	U.	-0.	0.	0.0	0.0	0.	-0.	0.
0208187	4.5 134.5 2	20 0		Ü.	-0.	0.	0.0	0.0		-0.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0509007	5.0 134.2	?5 0.		Ü.	-0.	0.	0.0		0.		0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	Ð.
0509062		25 0.		Ű.	-0.	0.	0.0	0.0	٥.	-0.	۰.	0.0	0.0	0.	-0.	0.	0.0	0.0	D +	-0.	0.
0509122		5 0.		ŭ.		ö.		0.0	0.	-0-	n.	n.0	0.0	0.	-0.	0.	N • D	0.0	D.	-0-	0.
0509182		., 0.		ŭ.	-0.		0.0	0.0	٥.	-0.	۰.	0.0	0.0	0.	-0.	0.	n • D	0_0	0.	-0-	0.
0510002					-0.	0.	0.0	0.0	0.	-0.	o.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0510067				٠.	-0.	0.	0.0	0.0	0.	-0+	ο.	u • 11	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ő.
0510127			2 130 • 8	20.	19.	-10.		127.0		130.	n.	11.4	123.2	20.	162.	-10.		119.3	25.	6.	-5.
			8 129.5	25.	30.	-5.	10.5	125.4	٠٥٤	123.	۶.	11.9	121.6		116.	-10.		117.7	25.	111.	-10.
0510187			4 127.0	25.	46.	-5.	11.2	121.6	25.	102.	٥.	12.4	119.7	25.	43.	-5.		116.5	35.	219.	
0511002			0 125.4	25.	30.	-5.	10.7	12n.7	25.	65.	0.		116.8		152.	ů.		115.9	35.	255.	-5.
0511062			8 124-9	25.	13.	U.	10.5	114.4	25.	41.	-5.		116.6		163	0.		115.8			-5.
0511122	9.9 123.4 2	۶, 9	9 123.4	25.	0.	0.	10.7	118.3	25.	35.	-6.	13.1			545	~5.				298.	0+
051118Z	10.2 122.2 2	?s 10.	2 155.4	25	6.	0.	11.1			134.	-5	13.R		35	320.	-5.	1700	113.3		474.	15.
0512002	10.4 121.4 2	5 10.	5 121.3	25.	9.	o.	12.1			129.	0.	14.5					10-1	113.0		571.	50.
0512062	10.5 120.6 3	n 10.	5 120+1	25	29.	-5.	12.6			175.	5.	15.6			339.	٠.		114.4		491.	25.
0512122	10.9 119.9 3		7 119+1	25.	48.	-5.	12.0			245.	0.	16.3			375.	10.		115.4		4 70 -	25.
0512182	11.7 119.5 3		9 118.9	30.	35.	ő.	15.0			193.	0.				424.	20.	19.0	116.6		459.	25.
0513002	12.2 119.4 3		5 118.7	30.	45.	ŏ.	15.1		40.			1R.5			299.	25.		122.5	50.	260.	25.
051306Z			5 118.7	30.	41.	0.	14.7			169.	n.	18.3			277.	25.		123.2	50.	255.	25.
0513122			119.2	35.	24.	0.	15.7				5.	17.1		50.		25.	20.0	121.4	50.	351.	25.
0513187			7 119.3	35.	39.	-5.				134.	15.	14.5			238.	25.		174.6	40.	255.	15.
051+002			7 120.2	40.			16.0			154+	15.	18.8			<b>741.</b>	20.		125.1	35.	329.	10.
0514067			0 120.6	35	.0.	0.	15.4		25.	60+	0.	17.2		40.	119.	15.	19.B	128.0	45.	313.	20.
0514127				25.	15.	٥.	15.5		30.	29.	۶.	17.7		45.	121.	20.	0.0	0.0	0.	-0.	0.
0514187			5 150.0		31.	0.	15.5		30.	86.	5.	17.6		40.	244.	15.	0.0	0.0	Ö.	-0.	0.
051 >00Z			5 121.5	25.	31.	0.		151.8	J0.	95.	5.	10,3	126.5	40.	307.	15.	0.0	0.0	ō.	-0-	0.
0515062			2 122.7	25.	я.	υ.	16.R		30.	104.	5.	18.9	127.5	35.	365.	10.	0.0	0.0	ō.	-0.	ő.
	15.6 123.3 2		4 123.2	25.	13.	0.	17.1		30.	170.	5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
0515122			9 124+0	25.	5.	0.	18.4	124.7	30.	161.	5.	0.0	0.0	0.	-0.	ů.	0.0	0.0	0.	-0.	
0515187		5 16.		25.	25.	0.	18.0	127.9	30, 2	225.	5.	0.0	0.0	0.	-0.	ő.	0.0				٥.
051600Z	17.8 126.2 2			25.	21.	0.	0.0	0.0	ō.	-0.	0.	0.0	0.0	0.	-0.	0.		0.0	0.	-0.	0.
051606Z	18.8 127.5 2	5 0.	0.0	0.	-0.	0.	0.0	0.0	ō.	-0.	0.	0.0	0.0	0.	-0.		0.0	0.0	0.	-0.	0.
0516122	20.0 129.n 2	5 0.	0.0	o.	-0.	Ŏ.	0.0	0.0	ů.	-0.	η.	0.0	0.0	0.		0.	0.0	0.0	0.	-0.	0.
0516182	S1.5 131.0 S	5 0.	0.0	0.	-0.	ō.	0.0	0.0	ō.	-0.	0.	0.0	0.0		-0.	٥.	0.0	0.0	٥.	-0.	0.
051700Z	22.2 133.n 2	5 0.		Ü.	-0.	ŏ.	0.0	0.0	0.	-0.	0.			٥.	-0.	٥.	0.0	0.0	٥.	-0.	0.
			-		٠.		• •	., .	•		***	0.0	0.0	0.	-0.	٠.	0.0	0.0	٥.	-0-	0.

	AI L	FORECAS	TS	
AVG FORFCAST POSIT FRANCE AVG RIGHT ANGLE ERROR AVG INTERSITY MAGNITUDE ERROR AVG INTERSITY BIG NUMBER OF FORECASTS	#HMG 73. 16. 2. -2. 24	74-4R 130. 79. 4. 3. 23	48-HR 246. 171. 13. 10. 20	72-48 315. 257. 16. 13. 15

## TROPICAL DEPRESSION 05

	HEST T	- ark			44444				24 Hr	HR. F(	HECA:			4H H(	nd Fo	RFCA*			15 40	UR Fr	RFCA	< T
							175	0-6		~ ( <b>v</b> )	וכנו	# [ NI)	P051		#1 NO	OST	#IND	P051	•	CVIW	nST	w y NID
0/Ja/H2		] 'VI	P05		-lw		-1 4)	Phs	, .		-0.		0.0	0.0	U .	-0.	0.	0.0	0.0	0.	-0.	0.
21/00/	19.1 115.7	10	0.0	0 • 0	0	- ()	ο.	0.0	0.0	0.	-0.	0.	0.0	0+0	U •	-0.	0.	0.0	0.0	٥.	-0.	0.
517062	18.8 115.0	~ 11	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	7.	0.0	0.0	U.	-0.	ő.	0.0	0.0	ů.	-0.	0.
751/16	18.6 114.5	20	0.0	0.0	٠.	-0.	0.	0.0	0.0	0.	-0.	6.	0.0	0.0	0.	-0.	o.	0.0	0.0	0.	-0.	0.
51/18/	10.2 114.2	٠, ١٠	0.0	0.0	0.	-0.	0.	0.0	6.0	0.	-0.	Λ.	0.0	0.0	ů.	-0.	0.	0.0	0.0	0.	-0.	0.
200510	1/.8 114.0	25	0.0	(1 • 1)	Ů.	-0.	Ű.		0.0	0.	-0.	0.	0.0	0.0	0.	-0.	o.	0.0	0.0	ő.	-0.	0.
219067	17.3 113.4	~ ~	0.0	0 • 0	υ.	-0-	0.	0.0	0.0			_	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
212151	16.7 113.7	< 0	U.n	0.0	Ü.	-0.	v.	0.0	n • o	0.	-0.	0.	0.0	0.0	Ů.	-0.	o.	0.0	0.0	ö.	-0.	0.
78181c	16.2 113.4	16	n • u	0 • 0	υ.	-0.	0.	0.0	0.0	0.	-0-	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	ŏ.	-0.	0.
31700Z	15.5 112.5	1 =	0.0	11 • n	υ.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
コーチリカイ	15.5 117.5	15	0.11	ր • ո	υ.	-0.	υ.	0.0	0.0	0.	-0-	n .		0.0	v.	-0.	0.	0.0	0.0	0.	-0.	o.
214157	15.3 112.2	15	0.0	I) • N	u.	- n •	0 •	0 • 0	0.0	٥.	-0.	0.	0.0			-0.		0.0	0.0	0.	-0.	0.
コ1 +1 57	15.1 111.0	15	0.0	0 + 0	u.	-n.	U.	0.0	0.0	٥.	-0+	n.	0.0	0.0	0.		0.	0.0	0.0	0.	-0.	9.
520007	15.0 111.4	<b>63</b>	0.0	0 • 0	u.	-0.	0.	0.0	0.0	٥.	-0.	n •	A.O	0.0	0.	-0.	0.			0.	-0.	0.
52006/	15.7 112.7	20	0.0	0.0	ů.	-0.	0.	0 • n	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
520127	16.5 112.9	20	0.0	0.0	υ.	-0.	υ.	0.0	u * u	0.	-0•	0.	D • 11	0 • 0	0.	-D.	0.		0.0			
520187	17.6 113.2	20	0.0	0.0	U.	-0.	0.	0.0	0 * 11	0.	- U •	n •	0.11	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	0.
521007	18.6 113.4	211	0.0	() • A	Ü.	-a.	υ.	0.0	0.0	ο.	-0.	۰.	U • II	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0+	0.
52106/	19.3 114.4	2.0	0.0	0.0	υ.	-0.	υ.	0.0	0.0	0.	+0.	۰.	U * II	0.0	0 •	-0.	0.	n • 0	0.0	0.	-0-	0+
52112/	20.1 115.4	5.0	0.0	0.0	υ.	-0.	0.	0.0	0.0	0.	-0-	η.	0.0	0.0	ŋ.	-0.	0.	0.0	0.0	0.	-0•	0.
521187	20.4 116.4	20	U.n	1) • 0	0.	- D .	0.	0.0	0.0	0.	-0.	0.	0.0	0 • 0	Ú.	-0.	0.	0.0	0.0	0.	-0 •	0.
522007	21.4 117.7	20	0.0	0.0	U.	-0.	0.	0.0	0.0	0.	-0+	ο.	0.0	0 • 0	U.	-Ù.	0.	n • 0	0.0	0.	-0-	0.
522067	21.6 119.0	26	0.0	0 + n	U.	-n.	0.	0.0	0.0	0.	-u.	٥.	0.0	0.0	0.	-u.	۰,0	0.0	0.0	0.	-0+	0.
255157	21.7 120.4	24	0.0	0.0	U.	-0.	0.	0.0	0.0	0.	-0.	ο.	0.0	0.0	0.	-0_	0.	0.0	0.0	0 •	-0.	0.
255187	21.8 172.3	25	0.0	0.0	U.	-0.	υ.	0.0	0.0	٥.	- v •	0.	0.0	0.0	G •	-0.	0.	0.0	0.0	0.	-0.	0.
523002	22.1 124.3	25	0.0	0.0	U.	-0.	U.	0.0	0.0	٥.	-u.	ο.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1523062	22.5 126.3	30		126.2	30	5.	0.	25.7	135.4	25.	72.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
52312Z	22.8 128.6	3 n	22.6	128.5	30	13.	U.	25.4	137.5	25.	181.	0.	0.0	0.0	ů.	-0.	0.	0.0	0.0	0.	-0.	0.
523187	23.6 130.9	3 1		130.7	30	21.	0.	26.5	134.4	۷5.	551.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	٠.	-0.	0.
1524002	24.9 172.9	25		133.0	30	19.	5.	0.0	0.0	0.	-u.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٥.
524067	26.6 134.4	25		134.4	25.	6	0.	0.0	0.0	0.	<b>-</b> U+	n •	0.0	0 • 0	0.	-0.	0.	0.0	0.0	٥.	-0-	0.
524127	28.2 1 16.2	25		136+1	25.	9.	v.	0.0	0.0	0.	<b>-</b> U•	п.	0.1)	0 + 0	Ů.	-0.	0.	0.0	0.0	0.	-0.	0.
524182	29.8 138.0	26	0.0	0.0	υ.	-0.	0.	0.0	0.0	0.	<b>+</b> U •	n.	0.0	0 + 0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
	1780 170411		V . "		- •	- •	•															
											*											

	ΔiL	FIRECAS	15	
	MHNG	74-4R	48-H3	72-4R
AVG FUNECAST POSIT FRAME	12.	158.	0.	n.
AVG RIGHT ANGLE ERROR	12.	150.	0.	0,
ING INTENSITY MAGNITUDE ERROR	1.	0.	0.	n,
IVG INTENSITY BYAS	1.	0.	n.	0.
HUMBER OF FORECASTS	4	3	U	າ
		1		

# TYPHOON ELLIS

	REST	TRACK			⊌AR41	NG			24 HI	NUR FO				48 HD	uR Fr	RECAS			72 H3	UR F	RFC45	¥T
	:					FRE	กลร				EKK	)4S				EB-50-					_	
40/DA/HR	POSIT	WIND	POS	11	wIN1	DST	WIND	Pos	TT	₩ I ND	DST	# T NID	PNS	IT	MIND	nst	#IND	P09	17	GF IW	n51	MIND
062900Z	11.7 135.4		0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-O·	0.
0629067			0.0	0.0	o.	-0.	ŏ.	0.0	0.0	ō.	-ů.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
	12.2 135.4						0.	0.0	0.0	ŏ.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
062912Z	12.6 134.5		0.0	0.0	o.	-0.				0.	-0.	0.	0.0	0.0	0.	-0.	ō.	0.0	0.0	0.	-0.	0.
062318Z	12.9 134.2		0.0	0.0	0.	-0.	0.	0.0	n.n			-	0.0	0.0	v.	-0.	0.	0.0	0.0	0.	-0.	0.
0630007	13.2 133.4	२ 25	0.0	0 • u	0.	-0.	0.	0 • n	ก₊ก	٥.	-0.	0.	-	-				-	-	0.	-0.	0.
063006Z	13.4 133.4	3 0	0.0	0 • n	0.	-0.	0.	0.0	U • U	0.	-4+	n.	U • U	0.0	0.	-0.	0.	0+0	0.0	0.	-0.	0.
063012Z	13.5 133.0	3.0	0.0	0 • 0	0.	-0.	٥.	0 • n	0.0	٥.	-0+	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0630182	13.6 132.6	5 3 n	0.0	0.0	0.	-0.	0.	0.0	n • n	0.	-0+	n.	0.0	0.0	٠٠.	-0.	.0.	0.0	0.0			
0701007	13.7 131.4	35	13.4	132.0	35.	19.	0.	14.5	124.8	45.	68.	™ln•		127.4		138.	-35.		152.5		223.	-5.
0701062	13.7 131.		13.4	131+4	40	19.	0.	14.6	150.0	45.	64.	•16.		126.5					124.2		235.	0.
0701122	13.8 130.			130.9	40	23.	0.	15.0	128.7	50.	104.	-15.		126.4			-25.		154.0		268.	ο.
070118Z	13.9 129.			129.3	50	13.	0.	14.4	125.4	60.	72.	*15.	15.6	121.6	<b>b</b> 5∙	173.	<b>-5.</b>		117.8		197.	-10.
070200Z	14.1 128.			128.6	55.	6.	ŏ.		125.3	65.		42n.	15.6	121.8	65.	205.	0.	16.B	118.0		225.	-5.
0702062	14.4 127.			127.4	55.	17.	-5.		123.A	65.	lib.	·15.	16.3	120.1	45.	191.	<b>+15</b> .	17.0	116.2	55.	205.	0.
0702127				126.9	55.	5.	-10.		122.2		111.			117.9	50.	188.	-10.	1P.5	115.0	55.	130.	0.
	15.0 126.				65.	9.	-10.		121.4		127.			117.3		171.	-5.	19.5	113.8	60.	103.	10.
070218Z	15.5 125.4			125-8					120.8	75.	77.	10.		117.2	90.	62.	35.		113.5	<b>B</b> 5.	111.	40.
070300Z	16.1 125.			124.9	85.	8.	.0.			80.	60.	20.		116.4	85.	67	30		8.511	75.	150.	50.
070306Z	16.8 124.			154.0	90.	17.	10.		120.1		48.	15.		116.5	75.	158.	20.	0.0	0.0	0.	-0.	0.
070312Z	17.8 123.			123.4	85.	16.	5.		120.2	75.					65.	199.	15.	0.0	0.0	ō.	-0.	0.
070318Z	18.4 122.	6 7n		155.1	70.	13.	0.		118.3	80.	151.	Su.		114.2						0.	-0.	0.
0704002	19.0 121.	2 65	19.0	121.3	60.	0.	-5.		114.6		51*	۴.		112.6	50.	61.	,5.	0.0	0.0			0.
070406Z	19.5 120.	2 6n	19.4	150•n	60.	13.	0.		115.6	>5.	52+	u •		111.7	40.	A9.	15.	0.0	0.0	9.	-0.	
0704122	19.8 119.	4 50	19.7	119.0	60.	23.	0.	21.0	114.8	45.	49.		0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0+	D.
07041BZ	20.1 117.		20.1	117.9	60	0.	0.	21.4	113.7	40.	51.	•1n.	0.0	0 + 0	0.	-0.	0.	u • 0	0.0	0.	-0.	ο.
070500Z	20.2 116.			116.2	60	8.	5.	21.5	111.8	50.	18.	5.	0.0	0 • 0	0.	-O.	0.	n•0	0.0	0.	-0.	0.
0705062	20.3 115.			114.A	60.	23.	5.	21.5	109.7	40.	37.	15.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0705122	20.5 114.			114.2	60.	5.	5.	0.0	0.0	0.	-0.	0.	0.0	0 + 0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
	21.0 112.			113.1	50.	16.	ő.	0.0	0.0		-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	٠.	-0.	0.
0705182						269.	-10.	0.0	0.0		-0.	0.	0.0	0.0	0.	-0.	o.	0.0	0.0	٥.	-0.	0.
070600Z	21.6 111.			111.6				0.0	0.0	ŏ.	-0.	0.	0.0	0.0	0.	-ò.	ō.	0.0	0.0	٥.	-0.	0.
0706062	25.0 110.	1 25	21.7	110.2	25.	19.	٥.	0.0	0.0	٠.		""	.,,		••	٠.	••					

	A) L	FORECAS	TS	
	WHNG	24-4R	48-HR	72-4R
AVG FORFCAST POSIT FRROR	25.	71.	145.	185.
AVG RIGHT ANGLE ERROR	21.	57.	103.	113,
AVG INTENSITY MAGNITUDE ERROR	3.	13.	13.	12.
AVG INTENSITY BIAS	-0.	-3.	-0.	A.
NUMBER OF FORECASTS	22	18	14	1 2
		13	13	10

#### TROPICAL STORM FAYE

	HEST TRA	rk		#4Kv1		70 <b>2</b> 5		24 40	אויר ד(	HELA			48 H	)u∃ F	THE CA			12 4.	)·j+ F	Un=C#	51
43/34/H4	POSIT WIN	n Pos	T T	VINS	DST	WIND	Phi		₩] vn	120	# 1 vil)			,	1847						
0628182	2.8 155.0 1		0.0	0.	-0.	0.	0.0				•	POSI		4140	nst	<b>4</b> ] ₩0	434	. į †	#I V J	15 f	HINI)
0629007	4.5 154.5		0.0	ŏ.	-0.	0.	0.0	0.0	0.	<b>-</b> 0•	r. •	0.0	0.0	0.	- U .	0.	0.0	0.0	0.	-n-	0.
062406Z		5 0.0	0.0	ů.				0.0	0.	-0.	u.	0.0	0.0	0.	-U.	0.	0.0	0.0	U.	-0.	U .
0629122		5 0.0			-0.	0.	0.0	0.0	٥.	-0.	n.	0.0	$0 \cdot 0$	Ú.	-0.	0.	0.0	0.0	0.	-0.	n.
062918Z		5 0.0	0 • 0	0.	,-n.	0.	0.0	0.0	0.	-0.	n.	n • 0	0.0	U.	- O .	0.	0.0	0_0	0.	-0.	0.
0630007	3.5 152.9		0 • n	v.	- n -	0.	0.0	0.0	0.	-0.	0.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0630067			0 • 0	υ.	-0.	٥.	0.0	0.0	0.	-u .	n.	n • 11	0 • 0	U.	-0.	0.	0.0	0.0	Ü.	-0.	n.
0630127			0-0	0.	-0.	0.	0.0	0.0	0.	-0.	А.	0.11	0+0	Ü.	-0.	n.	11 . 0	0.0	0.	-0-	0.
0630182			n • n	0.	-0.	0.	0.0	0.0	0.	-0.	n.	n • II	0 • 0	Ú.	-U.	0.	n • 0	0.0	Ü.	-0-	0.
0701007		0.0	0.0	0.	-0.	ο.	0.0	0.0	٥.	-u.	n.	0.0	0 + 0	0.	-0,	0.	0.0	0.11	Ú.	-0.	0.
0701067	5.3 150.4 2		0.0	0.	~O.	0.	0.6	0.0	0.	- u •	n.	0.0	0 • 0	U •	-0.	0.	0.0	0.0	0.	-0-	0.
0701127	5.7 150.n 2		0.0	٥.	-0.	0.	0.0	n • n	0.	- U +	n.	0.0	$0 \cdot 0$	Ų.	-u.	o.	0.0	U . D	Ŭ.	-0.	0.
	6.0 149.2 2		0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ο.	0.0	0.0	0.	-0.	0.	0.0	0.0	D.	-0.	0.
0701182	6.2 147.9 2		149.7	25.	B5.	v.	8.9	144.4		148.	ς.	10.7 14	42.9	25.	130.	15.		119.2	65.	177.	35.
070200Z	6.5 146.4 2		145.8	30.	36.	5.	7.2	141.6	40.	139.	10.	9.2 1.	37.5	20.	145.	10.		1 +3.3	60.	1-6-	30.
U7U2U6Z	7.3 145.5 2		145-1	3υ.	30.	5.	7.₽	141.7	40.	112.	5.	0.4 1.	36.8	άυ.	140.	15.		1.12.5			35.
0702122	8.0 144.9 2		44.R	30.	25.	ő.	9.4	141.0	40.	30.	5.	10.8 1	36.8	οo.	60.	15.	12.3			148.	
0702182	8.6 144.1 3	u B*5	143.R	30.	30.	0.	10.0	139.8	40.	59.	n.	11.2 1	35.5	20.	90.	20.		141.5			35.
0703UOZ	9.0 143.2 3	n 9.)	143.2	35.	5.	5.	11.1	134.7	50.	46.	la.	12.7 1			137	30.		1.51.4			
0703062	9.4 142.2 3	5 9 R	142.7	40.	25.	٦.		134.6	60.	104.	25.	14.4 1.			211.	50.		1 10 . 0		147.	45.
0703122	9.7 141.4 3	5 9.4	141.2	45.	13.	10.		137.3	65.	100.	30.	15.1 1.			213.	50.		179.1		217.	55.
	10.0 140.A 4	n 10.2 '	139.4	50.	72.	10.		134.7	70.		40.	15.5 1			285	50.				207+	55.
070+00Z	10.3 139.a 4	n 10.2 :	140-1	o6.	19.	10.		137.5	70.		40.	11.4 1		75.	25.	50.		125.3		240.	50.
070406Z	10.5 139.0 3	5 10.8	2.8E	45.	21.	10.		134.H	05.		40.	15.7 1			162.			140.3	80.	47.	60.
0704122	10.6 177.A 3			50 a	24.	15.		133.7	65.	95.	40.	14.6 12			125.	50.	n • 0	0.0	0.	-0.	0 •
070418Z	10.4 136.8 3			<b>&gt;5</b> .	30.	25.		132.2		141.	40.	14.1 12				50.	0.0	0.0	0.	-0.	0.
	10.4 135.6 3			55.	30.	25.		130.4		238.	40.		26.6		210.	55.	n • 0	0.0	0.	-0.	0.
	11.1 135.5 2			50.	75.	25.		130.5		226.	30	0.0	0.0		320.	55.	0.0	0.0	0.	-0.	0.
	11.9 135.1 2		35.3	35	49.	10.		137.4		250.				0 -	-0.	٥.	0.0	0.0	0.	-0.	٠.
	12.6 134.6 2			35.	70.	10.		132.9		235.		0.0	0.0	0.	-0.	0.	0.0	0.0	Ú.	-0.	Π.
	13.3 133.a 2			25.	5.	0.	0.0	0.0			٠.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
	13.8 133.0 2			25.	19.		0.0		0.	-0.	۰.	0.0	0.0	0.	-0.	0.	0.0	0.0	o.	-0+	n.
	15.2 131.9 2		32.1	25.		0.		0.0	٥.	-0.	0.	0.0	0.0	v.	-0.	0.	0.0	0.0	0.	-0.	0.
	16.1 130.7 2		0+0		42.	٥.	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	а.
	17.0 179.6 2		-	0.	-0.	٥.	0.0	0.0	0.	-0-	۰.	0.0	0.0	Ü •	-0.	0.	0.0	0.0	0.	-0.	0.
1.1.002	*1+0 149.P C	· 0.0	0 • 0	υ.	-0.	0.	0.0	0.0	٥.	-0.	п.	N•0	0 • 0	0.	-0.	0.	U • D	0.0	0.	-0.	0.

	AI L	FORECAS	TS	
	WHNG	24	48-H3	72~48
AVG FORFCASI POSIT FRANK	35.	136.	167.	len.
AVG RIGHT ANGLE EROOR	21.	86.	93.	94.
AVG INTENSITY MAGNITUDE ERROR	9.	21.	37.	45.
AVG INTENSITY BIAS	9.	21.	37.	45.
NUMBER OF FORECASTS	20	17	14	11
		5	9	10

#### TROPICAL DEPRESSION 08

	BEST	TRACK	i		WARV				24 H	NHK F	ORECA			48 H	Drink F:	nerca.			/2 H	OUR FO	HECAS	ï
							Rnas				EKK:	J45				FR30.	?≤					
MD/DA/HP		AIND		511	WINT	DST	WIND	Png	T18	PIN)	บรา	#IND	POS	TI	WIND		#IND	PDS	[†	CPIW	nST	WIND
0723062	19.5 140.1	8 SU	0.0	0.0	0_	-0-	0.	0.0	0.0	.0.	-U•	Λ.	0.0	0 • 0	0.	-0.	0.	0.0	• • •			
0723122	20.3 139.0	0.5	0.0	0.0	ō.	-0-	o.	0.0	0.0	•	-0-	0.	0.0	0.0	0.	-0.			0.0	0.	-0.	0.
0723187	21.2 137.0	5 20	0.0									-					0.	0.0	0.0	o.	-0.	o.
				0.0	0.	-0.	0.	0.0	Ո•Ո	0.	- U +	η.	0.0	0+0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
072400Z	22.0 135.0	a 20	0.0	0.0	0.	-0-	0.	0 • n	0.0	0.	-0.	0.	0.0	0.0	0.							
0724067	22.7 134.	4 20		133.6								-				-0.	0.	0.0	0.0	0.	-0.	0.
						105.	u.	58 • u	124.2	20.	183.	Λ.	29.0	119.0	15.	396.	-5.	4.0	0.0	0.	-0.	0.
072412Z	23.4 133.1	ი 2 ი	23.3	133.0	20.	6.	0.	25.0	127.2	20.	90+	5.	0.0	0 • 0	0.							
0724187	24.0 131.0														9 ♦	-0.	0.	n.D	0.0	0.	-0.	0.
			63.4	131.R	20.	17.	٥.	76.N	127.0	20.	203.	5.	0.0	0.0	0.	-D-	0.	0.0	0.0	0.	-0.	0.
072500Z	25.0 170.2	5 50	24.4	130.4	50.	42.	0.	26.6	125.9	1 2	299.	-5.	n n	0.0								
0725067	26.0 128.5	- ;;										•	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0·	0.
			60.5	129.5	20.	45.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.	0.0	0.0	0.	-0-	
0725127	27.4 127.4	15	0.0	0.0	0.	-0.	0.	0.0	0.0	ō.	-0.											
0725187										٠.	-0.	n.	0.0	0.0	٥.	-0.	0.	0.0	0_0	0.	-0.	Π.
	29.4 127.0		0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-u.	0.	0.0	0.0	Ú.	-0.	0.	0.0	0.0	0.	-0.	
9726002	31.5 126.1	3 20	0.0	0.0	0.	-O.	0.	0.0	0.0	Ā-	-41											0.
0726067						~ U •	٠.	v		٥.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	α.
0120002	33.3 124.0	50	0.0	0.0	0.	-0-	0_	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.		•
					-		- •			٠.				3.0	٠.	-u.	٠.		0.0	٠.	-0.	***

	Ai L	FORECAS	TS	
	MKNG	24IR	48-H₹	72-4R
AVG FORECAST POSIT FRANK	43.	195.	395.	0.
AVG RIGHT ANGLE ERROR	20.	70.	395.	0.
AVG INTENSITY MAGNITUDE ERROR	0.	4.	5.	n.
AVG INTENSITY ATAS	0.	1.	-5.	n.
NUMBER OF FORECASTS	5	4	i	ň
•			À	

 $(\mathbf{x}_{i}, \dots, \mathbf{x}_{i}) = (\mathbf{x}_{i}, \dots, \mathbf{x}_{i}) = (\mathbf{x}_{i}, \dots, \mathbf{x}_{i})$ 

## SUPER TYPHOON HOPE

	,	HFST 1	THACK			TVRAW		เกสร		24 Hr	HH FC	RECA:			48 m(	hid Fr	HFCA'			/2 H	OUR FO	DF C & G	17
10/JA/HR	PAST	т ,	eT vn	POS	T T	#INh		WIND	Pns	T T	w1 wo		HIND	ens	11	GM1 w	DST		204	.1+	CFIW	051	w ( NI)
724067	10.2		20	U_0	0.0	U_	-0.	U.	0.0	์ ก•ูก	0.	-0.	0.	0.0	0.0	v.	-U.	0.	0.0	0.0	0.	-0.	0.
	10.3		50	0.0	0.0	ů.	-0.	Ü.	0.0	0.0	o.	-0.	n.	0.0	0.0	u.	-u.	n.	0.0	0.0	0.	-0.	0.
724187	10.3		50	0.0	0.0	ů.	-0.	0.	0.0	0.0	ō.	-0.	n .	0.0	0.0	0.	-0.	ö.	0.0	0.0	ů.	-0.	0.
725007	10.4		50	0.0	0.0	ű.	-0.	0.	0.0	0.0	o.	-0.	0.	0.0	0.0	Ů.	-0.	a.	0.0	0.0	0.	-0.	0.
725067	10.7		24	0.0	0.0	ŏ.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ö.	0.0	0.0	0.	-0.	0.
725127	10.9		25		144.1	۷۶.	-0.	0.		140.4	JD.	42.	]^•		137.0		167.	15.		1 13.2	45.		10.
785187	11.1				143.0	25.	18.	0.		134.4	or.	58.	15.		134.4		246.	10.		110.3		361.	10.
726007	11.2		20		142.7	50.	19.	o.		134.1	JO.	92.	]4.		134.8		229.	5.		1.10.4	45.		5.
726067	11.5		Ş'n		141.5	20.	3.	ű.		137.H		171.	15.		133.4		295	0.		179.2		340.	-5.
726122	11.8		٥٤		140.R	Zo.	6.	o.		137.0		192.	10.		132.7		304.	ŏ.		120.5		345.	-25.
726182	12.3		15		139.7	20.	19.	5.		135.7		199.	۲.		131.4		305.	n.		177.0		417.	-25.
7270UZ	13.2				139.7	20.	46.	5.		135.4		172.	-6.		131.4		250.			1/7.5	35.	347.	-40.
727062	14.2				140.7	20.	38.	5.	0.0	0.0	0.	-0.	n.	0.0	0.0	0.	-0.	0	0.0	0.0	0.	-0-	0.
727122	15.0			0.0	0.0	Ü.	-0.	0.	0.0	0.0	ō.	-0-	a.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
72718Z	15.4		25	0.0	0.0	ŏ.	-0.	ŏ.	0.0	0.0	Ŏ.	-0+	Λ.	0.0	0.0	0.	-0.	0	0.0	0.0	0.	-Ö.	n.
72800Z	16.1		30		137.8	25.	6.	-5.		133.4		166.	п.	19.7	129.4	ōυ.	240.	-25.	20.3	175.2	60.	257.	-40.
728062	16.8		35		138.8	25.		-10.		136.0	40.	254.	₹10.	27.1	133.1	ŝυ.	359.	-30.	24.9	129.5	60.	349.	-55.
728122	17.2		35		137.2	25.		-10.		135.0		300.		24.0	131.3	45.	395.	-40	25.8	5.711	55.	374.	-75.
:726187	17.1		35		136+4			-10.		133.5	35.	331.	<b>*35.</b>	26.6	129.8	45.	397.	-45.	24.8	1/5.3	55.	402.	-75.
72900Z	16.7				135.2	35.		-5		132.2	50.	85.	#25.	19.5	128.6	60.	45.	-40.	10.4	124.3	65.	95.	-65.
729062	16.6				135-1	40.		-10.		132.4	>0.		<b>#3</b> 0.	17.1	130.1	5u.	185.	-55.	18.6	127.2	65.	341.	-50.
729122	10.5				134.0	65.	9.	0.		132.4	75.	39.	₩1n•	10.1	129.3	ქე.	192.	<b>-45</b> .	20.3	175.7	95.	321.	-25.
729182	16.7		70		134.5	70.	19.	v.		131.8	В0.	80.	·in.	1R.7	128 • 7	85.	240.	-45.	20.6	1/5.1	95.	390.	-50.
730002	16.8				133-4	75.	9.	0.		130.2	90.	56.	*10.	19.7	126+9	100.	214.	-30.	20.9	172.9	100.	344.	-5·
730062	17.1				132.4	80.	9.	0.	18.2	129.6		121.	*2K.	19.9	126+3	100.	269.	-25.	21.0	175.3	100.	474.	15.
73012Z	17.4				132.0	90.	17.	5.	18.1	129.3	110.	197.	<b>-20.</b>	10.4	125.8	120+	.334.	0.	21.0	141.8	115.	549.	45.
730182	18.0				131.1	75	41.	5.		124.0					124.9			5.		170.8			60.
731007	18.5	129.4	100	19.5	129.3	100.	я.	0.	20.5	124.4	110.	90.	-20·		150.0			<b>-</b> 5•		115.2	75.		40.
1731062	19.3				128.0		13.	-10.	21.7	123.2	110.	104.	4]5.		117.9		225.	-5.		113.8	25.		-5.
:73112Z	19.6	126.2	130	19.7	126•8	13ú.	13.	0.		120.1		0.			115.7		233.		D • 0	0.0	0.	-0.	0.
73118Z	20.1	124.7	130	20.1	124.4	130.	5.	0.		118.6		29.	5.		115-1		333.		0.0	0.0	0.	-0+	0.
1801002	50.6	123.2	130	20.7	153.5	130.	6.	0.		117.2	90.			0.0	0+0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
801067	50.8				151.5		6.	0.		116.0		116.		0.0	0.0	0.	-0.	0.	0.0	0.0	Ü.	-0-	0.
1801157	21.5				150+0		8.	0.		114.5		155.		0.0	0.0	0.	-0.	0.	0.0	0.0	Ű•	-0•	0.
1801182	21.7				118.4		16.	0.		113.6		5520		0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	Π Π.
)802U0Z	55.5				116.5		13.	٥.		110.4		183.	10.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
180506Z	22.5				114.0	90.	٩.	5.		106.5	30.	103.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
)80515Z	22.7				115.1	70.	53.	0.	0.0	0.0	٥.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0 ·	0.
1805182	55.6				110-1	60.	58.	10.	0.0	0.0	0.	-0.	n.		0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
)80300Z	55.5				108-0	35.	33.	0.	0.0	0.0	0.	-0.		0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
803062	21.7			0.0	0.0	ů.	-0.	0.	0.0	H.U	0.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	o.	-0.	B •
)80312Z	51.1		50	0.0	0.0	۰.	-0.	0.	0.n	n.n	0. 0.	-0.	0.	0.0	0.0	0.	-0.	o.	0.0	0.0	0.	-0.	0.
)80318 <u>/</u> )804007	20.8 20.7			0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	Ö.	-0.	0.
						0.			0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
)80406Z	20.7	99.2		0.0	0.0		-0.	o.	0.0	0.0	0.	~U+	η.	n_0	0.0	0.	-0.	o.	0.0	0.0	0.	-0.	0.
)80412Z )80418Z	20.7	97.9		0.0	0.0	0. 0.	-0.	o.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
)80500Z	21.2	45.4		0.0	0.0	0.	-0.	ŏ.	0.0	0.0	0.	-0.	0.	0.0	0 • 0	0.	-0.	õ.	0.0	0.0	0.	-0.	0.
180506Z	21.5	94.5		0.0	0.0	ŏ.	-0.	ö.	0.0	0.0	ŏ.	-0.	0.	0.0	0 • D	0.	-0.	0.	0.0	0.0	0.	-0.	0.
)805127	21.7	93.5		0.0	0.0	ŏ.	-0.	ŏ.	0.0	0.0	ŏ.	-0+	n.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	Ú.	-0.	0.
1805182	55.5	92.7		0.0	0.0	ŏ.	-0.	o.	0.0	0.0	ŏ.	-0.	۸.	0.0	0.0	Ű.	-0.	0.	0.0	0.0	0.	-0.	n.
	22.3	92.0		0.0	0.0	ŏ.	-0.	0.	0.0	0.0	ŏ.	-0.	0.	0.0	0.0	Ü.	-0.	0.	0.0	0.0	0.	-0-	0.
J80606Z		91.4		0.0	0.0	ŏ.	-0.	ŏ.	0.0	0.0	ŏ.	-0.	0.	6.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0+	0 •
)80612Z	55.5	90.R		0.0	0.0	ŭ.	-0.	Ů.	0.0	0.0	ŏ.	-0.	0.	0.0	0.0	Ü.	-0.	0.	n • 0	0.0	U+	-0-	0.
)80618Z		90.3		0.0	0.0	ŏ.	-0.	Ü.	0.0	0.0	ŏ.	-0.	0.	0.0	0.0	Ü.	-0.	0.	0.0	0.0	0.	-0-	0 •
)B07007	21.7	99.7		0.0	0.0	v.	-0.	0.	0.0	0.0	ŏ.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	n •
JBU7062	21.7	99.0		0.0	0.0	0.	-0.	0.	0.0	0.0	ŏ.	-0.	۸.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	⇒U•	n.
1807122	21.8	98.3		0.0	0.0	ō.	-0.	ō.	0.0	0.0	ŏ.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-O·	n.
J80718Z	55.5	97.2		0.0	0.0	Ů.	-0.	ō.	0.0	0.0	o.	-0.	0.	0.0	0.0	υ.	-0.	0.	0.0	0.0	0.	-0.	n •
180800Z	22.4	76.4		0.0	0.0	0	-0.	ō.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-O•	O.
380806Z	22.5	95.5		0.0	0.0	Ů.	-0.	0.	0 • n	0.0	0.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0•	0.
J84812Z		94.6		0.0	0.0	0.	-0.	0.	0.0	0.0	0.	~0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	v.	-0.	0 •

	۵۱٬۲	FIRECAS	TS	
	WHNG	24-48	48-47	72-4R
AVG FORFCAST POSTT FRHOR	23.	134.	265.	376.
AVG RIGHT ANGLE ERGOR	16.	75.	140.	les.
AVG INTENSITY MAGNITUDE ERROR	3.	14.	22.	74.
AVG INTENSITY BIAS	-1.	-9.	-13.	-16.
NUMBER OF FORECASTS	33	29	23	21
		12	u	3

## TROPICAL STORM GORDON

	REST	FRACK		*	WAKUI	NG			24 4	niiH F(	HECA:			48 H	);;≺ F′	RFCAS	T		72 43	UR Fr	)%FC#4	t T
						E 24	いっする				ERH.	nts .				FRKO	25					
PH/TP/OF	POSIT	MINU	POS	5 T T	WINT	DST	WIND	Pne	T T	WIND	บรา	4 [ M()	POS	3 I T	GNIW	DST	JIND.	100	11	CrIW	751	M I MI)
u725122	18.8 1 12.1	7 ] %	0.0	0.0	u.	<b>∽</b> 0.	0.	0.0	0.0	0.	-0.	6.	0.0	V + 0	0.	-u.	0.	0.0	0.0	0 .	-0-	0.
u725187	19.0 131.	5 20	0.0	U • N	U.	-O.	U.	0.0	6.0	0.	-0.	n.	0.0	0.0	0 •	-0.	0.	0.0	0.0	0.	-0-	η.
0726002	19.5 130.4	4 65	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	- U +	n.	0.0	0 • 0	0.	-0.	0.	0 + 0	0.0	0 -	-0.	n.
0720067	19.9 129.7	7 30	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	n .	0.0	0.0	0.	- U .	0.	0.0	0.0	٥.	-0-	0.
0720122	20.2 128.	7 35	50.5	129.5	30 .	45.	->.	21.0	127.7	45.	204.	-6.	24.0	125.2	• 0 c	3nj.	-5.	25.8	1/2.4	60.	449.	40-
7819270	20.4 127.9	5 40	20.5	124.0	Эυ.	85.	-10.	22.5	126.4		244.	-]n.	24.1	124.3	50 ·	323.	0.	0.0	0.0	0.	-0-	0.
072/002	20.5 126.2	9 40	20.5	126.7	35.	٤.	-5.	21.4	151.4	45.	43.	<b>4</b> ]5.		118.5		63.	0.	n • 0	0.0	0.	-0•	0.
0721062	20.6 125.	3 45	20.7	125-4	40.	А.	-5.	21.7	121.6	<b>&gt;0.</b>	50+	•10.	23.4	117.8	50.	lno.	5.	0.0	0.0	0.	-0.	8.
0727122	20.8 124.2	> 50	20.7	124.2	40.	6.	-10.	21.2	110.2	50.	67.	-5.	22.0	115.8	50.	63.	30.	0.0	0.0	0.	-0.	0.
0727182	50.8 155.4	R 55	20.9	123.1	45.	17.	-10.	21.4	114.1	73.	76.	5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	
0728002	20.9 121.1	7 60	20.4	121.5	5Π.	13.	-10.	20.0	114.2	D5.	150.	15.	0.0	0 + 0	0.	-0.	0.	0.0	0.0	0.	-0+	0.
0728062	21.3 120.5	a 6n	50.9	120.5	<b>55.</b>	29.	-5.	20.9	115.4	70.	134.	25.	U * IJ	0+0	Ü•	-0.	0.	n • 0	0.0	D .	-0-	0.
7516570	22.0 120.3	1 55	92.0	120.2	ΰS.	6.	Ü.	24.6	114.2	25.	511*	S.	n " II	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0.	n.
U728182	22.5 118.	9 50	22.9	119.7	<b>⇒</b> 5.	33.	5.	0.0	0.0	0.	- U •	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	9.
0724007	22.7 117.4	k 50	22.4	117.3	50.	8.	0.	0.0	0.0	0.	- U •	٥.	0.0	0.0	0.	-0.	0.	0.40	0.0	0.	-0.	٥.
0723067	23.1 116.0	0 45	23.1	116.2	45.	11.	0.	0.0	0.0	0.	U •	٥.	0.0	0 - 0	0 .	÷0.	0.	0.0	0.0	0.	-0-	0.
0723127	23.1 114.	7 2∩	23.3	115.2	30.	30.	10.	0.0	0.0	0.	-0.	۸.	0.0	0.0	0.	-0.	0.	0 - 0	0.0	0.	-0-	0.

	AI L	FRECAS	T5	
	HMNG	24-1R	48-H3	72-48
AVG FORFCAST POSIT FRHOR	23.	129.	173.	449.
AVG ALGHI AVGLE ERAPR	12.	90.	121.	27H.
AVG INTENSITY MAGNITUDE ERRUP	6.	11.	9.	40.
AVG INTENSITY BIAS	-3.	1.	5.	40.
NUMBER OF FORECASTS	13	9	5	1
		4	3	0

## TROPICAL DEPRESSION 11

	HFST	THECK			JARVI		1/1 <b>3</b> 5		54 HI	HH F	HECA:			48 H	אוול דו	PRECAS			¥5 40	UR Fr	IQFC&	¥T.
								Pos				41*0	en?	e T T	GNIE		JIND	400	1.0	CV I W	120	W T NI)
AD/JA/HD	POSIT	m   A11	208	7.1	# IN 7	1151	WINT			₩ [ NO		-										-
<b>UUU2U6</b> 2	11./ 135.	3 15	0.0	0.0	U.	-0.	ű.	0.0	0.0	0.	-0+	n.	0.0	0 • 0		-0.	0.	0.0	0.0	0.		0.
0802127	12.3 134.	9 14	0.0	0.0	υ.	-0.	U.	0.0	0.0	0.	-0.	Λ.	0.0	0.0	0.	-0.	0.	u • 0	0.0	0.	-0-	0.
0805187	12-8 134.	0 15	0.0	0.0	υ.	-0.	0.	0.0	0.0	0.	-0.	n.	0.0	0.0	U .	-0.	0.	H • D	0.0	0.	-0.	0.
0803007	13.4 133.		0.0	0.0		-0.	0.	0.0	0.0	0.	-0+	0.	0.0	0 • 0	ů.	-0.	0.	n.0	0.0	0.	-0.	0.
0803067	13.9 132.			131.7	15.		Ü.		124.0		60.	5.	17.4	123.7	35.	164.	10.	20.4	118.6	50.	185.	35.
0803127	14.2 131.			130.7		37.	5.		127.0			10.		122.7		158.	10.	20.9	117.5	50.	156.	35.
							ó.		124.2	35.	103.	15.		122.5		100.	25.	0.0	0.0	0.	-0.	0.
0803197	14.5 130.			154.4		47.						-										
0804007	14.9 129.	H 50	14.9	129.7	20.	5.	0.	16•₽	124.0		30.	lu.		122.0		74.	20.	0.0	QD	0.		0.
0804067	15.3 129.	1 20	15.7	128.5	20.	42.	0.	18.5	122.4	30,	551.	۶.		118.4		197.	25.	n.0	0.0	0.		Π.
0804127	16.0 128.	5 20	16.0	124.4	20.	121.	Ű.	18.0	122.2	25.	193.	۸.	20.2	118.0	35.	137.	20.	n • 0	0.0	o.	<b>-0</b> +	0.
0804187	16.7 128.	0 20	15.7	125.4	20.	149	0.	19.n	121.4	25.	i sb.	5.	0.0	0.0	0.	-0.	0.	P • 0	0.0	0.	-0.	0.
0805007	17.7 127.			127.4		5.	٥.	20.6	124.7	30.	94.	10.	0.0	0.0	ű.	-0.	О.	0.0	0.0	٥.	-0.	0.
0805062	19.6 126.			158.2		95.	0.	22.0	124.4	30.	285.	15.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
						30.	ŏ.		121.1		132.	15.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0402155	19.1 125.			125.4														0.0	0.0	0.		0.
0805187	19.2 174.	1 Sr	19.4	124.4	25.	29.	5.	0.0	n.n	0.		٠.	0.0			-0.	٥.					
<b>UBUBUUZ</b>	19.5 123.	n 20	19.7	123+1	25.	17.	٥.	0.0	0.0	0.	- Ú •	٠.	0.0			-0.	٥.	0.0	0.0	0.		0.
0806067	20.6 121.	0 15	20.0	122.2	20	40.	5.	0.0	በፈሽ	0.	-0.	Λ.	0.0	0.0	U.	-0.	٥.	0.0	0.0	٥.	-0.	0.
0806152	21.0 120.			120.4		13.	5.	0.0	n.n	0.	-0.	0.	V.0	0 - 0	0.	- U .	0.	0.0	0.0	0.	÷0•	0.

	41 L			
	HHNG	24-4R	48-H3	72-4R
AVG FORECAST POSTT FREDH	47.	144.	139.	171.
AVG RIGHT ANGLE ERANA	٦0.	94.	89.	129.
AVG INTENSITY MAGNITUDE ERROR	2.	9.	19.	75.
AVG INTENSITY RIAS	3.	9.	19.	35.
NUMBER OF FORECASTS	14	10	6	2
		u	6	2

# TYPHOON IRVING

REST TRACK WARVING					เดพร	24 HANN FOREURS!					48 HOIJR FORFCAST FRACAS					72 HOUR FORECAST				
.40 ( ) 4 ( ) 4	00017	en POSTT		DST		Pns	• •	w I vo		#TND	POS	17	wind		JIND	POS	1 +	w1 W0	nST	WIND
40/UA/HR	POSIT WIN					0.0		0.	-0.	٥.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
0807122			n 0.	-0.	٥.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	ő.
0807182		0.0 0		-0.	٥.				-0.	0.	0.0	0.0	0.	-0-	0.	0.0	0.0	D.	-0.	0.
			n 0.	-0.	0.	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	0.	n.0	0.0	0.	-0.	0-
080806Z			n 0.	-0.	٥.	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	0.	n.0	0.0	0.	-0.	0.
0808152			.0 0.	-0.	٥.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	n.0	0.0	0.	-0.	0.
0808187			0.	-0.	٥.	0.0	0.0	٠.	103.	5.		129.2	45.	229	15.		126.0	55.	239.	5.
080900Z		3n 17.9 136		_6.	٥.		137.4	35.		-		124.5		3R4.	15.		118.5	60.	528.	5.
080306Z		n 19.3 135		29.	0.		130.3	40.	188.	ln.									266.	5.
0803152		3n 19.3 135		23.	٥.		133.3		150.	10.		129.5		264.	10.		123.5			
080918Z	18.3 134.2 3	9n 18.0 135		49.	0.		134.4			10.		130 · B		245.	10.		125.0		211.	0.
061000Z	18.4 133.7 3	3n 18.5 133		13.	-5.		130.6		183.	5.		126.8		162.	-10.		122.5			-50+
081006Z	18.4 132.2 3	3n 18.8 132		37.	-5.		150.4		224.	n.		126.0		178.			121.3	45.	301.	-25+
0810122	18.3 131.1 3	3n 18.7 131		29.	0.		127.3		198.	n.		123.4		243.			118.8		399.	-50.
0810182	18.0 129.7	3n 18.7 130	.1 30.	48.	0.	19.4	125.7		198.	-5.		121.4		321.			116.9		462.	-50•
081100Z	17.2 128.4 3	3n 17.3 128		8.	0.	17.1	124.4		187.	-5.		120.4		365.			115.5		572.	-25•
0811062	16.5 128.5	35 17.0 127	A 30.	50.	-5.	17.2	127.7	45,	206.			119.4		423.			114.5			-52.
0811122	16.9 129.0	n 17.2 129	2 35.	21.	-5.	18.7	125.4	45.		-10.		151.5		341.			116.7			-25.
0811187	17.5 128.4	5 17.9 128	R 40	33.	-5.	19.0	124.9	50.	106.	-10.		120.8		340.	-15.		116.7		517.	-20.
0B1200Z		on 17.5 128	. 55.	39.	5.	18.7	125.5	65.	103.	٥.	19.1	121.7		321.	-5.	19.5	117.5			-50.
0812067		55 17.9 127		38.	0.	19.n	124.6	65.	168.	-5.		120.9	70.	364.	-5.	19.8	116.7		597.	<b>-50</b> •
0812122		55 18.5 126		26.	0.	19.4	123.4	65.	213.	-5.	19.6	119-6	70.	403.	-10.	14.9	115.5	75.	683.	-15.
0812187		50 18.8 125		61.	-5.	19.R	122.6	65.	226.	-5.	20.0	118+8	75.	478.	<ul><li>10.</li></ul>	14.2	115.5	80.	713.	-10.
0813007		55 20.1 126		9.	ō.	23.4	126.0	75.	58.	0.	27.4	127.5	80.	193.	-10.	24.9	141.0	80.	379.	-10-
0813062		70 21.1 126		11.	o.		120.6	75.	236.	0.	28.4	128+5	80.	249.	-10.	30.5	132.9	80.	473.	-10-
0813122		70 22.0 126		33.	ò.		127.0	75.	156.	-5.	29.5	129+0	80.	303.	-10.	31.7	132.9	80.	447.	-5•
0813182		70 23.2 125		41.	ō.		127.1	80.		-5.	31.0	131.2	85.	416.	-5.	32.6	137.0	85.	653.	5.
0814007		75 23.7 125		13.	~Š.		125.4		128.	<b>=</b> 10.	31.8	127.2	Bo.	223.	-10-	35.0	190.6	70.	2R2.	0.
081406Z		75 24.1 124		8.	o.		125.2		60.	-5.		126.8		163.			130.0	70.	174+	15.
0814122		Bn 24.6 124		16.	ŏ.		126.7			10.		126.7			25.	34.4	129.8	85.	167.	55.
0814187		95 25.3 124		9.	ŏ.		124.6		51.	15.		126.2			30.		129.5		301	55.
0815007		90 25.7 124		13.	ŏ.		124.0		68.	10.		124.7			30.		127.5		524.	55.
							124.2		82.	5.		125-1		201.	35.		128.3		626+	50.
0815062		90 26.5 124		29.	0.		127.6		72.	10.		125.1	90.		60.	0.0	0.0	0.	-0.	0.
081-12Z		90 27.5 123		11.	0.				76.	15.		126.0	60.		35.	0.0	0.0	0.	-0.	0.
0815182		90 28.3 123			٥.		123.8	85.	39.	15.		127.7	60.		35.	0.0	0.0	0.	-0.	0.
081600Z		9n 29.5 123		6.	5.		124.5							202	20.	0.0		0.	-0.	0.
081606Z		9n 31.1 123			0.		125.6			25.	_						0.0	0.	-0.	0.
0816122		95 31.6 123		6.	5.		124.5			54.	0.0	0+0	0.	-0.	٥.	0.0	0.0	0.	-0+	0.
0816187		8n 32.8 123			0.		126.0			50.	0.0	0+0	0.		0.	0.0	0.0	0.	-0+	0.
081700Z		70 34.1 124			0.		124.4			25.	0.0	0+0	0.	-0.	0.	0.0	0.0			
081706Z		55 35.2 126			5.	39 - 1	130.0		362.	10+	0.0	0+0	0.	-0.	0.	0.0	0.0	0.	-0+	0.
081712Z		3n 36.6 128			0.	0.0	0.0		-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0•	0.
081718Z		25 38.9 131		36.	5.	0.0	0.0		-0.	0.	0.0	0+0	0+	-0.	0.	0.0	0.0	0+	-0.	n.
081800Z		25 42.1 134		36.	0.	0.0	0.0	۰.	-0.	٥.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
081806Z	44.2 135.3	25 44.8 137	.n 25.	81.	0.	0.0	0.0	٥.	-0.	n.	0.0	0.0	Ü.	-0.	٥.	n • 0	0.0	g.	-0•	0.

	AI L			
	WKNG	>4IR	48-H3	72-4R
AVG FORFCAST POSIT FRROR	26.	163.	285.	441.
AVE RIGHT ANGLE ERODR	17.	98.	209.	344.
AVG INTENSITY MAGNITUDE ERROR	2.	11.	19.	20.
AVG INTENSITY BEAS	-0.	6.	Э.	-1.
NUMBER OF FORECASTS	38	34	30	25
		10	7	7

#### SUPER TYPHOON JUDY

	REST TRACK	₩ AR YING	24 HOUR FORECASE	48 HORR FORFCAST	TZAGGRAF SUCH SY
		ERRUAS	ENRUMS	FRANAS	
MO/DA/HP	POSIT WIND	POSTT WIND DST WIND	FINITE LEG UNIA TASH	POSIT WIND DST WIND	POSTT WIND AST WIND
0815127	10.5 151.0 15	0.0 0.0 00. 0.	0.n 0.n 0u. n.	0.0 0.0 00. 0.	n.0 0.0 D0. 0.
	11.3 150.1 15	0.0 0.0 00. 0.	0.0 0.0 0u. n.	0.0 0.0 00. 0.	n.0 0.0 D0. n.
	11.8 149.n 15	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. ".
	12.3 147.4 15	0.0 0.0 0D. D.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
	12.8 146.1 25	0.0 0.0 00. 0.	0.n n.o 0u. n.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
	13.3 144.7 30	13.6 144.5 35, 21, 5,	16.6 140.3 00. 109. 10.	20.8 136.8 70. 19220.	24.1 132.9 85. 23040.
	13.8 143.4 35	13.9 143.7 80. 13. 45.	16.5 13H.3 60, 64. 5.	19.1 134.5 78. 9940.	22.9 131.4 85. 14447.
	14.2 142.2 35	14.2 142.0 40, 12, 5.	16.7 137.1 60. 5215.	18.6 133.0 Tu. 17145.	20.8 179.0 85. 24850.
	14.5 141.1 40	14.6 140.6 45. 30. 5.	16.7 135.4 65. 11115.	18.8 130.9 75. 22145.	21.1 127.0 85. 32550.
	15.0 140.0 50	15.0 139.4 50. 35. 0.	17.1 134.5 65. 11425.	19.3 130.0 75. 25750.	21.9 176.4 85. 31240.
	15.7 139.0 55	15.4 138.9 55. 19. 0.	17.7 134.7 75. 101. +35.	19.3 130.1 85. 27945.	21.6 126.7 90. 26630.
	16.4 138.2 75	16.0 137.6 60. 4215.	18.1 133.1 75. 125. *40.	20.0 129.0 85. 26850.	22.5 125.7 90. 28720.
	17.1 137.3 80	16.8 137.3 70. 1810.	18.7 133.4 85. 95. 95.	20.2 129.1 90. 24545.	22.9 175.8 95. 2245.
	17.6 136.4 90	17.4 136.4 75. 1215.	19.4 132.6 85. 121. 44n.	21.1 128.2 90. 23735.	24.0 1/5.3 95. 1985.
	18.2 135.A 110	19.2 135.7 110. 6. 0.	20.4 132.3 130. 99. n.	22.4 129.5 135. 106. 15.	25.3 128.5 135. 40. 40.
	19.0 135.1 115	18.9 135.0 115. 8. 0.	21.2 131.5 130, 1095.	23.5 129.0 135. 97. 25.	26.2 178.9 135. 131. 45.
	19.7 134.7 120	19.7 134.5 125, 11, 5,	22.7 131.2 135. Bl. n.	25.0 129.5 135. 42. 35.	27.7 129.7 125. 240. 35.
0819182	20.5 134.4 125	20.2 134.2 130. 21. 5.	22.7 132.7 135. 53. 10.	24.6 130.5 135. R8. 35.	27.3 130.3 125. 251. 40.
0820007	21.3 133.8 130	21.3 133.9 135. 0. 5.	24.5 132.2 135. 89. 15.	27.3 133.2 135. 329. 40.	29.6 137.1 125. 649. 40.
0820067	22.2 133.2 135	22.2 133.2 135. 0. 0.	25.4 131.5 135. 97. 25.	28.3 133.0 135. 375. 45.	30.6 137.2 115. 700. 30.
0820122	22.7 132.4 135	23.1 132.8 135. 26. 0.	26.4 130.7 120, 139. 20.	29.2 130.6 110. 360. 20.	31.8 134.5 95. 616. 10.
0820187	23.1 131.9 125	23.3 131.2 130. 40. 5.	25.1 126.8 115, 121. 15.	27.4 125.3 105. 170. 20.	31.3 125.5 90. 252. 10.
082100Z	23.4 131.1 120	23.4 131.0 120. 5. 0.	24.5 120.0 110. 6. 15.	24.2 125.7 100. 24. 15.	30.0 125.8 85, 170. 5.
0821067	24.2 130.4 110	24.0 130.4 115. 16. 5.	24.0 130.4 105. 160. 15.	26.2 127.7 90. 175. 5.	32.5 127.5 85, 316, 15,
0B2112Z	24.3 129.4 100	24.5 129.4 115. 12. 15.	26.6 127.0 100. 125. 10.	28,7 125.7 90. 127. 5.	31.2 126.1 80. 199. 20.
0821182	24.4 128.9 100	24.7 128.7 115. 21. 15.	27.n 125.7 100. 118. 15.	29.2 124.5 90. 91. 10.	31.6 175.1 75. 142. 20.
0822007	24.4 128.0 95	24.4 127.9 90 115.	25.8 124.8 65. 43. 42n.	27.7 122.1 20. 7330.	29.9 119.9 25. 17530.
0822062	24.4 127.5 90	24.4 127.2 85 165.	25.4 124.4 60. 78. 425.	27.7 121.8 50. 10420.	30.1 119.7 25. 21525.
0822122	24.5 127.0 90	24.3 126.8 85. 165.	25.0 124.1 60. 151. 925.	27.0 121.5 50. 17710.	0.0 0.0 00. 0.
0822182	25.1 126.3 RS	24.9 126.1 80. 215.	26.8 123.3 55. 84. 425.	29.7 121.0 30. 11425.	0.0 0.0 00. 0.
0823002	25.8 125.4 85	25.8 125.7 85. 5. U.	27.9 123.1 70. 49. •1n.	30.2 120.6 40. 13515.	0.0 0.0 00. n.
082306Z	26.9 124.5 85	26.7 124.4 80. 205.	29.2 121.5 50. 582n.	31.7 119.4 25. 21525.	0.0 0.0 00. 0.
082312Z	27.5 123.7 85	27.5 123.7 BO. O5.	30.1 120.7 45. 100. #15.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
0823182	28.2 123.2 80	2B.0 123+N BO. 15. O.	30.4 120.1 40. 134. 415.	0.0 0.0 00. 0.	n.0 0.0 00. n.
082400Z	28.7 122.9 80	28.8 122.7 70. 1210.	31.2 120.3 30. 144. 425.	0.0 0.0 00. 0.	n.0 0.0 D0. n.
0824062	29.3 122.6 70	29.5 122.2 65. 245.	32.3 120.2 30. 181. •2n.	0.0 0.0 00. 0.	n.0 0.0 00. 0.
0824127	29.8 122.6 6n	29.9 122.7 55. 175.	32.5 120.6 30. 187. *10.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
0824182	30.4 172.7 55	30.6 122.2 55. 29. 0.	32.8 120.2 25. 2475.	0.0 0.0 00. 0.	n.0 0.0 00. n.
0825007	30.9 123.1 55	30.9 122.7 50. 215.	32.8 123.2 25. 16/s n.	n.n 0.0 0. +0. 0.	n.0 0.0 00. 0.
0825062	31.4 123.4 50	31.4 123.5 45. 55.	34.1 126.3 25. 41. 0.	n.n 0+0 u0. 0.	0.0 0.0 00. 0.
082512Z	31.8 124.2 40	32.0 124.1 40. 13. 0.	34.7 127.2 25. 66. 5.	n.n 0.0 00. 0.	0.0 0.0 00. 0.
0825187	32.5 125.1 30	32.3 125.3 35. 15. 5.	0.0 0.0 00. 0.	n. II 0.0 00. 0.	0.0 0.0 00. n.
0826007	33.2 126.1 25	33.6 126.7 30. 39. 5.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
0826067	33.9 127.1 25	34.4 127.6 25. 39. 0.	0.0 0.0 0v. n.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
0826127	34.4 128.5 20	0.0 0.0 00. 0.	0.n 0.0 0v. n.	0.0 0.0 00. 0.	0.0 0.0 00. 0.

	AIL	FORECAS	115	
	₩KNG	24-AR	4B-H7	72-4R
AVG FORFCAST POSIT FREOR	18.	105.	173.	277.
AVG RIGHT ANGLE ERROR-	12.	81.	139.	213.
AVG INTENSITY MAGNITUDE ERROR	6.	16.	29.	28.
AVG INTENSITY REAS	1.	-7.	-9.	-1.
NUMBER OF FORECASTS	39	36	27	23
		17	17	17

## TROPICAL DEPRESSION 14

	BEST	TRACK		WARVI	NG			24 H	NIK FO	RECA	1ê		48 H	OUR F	PFCA	F		₹2 H	OUR FA	PFCAS	i T
					Ξ ₽	Rกค\$				ENH	345				FRRO	15					
MD/DA/HR	POSIT	WIND	POSTT	wing	DST	CHIM	Pns	11	w I NO	DST	4]ND	POS	11	WIND	DST	<b>∢IND</b>	P05	[†	CVIW	nST	MT NI)
0818007	13.5 146.4	. 15	0.0 0.0	٥.	-0.	0.	0.0	0.0	0.	<del>-</del> ti •	٥.	0.0	0.0	0.	-0-	0.	0.0	0.0	0.	-0.	0.
0818062	13.9 166.2	50	13.8 166.3	20.	8.	G.	15.1	164.R	30.	130.	10.	14.5	161.8	•0.	296.	30.	n . o	0.0	0.	-0.	0.
0818122	14.5 155.4	. 21	14.6 166.2	20	35.	0.	16.0	164.H	30.	162.	10.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0.	1) .
081818Z	15.3 165.2	50	14.R 165.A	20.	39.	.0.	16.1	167.7	30.	209.	15.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0 -	П.
081900Z	16.1 144.4		15.7 164.7	20.	25.	0.	17.4	161.9	40.	165.	50.	0.11	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	4.
0819062	17.1 163.0	20	17.0 153.A	20.	3.	0.	19.1	160.3	15.	120.	5.	0.0	0.0	0.	-0.	0.	n • 0	0.0	0.	-0-	0.
081912Z	18.1 163.4	) SV	17.9 163.1	20.	13.	٥.	0.0	0.0	0.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0 •	0.
081918Z	19.2 142.0	15	19.4 162.2	20.	49.	5.	0.0	0.0	e.	-0.	n.	0.0	0.0	v.	-0.	0.	0.0	0.0	0.	-0-	0.
082000Z	20.0 140.0	20	19.5 160.4	20.	41.	10.	0.0	0.0	0.	-0+	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	G .
0820062	21.0 159.4	i in	19.8 160.1	20	77.	10.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0 -	0 .

	ALL FORECASTS							
	WHNG	24-4R	48-H3	72-48				
AVG FORFCAST POSIT FRANK	33.	157.	295.	0.				
AVE RIGHT ANGLE EROOR	19.	43.	113.	0.				
AVG INTENSITY MAGNITUDE ERROR	з.	12.	30.	ο.				
AVG INTENSITY BIAS	3.	12.	30.	0.				
NUMBER OF FORECASTS	q	5	1	Ó				
		•	^					

#### TROPICAL STORM KEN

	BEST	TRACK			wAK VI	NG			24 H	IUK F	DKEUA:	, i		48 HC	DIA FO	RFCAS	it		72 H	OUR FO	SRECA	ST.
	5.	, .,					เการ		-		ĒĸK.	)HS				FRRO-	łS					
MUZ0AZH2	POSIT	מא ז אַר	225	T T	#IN1		CHIM	Pag	ŢŢ	WIND	บรโ	# [ MI)	POS	TI	AIND	nst	#IND	909	11	MIA9		
0830007	22.3 142.0	15	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٥.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	-O·	0.
0830067	22.5 141.5		0.0	0.0	υ.	-0.	0.	0.0	0.0	0.	-U.	n.	0.0	0 • 0	0 •	-0.	0.	0.0	0.0	٥.	-0.	0.
0830122	22.9 140.1	15	0.0	0.0	0.	-0-	0.	0.0	0.4	0.	<b>-</b> ⊍•	a.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0830182	23.3 138.9	15	0.0	0.0	U.	-0.	0.	0.0	0.0	0.	-0.	۸.	0.0	0.0	0.	-0.	0.	n.0	0.0	0.	-0.	0.
2001680	23.7 147.8		0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0831067	24.0 146.6		0.0	0.0	0.	-0-	0.	0.0	n.n	D .	-0.	٠.	0.0	0.0	v.	-0.	0.	0.0	0.0	0.	-0 ·	0.
0831157	24.4 135.6		0.0	0.0	Ü	-0.	0.	0.0	0.0	0.	- U -	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0431187	24.6 134.9		0.0	0.0	0.	-0.	U.	0.0	0.0	0.	-0.	n.	0.0	0.0	ű.	-0.	0.	0.0	0.0	0.	-0.	0.
0901002	24.8 134.1	25		132+5	25	105.	0.	27.4	124.5	35.	200+	5.		120.2		217.			129.5		200.	n.
0901062	24.9 133.5			132.0	25.		n.	25.0	130.3	35.	64+	n.	27.4	128.3	٠ct	190.	<b>-25.</b>	30.0	177.4	30.	485.	5.
0401157	25.1 133.0			132.6	25	25.	0.	25.9	130.1	35	86.	-5.	27.6	120.3	35.	265.	-20.	30.7	127.6	30.	542.	5.
0901182	25.3 132.4			131.6	25.	43.	Ů.	26.5	120.0	35.	111.	-5.	24.2	158.5	35.	274.	-10.	0.0	0.0	0.	-0.	0.
0902002	25.8 131.A			131.7	30	19.	ō.		120.3	40.	151.	-5.	2R.4	127.6	40.	450.	10.	n • 0	0.0	0.	-0-	0.
0902062	26.5 131.2			131.9	30.	42.	-5.		130.A	40.	98∙	<b>-20.</b>	30.8	130-4	35.	343.	10.	0.40	0.0	0.	-0-	0 •
0905152	27.2 130.8			130.8	45.	0.	5.		130.0	50.	61.	-5.	74.1	133.5	30.	205.	10.	0.0	0.0	Ð.	~0•	0 •
0902187	27.8 130.5	40		130-3	45	21.	5.		130.5	50.		5.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0-	Π÷
0903002	20.8 110.2			130-1	+0.	13.	-5.		131.0		173.	5.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0+	₽.
				130.7	40.		-20.		137.6	30.		5.	0.0	0.0	0.	-0-	0.	0.0	0.0	0.	-0+	0.
0903062	30.0 130.4						-15.	0 • n	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
0403155	31.3 131.1			131.7	40. 35.			0.0	0.0	0.	-0-	0.	0.0	0.0	0.	-0.	o.	0.0	0.0	0.	-0.	0.
0903182	32.5 131.9			132+0				0.0	0.1	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0904002	34.0 133.5			133•0	30.	25.	0.		0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ŏ.	0.0	0.0	0.	-0.	
0904062	35.2 174.R		0.0	0.0	0.	-0.	υ.	0.0	0.0	0.	-0.	0.	0.0		0.	-0.	ö.	0.0	0.0	0.	-0.	
0904127	36.5 136.5	. 25	0.0	0.0	U.	-ß.	0.	0.0	0.0	٠.	-0+	".	11 . 11	0.0	•		٠.		3.0	٠.		., •

AVG FORFCAST POSIT FRHOR 29. 116. 273. 415. AVG INTENSITY MAGNITHOF ERROR 5. 6. 111. 105. AVG INTENSITY MAGNITHOF ERROR 73. -2. -5. 3. AVG INTENSITY FIAS 73. -2. -5. 3. AVG INTENSITY FIAS 73. -3. -2. -5. 3. AVG INTENSITY FIAS 73. -3. -5. -5. 3. AVG INTENSITY FIAS 74. AVG INTENSITY FIAS 75. AVG INT

#### TYPHOON LOLA

HEST THAC		24 HOHH FURECAST	48 HOUR FORFCASE	72 HOUR FORECAST				
	FRRARS	Енйэнг	ERRORS					
MO/JA/HR POSIT WIND	POSIT WIND DST WIND	POSTT WIND DST 41MD	POSIT WIND OST ⊄IND	DAIR TSU CRIM TISCO				
0902007 21.3 151.7 25	0.n 0.n 00. 0.	0.n n.n 0u. n.	n.n 0.0 00. 0.	0.0 0.0 00. 0.				
0902067 21.5 151.5 25	0.0 0.0 00. 0.	0.n n.n 00- n.	n.a 0.0 00. 0.	0.0 0.0 00. 0.				
0902127 21.8 151.4 3n	21.8 151.2 30. 11. 0.	24.5 150.5 45. 84. 15.	26.5 150.5 45. 20020.	29.1 152.7 45. 76830.				
0902187 22.1 151.3 30	22.6 150.7 30. 45. 0.	25.2 144.R 45. 108. 1n.	27.8 151.0 45. 27925.	30.0 154.2 45. 44735.				
0903002 22.4 151.1 30	22.6 150.0 30. 62. 0.	23.9 147.9 40. 61F.	25.4 145.4 50. 7025.	26.5 142.0 55. 24630.				
0903062 22.8 150.7 30	22.5 150.5 30. 21. 0.	23.2 149.6 45. 815.	24.4 147.3 50. Al25.	25.6 144.6 55. 14335.				
0903122 23.1 150.3 30	22.5 150.5 30. 37. 0.	73.7 144.4 30. 131. *35.	24.4 147.3 40. 12135.	25.6 144.6 45. 19545.				
0903182 23.4 149.7 35	23.1 150.2 30. 335.	24.5 148.9 35. 98. 435.	25.8 146.8 40. M2. =40.	26.6 143.9 45. 20535.				
090400/ 23.7 149.0 45	23.6 149.1 45. 8. 0.	25.2 146.8 60. 8. 415.	26.7 144+0 70+ 139. <b>-</b> 15.	28.4 141.7 75. 265. 10.				
0904067 24.0 148.4 50	24.0 148.4 50. 0. 0.	25.6 146.0 65. 32. 410.	27.2 143.6 70. 15320.	29.0 141.8 75. 271. 15.				
0904122 24.4 147.6 65	24.3 147.7 65. B. O.	26.0 145.2 75. 72. n.	27.9 143.0 80. 17710.	30.3 141.5 85. 294. 30.				
0904182 24.7 147.1 70	24.7 146.9 70. 11. 0.	26.8 144.2 75% 1235.	28.9 142.1 80. 220. O.	31.6 141.5 90. 324. 45.				
090500Z 25.3 146.7 75	25.2 146.5 75. 12. 0.	27.3 144.0 85. 133. n.	29.9 141.8 85. 238. 20.	37.1 142.0 85. 346. 45.				
0905067 25.6 146.6 75	25.8 146.0 75. 34. 0.	27.0 143.8 85. 137S.	30.2 141.9 85. 245. 25.	37.6 1+2.7 85. 795. 50.				
0905122 20.3 146.5 75	26.4 146.7 75. 12. 0.	29.2 146.5 HO. 49. #10.	32.3 150.0 65. 156. 10.	33.9 156.4 50. 255. 20.				
090518Z 26.8 146.5 80	27.0 146.4 80. 13. 0.	29.0 147.2 75. 595.	32.7 151.0 60. 167. 15.	37.9 157.5 45. 257. 15.				
0905002 27.4 146.5 45	27.3 146.5 80. 65.	29.8 147.4 75. 50. 10.	32.3 150.9 60. 163. 20.	n.0 0.0 00. n.				
090606Z 27.8 146.4 9n	27.9 146.5 90. 9. 0.	30.3 147.8 BO. 69. 20.	32.5 151.7 60. 170. 25.	n.o 0.0 DO. N.				
0906127 28.5 146.3 90	28.5 146.4 90. 5. 0.	31.1 148.0 75. 62. 20.	32.9 152.2 55. 190. 25.	n.o 0.o 00. n.				
0906187 29.3 146.3 80	29.3 146.3 B5. n. 5.	31.8 14H.3 65. 78, 20.	33.0 152.9 50. 216. 20.	n.0 0.0 DD. H.				
0907007 30.1 146.4 55		32.4 148.8 45. 119. 5.	33.5 154.1 40. 220. 10.	n.0 0.0 00. H.				
0907062 30.8 146.6 60	30.8 146.4 50. 10. 0.	33.n 149.6 45, 130. 1n.	n.n 0.0 0. +0. 0.	n.0 0.0 00. n.				
0907122 31.7 147.0 55		33.4 152.6 +0. 154. In.	n.n 0.0 00. 0.	n.0 0.0 0 n.				
0907182 33.0 147.7 45		0.n n.n 0v. n.	n.n 0.0 00. 0.	0.0 0.0 00. 0.				
	34.2 148.4 40. 23. 0.	0.0 0.0 00. 0.	n.n 0.0 00. 0.	n.o 0.0 Uo. n.				
		0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.				
0908062 35.1 150.3 35		0.n n.n 0u. n.	n.0 0.0 00. 0.	0.0 0.0 00. 0.				
090812Z 35.9 151.A 30		0.n n.n 00. n.	0.0 0.0 00. 0.	0.0 0.0 00. 0.				
090818Z 36.6 153.4 30		0.n n.n 00. n.	0.0 0.0 00. 0.	0.0 0.0 00. 0.				
0909002 37.1 155.1 30	0.0 0.0 00. 0.	04 04 -00		* =				

	AIL	FORECAS	15	
	MKNG	24-4R	4B-H3	72-48
AVG FORFCAST POSTT FRHOR	16.	88.	172.	297.
AVE RIGHT ANGLE ERPOR	10.	64.	143.	236.
AVG INIFASILY MAGNITHDE ERRUR	1.	12.	20.	31.
AVG INTENSITY BIAS	-0.	-0.	-2.	1.
NUMBER OF FORECASTS	23	21	19	14
		13	13	9

#### TYPHOON MAC

	REST TRA	rK	WARY	r NG			24 HI	OHR FO	MELA	< t										
				FAR	กสร		C	FC	EHR			48 H	J:17 F:				15 43	OUR F	79F.C4	\$ F
MOZDAZH			wINO	DST	CNIW	Pns	TT	MIND	DoT		ens	17	#IND	FRAN	∢IND					
0913007			0.	-0.	0.	0.0	0.0	0.	-0+	٠,	0.0	0.0	0.	-0.	0.		112	M1 // 3		טאדא
0913062	12.0 138.R 10		0.	-0.	0.	0.0	0.0	o.	-0.	٥.	0.0	0.0	0.	-0.	0.	n • 0	0.0	0.	-0.	0.
0913122	11.9 137.8 1		٥.	-0.	0.	0.0	0.0	Ď.	-0.	0.	0.0	0.0	u.	-0.	0.	0.0	0.0	0.	-0.	0.
091318z	11.9 137.3 1			-0.	0.	0.0	0.0	o.	-0.	۸.	0_0	0.0	0.	-0.	0	0.0	0.0	0.	-0.	0.
091400Z	11.8 136.6 1		٠ ٥.	-0.	0.	0 • n	0.0	ō.	-v.	6.	0.0	0.0	v.	-0.	0.	0.0	0.0	0.	-0.	0.
091406Z 091412Z	11.8 135.7 1			-O.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0		-0-	0.
0914182	11.8 134.R 1	,	- •	-0.	٥.	0.0	0.0	0.	-4.	0.	0.0	0.0	o.	-0.	0.	0.0	0.0	0.	-0.	n.
0915002	12.0 133.n 1		- •	-n.	٥.	0.0	0.0	0.	-0.	n.	0.0	0.0	0.	-0-	0.	0.0	0.0	0.	-0.	0.
0915067	12.3 133.n 1			-0.	0.	0.0	0.0	٥.	-0+	n.	0.11	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
0915127	12.7 131.0 19			-0.	0.	0.0	0.0	٥.	-0.	п.	0.0	0 - 0	0.	-Ů.	o.	0.0	0.0	0.	-0.	0.
0915122	12.9 131.0 20			5.	0.		[27.7	30.	70•	<b>*3</b> 0.	16.8	124.3		197.	-25.		1/0.5	50.	322.	0.
0916007	13.2 130.n 30				-10.		126.6	غ٥.	84.	35.	17.0	123.0		210.	-15.		119.5	40.	339.	
0916062	13.5 129.0 40				-15.	15.3		30.		<b>40.</b>	17.4	122.4		212			118.7			-5.
0916122	13.7 127.0 5			в.	-5.	15.4		60.	158.	<b>-</b> ]n.	14.4	119.5		205	10.	17.8	115.1		352.	
0916187	13.7 127.3 50			38		15.7		60.	184.	-5.	17.2	118.5		324.	10.		114.4		395.	30.
0917002	13.7 126.7 64 13.7 126.2 70			63		16.1		>5.		٥.	17.B	118.0		340.	15.		114.3		340.	30.
0917u6Z				94		15.7		55,		5.	15.5	117.4		250.	10.		113.3		335.	20.
0917127				55		14 • R		45.		-5.	15.4	118.0		164	20.		114.3		269.	25.
0917187					10.	14.4		55.	47.	5.	14.9	120.8	35.	35.	o.				139.	20.
0918007				13.	٥.	14.5		50.	53.	F	15.0		35.	41.	0.		117.6	60.	149.	30.
0918067	13.8 123.9 5n 13.6 123.9 5n			13.	5.	14.7		40.	46.	۰.	15.3	118.6	żυ.	56.	10.		115.5		190	304
0918127	13.6 123.7 5n 13.6 122.7 5n			30.	5.	14.R		35,	30∙	n.	15.4	117.6	٥Ü.	123.	10.		114.4		249.	25.
091818Z				24.	5.	14.0		>5.	40.	20.	15.0		5U.	159.	25.		115.5		217.	25
0919002	13.7 172.1 49			5.	5.	14.2		>5.	70.	5u•	15.1		50.	173.	30.		115.2		225.	25
091906Z	14.3 120.6 35			8.	ũ.	14.4		50.		] 0 •	15.3		55.	505	25.	14.7	114.2		259.	25.
0919122	14.8 120.2 35			30.	5.	14.6		45.		۳.	15.9			227.	20.	17.8	113.6		225.	30.
0919182	15.5 119.8 35		35.	33. 67.	0.	15.5		<b>+0.</b>		5.	14.8		45.		5.		111.9		297.	20.
092000Z	16.1 119.1 40				Ů.	15.7		<b>+0</b> .		10.	16.6		45.		5.		109.4	55.	371.	20.
0920062	17.1 118.8 4n				-5. 10.	17.4		35.		5.	18.3		40.	lRô.	0.	10.1	111.6	45.	212.	. n.
0920127	17.6 118.6 35				-5.	18.0				-1r.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0920182	17.9 118.3 3n			29.	0.	0.0	0.0	0.	-0.	0.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0-	-0.	0.
092100Z	18.4 118.1 30		30.	6.	0.		0.6	0.	-0-		0.0	0+0	0.	-0.	0.	0.0	0.0	0.	-0-	ο.
0921u6Z	19.0 117.9 35				-5.	20.5		25.		-15.	0.0	0+0	Ű•	-0.	0.	B + 0	0.0	0.	÷0•	0.
0921122	19.5 117.5 40		30.		10.	0.0	0.0	25.		•1n•	n • 0	0+0	0.	-0.	0.	n • 0	0.0	0.	-0-	11 .
092118Z	20.1 116.9 40				10	0.0	0.0	٥.	-0.	n.	0.0	0+0	0.	-0.	0.	0 • 11	0.0	0.	-0.	0 .
0922U0Z	20.5 116.4 40				10.	55.0		25.	41.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
092206Z	20.8 116.n 35				-5.	22.5		0.		9]5. 940.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0922122	20.9 115.6 35					22.5		35.	3/.		0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0922182	21.2 115.0 35		35	11		22.1		35.	12.	٥.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
092300Z	21.5 114.4 40		35		-5.		12.3	25.	35.	5.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	0.
0923062	21.8 114.0 40			5.	5.	0.0	0.0	0.	-0.	۸.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0923127	22.0 113.0 35		35	44.	ű.	0.0	0.0	0.	-0.	0.	0.0		o.	-0.	0.	0.0	0.0	0.	-0.	0.
092318Z	22.3 113.5 30		30	6.	ŏ.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-O·	0.
0924002	22.5 112.9 25	22.5 113.0		6.	ō.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0.	0.
			-	. •	-		•	•			17 4 17		٠.	-0.	۰.	0.0	0.0	0.	-0.	0.

	AI L	FORECAS	TS	
AVG FORFCAST POSIT FRYOR AVG RIGHT ANGLE ERROR AVG INTENSITY MAGNITUDE ERROR AVG INTENSITY BIAS NUMBER OF FORECASIS	WKNG 23. 16. 5. -4. 35	24-HR 93. 66. 12. -5. 27	48-HR 195. 152. 13. 4. 19	72-18 279. 227. 21. 21.
		719	-	

# TROPICAL STORM NANCY

0917182 16.8 112.2 2n 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	s r
0917127 16.0 113.0 20 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	
0917182 16.8 112.2 2n 0.0 0.0 0.0 00. U. 0.0 0.0 0.0 00. 0. 0.0 0.0 00. 0. 0.0 0.0	WIND
0918067 17.3 111.5 25 0.0 0.0 0.0 00. 0. 0.0 0.0 00. 0. 0.0 0.0	0.
0918062 17,7 111.5 25 0.0 0.0 0.0 00. 0. 0.0 0.0 00. 0. 0.0 0.0	Ö.
0918127 18:1 111.5 25 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	0.
091818Z 18.6 111.7 30 0.0 0.0 0. 0. 0. 0.0 0.0 0. 0.0 0. 0.0 0. 0.	0.
0919007 18.6 111.6 30 0.0 0.0 00. 0. 0.0 0.0 00. 0. 0.0 0.0	n -
0919062 18.6 111.2 3c 18.6 111.7 30. 285. 20.6 112.4 45. 20/* 10. 22.2 110.6 45. 30. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	0.
0010127 10 114 37 10-0 114 30 28 -5 20-4 117-4 45 20-6 10 22-2 110-6 35 304 0 0 0 0 0	0.
0011107 107 1007 35 15.8 110.8 45. 13. 10. 19.3 110.4 45. 90. 10. 20.3 108.7 50. 173 15 20.6 105.0 25 0.7	0.
000007 107 1003 45 19.3 110.4 50. 36. 5. 20.1 109.2 45. 132. 10. 20.6 107.1 50. 103. 20. 0.0 0.0	15.
22007 18-7 109-7 35 18-7 109-3 40. 23. 5. 18-5 106-4 30 1345. 18-2 104-3 2- 101	0.
072002 18.4 109.4 35 18.8 109.2 40. 26. 5. 19.3 106.4 35 132. 0. 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	0.
0920122 18-2 109-3 35 18-4 108-9 35, 26, 0, 18-3 104 g 40 74 F	ο.
0720102 1/-9 1/9-0 35 19-3 108-1 35, 56, 0, 18-2 105-6 25 12h, E	n.
092100Z 17.7 198.7 35 17.5 108.1 35 36 0 15 0 104.2 20 105 31	0.
0921062 17.6 108.3 35 37.4 107.8 35 23 0 00 00 00 100 100 100 00 00 00 00 00 0	0.
0921127 17-4 107-0 35 18-0 109-0 35 36 0 17-10-0 "" "" "" "" " " " " " " " " " " " "	0.
092118Z 17-3 107-6 30 17-7 107-2 30 23 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.
0922007 17 2 107 2 20 17 2 107 2 27 47 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	0.
0922067 17 1 107 0 20 17 2 10 0 13 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.
0922127 16 0 16 7 30 16 7 10 16 16 40 0 40 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.
0922127 16.9 106.7 20 16.5 106.5 20, 26, 0, 0,0 0,0 0, -0, 0, 0,0 0, 0,0 0, -0, 0, 0,0 0,0	0.

	AI L	FORECAS	TS	
AVG FORECAST PUSIT FRANK AVG RIGHT ANGLE ERRON AVG INTENSITY MAGNITHUS ERROR AVG INTENSITY BIAS NUMBER OF FORECASTS	28. 28. 19. 3. 1.	74-4R 116. 86. 7. 1.	48-HR 215. 185. 10. 3. 4	72-4R 227. 219. 15. 15.

#### TYPEOON OWEN

HEST TH	MEST THACK WARNING FRANCES				ny⊪H FC	HECAS CRHS		48	40µ⊀ F:	RFCAS			15 40	U⊰ Fn	orcas	т
UD CO- CUE CROTT CO	Trace no	.1 N.5	OST WIND	POSTT	w L un	1 40		POSIT	w L vD	051		204	I †	CVIW	957	# T NI)
TIECH PHYACKOM			58. 0.	13.5 135.0		123.	15.	14.3 131.			15.	14.9	173.6	70.	343.	0.
	20 13.0 138.			13.4 134.9		77.	15.	16.6 131		233.	5.	15.9			747.	-5.
	25 12.9 138		25. 0.	12.9 134.0		141.	1.4	13.H 130.		337.		15.5			740.	
	25 12.5 137.		33. 0.	12.7 132.7		550.		17.6 129.		474		15.3			479.	
	25 12.3 136.		54. 0.			550.		12.7 131.		497.		13.2			545.	
	25 12.3 136		21. 0.	12.4 134.5		313.		12.4 130.		503.		13.3			621.	
	3n 12.3 136.		66. 0.	12.5 133.6		309.		14.7 131.		445.		15.4			5110	
	35 13.3 136.		36. 10.			333.		15.4 129.		431.		16.3			516+	
	45 13.7 135		79. 0.	14.6 133.1			-10.	24.H 131.		149.		24.4			254.	
	45 16.4 135		19. 0.	21.0 132.4			-10.	26.0 131.		189.		24.4			298.	
	55 17.9 134		13. 0.	22.1 131.5		179.		27.9 130.		250.		30.4			247.	
	6n 19.2 133.		16. 0.			184.		29.7 130.		263.		31.0			114.	
	60 20.7 132		38. 0.	25.4 130.7		124.		26.7 125.		239.	-5.	24.6			242.	
	70 20.9 130.		8. 0.	23.8 127.0				24.2 125.		214	0.	20.3			190.	-5.
	75 21.7 130		29. 0.	24.1 127.1		120.		27.1 126.		183.	5.	30.7			192.	0.
	An 21.9 129:		23. 0.	24.7 127.0		130-					10.	30.3			150.	-5.
0925187 22.6 129.5 1			2810.	24.9 127.4			-5.	27.5 127.		161. 47.	5.	30.3			251.	-5.
092600Z 23.1 129.1 1	1n 23.3 129.		1315.	25.5 128.7		60.	10.	27.H 130.							359.	
092606Z 23.5 129.2 1			1610.	26.0 12H.		71+	15.	28.7 131.		108.	5.	31.2				-10-
0926122 23.8 129.3 1	10 24.0 129	1 100.	1610.	26.0 129.0		43.	Su.	2A.4 130.		64.	10.	30.9			240.	
0926182 24.4 129.4 1	05 24.4 129	5 105.	5. 0.	29.0 130.5		158.		29.H 132.		135.	٥.	31.1			339.	
0927002 24.9 129.6 1	00 24.8 129	4 100.	12. 0.	76.4 124.6			l n •	20.6 131·		99.		31.6			320.	
0927062 25.5 129.7	95 25.3 129	7 95.	12. 0.	27.3 130.4		35+.	ln.	20.2 132.		142.		32.3			247.	
	90 25.9 129	90.	8. 0.	78.3 131.1		Bu.	10.	30.4 133+		212.		37.3			176.	
9927182 26.5 129.8	85 26.6 129	7 85.	в. О.	29.0 130.5	75.	87.	0.	31.5 133.		) H 9.			1.48.5		133.	0.
	HS 27-1 129	9 65.	8. 0.	29.5 130.7		94.	٥.	32.2 133.		144.		35.0			297.	5.
	80 27.5 129	я НО.	12. 0.	30.7 [31.			∙0•	72.H 135.		103.		0.0	0.0	0.	-0-	0.
	75 27.7 129	A 75.	6. 0.	29.5 13n.4	1 70.		-5.	72.3 132.		189.	5.	0.0	0.0	0.	-0.	0.
	75 27.7 129		5. 0.	28.5 124.9		86.	-5.	31.2 131.		454.	15.	0.0	0.0	0.	-0.	0.
	75 28.0 129		8. 0.	29.8  30.4	70.		D .	72.4 132.		611.	25.	u • 0	0.0	٥.	÷0•	0.
	75 28.7 129		20. 0.	32.0 131.0		84.	•25.	n.n 0.		-0.	0.	n • 0	0.0	0.	-0.	٥.
	75 29.1 130		5. 0.	12.3 131.		191.	A.	0.0 0.		-0.	0.	n • D	0.0	0.	-0.	0.
	75 29.7 130		6. 0.	72.4 137.	50.	331•	5.	n.o 0.		-0.	0.	n • 0	0.0	0.	-0.	٥.
	70 31.0 131		12. 0.	35.0 135.	10.	417.	-5.	n.0 0.		-0.	0.	n • 0	0.0	0.	-0.	0.
	65 32.0 132		39. 5.	0.0 0.0	. 0.	-0-	n .	n_0 0-		-0.	٥.	u • 0	0.0	0.	-0-	0.
0930122 34.1 135.1	55 33.9 134		35. 15.	0 n 0 a	0.	- U +	0.	n.a 0.		-0.	0.	0.0	0.0	0.	-0•	0.
	45 35.4 137		72. 5.	0.0 0.0	0.	- U +	n.	n_n 0 •	0 0.	-0.	0.	0.0	0.0	0.	-0+	0.
1001002 39.8 141.9	35 39.0 141		55. 0.	0.0 0.0	0.	-0.	n.	n_0 0.	0 0.	-0.	0.	0.0	0.0	0+	-0+	0.
###### 37.6 141.4	33 3740 141															

	۵ı'L	FORECAS	TS	
AVG FORECAST POSIT FRANK AVG RIGHT ANGLE EROOK AVG INTENSITY MAGGITUDE ERROP AVG INTENSITY BIAS NUMBER OF FORECASTS	#RNG 25. 15. 2. -0. 37	24-HR 146. 78. 10. -3. 33	48-HR 250. 158. 15. -9. 29	72-4R 327. 256. 18. -18. 25

## TROPICAL STORM PAMELA

	REST	TRACK			MARVI				24 HC	NK F	HECAS			48 H	n)R Fn	PECAS			₹2 <b>∺</b> 3	uR Fn	QFC49	т
							₹り₹5		_								JIND	P05	14	CFIW	nST	a T NU
M0/04/HR	POSIT	WIND	POS	tΤ	⊌IN∋	DST	CNIW	PAS		~1 40	• -	● I wD	POSI		AIND			-		0.	-0.	0.
092300Z	18.0 150.0	1 15	0.0	0.0	0.	-0-	0.	0.0	0.40	0.	-0+	0.	0.0	0.0	0.	-0.	٥.	0.0	0.0			0.
0923067	18.2 148.	15	0.0	0.0	٥.	-0.	٥.	0.0	0.0	0.	-0.	n •	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	
0923127	18.3 147.4		0.0	0.0	0.	-0-	0.	0.0	0.0	0.	<b>-</b> 0 +	ο.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0923182	18.5 146.9		0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-U+	n.	n.n	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
092400Z	18.6 145.0		0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	n.	n.U	0 • 0	0.	-0.	0.	0.0	0.0	٥.	-0.	0.
092406Z	18.7 145.4		0.0	0.0	o.	-0.	o.	0.0	0.0	0.	-0.	n.	0.0	$0 \cdot 0$	Đ.	-0.	0.	n.0	0.0	0.	~O =	0.
0924122	18.8 144.0		0.0	0.0	ŏ.	-0.	ō.	0.0	0.0	0.	-0.	ο.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
			0.0	0.0	ŭ.	-0.	ö.	0.0	0.0	Ö.	-0.	0.	0.0	0.0	0.	-0.	0.	n • 0	0.0	0.	<b>+0</b> •	D.
0924182	19.0 144.			0.0		-0.	0.	0.0	0.0	ō.	-0-	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-Û-	n.
092500Z	19.2 143.		0.0	-	U.	-		0.0	0.0	ŏ.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	Π.
<b>09</b> 2506Z	19.4 143.		0.0	0.0	٠.	-0.	٠.		_	٠.	201.	125	0.0	0.0	ů.	-0.	ō.	0.0	0.0	0.	÷0 •	n.
092512Z	19.7 142.			142.0		13.	-5.	21.0		45.		25.	0.0	0.0	0.	-0.	o.	0.0	0.0	٥.	-0.	0.
0925182	20.3 140.	35		141+1	35.	39.	٥.			<b>+5</b> .		_		0.0	0.	-0.	0.	0.0	0.0	ō.	-0.	0.
0926002	20.8 139.	4 35		139.R		25.	υ.	0.0	0.0	0.	-U•	0.	n • I)				0.	0.0	0.0	Ď.	-0.	ñ.
0926062	22.0 137.	<b>9</b> 3n		137.R		25.	0.	0.0	0.0.		-U+	(i •	0.0	0.0	0.	-D.		0.0	0.0	0.	-0.	0.
8926127	24.1 137.	A 25	23.6	136.5	30.	67.	5.	0.0	0.0	0.	-U+	0.	0.0	0+0	0.	-0.	0.			_		0.
0926182	26.0 136.	a Su	26.0	136.8		0.	5.	0.0	0.0	٥.	-0.	۰.	0.0	0 + 0	0.	-0.	0.	n . 0	0.0	0.	-0.	0.

	AI L	FORECAS	TS	
	WHNG	24-4R	48-H3	72-48
AVG FORECAST POSIT FRHOR	28.	254.	0.	n.
AVG HIGHT ANGLE ERONR	22.	15.	0.	ο.
AVG INTENSITY MAGNITUDE ERRUR	3.	25.	0.	n,
AVG INTENSITY BIAS	1.	0.	0.	n.
NUMBER OF FORECASTS	4	5	0	3
		Α.		

#### TROPICAL STORM ROGER

	HEST THAC	WARV.		57 HUH	IN FUNECASI	48 HOUR FORFCAST	FZ HOUR FNAFCAST
			ERRORS		EHHJAS	FRADAS	
M0/J4/H		FOSTT #INT	DST WING	Pasit w	dat eine	POSIT WIND OST WINE	CHATH TEG DRIN 11209 C
1005001	11.7 142.7 20	0.0 0.0 0.	-0- 0-	0.0	0		
1002062	12.0 142.1 20	0.0 0.0 0.	-0. 0.	0.n n.n			
1002127	12.4 141.4 20	0.0 0.0 0.	-0. 0.		0u. n.	0.0 0.0 00. 0.	
1002187	13.2 140.8 25				0u. n.	n.n 0.0 00. 0.	. 0.0 0.0 00. 0.
1003007	14.2 140.2 30		-0. 0.	6-n n-n	00	0.0 0.0 00. 0.	0.0 0.0 00. 0.
1003067		0.0 O.n U.	-n. u.	0.n	0, -u. n.	n.u 0.0 u0. 0.	
	16.1 139.4 3n	15.7 139.A 25.	275.	18.4 137.3	35. 201	20.3 136+0 45+ 45, 0	
1003122	18.0 138.R 30	16.5 139.1 25.	85. +>.	20.2 137.1	35, 1705.	23.5 136.4 45. 129. 0.	
1003187	19.4 137.6 3n	19.5 138.1 30.	29. 0.	74.P 134.0	35. 265. *]n.	29.0 137.4 45. 387. 0.	
1004007	20.5 176.7 35	21.0 136.3 30.	245.		35. 360. Th.		
1004062	21.2 135.3 40	71.7 135.2 35.	305.	26.4 134.4	50. 379. 5.		
100+12/	21.5 134.4 40	21.5 134.7 40.	17. 0.				
1004187	21.0 133.5 45	22.5 133.6 45			50, 199, 5,	27.0 133.0 55. 123. 10.	
1005007					55. 254. ln.	79.1 134.5 45. AJ. 5.	0.0 0.0 0
100506/	19.9 1 14.2 45	20.2 133.0 40.	255.	23.4   34.7	50. 24. K.	29.0 137.8 40. 180. 5.	
	20.3 135.2 45	20.2 134.7 40.	295.	23.4 135.7	50. lls. 5.	79.3 137.9 40. 324. 10.	
1005127	21.5 135.5 45	21.4 135.1 40.	235.	27.2 134.1	45. 47. 0.	0.0 0.0 00. 0	
1005182	22.8 135.3 45	22.4 135.R 4U.	35. <b>-</b> 5.	26.7 138.0	40. 174. n.		
1006002	23.8 134.7 45	23.9 134.7 40	65.				
1006062	25.2 134.4 45	25.1 134.7 40.	175.			0.0 0.0 00. 0.	
1006122	26.8 135.3 45				35, 205, 5,	n.0 0+0 0. =0. 0.	n.D 0.0 DO. D.
1006182		26.4 135.3 40.	245.	0.0 0.0	0u. n.	n.(I U+O O. =O. O.	n.D 0.0 D0. G.
	29.1 136.2 40	29.4 136.2 40.	42. 0.	<b>0.</b> 0 0.0	0u- n.	n. 11 0.0 00. 0.	
1007002	32.0 137.4 35	31.9 137.4 35.	16. 0.	0.0 0.0	0u. n.	n.n 0.0 00. 0.	
1007062	34.4 140.1 3n	0.0 0.0 0.	-0. 0.	0.0 0.0	0u. n.	n.0 0.0 0D. 0.	

	AI L	FORECAS	TS.	
	MKNG	24-48	48-H3	72-4R
AVG FORFCAST POSIT FRENR	32.	195.	251.	3n3.
AVG AIGHT ANGLE ERONP	19.	93.	109.	174.
AVG INTENSITY MAGNITHUE ERROR	3.	5.	7.	11.
AVG INTENSITY BIAS	-3.	0.	-1.	-1.
NUMBER OF FORECASTS	15	13	9	4
		2	5	2.

## TYPHOON SARAII

	HEST THACK		MARUTNG	R075	5•	HD-IH F	UKÉLA EKK		41	в но	H≺ Fo	RFCAN FRROM			F2 40	uH Fn	# C V c	<b>:</b> T
40/JA/H-	DOLLT	PASTE	ZIN⊃ DST		PosiT	w1 w		4 [NI)	POSIT			051		P051	1 1	CVIN	oST	w į Ni)
0930127	POSIT WIND	0.0 0.0			0.0 0.		-0.	Α.		0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0930187	14.6 119.4 15	0.0 0.7				n 0.		ο.		0.0	Ű.	-0.	0.	n.0	0.0	D .	-0-	n.
1001007	14.5 119.4 15	0.0 0.7				, n D.		۸.		0.0	0.	-0.	Ö.	0.0	0.0	0.	-0.	0.
1001062	14.5 120.2 15	U.O 0.0				n 0.		Λ.		0.0	0.	-0.	0.	n • 0	0.0	0.	-0.	0.
1001127	14.5 120.6 15	0.0 0.0				n 0,		0.		0.0	Ü.	-0.	0.	n • 0	0.0	0.	-0.	0.
1001187	14.5 120.8 IS	0.0 0.0				0 0.		n.		0.0	0.	-0.	0.	0.0	0.0	0.	-0.	₽.
1002002	14.7 121.0 15	0.0 0.1				6 D.		0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1005062	14.8 121.1 15	0.0 0.0				o Ó.	-0-	n.	0.0	0.0	0.	-0.	0.	11 - 0	0.0	0.	-0.	0.
1002122	14.9 121.2 15	0.0 0.0				n 0.		0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-n.	0.
1002187	15.2 121.2 15	0.0 0.1				0.		0.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0-	0.
1003002	15.2 120.4 15	0.0 0.0				o 0,	-4.	0.	0.0	0.0	ű.	-0.	0.	0.0	0.0	0.	-0.	O.
1003067	15.0 120.4 15	0.0 0.0			0.0	n 6,	-0.	0.	0.0	0.0	U.	-0.	0.	0.0	0.0	0.	-0·	0.
1003122	14.8 120.3 15	0.0 0.0			0.n n	.0 0	0.	۸.	0.0	0.0	u.	-0.	0.	0.0	0.0	0.	-0-	0.
1003182	14.6 120.0 20	0.0 0.0			0.0 0	n B	0-	0.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	0.
1004002	14.4 119.7 20	0.0 0.0			0.0 0	.n e.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-O.	0.
1004062	14.2 119.5 30	0.0 0.0			0.n n	. 0	-0.	n.	0.0	0.0	Ü.	-0.	0.	0.0	0.0	٥.	-0.	0.
100412Z	13.8 119.1 30	14.0 119.			13.5 118	2 35.	88.	-5.	13.0 11	0 - 1	45.	555.	0.	12.5			346.	
1004187	13.5 118.8 35	13.9 119.			13.5 117	7 50	121.	10.	12.9 11	5.8		220.	0.	17.4			365.	
100-007	13.0 118.8 40	13.7 118.0			13.2 116	9 50.	160.	}n.	12.7 11	4 • 6	50.	282.		12.2			4 76 4	
1005062	12.7 119.0 40	12.5   18.			12.5 11R		. 7v.	n.	11.5 11		40.	79.		10.7			140.	
100512Z	12.5 119.3 40	12.5 119.		0.	12.0 118	. 9 40.			11.7 11		40.		-35.	10.6			159	
100518Z	12.5 119.5 40	12.1 119.0		. 0.	11.n 118			•1n•	10.3 11			136.			116.3		141.	
1006002	12.5 119.7 40	12.3 119.0		. 0.	12.1 11#	.7 40.	. 41.	45v*	11.5 11		35.	71.		1 n • B		30+		-55.
1006062	12.4 119.7 40	12.4 119.		. 0.	12.4 120	.я 35.	. 950	<b>440</b> .	12.3 12			160.		12.4			277.	
1006122	12.3 119.6 45	12.4 120.		-10.	12.5 120			<b>#40</b> *	12.5 12			179.		0.0	0.0	0.	-0-	0.
1000182	12.2 119.5 50	12.4 119.		-15.	12.4 120			445.	12.5 12			167.		0.0	0.0	0.	-0-	0.
100700Z	12.2 119.4 60	12.2 119.	45. n.	-15.	12.2 119	.4 35		*40.		0.0	.0•	-0.	۰.	0.0	0.0	0.	-0-	0.
1007062	12.1 119.2 75	12.2 119.		-10.	11.9 118			*1c.	11.5 11		50+		-40.	11.3			118.	
100712Z	11.4 119.2 75	12.1 119.		10.	11.8 11H			415.	11.6 11		50.		-40.	11.2		40.	93.	
100718Z	11.6 119.2 75	12.n 119.		, -10.	11.9 119			.sυ.	11.2 11		≥0•		-45.	10.7		40.		-60-
1008002	11.3 119.2 75	11.3 119.	1 65. 5.	10.	11.2 114			430.	11.1 11		50.		-60.	11.1		40.		-60.
1008062	11.0 119.2 75	11.1 119.		-10.	10.4 11A			•30.	10.7 11		25.		-55.	10.8		50.		-40• -35•
1008122	10.8 119.1 75	10.8 119.		-10.	10.1 11R			<b>430</b>	10.1 11		55.		-45.					-25.
100R1RS	11.0 118.A 75	10.6 119.		-10.	10.2 11R			-3n.	10.0 11			117.	-35.	1n.3 11.6			127.	
100+00Z	11.1 118.4 45	10.6 118+		-20.	10.4 116			<b>40.</b>	10.H 11		65. 80.		-10.	11.8		80.	70.	10.
1009062	11.3 117.8 9n	11.3 117.			11.4 116			425.	11.6 11		80.	29.	-5.	17.8		80.	39.	15.
100315Z	11.3 117.4 90	11.5 117+		. 0.	11.0 115			*15.	12.2 11		80.	92.	5.	13.0			111.	15.
1009182	11.4 117.1 95	11.7 116.			12.3 115		104	*15.	11.5 11			176.	5.	11.5			741.	20.
1010002	11.5 116.7 110	11.4 116.		-50-	11.4 113				12.0 11		90.	93.	50.	12.1			126.	30.
1010062	11.6 116.3 110	11.6 116.			11.0 114				12.0 11			100.	25.	12.1			126+	20.
1010122	11.7 116.0 100	11.6 115.			12.2 113				12.5 11		90.	RL.	25.	12.6			100.	15.
1010182	11.8 115.4 100	11.9 115.		-10.	12.5 114				13.0 11		70.	25.	10.	13.3		60.	41.	5.
1011002	11.9 115.5 100	12.0 115.			12.4 113				12.6 11		70.	R5.	10.	12.6		60.	76.	10.
1011062		12.0 114.			12.3 111				12.4 10			126.	0.		107.7	20.	123.	-30.
101112Z 101118Z	12.2 114.8 85 12.4 114.5 75	12.1 114.			13.n 111				13.2 10			105.	790.	0.0	0.0	0.	-0.	0 -
1012002	12.4 114.5 75	12.4 114.			12.5 112				12.9 11		50.	39.	-5.	13.2	109.3	40.	35.	20.
1012062	12.9 113.9 70	13.0 113.			13.5 112				13.8 11		50.	42.	0.	0.0	0.0	0.	-0-	0.
1012127	13.1 113.7 65	13.3 113.			14.0 111		•		14.6 10		65.	A0.	15.	0.0	0.0	0.	-0.	0.
1012187	13.2 112.9 65	13.5 112.			14.4 110				14.7 10		30.	101.	-5.	0.0	0.0	0.	-0+	0.
1013002	13.3 112.6 60	13.3 112.			13.2 110				13.1 10		30.	29.	10.	0.0	0.0	0.	-0.	0.
1013062	13.4 112.1 60	13.2 112.			13.1 110		•		0.0	0+0	0.	-0.	Ů.	0.0	0.0	0.	-0-	0.
1013122	13.4 111.7 60	13.5 111.			13.0 109				0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1013182	13.4 111.1 60	18.5 111.			13.3 10F				0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	<b>-0</b> +	
101400Z	13.4 110.6 55	13.5 110.			13.4 106			10.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0+	0.
1014067	13.3 110.0 50	13.4 110.				.0 0		n.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0+	0.
1014127	13.3 109.6 50	13.3 109.			0.0	.0 0			0.0	0 • 0	0.	-0.	0.	0.0	0.0	0 •	-0+	0.
1014182	13.2 119.1 35	13.3 109.				.0 0	0	. 0.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	
101500Z	13.1 108.7 20	13.1 108.		. 0.	0.0	.0 0	0	٠.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.

	AI'L	FORECAS	15	
	WHNG	24-4R	4B-H3	72-4R
AVG FORFCAST POSIT FRANK	26.	61.	110.	143.
AVG RIGHT ANGLE ERROR	16.	40.	85.	107.
AVG INTENSITY MAGNITUDE ERROR	6.	16.	47.	33.
AVG INTENSITY REAS	-2.	-9.	5.	-21.
NUMBER OF FORECASTS	43	39	34	27
		26	21	24

#### SUPER TYPHOON TIP

	HEST TRACK	JARVING	24 HOUR FO		48 HOUR FORECAST	12 HOUR FARECAST
HO/DA/HS	POSIT WIND PO	ERRORS STT #IND DST WIND		EHHJAS	F 4 7 7 7 7 8	
100400Z	6.3 154.1 20 0.0		Postt Wind	DSI #IND	POSIT WIND DST	
1004062	6.3 153.0 25 0.0		0.n n.n 0.	-u. n.	0.0 0.0 00.	0. 0.0 0.0 00. 0.
1004122	5.7 153.3 25 0.0		0.0 0.0 0.	-u. n.	0.0 0.0 00.	0. 0.0 0.0 00. 0.
100+187	5.4 153.9 25 0.0	0+n U. +0. O.	0.0 0.0 0.	-U- n.	0.0 0.0 00. 0.0 0.0 00.	0. 0.0 0.0 00. 0. 0. 0.0 0.0 00. 0.
1005002		154.5 25. 0. 0.	6.4 152.4 30.	685.		
1005062		155.2 25. 6. 0.	7.0 157.7 30.	405.		-5. 4.3 [47.] 45. 237. 5. -5. 10.4 [48.0 45. 2]9. 5.
1005122 1005182		155.3 25. 485.	7.9 157.7 J5.	45. n.	0.1 150.9 45. 161.	5. 10.5 1-8.0 50. 158. 5.
1005102		155.2 25. 995.	8.1 153.0 35.	274.	0.4 150.0 45. 199.	5. 10.5 1-7.0 50. 150. 0.
1006062		153.1 35. 12. 0. 152.4 35. 43. 0.	8.7 150.2 45.		9.H 147+6 55. 2R1.	15. 11.0 145.1 65. 173. 15.
100612Z		152.4 35. 43. 0.	9.1 150.0 45.	201- 5-		15. 11.3 144.4 65. 117. 10.
1006187		151-9 40. 43. 0.	9.4 149.4 50.			10. 11.8 144.9 65. 49. 5.
100/007		152.3 40. 18. 0.	9.3 150.6 50.			10. 12.0 144.4 70. 795. 10. 12.0 145.0 70. 16010.
100706Z		152.5 40. 19. 0.	8.7 151.5 45.		9.9 149.4 55. 269	10. 17.0 145.0 70. 160[0. 0. 11.5 146.6 70. 310[5.
1007122		151.7 40. 21. U.	8.2 149.6 45.			·5. 11.4 144.5 70. 26120.
1007182 1008007		151.5 40. 35. 0.	7.5 149.3 50.		9.4 147.2 60. 305	15. 11.0 144.4 75. 24540.
1008067		152.1 40. 61. 0.	7.7 151.3 65. 3		9.0 149.3 75. 468.	5. 10.5 146.4 75. 45955.
1008122		151.5 45. 19. 5. 150.3 45. 19. 0.	11.4 147.2 60.		14.0 142.6 70. 60	15. 14.6 138.0 75. 14945.
1008187		149.5 50. 18. 0.	12.2 146.0 60. 1	105. n. 120. "1n.	14.5 141.6 70. 56	
1009002		147-8 50. 6. 0.		77 -15	15.7 141-2 70. 119 19.0 137-2 75. 315	
100906Z		146.0 55. 21. 0.		04. 420.	IR.5 136+6 BO. 288	
1009127		344.7 60. 0. 0.		41. 425.	14.5 133-7 80. 320.	90. 21.6 JJ1.2 85. 45580. 90. 15.2 Id9.5 85. 44890.
100918Z		143.2 65. 1310.		1340.	14.2 133.3 85. 335	
1010007		142.4 80. 8. 0.		76. 430.	14.6 134.0 115. 268	5. 15.7 1/9.3 130. 40015.
1010062 1010122		141.6 85. 25. 0. 140.9 95. 12. 5.	13.0 137.3 105. 1	27. 435.	14.7 132.9 120. 303	5. 15.8 128.6 130. All. 0.
1010182			14.7 134.1 110.		15.1 134-1 125. 208	0. 16.2 131.3 130. 231. 5.
101100Z		140-0 100. 3015. 139-4 100. 930.	15.5 137.0 115. 1 15.2 136.3 145. 1		16.4 133.5 125. 196	
1011062		139.2 130. 1310.	15.2 134.4 150. 1		16.3 132.8 150. 196. 16.1 133.2 155. 148.	5. 17.4 128.8 160. 208. 35.
101112Z		139.2 135. 125.	16-1 137-6 150.			5. 17.0 130.0 160. 200. 45. 10. 18.8 134.7 160. 154. 35.
1011182	15.7 138.4 15c 15.8	138-9 135. 615.	17.2 136.H 150.			10. 18.8 146.7 160. 154. 35. 30. 20.3 133.6 160. 191. 35.
101200Z		138.3 135. 625.	18.6 136.1 140. i			0. 22.1 193.4 130. 277. 5.
101206Z 101212Z		137.6 145. 820.	19.4 134.H 140. 1	69. ln.		0. 26.9 134.8 130. 563. 5.
1012187		137-2 155. 1210.	18.9 134.8 140. 1		21.3 133.3 130. 243.	5. 24.0 133.0 130. 368. 5.
1013007		136.7 155. 32. 0. 136.4 140. 175.	18.7 135.0 135. 1		20.7 133.6 125. 211.	0. 23.0 132.8 120. 306. 0.
1013062		136+4 140. 175. 136+4 140. 54. 10.	16.9 137.5 130. 2 16.8 137.5 130. 2			5. 20.9 134.9 110. 33710.
101312Z		135.7 135. 0. 10.				5. 20.9 134.9 110. 341. 0.
101318Z		134.9 130. 8. 5.			17.3 130.0 120. 78 17.9 129.3 120. 61.	5. 18.0 127.1 110. 172. 0. 0. 19.0 126.6 110. 168. 5.
101400Z		134.2 120. 175.				0. 19.0 126.6 110. 148. 5. 5. 19.1 126.2 100. 179. 0.
1014062		133.3 120. 135.	18.n 13n.4 100.	26. •25.		0. 20.5 124.3 80. 23015.
101412Z 101418Z		132.5 120. 135.		8u. •25.	19.4 125.5 100. 715!	0. 19.5 122.0 90. 3455.
1015002		131.5 120. 185. 131.0 120. 95.		87• <b>=</b> 2n•	19.5 124.5 100. 272.	5. 21.0 121.0 90. 406. n.
101506Z		131 • 0 120	19.3 128.3 100. 20.0 126.9 100. 1	45. •2n. 12. •1n.	20.5 125.7 100. 147.	0. 22.0 123.0 100. 321. 10.
101512Z	18.6 129.8 125 18.7	129-9 135. 610.			21.5 124.5 100. 196. 21.3 124.6 100. 204.	5. 24.0 123.0 95. 777. 10. 5. 23.5 123.0 95. 401. 20.
1015182		129.0 110. 2910.	20.7 124.5 100. 1		21.H 124.0 95. 238	E
101600Z	19.4 129.1 12n 19.5	129-4 110. 1910.			23.5 126+4 95. 122.	5. 24.3 123.0 90. 540. 15. 5. 25.4 125.7 90. 638. 20.
1016067		129.3 110. 37. 0.	21.n  28.5 100.			0. 25.4 126.4 90. R47. 30.
101612Z 101618Z		128-7 105. 85.			25.4 127.0 90. 244. ]	5. 24.1 1/8.4 80.1145. 30.
101700Z		128-5 100. 195. 128-2 95. 65.				0. 28.6 128.9 80.1197. 30.
1017062	21.5 128.1 1nn 21.5 22.4 127.9 95 22.0					5. 0.0 0.0 00. 0.
1017122	23.0 127.8 95 23.2		24.6 (27.0 85. 1 26.0 127.3 75. 2			0. 0.0 0.0 0D. D.
101718Z	24.0 127.4 9n 23.8		26.4 127.4 75. 2			5. 0.0 0.0 00. 0.
1018002	25.1 127.8 9n 25.1		29.2 129.4 70. 3		0.0 0.0 00.	5. 0.0 0.0 00. 0. 0. 0.0 0.0 00. 0.
101806Z	26.5 128.4 85 26.4	128.4 80. 125.	31.7 131.4 55. 4		n.a 0.0 00.	0.
1018122	28.4 130.1 75 28.1		34.4 137.8 50. 5	39. n.	0.0 0.0 00.	0. 0.0 0.0 0 0.
1018182 1019002	30.3 131.6 75 29.9 33.0 134.3 70 32.9			22. n.	0.0 0.0 00.	0. 0.0 0.0 0
1019062	33.0 134.3 7n 32.9 36.2 138.6 6n 35.4			-0. n.	0.0 0.0 00.	0. 11.0 0.0 0
101912Z	41.5 145.2 5n 41.n			-0. n. -0. n.	0.0 0.0 00.	0. 0.0 0.0 00. 0.
1019182	43.1 146.1 Sn 42.8			-u. n.	n.H 0.0 00.	0.
			• • • •	- · · · •	0-0 00.	0. 0.0 0.0 0

	41 L	FORECAS	TS		
AVG FORECAST POSIT FRHOR	WHNG	24-4R	48-44	72-4R	
AVG RIGHT ANGLE ERROR	24.	135.	259.	345.	
ANG INTERCTION MAGNET CARREST	15.	69.	142.	214.	
AVG INTENSITY MAGNITUDE ERROR	5.	10.	17.	22.	
AVG INTENSITY BIAS	-3.	-6.	-5.	-7.	
NUMBER OF FORECASTS	61	55	52	43	
		מכ	2.3	24	

#### SUPER TYPHOON VERA

	AFST THUCK	#ARNING	24 HOUR FORECAST	48 HOUR FORFCAST	FARSTARD RUCH SE
		FARORS	EKKJ4S	FRANAS	
40/J4/H2	POSIT #150	POSIT WIND OST WIND	PASTT WIND UST WIND	POSIT WIND OST WIND	CAIR 150 CAIR 11504
1102007	7.0 145.4 25	6.5 145.4 20. 325.	7.n 142.4 30. 112. "35.	7.6 139.4 40. 41595.	R.3 136.4 50. 67085.
		7.3 145.6 50. 545.	8.7 143.2 70, 248. 0.	0.7 140.1 BD. 54160.	10.9 137.0 85. 72250.
1105065			8.7 141.8 75. 279. 20.	0.4 138.9 85. 57855.	11.2 135.9 95. 71220.
1102127	7.2 143.5 50			8.5 137.6 85. 61850.	0.1 144.4 95. 772. 0.
1105187	7.6 142.2 00	7.3 143.8 25. 955.		10.2 130.3 65. 29850.	12.6 174.8 95. 212. 0.
1103002	8.0 140.0 hs	7.3 141.8 35. 6810.	8.4 134.1 75. 222. 460.		17.6 122.3 75. 7815.
1103062	8.6 139.0 70	9.3 139.0 65. 195.	11.2 131.7 75. 41. 465.	13.2 125.9 75. 5960.	
1103122	9.2 137.1 95	9.2 137.n /0. 625.	11.7 124.4 H5. 30. #55.	14.7 124.5 80. 3335.	
1103187	10.0 115.1 130	9.8 135.2 85. 1345.	12.5 128.5 110. 50. #25.	15.7 123.9 100. 53. 5.	19.8 1/2.4 80. 197. 35.
1104007	10.5 133.0 135	10 6 131 6 125 30 -10	12-6 127-5 130. 950 -5.	15.3 123.9 120. 70. 25.	10.0 1/2.2 110. 01. 70.
		10.0 131 4 125 26 -15	13.0 124.0 130. 245.	15.3 122.7 120. 66. 30.	17.8 122.] 110. 112. 75.
1104062	11.1 131.0 140	10.4 131.4 105. 25. 45.	14.4 121.5 100. 15115.	19.1 121.1 60. 14020.	23.0 128.0 50. 670. 20.
1104157	11.6 129.2 140	11.4 150-1 150- 1310-	15.7 120.7 100. 170. 5.	19.6 121.8 50. 120. 15.	0.0 0.0 U0. U.
1104162	12.0 127.7 135			19.3 121.3 60. 90. 20.	n.0 0.0 UO. U.
110500Z	12.7 125.9 135	12.7 125.4 125. 610.			n.o 0.0 00. n.
1105062	13.4 124.0 135	13.6 124.7 120. 1715.	16.3 12n.4 80. 10y. "In.		0.0 0.0 0
1105122	14.3 124.1 115	14.2 124.1 120. 6. 5.	17.5 122.5 100. 34. 20.	20.7 126.0 70. 508. 40.	
1105182	14.8 123.5 45	15.0 123.1 120. 26. 25.	18.4 123.4 1UQ. 114. 55.	n.0 0.0 00. 0.	
		15.3 122.6 95. 13. 0.	18.7 127.2 60. 78+ 20-	n.a 0.0 00. 0.	0.0 0.0 00. 0.
1106007		16.4 122.5 90. 13. 0.	19.0 123.4 70. 202. 35.	ρ.ο 0•0 U• <b>-</b> 0. U•	n.o 0.0 00. n.
1106062	16.3 122.3 9n	10.7	20.3 122.8 70. 34U. 4n.	n_H 0.0 U0. U.	0.0 0.0 00. 0.
1106122	17.0 122.2 kn	17.1 122.2 90. 5. 10.		0.0 0.0 00. 0.	n.D 0.D 00. 0.
1106182	17.6 121.7 45	17.F 121.9 85. 16. 40.		0.0 0.0 00. 0.	n.0 0.0 00. 0.
1107002	17.8 121.2 40	18.3 121.7 60. 41. 20.	V • 11		0.0 0.0 00. 0.
1107067	18.3 120.2 35	19.2 121.8 35. 105. 0.	0.0 0.0 00. 0.		0.0 0.0 00. 0.
1107122	17.0 117.0 30	19.2 121.A 25. 2575.	0.n n.n 00. n.	n.o 0.0 00. 0.	11.0 U.U U(1.
	1,10 1,114				

	A: L	FRECAS	15	
	WHNG	24-4R	48-H₹	7>
AVG FORFCAST POSTT FHROR	43.	148.	247.	385.
AVE RIGHT ANGLE ERPOR	20.	69.	111.	247.
AVE INTENSITY MAGNITUDE ERROR	12.	28.	39.	74.
AVG INTENSITY BIAS	-3.	-10.	-19.	٦.
NUMBER OF FORECASTS	23	19	15	1,1
		7	9	6

# TROPICAL STORM WAYNE

	HEST TO	RACK			#ARUT				24 40	NIK FO				48 H	)uR Fr	RFCAS			#2 H3	UR Fn	PFC45	ŧτ
							กจร				ERRJ							P04	1.4	GFIW	nSF	CINT
MO/DA/HR	Posit ₩	1 90	POS	ŢΫ́	4IN3	DST	CMIN	Pns	ŢŢ	₩I#D		#I~D	205		GNIE		dIND		0.0		-0.	0.
110700Z	9.9 141.5	15	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	Λ.	0.0	0 • 0	0.	-0.	0.	0.0		0.	-0.	0.
	12.4 141.n	15	0.0	0 <b>•</b> n	0.	-0.	0.	0.0	0.0	0.	-0.	۰.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
	14.4 139.9	15	0.0	0.0	U.	-0.	0.	0.0	0.0	٥.	-0.	٥.	0.0	0 + 0	0.	-0.	0.	0.0	0.0		-0-	0.
	14.B 137.7	20	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	۰.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.		0.
	15.0 135.7	20	0.0	0.0	0.	-0.	U.	0.0	0.0	0.	-0.	0.	0.0	0.0	_0+	-0.	٥.	0.0	0.0		-0+	
1108067	15.4 133.6	25		134.5	25.	52.	0.	18.1	130.3	50.	134.	10.		130.3	25.	235.	5.	24.8	134.9		504.	10.
1108122	16.4 132.1	30	16.3		30.	13.	0.	19.6	127.4	n5.	232.	20.		126.4	65.	221.	15.	24.5	178.4	40.	335.	
	16.0 130.5	30	17.1		30.	66.	0.	19.5	125.R		252.	n.		124 - 1		321.	5.	24.8	125.8	35.	341.	10.
	15.8 129.9	35	16.0		35	53.	0.	18.0	124.1	45.	290.	-5.	22.H	123.5	30.		-10.	0.0	0.0	٥.	-0.	0.
1109067	15.8 129.9	40	15.9		35	57.	-5.	16.3	124.4	25,	272.	<b>-25</b> .	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
	16.2 129.7	45	15.8		45.	24.	o.	16.7	127.9	55.	90.	5.		123+6		272.	20.	n.0	0.0	0.	-0.	0 • D •
	16.9 129.3	45	16.5		50.	33.	5.	17.6	129.7	60.	47.	10.		129+5	50+		25.	23.0	133.3	30+	550+	
	17.5 129.n	50	17.7		50.	21.	0.	21.2	129.9	60.	174.	20.		134+9	45.		20.	0+0	0.0	0.	-0-	0.
	17.8 128.9	50	18.3		50.	34.	Ó.	21.6	129.9	55.	185.	20.		135+1	45.	630.	15.	n • 0	0.0	0.	-0+	n •
1110122	18.0 128.7	50	18.6		50.	42.	o.	20.5	126.4	55.	139.	30.		127.2	40+		10.	0.0	0.0	0.	-0+	0.
1110182	18.2 128.6	50	18.2		50.	6.	o.	19.5	127.1	55.	62.	30.		126.2	40.		10.	0.0	0.0	0.	~0·	0.
1111007	18.6 128.5	40	18.7		40.	6.	o.	20.R	128.4	35.	162.	10.	23.9	128.9	30+		5.	0.0	0.0	0.	-0-	0.
1111062	18.8 128.5	35		128.4	35.	13.	ò.	20.7	128.3	30.	177.	n.	23.0	128.6	30.	491.	5.	0.0	0.0	٥.	-0.	0.
1111122	18.9 128.2	25		128.5	25.	19.	ō.	0.0	0.0	0.	-11+	n.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0-	0.
1111187	18.7 127.8	25		128.5	25.	40.	o.	0.0	0.0	٥.	-8.	n.	0.0	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0-	9.
1112007	18.3 127.3	25	0.0	0.0	0.	-0-	o.	0.0	0.0	0.	-0 ·	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
1112067	18.1 126.9	30		126.9	30.	0.	o.	17.5	125.2	35.	110.	10.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
1112127	17.8 126.2	30		126.5	30.	zi.	ō.	17.3	124.9	35.	163.	10.	0.0	0 + 0	0.	-0.	0.	0.0	0.0	0.		0.
1112182	17.4 125.5	30	17.9		30	50.	o.	17.5	124.5	30.	225.	10.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.		0.
1112102 111300Z	16.9 124.8	25		125.0	25.	21.	ŏ.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.		0.
		25		123.A	25.	25.	ō.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	۰.	0.0	0.0	0.		0.
								0.0	0.0	0.	-0.	n.	0.0	0.0	0.	-0.	0.					
										Ò.	-0.	0.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	g .
111306Z 111312Z 111318Z	16.2 123.7 15.7 122.6 15.2 121.4	25 25	15.7	122.6	25.	0.	o. o.				-0.							n.0	0.0	0.		0.

	A: L	FRECAS	TS	
	MHNG	24-4R	48-H3	72-4R
AVG FORFCAST POSIT FRROM	27.	170.	362.	463.
AVG RIGHT ANGLE ERROR	14.	115.	295.	413.
AVE INTENSITY MAGNITUDE ERROR	0.	13.	12.	٩.
AVG INTENSITY BIAS	0.	10.	10.	9.
NUMBER OF FORECASTS	22	16	12	•
		ጌ	1	b

## TROPICAL DEPRESSION 26

<b>***</b>		THACK		WARN		RNZS		24 H	NºIH FO	АЭЗНІ ННЗ			48 H	Dii≺ Fr	RFC41			/2 a	ე∪∺ Fr	12FC#1	<b>.</b> 1
	POSIT      POSIT	w I wn	POSTT	41N7	, ,	w]N)	የሳ		4140	มือ I	#IND	POSI	Ŧ	GNIW		#IND	POS	ī t	CFIN	a 6 T	art No
	13.6 154.			0.0			0.0	-		-u.	۰.	0.0	$0 \cdot 0$	U.	-0.	0.	0.0	0.0	υ.	-0.	0.
	14.9 154.			0.0 0.0			0.0	0.0		- U -	ο.	0.11	0 + 0	U.	-0.	0.	0.0	0.0	Ü.	-0-	0.
	16.2 154.						0.0	0.0		- U •	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	ö.	-0.	ñ.
	17.4 153.			)•n 0.	-0.	0.	0.0	0.0	0.	-0.	۰.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
	18.5 152.		19.7 152		13.	0.	0.0	149.7	0.	<b>-</b> U+	٠.	0.0	0.0	٠.	-0.	0.	0.0	0.0	0.	-0.	0.
1201062 1	19.7 151.4	30	19.5 (5)		6.			150.0		19.	۸.	Λ.O	0.0	٠.	-0.	0.	$a \cdot 0$	0.0	0.	-0.	0.
	20.9 150.5	30	20.9 15		33.	0.		151.7	30.	80.	15.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	~ O •	0.
	22.5 150.0	36	22.2 150		33.	ö.	0.0	0.0	0.	-0.	17.	0.0	0.0	0+	-0.	0.	0.0	0.0	0 -	-0 ·	n •
	24.2 149.6		24.5 150	)•n 30.	21.	o.	0.0	0.0	ő.	-0.	0.	0.0	0 • 0	0 • U •	-0.	0.	0.0	0.0	0.	-0.	n.
	26.7 150.0		25.4 150	+4 JO.	19.	0.	0.0	0.0	o.	-0.	0.	0.0	0 • 0	U •	-0.	0.	n.D	0.0	0.	-0-	0.
1505155 5	28.2 152.1	15	0.0	•n 0.	-0.	0.	0.0	0.0	0.	-0.	η.	0.0	0.0	0.	-0.	0.	0.0 0.0	0.0	0.	-0.	0.

	AIL	FORECAS	TS	
	₩KNG	24 - 4R	48-m3	72-4
AVG FORECAST POSIT FRENR	21.	55.	n.	8.
AVG RIGHT ANGLE ERROR	16.	28.	0.	0.
AVG INTENSITY MAGNITUDE ERROR	0.	5.	0.	n.
AVG INTENSITY BIAS	0.	5.	0.	0.
NUMBER OF FORECASTS	4	3	Ó	'n
		- 3		

#### TYPHOON ABBY

	MEST TRACK	#ARVING FRRO⊰S	54 HUIH	FORECAS!	48 HOHR FORF		F2 HOUR FRECAST
40/04/H	TIZCH DIVING TIZCH P		Benefit			2035	
1129002	6.8 169.0 15 0.0 0.						CIPTW TEN GITH TIPO
1129067				-		0. 0. n.	0 0.0 00. 0.
1129127						0. 0. n.	
1129187						0. O. n.	
1130002			0.0 0.0 0		0.0 0.0 0	0. 0. n.	
1130067			0.0 0.0 0		0.0 0.0 0	0. O. n.	
1130122			0.0 0.0		0.0 0.0 0	0. O. n.	
1130187			0 n n n 0		n.n 0.0 0	U. O. n.	
1201002	6.3 164.2 20 0.0 0. 6.2 163.4 20 0.0 0.		0.0 0.0 0		0.0 0.0 0	0. Q. n.	
1501062			0.0 0.0 0		0.0 0.0 0	0. O. n.	
1201122	5.9 162.9 25 0.0 0.		0.n n.n p		0.0 0.0 0	0. 0. n.	
1501185	5.8 161.9 25 0.0 0.		0.0 0.0 0		0.0 0.0 0	0. 0. n.	
1202002	5.7 160.9 3n 6.0 161.		6.4 (58.) 30		7.6 154.4 35. 26		
1202062	5.8 140.3 4n 5.7 160.		7.0 156.0 45		9.1 151.6 6g. 4n	0. 15. 1n.	
1202122	5.9 159.9 en 5.9 159.		7.5 153.0 50		9.5 150.6 65. 40		
1202187	6.0 159.6 45 5.9 159.		6.7 156.4 50.		A.1 153.6 b0. 16		9 150.0 80. 225. 20.
1203007	6.1 159.3 45 6.0 158.		6.9 156.2 50.	. 156. ln.	A.5 152.7 60. 18		
1203062	6.3 159.1 45 6.3 159.		7.0 157.6 65.	. 78• 2n.	A.4 154.8 80. 3		5 150.6 90. 127. 55.
1203002	6.5 159.0 40 6.3 159.		6.7 154.1 /5.	. 99• 2n.	R.3 155.3 80. A		2 151.4 90. 64. 60.
	6.8 158.9 4n 6.4 159.		7.5 157.8 65.	. 93. s.	A.A 154.9 80. 10		
1203182	7.3 158.4 4n 6.7 158.		8.0 157.1 60,	. 76. n.	9.2 154.2 75. 11		5 150.4 90. 142. 60.
1204002	8-1 158-3 45 8-1 158-		10.0 155.1 65.	. 108. 5.	11.3 150.8 75. 16		5 1+6.0 90. 155. 50.
120406Z	8.2 157.4 55 8.9 157.		10.8 153.3 65,	, 170. K.	11.9 148.7 75. 21		6 1+3.9 90. 195. 55.
120412Z	8.2 156.4 6n B.2 156.		9.9 151.5 65.	. 155. 5.	11.6 147.1 75. 20		8 1+3.2 90. 140. 55.
120418Z	8.2 195.8 6n 8.3 154.		9.0 150.3 70.	. 161. 2n.	11.8 145.8 B5. 18		2 142.0 95. 210. 60.
120500Z	8.2 155.1 60 8.5 153.		10.n 149.2 70.	175. 35.	11.H 144.8 85. 15		7 140.3 95. 252. 60.
120506Z	8.1 154.2 fo 8.3 154.		9.5 150.7 70		11.2 146.2 85. A		
1205127	8.0 153.3 An 7.8 153.		8.7 144.4 70.	. 53. 4n.	10.8 145.6 85. P		0 141.3 95. 67. 65.
1205182	8.3 152.5 bn 7.8 152.		9.2 147.4 65		10.H 143.8 80. 60		
150600%	8.8 151.9 35 8.3 151.		9.2 147.6 60.		10.5 143.4 60. R		
1206062	9.2 151.n 3n 8.9 150.		10.n 147.2 50.	77. 15.	10.9 142.9 40. 7		
1206127	9.5 149.8 3n 9.4 150.		11.0 147.0 50.	. 103. 15.	11.5 142.9 45. 6		0 1.48.8 35. 1935.
1206187	9.8 148.1 3n 9.9 149.		11.7 144.9 50.	. 19. 15.	12.3 141.0 45. 39		
1207002	10.0 146.7 30 10.1 145.		11.2 136.1 40.	460. 5.	15.1 132.4 30. 435		
1207067	10.2 145.0 35 10.2 143.		12.0 135.5 40.	456. 10.	15.0 132.3 30. 3A		
1207127	10.6 145.3 35 30.8 143.		12.9 137.3 45.	283. 15.	15.7 133.3 30. 359		
1207187	11.0 144.9 35 11.0 145.		12.0 142.4 40.	135. 10.	13.0 141.0 30. 397		
1208007	11.7 144.1 35 11.4 144.		13.5 142.3 35.	. 235. n.	16.2 140.3 20. 5mg		
1208062	12.1 143.3 30 11.9 143.		14.3 141.6 30.	3145.	n. II 0.0 0I		
120812Z	12.2 142.1 3n 12.2 142.		15.2 124.1 20.	545. #2n.	n.u 0.0 u(		
1208187	11.8 140.6 30 12.5 140.0		0.0 0.0 0.	-U+ n.	n.0 0.0 0(		
1209007	11.4 138.9 35 11.4 139.		11.0 137.1 25.	18. 725.	10.4 127.2 20. PR		
1209062	11.0 137.4 35 11.3 137.		10.9 131.7 35.	82. 725.	10.7 125.7 30. 347		
1209127	10.3 136.n 4n 10.4 135.		10.0 [29.] 60.	, 223. <b>«</b> ]n.	10.1 123.6 30. 475		
1209182	10.5 134.7 45 10.0 133.		9.0 127.7 60.	284. =15.	0.0 0.0 00		
1210002	11.3 133.3 on 11.3 133.		12.4 124.7 70.	129. =1n.	14.0 123.6 75. 412		
1210062	11.7 132.9 6n 11.7 132.0			162. 1n.	14.2 122.2 55. 53		
1210127	12.3 132.1 7n 12.1 132.				14.2 124.0 75. 512		
7810187	13.1 131.2 75 12.9 131.4			144. 725.	14.6 124.9 /5. 535		5 120.7 50.119330.
1211002	13.7 130.4 NO 13.7 130.1			174. =4n.	14.4 122.5 45. 711		
1211067	14.2 130.1 KS 14.2 130.4		16.4 124.H 60.	242. 440.	16.6 122.7 45. 799		
1211127	15.0 130.1 90 14.7 129.5				16.7 123.3 45. H78		
1211187	15.7 130.2 Inn 15.8 13n.		20.1 132.0 50.		24.0 139.3 4U. 139		
1515005	16.4 130.3 10n 16.3 13n.;	70. S10.			24.6 141.6 45. 150		
							, v.u vu. Ua

1414067	17.1 131.0 100	17.4 130.0 10	0. 19.	0.	21.0 134.3	60. 135.	#5n.	24.H 147.	35.	276.	<b>~5.</b>	0.0	0.0	0.	-0.	٥.
1212127	18.0 132.0 100	17.9 131.8 9	75. 13.	-5.	21.8 [3H.]	b0. 3b.	<b>₹</b> 30.	n_n 0 •	0.	-0.	0.	0.0	0.0	٠.	-0.	0.
1212187	18.9 133.1 100	19.9 133.2 8	15. f.	-l>.	23.n 14n.1	45. 74.	<b>435.</b>	n.n 0.	0.	-0.	0.	n.0	0.0		-0.	0.
1213007	19.8 134.5 110	20.0 134.9 8	15. 25.	-25.	24.0 147.9	45. 135.	<b>"</b> 15.	n.n 0.	0 0.	-0.	0.	0.0	0.0			0.
1213067	20.5 136.2 110	21.1 136.9 8	10. 53.	-30.	25.n 144.4	35, 261.	-5.	0.0 0.	0.	-0.	0.	0.0	0.0			
1213122	21.2 138.1 40	21.4 138.2 10	0. 13.	10.	24.7 147.2	55. 123.	25.	0.0 0.	D 0.	-0.	0.	n.o	0.0			
1213187	21.8 140.1 40	22.0 140.2 8	15. 13.	5.	25.4 150.5	45. l68.	15.	6.0 0.		-0.					-0.	0.
1214002	22.2 142.4 6n	22.3 142.6 7	0. 13.	10.	0.n n.n	00.	0.	0.0 O+	0 0.	-0.			0.0			0.
1214062	22.6 144.9 40	22.5 (45.0 6	0. g.	20.	0.0	0	0.	0.0 0+		-0.		0.0	0.0	0.		0.
1214122	22.7 147.7 30	22.8 147.6 4	0. B.	10.	0.0	00.	n.	0.0 0.	0 0.			0 • D	0.0		-0-	0.
1214182	22.8 150.3 30	0.0 0.0	00.	Ű.	0.0	00.						0.0	0.0	0.		9.
1215002	23.0 153.0 25	0.0 0.0	00.	0.	0.0 0.0	00.	0.	n_n 0.	0 ⊍•	-0.	0.	n • 0	0.0	0.	-0.	17.0

	AIL	FIRECAS	TS	
	WHNG	24-4유	48-H3	7>-4R
AVG FORECAST POSTT FRENK	31.	164.	285.	378.
AVG HIGHT ANGLE ERANH	17.	108.	199.	215.
AVG INTENSITY MAGNITUDE ERROR	10.	20.	30.	42.
AVG INTENSITY HTAS	2.	-2.	-1.	22.
NUMBER OF FORECASTS	52	48	39	25
		16	19	19

# TROPICAL STORM BEN

HEST TRACK WARNING					24 HOUR FORECAST				48 HOUR FORFCAST				ST.	72 HOUR FRRECAST								
	111.31	, , , , , , ,					250				ERR:	JA'S				FRRN	?5					
#0/04/Ha	POSIT	HIND	POS		#INO		WINS	Pns	τT	WIND	DST	4 IND	POS	11	WIND	DST	JIND	P05	Į Ť	WIND	nST	MIND
				0.0	0.	-0.	0.	0.0	0.0	0.	-0.	· 0 ·	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
121700Z	7.0 149.		0.0	-				0.0	0.0	o.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1217062	7.3 148.		0.0	0.0	o.	-0.	٥.	0.0	0.0	o.	-0.	0.	0.0	0.0	ō.	-0.	ŏ.	D. 0	0.0	Ď.	-0.	0.
1217122	7.5 147.		0.0	0.0	٥.	-0.	0.		_		-0.	0.	0.0	0.0	ŏ.	-0.	ő.	0.0	0.0	o.	-0-	0.
121718Z	7.7 146.	n 15	0.0	0.0	٥.	-0.	٥.	0.0	0.0	٥.				0.0	0.	-0.	o.	0.0	0.0	0.	-0+	0.
1218002	8.0 145.	n 15	0.0	0.0	0.	-0.	٥.	0.0	0.40	9.	-0.	٥.	0.0							0.		0.
121806Z	8.2 143.	9 15	0.1	0.0	٥.	-0.	٥.	0.0	0.0	0.	-0-	0.	0.0	0.0	٥.	-0.	٥.	0.0	0.0		-0.	0.
1218127	8.5 142.	7 15	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.	0.0	0.0	٥.	-0.	٥.	0.0	0.0	0.	-0+	
121818Z	8.7 141.	4 15	0.0	0 • 0	0.	-0.	0.	0.0	0.0	٥.	-0-	n.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0•	0.
1219002	9-0 140-	n 15	0.0	0 • 0	Ű.	-0.	0.	0.0	0.0	0.	-0+	G.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
1219062	9.4 138.		0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
121912Z	9.9 137.		0.0	0.0	0.	-0-	0.	0.0	0.0	0.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	0.
121918Z	10.4 135.		0.0	0.0	o.	-0.	0.	0.0	0.0	٥.	-0.	٥.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1220002	10.9 134.		0.0	0.0	ō.	-0.	o.	0.0	0.0	0.	-0.	٠.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0-	0.
1220067	11.3 132.		0.0	0.0	ō.	-0.	ō.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1220122	11.6 130.		0.0	0.0	ŏ.	-0.	ŏ.	0.0	0.0	ō.	-0.	٥.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1220182	11.6 129.		0.0	0.0	ŏ.	-0.	ŏ.	0.0	0.0	ŏ.	-0.	0.	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	0.
				0.0	ŏ.	-0.	ŏ.	0.0	0.0	ŏ.	-0.	0.	0.0	0.0	0.	-0.	o.	0.0	0.0	0.	-0.	0.
1221007	11.5 127.		0.0				ő.		122.1	35.	93.			119.3	35.	199.	0.	0.0	0.0	0.	-0.	0.
122106Z	11.4 126.		11.5	125.9	50.	8.	š.		121.2	35	115.		15.1	118.8	35.	375.	10.	0.0	0.0	Ď.	-0.	0.
1551155	11.8 124.			124.6	45.	21.			118.0	35.	88.		0.0	0.0	0.	-0.	Ö.	0.0	0.0	0.	-0.	0.
1221187	12.2 123.		11.8	155.7	40.	30.	o.				130.		0.0	0.0	٥.	-0.	ŏ.	n.0	0.0	0.	-0.	0.
122200Z	12.7 121.			151.0		6.	5.		117.7	<b>+0.</b>				0.0	0.	-0.	ŏ.	n. 0	0.0	ŏ.	-0.	0.
15550eZ	13.0 120.			150.4	40.	6.	-10.		114.6	35.		٠.	0.0	0.0		-0.	ö.	0.0	0.0	ů.	-0.	0.
155515Z	13.8 119.	4 55	13.7		50.	24.	-5.		117.0			10.	0.0		0.					0.	-0.	0.
1222162	14.6 119.	2 60		118.2	50.	61.	-10.	0.0	0.0	0.	-0-	0.	n.0	0.0	٥.	-0.	٥.	0.0	0.0			0.
1223002	15.6 119.	5 55	15.6	119.4	55.	6.	٥.	0.0	0.0	0.	-0-	η.	n.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0+	
1223062	17.6 121.	n 35	16.9	119.9	45.	75.	10,	0.0	0.0	٥.	-0.	n.	0.0	0+0	0.	-0.	0.	0.0	0.0	0.	-0.	٥.
1223127	19.6 123.		19.4	122.1	25.	103.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.

	AI'L	FORECAS	TS	
	HHNG	24-HR	48-HR	72-4R
AVG FORFCAST POSTT FRROR	34.	181.	287.	0.
AVG RIGHT ANGLE ERODR	18.	89.	15.	٥.
AVG INTENSITY MAGNITUDE ERROR	5.	14.	ō.	ο.
AVG INTENSITY BIAS	-1.	-11.	5.	٥.
NUMBER OF FORECASTS	10	6	2	9
		-	1	

# 2. NORTH INDIAN OCEAN CYCLONE TRACK DATA

TC 17-79

		BEST T	RACK			WARUT				24 40	THE FO	HECA:			48 HC	na Fr				#2 43	IUR FO	narC4	<b>e</b> T
40 40 444-	0007					. 7		RORS	0-5					DOC		ON I w	ERRO		000				
MO/DA/HR	POSI		IND	POS		AINJ	DST	MINO	Pns		₩1 NO	051	.IMD	POS			nst	WIND	POS		MIND		H T NO
050508Z	6.3	90.9	15	0.0	0 • n	0.	-0.	0.	0.0	0.0	0.	~0.	۰,	0.0	0 • 0	0.	-0.	٥.	0.0	0.0	0.	-0.	n.
050514Z	6.4	90.4	50	0.0	0 • 0	٥.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	6.	-0.	0.	0.0	0.0	0.	-0.	n.
050520Z	6.5	89.7	5.0	0.0	0.0	٥.	-0.	٥,	0.0	0.0	0.	-0.	n.	n.⊕	0.0	0.	-0.	0.	0.0	0.0	0.	~0.	0.
050602Z	6.6	89.1	25	0.0	0.0	0	-0.	٥.	0.0	0.0	٥.	-0+	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
050608Z	7.0	88.6	25	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0-	n.	0.0	0.0	0.	-0.	.0.	0.0	0.0	0.	-0.	٩.
050614Z	7.5	AB.A	31	7.2	87.7	30.	45.	0,	8.7	85.8	35.	129.		10.1	84.5	45.	243.	-15.	12.0	H4.0		201-	-5.
050620Z	7.6	98.0	30	7.4	87.5	30.	35.	0.	8.9	85.5	35.	148.	410.	10.A	84.1		259.		12.7	H4.3	55.	155.	-5.
050702Z	7.1	97.A	35	7.9	88.0	35.	49.	υ.	9.6	88.2		262.	-5.	33.5	88.7		257.		13.3	49.7	65.		ο.
0507082	6.7	87.2	35	7.2	87.7	35.	42*	٥.	8.7	87.5		179.	435.	10.5	88.2		185.		12.6	N7.4	65.		-5•
050714Z	6.7	86.6	<b>4</b> ()	7.6	B7+1	40.	61.	0.	9.0	87.9			<b>-10.</b>	12.0	B9.0	65.	247.	5.	14.0	40.7	70.	420.	-5.
050720Z	6.4	86.1	45	7.5	86+6	45.	72.	٥.	9.5	85.8		148.	a •	11.6	86.7		113.	10.	13.0	M9.8	75.		0.
0508022	5.8	86.n	5 n	5.9	86•∩	50.	66.	0.	7.6	83.2	60.	184.	-5.	R.5	B0 • 0		315.		4.4	16.7		412.	-55.
050808Z	5.9	86.4	60	5.6	96∙1	60.	30.	0.	4.9	83.4	65.	254.	٠.	4.9	80.2		470.	0.	5.3	77.1			-10-
050814Z	6.5	86.4	60	5.2	85.4	60.	98.	Θ.	4.0	82.4	65.	330.	5.	5.0	79•2			-5.	5.5	76.1			-15.
0508202	7,1	86.4	60	5.9	86.7	60.	73.	0.	5.7	B5.7		275.	5.	5.4	84+0			-5.	5.4	MO.5	70.	521.	-15.
050902Z	7.6	86.7	65	7.3	86.2	65.	19.	٥.	B.>	84.2			٦.	9.1	81.5		249.		9.4	78.7	60.	328.	
0509082	8.2	A6.1	65	7.8	85.A	65.	30.	o.	9.n	84.1			n.	10.3	81+5				11.0	18.7	50.	244.	
0509142	9.2	A5.9	60	8.8	85+6	60.	30.	٥.	10.4	87.5		114.	<b>-20</b> •	11.9	81.5				12.7	18.9		, ,	
050920Z	10.3	A5:3	60	10.4	85.2	60.	8.	0.	12.2	82.7	60.	42+	<b>-15</b>	13.0	80.8	55.		-30.	13.3	18.9	30.		-50.
	11.2	94.6	65	10.9	84.3	65.	25.	0.	12.3	81.ª	60.	67.	*15.	0.F1	80.0		101.		0.0	0.0	0.	~O•	0.
051008Z	11.7	84.7	70	11.6	83.9	75.	19.	5.	12.5	81.4	45.	75.	5.	13.3	79.4		332.		0.0	0.0	0.	-O.	0.
	12.3	43.7	75	12.1	83.4	75.	21.	0.	13.2	81.2	H5.	42.	n.	14.0	79.4		120.		0.0	0_0	0.	-0.	0.
051020Z	12.7	83.2	75	12.7	83+4	75.	12.	0.	13.7	81.6	85.	33.	n .	14.5	79.8	50.	178.	0.	0.0	0.0	0.	-0-	0.
051102Z	13.0	82.7	75	13.1	82.6	В0.	8.	5.	14.1	80.9	H5:	25.	5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-8.	0.
051108Z	13.4	82.3	Bò	13.2	82∙3	90.	12.	10.	14.2	80.5	105.	64.	25.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	<b>.0.</b>	0.
051114Z	13.7	81.7	85	14.2	80.4	95.	55.	10.	16.5	78.2	30.	70.	<b>-3</b> 0.	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	0.
051120Z	14.1	81.2	85	14.1	B0 - 9	95	23.	10.	16.0	7H.5	30.	64.	<b>-20.</b>	-n.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
	14.5	90.8	80	14.4	80.5	90.	18.	10.	0.0	0.0	0.	-0.	B •	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0512082	15.2	80.1	80	14.R	80.5	85	33.	5.	0.0	0.0	0.	-0.	0.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	٥.	-0.	0.
	16.0	79.3	60	15.2	79.0	60	59.	0.	0.0	0.0	o.	-0.	n.	0.0	0.0	0.	-0.	0.	n.0	0.0	0.	-0.	0.
	17.0	78.1	5n	17.0	78-1	50.	0.	o.	0.0	0.0	0.	-0-	n.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0215507	11.40	18.1	20	11.0	(44)	50.	٠.	٠.	4.11	., .,	٠.	-0.	17 4		0.0	U.	-0.	٠.		V.0		-0.	17.

	ai'L	FORECAS	TS	
	WRNG	24-HR	48-H3	72-4R
AVG FORFCAST POSIT FRRAR	36.	139.	233.	346.
AVG RIGH! ANGLE ERROR	17.	95.	192.	296.
AVG INTENSITY MAGNITUDE ERROR	ż.	9.	13.	12.
AVG INTENSITY BIAS	2.	-5.	-11.	-12.
NUMBER OF FORECASTS	24	22	18	14

TC 18-79

BEST TRACK WARNING									24 H	NIK F(	RECAS	S ţ		48 H	Japan Fr	RFCA!	ST		92 H	UR Fn	OF CAS	т	
							FRI	2025				EHR	} <b>∢</b> S				FREG	₹5					
MO/DA/HR	POSI	T	WIND	POS	1 T	CNIN	DST	WIND	Pns	ŢΤ	w1 40	OST	4 I MD	POS	ĮΤ	WIND	nst	-IND	POS	1 *	WIND	OST	MIND
0617142	17.7	66.4	25	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ο,	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	6.
0617202	17.9	65.5	30	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	۰.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0618022	18.0	64.9	30	18.3	65∙7	40.	34.	10.	19.5	64.6	50.	238.	0.4	21.5	65 • 0	60.	476.	20.	0.0	0.0	0.	-0.	0.
0616087	18.0	64.0	35	18.4	64.9	40.	56.	5.	19.6	64.1	55.	248.	٩.	22.0	64 • B	60.	4R2.	35.	0.0	0.0	0.	~O.	۵.
0618147	18.2	63.1	40	18.2	63.A	45.	40.	5.	19.4	62.3	55.	170.	5.	22.6	63.5	60.	445.	40.	0.0	0.0	٥.	-0.	0.
0618202	18.2	61.4	45	18.5	62.4	45	38.	0.	19.7	50.3	55.	46.	5.	21.6	56.5	40.	100.	25.	0.0	0.0	0.	-0.	0.
061902Z	18.0	60.7	50	18.7	61.7	50.	70.	0.	20.0	58.6	50.	60.	10.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
061908Z	18.4	59.4	50	18.7	59.9	50	18.	0.	20.7	57.1	30.	77.	٩.	0.0	0 + 0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
061914Z	18.8	59.4	50	18.5	58+4	50.	59.	0.	20.2	54.1	25.	115.	5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
061920Z	19.1	58.A	5 n	19.0	58.3	50	29.	0.	0.0	0_0	0.	-0.	٥.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
062002Z	19.2	57.4	40	19.4	59.0	50.	69.	10.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	~O.	n.
062008Z	19.5	56.4	25	19.8	58.2	45.	92.	20.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
062014Z	19.8	56.1	20	20.0	56 • A		41.	15.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
062020Z	1.05	55.7	15	20.5	55.6	25	25.	10.	0.0	0.0	0.	-v .	п.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.

	AIL	FIRECAS	TS	
	MHNG	24-4R	48-H3	72-4R
AVG FORECAST POSIT FRANK	48.	137.	363.	0.
AVG RIGHT ANGLE ERDOR	24.	78.	284.	0.
AVG INTENSITY MAGNITUUE ERROR	6.	5.	30.	n.
AVG INTENSITY RIAS	6.	5.	30.	0.
NUMBER OF FORECASTS	12	7	4	9

## TC 22-79

	HEST THACK HARVING									24 H	VIR E	REUA:	<b>5</b>		48 H	nik Eu				72 4	OUR FA	RFCAS	\$T
							FOR	เกสร				EKR	)rtS				FRAGE	₹5					
94/44/01	Post	т .	ITNO	გენ	τT	WINT	DST	WINS	Pns	τT	WIND	051	*IND	PNS	IT	WIND	nst	<b>⊿IND</b>	POS	Ť	MIMD	ŋŞT	M I MD
920027	9.1	H7.9	20	0.0	′ 0 • n	0.	-0-	0.	0.0	0.0	0.	-0.	0.	0.0	0 • 0	0.	-0.	0.	n • 0	0.0	0.	-0-	0.
92008Z	9.7	97.4	50	0.0	0.0	Ŏ.	-0.	Ŏ.	0.0	0.0	0.	-0.	0.	0.0	0 + 0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
					-			Ü.	0.0	0.0	ō.	-0.	0.	0.0	0+0	0 -	-0.	0.	0.0	0.0	0.	-0-	0.
920147	10.1	H6.R	20	0.0	0.0	0.	-0.		0.0	0.0	Ň.	-0.	0	0.0	0.0	0.	-0.	Ö.	0.0	0.0	Ü.	-0.	0.
920202	10.4	16.4	50	0.0	0.0	٠.	-0.	Q.			0.	-0.	0.	0.0	0.0	0.	-0.	ů.	0.0	0.0	0.	-0.	0.
921022	10.7	86.0	50	0.0	0.0		-0.	٥.	0.0	0.0					80.9		137.	30.	0.0	0.0	ů.	-0.	0.
921087	11.1	45.6	25	11.0	85.5		в.	O.	12.5	87.4	35.	140.	10.	14.7							0.	-0.	0.
921142	11.6	95.2	25	11.0	84 - 0		79.	0.	12.2	82.7	35.		) n •	13.1	80.5		209.	30.	0.0	0.0			2.1
921207	12.8	95.0	25	12.1	84.9	25.	42.	0.	13.4	87.n			15.	14.4	80.9			30.	0.0	0.0	0.	-0+	0.
922027	14.0	94.7	25	12.5	84.4	30	91.	5.	13.7	82.5	J5.	146.	15.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	0.
922087	14.9	43.9	25	13.5	82.8		105.	10.	14.5	81.1	40.	121.	3 n .	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ο.
922142	15.3	93.1	25	15.0	84.0			5.	16.7	81.6	40.	63.	30.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	0.
					83.0		46.	10.	18.0	80.2		54.	n.	0.0	0.0	0.	-0-	0.	0.0	0.0	0.	-0.	ρ.
)92220Z	15.5	45.2	5.0	15.6					0.0	0.0		-0.	0.	0.0	0.0	0.	+0.	0.	0.0	0.0	٥.	-0.	o.
:92302Z	15.9	A1.4	5.0	16.0	82+2		46.	10.				-0.	0.	0.0	0.0		-0.	ŏ.	0.0	0.0	ō.	-0.	0.
1923082	16.5	40.R	1 n	16.5	81.4		.34.	15.	0.0	0.0		-	_						0.0	0.0	ŏ.	.0.	
1923147	16.6	80.5	10	17.0	80.A	15.	29.	5.	0.0	0.0		-0.	n.	0.0	0.0		-0.	0.					
1923202	17.1	40.3	<u>)</u> n	0.0	0.0	o.	-0.	0.	0.0	0.0	0.	-0.	٠.	0.0	0 + 0	0.	-0.	0.	0.0	0.0	0.	-0.	0.

	AI L	FORECAS	TS.	
	WHNG	74-4P	4B-H3	72-4R
AVG FORECAST POSTT FRHOR	54.	122.	170.	0.
AVG RIGHT ANGLE ERONR	34	90.	122.	ο.
AVG INTENSITY MAGNITUUF ERROR	6.	16.	30.	0.
AVG INTENSITY BIAS	6.	16.	30.	0.
NUMBER OF FORFCASTS	10	7	3	0

#### TC 23-79

	BES	T TRACK			24 H	HIR FO				48 HO	uA Fo	RECAS			72 HJ	UR Fr	RFC49	<b>T</b>				
						568	INRS				ERR					ERROR						
40/04/H9	POSIT	WIND	Pos	T T	WINT	DST	WIND	Pns	ŢŢ	MIMO	อรา	GNI	POS		MIND		MIND	POS		MIND		MIND
0918022	12.2 72	-0 15	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.	0.0	0 • 0	0.	-0.	٥.	0.0	0.0	٥.	-0.	0.
0918087	12.5 71		0.0	0 • 0	0	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
091814Z	13.0 71		0.0	0.0	o.	-0.	0.	0.0	0.0	0.	-0.	٥.	0.0	0.0	. 0.	-O.	0.	0.0	0.0	0.	-0.	0.
0918202	13.4 71		0.0	0.0	o.	-0.	ů.	0.0	0.0	0.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	~O·	0.
0919022	13.8 71		0.0	0.0	o.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
0919082	14.3 71		0.0	0.0	Ŏ.	-0.	o.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0+	0.
0919142	14.6 71		0.0	0.0	ŭ.	-0.	o.	0.0	0.0	o.	-U.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0+	0.
0919202	15-0 70		0.0	0.0	ŏ.	-0.	ů.	0.0	0.0	Ŏ.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
0920022	15.3 70		0.0	0.0	ŏ.	-0.	ō.	0.0	0.0	ō.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0-	0.
0920082	15.6 70		0.0	0.0	ŏ.	-0.	ŏ.	0.0	0.0	ō.	-0.	0.	0.0	0.0	0.	-O.	0.	0.0	0.0	0.	-0.	0.
092014Z			0.0	0.0	ŏ.	-0.	ŏ.	0.0	0.0	0.	-0.	n.	0.0	0.0	٥.	-0.	٥.	0.0	0.0	0.	-0.	0.
				0.0	o.	-0.	o.	0.0	0.0	ů.	-4.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ο.
0920207	16.4 49		0.0	0.0	0.	-0.	ŏ.	0.0	0.0	ŏ.	-0.	0.	0.0	0.0	ō.	-0.	ō.	0.0	0.0	0.	-0.	0.
0921022	16.8 69		0.0	-			0.	0.0	0.0	ŏ.	-0+	n .	0.0	0.0	0.	-0.	ō.	0.0	0.0	0.	-0.	0.
092108Z	17.4 48		0.0	0.0	٥.	-0.		0.0	0.0	ŏ.	-0.	0.	0.0	0.0	0.	-0.	Ö.	0.0	0.0	0.	-0-	0.
0921142	18.0 48		0.0	0+0	٠,	-0.	0. -5.		68.5	+0.	294.	-10.	22.0	68+6	<b>+5</b> •	459	5.	24.0	70.0	20.	716.	-5-
0921202	18.4 67		18.2	68.9	30.	97.		20.1	68.5	40.	331.	15.	22.7	68+9	45.		10.	24.5	10.7	20.	829.	0.
09220ZZ	18.6 66		18.7	68+7	30.	142.	-10.	20.7		45.	86.	-1	20.B	61.6	45.	119.	15.	0.0	0.0	0.	-0-	0.
0922082	19.0 45		19.2	65.7	40.	26.	-5.	20.2	67.5		13.	٠	20.5	58.0	0.	57.	-30.	0.0	0.0	0.	-0.	0.
0922142	19.3 44		19.0	64-6	40.	25.	-5.	19.9	61.3	50.	51.		20.9	55.9	20.	119.	-5.	0.0	0.0	0.	-0.	ñ.
0922202	19.6 43		19.4	63-7	60.	25.	10.	20.1	59.7	70.		30.		0.0	0.	-0.	0.	0.0	0.0	ŏ.	-0.	0.
0923027	19.7 62		19.6	62•7	65.	6.	10.	50.4	54.8	60.	73.	25.	0.0				ŏ.	0.0	0.0	ě.	-0.	0.
092308Z	19.9 42		19.5	61+7	65.	18.	15.	20.7	57.A	65.	107.	35.	0.0	0.0	0.	-0.	ö.	0.0	0.0	ŏ.	-0.	ő.
0923147	20.0 61		50.0	63.5	35.	118.	-10.	21.3	65.1	20.	362.	•1n•	0.0	0.0			ů.	0.0	0.0	ŏ.	-0.	ō.
092320Z	50.5 40	. A A B	20.3	60-3	35.	18.	-5.	22.1	57.7	50*	150.	-5.	0.0	0.0	0.	-o.		0.0	0.0	ŏ.	-0.	ŏ.
0924022	20.3 60	.1 35	20.6	59.6	35.	33.	0.	0.0	0.0	0.	-0+	0.	0.0	0.0	0.	-0.	o.	0.0	0.0	٥.	-0.	0.
0924082	20.1 59	.6 30	20,8	58•A	30.	61.	0.	0.0	0.0	0.	-0-	0.	0.0	0.0	0.	-0.	٥.	0.0		0.	-0.	0.
0924142	19.9 58	.R 30	20.3	58.7	25.	37.	-5.	0.0	0.0	٥.	-0.	0.	0.0	0+0	0.	-0.	٥.		0.0	0.	-0.	0.
0924207	20.0 57	.A 25	19.8	58•0	25.	16.	0.	0.0	0.0		-0.	0.	0.0	0+0	0.	-0.	0.	0.0	0.0	D.		0.
092502Z	20.0 56	.5 20	20.0	57.7	15.	45.	-5.	0.0	0.0	٥.	-0.	0-	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	u •

	A: L	FORECAS	T5	
	MHNG	24-4R	48-H3	72-4R
AVG FORFCAST POSIT FRROR	4B.	160.	253.	773.
AVG RIGHT ANGLE ERROR	21.	97.	184.	629.
AVG INTENSITY MAGNITUDE ERROR	6.	16.	13.	з.
AVG INTENSITY BYAS	-1.	6.	-1.	-3,
MIMACD OF ENGERAPTE	1.4	9	5	,

#### TC 24-79

	BEST TRACK									24 14	TIN FE				48 H	Durk F	nRFC4			F2 H3	UR Fr	AFC & S	= 7
							FRI	RORS				EKR.					FPR						
MO/DA/HR	Post	T 1	IND	۲nS	ŢΤ	⊌IN1	DST	WINO	Pns	ŧT.	₩ I NO	DST	4 [ e-()	PAS	11	WIND	DST	<b>♦IND</b>	P04	Ţt	CPIN	751	#7 NI)
1029022	11.1	90.8	20	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0+	n.	0.0	0.0	U.	-0.	0.	0.0	0.0	0.	-0.	Π.
1029082	11.7	90.1	20	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	<b>+</b> ₩+	۸.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-D.	0.
1023142	12.2	39.6	54	12.5	89.4	50.	21.	o.	16.3	84.0	40.	250.	15.	19.0	91.9	30.	673.	-5.	14.8	45.8	15.1	036.	0.
102920Z	12.4	99.0	25	13.5	89.0	25.	66.	δ.	16.0	84.2	40.	251.	10.	19.6	90.2	30.	629.	-5.	0.0	0.0	0.	-0.	0.
1030022	12.4	88.2	25	13.6	88.7	25.	77.	o.	15.5	87.5	35.	192.	5.	17.9	87.5	40.	499.	10.	0.0	0.0	0.	-0.	0.
1030087	12.8	87-1	25	12.6	88.2	25.	65.	o.	13.2	84.7	30.	163.	٥.	14.1	84.9	35.	295.	15.	0.0	0.0	0.	-0-	0.
1030142	13.1	96.2	25	12.5	87.0		105.	ů.	12.9	86.5		215.	-5.	14.6	85 • 1	35.	355.	20.	0.0	0.0	0.	-0.	0.
1030207	13.4	45.6	30	13.0	86.5	25	58.	-5.	14.0	83.	35.	121.	Λ.	0.0	0.0	Q.	-0.	0.	0.0	0.0	0.	-0-	0.
1031022	13.5	84.9	30	13.4	84.4	25.	30.	-5.	15.3	Bn.A	35.	167.	5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
103108Z	13.4	43.4	30	13.9	83.5	30	33.	Ö.	15.P	Bn.1	25.	197.	٩.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	0.
1031142	13.0	82.8	35	13.9	82 . A	30	54.	-5.	15-1	79.3	20.	143.	٩.	0.0	0.0	0.	~0.	0.	0.0	0.0	٥.	-0-	0.
1031207	12.7	81.0	35	13.R	82-4	30.	72.	-5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	G.	-0.	0.
1101022	12.5	80.4	30	12.7	Bl.n	30	13.	ō.	0.0	0.0	ō.	-0.	۸.	0.0	0.0	0.	-0.	o.	0.0	0.0	a.	-0-	0.
1101087	12.5	80.1	20	12.7	79.9		17.	0.	0.0	0.0	0.	-0-	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	.0.
1101142	12.7	79.3	15	12.7	79-6	15.	17.	o.	0.0	0.0	o.	-0.	۸.	0.0	0.0	0.	-0.	0.	n . Ø	0.0	0.	-0-	0.

AVG FORECAST POSIT FRROR 48. 190. 482. 1034.
AVG RIGHT ANGLE ERROR 48. 190. 482. 1034.
AVG RITHNSITY MAGNITHOF ERROR 2. 6. 11. 0.
AVG INTENSITY MAGNITHOF ERROR 2. 6. 11. 0.
NUMBER OF FORECASTS 13 9 5 1

#### TC 25-79

	REST TRACK #ARVING									24 H	וץ אוות	DRECA			48 H	DijiR F	PECA			72 40	uR Fn	arc4	<b>:</b> T
							EBR	2005				EKK					FRRO.	35					
MO/DA/HR	POSI	T	WIND	POS	T T	GNIE	DST	KEND	Pns	Ţ T	WIND	051	4IND	PAS	11	WIND	nst	dNI	POS	<b>1</b> 1	WIND	nST	WIND
1114022	12.3	70.1	50	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-U•	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	n.
111408Z	12.8	70.0	20	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
111414Z	13.0	69.9	20	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	9.0	0.	-0-	0.
1114202	13.3	69.A	50	0.0	0.0	0	-0.	0.	0.0	0.0	0.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1115022	13.6	49.8	20	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	۰.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0-	n.
111508Z	13.9	69.8	25	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-U.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
111514Z	14.2	69.4	30	0.0	0.0	٥.	-0.	٥.	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
111520Z	14.6	49.A	30	0.0	0 • 0	0.	-0.	٥.	0.0	0.0	0.	-0-	0.	0.0	0.0	ŭ.	-0.	Đ.	0.0	0.0	0.	-0.	n.
1116027	15.0	69.9	35	15.0	70-0	40.	6.	5.	17.0	70.3	45.	72•	5.	19.5	71.4	60.	121.	45.	0.0	0.0	٥.	-0.	О.
111608Z	15.6	70.0	40	14.6	69.7	40.	62.	0.	15.4	69.9	45.	191.	10.	0.0	0.0	U.	-0.	0.	0.0	0.0	0.	-0.	0.
1116142	16.4	70.2	4.0	14.6	69.7	40.	111.	0.	15.4	60.0	45.	234+	15.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
111620Z	17.3	70.4	4.0	17.3	70+8	40.	23.	ο.	20.2	74.7	0.	252.	<b>*25.</b>	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
111702Z	18.2	70.2	4.0	18,1	71.5	40.	74.	0.	0.0	0.0	0.	-0.	n.	0.0	0.0	٥.	-0.	٥.	0.0	0.0	0.	-0.	ο.
1117082	18.8	70.1	35	17.9	71.9	35.	115.	0.	0.0	0.0	0.	-0.	о.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ο.
111714Z	19.6	70.1	30	19,7	70.1	Эο,	6.	0.	0.0	0.0	0.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
111720Z	20.3	70.2	25	20.3	70.2	25	0.	0.	0.0	0.0	0.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	n.
111802Z	21.3	70.4	15	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٠.

AVE INTENSITY MAGNITUDE ERROR

AVE RIGHT ANGLE ERROR

AVE INTENSITY MAGNITUDE ERROR

AVE INTENSITY MAGNITUDE ERROR

AVE INTENSITY MAGNITUDE ERROR

AVE INTENSITY BASE

NUMBER OF FORECASTS

AUGUSTA

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TC 26-79

	. 1	AEST	TRACK		WARNTNG ERRORS					57 HL	VIH FO	RECAS			48 HO	uR Fo	RECAS			12 43°	UR Fn	RFCAS	iT.
							EBE	रंगएड				EKKJ					FRRAG		000		CFIW	251	WIND
10/04/H2	P051	Т	WIND	P05	1 T	WIND.	DST	CNIM	Pns	11	M I AU	051	⊕ [ MD	POS		MIND		#IND	P05				0.
120147	B.0	94.2		0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	n •	0.0	0 • 0	0.	-0.	۰.	0.0	0.0	0.	-0-	
120202	B.8	93.4		0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	Λ.	0.0	0 • 0	0+	-0.	0.	U • O	0.0	٥.	-0.	0.
121022	9.7	92.8		0.0	0.0	ō.	-0.	o.	0.0	0.0	0.	-0.	٥.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	٥.	-0.	D.
		92.4		0.0	0.0	õ.	-0.	Ö.	0.0	0.0	o.	-0.	۸.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	D.
.12108Z	10.4				0.0	0.		o.	0.0	0.0	0.	-0.	0.	0.0	0.0	0 •	-0.	0.	0.0	0.0	0.	-0.	0.
.121142	10.7	91.0		0.0	-		-0.	ö.	0.0	0.0	ŏ.	-0.	0.	0.0	0.0	v.	-0-	0.	0.0	0.0	0.	-O·	O.
:12120Z	10.8	91.7		0.0	0 • 0	٥.	-0.			0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
112202Z	10.9	91.4		0.0	0.0	0.	-0.	o.	0.0		٧.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1122082	10.8	90.9		0.0	0.0	0.	-0.	٥.	0.0	0.0	٠.	-0.	0.	0.0	0.0	0.	-0.	o.	0.0	0.0	o.	-0.	0.
112214Z	10.7	90.0	50	0.0	0.0	u.	-0.	٥.	0.0	0.0	0.		-	0.0	0.0	ŏ.	-0.	ō.	0.0	0.0	ō.	-0.	0.
1122202	10.5	48.7	5.0	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0+	n.		0.0	0.	-0.	o.	0.0	0.0	0.	-0.	0.
112302Z	10.4	87.6	50	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0+	0.	0.0		35.	162.	10.	0.0	0.0	ŏ.	-0.	0.
1123082	10.6	86.5	25	10.0	98.0	25.	95.	0.	10.7	84.9	30.	170.	0.	11.4	81.8						0.	-0.	0.
1123142	10.7	85.4		10.3	97 • 1	30.	103.	5.	11.2	84.0		159.	٠.	12.0	80.9	35.		20.	0.0	0.0	0.	-0.	0.
1123207	10.7	84.3		10.6	84.0	35.	19.	5.	11.0	80.6	<b>*5.</b>		50.	0.0	0.0	U.	-0.	0.	n • 0	0.0			
1124027	10.6	93.0		11.0	92.5	35.	38.	5.	12.2	7H. H	25.	124.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
1124087		92.0		10.6	B1 . A	35.	17.	5.	11.2	77.0	20.	256.	-5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
	10.8			11.0	80.6	35	47.	5.	0.0	0.0	0.	-0.	٥.	0.0	0.0	u.	÷0.	0.	0.0	0.0	0.	- O -	n •
1124147	11.4	91.3				30.	78.	5.	0.0	0.0	o.	-v.	٥.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0-	n.
112420Z	12.2	#0.9		11.9	79.6			5.	0.0	0.0	ŏ.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	n.
1125022	12.9	RO.F		11.9	79.4	30.	92.				ŏ.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	n.
1125082	13.B	90.5	25	13.6	80.n	25.	29.	٥.	0.0	n.1		-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
112514Z	14.5	79.7	15	14.5	79.6	20.	6.	5.	0.0	0 • 0	0.	-0.			340	•	٠.	••	• •				

	Ai L	FORECAS	15	
	WHNG	24-4R	48-H3	72-48
AVG FORFCAST POSIT FRHOR	52.	148.	163.	0.
AVG RIGHT ANGLE ERODR	31.	83.	21.	ο.
AVE INTENSITY MAGNITUDE ERROR	4.	6.	15.	ο.
AVG INTENSITY BIAS	4.	4.	15.	n.
WHATE OF FOURORES	10	5	2	2

## ANNEX B TROPICAL CYCLONE FIX DATA

# 1. WESTERN NORTH PACIFIC CYCLONE FIX DATA

NOTICE - THE ASTERISKS (\*) INDICATE FIXES UNREFRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

## TYPHOON ALICE

#### SATELLITE FIXES

FIX NÚ.	77ME (7)	FTX POSTTION	<b>₽</b> CC44	PAQSAK CODE	SATELL LIFE	COMMENTS	SITE
• 1	310400	3.94 (12.2E	PCN 6		Duspak		PGTw
2	011236	3.84 150.5E	PON 6		DMSP35		PGT₩
3	011414	5.8v 157.3E	PCN 6	12.5/2.5	DMSP37	INI ) Das	KGWC
4	012151	4.9v 156.0E	PCV 6	TZ.n/2.0	AF42MQ	INIT DOS	PGTW
* 5	012336	5.44 165.5E	PCN 6		Duguag		KG₩C
6	020351	5.54 357.58			GNFS3 DMSP37		PHIK
7 8	021218	5.04 167.0E	PON 6		DMSP35		PGTW PGTW
g	021400	5.34 JA7.0E 6.98 JA7.4E	Prn 6		DMSP37		KGWC
10	022133	7.04 147.7E	PCN 6	T2.0/2.0 /50.0/24HR			PGTW
11	024318	4.54 167.3E	PCN Z	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	DMSP35		KGWC
12	070741	A.5N 168.0E	PCN 6		DMSP37		PGTW
13	002150	H. SN 168.3E	Prn 6	T3.5/3.5 /D].0/29HR			KG⊮C
14	031940	4.50 163.1E	BCA P		DMSP37		PHIK
15	032115	9.24 168.0E	PCA 6	T3.0/3.0 /D1.0/24HR	GOF53		PGT
16 17	032150 040042	9.50 168.0E 9.34 157.6E	PCN 5		DMSP35		PHIK PGTW
18	040350	9.8v 167.1E	,,,,,		GOF S3		PHIK
19	040957	3.6% 167.4E	PCN 6		DMSP36		PGT#
20	045005	9.64 165.6E	PCN 4		DWSP37		PGT₩
21	04205B	4.5% 365.5E	PCN 4	T3.5/3.5 /D0.5/24HR			PGTW
22	050024	9.54 165.0E	PCN 3		DMSP35		PGTW
23	040350	9.9N 164.5E			GOFSA		PHIK
24	050939	10.1H 163.7E	Prin 6		DMSP36		PGTW
25 26	051305	10.4M 163.6E	PCN 6	T4.0/4.0 /00.5/23HR4	DMSP35 : DMSP37		PGTW PGTW
27	040006	11.05 162.4E 11.14 161.7E	PCN 1	144074*0 100*3/53HK	DMSD35		PGTW
28	040923	11.84 160.0E	PCV 2		DMSP37		PGTW
29	256040	11.9N 159.7E	PCN 2		DMSD36		PGTW
30	061247	12.2N 150.2E	PCN 2		DMSP35		PGTW
31	041353	12.44 15A.1E	PCN 1		DMCD37		PGTW
35	045502	12.5N 157.9E	PCN 1	T5.0/5.0 /D1.0/26HR			PGTW
33	042348	12.4N 157.4E	PCN 2		045635		PGTW
34 35	070350 070504	12.4N 157.0E 12.3N 156.3E	PcN 2		GOFS7 DMSP37	CLUP	PHIK
36	071019	12.5N 155.BE	FLM Z		GOFS3	CI OF	PGT# PHIK
37	071047	12.4M 155.7E	PCN 2		DMSP36		PGTW
38	071230	12.4N 155.3E	PCN 2		DMSP35		PGTW
39	072147	12.2N 153.2E	PON 1	T6.0/6.0 /D1.0/24HR			PGTW
40	040115	12.24 152.5E	PCN 1		DMSP35		PGTW
41 42	3560¤0	12.04 151.2E	PCN 5		DMSP37 DMSP37	THE THE	PGTW
43	091029	12.0N 152.1E 12.0N 151.0E	PCN 6 PCN 5		AFGPMG	INII 392	RODN Pgiw
44	0a1353	11.9N 150.1E	PCN 2		DMSP35		PGTW
45	092025	11.9N 14R.6E	PCN 5		DMSP37		PGTW
46	040054	11.9N 147.5E	PCN 4	T4.5/5.5 /41.5/27HR4	DMSP35		PGTW
47	090906	12.3N 145.7E	PCN 6		DMSP37		PGTW
48	091011	12.3N 145.7E	PCN 6		DMSP36		PG <u>T</u> W
49	0-01-335	12.0N 145.2E	Pen 6	-3	0MSP35		PGTW
50 51	092254	11.9N 147.3E 12.0N 147.6E	PCN 1 PCN 1	T3.5/4.5 /W1.0/23HR	DMSP36		PGTW PGTW
52	100946	12.4N 140.2E	PCN 6		DMSP37		RODN
53	100946	12.2N 140.9E	PCN 6		DMSP37		PGTW
54	101136	12.2N 140.4E	PCN 1		DMSP36		PGTW
55	101317	12.2N 140.1E	PCN 2		DMSP35		PGTW
56 57	102127	12.3N 139.3E	PCN 1	T4.0/4.5 /W0.5/19HR9			RPMK
57 58	102127	12.3M 139.3E	Pon 2	T3.5/3.5 /S0.0/23HR	7,592MG 1,592 1,59		PGTW
59	110159	12.3N 139.1E 12.7N 138.7E	PCN 1		DMSP35		PGTW PGTW
60	111008	12.9N 13A.0E	PCN I		DMSP37		RODN
61	111008	13.0N 13A.0E	PCN 1		DMSP37	Cl UP	PGTW
62	111118	13.04 137.8E	PCN 2		DMSP36		PGTW
63	111441	13.3M 137.7E	PCN 1		DMSP35		PGTW
64 65	112107	13.6N 137.5E	PCN 2 PCN 2		DMSP37 DMSP37		PGT# RODN
66	112518	13.7N 137.4E 13.6N 137.1E	PCN 2	13.5/3.5 /S0.0/25HR			HOUN PGTW
67	120141	14.0M 137.1E	PCN 1	T4.0/4.0 /S0.0/2RHR	DMSP35		RPMK
68	120141	13.9N 137.1E	PCN 1	, 5000, 5000	DMSP35		PGTW
69	120948	15.2N 136.6E	PCN 6		DMSP37		RPMK
. <u>7</u> 0	120949	14.9N 136.3E	PCN b		DMSP37		PGTW
71	171100	15.0N 136.2E	PCN 6		DMSP36		PGTW
72	121423	15.1N 136.4E	PCN 4		DMSP35		PGTW
73 74	122343	15.4N 136.6E	PCN 5 PCN 3	T3.513 5 450 0434100	DWSP37 DWSP36		PGTM
* 75	130928	15.4N 136.7E 16.7N 137.5E	PCV 4	T3.5/3.5 /S0.0/26HR	DMSP37		PGTW PGTW
* 76	130329	16.7N 137.6E	Prn 2		DMSP37		RODN
<ul><li>77</li></ul>	131042	16.9N 137.7E	PCN 6		DMSP36		PGTW
78	131405	14.3N 137.4E	PC4 6		DMSP35		PGTW

- 79	132028	18.2v 14n.1E	PCN 6		DMSP37	RODN
60	132028	16.1N, 136.1E	PCN 5		DMSP37	PGTW
81	132325	16.1N 136.6E	PCN 5	T2.0/3.0 /W1.5/24HRS	DMEDSK	PGT#
		16.0N 136.4E			DMSPRS	PGTW
* B3	140909	17.4N 140.7E	PCN 6		DMSP37	RODN
B4	140909	14.2N 135.4E	PCN 6		DMSP37	PGTW
85	142307	17.1N 137.1E	APCN 3	T1.0/2.0 /W1.0/24HR9	DMSP36	PGTw

## ATRCHAFT FIXES

Fix NG.	TTME- (7)	F1X P051TION	FLT LVL	70043 HGT	DBS MSLP		-SFC- /RRG/						ACC VAAA		EYE Shape		PRIEN- FATION			MP (C) / DP//SST	45N NO+
1	0>0115	5.3N 168.5E	1500F F		986	65	180	35	220		180	35		2					+25		1
5	021250	6.5N 167.6E	700MB	2949	984				n e n		290	30	12	5				+12	+15		2
3	030053	7.2N 168.0E	700MB	2973			150	15	510		150	24							+16		3
•	030310	7.7N 168.3E	700MB	2934	982		060	4.0	160		000	35	2	2					+15		3
5	040510	9.3N 167.8E	700MB	2947	983	55	310	45	050		310	45	2	4					+17		6
6	041523	9.5% 166.2E	700MH	2931	983				310		200 040	40	•	5				+11	+11		7
7	051302	10.3N 163.3E	70048	2847	972				130			30			CIRCULAR	3-			+15		10
9	051423 060259	10.4N 163.1E	700MH	2825 2807	969		240		100		100 340	50 50	10	3	ELLIPTICAL	35	010		+15		10 11
10	061213	11.5N 161.0E	700MH 700MH	2763	968 963	35	340	19	120		630	23	-	•	CELTAITORE	30 60	010	+10	+14		15
11	061427	12.2N 159.0E	700MB	2762	961				040		300	in	4	5	ELLIPTICAL	26 15	030	.12	+15		12
12	070008	12.3N 157.6E	70048	2674	401				114	90	300	Į.,	4	6	CELLICAC	29 13	030	₩12	+15	-13	13
13	070256	12.4N 157.0E	700MB	2646	949	0.0	010	20	170	102	040	20	ũ	Ä	CIRCULAR	27		412	+19	+13	13
14	071407	12.5N 154.7E	700MB	2541	937	50	0.10	60	170		090	24	15	4	CIRCULAR	17			+19		14
15	071820	12.2N 154.2E	700MB	2479	930				070	126		14	•						+21		14
16	072040	12.2N 153.5E	700MB	2477	928	100	330	. 5		105		15	15	2	CIRCULAR	15		+15	+24		14
17	010080	12.2N 152.BE	700MB	2544	938	100	170		170	115	140	30							+55	+12	15
18	745080	12.1N 152.4E	700MH	2537	935	130	060	20	140	115	060	10	5	4	CIRCULAR	15		+13	+50	+12	15
19	206180	12.2N 149.8E	700MH	<b>269</b> 0	954	-		-	120	60	0.40	30							+24	+ B	16
20	0a150B	11.9N 149.6E	700MH	2743	957				040		360	21	3	5	ELLIPTICAL	25 15	020		<b>65</b>		16
21	015519	11-AN 14A-1E	70 <del>04</del> 8	2173	964		250	1-0	330		<b>27</b> 0	60	4	*	CIRCHLAR	30			+53		17
55	000505	11.9N 147.4E	700MB	2771	964		180	10	630			10	4	4	CIRCILLAR	30		+11	+53		17
23	000501	12.1N 146.6E	700MB	2845		85	510			107		14							+53		18
24	040940	12.14 146.1E	700MB	2857	974				0.00		230	Su	5		C   CC   1 AC				+55		18
25	091434	12.1M 144.8E	700MH	2849	973		- 0 0		140		040	1R		4	CIRCULAR	35			+19		19
56	092054	33.F41 NT.EE	700MH	2842	970		030	50	110		040	30	5		ELLIPTICAL	25 18	D40		+15	+10	50
27	100445	12.3N 141.8E	710MB	2804	965	65	090	Š0	150		090	10	4	S	CIRCIJLAR	20			+18		21 23
28 28	101742	12.3N 130.2E	7n0m8 7n0m8	2689 2646	953 949				350 060		33D 580	16 3n	_	4	CIRCIILAR	17		+12	+19		23
30	102105 110210	12.3N 139.ZE	7 n D M H	2609	943	0.5	360	15		105		30		5	CIRCULAR	13		.19	+21		23
31	111245	13.3N 137.6E	70048	2597	743	50	,,,,,	15		B0		15	•	,	CIRCULAR	1,		-11	+15		24
32	111530	13.3N 137.3E	70046	2563	938				090		340	15	10	5	CIRCULAR	10		419	+21		24
33	170104	13.9N 137.1E	700MB	2073	930	120	150	8		110		15		•	D-110()&A11	117		*15		+10	25
34	120254	14.0N 137.0E	700MB	2625	946	150		Ä		iio		15	4	3	CIRCULAR	12		411	+22		25
35	121459	14.9N 136.5E	70048	27B9	965			٠	130		050		5	5	CIRCULAR	10			+15		56
36	121804	15-1N 136-5E	700MB	2766	963				120		090	0				•					26
37	122013	15.2N 136.7E	700MB	2761	961				100		360	7	10	3	CIRCULAR	13		+11	+17	+11	26
38	130028	15.4N 136.8E	700MB	2859		40	030	35	110		030	18	-						+53		27
39	130253	15.7N 136.7E	700MB	2925	977		090	15	0.00		340	60	5	2	CIRCULAR	10		+12	+19		27
40	131559	16.1N 137.2E	700MB	2959	985			-	170	67	100	50							+19		58
•1	131517	16.3N 137.ZE	70048	3017	989				040		580	30	5	5				+13	+50		58
42	140004	16.5N 136.7E	710MB	7126	1005		330	50	160		040	60							+18		29
43	140308	16.1N 136.2E	700MB	7145		30	350	70	140	35	370	90	5	5				+14	+15	+ +	29

#### RAJAR FTES

Flx	TTME:	FIX			EYE	EYF	RADOS-CODE		RADAR	SITE
NO.	(7)	POSTTION	RADAR	ACCHY	SHAPE	DIAM	ASWAR TOOFF	COMMENTS	POSTTTON	WMO NO.
1	030330	7.7N 16A.2E	LAND	POOR				PSBL CNTR	8.7N 167.7E	91366
ž	030620	4.4N 168.0E		PhOR				PSBL CNTR	8.7N 167.7E	91356
3	030730	4.2N 168.2E		FAIR				PSBL FYF	8.7N 167.7E	91366
4	030830	8.5N 168.2E		FAIR				PSBL CNTR	8.7N 167.7E	91366
5	030930	8.5N 168.ZE		POOR				PSBL CNTR	8.7N 167.7E	91366
6	031130	4.6N 164.PE		POUR				PEBL CNTR	8.7N 167.7E	91366
7	032230	9.1N 167.7E		FAIR				PEBL CHTR	B.7N 167.7E	91366
В	040130	9.3N 167.4E		POOR				PSBL CNTR	8.7N 167.7E	91366
و	040530	9.44 167.6E		POOR				PSBL CNTR	B.7₩ 167.7E	91366
10	040730	9.4N 167.6E	LAND	6200				PSBL FYF	8.7N 167.7E	91366
11	040900	9.6N 167.5E		GOOD				PSBL FYF	8.7N 167.7E	91366
12	040830	9.5N 167.5E		Gn00				PSBL FYF	8.7N 167.7E	91366
13	040900	9.5N 167.2E		GOUD				PSHL FYF	8.7N 167.7E	91366
14	040930	9.5N 167.1E	LAND	FAIR				PSBL FYF	8.7N 167.7E	91346
15	041000	9.5N 167.1E	LAND	FAIK				PSHL FYF	8.7N 167.7E	91366
16	041100	9.5N 166.9E	LAND	POUR				PSBL CNTH	8.7N 167.7E	91346
17	041130	9.5N 166.BE	LAND	POUR				PSBL CNTR	8.7N 167-7E	91366
18	090435	12.3N 146.HE	CAND	POJR				WALL FIR VSB SSW-NNE	13.6N 144.9E	81510
19	090510	12.3N 144.7E		POUR					13.6N 144.9E	91218
20	090535	12.3N 144.7E		POOR					13.6N 144.9E	91218
21	090610	12.3N 144.5E		POUH				WALL OUD VSBL SW-N	13.6N 144.9E	91218

22	090535	12.2M 146.4E	LAND	PauR		WALL CLO VSBL SSW-N	13.6N 144.9E	91218
23	000705	12.34 146.3E		PhOR		WALL CLD VSBL SSW-NNF	13.6N 144.9E	91516
24	090735	12.34 146.ZE		PhOR		WALL OLD VSBL SSW-W	13.6N 144.9E	91218
25	090505	12.4N 146.2E		POR		WALL CID VSBL SSW-NNW		
							13.6N 144.9E	91218
26	090835	12.34 145.BE	LAND	FAIR		WALL CLO SSW+NNE	13.6N 144.9E	91518
21	090910	12.3N 145.BE	LAND	PoDR		WALL CLD W-N	13.6N 144.9E	91218
28	090935	12.4N 145.7E	LAND	FAIR		WALL FLD SW-N	13.6N 144.9E	91218
.24	01010	12.4% 145.7E	LAND	PhOR		WALL CLO SSW-N-NNE	13.6N 144.9E	91218
30	091035	12.3V 145.7E	LAND	FAIR		WALL CLO S-N-NE	13.6N 144.9E	91218
31	091105	12.4N 145.5E		FAIR		WALL CLO S-NNE-NF	13.6N 144.9E	81516
35	nq1135	12.3N ]45.3E		FAIR		WALL CLO S-N	13.6N 144.9E	91218
33	041205	12.3N ]45.3E	LAND	GNUD		WALL SSW-NNE	13.6N 144.9E	91218
34	0:1235	12.7N 145.2E	LAVD	F41K		WALL S-NW	13.6N 144.9E	9121B
35	091310	12.7N 145.0E	LAND	6n0u	26	GOOD ETP WALL CLO OPEN ELSSW	13:64 144.95	+1218
36	091335	12.34 144.9E	LAND	Gn00	20	GOOD CIR WALL CLD DPEN ENE-S-SH	13.6N 144.9E	91218
37	091410	12.34 144.8E	LAND	FAIR		HVY ATTFNUATION	13.6N 144.9E	91218
38	091435	12.4N 144.7E	LAND	FAIR		HVY ATTENUATION	13.6N 144.9E	41218
39	091510	12.4N 144.7E		FAIR		HVY ATTENUATION	13.6N 144.YE	91218
41)	091535	12.44 144.6E	LAND	FAIR		HVY ATTENUATION	13.6N 144.9E	91218
41		12.44 144.5E	LAND	FAIR		HVY ATTENUATION	13.60 144.9E	41218
	001510							
42	091635	12.3N 144.4E	LAND	FAIR		HVY ATTENUATION	13,6₩ 144.9€	91218

#### TYPHOON BESS

# RATELLITY FIXES

FIX NO.	TTME (7)	FTX POSTTTON	<b>ACCRY</b>	DVORAK CODE	51	ATF() TTL	c	) MMFNTS	<b>i</b>		SITE		
i	161109 180043 184315 191157 191306 194103 104258 200148 200148 201480 20	2.0N 148.5E 3.0N 144.0E 10.0N 145.6E 10.5N 142.5E 10.5N 142.8E 10.4N 142.8E 10.4N 142.8E 10.4N 142.8E 10.5N 141.2E 10.5N 141.2E 11.5N 142.2F 11.5N 130.4E 11.5N 130.4E 11.5N 130.4E 11.3N 134.4E 11.3N 134.4E 12.5N 137.5E 13.1N 137.5E	PC0 N N D D D D D D D D D D D D D D D D D	T0.0/0.0 T1.5/1.5 /01.5 T2-5/2.5 /01.0 T1.5/1.5+	/23HRs /22HRs	OWENTA DWEDTH DWEDTH DWEDTH DWEDTH DWEDTH DWEDTH DWEDTH DWEDTH OWENTA OWENTA OWENTA OWENTA OWENTA OWENTA OWENTA OWENTA	INII	)4S			PGTW PGTW PGTW PGTW PGTW PGTW PGTW PGTW		
21 22 23 24 25 26 27 28	220112 221104 221353 221353 222144	11.34 138.7E 13.9N 136.9E 13.9N 136.9E 13.9N 136.3E 14.6N 136.0E 15.0N 136.1E 16.0N 136.1E 16.0N 134.9E	6 PCN 6 PCN 4 PCN 3 PCN 1 ECN 3 ECN 3 ECN 3	T4-0/4-0 /00-5		DWSP37 DWSP36 DWSP36 DWSP36 DWSP36 DWSP36 DWSP36 DWSP37	INI	J#S			RODA PGTW PGTW RODA PGTW PGTW PGTW PGTW PGTW		
29 30 31 32 33 34 35 36 47 38	272346 210235 210235 211025 211228 211217 211517 211517 212125 212328 240216	16.04 134.9E 16.5M 134.9E 16.3M 135.1E 17.5M 136.7E 17.9M 136.3E 17.9M 136.4E 19.1M 136.5E 19.1M 137.7E 14.3M 137.9E	PCN 1 PCN 2 PCN 2 PCN 4 PCN 3			OMEDIAN DMEDIAN DMEDIA DMEDIAN DMEDIAN DMEDIAN DMEDIAN DMEDIAN DMEDIAN DMEDIAN DMEDIAN DMEDIAN DMEDIAN DMEDIAN	INII	Jas			PGTH PGTH PGTH PGTH RKSO RPMK PGTH PGTH PGTH RPMK		
40 41 42 43 44 45 46 47	240217 240217 241005 241005 241210 241317 242104 242105	19.7N 13A.9E 19.9N 13A.5E 21.20 140.1E 20.3N 140.0E 21.3N 140.8E 21.5N 141.3E 23.7N 141.8E 23.7N 145.1E	PCN 5 PCN 5 PCN 5 PCN 5 PCN 5 PCN 5 PCN 5	13.0/3.0	0/24HRS	DMSP35 OMSP37 OMSP37 DMSP37 DMSP35 OMSP35 OMSP37	CI DO				RKSO PGTW RKSO PGTW PGTW PGTW RKSD		
					61	#Chwei +	[ XES						
FIX NO.	T +ME (7)	ETX POSTTION	FLT I VL	700WR OBS M MGT MSLP V	&X+SFC-# EL/HRG/R	140 MPX-	FLT-LVL VEL/8HG	-#NU -#NU	ACCRY IAV/MET	EYË SHAPE	FYE ORIEN- DIAW/TATION	HYF TEMP (6	
1 2 3 4 5	200259 200330 200855 201200 201433 210213 211500	10.50 141.1E 10.70 140.8E 10.60 140.3E 10.60 130.8E 10.90 130.6E 11.90 138.5E 13.10 136.1E	1500F1 700MB 700MB 700MB 700MB 700MB 700MB	3088 1001 3101 1002 3090 1004 3032 994	35 300 30 050 35 340	\$0 0611 50 130 250 360 360 50 070 170	50 300 30 050 23 160 32 310 46 340 61 080	n 22 n 30 n 60 n 150	7 5 5 10 5 10 5 13 5 4 2 5	CIRCULAR	3n	+24 +26 +23 +17 +12 +10 +11 +11 +11 +11 +13 +13 +12	1 2 2 4 5
8 9 10 11 12 13 14	211744 212006 220320 220025 220607 220835 221842 232122	13.3N 135.6E 13.3N 135.6E 14.4N 135.0E 15.2N 134.6E 17.1N 135.2E 17.4N 135.4E 14.4N 135.4E 14.4N 137.3E	700MH 700MH 700MH 700MH 700MH 700MH 700MH 700MH	2945 984 2922 981 2819 969 2764 963 2731 959 2747 961 2841 372 2863 974 1	75 090 55 130 80 120 70 140 20 270 10 310	220 30 180 45 200 15 070 10 200 140	63 156 90 136 69 146 78 346 128 146 63 136 110 236	0 40 0 60 0 30 0 25 0 15 0 20	10 5 2 2 2 2 4 2 4 2 7 2	CIRCILLAR ELLIPTICAL CIRCIJLAR CIRCILLAR CIRCILLAR CIRCIJLAR	30	+14 +14 +11 +13 +17 +11 +20 + B +10 +19 + 4 +10 +21 +14 +24 + 4	5 7 8 9 10 10
17	240819	2n.RN 139.8E	7n0mB	2999 990 1	00 310	10 280	86 17	u jn	2 10			+ H +15 +10	11
					P	AJAN FTYE	s						
	T#ME (7)	F14 P051T10H	РАСАН	ACCHY SHAPE	EYF DI 6		-CODE		•	COMMENTS		HADAR POSITION	GITF WWO NO.
1	21,1200	12.7N 136.9E	SHIP	G100				NUA	G NW AT	6 ANOTS		13.1N 137.3E	үнү

#### TYPHOON CECIL

# SATERIAN FIXES

FIX NO.	TTME: (7)	FTX POSTTION	ECCAY	DAJSWK CODE	SATFILITE	CJAMENTS	SITE
1	072225	3.0V 143.6E	Prn 5	TU•0/0•0	OMSO JA	INII JAS	PGTW
2	0 a 2 3 + 9	3.44 143.6E	PCN 6	TU.0/0.0 /50.0/25HRS			PGIW
£	092331	5.14 141.7E	PCN 6	T1.0/1.0 /D1.0/24HRs			PGT#
4 5	101212	6.3N 140.0E	PCV 6	#1 5 c 5 co = 12.40=	DHEBAK		PGTW
6	110910	6.4N 139.0E 6.4N 13R.BE	PCN 5	T1.5/1.5 /00.5/24HR	DWGP34 DWGP37		PGTW
7	110911	5.9N 13R.3E	PCN 6		0MSP37	INTE DES STORM ON EDGE OF DATA	PGT# RODN
9	111155	6.3N 13A.5E	PCN 5		DMSP34		PGTW
9	111434	5.3N 138.3E	PCN 6		DWSD 35		PGTW
10	111434	5.5N 139.4E 7.0N 137.6E	PCN 5	T3.0/3.0 /01.5/23HRS	Duspa4 Duspa7	INII 398	RPMK
15	112256	7.0N 137.4E	PCV 5	1000// 100 ///103/23/6/	DACESA		PGTW PGTW
13	1 > 0 1 3 4	7.04 136.1E	PCN 5	73.0/3.0	DAGPIS	INII JOS	RODN
14	120134	7.14 136.8E	PCV 5	-5	DMSP35		PGIW
15	120135	4.7N 136.6E 6.9N 136.7E	PON 5	T3+0/3+0+	DMCD34	SPC 11N1	RPMK
17	121416	7.0N 135.8E	PoN 5		045035		PGTW RODN
18	122131	7.14 135.6E	PCN 5	T3.0/3.0 /50.0/24HRS			PGTW
19	130020	7.4M 134.5E	PCN 3		DMSP34		PGTW
20	1 30 25 6	7.6M 134.4E	PCN 3		0M4632		PGIW
55	11011	7.9V ]37.8E 4.1N [37.6E	PCV 6		DMSP34		PGTW
23	131357	H. 24 133.2E	PCN 5		DMSP 15		PGTW PGTW
24	131356	8.0N 133.2E	PCN 6		DMSP35		RODN
25	131358	4.3M 132.9E	PCN 5		DMSP75		RPMK
26 27	140002	4.34 137.2E	PCN 3	T3 543 5 400 5434HPc	DMSP36		PGIW
28	140239	4.14 131.5E 4.44 131.1E	POVI	T3.5/3.5 /00.5/26HRC	DMCD3H	Sec 11ml	PGTW RODN
29	140239	4.1N 131.1E	PCN 3		DMSP35	1	PGTW
30	140239	9.2N 131.1E	PCN 3	r3.5/3.5	DMSP35	INII Jas	RPHK
35	140952	8.4N 129.4E	PCN 6		DWSDA7		PGTW
33	141243	4.5N 120.2E	PC4 6		Decase		PGTW
34	141521	4.54 128.6E	Pri 5		DMSP35		PGTW ROUN
35	141521	9.5N 129.6E	PON 5		DWSP 15		RPHK
36	142233	9.2N 128.0E	PCN I	T4.5/4.5-/01.0/23HRS			PGTW
37 38	142344	9.4N 127.5E	PCN 1 PCN 1		Duspak Duspas		PGTW
39	150221	3.9N 127.1E	PCN 1	T4.5/4.5-/01.0/24HRS			PGTW RPMK
40	140932	10.6N 125.6F	PCN 1		DHSP37	SPLIT PARS	PGTW
41	151225	10.74 125.6E	PCN 3		Duchar		PGTW
42 43	151502 151502	11.50 124.7E	Prn 1 Prn 3		Duspas		PGTW
44	142213	11.50 124.7E 11.84 123.5E	PCN 3	T4+0/4+5 /H0+5/2+HRS	045075 045077		RODN PGTW
45	152213	11.7N 123.4E	PCN 5	T3.0/4.0 //1.5/20HRS		•	RPMK
46	140203	30.FSI NO.SI	PCN I	T4.0/4.0	DMCP35	INII Jas	RODN
47 48	140203	12.14 121.0E	PCN 3		DMSP35		PGT₩
49	140203 141053	11.9N 123.0F 12.7N 122.4E	PON 5		DMSP35 DMSP37		RPMK
50	141053	12.3H 122.5E	PCN 2		DMSP 17		PGT# RODN
51	141053	12.5N 122.5E	Pow b		DHSP 17		RPMK
52 53	141509	12.7m 122.2E	PCN 3	the state of the state of	DMSP 36		PGTW
54	151444	12.7N 122.2E 12.7N 122.0E	PCN 3		DMSP35		RODA
55	162153	12.84 121.9E	Pon 1	T4.0/4.0 /50.0/24HRS	DMSP37		PGTW PGTW
56	142153	12.9M 122.DE	PCN L	T4.5/4.5 /01.5/23HHS	OMSP 17		RPHK
57	170050	12.4M 122.3E	PCN 1	T4.5/4.5+/00.5/22HRC	AF GOMG		ROUN
58 59	170326	13.2N 122.2E	PCV 1		DMSP35		RPMK
60	171033	13.9N 122.3E 13.7N 122.5E	PON 2		DMSP37 DMSP37		RPMK PGTN
61	171332	13.9N 127.4E	PCN 1		DWCDAY		RODN
62 63	171426	13.94 122.4E	Pow 1		DMSP35		PGTW
64	171508 171608	14.1N 122.4E 13.9N 122.3E	PCA 5		Dwgp35		RPMK
65	172133	14.34 122.HE	PCN 5		DMSPR7	N/A DUE TO TERMINATOR	RODN PGTW
66	180032	14.5N 123.1E	PCN 3	T2.5/3.5 /WI.5/26HRG	DMSP36		PGTW
67 68	190308	14.9N 123.2E	Pon 3	T3.0/6.0+/4].5/3nHRc	DMSP35		RPMK
69	190308	14.5N 123.2E 15.4N 124.2E	PON 3 PON 3	T3.0/4.0 /wl.5/26HRs	044P75 044P77		RODN
70	191314	14.7N 123.7E	PCW 5		DMSP34		PGTW RODN
71	181549	15.7N 124.6E	PCN 5		DMSP35		RPMK
72	181549	15.5N 124.7E	PCN 4		Duchse		RODN
73 74	190014	14.8M 125.1E	PCN 3	T3.5/3.5 /D1.0/24HRS	045936		PGTW
75	190249	17.1N 125.2E 17.2N 125.7E	PCN 3	T3.0/3.0 /50.0/24HRs	Dwsp35		PG1#
76	190953	17.7N 124.5E	PCN 6		DMSP 17	CI SAME	PGTW
77	191531	18.5N 127.2E	PCN 6		DMCB34		RODN
75 79	191531 192357	14.3N 127.6E 21.1N 129.0E	Prn 6 Prn 5	72 man =	Duces	That I had	PGTW
80	192357	20.9N 120.0E	PCN 5	T2.5/2.5 T3.0/3.5 /WD.5/24HRS	DMSP34	INII Das	R004
61	200933	22.5N 132.0E	PCN 6	1-107 103 7 400 37 E011114	045637	CI nows	PGTw PGTw
82	201538	21.4N 133.7E	PÇN 5		DMCP36		RPMK
83 84	2u153B	27.9N 132.7E	PCN 6		DMCP36		PGIW
85	2n1513 2n1513	24.5N 134.6E 23.7N 134.5E	PCN 5		DMSP35		₽P#K
86	201513	22.9N 137.6E	POV		DMSP34		RODN PGT#
87	2n2338	22.9N 136.4E	PCN 5		DHEBAR	EXPUSED ILC SYSTEM DISSTPATED	PGTW

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#### ATTOMET ATTEN

	#13CHAFT FIXES																		
F1x NO+	TTME (7)	FTX 12051110%	£ <b>L T</b> 1 <b>V L</b>	700 43 HGT		MAX-	SFC- '∢RG/	₩ 40 ₩ 40	MAX-	FLI-	-FAF-	4NU	ACC NAV/	HF I	EYÊ SHAPE	EYE DRIEN- DOLFAT/WATC	UNITY THE SEND !		45N 40•
	1n2353	6.4K 130.7F	700MH		1000	30	290	5	240	30	120	30	4	4			+11 +16 +11	26	3
1		7.14 137.0E	700mH	305A	995		060	10	350		040	31	4	1	CIRCILLAR	12	+1.4 +15 + B		4
5	112129	4.94 134.6E	7n0***	3023	993		220	50	110		060	50	R	5			+13 +11		5
	120309	6.84 [36.4E	700MH	3030	995		180	10	210		100	30	3	5			+13 +14 +12		5
•	120900	7.3v 135.3E	700HB	3034	997		330	50	040	44	330	90	4	5	CIRCULAR	<b>4</b> ft	+10 +17 +10		6
-	130510	7.9N 134.2E	ZOOMH	1007	• • • • • • • • • • • • • • • • • • • •		090	5	170	35	000	30	4	5			+15 +12		7
6	130704	7. RN 137. HE	700MB		988		140	30	020	41	300	30	2	4			+11 +14 +14		7
į.	140304	4.2N 131.HE	700MH	2494	984		330	50	100	78	020	25	9	3	CIRCHLAR	50	+17 +17 +12		8
š	140520	4.4H 130.35	700MH	2939	985	98	070	8	NAI		Q7U	Я					-18 -11		9
Łú	140932	4.44 129.8E	760MH			90	160	10	A J D		3.10	15	12	10	C1RC( LAR	50	+1* +18 +12 +15 +15		10
11	141932	9.18 120.3E	7n0mH								000	25		_	0100 4 40		+11 +15 +11		10
16	142147	9.04 127.9E	7 n 0 MH		965	100		4	0.30		020	15	6	2	CIRCULAR	12	+13 +21 +10		14
13	150957	19.44 125.4E	7 n 0 M H	2800	966		150	8	080	90	320	16	2	3	CIRCHLAR CIRCHLAR	50 20	413 461 .10		íż
14	140950	12.4x 122.4E	790MB			50	0				300	10	3	5	CIRCILLAR	15	+ 3 + 3		14
15	152153	12.9h 122.1E	700mb		_				020		300	50	2	3	CIRCULAR	20	+13 +12		14
16	170344	11.24 122.3E	700MM	2937	982		090	10 8	070 050		320	25	5	2	CIRCULAR	21)	+11 +11		14
17	170649	13.3N 122.4E	700MH			50	090	В	360		090	10	á	Ś	CIRCULAR	20	+ H +10 +10		15
18	171546	14.14 127.6E	700Mh		976				240		160	30	ź	3	G 511.01, 51111		+11 +10		15
19	172005	14.24 122.98	7 10 MH	- 47-			360		240		240	Ξ.	. 1	1	CIRCILAR	10	. 7 .13 + 8		15
50	174510	14.64 123.0E	70048				150	10	280		150	15	Ġ				+19 +11		16
51	100747	15.20 123.AE	7n0MH 7n0MH		990		110	10	180		110	50	5		CIRCULAR	30	+14 +19 +11		16
22	101055	15.6% 123.9E	7n0m6	277h	770	33		• •	200		120	3n	5	5			+15 + 9		17
23 24	141910	14.54 124.4E	700MH	3002	989	35	240	50	300	64	240	30	5	5	CIRCIJLAR	25	+1m +15 + 9		17
25	190600	17.3N 124.0E	70040		7117		040	15	290	80	180	15	- 5		CIRCIJLAR	40	+15 + 7		18
26	190800	17.54 124.2E	700MB		986		120	25	260	70	120	25	5	R	CIRCIILAR	40	+13 +15 + 5		18
21	191958	20.1N 127.9E	700MP						በደብ		350	10				_	+11 +11		19 19
54	192030	25.5H 128.5E	700MH						250		160			10	CIRCILLAR	31	+10 +11 +11 +12 +11 +11		20
29		22.7N 130.9E	70041		1004	50	230	25	540	50	140	51	5	6			+15 +11 +11		
							1	PA JA	e FTX	£5									
FIA	TIME:	FIX			ΕY	F	EY	F	PANO								RADAR	911	
NU.	(7)	90STT109	PAGAR	VCCSA	SHA	PE	DI.	A M	ACMA	H TE	)UFF				COMMENTS		POSTTTON	HM0	٠.
												_	_				15.2N 120.6E	983	227
1	142200	13.34 122.2E		PODR	CIRC			19				Ev	IRAL	BAN	an.		15.2N 120.6E	983	
5	142230	13.4H 121.7E	LA√D	POUR	CIRC			19					TRA				15.2N 120.6E	98	
3	142305	13.24 121.9E		PoDK	CIRC			19					IRAL				15.2N 120.6E	98	327
4	[62335	13.3H [21.9E		POUR	CIRC			1 R 1 7					IRAL				15.2N 120.6E	983	327
5	170003			POOR	CIRC			7?					IRAL				15.2N 120.6E	98	327
ь	170030	13.3N 121.8E		GOUD	CIRC			13									15.2N 120.6E	98	
7	170455	13.3N 122.3E		6า00 6า00	CIRC			13				SF	IRAI	BAN	4D		15.2N 120.6E		327
8	170530	13.5N 122.1E		6000	CIRC			14									15.2N 120.6E		327
	170503	13.5N 122.2E 13.5N 122.2E		6100	CIRC			14				ŞF	IRAI	RAN	HD CH		15.2M 120.6E		327
11	170700	13.7N 122.2E		6200	CIRC			15									15.2N 120.6E		327
15	170700	13.6M 122.4E		6100		PTICA	L					٤١	E A)	115 2	20/15		15.2N 120.6E		327 327
12	170905			GOUD	CIRC			1 R									15.2N 120.6E		327
1+	170330			FAIR	CIRC	HLAR		14									15.2 120.6E		327
15	171005		LAND	GODD		ULAR		12									15.2N 120.6E		327
16	171030	13.90 122.5E	LA∧ID	GUUD	CIRC	HLAR		17			3614						14.1N 123.0E		44 G
17	171100			- 05					105	,, ,	2014						15.2N 120.6E		327
18		13.94 122.58		GnOD		IILAR		15					t DA	avi	ERLAY		15.2M 120.6E	98	327
19				FAIR	CIRC	ULAR		15	1061	.,	1111	31	- 4 11 11	1,,,,			16.3W 120.6E	98	321
20	171200	13.7N 122.7E	LAND						1,,,,,	., ,							15 2N 120 65	~8	327

LAND

EVE 50 PCT ELLIPTICAL OPEN SW EVE CTROULAR UPEN

EYE ON PCT CIRCULAR OPFN E

98321 98440 98321

### TROPICAL STORM DOT

FIX	TIME						
NO.	(7)	FTX POSTT10N	ACCRY	DVDRAK CONE	CATELLATA	C Mariana	
		******		STITTE LONE	SATFLETTE	CJMMFNIS	SITE
1	0 = 155 =						
ځ •	041116	4.04 147.7E 4.28 142.3E	PON 5		DMSD34	Sec lini	PGT₩
3	042217	4.2N 147.6E	Pow 5		Duchay		PGľ₩
4	072138	5.5N 139.0E	PCN 5	TU.0/0.0 /SO.0/24HRS			PGTW
Ś	041525	4.04 135.0E	PCN 5	10007000 750agyEJHRC	DHChit		PGTW
6	042323	5.0N 134.1E	PCN 5	11.0/1.0 /D1.0/25HRS			PGTW
7	090147	5.1N 134.0E	PON 5		DMSP35		PGTW PGTW
9	090958	6.2N 137.4E	PON 6		DMSP37		PG I #
10	091504	7.2N 134.2E	PCV 5		DMSP3A		PGTW
ii	092059	7.4N 133.7E 7.3N 133.8E	PCN 6		DMCD32		PGIW
12	092305	7.9% 131.7E	PCN 5		DWSP37 DWSP3A	NOT AVAIL EDGE OF DATA	PGTW
13	100129	7.54 131.6E	PCN 5		DMSP35	NOT AVAIL EDGE OF DATA	PGT₩
e 14	100310	9.1N 130.0E	PCN 5	T1.5/1.5	Duspas	NUT AVAIT EDGE OF DATA INIT DOS	PGTW
15	100938	8.5N 129.8E	PCN 6		045017	111 0-3	RPMK PGTW
16	101146	8.9N 129.1E	PCN b		DMSP36		PGTW
17	101410	8.9N 12R.7E	PON 5		0wgp35		PGTW
1 s 1 9	101411	8.9N 127.6E	PCN 6		DMSPRS		RODN
50	102219	R. 9N 126.1E	PCN 5	-3	DMSP37	N/A OVER LAND	PGTW
21	150029	9.8N 126.8E 4.1N 125.7E	PON 5	T.2.5/2.5-/01.0/19HRs		44. 0	RPMK
22	110252	9.4N 125.5E	PCN 3		DMSP35	N/A DVER LAND	PGTW
23	110252	9.5N 125.5E	PON 3		DMSP35	N/A DVÉR LAND	PGTW
24	111059	9.9N 123.6E	PCN 6		DMSP37		RPMK RPMK
25	111100	10.0N 122.0E	PCN 6		DMSP37		RODN
26 27	111310	9.8N 122.9E	PCN 6		PLASMO		RPMK
* 28	111533	10.1N 122.8E	PCN 5		Duspas		RPMK
29	112159	9.7N 122.1E 10.2N 122.0E	Pon 5		DMSP35		ROUN
* 30	112159	10.6N 127.4E	PON 5	T1.5/2.5./W1.D/24HRS	DMSP37	N/A DJE TO TERMINATOR	PGTW
31	120011	10.7N 121.5E	PCN 5	T1.5/1.5	DMSP36		RPMK
* 32	120234	10.9N 121.2E	PCN 5		Duspas		PGTW
* 33	121039	11.5x 119.2E	PCN 6		DMSP37		PGTW
34	121040	10.5N 120-4E	PCN 6		DMSP37		PGT# Rodn
35 36	121252	10.7N 120.1E	PCN 5		PERSMG		PGTW
37	121515 121515	11.7N 119.6E	PCN 5		DHSP35		PGTW
38	122139	11.9N 119.4E 12.1N 119.4E	PCN 6		DMSP35		RODN
39	122139	12.1N 119.7E	PCN 5		Duspak Duspat	N/A DJE TO TERMINATOR	PGTN
40	122353	12.00 119.8E	PCN 5	T3.9/3.0+	DMSD47		RPMK
41	122353	12.1N 119.6E	PCN 5	T2+0/2+0 /DD+5/29HR5	DMSP36		RODN
42	130215	12.2N 119.9E	PCN 3		DMSP 35		PGTW
43	170215	12.34 119.8E	PCN 3		DMSP35		ROD∜ PGT⊌
44 45	131020	13.14 119.5E	PCN 4		DMSP37	CI UP BANDING FYE	PGTW
46	131020	13.1N 110.5E	PCN 4		DMSP37		RPMK
47	131457	13.1N 110.6E 13.5N 110.5E	PCN 1 PCN 3		DWCDJY	CI UP MARGED FYE	PGTW
48	131457	12.9N 119.3E	PCN 3		0#5835 0#5835	EYE HAJGFO	PGTW
49	132300	13.7N 120.1E	PCN 5		DHSP37		RPMK
50	132301	13.9N 120.1E	PCN 3	T2+5/3+0+/W0+5/24HRS	DMSP37		RPMK
51	140117	14.2N 12n.1E	PCN 3		DMSP3A		RODN Rodn
52 53	140117	14.04 120.3E	PCV >	T1+5/1+5+	DMSP36	INIT Jds	RPMK
54	140339	31.9N 120.1E	PCN 5		045935		RODN
54 55	141000	13.9N 120.3E	PCN 5		DMSP35		RPMK
	141000	14.1N 120.6E 14.0N 120.6E	PCN +		DMSP37		PGTW
57	141217	14.0M 121.1E	PCN 5		DMSP37		RPMK
58	141517	14.2N 121.0E	PCN 5		DMCD34	PSBL SECONDARY 14.0N 119.7E	RODN
	141439	14.3N 121.4E	PCN 5		DMSP35	SECUNDARY AT 14.5N 121.0E	PGTW
	141439	13.9N 121.0E	PCN 5		DAZES		PGT# RPMK
	142240	15.2N 122.5E	PCN b	TU+0/1.0-/w1.5/23HRs	DMCD37		RPMK
	142241	15.1N 122.3E	PCN 5	T1-0/S.0 /W1-5/24HRS	DMSP37		RODN
	150320	15.34 122.6E 15.2H 122.7E	PCN 5		AFUPMO		RODN
	150320	15.9N 123.2E	PCN 5	T1.0/1.5+/W0.5/26HRS	045235 045235		RODY
66	151121	14.2N 123.9E	PCN 3		DMSP35		RPMK
	151159	14.24 123.9E	PCN 5		PEASHO		RPMK
	151159	15.6N 123.8E	PCN 5		Duce 14		PGT₩ Rodn
	151420	16.4N 124.5E	PCN 6		DMSP35		PGTW
	152220 160041	16.9N 126.1E	PCN 6	T1+0/1+0	DMSP37	INII 792	PGTW
• •	170041	14.9N 126.4E	PCN 5	T1+0/1+0 /S0+0/25HRS	DWGDJK		RODN

### ATRCMAFT FIXES

	T TME (7)	£1X 20\$11∫98	FLT LVL		OBS MSLP										EYE SHAPE			RIEN- TATION			EMP (C) I/ DP/SST	usn ND•
1	120313	10.2v 120.5E	7n0MH	3090	2001	25	60	55	210	34	160	70	2	40					. 4	+10	+10	•
۲	130209	12.24 11R.9E							240												+10	5
Ŀ	132117	13.5% 170.0E			986	•			020	35	180	15	2	2	ELLIPTICAL	30	20	360			+10	6
4	140100	13.74 120.2E	700MB	2452		15	40	30	110	32	350	15	ŧ	2								6
ċ	140314	13.3N 120.5E	700MB	รูบ3รั		15									ELLIPTICAL	30	20	360	+ 4	+13	+12	6
ь	1=2120	17.24 125.58	1500F1			25	10	120	210	32	310	9.0	10	5						+24	+24	ь
1	12535	17.4N 125.58	700MH	3127	1004	25	40	40	160	58	240	30	1 n	H					+11	+11	+ 9	8

### RAJAH FTYES

10. 1x	T1ME (7)	FTX POSTTION	RAUAR	AECHY	EYF. SHAPE	EYF Dlam	MANUH-COUE ASWAH TOUFF	COMMENTS	HADAR Position	GITF WMO NO.
1	1 3 2 2 3 3	13.74 120.18	LAND	PODR	CIRCULAR	>n		PSHL CENTER	15.2N 120.6E	98327
2	132303	13.44 120.15	LAMO	POUR	CTRCIILAR	>0			15.2N 120.6E	98327
3	132330	11.94 120.1E	LAND	POR	CIRCULAR	20			15.2N 120.6E	98327
4	160033	13.9N 12n.ZE	LAHO	FAIR	CIRCILAR	>0			15.2N 120.6E	98327
5	140105	13.9N 120.2E	LA 40	FAIR	CIRCIILAR	>5		CHTR STARY SINCE LAST REPORT	15.2N 120.6E	98327
6	140135	13.8M 120.3E	LAND	FAIH	CTRCIILAR	25		•	15.2W 120.6E	98327
7	140205	13.9N 120.2E	LAMO	Falk	CTRCHLAR	25			15.2N 120.6E	98327
5	140235	13.94 120.3E	LAND	FAIR	CTRCULAR	25			15.2N 120.6E	98327
ý	140305	13.9N 120.3E		FAIR	CTRCULAR	25			15.2N 120.6E	98327
iu	140410	13.9N 120.6E		GOUD	CIRCHLAR	>5			15.2N 120.6E	98327
11	140432	14.0N 120.7E	LAND	ຣາບບ	CIRCULAR	25			15.2N 120.6E	98327
15	142346	14.5M 121.8E		POUR	CIRCULAR			EYE DIAM UNK	15.2N 120.6E	98327

### SYNDOTIC FIXES

	T 1 M E (7)	FIX POSTTION	INTENSTIY ESTIMATE	VEAREST DOTA (NM)	COMMENTS
2	170000	20.04 129.0E 22.34 133.0E 27.08 140.5E	25 25 25	120 60 60	

### TROPICAL DEPRESSION 05

### SATELL TIF FEXES

FLX NO.	TTME- (7)	FTX POSTTION	<b>ACCRY</b>	DVDRAK CODE	SATFI I TTE	COMMENTS	SITE
1	210311	18.3% 114.2E	PCN 5	T1.5/1.5	DMSPRS	INII Das	RPMK
5	220035	21.4× 118.0E	PCN 3	T1.0/1.0	DMSP36	INIT DAS	PGTW
3	220253	21.4N 118.3E	PCN 3	T1.5/1.5 /S0.0/24HR	DMSP35		RPMK
4	220253	22.1N 118.5E	PCN 3	T1.5/1.5	DMSP35	INIT DOS	RODN
ć	230018	22.0N 124.BE	PCN 3	T2.5/2.5-/01.5/24HR	DHSP36		PGTW
6	270235	22.2N 125.3E	PCN 4		DMSP35		PGTW
7	270235	22.0N 125.5E	PCN 3	T2.5/2.5 /01.0/24HR9	DMSP35		RODN
8	231055	22.5N 120.0E	PCN 3		DMSP37		PGTW
ÿ	231022	22.7N 12A.0E	PCN 3		DMSP37		RKSD
10	231259	22.9N 129.0E	PCN 3		D45P36	PSN BASEN ON CR BANDS	PGTW
11	231516	22.9N 129.7E	PCN 5		DMSP35		RODN
12	231516	23.2N 129.BE	PCN 5		DMSP37		PGT₩
13	232121	24.1N 132.0E	PON 5	T1.5/2.5 /#1.0/21HR9	DMSP37		PGTW
14	232121	24.4N 133.5E	PCN 5	T2+0/2+0	DMSP37	INII DUSZUPR LVL	RPMK
15	240000	24.9N 132.7E	PCN 5		DMSP36		PGTW
16	240216	25.4M 133.1E	PCN 3		DMSP35		PGTW
17	240216	25.1N 133.8E	PCN 3	71.n/1.0	DMSP35	INI DOS	RKSO
18	241000	27.7N 134.0E	PCN 5		DMSP37		PG1W
19	241005	35.7E NO.RS	PCN 5		DMSP37		RODN
20	241002	27.1N 136.0E	PCN 5		DMCD37		RKSO

# RAJAR FIXES

	TTME.	FTX POSTTTON	RADAR	ACCHY	EYE SHAPE	EYF DIAM	RADOB-CODE ASWAR TOOFF	COMMENTS	RADAR Position	SITE
1	230200	22.2N 125.1E	LANO				21872 50511		24.8N 125%3E	47927
ē	220200	22.2N 125.1E					10823 50716		24.3N 124.2E	47918
3	230400	22.3N 125.7E					21812 50914		24.8N 125.3E	47927
4	230400	22.3M 125.7E					20942 50812		24.3N 124.2E	47918
	230500	35.4N 154.0E					10872 50816		24.8N 125.3E	47927
6	230500	22.4N 126.0E					35/41 50819	•	24.34 124.2E	47918
7	230600	32.4N 124.2E					22912 50814		24.8N 125.3E	47927
B	230600	22.4N 124.2E					20781 50911		24.3N 124.2E	47918
9	270700	22.5N 126.6E					24842 50822		24.8N 125.3E	47927
16	270800	22.5N 126.9E					24811 50816		24.8N 125.3E	
ii	271500	23.64 129.5E					7//// 40522		26.14 127.7E	7937

# SYNOPTIC FIXES

FIX	T1ME	FTX	INTENSITY	NEAREST	COMMENIS
NO.	(7)	POSITION	ESTIMATE	DATA (NM)	
		18.0% 114.0E 20.0% 115.0E	15 15	60 60	

#### TYPHOON ELLIS

FIX NO.	TYME:	FIX	ACCRY	DVDRAK CODE	SATFII TTE	CUMMENTS	SITE
40.	(7)	POSTTION	401.41	DANAME COOF	74171111	00 MP 413	•,
1	260019	5.9N 139.3E	PCN 5	T0.0/0.0	AFRANG	INI 20C IINI	PGIW
ź	241119	8.0N 141.7E	PCN 5	19.070.0	DMSDAK	1	PGT
3	261441	8.9v 139.0E	PCN 6		DUGUAS		PGT₩
4.	270001	9.0N 140.4E	PCN 6	TU.0/0.0 /S0.0/24HRS	Duspa4	POSSIBLE SECONDARY 10.8N 139.4E	PGT₩
5	270200	8.7N 140.3E	PCN 6		DMSHJS		PGT₩
6	270847	8.6N 139.5E	PCN 5		DMSP37		PGTW
7	271102	8.7N 139.4E	PCN 6		DMSD34		PGT# PGT#
8	272128	11.3N 13R.9E	PCN 6		DWGP47 DWGP46		PGT#
9	272343	11.6N 138.7E	PCN 5		D#5235		PGTW
10 11	290141 291008	11.8N 13A.6E 12.1N 13A.4E	PCN 6		DM5P37		PGTW
15	2A1225	12.94 13A.6E	PCN 6		DMSP36		PGTW
13	291423	13.2N 13A.7E	PCN 6		DHSP35		PGTW .
14	ZA2325	12.5N 136.0E	PCV 5	T0.0/0.0 /S0.0/25HRS	DMSP36		PGTw
15	291208	12.9N 133.6E	PCN 6		DHChav		PGTW
16	292307	13.7N 135.ZE	PCN 5	T0.0/0.0 /50.0/24HRS	DMSP36		PGT₩ PGT₩
17	3n1150	13.7N 132.6E	n		DMSD36		PGT
18 19	301346	13.8v 132.3E	PCN 5	T1.0/1.0 /01.0/23HRS			PGTW
20	3n220B	13.7N 132.7E	PCN 6	11407[10 70140723001	DMSP34		PGTW
21	010227	13.2N 131.5E	PCN 5		DM5P35		PGTW
55	010227	12.9N 131.3E	PCN 5	12.0/2.0	045035	Sec Jini	RPMK
23	011050	13.7N 131.0E	PCN 5		DMSP37	CI UP	PGTW
24	011050	13.8N 130.9E	PCN 6		DMSP37	UPR LVL OUTFLOW	RODN
25	011313	13.9N 130.7E	PCM P		DWEBSY		PGTW
56	011313	13.7N 13n.7E	PCN 6		DWSP36 DWSP36		RODN PGTW
27 28	011509	13.9N 130.2E	PCN 6 PCN 5		DMSP35	UPR LVL ANTI/RANDING	RPMK
29	011509 012148	13.6N 130.1E	PCN 5		DUSP37		RPMK
30	050013	14.5N 129.1E	PCN 5	T3.0/3.0 /D2.0/26HRS			PGTW
31	050137	16.4N 125.0E	PCN 1	14.5/4.5 /DO.5/24HRS	DMSP39		RODN
32	020155	14.1N 12A.3E	PCN 5		DMSP39		RPMK
33	0>0209	14.5% 12A.1E	PCN 3		DMSP35		PGTW
34	602000	14.5N 128.5E	PCN 5	_	DMSP35	**** ***	RPMK
35	020209	14.4N 12A-1E	PCN 3	T4.0/4.0+	DWSP35 DWSP37	INIT DAS CI UP	RODN PGTW
36	021029	15.0% 127.1E	PCN 6		DWZBZK	CI Or	PGTW
37 38	021255	15.1N 126.6E	PCN 5		DMSP35		RPMK
39	021451	15.3M 126.4E	PCN 5		DMSP35		PGTW
40	0>2128	15.9N 125.0E	PCN 5		DMSP37		RPMK
41	022129	15.9N 125.3E	PCN 5	T4.0/4.0 /01.0/21HRS			PGT
42	022356	16.0M 125.0E	PCV 5		DMCD3K		PGTW
43	030137	16.2M 124.8E	PCN 1	T5.0/5.0 /D2.0/28HRS			RPMK PGT⊯
44	0,21009	17.5N 123.4E	PCV 6		0MSP37 0MSP36		PGTW
45 46	031237 031432	17.RN 122.6E	Pon 6		DMSP35		PGTW
47	031435	18.1N 122.6E	PON 6		DMSP35		RPMK
48	032249	18.6N 119.5E	PCN 3	T4.5/3.5 /W1.0/21HRS			RODN
49	032249	18.7N 121.5E	PCN 5	13.0/4.0+/WZ.0/21HRS	0M5P37		RPMK
50	040300	18.9N 120.6E	PCN 5		DMSP74		RPMK
51	040314	19.5N 120.4E	PCN 3		DMSP35	EXPUSED I LCC	RODN
52	041131	19.8N 119.4E	PCN 4		DMSP37		RODN RPMK
53	041555	20.1N 118.0E	PCN 3		DMSP35	EXPOSED ILCO NE OF DENSE CONV	RODN
54	041555	20.2N 118.1E	PCN 3	T3.5/2 6 /D0.5/24HD6		TWINDER LEGE ME OF DENIES COMM.	RPMK
55 56	042230	20.1N 116.3E	PCN 5 PCN 3	T3.5/3.5 /D0.5/24HR9	DMCD3A		RPMK
57	050255	20.1N 115.8E	PCN 3		DMSP35		RPMK
58	050256	20.2N 115.9E	PCN 3	T4.5/4.5-/W1.0/24HR9			RODN
59	051110	20.5N 114.3E	PCN 3		DMSP37		RODN
60	051110	20.44 114.5E	PCN 4		DMSP37	EXPUSED I LCC	RPMK
61	051343	20.6N 113.7E	PCN 3		0msp35 0msp35	WELL DEFINED HICC	RODN RPMK
62	051537	20.7N 113.7E	PCN 5		DMSP37	N/A DJE TO TERMINATOR	PGTW
63 64	052210 052210	21.7N 111.8E 21.5N 111.7E	PCN 5		0MSP37		RPMK
65	060043	21.5% 111.9E	PCN 5	12.5/2.5-/WZ.4/22HR			RODN
66	060237	21.4N 110.0E	PCN 5		DMSP35	•	RKSO

### ATRCHAFT ETXES

FIX NU.		FTX P051710**	FLT LVL	70843 HGT	DBS MSLP		~SFC- /4RG/			-FLT-LV /VEL/BK	L-4Nr	AC.	CRY /MF [	EyE Shape	DRIEN-	FAL LEWE	' (r) Pysst	45N ND.
1 2 3 4 5 6 7 8	\$0050 \$2550 \$2550 \$2150 \$250 \$150 \$250 \$250 \$250 \$250 \$250 \$250 \$250 \$2	13.3M 132.3F 13.3M 132.3E 13.9M 120.1E 14.1M 120.1E 14.4M 127.7E 14.4M 127.7E 15.7M 125.3E	700MH 700MH 700MH 700MH 700MH	7084 7085 2945 2951 2857 2859 2739 2725	1000 1000 984 981 974 971 955	55 55 50	270 180 020 320	15 15 40 20	150 140 140 250 100 040 210 230	19 04 32 08 55 07 60 18 85 02 62 31 74 13 92 13	0 6n 0 6n 0 15 0 35 0 45	8 7 5 6 6	5554	CIRCHLAR ELLIPTICAL ELLIPTICAL	180	+12 +10 +1 +19 +1 +10 +19 + +17 +1 +11 +17 +1 +15 +1	3 2 2	3 3 4 5 5
15 ] 1 ] 0	030544 030346 040352 042155	16.99 124.1E 17.39 123.9E 19.58 119.9E 20.28 116.7E	700MH	275n 2731 2979 3011	961 956 984 982	50 70	030 350 100 150	40 50 5	110 090 200 160	48 03 88 36 50 16 62 24	U 40 U 30 D 20	5 5 2	6	ELLIPTICAL		+13 +17 +1 +13 +1 +15 +19 +1 +16 +17	<b>+</b>	6 7 1 9
				,	70.0			-	FTYL		11,	•				+14 +19 +	9	10
F1X Nu.	1 TME (7)	FTX POSTTION	а Рабан	CCRY	EYE SHAPI		EYF Dla			-CODE			(	COMMENTS		HADAR Posttion	411F	
1 2 3 5 5 7 8 9 10 11 12 13 14	N 3 U 5 U D N 4 U D D N 4 U D D N 4 U 5 U D N 5 U D N 6 U 5 U D N 7 U D N	16.4N 123.HE 17.0N 124.DE 17.9N 123.HE 17.9N 123.HE 17.9N 123.HE 19.0N 121.SE 19.0N 121.SE 19.0N 121.SE 19.4N 120.SE 19.5N 110.TE 20.7N 115.SE 21.5N 112.SE 21.5N 112.SE	LAND LAND LAND LAND LAND						31901 31911 35471 35411 35351 1090/ 1091/ 5/// 659// 659//	5//// 529// 629// 52920 52712 /999/ ///// ///// ///// /////////////	SP Ev		PERC			14.1N 123.0E 16.3N 120.6E 16.3N 120.6E 16.3N 120.6E 16.3N 120.6E 16.3N 120.6E 16.3N 120.6E 16.3N 120.6E 16.3N 120.6E 16.3N 120.6E 22.3N 114.2E 22.3N 114.2E 22.3N 114.2E	9844( 9832) 9832) 9823) 9823) 9823) 98321 98371 45005 45005	1 1 1 1 1 1 1 1 5 5
							SYN	) <b>) †</b> (	n FTX	E6								
Flx NO.	TTME (7)	FTX Position	INTENSTI ESTIMATE		REST A (NM)				C	DMMENTS	,							
1 2 3 4 5 6	250000 251200 270500 260000 261200 300000 300500	7.0N 141.0E 7.0N 140.0E 8.9N 136.3E 17.0N 135.0E 13.0N 134.5E 13.5N 133.5E 14.0N 132.0E	15 20 15 20 25 25		150 120 100 60 100 180		BRn#	) F-	-W TRI -W TRI -W TRI	DIJGH DIJGH								

### TROPICAL STORM FAYE

FIX NO.	TT:45- (7)	PTX POSTTION	<b>ACCRY</b>	DYDRAK CODE	SATFLETTE	COMMENTS		SITE		
1	292307	2.0N 152.3E	PcN 5	T0.0/0.0	DMSP34 DMSP35	INII 365		PGTW PGTW		
3	3n2346 3n2349	3.6N 151.7E 5.6N 151.1E	PCN 5	T1.0/1.0 /01.0/2				PGTW		
4	010906	5.7N 150.2E	PCN 6		DMCD37	CI SAME		PGTW		
5	011132	4.1N 150.0E	PCN 6		DMSP36 DMSP35			PGTW PGTW		
6 7	011328	6.4N 149.7E	PCN 6		0HSP37			PGTW		
,	012007 020209	6.3N 147.3E 7.4N 146.2E	PCN 5	12.072.0 /01.0/2				PGTW		
ÿ	020948	7.9N 145.0E	PCN 6	1-10/1/40 /02/0/-	DMSP37	CI SAMÉ		PGT₩		
10	021114	7. RN 144.8E	PON 5		DMSP36			PGT# PGT#		
11	021309	3.0K 144.5E	Prn 6	*3 0.2 0	045632 046637	INI) Ods		RPMK		
12 13	022128 022129	9.0N 147.6E 9.2N 142.9E	PCN 5 PCN 6	13.0/3.0	DHSP37	1.11. 4-3		PGTW		
14	052356	9.4N 147.5E	PCN 5		AFUZHO			PGTW		
15	600160	9.3N 140.7E	PCN 6		045037	EDGE DE NATA EDGE JE NATA		PGTW PGTW		
16	031055	9.7N 140.3E	PCN 6		045634 045635	EDGE J. HATA		PGTW		
17 16	5E41F0	10.0% 130.6E	PCN 6		DMSP35			RPMK		
19	012109	10.4N 139.3E	PCN 5	T3.0/3.0 /SU.0/2				PGŢwl		
20	072338	10.3N 139.3E	PCN 5		DMCB34			PGTW		
21	040118	10.9N 139.4E		T4.0/4.0 /01.0/2		EXPUSED   LCC		RPMK PGTW		
55	0.0132		PCN 3	-3 o.2 o	DMSP35 DMSP35	Sportini		RODN		
23 24	040132 040949	10.4N 140.2E 10.4N 138.7E	PCN 4 PCN 6	T3.0/3.0	DMSP37	1.11. 0=3		PGTW		
25	041519		PCN 4		AF45M0			PGTW		
26	041413	10.7N 137.1E	PON 6		045235			PGTW		
27	041414	10.5N 136.7E	PCN 5		0#5P35 0#5P37	UPR LYL CNTR 10.5M	1.35.0F	RDDN PGTW		
28 29	04204B 042320	10.54 136.BE	PCN 5		PERSMO	0. 4 = 0. 4		PGTW		
30	050114	10.3N 135.9E	PCN 3	T3.0/3.0 /S0.0/2	RHRS DWSP35			PGTW		
31		10.1N 136.1E	PcN 3	T3.0/3.0 /50.0/2	4HRS DWSP35			RODN		
32		11.4N 135.6E	PCN 4		DM5P37 DM5P36	EXPUSED FLCC		PGTW PGTW		
33 34		11.9N 135.4E	PÇN 4 PCN 4		DMSP35	EXPOSED 1 CCC		RPMK		
35	051355 051355	17.0N 134.9E	PCN 3		DM4P35	EXPUSED ILCC		PGTW		
36	051355	12.34 135.0E	PCN 3		DMとわると			RODN		
37	052210	12.9N 137.8E	PCN 3	\$10.1W\ 0.E\0.ST	TEMPORAL PRINTS			PGTW PGTW		
38 39	062302 060237	13.1N 137.7E	PCN 3		DMSP35			PGTW		
40	060237	13.74 137.4E 13.60 137.3E	PCN 3	T2.0/3.0-/W1.0/2				RODN		
41	040909	15.0N 132.4E	PCV 6		DMCD37			PGTW		
42	041144	15.2N 132.0E	PCN 4		DMSP36			PGTW		
4.3	041518	15.4N 131.5E	PC4 4		DMSP35 DMSP35			PGTW RODN		
44 45	051519 070026	15.6N 131.3E 17.3N 129.6E	PCN 3	T0.0/1.0 /WZ.0/2				PGTW		
46	971308	17.7N 127.2E	PCN 6	1000,100 , 4500,5	AFGPMG	CI UP		PGTW		
47	090008	18.6N 126.4E	PCN 5	T0.0/0.0 /S0.0/2	AFGPMQ PRHA			PGTW		
48	081250	50.5W 154.3E	PCN 5		DMSP34			PGT₩		
					ATRCPAFT (	IXES				
FIX	TTHE	FIX	FLT			FLT-LVL-4ND ACCRY	EYE	EYE ORIEN-	EYE TEMPI (C)	45N 40.
NO.	(7)	POSTTION	FAF	HGT MSLP VEL	ARG/RIG DIP	VEL/BRG/HNG NAV/MET	SHAPE	MOTIVION	DEPLOY IN DEPLOY	40.
1	012300	6.1N 146.5E	15n0FT	1008						1
2	020652	7.6N 145.5E	1500FT		320 45 280	20 180 30 2 5			Ar FEA CE. CE.	5
3	020845	7.6N 145.3E	1500FT		080 50 280	25 200 100 5 5 36 360 60 4 8			+29 +23 +23 70	3
5	021909 02050	9.9% 143.6E 8.8% 143.8E	700MH 1500F1	3094 1001 40	270 15 250	37 270 15 4 2			+24 +25 +25 27	. 3
6	030910	9.5N 141.6E	7n0mH	3084 998 45	270 40 360	55 270 4n 5 7			+12 +15 + 6	•
7	032014	10-1N 140-6E	70048		170 30 140	46 040 7n 5 3 55 050 5n 5 5			+14 +15 +12 +14 +15 + 5	6
6	040804	10.5N 13R.5E	700MB		180 45 11# 170 15 #60		ELLIPTICAL	5 13 090	+1+ +17 + +	7
10	042122 050804	1n.2N 135.8E 11.3N 135.4E			240 10 230	30 140 7 6 5	0-20/ 10-44	•	+23 +26 +24	8
* 11	051925	11.4H 137.6E	700MB	<b>710</b> 0	220	33 150 6n 5 5			+11 +11	9
* 12	052200	12.6N 132.3E	1500F	1004 30	180 140 530	40 180 44n 5 18 5 5			26	11
13	040717	13.9N 132.7E		1001	090 70 170				+14. + 6	12
- 14	1170534	16.0N 127.5E	1 () O ML	1117 10	0,00 ,00 1	20 010 111 1 3				
					SYMOPTIC FT	xes				
FIX	TTAE	FTX		TTY VEAREST						
	(7)	P051110H	FSTIMA		•	COMMENTS				
							407105			
1	201500	3.04 155.0E	15			DOUBLE-VORTICE INTER				
2	290000	2.5N 154.0E	15 15		EST WSIP IO	DDIJBLE-VOMTTCE TNTER ORMH	NO 1 4 0 14			
3	291200 3n0000	3.0N 153.5E 3.5N 153.0E			EST 451P 10					
5	301200	4.NN 152.0E			SEC TROF NO					

# TROPICAL DEPRESSION 08

F1x NO.	TIME	FTX		014							
NO.	(7)	POSITION	<b></b> CCRY	DAUSTR	CODE	SATFLETTE	COMMENTS		SITE	•	
<b>*</b> 1	202338	5.9N 174.4E	PCN 5	T0.0/0.D		DMSP36	INIT 34S		no.Tu		
	211220	9.3N 135.5E	PCV 5	1000000		AFRZMO	CI SANE/HPR (V)		PGTW PGTW		
* j		13.5N 139.8E	PCV 6			DMSP36	CI SHIEVINER ( O)		PGTW		
4		18.8M 139.6E	PCN 5	11.0/1.0		DMSP36	INIT DUS/LLCC 235N	14075	PGTW		
>	231015		PČ4 6			DMSP37			PGTW		
6	2-1144	20.34 13A.9E	PCN 6			AFRAMO			PGTW		
7	221303	20.5N 13A.7E	PCN 6			DMSP39			PGTW		
븅	231328	30.5N 13R.6E	PCN 5			DMSP35			PGTW		
<b>•</b> 9	2-2111	22. DN 137.0E	PCN 5	T1.0/1.0	/S0.0/22HR	TF92MG 2			PGTW		
• 10	232245	22.4N 136.6E	PCN 5			PERSMO			PGTW		
* 11	240145	23.2N 135.1E	PCN 5			DHSb30	•		PGT₩		
• 12	240209		PCN 5	T1.0/1.0		DMSP35	INIT 345		RPMK		
* 13	240510	23.74 134.8E	PCN 5			DHSP35			PGTW		
* 14	240951		PCN 5			DMSP37			PGĬ₩		
* 15	241244		PCN 6			DMSP39			PGTW		
* 16 * 17	241307		PCN 6			OMSP36			PGTW		
• 18	241451		PCN 5			0MSP35	THAT HEOLITANS AND		PGTW		
+ 19	250008		PCN 5	-0	441 5 43 5 19		INIT NIGHTIME ORS	22 4 12- 5	RODN		
* 50		25.6N 130.9E 26.2N 130.4E	PCN 5	10.011.0	/W1 - D/27HR	DMSP30	POSSIBLE SECONDARY	S NN 130-3	E PGTW PGTW		
* 21	250150	26.6N 130.1E	PCN 5			DMSP35					
* 22	250151		PCN 5	T1.0/1.0		DMSP35	INIT Ods		PGTW Rodn		
23		30.7N 127.6E	PCN 5			DMSP39	12. 0-3		PGTW		
24	251250		PCN 5			DMSP36			PGTW		
25	251433	30.9N 127.4E	PCN 5			DMSP35			PGTW		
	252350	31.6N 125.7E	PCN 5	T4.0/4.0		DMSP36	INIT DUS		RKSO		
15		31.9N 125.5E	PCN 5		-/D2.0/24HR				PGTW		
28	260133		PCN 5			DMSP35			PGTW		
29	260314	32.9N 125.3E	PCN 3			DMSP35			RK50		
						AIRCRAFT FI	χES				
	TTHE	FTX	FLT	70043 D	BS MAX-SFC.	-WYD MAX-F	LT-LVL-4ND ACCRY	EYE	EVE ORIEN-	RYF TEMP (C)	458
NG.	<b>(7)</b>	POSTTION	LVL	HGT MS	LP VEL/ARG	RYG DIR/Y	EL/BRG/HNG NAV/MET			OUT! THE DPYSST	ND.
1	241016	23.1N 133.5E	700MB	3127 10	A 15 130	120 150	15 060 ln 2 ln				
•	-41410	E3414 13343E	1 () 0 40	1227 10	15 110	150 170	12 600 10 > 10			+10 + 7 + 8	,
						_					
					SY	OPTIC FIXE	5				
FIX	TTHE	FTX	INTENST	TY NEARE:	eT						
ND.	(7)	POSTTION	ESTIMATE			CO	MMENTS				
		3		- 57.7							
,	3.0000	21 2 22 22			_						
2	240000	21.5N 136.0E 23.5H 133.0E	15 20	61							
		24 Eu 120 9E	20	6							

17HE:	POSTTION	ESTIMATE	DATA (NM)	COMMENT
240000	21.5N 136.0E	15	60	
241200	23.5H 133.0E	50	60	
250000	24.5N 129.9E	20	60	
251200	29.0N 127.5E	20	60	
240000	31.0N 126.5E	15		
261200	33.0N 125.0E	15		
270000	36.0N 124.0F	1 4		
	240000 241200 250000 251200 240000 261200	24.0000 21.5N 13A.0E 24.1200 23.5N 133.0E 25.000 24.5N 129.9E 25.1200 24.0N 127.5E 24.1200 33.0N 126.5E 24.1200 33.0N 126.0E	24.0000 21.5N 13A.0E 15 24.1200 23.5N 133.0E 20 25.0000 24.5N 129.9E 20 25.1200 24.0N 127.5E 20 24.0000 31.0N 126.5E 15 24.1200 33.0N 126.0E 15	(7) POSTTION ESTIMATE DATA (NM)  240000 21.5N 13A.0E 15 60 241200 23.5N 133.0E 20 60 251200 24.5N 129.9E 20 60 251200 24.0N 127.5E 20 60 240000 31.0N 12A.5E 15 60 241200 33.0N 12A.5E 15 60

#### SUPER TYPHOON HOPE

F12	T 1 M E (7)	FTX POSTTION	&CCRY	UNUSUK CODE	SATELLIE	COMMENTS	SITE
1 2	250151 250932	10.5N 145.2F 10.4N 143.4E	PON 5 PON 6	11.0/1.0	DWSP35 DWSP37	Sec 11N1	PGT₩ PGT#
• 3	251105	10.3N 142.7E	Pry 5		DACRIV		₽GŢ₩
• 4	251226	111.44 142.65	PCN >		DMcb3o		PGTW PGTW
• 5	251433	10.24 142.1E	PCN 6		Dwsp35 Dwsp36		PGTW
6	252350	11.40 140.HE	PCN 6	T1.0/1.0 /50.0/22HRS	Dwdbdd		PGTW
7	240107	11.44 140.55	PCN 5		045835		PGT₩
병	240133 240133	11.5N 140.5E 11.0N 141.5E	PCN 5	T1.0/1.0-	DMSP35	INIT 3dS	RODN
1ú	240915	11.7N 140.3E	PON 6		DWCP37		PGTW
11	241207	12.00 140.0E	PON 5		DMCb30		PGT⊎ PGT₩
12	541535	12.0N 134.4E	PCN 6		DMSP35		PGTW
13	261414 261414	]].9v ]30.5E	PON 5		D45P35	INI! NIGHTIME ORS	RPMK
15	270048	13.6M 160.7E	PCN 3		DMCP39		PGTW
16	270114	13.4M 140.5E	PCN 3	TU. 0/1.0 /W1.0/24HRS	DMSH35		RODN PGTW
17	270114	13.5N 140.6E	PCN 3	T1.0/1.0 /W1.0/25HR	045632 045632	EXPUSEM ! LCC	PGTW
18	270951	14.7N 140.3E	PCN 4 PCN 3	T1.0/1.0 /01.0/26HR		EAFORE ! ECC	PGTW
50 13	272314 290237	14.34 139.0E		11.00/1.0 /01.00/20000	Duspas		PGTW
+ 51	240531	14.2N 134.5E	PCN 6		DWSP37	BASED UN HPR IVL	RPMK
22	2a1013	17.7N 137.5E	PCN 5		DMSP37		PGTW PGTW
* 23	241156	19.00 137.UE	PCN 6		DMZb3A		RPMK
a 24	541310	18.3v 136.3E			DMSP35		PGTW
* 25 26	241337 202112	18.4M 136.8E		T2+0/2+0 /01+0/22HR4			₽ĠŢ₩
27	282257	15.9N 135.7E			DMSP34		PGTW RPMK
28	240151	14.4N 134.9E	POND	T3.0/3.0	Duchad	INIL 292	PGTW
29	290213	14.1N 135.7E	POND	-3 4	DMSP35 DMSP35	INI1 Ods	RODN
31 30	501138 500513	16.2N 135.68 16.5N 135.18		T3.0/3.0	DMSP36	C1 UP	PGTM
35	201136	14.7N 134.9E			PFRPMG		PGTW
33	291500	16.94 134.76	PCN 6		DMSP35		PGT⊯ Rodn
34	291500	14.7v 134.78	PÇN 6		DMSP35 DMSP36		RODN
35	300014	14.4N 137.36		T4.0/4.0 /D2.0/21HR	•		PGTM
36 37	300020 300132	16.7N 133.48 15.5N 133.48		T4.0/4.0+/01.0/24HR			RPMK
38	300133	14.7N 133.36		,	DMSP39		PGTW RODN
3+	3nu201	15.9v 133.38	PCN 1	T4.5/4.5 /D1.5/24HR	g DMSP35		PGTW
40	300501	14.9N 133.28	PCN 2		0msp35 0msp37		PGTW
41 42	300932	17.0N 132.18			DMSP39		RODN
43	301233	17.4N 132.0			DMSP 79		PGTW
44	301301	17.2M 131.7E	PON 4		DMSP36		PGTW PGTW
45	3n1441	17.70 131.30	PCN 1		DMSP35 DMSP37		RKSO
46	301442	17.7N 131.45		15.5/5.5 /01.5/21HR			RPMK
47 48	302213	18.5N 129.58	PCN 3	T5.0/5.0 /D1.0/22HR	S DMSP37		PGŢW
49	310002	19.4N 129.3	PCN 1		DMSP3A		PGTW
50	310114	19.9N 179.9	PCN 1		DMSP39 DMSP37		PGTW PGTW
51	311053	19.3N 184.6	PCN 2		DMABAY		PGTM
52 53	311244 311355	]9.7N ]25.91 ]9.7N ]25.91	PCN 2		PERPHO		RPMK
54	311355	19.7N 125.6	PCN 1		DMSP39		RODN
55	311423	19.84 125.5	PON 1		DMSP35		PGTW Rodn
56	311424	19.54 125.7	E PCN I	T6-5/6-5-/D1-5/24HR	DWSP35 c DWSP37		PGTW
57 58	312153 312153	20.5N 123.7		T6.5/6.5-/D1.5/24HR			RPMK
59	312153	20.5H 123.7	E PCN 1	T6.5/6.5	DMSP37	INIT DAS	RODN PGTV
60	312344	20.6H 123.3	E PON 1		DMSP36		RPMK
61	010236	20.74 127.6	E PCN 1		PF92MQ PF92MQ		RODN
62 63	010236 011033	20.6N 122.4 21.3N 120.6			DMSP17		PGT#
64	011336	21.5N 119.5			DHSP39		PGTW
65	011336	21.6N 119.6	E PONI		DMSP39		RPMK Rodn
66		21.64 119.5	E PCN 1		DMSP39 DMSP3A		RPMK
67 68		21.5× 119.5 21.7× 118.6	E PON 1 E PON 1		DMSP35		RODN
69		22.04 117.1		T5.5/6.5-/W1.0/24HR	C DMSP37		RPMK
70	020217	22.4N 115.7	E PCN 1	T5.0/5.5-/W1.5/ZAHR	C DMCP39		PGTW PGTW
71		22.1N 115.3	E PCA j	-5 au 6 201 c 2 3 au 6	DMSP35		RODN
72		22.34 115.3	E PCN 1 E PCN ◆	T5.0/6.0-/W1.5/29HF	045P17		RPMK
73 74		22.5N 112.4 22.7N 113.1			DMSP37		RODN
75		22.7N 11n.8	E PCN 4		DMSP35		PGTW RPMK
76	021528	22.74 107.9	E PC46		DMSP35 C DMSP37		RODN
77 • 78		21.6N 189.4	E PON 5 E PON 5		DMSP37	INIT 045	RKSO
- 18	0>2254	22.6N 10A.8	- 11,43			-	

# ATREPART FIXES

FIX NO.	11HE: (7)	FTX POSTTION	FLT LVL			MAX-FLT-LVL-MI DTR/VEL/BHG/HI		EYE SHAPE O	FYE ORIEN 144/TATIO	- FAL LEMS	
123456789 1011231451671819 20122	240928 262113 264503 264035 272307 261833 26205 272307 261833 262031 360615 360925 360925 360925 370925 37093 37093 37093 37093 37093 37093 37093 37093 37093 37093 37093 37093 37093 37093 37093 37093 37093 37093 37093	10.8N 144.5E 11.2N 147.4E 11.4N 141.7E 11.9N 141.3E 12.3N 139.8E 12.5N 141.0E 16.7N 136.7E 16.6N 136.5E 16.6N 136.5E 16.6N 136.5E 16.6N 137.4E 17.1N 132.4E	1500FL 700MH 700MH 700MH 150NF1 790MH 700MH 700MH 700MH 700MH 700MH 700MH 700MH 700MH 700MH 700MH 700MH 700MH 700MH 700MH 700MH 700MH 700MH	1005 3085 1000 3081 1000 3091 1002 309n 3092 3097 3047 995 2065 2064 972 2777 965 2745 961 2556 2509 934 2447 926 2323 912 2203 988 2237 902 2381 970	25 310 120 25 050 50 15 050 40 15 130 100 10 080 50 50 120 15 40 100 30 75 340 20 70 130 20 80 360 30 85 170 12 40 220 50 95 160 50 95 160 10 100 360 10 140 110 20 95 060 30	100 17 130 4 230 50 300 300 310 310 320 320 320 320 320 320 320 320 320 32	40 4 70 90 7 25 26 5 25 30 30 10 10	ELLIPTICAL	0 B 140 5 4 0	*25 *23 *23 *25 *21 *11 * 9 *12 *13 * 9 *10 * 7 *25 *23 *11 * 11 *11 * 12 *13 * 10 *14 * 13 * 10 *15 * 15 *15 * 15 *19 * 15 *19 * 15 *10 * 17 * 15 *11 * 15 * 16 *15 * 16 *15 * 16 *15 * 16 *17 * 17 *18 * 17 * 17 *19 * 16 *10 * 17 * 17 *10 * 17 * 17 *10 * 17 * 17 *10 * 17 * 17 *11 * 17 * 17	23 1 28 2 3 4 4 4 28 5 6 6 7 7 7 8 8 8 9 9 10 10 11 11 11 12
					RA JAR	FIXES		i			
Fix NO.	TTME (7)	FIX POSTTION	RADAR A	EYE CCRY SHAP		RADON-CODE ASWAK TODEF	c	COMMENTS		HADAR POSTTION	SITE WHO NO.
1 2 3 3 4 5 5 6 7 7 8 9 9 10 11 12 13 14 15 116 17 18 119 20 21 22 23 32 4 25 6 26 27 28 33 34 35 35 35 35 36 37 4 4 4 4 4 4	01 00 00 01 01 00 01 01 00 01 01 00 01 01	20.5N 123.0E 20.7N 122.5E 20.7N 122.2E 20.5N 122.2E 20.5N 122.2E 20.5N 121.20 20.5N 121.4E 20.7N 121.5E 21.3N 12.5E 21.3N 12.5E 21.3N 12.5E 21.3N 12.5E 21.3N 12.5E 21.3N 12.5E 21.5N 12.5E 22.5N 11.5E	LAND LAND LAND LAND LAND LAND LAND LAND		ה עניני ע היים ערים איני פיני פיני פיני פיני			RLAY 15 DEGREE'		14.2N 122.7E 14.2N 121.6E 14.2N 121.6E 16.3N 120.6E 16.3N	98791 46596 98231 98231 98231 46731 46731 46639 46639 46649 46649 46649 46649 46744 46746 457005 450005 450005 450005
					SYNOST	C FTXES					
F1X	TIME:	F1X P051710H	INTENST	TY NEAREST	)	COMMENIS					

FIX TIME: FIX INTENSITY WEAREST
NO. (7) POSITION FESTIMATE DATA (NM) COMMENIS

1 241200 10.5N 147.0E 15 100

The state of the s

# TROPICAL STORM GORDON

Fix Nu.	11HE (7)	6021110V	VECSA	NAUSTR CODE	SATFII TTE	CUMMENTS		SITE		
* 1 23 4 56 7 8 9 0 1 1 1 2 3 4 5 6 7 8 9 1 1 1 1 2 3 4 5 6 7 8 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	241226 241253 2512310 2512310 2512310 2512310 2512310 251232 251232 271225 271225 271225 271225 271225 271225 271225 271225 271225	20.34   20.26 20.44   24.82 20.54   124.36 20.74   124.36 20.74   124.76 20.75   124.76 20.76   124.76 20.76   124.76 20.77   124.76 20.76   124.76 20.77   124.76 20.78   124.76 20.79   121.46 20.79   110.76 20.79   110.76 20.79   114.76 20.79   114.76	PCN 5	(2.0/2.0 (2.0/2.0 (2.0/2.0 (2.0/2.0 (2.0/2.0 (3.0/3.0 (1.0/2.0 (3.0/3.0 (1.0/2.0 (3.0/3.0 (1.0/2.0 (3.0/3	0 M S P 3 O M S	INII 1 DOS  INII DOS  INII DOS  INII DOS  PARTIALLY EXPONSEI INII DOS  CI UP  BANDING TYPE FYE CI SANE  INII DOS		PGTW PGTW PGTW PGTW PGTW PGTW PGTW PGTW		
				٨	19CHAFT F	KES				
F1x NO+	TTME (7)	FTX POSTTION	FLT 7			ET-LVL-4ND ACCRY EL/BRG/HNC NAV/HE		EVE ORIEN-		
* 2 3 4 5 * 6 7	260827 262036 262152 270810 270948 271936 272152 241050	19.9% 120.7E 20.0M 127.2E 20.5M 126.5E 20.5M 126.0E 20.7M 124.8E 21.1M 122.4E 21.1M 122.4E 21.1M 121.4E	700MB 3 1500FT 700MB 3 700MB 3	1065 997 50 050 1063 994 50 320 1004 50 330 1004 991 40 020 100942 983 100942 981 50 040 100942 981 50 040 100942 981 50 040 100942 981 50 040	120	45 050 2n 4 5 39 050 47n 4 15 35 320 6n 4 3 40 330 35 5 54 020 120 5 8 51 400 28 5 2 53 040 30 0 2 45 120 42n 2 4	CIHCIJLAR ELLIPTICAL	5 40 25 010	+25 +25 +25 +13 +25 +12 +10 +12 +11 +11 +14 +12 +11 +17 +14 +15 +15 +11	29 2 3 3 4 4 5 5
				R	ADAH FTXES	3				
F1X NO.	TTME (7)	FTY POSTTION	HADAR ACC	EYE EYE RY SHAPE DIA			COMMENTS		HADAR POSITION	SITE
1	20000 20000 20000 20000 20100 20100 20120 201300 201300 201300 201300 201500 201700 201700 201900 201900 201900 201900 201900	20.94   21.2E 20.94   271.1E 21.00   271.1E 21.00   271.1E 21.24   20.4E 21.34   20.4E 21.35   10.4E 21.37   20.4E 22.34   20.4E 22.34   10.4E 22.34   10.4E 22.35   10.4E 22.35   10.4E 22.35   10.4E 22.35   10.4E 22.35   10.4E 22.35   10.4E 22.35   10.4E 22.36   11.4E 22.36   11.4E 22.37   11.4E 22.38   11.4E 22.39   11.4E 22.39   11.4E 23.16   11.4E 23.16   11.4E	LAND LAND LAND LAND LAND LAND LAND LAND		55555555555555555555555555555555555555	73111 73010 72813			75.1% 121.6E 75.1% 121.6E 75.1% 121.6E 72.6% 120.3E 72.6% 120.3E	46596 46596 46744 45744 46744 45745 45705

### TROPICAL DEPRESSION 11

FIX NO.	TIME (7)	FIX POSTTION	&CCRY	DVD24K CODE	C. 7511 175	Chaurage	E++E		
	177	-0511 for	PCCRT	DADSVK CODE	SATFLLITE	COMMENTS	SITE		
1	021317	12.1N 135.3E	PON 6		DMGD3Q	INII NIGHTIME OHS	PGTW		
• 2	855050	13.4N 131.ZE	PON S	TU.( '0.0	DMCD35	INIT JUS	PGTW		
3	030953	13.9N 130.4E	PCN 6		DMSP37	1711 0-3	PGTW		
4	030953	14.5M 131.0E	PCN 6		DMSP37		RPMK		
5	071150	14.2M 130.2E	PCN 6		DMSP36		PGTW		
6	031258	14.5N 13n.3E	PC4 5		DMCDJO		PGTW		
<b>*</b> 7	031510	13.3N 128.9E	PCNS		DMCD35		RODN		
8	031310	14.9N 13n.3E	PCN 6		DMSP35		PGTW		
• 9 • 111		15.0N 127.7E	PCN 5	T0.0/0.0 /S0.0/22HR			PGTW		
* 10 * 11		15.7N 12R.1E	PCN 5	T0+0/0+0	. 0w2b32	INII Jas	PGTW		
• 12		15.4N 128.1E	PCN 5	10+070+0	DMSP35	1411 202	RODN PGTW		
+ 13		15.9N 127.0E	PCN 6		DMSP37		PGTW		
+ 14		16.4N 126.3E	PCN 5		DMSP30		PGTw		
+ 15		16.5N 126.3E	PCN 5		DMSP36		PGTW		
* 16		16.5N 126.0E	PCN 5		DMSP35		PGTW		
* 17		14.2N 125.9E	PCN 5		Dwebse		RPMK		
* 18		17.84 126.2E	PCN 5		Duspa7		PGTW		
19		17.7N 127.8E	PCN 5	T2.0/2.0 /D2.0/24HR			PGTW		
20		17.7N 12R.0E	PCN 3		DMSP 14		PGŢW		
51	050151	17.3N 12R.0E	Prin 3	-1	DMSP35		PGTW		
53 55		18.0N 126.9E	PCN 5	T1-0/1-0+/D1-0/24HR		EXPOSED   LCC	RODN		
24		19.9N 126.2E	PON 3 PON 6		DMSP34	EXPOSED   LEC	PGTW ROOM		
25		14.00 125.8E	PCN 3		D45935		PGTW		
* 26		14.8M 122.8E	PCN 5	T2.0/2.0 /S0.0/22HR			PGTW		
27		39.FS1 WE.P1	PCN 5	T1.0/1.0	DMSP37	INI 1 Das	RPMK		
* 28		18.5N 122.9E	PCN 5		OMERSE		PGTw		
29		19.3N 127.5E	PCN 5	T1.0/1.0 /S0.0/25HR	C DMSP39		RODN		
30		19.34 123.4E	PCN 5		DMSP35		RODN		
31		19.3N 123.5E	PCN 5	_	DMSP35		RPMK		
32		31.1W 155.0E	PCN 5	T0-0/0-0	DMCP37	INI 1 DOS	RKSO		
33	061317	21.0N 119.6E	PCN 5		Drabia		RODN		
					ATREPART FI	XES			
				_					
	TTME	FIX	FLT			LT-LYL-MAN ACCRY	EYE EYE ORIEN-	EYF TEMP (C)	458
NO.	(7)	POSITION	LAL	HGT MSLP VEL/ARG	ANG UINNA	EL/BHG/HMG NAV/MET	SHAPE DIAM/TATION	OUT/ INV DP/SST	4O.
1		14.0N 132.1E	7n0+14	3099 1003 10 230		15 060 48 5 5		+11 + 9 28	2
5	0.45500	14.7N 129.9E	700HB	1079 1004 15 150		12 330 10 5 5		+15 +15 + 8 28	5
3		17.3N 127.6E	1500F [	1001 30 180		30 180 35 4 15		+25 +23 28	4
		19.0N 125.9E	1500FT	997 25 060		25 060 6n 5 5		+25 +25	5
* 5 6	052130 052222	14.9N 122.8E 19.3N 123.4E	7n0MB 15n0Fí	7097 1001		25 150 in 3 iii 15 330 5 4 2		at .35 -5	6
٥	V7666	14.40 151.45	12001	1007 20 360	4 060	15 330 5 4 2		+25 +25 >7	6
				SY	かわってけた チリメモ	s			

FIX NO.	TTME (7)	FTX P0517]UN	ESTIMATE	NEAREST DATA (NM)	COMMENTS
5 I		12.0% 136.0E 20.7% 121.9E	15 15	120 30	

### TYPHOON IRVING

F1X NU•	T1 4E (7)	602111ibii t 1 x	ACCRY	DVORAK CODE S	ATFILITTE	COMMENTS	SITE
1	071220	14.19 137.55	PCN 6		Dadbay	1017 340	PGTW
2	090023	16.14 134.15	PCN 4	TG.0/0.0	DMZBSK DMZBSA	INI Jas	PGT# PGT#
3	0s1202 0s2303	34,50 137.9E 17.70 136.6E	PON 3	T1.0/1.0 /01.0/23HRs	AFG2#G		PGTW
5	612040	17.94 135.9E	PON 5	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	Duspas		PGTW
6	090733	19.34 135.55	PCN 4		Duch37		PGTW
7	001144	14.3v 134.3E	PCN 3		DMZ632		PGTW PGTW
y V	041200	17.44 134.0E	PCN 3		DMZD3H		RPMK
10	005160	17.74 1 14.HE	PCN 3		DMSP35		RODN
11	004214	14. AM 197.3E	PCN 4		DMSP37		PGTW
15	100026	18.8× 133.2E	PCN 3	T1.0/1.0 /S0.0/25HRS	DMCb34		PGIW PGIW
13	100127 100127	19,40 133.15	E 709	T1+0/1+0	OMEBSA	INIT DOS	RODN
15	100727	14.5N 137.1E 14.3N 132.0E	PCN 6	12407140	DMSP37		PGTW
16	100913	14.44 132.2E	Prn 6		DHEBSI		ROON
17	141556	19.3N 131.4E	Prin 3		DMEBJY		PGTW PGTW
19	101307	19.5N 131.4E 12.1N 129.8E	Pry 6 Pry 5		DHSP35		RPMK
20	101442	14.3× 130.25	PCN 5		DM2631		PGTW
51	101442	17.00 130.1E	PCN 3		DMSP35		RODN
55	102154	17.04 129.8E	PCN 5	->	Duspa7 Duspa7	INII Jds	PGTW RPMK
23	1n2154 110009	17.0N 129.8E	PCN 5	T1.0/1.0 /D1.0/24HRs	DMSP3n	1411 003	PGTW
24 25	170108	16.7N 129.6E	PCN 5	121,7210 7011,0704	Duspay		PGIW
26	110142	14.9N 120-4E	PCN 5		DMCD35		PGTW
21	110142	16.7N 129.5E	PCN 6		Duspas Duspa7		RPMK PGTW
28	111034	16.6N 129.5E	PCN 5		DMCBSP		PGTW
29 30	111250	17.2N 129.2E	PCN 6		DHSP39		PGTW
31	111423	17.3N 170.3E	PON 5		DHSP35		PGTW
32	111423	17.1N 130.BE	PCN 5	-1	DMSP35 DMSP37		RKSO RPMK
33 34	112134 112134	17.5N 12R.1E	PCN 5	T2.5/2.5 /01.5/24HHS	DMSP37		PGTW
35	112351	17.34 124.7E	PON 3	73.0/3.0 /01.0/24HRS	DMSP36		PGTW
36	120230	17.5H 127.7E	PCN 5	T3+0/3+0	DMCb3A	SPC JINI	RODN
37	120230	17.7N 127.0E	PCN 5		DMGB39		RPMK Rodn
38	120305	17.4N 127.6E	Pon 5		DMSP35 DMSP37	CI UP	PGTW
39 40	121232	14.7N 127.0E	PCN 5		DMSP36	<b>4. 6</b> .	PGTW
41	121330	18.8N 126.3E	PCN 6		DMZD39		RPMK
42	121330	19.9N 126.6E	PCN 5		045P39 045P35		PGTW Rodn
43	121537	18.9N 126.3E	PCN 5		DMSP37		PGT#
44 45	122114	19.94 126.7E	PCN 5	T4.5/4.5 /D1.5/24HRS	DMSP36		PGTW
46	130211	20.00 126.9E	PCN 3	14.0/4.0 /D1.0/24HRS	DWSP49		RODN
<b>47</b>	130211	20.6M 127.0E	PCN 3	T4.0/4.0+/01.5/29HRS	Duchio		RPMK Rodn
48	130247	20.3v 124.9E	PCN 3		0m5P35		PGTW
49 50	130247 130954	20.7N 127.0E 21.5N 124.4E	PCN 4		DMSP37		RODN
51	130954	21.4N 126.7E	PCN 6		DMSP37		PGTW
52	171214	22.1N 125.9E	PC4 >		DMSP36		PGTW PGTW
5 J 5 4	121311	22.3N 125.4E 22.5N 125.4E	PCN 3		OMSP39 OMSP35		RODN
55	131528	22.7N 125.4E	PCN 5		DMSP35		RPMK
56	132234	23.44 125.1E	PCN 5	T5.0/5.0-/01.0/21HRS	DMSP37		RPMK
57	132532	23.0N 125.1E	PCN 5		DMSP37		RODN RPMK
58	140056	23.9N 124.0E 23.3H 125.1E	PCN 5 PCN 1	T4.5/4.5 /00.5/24HRS	DMSP36		RODN
59 60	140152 140152	23.5N 124.BE	PCN 3	T5.0/5.0-/D0.5/26HRS	Duspag		PGTW
61	140152	23.7H 125.1E	PON 3	T4.5/4.5	DMCD30	INIJ DØS	RKSD
62	140558	23.5M 124.9E	PCN 1		045P35 045P35		PGT# RKSD
64	141115	23.5N 125.0E 24.7N 125.0E	PCN 2		DMSP37		RPMK
65	141116	24.54 124.7E	PCN 2		DMSP37		RODN
66	141252	24.7N 124.4E	PCN 1		DMSP39		RPMK
67	141252	24.5x 124.6E	PCN 3		DMSP36		PGTW RKSO
68 69	141338	24.5N 124.5E	PCN 2		DMSP35		PGTW
70	142214	24.54 124.8E	PCN 1	T5.5/5.5 /D0.5/24HRS	DMSP37		RPMK
71	142215	25.44 124.7E	PCN 1		Duspat		RODN
72		25.9N 124.4E	PCN 3		PF92m0		RK50 Rodn
73 74	150039 150133	25.4M 124.4E 26.6M 124.6E	PCN 3 PCN 3	T5+0/5+0 /90+5/23HRS T5+0/5+0 /S0+0/24HRS			PGTW
75	150209	26.7N 124.7E	PCN 3		DMSP75		PGTw
76	150210	24.4N 174.4E	PCN 3		DMSP35		RODN
77	150210	24.3E	PCN 3		0msp35 0msp37		RKSO RPMK
76 79	151055 151055	27.2N 123.BE	PON 2		DMSP37	PSN BASEN ON FYF	RODN
80	151233	27.5N 123.7E	PCN 1		DM2630		PGTW
81	151233	27.4N 123.6E	PCN I		DMSP39		RKSO
85	151319				DMSP36		RPMK PGTH
83 84	151320 151451	27.5N 12358E 29.1N 124.0E	PCN 3		DMSP36 DMSP35		PGTW PGTW
85		27.9N 123.HE			DMSP35		RKSO
		· · · · · · · ·					

86 87 88 89 90 91 92 93 94 95 96 97 100 101 103 104 105 107 118 111 113 114 115 116 117 118 119 121 121 122 123 124	7 152155 3 1A0020 1 1A0151 1A0151 1A0155 1 1A0255 1 1A0255 1 1A0255 1 1A1035 1 1A103	29.2N 123.7 29.2N 123.7 31.4N 123.7 30.1N 123.5 30.2N 123.7 31.4N 123.7 31.4N 123.7 31.4N 123.7 31.7N 123.8 31.7N 123.8 32.2N 123.8 32.2N 123.8 33.5N 124.9 33.5N 124.9 33.5N 124.9 34.5N 124.9 34.5N 125.7 34.5N 125.7 35.5N 125.7 36.5N 125.7 37.5N		1 15-0/5 2 1 15-0/5 1 15-0/5 1 15-0/5 1 15-0/5 1 17-0/5 1 17-0/5 1 17-0/6 1	.0-/S0.0/20HR .5 /W0.5/24HR .0 /O1.0/25HR .0 /S0.0/20HR .0 -/W2.0/27HR .5 /W0.5/21HR .0-/W2.0/27HR	DMSP3;				PGTW PGTW PGTW PGTW PGTW PGTW PGTW PGTW		
FIX NO.	TIME (7)	FTX POSTTION	FLT L¥L	70043 HGT M		MAD WEX	-FLI-LVL-4NN /VEL/BKG/ANG	ACCRY	ξγE	EYE ORIEN-	PYF TEMP	
1 2 3 4 5 5 6 6 7 8 9 10 11 1 1 2 1 3 1 4 5 1 6 1 6 7 1 8 9 2 1 1 2 2 2 3 3 2 5 5 5 6 6 7 8 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0-0008 0-0088 0-0088 0-1926 0-02122 100716 1-00814 1-0207 1-10631 1-10631 1-10631 1-10918 1-10	17.4N 136.0E 18.1N 135.5E 17.4N 134.6E 18.3N 131.8E 18.4N 131.8E 17.4N 120.2E 16.4N 120.2E 17.5N 120.2E 17.5N 120.2E 17.5N 127.0E 19.3N 127.0E 19.3N 127.0E 21.2N 126.7E 23.0N 125.1E 23.2N 126.7E 23.0N 125.1E 24.0N 126.9E 24.0N 126.9E 27.1N 127.9E 27.1N 127.9E 27.2N 127.9E 27.2N 127.9E	15n0FT 15n0FT 7n0MB 15n0FT 7n0MB 7n0MB	3077 3037 3078 3067 3066 3065 3016 3994 2998 2998 2907 2870 2870 2843 29770 2843 27770 27770 27770 27717 92717 92717	996 45 220 998 20 270 30 030 998 30 330 996 30 210 996 30 210 996 30 210 997 25 290 187 25 290 187 25 310 187 35 180 187 35 180	35 280 35 190 140 70 740 10 120 20 110 50 110 50 110 50 120 110 50 120 140 120 100 120 100 140 120 140 120 140 140 140 140 140 140 140 140 140 140	15 220 2n 30 100 3s 33 090 42n 33 090 12n 30 050 12n 31 290 60 45 090 6n 47 090 15n 48 280 6s 60 310 9s 65 030 12n 55 030 12n 55 330 10n 56 230 9n 68 340 6n 68 340 6n	15025453306555512 15452255266227555	CIRCULAR CIRCULAR CIRCULAR	30 30 30	011+/ 1V/ 0P;  +13 +16 +25 +2b +25 +24 +12 + 8 +25 +25 +15 + 5 +26 +28 +13 + 9 +13 +12 + 8 +16 +12 +15 +13 + 8 +16 +10 +16 +16 +16 +16 +16 +16 +16 +17 +12 +16 +17 +12 +16 +17 +12 +10 +15 +15 +16 +17 +12 +10 +15 +15 +16 +17 +12 +10 +15 +15 +16 +17 +12 +10 +16 +17 +12 +10 +15 +15 +16 +17 +12 +10 +15 +15 +16 +17 +12 +10 +16 +17 +12 +10 +15 +16 +10 +15 +16 +10 +15 +16 +14 +15 +16	
Fix	TTME	F+4				IJAH FIKE						
NO.	(7)	POSTTION-	A PAGAH		EYF EYF HAPE DIAM	Hanna Hanna	-CODE	c	COMMENTS	P	HADAR POSTTION	SITE
23 45 67 89 10 11 13 14 15 16 17	131700 131730 131900 131900 131900 132000 132000 13200 132100 132200 132200 132200 132300 132300	22. 9N   125.1E 23.2N   125.3E 23.2N   125.2E 23.2N   125.2E 23.2N   125.3E 23.3N   125.3E 23.3N   125.3E 23.3N   126.3E 23.3N   126.3E 23.3N   126.3E	LAND LAND LAND LAND LAND LAND LAND LAND	P10A P10A P10A	e0 e0	6///2 5///2 5///2 5///2 6///2 6///2 6///2 6///2 6///2	52816 5//// 5//// 51/16 73105 52806 52805 ///// 53308 51805 EVE	MOVE 33	14	24 24 24 24 24 24 24 24 24 24 24 24	.3N 124.2E .3N 126.2E .3N 126.2E	47918 47918 47919 47919 47919 47918 47918 47918 47919 47927 47927 47918 47918 47918 47918 47918 47918 47918 47927 47927

1	140000	22 441	196.65	LAND	POUR	50		EVE MOVE 3115	24.8N 125.3E: 47927
Žΰ	14000 14000 14000 14000 14010 14010 14010	23.44	125.0E	LA-ID	Files	-,0	5///2 529//	Eve With 2112	24.3N 124.2E 47918
21	140000	27.74	125.0F	LAND			2///4 5000U		24.8N 125.3E 47927
22	140030	23.5M	124.9E	LAND	Phos	50		EYE MOVG 3220	24.8N 125.3E 47927
23	140100	21.5M	124.HE	LAND	PhOR	6.0		EYE MOVG 3220 EYE MOVG 2815	24.HN 125.3E 47927
24	140100	23.50	124+HE	CIAAJ			3///4 53215		24.8N 125.3E 47927
25	140100	23.54	124.9E	LAND			5///2 53108		24.3N 124.2E 47918
* 26	140100	25.3N	125.5E	LAND			65//3 05516		24.0N 121.6E 46609
* 27	140100 140200 140200 140200 140200 140200 140300	23.5N	124.BE	(AMD	POUR	60		EYE STNR	24.8N 125.3E 47927
58	140200	23.4N	124.7E	CIPAJ			6///2 52511		24.3N 124.2E 47918
5.3	140200	23.50	124.7E	LAND			9///4 52705		24.8N 125.3E 47927
30	140200	27.4N	125.08	LAND			25443 52421	•	24.0M 121.6E 46649
31	140300	23.6N	124.9E	LAND			5///4 50415		24.8N 125.3E 47927
32	140300	23.54	124 · /E	LAND			6///2 72905		24.3N 124.2E 47918
33	140300 140400 140400	23,7N	125.05	LAND			21944 50120 22974 50105		24.0N 121.6E 46699
34	140400	23.9N	125.16	LAND			6///2 50515		24.0N 121.6E 46699 24.3N 124.2E 47918
35	140400	23.7N	164.76	CAMO			5///4 50208		
36 37	140400 140500 140500	24.30	174.75	LAND			10944 53428		24.8N 125.3E: 47997 24.0N 121.6E: 46689
38	140300	24 CN	124.95	[ A 4 0			5///3 53514		24.8N 125.3E 47927
	140500	23 34	124.95	LAND			5///2 53611		24.3N 124.2E 47918
40	140500	24 34	124 + 75	LAND			24444 53407		24.0M 121.6E 46699
41	140500	24 11	125.0E	LAND			5///3 50308		24.8N 125.3E 47927
42	140500	24-16	124.HF	LAND	GOUD	40		EYE MNYG 3335	24.8N 125.3E 47927
43	140500	24 - 1N	124.7E	LAND	0.7-2		5///2 73612	-	24.3N 124.2E 47918
44	140700	24.1N	124.7E	LAND			20773 52714		24.8N 125.3E 47927
	140700	24.2N	124 -8E	LAND	<b>ცე</b> ნნ	4 D		EVE MOVA 3205	24.8N 125.3E 47927
46	140700	24.2N	124 . RE	LAND			1ng84 52407		24.0N 121.6E 46699
47	140700	24.14	124.7E	LAND			9///2 73315		24.3N 124.2E 47918
48	140900	24-1N	124.7E	LAND			11/14 52105		24.0N <u>i</u> 21.6E. 46609
49	140900	24.1M	124.6E	LAND	G100	10		EYE STAR	24.8N 125.3E 47927
	140800	24+1N	124•7E	LAND			6///2 73305		24.0N 121.6E 46699 24.8N 125.3E 47927 24.3N 124.2E 47918
	140800	24.14	124.7E	LAND			5//43 50000		24.8N 125.3E 47997
	140900	24.3N	124.9E	LAND			24/23 50316		24.8N 125.3EI 47997
	140900	24.24		LAND			6///3 70604		24.3N 124.2EI 47918 24.8N 125.3EI 47927
	141000	24.4N	124.7E	LAND			20713 53114		24.8N 125.3EI 47927
	121100	24.51	124.7E	LAND			6///3 73507		24.3N 124.2E 47918
	141100	24.5N	124.6E			50	54/63 5300¥	ENE MONO 3220	24.8N 125.3E 47927 24.8N 125.3E 47927
57	141100		124.5E	LAND	FAIR	~11	32993 63006	E4E MUNU 3550	24.8N 125.3E 47927 24.0N 121.6E 46649
	141200	24.59	38.6E	LAND			6///3 50108		24.8N 125.3E 47927
	141200				FAIR	58	A7773 30100	EVE MOVO 3220	24.8N 125.3E 479P7
	141200	24.79	124.58	LAND	F 4 4 ft		6///3 73407	Eve interior	24.3N 124.2E 47918
	141235	24.74	124.8E	LAND	POOR		117775 15101		26.4N 127.8E 47931
	141235		125•0E 125•2E	LAND	PODA				26.4N 127.8E 47931
	141300	24 . BN	124.5E	LAND	FAIR	30		EAE HUNE 3550	24.8N 125.3EI 47997
65	141300	24. AN	124.6F	LAND	,		22933 53608	• • • • • • • • • • • • • • • • • • • •	C4"AM 151"DEI VODAA
66	141300	24 - TN	124-6F	LAND			65/63 53607		24.8N 12543EI 47927
67	141300	24.5N	124.7E	LAND			6///3 73005		24.8N 125.3E 47977 24.3N 124.2E 47916 26.4N 127.8E 47931
	141310	24.5N	125.4E	LAND	Pn0R				26.4N 127.8E 47931
69	141400	24.9N	124.5E	LAND	FAIR	30		EVE MOVE 3270	24.8N 12563E 47927
70	141400	23.9N	124.6E	LAND			6///3 53605		24.8N 125.3E 47927
71	141400	24.7N	124.6E	LAND			6///3 73404		24.3N 124.2E 47918
7.2	141435	<del>24 - 9</del> N	124-85	f"₩N@	PODE				26.4H 127.8E 17991 24.3H 124.2E 17998
73	141200	24.4N	124075	LANU			6///3 73208		24.3N 124.2E 47918
74	141500		124.5E		- •-		6///3 53211	5E No 2220	24.8N 125.3EI 47997
75	141500			LAND	FAIR	30		EYE MNYG 3220	24.6N 125.3E 47927
76	141500	24.9N		LAND			6///3 52705		24.8N 125.3E 47927 24.0N 121.6E 46699
77			124 - 2E				21964 52720 6//3 73306		24.3N 124.2EI 47996
79	141600 141600	24.9N	124.6E 124.4E	LAND	FAIR	30	1,7775 75540	EVE MOVE 3610	24.8N 125.3E 47997
	141700	25 - TN	124.3E	LAND	PRIN	71/	21983 53311	Erc Amera Solo	24.8M 125.3E 47997
	141700	25 04	124.5E	LAND			6///2 73407		24.3N 124.2E 47918
	141700	24 3W	124.3E	LAND	FAIR	30	(),,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	EYE MOVE 3510	24.8N 125.3E 47927
	141700	25 - 1 M	124.4E	LAND				•	24.0N 121.6E 46699
84	141800	25.2N	124.3E	LAND			55/43 53410		24.8N 125.3EI 47927
85	141800	25.2N	124.5E	LAND			6///2 73608		24.3N 124.2E: 47918
86	141800	25.3N	124.4E	LAND	FAIR	30		EYE HOVG 3610	24.8N 125.3E: 47927
<ul><li>B7</li></ul>	141310	25.1N	124.4E	LAND	FAIR .				26.4N 127.8E 47931
	141935	24.5N	124.5E	LAND	Pn0R				26.4N 127.8E 47971
	141900	25.4N	124.3E	LAND			10915 50316		24.0N 121.6E 46699
90	141900	25.3N	124.SE	LAND	FAIR	30		EVE MOVE 3220 EVE STAR	24.8N 125-3E 47977
91	142000	25.3N	35.45E	LAND	FAIR	70	nc.113 coss.	EVE STAR	
	142000						25/13 50000		
	142000				na NA		6///2 73507	PSBL CNTR	24.3N 124.2E: 47918 26.4N 127.8E: 47931
94	142010	25.14	124-3E	LAND	PnOR		21944 50509	SOF CHIK	24.0N 121.6E 46599
	142100						6///2 73207		24.3N 124.2E 47918
96 97	142100 142100	25 41	124.25	OHA.I	FAIR	30	WALLE LACAL	EVE MOVA 3610	24.8M 125.3E 47997
	142100		124.3E				25/43 50508		24.8N 125.3E 47927
60	142135	25.5	124.2F	LAND	POOR		2	PSBL CHTR	26.4N 127.8E 47931
	142200		124.4E				5//43 50607		24.8N 125.3E 47927
101	142200	25.4N	124.4E	LAND			6///3 73303		24.3N 124.2E: 47918
	142200	25.4N	124.38	LAND			25/45		24.0N 121.6E 46699
	142200		124.3E		Pn0R			EYE MOVG 3605	24.8N 125.3E 47927
	142210		124.2E	LAND	PnOR			PEBL CHTR	26.4N 127.BE 47931
105	142235	25.3N	324.4E	LAND	POOR			PSBL CNTR	26.4N 127.8E 47991
106	142300	25.50	324.4E	LAND			6///2 73403		24.3H 124.2E 47918
	142300		124.6E	LAND			5//43 50311		24.8H 125.3E 47927
	142300		124.3E		PnOR			EYE MOVE 3210	26.3N 125.8E 47929
109	142310		124.SE	LAND	PnOR			PSBL CNTR	26.4M 127.8EI 47931
	150000		124.5E	LAND	Pn0R		F * * * * * * * * * * * * * * * * * * *	EYE MUNG 0550	26.3N 125.8E 47929
111	150000	25.9N	124.5	LAND			5///3 51415		24.8m 125.3E 47927 24.3m 124.2E 47918
112	1 < 0 0 0 0	25.5N	124.4E	LAND	POOR		6///2 70104	PSBL CNTR	24.3N 124.2E 47918 26.4N 127.8E 47931
112	150010								

114	150035	26.0N 124.3E	LAMO	POUR			PERE CATH	38.751 MA.85	47931
115	150100	24.9N 124.3E	LAND	POUR			EYE HOVE 3220	26.3₩ 125.8%	.7925
116	150135	24.2N 124.5E	LAVD	POUR			PSBL CNTR	26.4N 127.8E	47931
117	150200	24.4N 174.5E	LAND			6///3 53611		24.8N 125.3E	47927
118	1=0200	26.2N 174.3E	CHAJ	POOR			EVE MOVE 3620	26.3N 125.8E	47929
119	150235	76.4N 174.5E	LAND	POUR			PSBL CNTR	26.4N 127.8E	47931
120	150300	25.5N 124.4E	LAND			6///4 53414		24.8N 125.3E	47927
121	140300	26.4N 124.JE	LAND	POOR			EYF MOVE 3620	26.3N 125.BE	47929
122	150310	24.74 124.7E	LAND	POOR			PSBL CNTH	26.4N 127.8E	47931
123	150500	23.9N 125.0E	LAND	GOUD	50		EYE MOVG 3120	24.HN 125.3E	47927
124	150500	27. 2M 123.9E	LAND			6///4 53226		24.8N 125.3E	47927
*125	150535	27.74 124.2E	LAND	Phük			PSAL CATH	26.4N 127.8E	47931
126	150700	27.2N 123.8E	LAND	FAIR	40		EYE MOVE 2920	26.3N 125.BE	47929
*127	150710	27.9H 124.2E	LAND	POUR			PSBL CNTR	26.4N 127.BE	47931
+128	150735	27.2N 125.0E	LAND	PODR			PERL CUTH	26.4N 127.8E	47931
129	150800	27.1v 123.7E	LAND	, ,,=,,		6///3 72909	FADE CATA	24.8N 125.3E	47927
130	150800	27.2N 123.8E	LAND	FAIR	50		EYE STNR	26.3K 125.8E	47929
131	150900	27.1N 123.8E	AND			20973 50000	C. C. C	24.84 125.3E	47927
132	150900	27.2N 123.9E	LAND	FAIH	50	7.177.5 30-07	EVE STUR	26.3N 125.8E	47729
133	151000	27. IN 123.4E	LAND	, 41,	-,	5//43 50000	210 3144	24.8N 125.3E	47927
134	151100	27.3N 123.RE	LAND			5//43 53609		74.RN 125.3E.	17927
135	151100	27.24 123.BE	LAND	FAIR	55	17743 13007	EYE MOVE 3210	26.3N 125.8E	47929
136	151100	23.8× 123.8E	LAND	FAIR	55		EVE MOVE 3210	26.2₩ 127.7E	47930
137	151200	27.5N 123.9E	LAND	7 411		6//44 50211	EAL MONEY DETA	24.8N 125.3E	47927
138	151200	27.5M 123.7E	LAND	FAIR	55	, 30211	EVE MOVE 3210	26.3N 125.8E	7929
139	151300	27.5N 123.9E	LAND	F 44 F	٦.,	h//14 50000	EAS MINER SETO	24.8N 125.3E	47927
140	151300	27.5N 123.8E	LAND	FAIR	30	, (+ 30000	EYE MOVE 3610	26.3N 125.8E	47929
141	151400	27.5N 123.9E	LAND	7 4 2 11	***	6///4 53606	EAC MILEU 2010	24.8N 125.3E	47927
142	151400	27.3N 124.0E	LAND	GOOD	55	m///4 33000	EVE MOVG U215	26.3N 125.8E	47929
143	151500		LAND	6700	60		EYE MOVE 0120	26.3M 125.0E	47929
144	151700	27.94 124.0E	LAND	6า0ย	40 40		EVE MOVE 3620	26.3N 125.8E	
145		28.3N 123.8E		POOR	<b>►</b> U		EAE WOAR 3050		47929
145	151900	24.5N 123.8E	LAND	Pilok			NAV ACCIHACY ON	36.38 PE.35	47929
	151930	30.451 NE.RS	ACFT				NOT MULTIPACT ON		54435
147	152151	29.2N 123.RE	ACFT	0.00			PSHL CATR	26 45 407 05	54435
148	152335	25.4N 124.2E	LAND	POOR			PAGE CHIM	26.4N 127.BE	47931

#### SUPER TYPHOON JUDY

Flx	TIME	FTX					
NO.	(7)	POSITION .	ACCRY	DAJSWK CODE	SATFIFTE	COMMENTS	SITE
1	151310	13.7N 150.1E	PCN 6		DMSP35		PGTW
2	152238	13.2N 150.4E	PCN 5	T0+0/0+0	DMSP3A	INI Jas	PGT#
3	141120	17.5% 145.48	PCN 5		DMCD34		PGTW
4	162134	13.1N 144.1E	PCN 5		Dwsp37	EDGE OF DATA	PGTW
5	170055	13.7N 143.2E	PCN 5	T3.0/3.0 /D3.0/27			PGT#
6	170132	13.7N 142.9E	PCN 6		DWCB34		PGTW
7	170133	14.1N 142.9E	PCN 5	T3.0/3.0	りゃくりょう	INI Jas	RPHK
8	171015	13.0N 140.8E	PCN 5		045037		PGTW
¥	171155	14.44 140.3E	PCN 5		044534		PGTW
10	171414	14.4N 140.5E	PCV 5		0490 15		PGTW
11	171414	14.9N 140.4E	PCN 6		DMSP35		RODN
12	172114	15.4N 138.7E	PCN 6		DMSP37		PGT#
13	172345	15.4N 138.6E	PCN 5	T4-0/4-0 /D1-0/231	IRC DUSPIA		PGT₩
14	172345	15.4N 13A.7E	PCN 3	T4.0/4.0	りゅくちょん	SPC IINI	RODN
15	180036	15.4N 139.5E	PCN 5		りゃくちょう		PGTW
16	140036	15.5% 138.5E	PCN 5	T4+0/4+0+/01+0/23	IRC DHSP39		RPMK
17	180114	15.6N 138.4E	PCN 5		DWSP35		PGTW
18	190954	14.4N 137.6E	PC4 6		D45P 77		PGTW
19	141226	16.7N 137.1E	PCN 5		DWSP3A		PGTW
20	191355	17.1M 137.0E	PCV 5		DMSP75		PGTW
21	191355	14.54 137.2E	PON 5		DMSP 15		RODN
22	181455	16.74 137.0E	PCN 5		ひゃくりょう		RPMK
23	192054	17.9N 136.1E	PCN 1		DMSP37		PGTW
24	142327	18.24 135.BE	PCN 1	T6.0/6.0 /D2.0/24	IRC DMSPRA		PGTW
25	190159	14.54 135.6E	PC4 I		Duspas		PGTW
59	190237	14.3N 135.5E	PCV I	T6.0/6.0 /D1.5/26	IRC DMSP35		RPMK
27	100237	14.54 135.58	PCN I		DMense		PGTW
28	190734	19.4x 134.9E	Prv 2		Duch 37		PGTW
29	131208	19.74 134.6E	PCV 1		りゃんのろぞ		PGT₩
30	191258	14.9N 134.7E	PCN 1		DMCDJA		PGTW
31	191337	20.0M 134.8E	PCV 2		045075		PGTW
35	laisla	17.74 134.7E	PCN 1		DWSP75		RPMK
33	191519	19.7N 134.4E	PCN 1		DMCDJ5		RODN
34	192034	20.5N 134.4E	PCN 5		Deces 1		PGTW
35	192309	21.3N 133.8E	PCN L	T5.0/6.0 /41.0/241	ARC DACPER		PGTW
36	200140	21.6N 133.6E	PCN I	T7.0/7.0 /D1.0/23			RPMK
37	200140	21.54 133.6E	PCN I	T6.0/6.0	DHSP34	SPC 11NI	RODN
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38	5005T3	51.7N	137.6E	PCN 1		DMCB32		ROON
39		21.7N		PCN 1		044634		PGTW
40	200914		132.8E	PCN 2		045P37		PGTW
41	Zn1055		132.4E	PCN 4		DMSP37		RPMK
42	201150		132.5€	PCN 5		DMCDAR		PGTW
43	541533		132.1E	PCN 5		Ducoso		PGTW
4.4	201500		131.9E	PCN ≥		OMEDSA		RPMK
45	201500		131.9E	PCN 3		DMZB35		RODN
+6	201500		131.7E	PCN 1		045935		PGTW
47	2n2155		331.68	PCN 3	12.0/6.0 /MS.D/SOHHS	DMSP37		RPMK
48	202155		31.16	PC4 3		DMCD31		PGT#
4.		23.4N	131.1E	PCN 3	T5.0/5.0 /W1.0/22HRS	042h3Y		RODN
5υ	210033	23.34	131.JE	PON 3	T3.0/5.0 /SU.0/25HHS	OMERS		PGTW
51	510151		130.9E	PON 3		ひゃくちょう		ROUN
52	210121		130.9E	PCN 4		DWZDZU		RPMK
53	210121		34.061	PCN 3		Owebsa		PGTW
54	210200	23.54	330.8E	PCN 3		045632		PGTH
55	211036	24.34	124.9E	PCN 5		Dusear		RODN
56	211036	23.7N	129.7E	PCN 4		045977		PGTW
57	211550	74.4N	129.6E	PON 5		Omeban		PGI⊯
58	211314	24.5N	120.3E	PCN 5		DMSP34	CI DOWN	₽ĢT₩
59	211441	24.3N	150.5E	PCN 2		045632		RPMK
60	211442	24.3N	150.SE	PCN 1		Duspas		RODN
6ì	211442	24.7N	120.DE	PCY 5		045612		PGTW
62	212135	24.5N	128.2E	PCN I		DMSP37		RODN
63	212135	24.44	12R.1E	PCN I	T5.0/5.0 /S0.0/Z4HRS	Dadbill		RPMK
64	212135	24.44	12R.1E	Pr4 2		DWSP37		PGT#
65	220015		127.7E	PCN 3	T4.5/5.0 /W0.5/24HRS	DMSP 34		RODN
66	220015		127.7E	PCN 3	74.5/4.5 /WD.5/24HRS	Dadbdy		PGT₩
67	20105		127.4E	PrN 3		Dwcozu		RODN
68	220142		127.4E	PCN 3		DWSP75		PGTW
69	220243		127.5E	PCN 3		Duspay		RKS0
70	2>0243		127.4E	PCN 3		DMSP39		RODN
71	221016		126.8E	PCN 6		DMSP37		RODN
72	221016		127.0E	PCN 6		Dugu 37		₽GT₩
73	221256		126.7E	PCN 3		Duchav		PGT₩
74	221256		124.8E	PCN 5		DMSH3H		RODN
75	221343		124.4E	PCN 4		DMSP39		RPMK
76	271343		124.8E	PCN 5		Duchad		RKSO
77	221343	25. IN	126.8E	PCN 5		DMSP39		RODN
78	271423	25. AN	124.6E	PCN 5		DMSP35		PG₹₩
79	2>2115		125.9E	PCN 3		DMSP37		PGTW
80	222115	25.5M	126.1E	PCN 3		0MSP37		ROUN
81	222115		125.9E	PCN 2		DMSP37		RPMK
82	222357		125.8E	PCN 5	T5.0/5.0	DMSP36	INI 1 DOS	RKS0
B3	222357		125.5E	PCN 5	T5.0/5.0-/00.5/24HRS	DMSP36		PGTW
84	230224		125.2E	PCN 1	T5.0/5.0 /50.0/29HRS	DMSP39		RPMK
85	230224		125.1E	PCN 1	T5.0/5.0 /00.5/26HHS	DMCD30		RODN
86	230224		125.3E	PCN 1	12000 7 700 37 200	DMSP39		RKSO
87	230305		125.1E	PCN 1		0MSP35		RODN
88	230955		123.9E	PCN 2		DMSP37		RPMK
89	230955		123.HE	PCN 2		DMSP37		RODN
90	270955		124.0E	PCN I		Duspa7		PGTW
91	231136		123.7E	PCN 2		DMSP37		RPMK
92	271238			PCN 1		DUSPRA		PGTW
93			123.7E	PCN 1		DMSP34		RODN
94	231238		123.7E	PON I		045939		RKSO
95	231324		123.6E	PCN 1		DMSP39		PGTW
96	231324		123.7E	PCN 3		045935		RKSO
97	211547		123.35			DMSP35		RODN
	231547		127.3E	PCN 1		Dugp 37		RPMK
98	232236		123.25	PCN 2		045937		RODN
99	232236		123.05	PCN 1	-4 0/5 0 /U3 0/24MDs	DMSP36		PGTW
100	212338		122.7E	PCN 1	T4+0/5+0 /W1+0/24HRS	DWSP36		RPMK
101	240120		122.1E	PCN 3 PCN 1		DMSP39		PGTW
102	240205		122.7E		-6 a.m a (u) a.2449c	DWSP39		RPMK
103	240205		122.5E	PCN 1	T4.0/5.0-/W1.0/24HRS	DMSP39		RKSO
104	240205		122.6E	PCN I	T6.0/6.0-/D1.0/26HRS	DMSP35		RKSO
105	240246		122.6E	PCN I PCN I	16.0/6.0-/D1.0/24HRS	DASP35		RODN
106	240247		122.7E		0 / D - V - / D I - U / C - OK	DMSP37		RKSO
107	241117		122.6E	PCN 3		DMSP37		RPMK
108 109	241117		122.8E	PCN 4 PCN 3		OMSP39		PGTW
110	241401			PCN 3		DMSP36		RPMK
111	241525	30 30	122.4E	PCN 3		DMSP35		RKSO
112				PCN 3		045632		RODN
113	241528	30.41	155.2E	PCN 3	T3.0/4.0 /W1.0/20HRs	DMSP37		RPMK
114				PCN 3		DMSP37		RODN
115	242216		122.8E	PCN 3	T4.0/5.0-/WZ.0/23HRS	DMSP3A		RKSO
116	250102		123.2F	PCN 3	T3-0/4-0 /W1-0/26HRs	DWChid		PGTW
117	250146		123.2E	PON 3		DWZDJA		RKSO
	250558			PCN	T4.0/5.0-/WZ.0/24HRS	Duspah		RODN
118	250228		123.4E	PCN 3	· · · · · · · · · · · · · · · · · · ·	DMSP37		RPMK
119 120	251056 251056		124.3E	PCN 3		0#5937		ROUN
121	251246		124.0E	PCN 5		OMED38		RKSO
155	251246		124.4E	PCN 5		DM2634		PGTW
123	251246			PCN 3		045034		RPMK
124			124.4E	PCN 5		045935		PGTW
	251510		124.55	PCN 3		0m5P35		RODN
125	251510		124.7E	PCN 5		045935		RKSO
126	251510			PCN 3	T2.0/3.0-/W1.0/24HRS	D#5P37		RPMK
127	252155		125.9E	PCN 3	, ==U/ 3eU-/ RIeU/ 5eDK	DMSP37		RODN
128	252156		126+1E			DMCB36		RPMK
129	240045		127.5E	PCN 3	T2.0/3.0 /W1.0/24HRS	DMZB34		PGTW
130	240127		124.2E			DMSP35		RODN
131	240210		154.8E	PCN 3	T2.0/3.0-/W2.0/24HRS	DMSP35		PGTW
132	240210		124.55	Prv 5	12.0/3.0-/42.0/25HRS	DMSP35		RK\$0
133	240210		124.7E	PCN 3	1-41/36V-/#C4U/C3UK	DMSP37		RODA
134	261036		120.55			DHSP37		RPMK
135	241036	3 7# <del>4</del> 4	128.3E	PņN 3		U-3F 1/		nr m

137 138 139	261227 261325 261451	34.3N 120.2E 34.5N 129.0E	PAN 3 PAN 5 PAN 5	Dweb 34 Dweb 34 Dweb 30 Dweb 30 Dweb 30	RKSO PGTW RPMK RKSO BOOM
140	541421	34 + 24 [29 + 0];	PCA 6	DWSP35	RODN

# ATROPART FIXES

FIX NO.	TTME (7)	FTX POSTTION	FLT LVL	700 w 3 HGT	08S MSLP			\B 4G - A 4D				-#NU		CRY /MET	EYE SHAPE	EYE ORIEN- OTAW/TATION	ONTY THE DEVECT	MSN NO.
1	152341	13+5A: 193+5E	70048	3069	998	35	110	70	090	54	030	15	,	5				_
2	170303	14.0N 142.7E	700MH	3043	995		360	15	060		350	90		10			+1H +12. +12	
3	170,505	14.24 147.2E	7 n g m d	3025	994		090	16	180		090	16		10			+11 +11 +10 +11 +10	5
4	174048	14.3M 139.5E	700MH	2992	987		090	15	170		090	10	4		CLRCULAR	10	+11 +12 +14 26	•
כ	140554	15.3N 13R.ZE	700mb	>707	956	55	270	10	0.30	64	260	• 5	1	ä	CIRCULAR	•	+15 +11	
6	180945	16.5N 137.HE	700MB	2717	956		320	5	350	90	330	5	2	2	CIRCULAR	5	+13 +18 +10	I
7	181932	17.7N 136.3E	700MB	2411	922				360	93	280	5	3	7		•	+18 +17	5
В	192149	17.7N 134.2E	700MB	>336	7]4	55	260	12	720	90	260	7	- 1	ı	CIRCULAR	5	+14 +23 +18	5
9	191036	19.5M 134.8E	70048	2295	909				280	92	170	15	•	3	CIHCHLAR	ž	+15 +15	6
lu	191921	20.7N 134.3E	7.0MH	2121	889				270	108	160	Ε,	5	5			+34 +18	7
11	192145	21.0N 134.0E	70000	2041	987		060	15		110		5	5	2	CIRCHLAR	5	+13 +24 +15	7
12	2n0500	22.1× 137.1E	7 n 0 mH	2591	908	130	030	3	150	136	030	4	7	2			+19 +18	8
13	200843	22.54 133.0E	700MH	238n	919		580	40	340	110	270	10	2	2	CIRCULAR	7	+18 +19 +15	8
34	202259	23.3N 131.2E	700MB	2579	940		n 2 0	30	0.20		120	14	5	5	CIRCULAR	10	+17 +18 +12	9
15	210300	23.5N 130.HE	710MB	2611	945		010	30	979		010	30	5	10	CIRCULAR	25	*18 *18 *14	9
16	210503	24.2N 130.5E	7 r OMB	2613	945	100		10	259		170	40	10	5			+20 +15	10
17	210842	24.2N 130.2E	70 NMB	2614	944		360	10	340	76	270	3 n	5	2	CIRCULAR	30	+14 +18 +15	10
18	212506	24.2N 12A.2E	7 n OMB	267a	952			50	110		360	155	4	5			+16 +15 +15	11
19	250117	24.3N 127.8E	700MB	2679			350	15	340			30		5			+19 +16	11
20	220247	24.3N 127.6E	700MB	>684	951	95	030	35	150		030	150	4	5			+18 +19 +17	11
21	220650	24.2H 127.3E	700MB	267a	953				120		020		5	3			+16 +15	12
22	2>0958	24.3N 127.2E	700MB	2665	949	₹5	300	15	290			62	•	5	CIRCHLAR	35	+14 +15 +15	12
23	221335	25.2N 126.2E	7 n 0 MB	2636	948				1.40		050	91	7	В			+18 +15	13
24	5>5500	25.6N 125.9E	710MB	2667	946		120		1 AO		120	91	3		CIRCULAR	20	+13 +18 +16	13
25	230600	26.9N 124.3E	7 a 0 M H	2669	952			1 90	150		080	15	5	2			+16-+15	14
26	230818	27.1N 174.2E	700MB	2669	950	40	140	140	510	65	140	30	- 5	5	CIRCHLAR	15	+14 +15 +15	14

### PAJAH FIXES

F1x Nu.	11ME (7)	FTY POSTTĮŪN	RADAR	ACCRY	EYE SHAPE	EYF	RANNH-CODE ASWAH TOUFF	COMMENTS	RADAR Posttton	SITF WHO HO.
1	161635	13.1N 145.1E		FAIR				NFG WALL CLD	13.6H 144.9E	91218
2	161710	13.2N 144.9E	LAND	FAIR	ELLIPTICAL			AXIS 10/5	13.6M 144.9E	91218
3	141935	13.54 144.5E	LAND						13.6N 144.9E	91218
	142010	13.5M 144.2E	LAND	FAIR	CIRCULAR	75		CNTR OPFN SW-N	13.6N 144.9E	91518
5	142135	13.9N 147.BE	LAND	FAIR	CIRCULAR	30		NFG WALL CLD OPEN SW AND NE	13.6N 144.9E	91218
6	210600	23.4N 13n.3E	LAND				308/4 4////		26.1M 127.7E	47937
, K	210700	24.0N 130.4E	LAND				30842 53022		26.1M 127.7E	47937
9	210500 210900	24.0N 130.2E	LAND	00			35/// 52709		26.1M 127.7E	47937
10	210900	24.2N 130.2E 24.1N 130.1E	LAND	60 <b>0</b> D		40	25 / 52010		26.1M 127.7E	47937
ii	210300	24.1N 130.1E	LAND	GnOD		4.0	35/// 53010		26.1M 127.7E	47977
15	211000	24.1N 129.8E	LAND	65DD		4.0		E.E. Maria 2004	26. IN 127.7E	47937
13	211100	24.04 129.8E	LAND	9:100		76	35//0 52412	EAE MUNU 5850	26.1N 127.7E	47997
14	211100	24.1N 129.7E	LAND	FAIR		40	37770 32712	EYE MOVG 2720	26.1W 127.7E	47937
15	211200	24.0N 129.4E	LAND	1440		417	5///2 72611	EAE MINAN SISA	26.1N 127.7E	47937
16	211200	24.1N 129.5E	LAND	FAIR		40	17772 12011	EVE MOVG 2720	26.1% 127.7E	47937 47937
17	211300	24.0N 129.3E	LAND			-•	5///1 72710	Fig. Will File	26.1N 127.7E	47937
18	211300	24.1N 129.4E	LAND	GOOD		4.0		EYE MOVE 2720	26.1N 127.7E	47937
19	211400	24.1N 129.2E	LAND	3.,			5///2 72707	CIC MINI EIE	26.1N 127.7E	47937
20	211400	24.14 120.2E	LAND	6000		40		EYE MOVE 2720	26. IN 127.7E	47937
51	211500	24.1v 129.1E	LAND	0			5///2 72806	Ere Mire Eree	26.1N 127.7E	47937
22	211500	24.1N 129.1E	LAND	POOR				EVE MONE STED	26.1N 127.7E	47937
23	211500	24.24 129.2E	LAND				5///2 70408	•	26.1W 127.7E	47997
24	211200	24.1N 12R.9E	LAND	POOR				EYE MOVA 2720	26.1N 127.7E	47937
25	211700	24.3N 12R.9E	LAND				5///3 73107	_	26.1N 127.7E	47937
26	211700	24.2N 12R.7E	LAND	PODR				EYE MOVG 2720	26.1N 127.7E	47937
27	211800	24.3v 128.9E	LAND				35//3 73307		26.1N 127.7E	47937
28	211900	24.24 12A.5E	CNAJ	PODR				EVE MOVE 2720	26. IN 127.7E	47937
29	211900	24.3N 12A.7E	LAND				25//3 72909		26.1N 127.7E	47937
30	211910	24.24 128.5E	LAND	POOR				EYE STUR	26.1N 127.7E	47997
31	212000	24.3N 12R.6E	LAND				6///1 72706		26.1W 127.7E	47937
32	212000	24.4N 128.5E	LAND	GOOD		<b>4</b> 0			26.1M 127.7E:	47937
33 34	212100	24.34 12R.3E	LAND	00			6///1 72611		26.1W 127.7E	47937
35	212100 212200	24.6N 12R.3E 24.2N 12R.2E	LAND	POOR			F	EVE MOVA 2715	26.1N 127.7E	47937
36	214200	24.34 17A.3E	LAND	Pn0R			5///1 72609		26.1N 127.7E	47937
37	212300	24.3N 12R.0E	LAND	POOR				EYE MOVE 2715	26.1N 127.7E	47937
38	220000	24.3N 127.9E	LAND	PHOR			F	EYE MOVE 2715	26.1W 127.7E	47937
39	220000	24.3N 127.9E	LAND	POOR			5///3 72808	Euf Have 2725	26.IN 127.7E	47977
40	220100	24.3N 127.7E	LAND	PODR				EVE MOVE 2720	26.14 127.7E	47977
41	220200	27.0N 127.5E	LAND	F 1,0011			3///2 72719	EYE MOVG 2730	26.1M 127.7E	47937
42	220300	24.24 127.5E	LAND				3///2 72507		26.1M 127.7E:	47937
43	220300	24.3N 127.2E	LAND	POOR				EVE MOVE 2320	26.1N 127.7E	47937 47937
44	2>0400	24.14 127.2E	LAND				22704 5////	Era Inchia Rapa	24.8N 125.3E	47927
45	220400	24.1N 127.3E	LAND				3///1 72511		26.14 127.7E	47937
46	220500	24.1N 127.1E	LAND				6//// 50000		24 3M 124 2E	47918
47	220500	24.2N 127.2E	LAND				22814 5330b		24.8N 125.3E	47927
46	220500	24.1N 127.3E	LAND				5///1 72405		26.IN 127.7E	7937
			-							41.71

44	250500	24.34 127.3	35 1	A.O	ดาขม	70			FVF	MOVE	0920	76.1×	127.7F	47937
50		24.0N 127.1			4 100	,	6////	51204			0,20	24.31		47+1B
51		24.3N 127.3			GNUU	70			EYE	STNR		26.1N	127.75	47937
52		24.2N 127.2		AUD			5///1					26.1%	127.75	47937
53	220700	23.9N 127.1	IE L	AuD			6////	71604				26.1N 24.3N 26.1N	124.25	47918
54		24.1N 127.			PhoR				EYF	MOVG	2430	26.1%	12/./6	47937
55		24.3N 127.2		AND.			5///3 22803					26.1N 24.8N	121.15	47937 47927
56 57		24.1N 127.2 24.0N 127.1		AND ONA			6////					26 IN	124.25	47718
58		24.1N 127.			POOR		*****	,,,,,,,	EYE	STAR		26.3N 26.1N 26.4N	127.7E	47937
59		24.3N 127.2			POUR					•		26.4N	127.85	47991
60		24.1N 127.			POR				EVE	STNP		26.1N 24.HN	127.72	47997
61	220900	24.3N 127.2	SE Ĺ	AND			50974					24.HN	125.35	47927
62		24. 3N 127.2					21A7J	73605				26. LN	127.15	47937
63	220910	24.3N 127.	SE r		POUR			~ 7 t 0 t				26.4N	151.85	4797] 47927
64		24.4N 127.	2E L	AND	2-00		22963	23002				24.HN 26.4N	123+JE	47931
65	221035	24.3N 127-		OMA.	PooR		21473	52711				24.HN	125.38	47727
66 67	221100 221100	24.4N 127.			PhDR		,,,,,	34.14	EYE	Move	2420	26.1N	127.7E	47977
68	271100	24.4N 127.		AND			3///3	73204			-	76.IN	127.7E	47937
69	221110	24.1N 126.		AND	POUR							26.4N	127.BE	47971
70	221135	24.4N 127.		AND	POUR							26.4N 26.1N	127.BE	47931
71	2>1200	24.6N 126.	YE L	.AND	PoOR				EYŁ	MOUR	3525	26.1N	12/1/6	47937
72	551500	24.5N 126.		AND			2///3					26.1M 24.HN	12/1/2	47937 47927
73	2>1200	24.4N 126.		AND	0.00		21644	53414				26.4N	127.8F	47931
74	521510	24.4N 127.		AND	PhOR							26.4N	127.8E	47931
75 76	221335 221300	24.5N 126.		AND AND	POOR		22712	52814				24.HN	125.3E	47927
77	221300	24.74 126.		AND	<b>ცე</b> 00	45	, , , ,		EYF	MOVE	3020	26.1N	127.75	47937
78	221300	24.6N 126.		AND	4.,,••		21112	73011				26.14	127.7E	47937
79	2>1310	24.7N 126+		AND	POR							26.4N	127.8E	47931
80	2>1335	24.5N 126.		AND	PnOR							26.4N	127.8E	47991
81	221400	24.6N 126.	5E L	AND				11111				74.3N	124.2E	47918
82	551400	24.7N 126.		AND			21442	52906	E F	Move	3020	26 14	124.2E 125.3E 127.7E 127.7E 127.8E 127.8E 127.7E 127.7E 127.7E 127.7E 127.7E 127.8E 127.8E 127.8E	47927 47937
В3	5>1+00	24.7N 126.		AND	6100	45	c	73111	EVF	Mil Mit	3020	26 IN	127.7F	47937
84 85	2>1400 2>1410	24.7N 126.		_AND _AND	PODR		7///3	, 3 + 1 4				26.4N	127.82	47771
86	221435	24.7N 126.		AND	PnDR							26.4N	127.8E	4793]
87	221500	24.7N 126.		AND	GnDD	45			Ε×Ε	MOVE	2710	26. IN	127.7E	47937
88	221500	24.7N 126.		AND	J.,		5///3	73010				26.1N	127.7E	47937
89	221500	24.9N 126.		AND			21713	52911				24.BN	125.3E	47927
90	221500	24.6N 126.		AND			6////	00000				24 3N	124.2E	47918
91	2>1510	24.7N 126.		LAND	PoOR							26,4N	12/.BE	47931
92	221535	24.7N 126.	7E L	LAND	FAIR					Mous	2220	26 IN	127.0L	47931 47937
9.3	221600	24.1 126.	SE (	LAND	Gn <sup>O</sup> D	4.5	01717	53107	FAE	MINAR	3220	26 RM	125.3F	47927
94	271600	24.8N 126.	3E -	_AND			6////	53310				24.3N	124.2E	47918
95	2>1600 2>1610	24.7N 126.		_AND _AND	FAIR			33014				26.4N	127.BE	47971
96 97	221635	24.9N 126.		AND	FAIR							26.4N	127.BE 127.BE 127.7E	47931
98	221700	24.9N 126.		AND		45			EYE	Move	3520	26. IN	127.7E	47937
99	2>1700	24.7N 126.		AND			6////	73004				24.3N	124.2E 127.7E	4791B
100	2>1700	24.9N 12K.	3E L	AND			5///3	73004				26.1N	127.7E	47937
101	221700	25.9N 12A.		AHD			21413	53406				26 AN	125.3E	47927
102	2>1710	25.4N 126.	7E L	_GNA_	PhOR							26.48	127.8F	47931 47931
103	221735	25.2N 126.		_AND _AND	FAIR		21414	52904				24.8N	125.3E	47727
104 105	221800 221800	25.0N 126. 24.9N 126.		AND				73203				26.1N	127.8E 127.8E 125.3E	47937
106	221900	25.0N 126.		AND	G70D	45			EYF	MOVE	3510	70.1N	121.16	47937
107	221900	24.9N 126.		AND	0 / 0		6////	73207	_			24.3N	124.2E	47918
108	251900	25.0N 124.	3E L	LAND			6////	73405				24.3N	124.2E	47918
	521300	25.0N 126.	<b>3€</b> ι	L AND	_	_	5///2	73504				26.IN	127.7E	47937
	221900	25.0N 126.	0E (	LAND	ดา0ย	4.5	-1473	E4140	EVE	MOVE	3510		127.7E 125.3E	47977 47927
	2>1900	25.1M 124.	5E 1	LAND			216/3	50108					127.BE	7971
	221910	25.1M 126.	SE I	LAND	POUR POUR							26.4N	127.BE	47931
	2>1935 2>2000	25.2N 126.		LAND LAND	Pilon		3///3	73410				26.1N	127.7E	47937
	525000 525000	25.7N 125.	31	LAND				73512				74.JN	124.2E	47918
	222000	25.3N 126.		LAND			22513	53512				24.8N	125.3E	47927
117	2>2010	25.4N 126.	IE L	LAND	PnOR								127.8E	47931
118	254100	25.54 175.	.9E (	LAND			3///2	73415					127.7E	47937 47927
119	222100	25.5N 126.		LAND			47713	53514 73511					124.2E	47918
12u 121	2>2100	25.3N 126. 25.6N 126.	IF I	LAND LAND	PoOR		5////	10011					127.8E	47931
155	252110 252135	25.7N 126.	IF I	LAND	Pour							26.4N	127.8E	47931
123		25.7N 126.					3///2	73415				26,14	-127.7E-	47-227
	525500	25.5N 126.	0E (	LAND			6////	73308					124.2E	47918
	5>5500	25.7N 125.	9E (	LAND			5///3	53219				24.BN	125.3E	47927
126	2>2235	26.0N 126.	1E t	LAND	FAIR			72716				26 1M	127.8E	47931 47937
127	2>2300	26.0N 125.		LAND				73315					124.2E	47918
	252300	25.5% 125.		L AND				73109 53412					125.3E	47927
	252300 252310	25.9N 125.		LAND LAND	FAIR		, 3	J 1 -				76.4N	127.8E	47931
	222335	24.1N 124.		LAND	FAIR							26.4N	127.8E	47931
	230000	26.1N 125.	4E	LAND				53030					125.35	47927
133	230000	26.0N 125.	6E 1	EAID			5///4	73325					127.7E	47937
134	230010	24.14 124.	.1E 1		FAIR								127.8E	47931 47931
		54.5N 154.		LAND	FAIR		2000	53612					125.3E	47927
136	210100	25.4N 125.	9E	LAND				73116					127.7E	47937
	530100	26.3N 125.	15E	CIVAL	Po0R		-,,,,						127.BE	47931
	230110	26.4N 125.	SE	LAND	Pn0k								127.8E	47931
140	230200	26.4N 125	SE		***		20514	52816					125.3E	47927
141	230200	26.5N 125	4E	LAND				73312					127.7E	47937
142	230210	24.4N 125.	4E	LAND	P10H								127.8E	47931
143	230235	24.4M 125.	.4E	LAND	POR								127.8E	47971 47927
144	230300	24.5N 125	•0E					53113					123.3E	47937
		26.5N 124		CVAJ	0000		7///5	73115					27.8E	47931
		26.4M 125			P00R P00R								127.8E	47971
147	240135	25.70 125.	• • • •	LAND	Figur									. •

157 159 160 161 163 164 165 166 167 171 172	2 240 400 2 240 400 2 240 400 2 240 430 2 240 500 2 240	) 2n. Hn   2a. HE   26. Hn   124. TE   26. Hn   124	LAND POUR LAND FAIR LAND POUR LAND LAND POUR LAND LAND LAND LAND LAND LAND LAND LAND	45 45	30415 72805 22515 53012 21735 53008 31835 52909 31815 53408 6///5 53312	EYE MOVE 3330  EYE MOVE 2720  EYE MOVE 3320  EYE MOVE 3320  EYE MOVE 3320  EYE MOVE 3320  EYE MOVE 3220  EYE MOVE 3220  EYE MOVE 3220  EYE MOVE 3205  EYE MOVE 3205  EYE MOVE 3430  EYE MOVE 3415  EYE MOVE 3120		76.3N 125.8E 74.8N 125.3E 74.8N 125.3E 74.8N 125.3E 76.3N 125.8E 26.3N 125.8E 26.3N 125.8E 26.3N 125.8E 26.3N 125.8E 26.3N 125.8E 26.3N 125.8E 24.8N 125.3E 26.3N 125.8E 26.3N 125.8E 26.3N 125.8E 26.3N 125.8E	47937 47937 47937 47931 47931 47931 47931 47931 47931 47939
F1X NO.	T   M =   7	ETX MOTTTEOM	INTENSITY NEARE ESTIMATE DATA	ST (NM)	COMMENTS				
1	1=0000 151200	9.04 154.0E 11.50 150.0E	015 25 . 020 25						
NU.  1 2 2 3 3 4 4 5 6 6 7 7 8 8 9 9 10 11 12 13 16 16 17 18 17 18 12 22 21 22	181214 181912 181913 182145 182314 190753 190753 191026 191117 191155 192127 192358	FIX POSITION 12.0N 168.2E 16.7N 168.3E 16.9N 168.3E 16.5N 160.5E 13.6N 166.5E 13.6N 166.5E 14.8N 165.9E 14.8N 165.5E 14.8N 165.5E 14.8N 166.2E 15.6N 164.2E 17.7N 163.7E 19.1N 163.6E 18.9N 164.2E 17.7N 163.7E 19.1N 163.6E 18.9N 164.8E 27.0N 163.8E 27.0N 163.8E	PON 6 PON 6 PON 6 PON 5 PON 3 TILDO	CODE 54 /S0.0/24HR< /S0.0/21HR< /D0.5/24HR<	DMSP35 PSN 8S DMSP37 DMSP36 DMSP36 DMSP36 DMSP37 DMSP37 DMSP37 DMSP37 DMSP37 DMSP37 DMSP37 DMSP37 DMSP37 DMSP37 DMSP37 DMSP37 DMSP37 DMSP37 DMSP37 DMSP37 DMSP37 DMSP37	MMFNTS U on wk hl <sub>i</sub> conv activi	SITE TY KGMC PHIK PHIK PGTW PGTW PGTW PGTW PGTW PGTW PGTW PGTW		
FIX NO.	T†MEi (7)	FTX POSTTION	ĖL∏ 700w3 00 LVL HGT MSI		D MAX-FLT-LVL-G	NO ACCRY EYE	EYE' ORIEN-	EYF TEMPI (Ĉ)	MSN
1	190026	13.6N 166.6E	1500F1 100	7 25 330 56	0 140 25 060 1	20 4 10	DIAW/TATION	+25" +2A 3	T ND+
3	200100	17.0N 163.9E 19.7N 160.5E	1500FT 100 700MB 3165	9 10 120 75	5 210 15 110 180 15 230	35 5 5		+24 +24 2	
				SYN0>1	TTC FIXES				
FIX NO.	TYME! (7)		INTENSITY NEARES ESTIMATE DATA (		COMMENTS				
• 1 • 2	160000 170000	12.0N 168.0E 13.0N 168.0E	15 300 15 300						

### TROPICAL STORM KEN

Fix NU.	T t M = (7)	ETX POSTIJON	ACCRY	UVDPAK CONE	:	5475117	1E (	CO4MFN	rs		SITE		
• 1	010115	25.74 133.0E 25.84 132.4E	PCN 5	T1.0/1.0		Dwdnd	4	Jos			PGT# PGT#		
3	010200 010200	25.24 137.3E	PCN 5	T1.0/1.0		Dadh.i Dadh.i	S INII	SpC			PGTW RODN		
c 6	011016 011016	24.9H 132.6E	PCN 6			Dachs Labad					PGTW RODN		
7	011214	24.9N 137.2E 25.1N 132.5E	PON 5			DMCDA					PGTW		
B	011320	25.3N 132.2E	PCN 5			DMSPR					PGTW PGTW		
10	011442 012115	25.2N 132.1E 25.4N 132.2E	<b>PCA 7</b>	71.0/1.0 /S0	0.0/20HR9						PGT⊯		
11	020020	25.74 131.7E	PCN 3	•		Dweb3					PGTW PGTW		
13	020055 020141	25.44 131.9E 26.04 132.1E	Pris 3			DMSPR					PGTW		
14	020142	25.9N 132.7E	PCN 3	T1.0/1.0 /S0	0.0/24HR9	FASHO :					RODN PGTW		
15 16	020956	27.2N 131.3E	PCN 5			DMSPR	6				PSTW		
17 18	021423 022055	24.0N 131.7E	Prn 5 Prn 5	Tl.5/1.5		DMSP3		ads			PGTW RPMK		
19	022055	28.8N 130.8E	Prin 6	1743/143		DMSP3	7				#Tag		
20 • 21	020005	24.1N 129.9E	PCN 5	12.5/2.5-/01	1.5/27HR	РФРИД : РФРИД					PGT# RPMK		
55	030123 ES10F0	29.24 120.HE	PCN 5			DMSP3	15				PGTW		
23 • 2•	7150F0 7150F0	29.1N 129.4E 23.2N 130.1E	PCN 5	T3.0/3.0=/D2 T3.0/3.0	2.0/24HR	FGPMG :		365			RODN RKSO		
25	030936	30.7H 130.3E	PCN 6	13007,300		DMCD3	17				RODN		
26 • 27	070936 071117	31.1N 130.3E	PON 5			045P3					PGTW RODN		
28	031244	31.5N 131.0E	PCN 5			DMSP3	th.				PGTW		
30	031317 031318	31.7N 131.5E 31.7N 131.0E	PCN 3			DHSP3 DMSP					RPMK PGTW		
31	031404	32.0N 131.5E	PCN 3			DMSP3	15				RKSO		
32 33	031405 031405	31.74 131.2E 31.54 131.3E	PON 5 PON 6			DMSP3					PGT₩ Rodn		
34	031546	37.1N 131.3E	PON 6			DMSP3	15				RODN		
35 36	032035	32.5N 131.7E 32.9N 132.4E	PON 5			DMSP3					RKSO Rodn		
37	032035	33.0N 132.2E	PCN +			DMSP3					PGTW		
38 39	032035 032344	33.1N 132.3E	PCN 3	12.5/2.5=/DI	1.0/27HR	FARMO :					RKSO RPMK		
40	032344	33.9M 133.1E	PCN 3	T1.0/2.0 /W			16	LED na			PGTW PGTW		
41	040158	34.3N 134.4E	PC4 4			UMAPA		(IC			F01#		
					,	TREPART	FIXES						
FIX NO.	TIME (7)	FTX POSTTION	FLT LVL	70043 085 MGT MSLP	MAX-SFC- VEL/ARG	WND MA	X-FLT-LVI R/VEL/BR			EYE SHAPE	EYE ORIEN- DIAM/TATION		(C) MSN /SST NO.
1	012105	25.4v 132.1F	1500FT	998	40 030	40 12			2 5			+25' +25	1
2	020928	27.0N 131.0E 28.3N 130.4E	700MB	2884 977 3068 998	60 200 35 030	50 22			5 20 2 5	CIRCHLAR	50	+15 +18 +18 +11 +12 + 9	2
4	030725	30.3N 130.8E	7n0MB	2984 988	50 090	5 21	0 65 11	0 4ก	2 10			+10 +12: + 2:	
5	020913	30.7N 130.7E	700MB	2976 988	50 180	10 21	n 65 19	U 40	2 15			+13 +12 + 2	5
					:	PAJAH FI	XES						
FIX NU.	TTME (7)	FIX POSITION	RADAR A	EYF CCRY SHAPE	E DI		INB-CODE			COMMENTS		RADAR Position	SITF
1	012000	24.0N 130.5E	LAND			65/	// 50113					28.4N 129.5E	479n9
Š	020700	24.7N 131.2E	LAND			65/	18 11111					28.4N 129.5E	47909
3	020300	26.9N 131.2E 27.1N 131.1E	LAND LAND				//1 53512 //1 53413					28.4N 129.5E	47909 47909
5	021000	27.3N 130.9E	FWHD			65/	// 53113					28.4N 129.5E	47909 47909
.7		27.3N 130.7E	LAND LAND				// 52811 /// 52309					28.44 -129-5E	47909
8	021300	24.9N 130.6E	LAND				/// 51808					28.4N 129.5E	47909 47909
10	021400	27.1N 130.6E 27.2N 130.5E	LAND LAND			65/	/// 53512 /// 53211					28.4N 129.5E	47909
11	0>1600	27.4N 130.4E	LAND			65/	/// 53511 /// 50211					28.4% 129.5E	47909 47909
12 13	021700 021800	27.5N 130.5E	LAND LAND			65/	/// 50106					28.4N 129.5E	47909
14	021900 022100	27.9N 13n.5E	LAND				/// 53608 /// 50211					28.4N 129.5E	47909 47909
15 16	055500	29.24 130.6E 28.44 130.7E	LAND LAND			65/	/// 50113					28.4N 129.5E	47909
17 18	020000 020000	29.5N 130.6E 29.9N 130.4E	LAND LAND				/// 53308 /// 53319					28.4N 129.5E	47909 47909
19	0-0100	29.0N 130.2E	LAND			65/	/// 53212			-		28.4N 129.5E	47909
20 20	030200 030300	29.5N 13n.2E 29.6N 13n.3E					/// 53513 /// 50210					28.4N 129.5E	47989 47989
22	020400	24.6N 130.4E	LAND			6//	113 5////					30.6N 131.0E	47869
23 24	03U5D0 03U5D0	39.0N 130.4E 30.0N 130.5E				65 <i>/</i>	/// 50122 //4 50216					28.4M 129.5E	47969 47969
	031300	31.5N 131.1E					41 50208					33.4N 130.3E	47906
25	941300												

		0.04 T & U	31.74	131.5E	LAND	Phuk					
	27	031400	31.54	131.35	LAND				32 1	131.5E	47454
	28	031455		131.68		POUR	55/4	1 50316		130.3E	47406
		031500			LAND	E:JUR				131.55	
		031500			LAND			1 5////	36.26	132.65	47954
		031500		131.6E			55/1	l 50319			47792
	_ :	0 3 4 5 0 0			LAND		65//	1 50211		130.35	47406
		011500		131.78	LAMD		55/4	1 50319		132.0E	47792
		031700		131.68	LAND	POUR		· · · · · · · · · · · · · · · · · · ·		130.3E	47406
				131.7E	LAND		55///	/ 5////		131.55	47954
		031700		131.7E	LAND			50316		134.2E	47409
		031700	32.44	131.9E	CIVAJ			50222		132.6E	47792
		031701	32.44		LAND	PODR	,	30422		130.3E	47906
		031755	32.74		LAND	FAIR			32.IN	131.5€	47454
		UNEIFO	37.5N	131.9E	LAND		46441	50416	32.14	131.55	47454
		006160	32.54	132.08	LAND				34.3N	132.6E	47792
		008150	32.4N		CAND			1 50422	33.2N	134.25	47999
-	42 (	031855	32.48		LAND	FAIR	20241	50111		130.3E	47906
4	13 (	031900	32.94		LA/ID	. 43.1			33.7N	131.0E	474R0
4	4 (	041900	32.30		LAND			50322	34 3N	132.6E	47792
4		071955	31,2N		LAND	0-00	55///	50319		134.25	
		0.0026.0	33.14			POUR			33 7	131.05	47999
		032000			LAND		55//1	50516	36 36	131.05	47440
		012000	33.1N		LAND		55///	50314	37.3	132.66	47792
			33.3N		LA 10		24411	50316	33./N	134.25	47999
		001550	33.2N		LAND		55///	50411	.14 . 5N	135.66	47792
		14500	33.4N		LAND		2/4/1	50516 50619 50527	33.7N	134.2E	47999
		0.45500	33.3v		LAVD			50619	34.3N	132.6E	47792
		72300	31.7N		LAND			50527	33,2N	134.2E	47499
		172300	37.5N		LAND	*		50527	34.3N	132.6E	47792
			33.74		LAND	3		11111	33.20	134.25	47999
		40000	37. 9N	133.4E	LAND			50522	34.6N	135.6E	47773
5	6 0	40000	33.9N	133.5E	LAND			50616	34,6N	135.6E	47773
5	7 0		33.6N		LAND			50532	34.3N	132.6E	47792
5	8 0	40200	34.7N		LAND					134.2E	47499
5	9 0	14UB0U	35.5N 1		LAND			5////	34.3N	132.6E	47792
• 6	0 0		35.2N 1		LAND			50722	35.3∾	133.7E	47539
6	1 0		35.9N ]		LAND			40415	36.2N	135.1E	47705
6	5 0		36.1N 1		LAND		2201/		35.4N	138.78	47639
6			34.1N 1		LAND		2204/		35.3N	138.7E	47639
6			36.1N I		LAND		11772		36 2h	135.1E	47705
			36.4N 1		LAND		4586]		35 2N	137.0E	
6			34.2N 1				6586/	50525	35 24	137.0E	47536
					LAND		35/0/		33.2	137.05	47596
6			35.24 1		LAND		11712	50720	36 36	138.8E	47572
6			36.6N 1		CNAJ		6586/	50527	30.20	135.18	47705
	-		34.5N 1		LAND		21642	50630	33.2N	137.0E	47536
7			34.4N 1		LAND		60831		36.2N	135.1E	47705
7				37.2E			3581/		37./N	139.8E	47572
7			36.9N I		LAND		51742		37.7N	138.8E:	47572
7	. 0	41500	35.5N 1	34.8E	LAND		127//		36.24	136.lE	47705
									35.3∾	138.7E	47539

## TYPHOON LOLA

FIX NO.	TTME (7)	F   X P   O S   T     O W	&CnRY	DV1SAK	CODE	SATFLI TTE	COMMENTS	£11¢
								SITE
1	021120	21.9N 151.3E	PCN 5			Outeman		
2	021242	22.1N 151.0E	PCN 5			0msp36 0msp35		PGTW
3	022055	22.9H 150.9E	PCN 5	Tl.0/1.0	1	DMSP37	INIT 3ds	PGTW
4	U22056	22.4H 151.1E	PCV 6		•	D45037	1411 702	RPMK
5	0>5551	22.5M 151.3E	PCN 6			DASPRA		PGŢW
6	030036	22.34 151.1E	PCV 6	T2.0/2.0	)	DMSP39	Zec IINI	PGTW
7	070123	22.0H 151.3E	PCN 5	T1.0/1.0		DMSP35	INIT OUS	PGTW
8	020153	23.04 150.7E	Pon 5	T2.0/2.0		DMSP35	INII Das	RODN
9	030123	35.54 151.1E	PCN 6			DMSP35		RKSO
10	030936	22.7N 150.7E	Prv 5			DMSP37		PGTW
11	031103	23.04 150.7E	PCN 5			DMSPRA		PGTW
12	031136	23.1N 150.6E	PCN 5			DMSP39		PGTW PGTW
14	031405	22.5N 150.5E	PCN 5			DMSP35		RKSO
15	031405	23.54 150.4E	PCN 5			DUSPRE		PGTW
16	0720J5 0720J5	23.5N 144.0E	PCN 5	_		045937		RODN
17	032203	23.24 149.5E	PCN 6	13.0/3.0	/01.0/20HRs	DMSP77		PGIW
18	040017	23.3N 140.1E	PCN 4			DMSP3A	BEGINAING OF FYE	PGTW
19	040117	23.4N 14R.RE	PCN 3	_		DMCP34		PGTW
20	040104	23.94 149.DE	PCN 5		702.0/24HRs	DMSP35		RODN
21	040105	23.74 14A.HE	PCN 3	T3+5/3+5	/01.5/24HRs	DMSP3S		RKSO
25	040916	23.5% 14R.HE	PCN 4			DMSP35		PGT#
23	041117	24.1N 147.HE 24.3N 147.7E	PCN 3			Duspa7		PGTW
24	041226	24.4N 147.5E	PCN 5			DMCD34		PGTW
žš.	041346	24.5N 147.4E	PCN 3			DMSP36		PGTW
26	041346	24.7N 147.5E	PCN 3			DMSDAR		PGTW
21	041346	24.7N 147.6E	PCN 4			PF4PMG		RKSO
58	042015	24.7N 147.0E	PON 3 PON L			DMSP35		RODN
29	044015	24.94 146.7E	PCN 1		400 - 12 110-	DMSP37		RODN
30	042327	25.1M 146.7E	PCN I	13.075.0	\US-0\5+H&c	DMSP37		PGTW
31	042358	25.54 146.4E	PCN 2	-6		DMSP39		PGTW
32	042358	25.2N 146.5E	PON 1	13407540	<b>ND5.0\53H82</b>	Duchia		RODN
33	050046	25.3N 146.5E	PON 1			ONCD-10		PGTW
34	050046	25.2N 144.6E	PCN L	T4.54 5	403 - 42440-	DMSP35		RODN
3 5	0500+6	25.3N 144.5E	PON 1	1743/4+5	/D1.0/24HRS	DMSP35		RKSO
36		24.0N 144.4E	PCV 1			DMSP35		PGIW
			. 1, 7			DMCD77		PGTW

37	051208	26.1N 146.5E	Pon I		OMSPRA			PGTh
38	051240	26.3N 146.6E	PCN 1		Dusp39			PGTW
	051328	26.5N 146.4E	PCN 1		DMSP35			PGTW
39			PCN 2		DMSP35			RODN
40	051328	26.2N 146.3E			DMSP37			PGT₩
41	051955	27.0N 146.3E	PCN 2	"E A . F A . C A . (2) HDC	DMSP36			PGTW
42	052309	27.3N 146.6E	PCN 1	T5.0/5.0-/S0.0/21HRS	DMSP35			PGTW
43	040028	27.5N 144.6E	PCN I					PGTW
44	060121	27.5N 146.6E	PCN 1		DMSP39	**** *	040	RPMK
45	040121	27.5N 346.5E	PCN 1	T4.5/4.5	DREDSO	INI	045	PGTW
46	040835	27.7M 146.2E	PCN 4		DMCD37			PGTW
47	061150	29.3N 146.0E	PCN 1		DMSP36			
48	155190	28.9N 146.2E	PCN 1		045636			RODN
49	041551	28.7N 146.2E	PCN I		DMGD39			PG1w
50	061309	28.9N 146.0E	PCN-1		DMSP35			PGTW
51	061935	29.5N 144.0E	PCN 2		Trapmo			PGTW
52	070009	29.7N 146.2E	Prn 2		Duspah			PGTW
53	070101	30.1N 146.4E	PCN 1	14.5/4.5-	Duspay			RODN
54	070102	30.0N 146.4E	PON 3	T3.5/4.5 /W1.5/26HRS	DUSPRU			PGTW
55	070957	30.7N 146.5E	PCN I	100,574.5 7 42.057 = 5	DMSP37			PGTW
			PCNI		DMSP36			PGTW
56	071137	30.9N 146.4E	PCN 5		Dazosa			RODN
57	071202	31.7N 149.2E			DMSP39			PGTW
58	071202	31.7N 147.0E	PCN 5		DMSP35			PGTW
59	071432	32.0N 147.1E	PCN 3	-3	DMSP37			PGTW
60	072056	33.7N 148.2E	PCN 3	T2.0/3.0 /W1.5/20HRs	DMZD3V			PGTW
61	072233	34.0N 14R.6E	PCN 3	0 3 - 3 - 13 - 110 -				RODN
62	090043	34.2N 14R.9E	PCN 3	T2.5/3.5 /W2.0/24HR4	DMSP39			PGTW
63	040043	34.3N.148.8E			Deshar			FOIR

#### ATOCHAFT FIXES

F1X NO.	.TTME (7)	FIX POSTTION	FĹT ĻVL	70043 HGT	08S MSLP	MAX-SFC VEL/SRC	-WVD	MAX-						EYE SHAPE			RIEN- ATION			MP (F) / DP/SST	45 <b>N</b>
		D# 41 1.0 75	700MH	3046				0.40	45	270	15	R	3						.14.	+13	4
Ţ	031935		700MH	3001	990	45 090	>0	170.	49			6	2	ELLIPTICAL	25	20	170	+11	+15	+13	. 4
2	072046	23.5N 149.4E				65 320		360	71			>	5		15			+09	+14	+12	5
3	040809	24.9M 14P.1E	700MB	2913	978	35 270			50				5	•					+17		6
+	041913	24.4N 147.0E	700MB	2811				020	68				10	CIRCULAR	3 n				+15		6
ō.	042118	25.1N 146.HE	700MB	2/51	965	75 350							5	CIRCHLAR	311			• • •	+19		7
6	050504	25.7M 146.6E	7 n 0 4 H	2743		90 300		310	87				_		34			. 13	+19		,
7	050848	25.9N 146.5E	7 n 0 mH	275g	959	40 210			86		10		3	CIRCILLAR							8
. 8	051943	27.0V 146.4E	700MH	2065		45 250			82				3	ELLIPTICAL			0.50		+53		ü
ŭ	052120	27. IN 146.5E	7110415	2656		95 070	40	670		360			4	ELLIPTICAL	17	12	030		+17		•
10	040610	27.9N 146.5E	7 n p м H	2687	953	70 280	50	040	71	540	50	7	4						+13		
11	040850	28-1N 146-4E	700MH	2745	960	50 080	40	180	72	りより	95	2	5	CIRCULAR	50				+17		9
		24.7N 146.3E	70046	2869	70.5	75 080		050	60	330	30	45	0	CIRCILAR					+14		10
12	061943		700MB	289n	984	75 08		230	60	1/0	3.0	5	10	CIRCULAR	30			+11	+15	+14	10
13	042137	29.7N 146.2E			707	50 260		020		310		3	fi						+15	+12	11
14	070539	30.7N 146.4E	700MH	2907						1/0			3					. 4	+15		11
15	070929	31.2N 146.BE	700HB	2924	979								5							+12	jž
16	071846	33.2N 147.9E	70046	ンオカン		45 12				150									+17		12
17	072105	33.6N 148. LE	70048	3004		40 A6	140	170	49	000	152	4	5					+1=	+1,	¥16	1-

#### TYPHOON MAC

FIX	TIME:						
NO.	(7)	FIX Position	ACCRY	DADSAK CODE	SATFLETTE	COMMENTS	SITE
1	140008	11.8N 136.5E	PON 5	T0.8/N.0	DHEHBY	INII Ods	PGTW
2	140030	11.9N 134.5E	PCN 5		DWZD30		PGTW
3	140917 141250	11.5N 134.9E 11.9N 134.7E	PCN 5		DMSP37		PGT₩
5	141404	12.0N 134.2E	PCN 5		DMSP36 DMSP35		PGT# PGT#
6	142157	12.2N 133.6E	PCN 5	TU.0/Q.Q	0MSP37	INII Ods	RPMK
7	142350	12.2N 133.0E	PCN 5	T1.0/1.0 /D1.0/24HR9			PGTW
8	151037 151232	12.8N 131.6E 12.9N 130.8E	PCN 6		DMSP37		RPMK
* 10	151252	12.5N 130.0E	PCN 5		DMSB36		PGT# PGT#
11	151346	12.2N 131.9E	PCN 6		DMSP35		RODN
12	151527 152136	12.2N 131.0E	PCN 5	TO 5	DMSP35		RODN
14	152137	12.9N 129.1E 13.0N 129.6E	PCN 5	T0.5/0.5 /00.5/24HRS	DMSP37		RPMK
15	152332	13.3N 120.0E	PCN 5	T1.0/1.0 /50.0/24HRS	•		PGTW PGTw
16	140133	13.5N 128.BE	PCN 5		DMCDJO		PGTW
17 18	160227	13.6N 129.7E 13.4N 127.3E	PCN 5		DMSP35		PGT
19	161017	13.9N 127.0E	PCNO		DMSP37		PGT⊌ RPMK
* 20	161214	13.2N 124.3E	PCN 5		AFGPMO		PGTW
22 21	162117 170114	14.1v 125.2E	PCN 6	+2 E +2 E +01 E +3 + H0E	DMSP37 DMSP39		PGTW
23	170114	13.6N 125.4E	PCN 5	T2.5/2.5 /01.5/26HRS T2.6/2.0 /01.5/24HRS			PGTW RPMK
24	170957	13.9N 125.3E	PCN 5		DMSP37		PGTW
25 26	171355	13.9N 125.0E	PCN 5		DMSP39		RPMK
27	172238	13.6N 125.2E 13.8N 124.4E	PCN 5		DMSP39 DMSP37		RODN
28	180038	13.5N 123.8E	PC4 5	13.5/3.5-/D1.0/23HRs			RPMK PGT⊮
29	190237	13.7N 123.5E	PCN 3	T3.5/3.5 /D1.5/24HRs	DMSP39		RPMK
30	190237 191118	13.6N 123.4E 13.9N 122.3E	PCN 3 PCN 4	13.5/3.5	DMSP39 TERRMO	INIT DAS	RODN
32	141118	13.34 122.7E	PON D		DMSP37	•	RPMK RODN
33	141320	13.2M 12702E	PCN 5		DMSP36		PGTM
34 35	1R1336	13.2N 127.3E	PON 5		DMCD34		RPMK
36	182518	13.7N 121.5E	PCY 6		DMCD37		PGT# RPMK
37	182518	13.50 121.4E	PCN 0		DMSP37		PGTW
38 39	190820	13.4N 121.1E	PCN 5	12.5/3.5+/V1.0/24HRS			PGTW
40	190518	13.9N 120.7E 13.2N 120.8E	PON 5	T2.5/3.0 /W1.0/24HRS T2.5/3.5 /W1.0/24HRS			RPMK
* 4 <u>1</u>	191058	13.7N 120.6E	PCN 6	1203/363 /#180/24/11/1	DMSP37	PSBL 240 CATH AT 1534 1206E	RODN
• 42 • 43	141058	13.7v 119.7E	PCN 5		DMSP37		RODN
• 44	191302	13.5N 118.8E 13.2N 118.6E	PCN 5 PCN 5		Ducase Ducase		PGTW
+ 45	191317	13.7N 119.3E	PCN 5		Deseas		RODN RP4K
* 46 * 47	191318	13.5N 119.8E	PCN 5		DMSP34		PGTW
# 47 # 48	192157	14.5N 11R.4E 14.7N 117.8E	PCN 5		DMSP37		PGTW
# 49	192157	13.9N 118.2E	PCN 6		DHSP37		RODN RPMK
50	200144	16.5N 118.8E	PCN 5	T1.0/2.0 /W1.5/84HRS			ROON
51 52	200159 200159	16.8N 118.9E 16.9N 118.8E	PCN 3 PCN 3	12.0/2.0 /W0.5/24HRS	DMSP39 DMSP35		RPMK
53	201038	17.5N 11A.SE	PCN 5	T1.5/2.5 /WI.0/24HRG	DMSP37		PGT#
54	201244	17.5N 117.7E	PCN 5		DMSP36		PGTW
55 56	201439 201440	17.7N 117.5E 17.8N 118.3E	PCN 6 PCN 5		Desora		RPMK
57	202137	18.4N 117.3E	PCN 5		DMSP39		RODN PGTW
58	202319	18.44 117.7E	PCN 5		DMSP37		RODY
59 60	210114	19.9N 117.3E 18.7N 117.7E	PCN 5	11.0/1.0 /S0.0/24HRS	DMSP39 DMSP36		RODN
61	270140	18.94 117.2E	PCN 5	T1.0/2.0 /W1.0/24HRC T1.0/1.5 /S0.0/24HRC	DMSD30		RPMK PGTW
* 62	210321	19.0N 11K.8E	PCN 5		DMSP39		RODN
63	211018	19.4N 117.4E 19.4N 117.1E	PC4 5		DMSP37		PGTW
65	211421	19.4N 116.9E	PCN 5 PCN 5		DM4630		RPMK RODN
* 66	212258	19.4N 116.6E	PCN 5	T2.0/2.0-/D1.0/24HRS	DMSP37		RPMK
67 68	212258 220108	20.4N 116.4E 20.4N 116.6E	PCN 5 PCN 5		DMSP37		RODN
69	220302	20.8N 116.4E	PCN 5	13.0/3.0 /02.0/25HRs	045P34 045P34		RPMK
70	220305	20.8N 11K.1E	PCN 5		PF92MO		RPMK
71	221139	20.34 116.8E	PCN 5		DMSP37	PSN BSD ON EXTRAP OF CLD LINES	RODN
73	271402	20.60 116.9E	PCN 5		DMSP39		RODN
74	525538	21.4N 114.7E	PCN 5	T2.0/2.0 /50.0/24HRS	DMSP37		RPMK
75 76	230050 230050	21.4N 114.5E	Por L	T2.5/3.0 /W0.5/23HRs	Duspas	THE CHA	ROUN
77	540020	21.5N 114.5E 21.5N 114.1E	PCN 5 PCN 3	12.5/2.5-	DMEP34 DMEP39	INI ORS	PGTW
78	230243	21.9N 117.9E	PCN 5		0=9235		RDDN RPMK
79 80	231118	34-F11 NS-55	PC4 6		DMSP37		RPMK
18	271119 271342	22.1N 113.9E 22.1N 113.6E	PCN 6 PCN 5		DMSP37 DMSP39		RODY
82	271343	22.6N 117.3E	PCN 6		DMSP39		RPMK
83	231343	55*IN 113*BE	PCN 5		Dwebsa		PGI₩
84 85	232218 240031	22.5N 112.8E 22.5N 112.9E	PCN 5		Duspa7 Duspak		RKSO
86	240224	22.5N 112.8E	PCN 3	T1.5/2.5 /W1.0/24HRs			RPMK ROD4

# ATRCHAFT FIXES

FIA NO.	T TME (2)	FTX POSTTION	FLT LVL	70043 HGT	285 MSLP		-SFC-		46 X-						EYÊ SHAPE	FYE ORIEN-	EYF TEMP (C)	45N NO.
1	144503	13.7N 12R-0E	700MH	3056	995	50	n50	10	170	68	0 = 0	10	3	5			+16 +15 +11	2
5	170507	13.64 125.6E	700MH	3043	984	90	110	30	160	58	040	4.0	5	5			+13 +11	4
£	170918	11.9N 125.5E	700MH	7054	994	90	360	30	100	52	340	30	5	20			.15 .14 + B	4
4	114641	13.64 122.4E	7nom8	2961		40	360	75	090	65	300	50	2	4			+11 +15 + 9	6
5	191936	13.94 121.4E	700MH	7035					770	45	230	25	3	5			•11 •11	7
ь	182042	13.54 121.7E	7กฤษท	7044					350	27	520	50	- 3	5			+1m +11 +11	7
1	190929	14.74 120.3E	70048	7101		50	310	30	080	28	050	24	3	5			+in +li +li	9
В	200009	16.24 119.18	7 n 0 MB	3109	1005			25					5	2			+11 + 4	10
بَ	200300	17.49 TIR.BE	7ngmm	3087	1000		070		130	31	050	15	2	4			+11 +13 + 8	12
10	201933	17.94 11R.1E	700MB	3061					110	60	360	120	4	5			+12 +10	14
11	202151	18.1N 118.1E	700MB	3067	997	20	090	30	150	24	090	.60		4			+1₽ +15' + 9	14
12	210619	14.14 118.0E	700MB	3093	998	40	350	30	050	50	300	45	10	10				15
13	210904	19.2N 117.5E			999	40	070	60	110	37	070	4.0	20	1			+26 +26 28	15
14	212100	21.0N 114.1E															•	36

#### RAJAR FIXES

	TIME	FIX	D4D40		EYE	EYF Diam	RADDU-CODE ASWAR TODEF	COMMENTS	HADAR POSTTON	SITE
NO.	(7)	P051T10H	HAUAR	ACCRY	SHAPE	OIAM	ASBAN IDON	COMMENTS	F(3) 1   U 4	WHO WO.
1	171859	13.7N 124.3E	ACFT		-					SANAS
ż	172300	13.8N 123.9E	LAND				10210 ////		14.1N 123.0E	98440
ē	172300	14.5N 123.5E	LAND				4//// /////		16.3N 120.6E	98321
4	140900	13.3N 122.9E	LAND				2021/ 52116		14,1H 123.0E	98440
5	191030	13.7N 122.9E	LAND				25/11 /1/11		22.3N 114.2E	45005
6	] n 1 1 0 0	13.4N 122.BE	LAND				1944/ ////		16.3M 120.6E	98321
7	191100	13.7M 122.9E	LAND				25/// /////		16.3N 120.6E	98321
Ħ	141200	13.5N 122.7E	LAND				11561 11111		16.3N 120.6E	98321
	141300	13.64 122.7E	LAND				1042/ ////		16.3N 120.6E	98321
10 11	1#1500 1#1530	17.4N 122.6E					1056/ ////		16.3N 120.6E	98371 98440
12	181600	13.5N 122.3E 13.6N 122.5E	LAND				1173/ 52705		16.3N 120.6E	48371
13	182145	13.9N 121.6E	LAND	FAIR	CERCULAR	15	11177 32.03		15.2N 120.6E	98327
14	182230	13.9N 121.5E	LAND	FAIR	CIRCULAR	15			15.2M 120.6E	98327
15	192255	13.9N 121.4E	LAND	FAIR	CIRCULAR	15			15.2N 120.6E	98327
16	191205	15.1N 120.5E	LAND	POOR	CIRCILAR	5			15.2N 120.6E	98327
17	191300	15.2N 12n.4E	LAND	POUR	CIRCULAR	5			15.2M 120.6E	98327
16	101300	14.7N 120.2E	LAND				41/11 11/11		16.3M 120.6E	98371
19	191335	15.3N 120.4E	LAND	POOR		5			15.2N 120.6E	98327
20	101400	15.0N 120.0E	LAND				4//// /////		16.3M 120.6E	98371
21	105500	16.0N 119.4E	LAND				104// 104//		16.3M 120.6E	98321
22	200000	14.34 119.0E	LAND				105// ////		16.3N. 120.6E	98371
23	200040	14.9N 11R.5E	LAND				1266/ 52912		16.3M 120.6E	98371
24 25	2n0100	16.6N 118.8E	LAND				1051/-53218 106//-5///		16.3% 120.6E	98371 98371
26	200130	17.5N 118.5E	LAND				1042/ 42916		16.3M 120.6E	98321
27	200300	16.2N 118.9E	LAND				1051/ 630//		16.3N 120.6E	98321
28	200500	17.04 114.6E	LAND				1089/ 6////		16.3N 120.6E	98371
29	200700	17.2N 119.5E	LAND				10932 5////		16.3N 120.6E	98321
30	200800	17.3N 118.7E	LAND				1068/ 5////	:	16.3N 120.6E	98321
31	200900	17.3N 119.7E	LAND				1061/ 5////		16.3N 120.6E	98321
32	2n1200	17.64 118.4E	LAND				4561/ 6////		16.3N 120.6E	98371
33	550500	20.6N 115.HE	LAND				6///2 /////		22.3N 114.2E	45004
34	520500	20.5N 115.9E	LAND				6///2 /////		25.3H 114.5E	45004
35	220500	20.5N 116.0E	LAND				65/// /////		25.3N 114.5E	45004
36	2>0900	20.9N 115.9E	LAND				60/// /////		22.3N 114.2E	45004
37 38	521500	20.9N 115.5E	LAND				60/// //// 50913 5//00		22.3N 114.2E	45004
39	221400	20.9N 115.5E 20.9N 115.5E	LAND LAND				40913 54400		22.3N 114.2E	45004 45004
40	222100	21.2N 114.7E	LAND				40523 53106		22.3N 114.2E	45004
41	252300	21.4N 114.6E	LAND				40523 53007		22.3N 114.2E	45084
42	230000	21.4N 114.5E	LAND				40523 53001		22.3N 114.2E	45004
43	230200	21.4N 114.3E	LAND				50562 32906		22.3M 114.2E	45004
44	230300	21.6N 114.1E	LAND				5///2 52906		22.3N 114-2E	45004
45	230600	21.7N 113.8E	LAND				5///2 52906		22.3N 114.2E	45004
46	230900	21.7N 113.7E	LAND				5///2 52903		22.3N 114.2E	45004
4.7	531500	51.9M 113.9E	LAND				6/1/2 /////		22.3N 114.2E	45004
48	231500	22.2N 113.8E	LAND				11111 11111		22.3N 114.2E	45004
49	271900	22.3N 113.3E	LAND				6//// ///// 50912 ////		22.3N 114.2E	450n4 450n4
50 51	232000 232100	22.3N 113.0E					5/// ////		22.3N 114.2E	45004
52	232200	22.3N 117.0E	LAND LAND				6/// ////		22.3N 114.2E	45004
53	540000	22.3N 117.0E					5//// /////		22.3N 114.2E	45004
54	240100	22.3N 112.6E					5//// /////		22.3N 114.2E	45004
55	240300	22.3N 112.6E					6/11/ ////		22.3N 114.2E	
	•									-

### TROPICAL STORM NANCY

# SATELLITE FIXES

FIX NO.	T1ME	FIX POSITION	<b>∆</b> C(RY	DADSAK CODE	SATFLE TTE	COMMENTS	SITE
1 2 3 4 5 6 7 8	1 8221 8 1 9221 8 1 9021 8 1 9021 8 1 9105 8 1 9145 9	19.3M 111.9E 19.1N 111.5E 18.4N 111.2E 18.6N 112.0E 18.6N 112.0E 18.5N 112.0E	PCN 6 PCN 6 PCN 5 PCN 4 PCN 3 PCN 3	T1.0/1.0 T3.0/3.0	DMCP37 DMCP37 DMCP34 DMCP39 DMSP37 DMSP37	INIT JOS SOUTH JOS EYE BANTONG PRESIBLE	PGTW RPMK RPMK ROON RPMK RODN
10 11 12 13 14 15 16	191459 192338 192339 200144 200340 201219 201219 201439 201440 202319	19.6% 110.5E 19.6% 100.5E 19.0% 110.0E 19.0% 100.4E 19.4% 100.8E 18.7% 100.2E 19.9% 108.6E 18.4% 108.7E 19.6% 108.4E	PON 4 PON 4 PON 4 PON 4 PON 4 PON 4 PON 4 PON 3	T3.0/3.0 /D2.0/21HRC T3.0/3.0 /S0.0/24HRC	DMSPRA DMSPRA TPREMA DMSPRA DMSPRA DMSPRA DMSPRA		KPMK KGMC RPMK RODN RPMK RPMK KGMC RPMK RODN
18 19 20 21 22 23 24 25	202319 210108 210126 210321 210321 211159 211421 211421	17.54 108.3E 14.2N 108.6E 17.6N 107.0E 18.2N 108.2E 17.7N 107.9E 18.1N 108.1E 18.1N 108.1E 17.9N 107.4E 17.9N 107.9E	PCN 5 PCN 5 PCN 5 PCN 3 PCN 4 PCN 4 PCN 3	T2-5/3-0 /W0-5/24HRQ T4-0/4-0-/D1-0/25HRQ	DMSP37 DMSP37 DMSP36 DMSP36 DMSP36 DMSP30 DMSP37 DMSP37 DMSP34 DMSP30		RODN RPMK RPMK RPMK RODN RPMK RPMK RODN
26 27 28 29 30 31 32 33	212258 212258 220302 220302 22139 221139 221402 221402	17.3N 107.3E 17.6N 107.9E 17.3N 107.2E 17.5N 107.2E 17.5N 106.9E 16.4N 106.6E 16.4N 106.5E 16.4N 106.1E	PON 5 PON 5 PON 3 PON 3 PON 6 PON 5 PON 5	T1.5/2.5 /W1.0/24HRC T+.0/4.0-/50.0/24HRC	DMSP37 DMSP37 DMSP39 DMSP39 DMSP37 DMSP37 DMSP37 DMSP39		RPMK RODN RPMK RODN RPMK RODN RPMK RDDN RPMK

# SYMPOTIC FIXES

FIX NO.	TTME: (7)	PIY POSITION	INTENSITY ESTIMATE	NEAREST Data (NM)	COMMENTS
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	171200 140000 141200 141200 200000 200000 211200 211200 211200 212000 2200000 2200000 221200 2200000 2200000 240000	16.0% 117.0E 17.5% 111.5E 14.0% 111.5E 14.0% 111.2E 14.3% 110.5E 14.1% 100.5E 17.2% 100.5E 17.2% 100.5E 17.3% 100.0E 17.0% 107.0E 16.3% 106.0E 16.3% 106.0E 15.0% 104.0E	15 15 20 25 20 20 20 5 5 25 16 17	120 90 60 120 20 70 20 70 21 120 120 120	

# TYPHOON OWEN

FIX NO.	T1ME (7)	FIX POSTTION	<b>ACCRY</b>	DAUSAK CODE	Salfertile	COMMENTS	SITE
• 1	210140	12.74 130.4E	PCN 5	T1+0/1+0	0MSP39	INII DOS	PGTW
• 3	21117	11.9N 130.4E	PCN 5		045P34 045P47		PGTW PGTW
. 4	212326	11.34 136.6E	PCN 5	TZ.0/2.0 /01.0/23HRS			PGT#
* 5	220120	11.0* 136.7E	PCN 5	7.2011.2111	UMCDJU		PGTW
. 6	220357	11.5N 137.2E	PCN 5		DMSP17		PG[W
* 7	221209	11.5M 136.4E	PCN 5		AF GP#G		PGTW
* A	221220	11.6H 136.5E	PCN 5		DMCB3A		PGT# RODN
* 10	2>1220 2>2057	11.5M 136.2E	PCN 5		DMSP37		PGTW
* 11	22230B	17.0M 136.7E	PCN 5		DMSP36		PGTW
12	230102	11.8M 135.4E	PCN 5	TU.0/0.0	DMSP39	Sec 11ni	RPMK
13	230105	12.4N 134.5E	PCN 5	T2.0/2.0 /50.0/26HRS	PERSON		PGT#
14	230937	12.4N 135.6E	PCN P		0 M S D 3 7 D M S D 3 4		PGTW PGTW
15	525036 531501	13.7N 136.2E	PON 5		DMSP37		PGTW
17	240031	16.60 134.7E	PON 5	12.0/2.0 /DZ.0/23HRS			RPMK
16	240035	14.74 135.0E	PCN 5	7=	DMSP36		PGT#
19	240042	16.9V 135.0E	PCN 3	T3.0/3.0 /D1.0/24HRS			PGTW
20	240043	16.9M 134.7E	Pry 3	T3.0/3.0	DMSP39	INII 292	RODN
25 51	240917 240917	14.2N 137.7E 14.7N 133.3E	PCN 5		045P37 045P37		PGTW RODN
23	241313	19.4N 137.2E	PCN 3		DMSD3A		RPMK
24	241314	19.3H 132.7E	PCN 5		DMCD3A		PGTW
25	241324	19.24 132.7E	PON 5		DWCD34		PGTW
56	241324	19.1N 133.1E	PCN 5		045030 045037		RODN RPMK
27 28	242157 242158	20.34 131.2E	PON 3 PON 3	14.0/4.0 /DZ.0/22HRC	DM45237		PGTu
29	242158	20.7M 130.9E	PCN 3		DMSP37		RODN
30	250014	21.0N 130.HE	PCN 3	T4+5/4.5 /01+5/24HR4			PGTW
31	250205	21.34 130.0E	Prn 3		Daeban		PGTW
32	250205	21.24 130.58	PCN 1	14.5/4.5 /D1.5/25HR			RODN
33	251038 251039	21.9x 129.7E 21.3x 129.7E	PCN 1 PCN 1		045P37 045P37		PGTW RODN
35	251256	27.0N 129.8E	PCN 1		DHSHIA		PGTW
36	251304	24.3× 129.9E	PCN 2		PFRPMO		RPMK
37	251305	22.0N 129.7E	PCN 1		DMSP34		RODN
38	252137	23.1m 150.2E	PCN 1		0MSP37		PGTW
39	252137 250146	22.9N 120.2E	PCV 1	15.5/5.5 /D1.5/24HR	DMSP37		RPMK RPMK
4 U	260146	23.3N 129.9E	PCN 1	16.0/6.0 /0).5/24HR			RODY
42	240146	23.3N 120.0E	PCN 1	T6.0/6.0 /01.5/25HR			PGTW
43	251018	23.9N 120.2E	PON I		Duspar		PGTW
44	241018	23.8N 129.2E	PCN 1		DMSP37		RODN
45	261238 261238	24.0M 129.3E	PCN I		DMSP3A DMSP37		PGT# RDDN
46 47	241246	23.8N 129.1E	PCN I		DMCB3A		RPMK
48	241546	27. 3N 129.3E	PCN 3		DECONO	EYE NOT VSBL	PGT⊯
49	261246	24.0M 120.2E	PCN 3		Discosa		RKSO
50	262117	24.54 129.58	PCN 1		DMSP37		PGTW
51 52	242117 242338	24.3N 129.5E	Prv 1 Prv 1	15.0/4.0 /W].0/22HR4	1FAPHQ AFAPHQ		RODN PGT#
53	245338	24.74 129.5E	PCN 1	T5.0/6.0 /W1.0/22HR			RODN
54	270127	24. RAI 129.5E	PCN 1	16.0/6.0 /00.5/29HR			RPMK
55	270127	25.0% 129.5E	PCN 1		DMen.se		PGTW
56	270127	24.9AI 120.3E	PCN L		Duchas Duchas		RODN RODN
57 58	270958 270958	25.7N 129.6E	Pri I		045631 124540		PGT#
59	271220	26.1H 120.HE	PCN 1		DUSPA		PGTW
60	271226	24.0N 129.9E	PCN I		DMSD34		RPMK
61	271227	34.1N 130.6E	Pcv 1		046034		PGTW
62	271227	25.9N 129.5E	PCN 1 PCN 1		Dwsp34 Dwsp37		RODN PGTW
63 64	272057 272057	26.54 ]30.0E	PON 1		DMSP37		RODN
65	272320	27.HM 129.8E	PCN 1	14.0/5.0 /W1.0/24HR			PGTW
bb	290108	27.24 120.8E	PCN 1		Ondban		PGTW
67	240108	27.1N 129.5E	PCA I	14.5/5.0 /WO.5/26HR	DMCD30		RODN
68	240937 241119	27.7% 120.7E	PCN L		045037 045037		PGTW RODN
6 <del>7</del> 70	241119	27.44 120.BE	PCN L PCN L		AF42MO		PGTW
71	2R1207	27.5N 120.6E	PCN J		PrupuO		RKSO
72	241501	27.5M 120.3E	PCN I		046644		PGTW
73		27.8N 120.6E	PCN 2		0wsp37		PGTW
74 75	294025	30.7N 131.ME	Pry 3 Pry 1	14.0/4.5 /W0.5/22HR4			RK50 RODN
76		24.0% 120.9E 28.2% 120.7E	PCV 1	T4.5/4.5 /S0.0/24HR	PERSON	INII JOS	RKSO
77	291058	2H.RN 130.2E	PCN 1	1.4.77443	UMSP37		RPMK
78	501355	29.24 130.4E	PCN I		DMSP34		PGTW
79	591355	28.24 130.0E	PCN I		045074		ROON
80	201330	20.24 1 to 5E	Prv l	74 044 0	Duchia	INTI Das	RKSO PGTW
85 81	292158 292153	37.4N 131.3E	PCN 3	14.0/4.0	Dusp37 Dusp37	INII Ja2	RODN
83	300511	31.54 112.08	Pry J	14.5/4.5	DMCD34	INII 335	RPMK
84	300211	31.44 172.2E	PCV		DACB30	-	PGT₩
ಕಶ	301159	34.0N 135.5E	PCV 6		PERPMO		PGTW
86	3n1311	34.54 136.2E	PON 5		Drichia		RPMK RODN
87	301311	34.54 [3K.HE	PC1 5		044044		ROUN

#### ALDCHAFT FIXES

FIX NO.	TIME (7)	FTX POSTTION	FLT I VL	700uq HGT	985 MSLP	MAX-SFC-WVD VEL/ARG/RVG		T-LVL-ANI EL/3HG/4NI			EYE OR			
1	220315	12.5% 138.5E	1500F1		999	15 250 55		16 100 6					+24 +25 +22	9 1
- 2 - + 3	221904	12.3M 137.HE	1500F1 7009B	3077	1002	15 290 30		28 310 3°					+24 +25 +25	27 2
4	222213	12.2N 137.0E	1500FT	4077	1002	15 n60 30		18 040 Se					+25 +25 +23	3
5	230530	13.3M 134.7E	1500FT		999	70 150 25	160 6	60 140 14	5 15				+25 +23	•
7	230 <del>3</del> 01 231 <del>3</del> 23	13.3N 136.4E 14.9N 135.HE	7004B 7004B	3091 3015	1005	15 0		33 210   79 45 120 151					+ 9 + 8 +11 +10	<b>4</b> 5
8	535516	16.2N 135.4E	70048	7747	990	40 090 8	170 4	6 110 91	5 2	CIRCULAR	20		+12 +13 +10	5
10 3	240609 240858	17.5N 134.2E	7 กอพษ 7 ก อ พ ษ	1001 2052		65 100 45 45 090 30		50 060 100 65 <b>05</b> 0 51		CIRCULAR			*13 +10 +11 +15 +10	6
11	541310	18.5N 133.8E 20.5N 131.8E	7n0MB	2827		<b>\$5</b> 1170 30		70 LUU 31		CINCHEAN	a		+18 + 4	7
12	242155	20.6N 131.2E	700MH	2833	967	30 040 5		63 040 91					+1H +19 + 6	7
13 14	240733 240904	21.5N 129.8E	700MH 700MH	2701 2655	949	90 360 8 90 110 8		?5 080 1: 79 340  4			15		+18 +15 +14	8 8
15	252131	25.4M 150.4E	700MB	2375	918	<b>90</b> 050 3	11	10 12 4		CIRCHLAR	10		+13 +20 +13	9
16 17	540555 540033	23.2N 120.0E	700MB 700MB	2403 2414	922	100 250 3 30 330 3		95 250		CIRCULAR	8		+15 +18 +15	9
16	240330	23.5N 120.2E	700MB	2382	919	90 250 15		95 250	5 8	CIRCULAR	12		+15 +17 + 7	10
50 19	242140	24.5N 129.4E	700MB 700MB	2594 2632	942	90 170 18 90 270 72		84 230 ]° 60 270 30		CUNCENTRIC CIRCILAR	25 12	180	+19 +16 +16	11
21	270240 279848	24.9N 120.6E 25.4N 120.7E	7,0 MB	2599		70 190 35		70 190 3		CIRCULAR	50		+14 +17 +14 +17	11
22	240112	27. IN 149.6E	70048	269R	953	90 S30 30		61 230 90		ELLIPTICAL		030	+16 +15 +15	13
23 24	280315 280414	27.9N 129.7E	700MH 700MH	2697 2694		50 090 120 50 040 50		65 270 31 78 040 51		ELLIPTICAL	35 15	250	+16 +16 +16 +16++16	13 13
25	2RU835	27.4N 120.8E	7n0#8	2701	954	70 090 30	140 8	81 090 60	5 3	ELLIPTICAL		120	+15 +17 +13	14
26 27	282147 290048	27.94 129.8E 28.04 129.7E	7,0MH 7,0MH	2683 2683	952	65 040 70 70 250 30		75 020 61 70 260 6		CIRCILAR	5		+16 +17	15 15
28	200218	24.0N 129.7E	70048	2685		45 050 120	190 1	75 090 l	. 2 1	CIRCULAR	ıs		+14 +15	15
29 30	290642	3H. PAI 129.HE	700MB			40 090 120 55 270 40		64 110 7: 64 270 2:			15.10	210	+17 +15	16
31	290548 292142	24.4N 130.3E 30.4N 131.1E	700MB 700MB	2686 2702	957 956	55 270 40		64 270 2: 74 848 6:			9	210	+14 +18 +15 +15 +15	16 17
32	310006	30.9N 131.4E	700MB	2707		90 160 19	230 10	00 160 1	5 5 5	CIRCHLAR			+15: +12:	17
33 34	300500 300500	31.2N 131.HE 32.9N 133.4E	700MH 700MH	2702 2694	954 957	100 250 20 90 310 9		78 0/0 4: 60 360 1:			10		+37 +18 +10 +16 +17 + 6	17 18
													-	-
						RADI	P FIXES							
	TIME	Ftx			EYE		PARION-(						RADAR	SITE
NO.	T1ME (7)	FTX Posttion	RAGAR	ACCRY	EYE		PARIOS-C			COMMENTS			HADAR Postiton	SITE:
NO.	(7)	POSTTION		ACCRY			ASHAR T	TODFF		COMMENTS			POSITION	HM0 NO.
		POSTTION 22.90 129.3E	CNAJ	ACCRY			ASHAR 1	1DDFF 43316		COMMENTS			P051T104	HMO NO.
NO.	252100 252200 252300 252300	22.9N 129.3E 23.1N 129.3E 23.2N 129.2E	LAND LAND LAND				ASHAR T	TDDFF 43316 53411		COMMENTS			POSTTONI  26.2N 127.8EI  26.2N 127.8EI  26.2N 127.8EI	47937 47937 47937
NO.	252100 252200 252300 252300 252300	POSTTION  22.9N 129.3E 23.1N 129.3E 23.2N 120.2E 23.3N 129.2E	LAND LAND LAND LAND	PODR			35//6 4 34//2 9 34//2 9	TDDFF 43316 53411 53411		COMMENTS			POSTTONI  26.2N 127.8EI 26.2N 127.8EI 26.2N 127.8EI 26.3N 126.8EI	47937 47937 47937 47937 47929
NO.	252100 252200 252200 252300 252300 260000 260100	22.9N 120.3E 23.1N 120.3E 23.1N 120.2E 23.3N 120.2E 23.3N 120.2E 23.2N 120.2E 23.1N 120.1E	LAND LAND LAND LAND LAND LAND	PODE		PE DIAM	35//6 4 34//2 5	TDDFF 43316 53411 53411 53308		COMMENTS			POSTTONI  26.2N 127.8EI 26.2N 127.8EI 26.2N 127.8EI 26.2N 127.8EI 26.2N 127.8EI 26.2N 127.8EI	47937 47937 47937 47937 47937 47937
NO. 1 2 3 4 5	252100 252200 252200 252300 252300 260000 260100	22.9N 129.3E 23.1N 129.3E 23.1N 129.2E 23.3N 129.2E 23.2N 129.2E 23.1N 129.1E 23.2N 129.1E	LAND LAND LAND LAND LAND LAND LAND				35//6 / 34//2 9 34//2 9 55//3 9	TDDFF 43316 53411 53411 53308 52005		COMMENTS			POSITIONI  26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.3M 126.8E: 26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E:	47937 47937 47937 47937 47937 47937 47937
NO.	252100 252200 252200 252300 252300 260000 260100	22.9N 120.3E 23.1N 120.3E 23.1N 120.2E 23.3N 120.2E 23.3N 120.2E 23.2N 120.2E 23.1N 120.1E	LAND LAND LAND LAND LAND LAND	PODE		PE DIAM	35//6 6 34//2 9 34//2 9	7DDFF 43316 53411 53411 53308 52005 53416	rE MOVA				POSTTONI  26.2N 127.8EI 26.2N 127.8EI 26.2N 127.8EI 26.2N 127.8EI 26.2N 127.8EI 26.2N 127.8EI	47937 47937 47937 47937 47937 47937
NO. 12 3 45 6 7 8 9	252100 252200 252200 252300 252300 260300 260100 260100 260100 260200 260300 260300	POSTTION  22.9N 129.3E 23.1N 129.3E 23.2N 129.2E 23.3N 129.2E 23.1N 129.2E 23.3N 129.0E 23.3N 129.0E 23.3N 129.0E 23.3N 129.0E	1AND LAND LAND LAND LAND LAND LAND LAND L	Pn0H 6n0D Pn0R		PE DIAM	35//6 / 34//2 9 34//2 9 55//3 9	YDDFF 43316 53411 53411 53308 52005	YE MNVA				POSTTONI  26.2M 127.8E: 26.1M 127.8E: 26.1M 127.8E: 26.1M 127.8E:	47937 47937 47937 47937 47937 47937 47937 47937 47937
NO. 1 2 3 4 5 6 7 8	252100 252200 252300 252300 260300 260100 260100 260200 260200	POSTTION  22.9N 129.3E 23.1N 129.3E 23.3N 129.2E 23.3N 129.2E 23.1N 129.2E 23.1N 129.1E 23.2N 129.0E 23.3N 129.0E 23.3N 129.0E 23.3N 129.0E 23.3N 129.0E 23.3N 129.0E	1 AND LAND LAND LAND LAND LAND LAND LAND L	PODA GOOD		PE DIAM	35//6 4 34//2 9 34//2 9 55//3 9 65//3 9	7DDFF 43316 53411 53308 52005 53416 501//	rE MNVG	3225			POSTTONI  26.2N 127.8E: 26.2N 127.8E: 26.3N 127.8E: 26.3N 127.8E: 26.2N 127.8E: 26.3N 126.8E: 26.3N 127.8E: 26.3N 127.8E: 26.3N 127.8E: 26.1N 127.8E: 26.1N 127.8E: 26.1N 127.8E: 26.1N 127.8E: 26.1N 127.8E:	47937 47937 47937 47937 47939 47937 47937 47937 47937 47937 47937 47929
NO. 1 2 3 4 5 6 7 8 9 10 11 12 13	252100 252200 252200 252300 252300 260100 260100 260100 260200 260300 260300 260300 260300 260300 260300	POSTTION  22.9N 129.3E 23.1N 129.3E 23.2N 129.2E 23.3N 129.2E 23.1N 129.1E 23.2N 129.0E 23.3N 129.0E	LAND LAND LAND LAND LAND LAND LAND LAND	POOR GOOD POOR GOOD POUR		PE DIAM	35//6 4 34//2 9 34//2 9 55//3 9 65//3 9	7DDFF 43316 53411 533411 532005 53416 501//	E MOVA	3225 3610			POSTTONI  26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.3M 125.8E: 26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.2M 127.7E: 26.3M 125.8E: 26.1M 127.7E: 26.3M 125.8E: 26.3M 125.8E: 26.3M 127.8E: 26.3M 127.8E:	47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937
NO.  1 2 3 4 5 6 7 8 9 10 11 12	252100 252200 252200 252300 260300 260100 260100 260100 260300 260300 260300 260300 260300 260300	POSTTION  22.9N 129.3E 23.1N 129.3E 23.3N 129.2E 23.3N 129.2E 23.2N 129.0E 23.3N 129.0E 23.3N 129.0E 23.3N 129.0E 23.3N 129.0E 23.3N 129.0E 23.5N 129.0E	LAND LAND LAND LAND LAND LAND LAND LAND	PADR 6ADD PADR GADD PADR GADD		PE DIAM	35//6 4 34//2 9 34//2 9 55//3 9 65//3 9	7DDFF 43316 53411 533411 532005 53416 501//		3225 3610			POSTTONI  26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.3M 126.8E: 26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.1M 127.8E: 26.1M 127.7E: 26.2M 127.8E: 26.1M 127.8E:	#MO NO.  47937 47937 47937 47937 47937 47937 47947 47947 47947 47947 47947 47947 47947
NO. 1 2 3 4 5 6 7 7 8 9 10 11 2 13 14 15 16	(7) 252100 252200 252300 252300 252300 252300 260100 260100 260100 260300 260300 260500 260500 260500	POSTTION  22-9N 129.3E 23.1N 129.3E 23.3N 129.2E 23.3N 129.2E 23.1N 129.1E 23.3N 129.0E 24.5N 129.0E 24.5N 129.0E 24.5N 129.0E 23.4N 129.0E	1 AND LAND LAND LAND LAND LAND LAND LAND	POOR GOOD POOR GOOD POUR		PE DIAM	35//6 4 34//2 9 34//2 9 54//3 9 65//3 9 65//2 9 35//1 1	7DDFF 43316 53411 53411 53308 52005 53416 501//  70204 E 70204	E MOVA	3225 3610			POSTTONI  26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.3M 126.8E: 26.2M 127.8E: 26.3M 126.8E: 26.3M 126.8E: 26.3M 127.8E: 26.1M 127.8E: 26.1M 127.8E: 26.1M 127.8E: 26.1M 127.8E: 26.1M 127.7E:	#MO NO.  47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937
NO. 1 2 3 4 5 5 6 7 8 9 10 11 12 12 12 12 15 16 17.	252100 252200 252200 252300 260300 260100 260100 260200 260300 260300 260500 260500 260500 260500 260500 260500 260500 260500	POSTTION  22.9N 129.3E 23.1N 129.3E 23.2N 129.2E 23.3N 129.2E 23.3N 129.0E 23.3N 129.0E 23.3N 129.0E 23.3N 129.0E 23.5N 129.1E 23.6N 129.1E	LAND LAND LAND LAND LAND LAND LAND LAND	PADR GAOD PAOR GAOD PAUR GAOD		PE DIAM 30 30 30 30	35//6 4 34//2 9 34//2 9 34//2 9 55//3 9 65//3 9 65//2 9	7DDFF 43316 53411 53411 53308 52005 53416 501//  70204 E 70204	E MOVA	3225 3610			POSTTONI  26.2M 127.8E: 26.1M 127.7E: 26.2M 127.8E: 26.1M 127.7E: 26.1M 127.7E: 26.1M 127.7E: 26.1M 127.8E:	#MO NO.  47937 47937 47937 47937 47937 47937 47947 47947 47947 47947 47947
NO. 1 2 3 4 5 6 7 7 8 9 10 11 2 13 14 15 16	(7) 252100 252200 252300 252300 252300 252300 260100 260100 260100 260300 260300 260500 260500 260500	POSTTION  22-9N 129.3E 23.1N 129.3E 23.3N 129.2E 23.3N 129.2E 23.1N 129.1E 23.3N 129.0E 24.5N 129.0E 24.5N 129.0E 24.5N 129.0E 23.4N 129.0E	1 AND LAND LAND LAND LAND LAND LAND LAND	PADR 6ADD PADR GADD PADR GADD		PE DIAM	35//6 4 34//2 9 34//2 9 54//3 9 65//3 9 65//2 9 35//1 1	7DDFF 43316 53411 53411 53308 52005 53416 501//  70204 E 70204	E MOVA	3225 3610			POSTTONI  26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.3M 126.8E: 26.2M 127.8E: 26.3M 126.8E: 26.3M 126.8E: 26.3M 127.8E: 26.1M 127.8E: 26.1M 127.8E: 26.1M 127.8E: 26.1M 127.8E: 26.1M 127.7E:	##O NO.  #7937 #7937 #7937 #7937 #7937 #7937 #7937 #7937 #7937 #7937 #7937 #7937 #7937 #7937 #7937
NO. 123345 6678 910112 11415 11516 11718 11920	252100 252200 252200 252300 252300 252300 260000 260100 260200 260300 260500 260500 260500 260500 260500 260700 26	POSTTION  22.9N 129.3E 23.1N 129.3E 23.3N 129.2E 23.3N 129.2E 23.1N 129.2E 23.1N 129.1E 23.1N 129.1E 23.1N 129.1E 23.1N 129.1E 23.1N 129.1E 23.3N 129.0E 23.3N 129.0E 23.3N 129.0E 23.5N 129.1E 23.5N 129.3E 23.6N 129.3E	LANDD	PADR GAOD PAOR GAOD PAOR GAOD GAOD GAOD		PE DIAM	35//6 4 34//2 9 34//2 9 54//3 9 65//3 9 65//2 9 35//1 1	7DDFF 43316 53411 53411 53308 52005 53416 501// 70204 E 70204 70204 70304	VE MOVA YE MOVA	3225 3610 3210			POSTTONI  26.2M 127.8E: 26.1M 127.7E: 26.2M 127.8E: 26.1M 127.7E: 26.2M 127.8E:	#MO NO.  47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937
NO.  1 2 3 4 5 6 7 8 9 10 112 13 14 15 14 15 14 19 22 1	252100 252200 252200 252300 252300 260000 260100 260100 260300 260300 260300 2605000 2605000 2605000 2605000 2605000 260500 260500 260500 2605	POSTTION  22.9N 129.3E 23.1N 129.3E 23.3N 129.2E 23.3N 129.2E 23.3N 129.0E 23.5N 129.1E 23.6N 129.2E	LANDO LANDO	PADR GADD PADR GAOD PAUR GAOD GAOD GAOD GAOD		PE DIAM  30 30 30 30 30 30 30	35//6 4 34//2 9 34//2 9 55//3 9 65//3 9 65//2 9 35//1 9 35//1 9	######################################	VE MOVA	3225 3610 3210			POSTTONI  26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.3M 126.8E: 26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.1M 127.7E: 26.2M 127.7E: 26.1M 127.8E: 26.1M 127.7E: 26.1M 127.7E: 26.1M 127.8E:	##O NO.  47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937
NO. 1233 4567 8910 111 113 145 145 145 145 145 129 220 221 223	252100 252200 252200 252300 252300 260000 260100 260100 260100 260300 260500 26	22-9N 129-3E 23-1N 129-3E 23-1N 129-2E 23-3N 129-2E 23-3N 129-2E 23-3N 129-0E 23-5N 129-0E	LAND LAND LAND LAND LAND LAND LAND LAND	PADR GAOD PAOR GAOD PAOR GAOD GAOD GAOD		PE DIAM	35//6 434//2 934//2 934//2 954//3 965//3 965//3 965//3 956//3 976//1 976	7DDFF  43316 53411 53411 53308 52005 53416 501//  70204 E 70204 70603 E 53306	VE MOVA YE MOVA	3225 3610 3210			POSTTONI  26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.3M 127.8E: 26.3M 127.8E: 26.3M 127.8E: 26.3M 127.8E: 26.3M 127.8E: 26.3M 127.8E: 26.1M 127.7E:	##O NO.  #7937
NO. 12345 5078 9011122 11415 11516 11718 12922	252100 252200 252200 262300 262300 260000 260100 260100 260300 2605000 2605000 2605000 2605000 2605000 260500 260500 260500 2605	POSTTION  22.9N 129.3E 23.1N 129.3E 23.3N 129.2E 23.3N 129.0E 23.5N 129.0E 23.5N 129.0E 23.5N 129.2E 23.5N 129.2E 23.6N 129.2E 23.6N 129.2E 23.6N 129.2E 23.7N 129.2E	LAND LAND LAND LAND LAND LAND LAND LAND	PADR GAOD PAOR GAOD GAOD GAOD GAOD GAOD		PE DIAM	35//6 34//2 9 34//2 9 54//3 9 65//3 9 65//2 9 35//1 9 35//1 9 70411 9 70411	70DFF  43316 53411 53411 53308 52005 53416 501//  70204 E 70204 F 70204 E 70206 53306 70506	VE MOVA VE MOVA	3225 3610 3210			POSTTONI  26.2M 127.8E: 26.1M 127.7E: 26.2M 127.8E: 26.1M 127.7E: 26.2M 127.8E: 26.2M 127.8E:	##O NO.  47947
NO.  1234 556789 10112314 11514 11514 12222324 225	252100 252200 252200 252300 252300 260000 260100 260100 260200 260300 260500 26	POSTTION  22.9N 129.3E 23.1N 129.3E 23.3N 129.2E 23.3N 129.2E 23.2N 129.0E 23.3N 129.1E 23.4N 129.1E 23.4N 129.1E 23.4N 129.1E 23.4N 129.1E 23.4N 129.1E 23.4N 129.3E 23.7N 129.3E	LAND D LAND	PADR GADD PADR GAOD PAUR GAOD GAOD GAOD GAOD		PE DIAM	35//6 4 34//2 9 34//2 9 55//3 9 65//3 9 65//2 9 35//1 9 35//1 9 20//1 9 55//1 9	7DDFF  43316 53411 53411 53308 52005 53416 501//  70204 E 70204 70304 70603 E 53306 70504 E E	VE MOVA	3225 3610 3210			POSTTONI  26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.3M 126.8E: 26.3M 126.8E: 26.3M 127.8E: 26.3M 127.8E: 26.3M 127.8E: 26.1M 127.8E: 26.1M 127.7E: 26.1M 127.8E: 26.1M 127.7E:	##O NO.  #7947
123455077899111123114511501171181190211233224527	252100 252200 252200 252300 262300 260000 260100 260100 260300 260500 260500 260500 260500 260500 260500 260500 260700 260700 260700 260700 260700 260700 260700 260700 261000 261000 2611000 2611000 2611000 2611000 261200	22.9N 129.3E 23.1N 129.3E 23.3N 129.2E 23.3N 129.2E 23.3N 129.2E 23.1N 129.2E 23.1N 129.1E 23.1N 129.0E 23.1N 129.0E 23.3N 129.0E 23.3N 129.0E 23.3N 129.0E 23.5N 129.2E 23.7N 129.3E 23.6N 129.2E 23.7N 129.2E 23.7N 129.2E 23.7N 129.2E 23.9N 129.2E	LAND D LAND	PADR GAOD PAOR GAOD GAOD GAOD GAOD PAOR PAOR PAOR		PE DIAM	35//6 434//2 934//2 934//2 954//3 965//3 965//3 965//3 956//3 976//1 976	#3316 #3316 #53411 #53411 #53308 #52005 #52005 #53416 #70204 #70204 #70204 #70204 #704003 #70603 #70603 #706004 #706004	VE MOVG VE MOVG VE MOVG VE MOVG VE STUP VE STUP	3225 3610 3210 0205 0205			POSTTTONI  26.2M 127.8E1 26.2M 127.8E1 26.2M 127.8E1 26.2M 127.8E1 26.2M 127.8E1 26.2M 127.8E1 26.2M 127.8E2 26.1M 127.7E1 26.2M 127.8E1 26.1M 127.7E1 26.1M 127.7E2 26.2M 127.8E2 26.1M 127.7E2 26.2M 127.8E2 26.1M 127.8E2	##O NO.  #7997
NO. 1233 456789 1011233145167189 120224 2267829	252100 252200 252200 252300 252300 260000 260100 260100 260200 260200 260300 2605000 2605000 2605000 2605000 2605000 2605000 260500000 2605000	22.9N 129.3E 23.1N 129.3E 23.3N 129.2E 23.3N 129.2E 23.1N 129.2E 23.3N 129.2E 23.1N 129.0E 23.1N 129.0E 23.1N 129.0E 23.5N 129.2E 23.7N 129.2E 23.7N 129.2E 23.7N 129.2E 23.7N 129.2E 23.9N 129.2E 23.9N 129.2E 23.9N 129.2E 24.0N 129.2E 24.0N 129.2E	LANDD	PADR GAOD PAOR GAOD GAOD GAOD GAOD GAOD GAOD PAOR		PE DIAM	35//6 4 34//2 9 34//2 9 54//3 9 65//3 9 65//3 9 65//2 9 35//1 9 75//1	70DFF  43316 53411 53411 53308 52005 53416 501//  70204 E  70204 E  70204 E  70206 E  70206 E  70306 70506 E  7	VE MOVE VE MOVE VE MOVE VE MOVE VE STAR	3225 3610 3210 0205 0205			POSTTONI  26.2M 127.8E: 26.1M 127.7E: 26.2M 127.8E: 26.1M 127.7E: 26.1M 127.8E: 26.1M 127.8E: 26.1M 127.8E: 26.1M 127.8E: 26.1M 127.8E: 26.1M 127.8E:	MMO NO.  A7937 47937
12 3 4 5 6 7 8 9 10 112 3 14 5 15 6 17 8 9 21 22 3 24 5 6 7 8 9 22 22 3 24 5 26 7 28 9 20	252100 252200 252200 252300 252300 260000 260100 260100 260100 260300 260300 260500 26	22-9N 129-3E 23-1N 129-3E 23-1N 129-2E 23-3N 129-2E 23-3N 129-2E 23-3N 129-0E	LANDO DA LAN	PADR GAOD PAOR GAOD GAOD GAOD GAOD PAOR PAOR PAOR PAOR GAOD		PE DIAM  30 30 30 30 30 30 30	35//6 4 34//2 9 34//2 9 34//2 9 55//3 9 65//3 9 65//3 9 65//3 9 55//1 9 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	7DDFF  43316 53411 53411 53308 52005 53416 501//  70204 E 70204 70603 E 53306 70504 F 73605 E 73605 E	VE MOVE  VE MOVE  VE STUP  VE STUP  VE STUP	3225 3610 3210 0205 0205			POSTTONI  26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.3M 127.8E: 26.2M 127.8E: 26.1M 127.7E: 26.2M 127.8E: 26.1M 127.7E: 26.1M 127.8E: 26.2M 127.8E:	### NO NO
NO. 1233 456789 1011233145167189 120224 2267829	252100 252200 252200 252300 252300 260000 260100 260100 260200 260200 260300 2605000 2605000 2605000 2605000 2605000 2605000 260500000 2605000	22.9N 129.3E 23.1N 129.3E 23.3N 129.2E 23.3N 129.2E 23.1N 129.2E 23.3N 129.2E 23.1N 129.0E 23.1N 129.0E 23.1N 129.0E 23.5N 129.2E 23.7N 129.2E 23.7N 129.2E 23.7N 129.2E 23.7N 129.2E 23.9N 129.2E 23.9N 129.2E 23.9N 129.2E 24.0N 129.2E 24.0N 129.2E	LANDD	PADR GAOD PAOR GAOD GAOD GAOD GAOD PAOR PAOR PAOR		PE DIAM	35//6 4 34//2 9 34//2 9 54//3 9 65//3 9 65//3 9 65//2 9 35//1 9 75//1	70DFF  43316 53411 53411 53308 52005 53416 501//  70204 E  70204 E  70204 E  70206 F  70405 E  70506 E  73605 F  73606 E	VE MOVG VE MOVG VE MOVG VE MOVG VE STUP VE STUP	3225 3610 3210 0205 0205			POSTTONI  26.2M 127.8E: 26.1M 127.7E: 26.1M 127.8E: 26.2M 127.8E:	##O NO.  #7947
NO.  123456789 101123141561789 2012232452678290 31233	262100 262200 262200 262300 262000 260000 260100 260100 260300 260300 260500 26	22.9N 129.3E 23.1N 129.3E 23.3N 129.2E 23.3N 129.2E 23.3N 129.0E 23.5N 129.1E 23.6N 129.1E 23.6N 129.1E 23.6N 129.1E 23.7N 129.3E 24.0N 129.3E 24.1N 129.3E 24.2N 129.3E	LANDO DO LAN	PADR GAOD PAOR GAOD GAOD GAOD GAOD GAOD PAOR PAOR GAOD		PE DIAM  30 30 30 30 30 30 30 30 30 30 30 30 30	35//6 4 34//2 9 34//2 9 34//2 9 55//3 9 65//3 9 65//3 9 65//3 9 55//1 9 9 55//1 9 55//1 9 55//1 9 9 55//1 9 55//1 9 55//1 9 55	TDDFF  43316 53411 53411 53308 52005 53416 501// E  70204 E  70204 E  70204 E  70204 E  70406 E  70504 E  70506 E  73605 E  73606 E  73606 E  70106	VE MOVG VE MOVG VE MOVG VE STUP VE STUP VE MOVG	3225 3610 3210 0205 0205			POSTTONI  26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.3M 126.8E: 26.2M 127.8E: 26.3M 126.8E: 26.3M 127.8E: 26.3M 127.8E: 26.1M 127.8E: 26.1M 127.7E: 26.2M 127.8E:	### NO NO
NO.  123456789111234516718992123342567899312334	252100 252200 252200 252300 252300 252300 260000 260100 260100 260100 260500 26	22.9N 129.3E 23.1N 129.3E 23.3N 129.2E 23.3N 129.2E 23.3N 129.0E 23.1N 129.0E 23.1N 129.0E 23.1N 129.0E 23.1N 129.0E 23.1N 129.0E 23.1N 129.0E 23.3N 129.2E 24.0N 129.3E 24.2N 129.3E 24.3N 129.3E	LAANDD LA	PADR GAOD PAOR GAOD GAOD GAOD GAOD GAOD GAOD GAOD GAOD		PE DIAM  30 30 30 30 30 30 30 30 30 30 30 30 30	35//6 434//2 9 34//2 9 34//2 9 34//2 9 34//2 9 35//1 9 35//1 9 35//1 9 35//1 9 35//1 9 35//1 9 55//1 9 9 55//1 9 9 55//1 9 9 55//1 9 9 55//1 9 9 9 55//1 9 9 5	# # # # # # # # # # # # # # # # # # #	VE MOVG VE MOVG VE MOVG VE STUP VE STUP VE MOVG	3225 3610 3210 0205 0205			POSTTONI  26. 2M 127.8E1 26. 3M 126.8E. 26. 3M 127.8E1 26. 1M 127.7E1 26. 2M 127.8E1 26. 1M 127.7E1 26. 2M 127.8E1 26. 1M 127.7E1 26. 2M 127.8E1	MMO NO.  A7937 47937
NO.  123456789111234456718991222234562722993012233456335	252100 252200 252200 252300 252300 260000 260100 260100 260200 260500 260500 260500 260500 260500 260500 260500 260500 260500 260500 260500 260500 260500 260500 261000 261000 261000 261100	22.9N 129.3E 23.1N 129.3E 23.3N 129.2E 23.3N 129.2E 23.3N 129.0E 23.1N 129.0E 23.1N 129.0E 23.1N 129.0E 23.1N 129.0E 23.1N 129.0E 23.1N 129.0E 23.3N 129.2E 24.0N 129.2E 24.0N 129.2E 24.0N 129.2E 24.0N 129.2E 24.0N 129.2E 24.0N 129.2E 24.3N 129.3E 24.2N 129.3E 24.3N 129.3E 24.3N 129.3E 24.3N 129.3E 24.3N 129.3E	LAANDO LA	PADR GAOD PAOR GAOD GAOD GAOD GAOD GAOD GAOD GAOD GAOD		PE DIAM  30 30 30 30 30 30 30 30 30 30 30 30 30	35//6 4 34//2 9 34//2 9 34//2 9 55//3 9 65//3 9 65//3 9 65//3 9 55//1 9 9 55//1 9 55//1 9 55//1 9 9 55//1 9 55//1 9 55//1 9 55	### ##################################	VE MOVE VE MOVE VE STUP VE STUP VE STUP VE MOVE VE MOVE VE MOVE	3225 3610 3210 0205 0205 0205			POSTTTON  26. 2M 127.8E1 26.2M 127.8E1 26.1M 127.7E1 26.1M 127.7E1 26.1M 127.7E1 26.1M 127.7E2 26.1M 127.8E2	MMO NO.  A7997 47997
NO.  123456789 1011231451169021223456789033123345637	252100 252200 252200 252300 252300 260000 260100 260100 260100 260100 260500 26	22.9N 129.3E 23.1N 129.3E 23.1N 129.2E 23.3N 129.2E 23.3N 129.2E 23.3N 129.0E 23.3N 129.0E 23.3N 129.0E 23.5N 129.2E 23.5N 129.2E 23.5N 129.2E 23.7N 129.2E 24.1N 129.3E 24.1N 129.3E 24.2N 129.3E 24.3N 129.3E 24.3N 129.3E 24.3N 129.3E 24.3N 129.3E	LAANDO LA	PADR GAOD PAOR GAOD GAOD GAOD GAOD PAOR PAOR GAOD GAOD		PE DIAM  30 30 30 30 30 30 30 30 30 30 30 30 30	35//6 434//2 9 34//2 9 34//2 9 55//3 9 65//3 9 65//3 9 65//3 9 75//1 1 7 75//1 1 7 75//1 1 7 75//1 1 7 75//1 1 7 7 7 7 7 7 7 7	70DFF  43316 53411 53411 53308 52005 53416 501//  70204 E  70204 70603 E 53306 70504 73605 E 73605 F 70106 73603 E F 70106 F 70105 773603	YE MOVG YE MOVG YE MOVG YE STNR YE STNR YE MOVG YE MOVG	3225 3610 3210 0205 0205 0205			POSTTONI  26.2M 127.8E: 26.2M 127.8E: 26.2M 127.8E: 26.3M 127.8E: 26.3M 127.8E: 26.3M 127.8E: 26.3M 127.8E: 26.3M 127.8E: 26.3M 127.8E: 26.1M 127.7E: 26.1M 127.8E: 26.1M 127.7E:	MMO NO.  A7937 47937
NO. 123456789 111234156789 222224 226789 2312333456789 2312333456789 2312333356789 2312333356789 2312333356789 231233356789 231233356789 231233356789 231233356789 231233356789 231233356789 23123356789 23123356789 23123356789 23123356789 23123356789 23123356789 23123356789 23123356789 231256789 23125678789 2312567878789 23125678789 23125678789 231256787878787878789 23125678787	262100 262200 262200 262300 262300 260000 260100 260100 260200 260500 260500 260500 260500 260500 260500 260500 260500 260500 260500 260500 260500 260500 261100 26	22.9N 129.3E 23.1N 129.3E 23.3N 129.2E 23.3N 129.2E 23.3N 129.0E 23.1N 129.0E 23.1N 129.0E 23.1N 129.0E 23.1N 129.0E 23.1N 129.0E 23.1N 129.0E 23.3N 129.2E 24.0N 129.2E 24.0N 129.2E 24.0N 129.2E 24.0N 129.2E 24.0N 129.2E 24.0N 129.2E 24.3N 129.3E 24.2N 129.3E 24.3N 129.3E 24.3N 129.3E 24.3N 129.3E 24.3N 129.3E	LANDO DO LANDO D	PADR GAOD PAOR GAOD GAOD GAOD GAOD GAOD GAOD GAOD GAOD		PE DIAM  30 30 30 30 30 30 30 30 30 30 30 30 30	35//6 434//2 9 34//2 9 34//2 9 34//2 9 34//2 9 35//1 9 35//1 9 35//1 9 35//1 9 35//1 9 35//1 9 55//1 9 9 55//1 9 9 55//1 9 9 55//1 9 9 55//1 9 9 9 55//1 9 9 5	70DFF  43316 53411 53411 53308 52005 53416 501// E  70204 E  70204 E  70204 E  70204 E  70405 E  70506 E  70603 E  70603 E  70605 E  70106 E  70105 70105 70105 701005 70204	VE MOVE VE MOVE VE STUP VE STUP VE STUP VE MOVE VE MOVE VE MOVE	3225 3610 3210 0205 0205 0205			POSTTTON  26. 2M 127.8E1 26.2M 127.8E1 26.1M 127.7E1 26.1M 127.7E1 26.1M 127.7E1 26.1M 127.7E2 26.1M 127.8E2	MMO NO.  A7997 47997

+0	241900	24.44 129.3E	LAND	ცესს	20			EVE	Move	0510	26 NH	127.7E	47937
41	242000	24.54 120.4E	LAND	GnOD	20			FYE	MUAR	0510	26.1N	127.7E	67337
42	262000	24.5N 129.4E	LAND			3//11	70205				26 24		47977
43	245100	24.6N 129.5E	LAHD			5//11					26.1N 26.1N 26.1N 26.1N	127.85	47937
44	242100	24.5N 129.5E	LAND	FAIR	45					0515	56°IN	127.7E	47977
45	245500	24.7N 129.5E	LAND	FAIR	65			EAE	MUAG	<b>U</b> 515	26.1N	127.7E	47937
46 47	262200	24.7N 129.5E	LAHD	- 10		5//41	70204	F C	****	0.E.1.E	26.2N	127.85	47937
48	242300 270000	24.9N 129.5E 24.9N 129.6E	LAND	FAIR GOOD	65					0515 0515	26.1N	127.7E	47937 47937
49	270000	24.9N 129.5E	LAND	Gijoo	6.7	6//41	73607	E V C	14.18(4	0313	26.IN	127.7F	47937
50	270000	34.5N 129.5E	LAND			7////	/999/				28 AN	123.55	47709
51	270100	25.0N 129.5E	LAND			6//11	73006				26.1N	127.7E	47477
52	270100	24.8N ]29.6E	LAND			7////	50211				28.4N	129.5E	479119
53	270100	25.NN 120.6E	LAND	G70U	45			EYE	Move	3620	26.IN	127.7E	47977
54	270200	25.14 129.6E	LAND		_	65///	53616				28.4N 76.1N	129.5E	479119
55	270200	25.1N 120.6E	LAND	G100	65		*2662	EAF	MUAR	3610	26.IN	12/./5	47937 47937
56	270200	25.14 129.5E	LAND	4-00		6//11	73602	CHE	Mauc	3610	26.1N	127.75	47937
57 58	270300 270300	25.2N 129.6E 25.2N 129.5E	LAND LAND	6 <b>100</b>	20	6//11	53602	EAE	MITAL	3610	26.1N	127.7F	47937
59	270300	25.2N 120.6E	LAND				53608				28.4N	129.5E	479119
60	270400	25.4M 129.4E	LAND			6//41	73509				26 IN	127.7F	47937
61	270400	25.3N 129.6E	LAND			65///	53608				28.4N 26.1N 26.1N	129.5E	479119
62	270400	25.2N 129.6E	LAND	6000	45			E∀E	MOVE	3610	26.1N	127.7E	47977
63	270500	25.4N 129.3E	LAND				73604				26.1N	127.75	47937
64	270500	25.4N 129.6E	LAND			65///	53603				28.4N	129.5E	479119
65	270510	25.5N 129.0E	LAND	6n0D							26.4N	127.5E 127.83 127.8E	47931
66	270535	25.5N 129.6E	LAND	G10D							20.4N	151.8F	47931
67	270500	25.4N 129.6E	LAND			65///	70205				70.10	127.7E	47937 47909
68	270500	25.4N 129.6E	LAND	2-30		N-///	50000				26 AN	127.85	47931
69	270610	25.74 129.5E	LAND	6000							26.4N	127.8E	47931
70 71	270630 270700	25.7N 129.5E	LAND LAND	Gn0D		45///	50108				28.4N	127.8E 129.5E 127.7E 127.7E	47909
72	270700	25.5N 129.6E 25.5N 129.7E	LAND	Gn00	55	., ,, . ,	30.00	FYE	MOVE	3610	26.1N	127.7E	47937
73	270700	25.5N 129.7E	LAND	9 100	• •	55/11	70605				26.1N	127.75	47937
74	270710	25.74 129.4E	LAND	6า0ย							76.4N	127.8E 127.7E	47931
75	270900	25.5N 129.7E	LAND	G100	5.0			E∀€	HOVE	3610	26.1N	127.7E	47937
76	270800	25.7N 129.7E	LAND				70206				26. IN	127.7F	47937
77	270800	25.5N 129.6E	LAND			65///	53505				2B.4N	127.5E 127.8E 127.8E 127.7E	47309
78	270810	25.7N 129.3E	LAND	Gn0D							26.4N	127.8E	47931
79	270940	25.7N 129.3E	LAND	Gabu		3	70205				76.4N	151.9F	47931 47937
80	270900	25.7N 129.7E	LAND								20.1×	127.15	47909
81	270900	25.84 129.7E	LAND	<b>G</b> ე00	60	65///	50208	EVE	Maye	3615	26.14	129.5E 127.7E	47937
82 83	270900	25.7M 129.8E	LAND	Gn00				210		, 3013	26.4N	127.8F	47931
84	270910 270940	25.9N 129.4E	LAND	6100							26.4N	127.8E 127.8E 127.5E	47931
85	271000	25.8N 129.7E	LAND	6,100		65///	50000				28.4N	129.5E	47909
86	271000	25.9N 129.8E	LAND	6000	6.0			EYE	MOVE	3610	26.IN	127.7E	47937
87	271000	25.7N 129.7E	LAND	• • •		6//41	73604				26.1N	127.7E	47937
88	271035	25.9N 129.6E	LAND	PnOR							26.4N	127.8E 127.7E	47931
89	271100	25.8N 129.8E	LAND	Gn0D	60			EYE	Move	3610	26.1N	127.7E	47937
90	271100	25.8N 129.8E	LAND			2//41	70502				26.1N	127./6	47937
91	271100	25.9N 179.8E	LAND	- 00		65///	50602	~		7470	58.4N	127.7E 127.7E 127.7E 127.7E	47909 47937
92	271200	25.0N 129.7E	LAND	GnOD	60		70100	EAF	MUA	3620	26 IN	121+16	47937
93	271200	25.9N 129.8E	LAND			5//11	70104 73507				26.1W	127.7E	47937
95	271300 271300	26.1N 129.7E 26.8N 129.7E	LAND	G100	60	3//11	,350.	FVF	MOVG	3615	26.1N	127.7E	47937
96	271400	26.2N 129.7E	LAND	6100	60					3515	26.1N	127.7E	47937
97	271400	36.24 129.6E	LAND			5//11	73309	_			26.1N	12747E	47937
98	271400	26.1N 129.6E	LAND			65///	53011 73505				28.4N	129.5E	47909
99	271500	26.2N 129.7E	LAND			6///1	73505				26.1W	127.75	47937
100	271500	24.34 120.6E	LAND			65///	53608 73605				78.4N	127.7E	47909
101	271600	25.3N 129.7E	LAND			6///1	73605				20.14	151.15	47937
102	271600	26.5N 129.6E	LAND	2-00		65///	53611		Me	2415	26 11	129.5E	479n9 479:R
103	271500	26.5N 129.7E	CAND CAND	Phon		46.44	51104	FAF	HITCH	3615	28 AM	127.7E 129.5E	47909
104	271700	26.4N 129.7E		PnOR		H-7//	34407	FVF	Mone	3 0410	26. IN	127.7F	47977
105 106	271700 271700	26.5N 129.8E 26.4N 129.8E	CMAJ	e.pvn		6///1	70204	_ + c	17.1419	· • · • •	26. IN	127.7E	7937
107	271800	26.6N 129.8E	LAND	POOR		.,,,.	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	FYE	MOVE	; 0510	26.1N	127.7E	47937
108	271900	26.6× 129.7E	LAND			6///1	70106				26.1N	127.7E	47937
109	271900	26.5N 129.7E	LAND			65///	53604				28.4M	129.58	47909
110	271900	26.5H 129.7E	LA+ID			65///	53203				28.4N	129.SE:	47909
111	271900	26.6N 129.6E	LAND			6///1	73506	_	1.		26.1N	129.5E	47937
112	271900	24.6N 129.8E	LAHD	PhDR			-25	EYE	STNR	7	76.3N	125.8E	47929
113	272000	26.7N 129.7E	LAND	n-03		6//11	73506		uc	A 2.4E	27 AM	125.8E 127.7E 128.7E	47937
114	272000	26.5N 129.7E	LAND	PnDR						3 0305	27 AA	1630/6	47942 47942
115 116	272100 272100	26.7N 129.8E 26.8N 129.7E	LAND LAND	POUR		5//11	73605	545	HUAG	3 0310	26.1N	128.7E 127.7E 129.5E	7937
117	272200	54-84 154-8E	LAND				50205				28.4N	129.5E	47909
118	272200	26.9N 129.8E	LAND	FAIR	40			EVE	MOVE	3610	27.4N	128.7E	47942
119	272300	27.0N 129.8E	LAND	ดกขบ	30					3615	27.49	129.7E	47942
120	272300	27.0N 129.BE	LAND	•			53611				78.4W	127.5E 127.5E	47909
121	20000	27.0N 129.8E	LAND				50000				28.4N	123.5E	47909
155	240000	27.1N 129.BE	LAMD	6500	45			EYF	Move	3610	27.4N	128.7E	47942
123	2a0035	27.0N 129.3E	LAND	<b>ცი</b> მს							76.4N	127.85	47971
124	280110	27.3N 129.9E	LAND	FAIR							26.4N	127.8E	67931 47931
125	2m0135	27.4N 179.0E	LAND	FAIR		46	53108				28 4	127.5E	47909
126	2AU200	27.1N 129.6E	LAND			H-7///	33.00						4

12		0 27.44	120.6	LAND	FAIR										
12		0 52.34	129.76	LAND	ดวบบ	45	5		FV	Mov	a 3510			127.8E	47931
15			129.68					// 53303			. 3310		76.1N	127.7E	47937
13 13			120.H		eunn	61	n			Mov	G 3610		27 AN	129.5E	47909
13			120.98	LAND	POUR								26 41	127.8E	47942
13.		U (1.44)	129.7E	LAND	6200	41			EVI	MOV	R 3205		27.4N	128.7E	47931 47942
13			150.06	LAND				71 70601					26.2N	127.8E	47937
13			129.88	LAND				// 50203					28.4N	129.5E	47909
13			150.46					11 70502						127.8E	47937
13			129.86		ცემს			// 5030B					28.4N	129.5E	47909
130			129.88		GNUD	E (					3605		27.4N	128.7E	47942
1.3			120.85		0:100	50		. = 0.20.	EYE	Move	3605		27.4N	128.7E	47942
14(			120.96					1 70204					26,2№	127.8E	47997
141	28070		129.HE		6900	41		// 50603					28.44	129.5E:	47989
142			129.95	LAND	Gn00	4.0					3605		27.4N	123.7E	47942
14:		27.44	120.45	LAND	0.,	-,,		/ 53504	E * 2	MOUN	0305		21.4N	128.7E	47942
144			129.78	LAND	GOUD		,,,	, 33504					28.4N	129.5E	47909
14:			150.95				55//	/ 50103					20,4N	127.BE	47931
1+6			129.9E		GnDD	20	)		FYE	STNE	•		20.4M	129.5E	47909
147			150.BE		FAIR					•			26.44	128.7E	47942
148			129.BE		FAIR								26 44	127.8E	4793 <u>1</u> 4793 <u>1</u>
150			129.9E		GnOD	25			EYE	Move	0505		27 AM	128.7E	47942
151			129.9E				55//	/ 53604					28.4N	129.5E	47909
152			124.58		POR								26.4N	127.8E	47931
153			129.78		6n0D								26.4N	127.8E	7931
154			129.9E	LAND LAND	GnDD	25			EYE	MOVE	3610		27,4N	128.7E	47942
155			129.8E		FAIR		55.4						26,4N	127.8E	47931
156			129.9E		GnDD	25	55//	/ 52004					28,4N	129.5E	47909
157			129.88	LAND	0.,00	7.7		/ 52003	EVE	STNR	,		27.4W	128.7E:	47942
158			129.9E	LAND	GODU	25	77//	, 25003	EVE	Mous	3205		28.4N	129.5E	47909
159			129.9E	LAND	GOUD	30					3605		27.4N	128.7E	47942
160		27.4N	129.8E	LAND		***		/ 51203	E + C	HUAN	3003		27.4N	128.7E	47942
161	291535	27.5N	129.9E	LAND	6000	3.0		. 31-00	EVE	Move	3605			129.5E	47909
162		27.6N	129.9E	LAND				/ 53404		1417419	3003			128+7EI	47942
163		27.6N	129.9E	LAND	Gn00	30		. 55.0.	FVF	STNR			28,4N	129.58	47909
164			129.8E	LAVO				/-53302		3144			27.4N	128.7E	47942
165			120.95	LAND	GnOD	30			EYE	STAR			27 44	129.5E	47909
166			124.8E	LAND	GDOD	30					3610		27.4N	128.7E	47942
167			150.85	LAND			55//	/ 53604	_				28.4N	120-151	47942
168			129.8E	LAND	GnOD	30			EYE	STNR			27.4N	128.7E	47909
169 170			129.BE	LAND				/ 53403					28.4N	129.5E	47942 47909
171			129.7E	LAND	0-00		45//	/ 53102					28.4N	129'-5E'	47909
172			129.7E	LAND	GOOD	nF			EYE	STNR			27.4N	128.7E	47942
173			129.8E	LAND	GnOD		55//	/ 53605		_			28.4N	129.5E	47909
174			129.8E	LAND	GIJOD	0F			EAE	STNR			27.4N	128.7E	47942
175			129.8E	LAND	GnOD		77//	/ 50903					28.4N	129.5E	479119
176			129.8E	LAND	61,00	90	EE	53405	EYE	MOVG	3610		27.4N	128.7E	47942
177			129.7E	LAND	Gn0D	30	27//	53403		Maria	3210		28.4N	129.5E	479119
178	290500		129.7E	LAND	0.,,	707	55//	2 53504	245	MUAG	3210		27.4N	128-7E	47942
179		28.1h	129.7E	LAND	GnOD	30	,,,,,	. 55504	FUF	Move	3605		28.4N	129.5EI	47919
180			129.7E	LAND			10382	2 50205	ETC	MILLOW	3003		27.4N	128.7E	47942
181	290300	28. SN	150.8E	LAND	GODD	30	• " - "	- 50-00	FVF	Move	3605		28,4N	129.5E	47909
182	290400		129.8E	LAND	GnDD	30					3615		27.4N	125+7E	47942
183 184	290400		129.BE	LAND			10412	50105	_				27.4N 28.4N	1204 [ [	47942
185	290500		129.7E	LAND			11512	2 53608					28.4N		47909 47909
186	290500 290520		129.8E	LAND	6200	9.0			EYE	MOVE	3610		27.4N	128.7F	47942
187	290500		129.BE	LAND	FAIR					STNR		TAKAHATA	21.	1204.2	41746
188	290610	29.5N	129.8E	LAND	0000		11322	2 50208					28.4N	1295EI	47909
189	290700	28.5N		LAND	GOOD	20				STNR		TAKAHATA	•		4,50,5
190	290700	29.6N		LAND LAND	G00D G00D	20			EYE	STAR		TAKAHATA			
191	290700	28.5N		LAND	0.,00	96			EAE	Move	3610		27.4N	128.7E	47942
192	200700	28.4N	129.8E	LAND				5////					30.6N	31.0E	47969
193	290800	28.6N	129.9E	LAND				50405					28.4N	29.5E	47909
194	290800	28.6N		LAND	GOOD	30	11716	30405	FUE	Maria	3610		28.4N	29.5E	47909
195	290800	28.6N	129.9E	LAND	GOOD	25			FVF	AVON	3010	74744474	27.4N	128+7E	47942
196	290800	28.7N	129.8E	LAND			5///1	53505	EVE	HUVE	0310	TAKAHATA	24 45		
197	200900	28.7N	129.9E	LAND				50505					30.6N		47869
198 199	290900	29.74		LAND				50605					30.6N -	20 50	47869 47909
200	290300	29.7N	129.YE	LAND	GOOD	25			EYE	AVON	0310	TAKAHATA	20,71	E 7 8 3 C.	41303
201	291000	28. AN		LAND	****		11412	50505				10.70010	28,4N	29',5F	47909
			1.30 a LE	LAND	GODD	20	_		EYE	Move	0000	TAKAHATA			4.207
202	291000	28.7N	130.05								0020				47869
202	291000	28.8N	13n.0E	LAND				50508	_		0620		30.6N	31.UE	
202 203 204	291000 2 <sub>0</sub> 1100	29.9N	13n.0E 13n.1E	LAND	eann.			50508 50108					30.6N 1	29.5E	4/909
203	201100 201100	28.8N 28.9N 28.8N	13n.0E 13n.1E 13n.1E	LAND LAND LAND	6n00	20			€¥E	Move	0215	TAKAHATA	30.6N 1 28.4N 1	29.5E	47909
203 204	501100 501100 501100 501000	24.9N 24.9N 24.9N	13n.0E 13n.1E 13n.1E 13n.1E	ONAJ ONAJ LAND LAND	ცი0ს ცი <b>ს</b> 0	30- 20	11532	50108	€¥E		0215		30.6N 1 28.4N 1 27.4N 1	29%5EI	47919
203 204 205 206 207	201200 201100 201100 201100 201200	24.9N 24.9N 24.9N	13n.0E 13n.1E 13n.1E 13n.1E 13n.1E	CAND CAND CAND CAAL ONAL	6400	30	11532		E4E	Move Move	0215 2020		28.4N 1 27.4N 1 30.6N 1	29.5EI 28.7EI 31.0E:	47942 47869
203 204 205 206 207 208	201200 201100 201100 201100 20100 201000	29.9N 29.9N 29.9N 24.9N 24.9N	13n.0E 13n.1E 13n.1E 13n.1E 13n.1E	ONAJ ONAJ LAND LAND			5///1	50108	E4E	Move	0215 2020		28.4N 1 27.4N 1 30.6N 1 27.4N 1	29.5EI 28.7EI 31.0E: 28.7EI	47942 47869 47942
203 204 205 206 201 208 209	291200 291200 291100 291100 291200 291200 291200	24.9N 24.9N 24.9N 24.9N 24.9N	130.0E 130.1E 130.1E 130.1E 130.1E 130.2E	LAND LAND LAND LAND LAND LAND	6400	30	11532 5///1 5///1	50108 50311 50405	E4E	Move Move	0215 2020		28.4N 1 27.4N 1 30.6N 1 27.4N 1 30.6N 1	29.5EI 28.7EI 31.0E: 28.7EI 31.0E:	47942 47869 47942 47869
203 204 205 206 207 208 209 210	291000 201100 291100 291100 291200 291200 291200 291300	28.8N 28.9N 28.8N 24.9N 24.9N 29.0N 29.0N 29.0N	130.0E 130.1E 130.1E 130.1E 130.1E 130.2E 130.2E 130.2E	LAND LAND LAND LAND LAND LAND LAND	6400	30	5///1 5///1 5///1 11412	50108 50311 50405 50107	E4E	Move Move	0215 2020		28.4N 1 27.4N 1 30.6N 1 27.4N 1 30.6N 1 28.4N 1	29.5EI 28.7EI 31.0EI 28.7EI 31.0EI 29.5EI	47942 47869 47942 47869 47989
203 204 205 206 207 208 209 210 211	201300 201300 201300 201300 201300 201300 201300 201300	29.8N 29.9N 29.9N 24.9N 29.0N 29.0N 29.0N 29.1N 29.1N	13n.0E 13n.1E 13n.1E 13n.1E 13n.1E 13n.2E 13n.2E 13n.2E 13n.2E 13n.2E	LAND LAND LAND LAND LAND LAND LAND LAND	600D	30	5///1 5///1 5///1 11412 5///1	50108 50311 50405 50107 50208	E4E	Move Move	0215 2020		28.4N 1 30.6N 1 27.4N 1 30.6N 1 28.4N 1 30.6N 1	29.5E1 31.0E: 28.7E1 31.0E: 29.5E1 31.0E1	47942 47869 47942 47869 47989
203 204 205 206 207 208 209 210 211 212	291000 201100 291100 291100 291200 291200 291200 291300 291300 291300 291400	29.9N 29.9N 24.9N 24.9N 24.9N 29.0N 29.0N 29.1N 29.1N 29.1N 29.2N	130.0E 130.1E 130.1E 130.1E 130.2E 130.2E 130.2E 130.2E 130.2E	LAND LAND LAND LAND LAND LAND LAND LAND	6400	30	5///1 5///1 5///1 11412 5///1	50108 50311 50405 50107	E4E E4E	MOVA MOVA MOVA	0215 2020 0215		28.4N 1 30.6N 1 27.4N 1 30.6N 1 28.4N 1 30.6N 1 28.4N 1	29.5EI 28.7EI 31.0EI 28.7EI 31.0EI 29.5EI 31.0EI	47942 47869 47942 47869 47909 47969
203 204 205 206 207 208 209 210 211 212 213	291000 201100 201100 201100 201200 201200 201200 201300 201300 201400 201400	29.9N 29.9N 24.9N 24.9N 24.0N 29.0N 29.0N 29.1N 29.1N 29.2N 29.2N	130.0E 130.1E 130.1E 130.1E 130.2E 130.2E 130.2E 130.2E 130.2E 130.2E	LAND LAND LAND LAND LAND LAND LAND LAND	600D	30 <u>-</u>	5///1 5///1 5///1 11412 5///1 11412	50108 50311 50405 50107 50208	E4E E4E	Move Move	0215 2020 0215		28.4N 1 27.4N 1 30.6N 1 27.4N 1 30.6N 1 28.4N 1 30.6N 1 28.4N 1 27.4N 1	29.5EI 31.0E: 28.7EI 31.0E: 29.5EI 31.0EI 29.5EI 29.5EI 29.5EI	47942 47869 47942 47869 47909 47969 47969
203 204 205 206 207 208 209 210 211 212 213 214	291000 201100 291100 291100 291200 291200 291200 291300 291400 291400 291400	29.9N 29.9N 24.9N 24.9N 24.9N 29.0N 29.0N 29.1N 29.1N 29.2N 29.2N 29.2N	130.0E 130.1E 130.1E 130.1E 130.2E 130.2E 130.2E 130.2E 130.4E 130.4E	LAND LAND LAND LAND LAND LAND LAND LAND	600D	30 <u>-</u>	5///1 5///1 5///1 11412 5///1 11412	50108 50311 50405 50107 50208 50105	EYE EYE EYE	MOVA MOVA MOVA	0215 2020 0215 0520	TAKAHATA	28.4N 1 30.6N 1 27.4N 1 30.6N 1 28.4N 1 30.6N 1 28.4N 1	29.5EI 31.0E: 28.7EI 31.0E: 29.5EI 31.0EI 29.5EI 29.5EI 29.5EI	47942 47869 47942 47869 47909 47969
203 204 205 207 208 209 210 211 213 214 215	291000 201100 201100 291100 201200 201200 201200 201300 201400 201400 201400 201400 201400	29.9N 29.9N 29.9N 29.0N 29.0N 29.1N 29.1N 29.2N 29.2N 29.2N 29.2N 29.2N	130.0E 130.1E 130.1E 130.1E 130.2E 130.2E 130.2E 130.2E 130.4E 130.4E	LAND LAND LAND LAND LAND LAND LAND LAND	6000 6000 6000	30- 30 25 20	5///1 5///1 5///1 11412 5///1 11412	50108 50311 50405 50107 50208 50105	EYE EYE EYE	HOVG MOVG	0215 2020 0215 0520		28.4N 1 27.4N 1 30.6N 1 27.4N 1 30.6N 1 28.4N 1 28.4N 1 27.4N 1 28.4N 1	29,551 28,751 31,051 28,751 31,051 29,551 31,051 29,551 29,751 29,551	47942 47942 47942 47949 47949 47949 47949 47942 47942
203 204 205 206 207 208 209 210 211 213 214 215 216	291000 201100 291100 291100 291200 291200 291200 291300 291300 291400 291400 291400 291400 291500	29.8N 29.8N 29.8N 29.0N 29.0N 29.0N 29.1N 29.1N 29.1N 29.2N 29.2N 29.2N 29.2N 29.2N 29.2N	130.0E 130.1E 130.1E 130.1E 130.2E 130.2E 130.2E 130.2E 130.2E 130.3E 130.3E 130.3E	LAND LAND LAND LAND LAND LAND LAND LAND	600D	30. 30 25	5///1 5///1 5///1 11412 5///1 11412 11511 204/1	50108 50311 50405 50107 50208 50105 50309 50309	EYE EYE EYE	HOVG MOVG	0215 2020 0215 0520 0315	TAKAHATA	28.4N 1 27.4N 1 30.6N 1 27.4N 1 30.6N 1 28.4N 1 30.6N 1 28.4N 1 27.4N 1	29,551 28,751 31,051 28,751 31,051 29,551 31,051 29,551 29,751 29,551	47942 47869 47942 47869 47909 47969 47969
203 204 205 207 208 209 211 212 213 214 215 217	291000 201100 291100 291100 291200 291200 291200 291300 291300 291400 291400 291400 291500 291500	29.8N 24.9N 24.9N 24.9N 29.0N 29.0N 29.1N 29.1N 29.2N 29.2N 29.2N 29.2N 29.3N	13n.0E 13n.1E 13n.1E 13n.1E 13n.2E 13n.2E 13n.2E 13n.2E 13n.3E 13n.3E 13n.3E 13n.3E	LAND LAND LAND LAND LAND LAND LAND LAND	6000 6000 6000	30- 30 25 20	5///1 5///1 5///1 11412 5///1 11412 11511 204/1 21411	50108 50311 50405 50107 50208 50105 50309 50305 50307	EYE EYE EYE	Move Move Move Move	0215 2020 0215 0520 0315	TAKAHATA TAKAHATA	28,4N 1 27,4N 1 30,6N 1 27,4N 1 30,6N 1 28,4N 1 27,4N 1 28,4N 1	29.5EI 28.7EI 31.0Ei 28.7EI 31.0Ei 29.5EI 31.0EI 29.5EI 28.7EI 29.5EI	47942 47869 47942 47869 47909 47909 47942 47909 47869
203 204 205 207 208 209 210 211 212 213 214 215 216 217 218	291000 201100 291100 291100 291200 291200 291200 291300 291400 291400 291400 291500 291500	29.9N 29.9N 29.9N 29.9N 29.0N 29.0N 29.1N 29.2N 29.2N 29.2N 29.2N 29.2N 29.3N 29.3N 29.3N	13n.0E 13n.1E 13n.1E 13n.1E 13n.2E 13n.2E 13n.2E 13n.2E 13n.3E 13n.3E 13n.3E 13n.3E 13n.3E	LAND LAND LAND LAND LAND LAND LAND LAND	GOOD GOOD GOOD	30. 30 25 20 20	5///1 5///1 5///1 11412 5///1 11412 11511 204/1 21411	50108 50311 50405 50107 50208 50105 50309 50309	EAE EAE EAE	HOVE MOVE MOVE MOVE	0215 2020 0215 0520 0315	TAKAHATA TAKAHATA	28.4N 1 27.4N 1 30.6N 1 27.4N 1 30.6N 1 28.4N 1 28.4N 1 27.4N 1 28.4N 1 28.4N 1	29,5EI 28,7EI 31,0Ei 28,7EI 31,0Ei 29,5EI 31,0EI 29,5EI 31,0EI 31,0EI	47942 47869 47942 47869 47909 47909 47909 47909 47869 47869
203 204 205 207 208 209 211 212 213 214 215 217	291000 201100 291100 291100 291200 291200 291200 291300 291400 291400 291400 291500 291500 291500 291500	28.8N 28.9N 28.9N 28.9N 29.0N 29.0N 29.1N 29.1N 29.1N 29.2N 29.3N 29.3N 29.4N	13n.0E 13n.1E 13n.1E 13n.1E 13n.2E 13n.2E 13n.2E 13n.2E 13n.3E 13n.3E 13n.3E 13n.3E 13n.3E	LAND LAND LAND LAND LAND LAND LAND LAND	6000 6000 6000	30- 30 25 20	11532 5///1 5///1 11412 11511 204/1 21411 5///1	50108 50311 50405 50107 50208 50105 50309 50309 50307 53608	EAE EAE EAE	Move Move Move Move	0215 2020 0215 0520 0315	TAKAHATA TAKAHATA	28.4N 1 27.4N 1 30.6N 1 27.4N 1 30.6N 1 28.4N 1 27.4N 1 28.4N 1 30.6N 1	29.5E 28.7E 31.0E 28.7E 31.0E 29.5E 31.0E 29.5E 29.5E 31.0E 29.5E	47942 47869 47942 47869 47969 47969 47969 47969 47969 47869
203 204 205 207 208 209 210 212 213 214 215 216 217 218 219	291000 201100 291100 291100 291200 291200 291200 291300 291400 291400 291400 291500 291500	29.84 24.84 24.84 24.04 29.04 29.04 29.10 29.10 29.10 29.20 20.20 20.20 20.30 20.30 20.30 20.30 20.30	130.0E 130.1E 130.1E 130.1E 130.2E 130.2E 130.2E 130.2E 130.2E 130.3E 130.3E 130.3E 130.3E 130.3E	LAND LAND LAND LAND LAND LAND LAND LAND	GOOD GOOD GOOD	30. 30 25 20 20	11532 5///1 5///1 11412 5///1 11412 11511 204/1 21411 5///1	50108 50311 50405 50107 50208 50105 50309 50309 50307 53608 50308	EAE EAE EAE	HOVE MOVE MOVE MOVE	0215 2020 0215 0520 0315	TAKAHATA TAKAHATA	28.4N   27.4N   30.6N   28.4N   27.4N   28.4N   27.4N   27.4N   28.4N   27.4N   30.6N   28.4N   30.6N   27.4N   30.6N   30.6N	29.5EI 28.7EI 31.0Ei 29.5EI 29.5EI 29.5EI 29.5EI 29.5EI 31.0EI 29.5EI 31.0EI 29.5EI 31.0EI	47942 47869 47942 47869 47909 47909 47909 47909 47869 47869
203 2045 205 207 209 210 211 213 214 215 216 217 218 217 218 217 218 219 220	291000 201100 291100 291100 291200 291200 291200 291300 291400 291400 291400 291500 291500 291500 291500 291600	24, 9N 24, 9N 24, 9N 24, 9N 24, 9N 24, 9N 24, 9N 24, 1N 24, 1N 24, 1N 24, 2N 24, 3N 24, 3N 3N 3N 3N 3N 3N 3N 3N 3N 3N 3N 3N 3N 3	13n.0E 13n.1E 13n.1E 13n.1E 13n.2E 13n.2E 13n.2E 13n.2E 13n.3E 13n.3E 13n.3E 13n.3E 13n.3E 13n.3E 13n.3E	LAND LAND LAND LAND LAND LAND LAND LAND	6000 6000 6000 6000	30- 30- 25- 20- 20- 25-	11532 5///1 5///1 11412 5///1 11412 11511 204/1 21411 5///1	50108 50311 50405 50107 50208 50105 50309 50309 50307 53608	EYE EYE EYE EYE	Hove Move Move Move Move	0215 2020 0215 0520 0315 0315	TAKAHATA TAKAHATA	28.4N 1 30.6N 1 28.4N 1 28.4N 1 28.4N 1 28.4N 1 28.4N 1 28.4N 1 28.4N 1 30.6N 1 30.6N 1 27.4N 1 30.6N 1 27.4N 1 30.6N 1	29-55: 28-75: 31-05: 29-75: 31-05: 29-55: 31-05: 29-55: 31-05: 29-55: 31-06: 29-56: 31-06:	47942 47869 47942 47969 47969 47969 47969 47969 47969 47869 47969 47869
203 204 205 207 208 209 211 212 213 215 216 217 218 217 218 217 218 219 220 221 221 222 223	201000 201100 201100 201100 201200 201200 201200 201200 201300 201400 201400 201400 201500 201500 201500 201500 201500 201500 201500 201500 201500	24,9N 24,9N 24,9N 24,9N 24,0N 29,0N 29,1N 20,2N 20,2N 20,2N 20,2N 20,2N 20,2N 20,5N 20,5N 20,5N 20,5N 20,5N 20,5N	130.0E 130.1E 130.1E 130.1E 130.2E 130.2E 130.2E 130.2E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E	LAND LAND LAND LAND LAND LAND LAND LAND	6000 6000 6000 6000 6000	30- 30- 25- 20- 20- 25- 25-	11532 5///1 5///1 11412 5///1 11412 11511 204/1 21411 5///1	50108 50311 50405 50107 50208 50105 50309 50309 50307 53608 50308	EAE EAE EAE EAE EAE	Hove Hove Move Move Move Hove	0215 2020 0215 0520 0315 0315 0315	TAKAHATA Takahata Takahatà	28.4N   27.4N   30.6N   28.4N   27.4N   28.4N   27.4N   27.4N   28.4N   27.4N   30.6N   28.4N   30.6N   27.4N   30.6N   30.6N	29-55: 28-75: 31-05: 29-75: 31-05: 29-55: 31-05: 29-55: 31-05: 29-55: 31-06: 29-56: 31-06:	47942 47942 47942 47949 47949 47949 47942 47942 47949 47869 47869 47869 47869
203 2045 206 207 208 209 211 213 213 214 215 218 221 221 222 222 223 224	201000 201100 201100 201100 201200 201200 201200 201300 201300 201400 201400 201400 201500 201500 201500 201600 201600 201600	24, 8N 24, 9N 24, 9N 24, 9N 24, 0N 24, 0N 20, 1N 20, 1N 20, 2N 20, 2N 20, 2N 20, 5N 20, 5N	130.0E 130.1E 130.1E 130.1E 130.2E 130.2E 130.2E 130.2E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E	LAND LAND LAND LAND LAND LAND LAND LAND	6000 6000 6000 6000	30- 30- 25- 20- 20- 25-	5///1 5///1 11412 5///1 11412 11511 204/1 21411 5///1 51///1	50108 50311 50405 50105 50208 50105 50309 50305 50307 53608 50107	EAE EAE EAE EAE EAE	Hove Move Move Move Move	0215 2020 0215 0520 0315 0315 0315	TAKAHATA TAKAHATA	28,4N 1 27,4N 3 30,6N 1 28,4N 1 28,4N 1 27,4N 1 28,4N 1 20,6N 1 28,4N 1 30,6N 1 28,4N 1 27,4N 1 27,4N 1 27,4N 1 27,4N 1 27,4N 1 27,4N 1	29,55: 28,75: 31,05: 29,75: 31,05: 29,55: 29,55: 31,06: 29,55: 31,06: 29,55: 31,06: 29,55: 31,06: 29,55: 31,06: 29,55: 29,56: 29,56:	47942 47849 47942 47849 47969 47969 47962 47969 47969 47869 47982 47869 47849 47849 47942
205 205 206 206 206 209 2112 213 214 215 217 218 220 221 222 223 223	201000 201100 201100 201100 201200 201200 201200 201200 201300 201400 201400 201400 201500 201500 201500 201500 201500 201500 201500 201700 201700	24, 8N 24, 9N 24, 9N 24, 9N 24, 0N 24, 0N 20, 1N 20, 1N 20, 2N 20, 2N 20, 2N 20, 5N 20, 5N	130.0E 130.1E 130.1E 130.1E 130.2E 130.2E 130.2E 130.2E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E	LAND LAND LAND LAND LAND LAND LAND LAND	6n00 6n00 6n00 6n00 6n00 6n00	20 25 20 20 25 25	5///1 5///1 11412 5///1 11412 11511 204/1 21411 5///1 51///1	50108 50311 50405 50107 50208 50105 50309 50309 50307 53608 50308	EYE   EYE	Move Move Move Move Move Move	0215 2020 0215 0520 0315 0315 3625	TAKAHATA Takahata Takahatà	28,4N 1 27,4N 1 30,6N 1 30,6N 1 30,6N 1 28,4N 1 30,6N 1	29,551 28,751 31,051 28,751 31,051 29,551 29,551 29,551 29,551 31,061 29,561 29,561 29,561 29,561 29,561 29,561 29,561	47942 47849 47949 47949 47949 47949 47949 47949 47949 47949 47949 47949 47942 47949 47942 47949 47942 47949
205 205 206 206 206 207 208 209 211 212 214 215 217 218 218 223 224 223 224 225 226	201000 201100 201100 201100 201200 201200 201200 201200 201300 201400 201400 201400 201500 201500 201500 201600 201600 201700 201700 201700	24,8N 24,9N 24,9N 24,9N 24,0N 24,0N 24,0N 24,0N 24,1N 24,2N	130.0E 130.1E 130.1E 130.1E 130.2E 130.2E 130.2E 130.2E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E 130.3E	LAND LAND LAND LAND LAND LAND LAND LAND	6000 6000 6000 6000 6000	30- 30- 25- 20- 20- 25- 25-	11532 5///1 5///1 11412 5///1 11511 204/1 21411 5///1 5///1	50108 50311 50407 50107 50208 50105 50309 50307 53608 50308 50107	EYE   EYE	Hove Hove Move Move Move Hove	0215 2020 0215 0520 0315 0315 3625	TAKAHATA Takahata Takahatà	28,4N 1 30,6N 1 30,6N 1 30,6N 1 30,6N 1 28,4N 1 27,4N 1 30,6N 1 28,4N 1 30,6N 1 27,4N 1 30,6N 1 27,4N 1 27,4N 1 27,4N 1	29,551 28,751 31,051 29,551 31,051 29,551 31,051 29,551 31,051 29,551 29,551 29,551 29,551 29,751 29,751	47942 47849 47849 47849 47969 47949 47942 47949 47942 47969 47942 47949 47942 47949 47942 47949 47942 47949
205 205 206 206 207 209 211 212 214 215 217 217 218 221 221 221 222 223 225 227	201000 201100 201100 201100 201200 201200 201200 201200 201300 201400 201400 201500 201500 201500 201500 201500 201700 201700 201700 201700 201700	24, 8M 24, 8M 24, 8M 24, 8M 24, 9M 24, 9M 24, 9M 24, 1M 24, 1M 24, 1M 24, 1M 24, 3M 24, 3M 24, 3M 24, 3M 24, 5M 24, 5M 24, 5M 24, 5M 24, 7M 24, 7M 24	130.0E 130.1E 130.1E 130.1E 130.2E 130.2E 130.2E 130.2E 130.3E 130.5E 130.5E 130.5E	LAND LAND LAND LAND LAND LAND LAND LAND	6n00 6n00 6n00 6n00 6n00 6n00	20 25 20 20 25 25 15	11532 5///1 5///1 11412 5///1 11511 204/1 21411 5///1 5///1	50108 50311 50405 50105 50208 50105 50309 50305 50307 53608 50107	EVE   EVE   EVE   EVE   EVE   EVE	Hove Move Move Move Move Move	0215 2020 0215 0520 0315 0315 3625 3625 0325	TAKAHATA TAKAHATA TAKAHATA	28,4N 1 27,4N 1 30,6N 1 30,6N 1 30,6N 1 28,4N 1 30,6N 1	29,551 28,751 31,051 29,551 31,051 29,551 31,051 29,551 31,051 29,551 29,551 29,551 29,551 29,751 29,751	47942 47849 47949 47949 47949 47949 47949 47942 47949 47949 47849 47942 47849 47942 47849 47942 47949 47942
205 205 206 206 207 209 211 212 214 215 217 217 218 221 221 221 222 223 225 227	201000 201100 201100 201100 201200 201200 201200 201200 201300 201400 201400 201400 201500 201500 201500 201600 201600 201700 201700 201700	24,8N 24,9N 24,9N 24,9N 24,0N 24,0N 24,0N 24,0N 24,1N 24,2N	130.0E 130.1E 130.1E 130.1E 130.2E 130.2E 130.2E 130.2E 130.3E 130.5E 130.5E 130.5E	LAND LAND LAND LAND LAND LAND LAND LAND	6000 6000 6000 6000 6000 6000	20 25 20 20 25 25	11532 5///1 5///1 11412 5///1 11511 204/1 21411 5///1 5///1	50108 50311 50405 50107 50208 50105 50309 50307 53608 50307 50411	EVE   EVE   EVE   EVE   EVE   EVE	Move Move Move Move Move Move	0215 2020 0215 0520 0315 0315 3625 3625 0325	TAKAHATA Takahata Takahatà	28,4N 1 30,6N 1 30,6N 1 30,6N 1 30,6N 1 28,4N 1 27,4N 1 30,6N 1 28,4N 1 30,6N 1 27,4N 1 30,6N 1 27,4N 1 27,4N 1 27,4N 1	29.55: 28.75: 31.05: 29.75: 31.06: 29.55: 31.06: 29.55: 31.06: 29.55: 31.06: 29.55: 31.06: 29.55: 31.06: 29.55: 31.06: 29.55: 31.06: 29.56: 31.06: 29.56: 31.06:	47942 47849 47849 47849 47969 47949 47942 47949 47942 47969 47942 47949 47942 47949 47942 47949 47942 47949

229	291900	29.9K 13n.5E	LAHD			21771	50108					30.6%	131.0E	47849
230	291900	24.9N 130.7E	LAND				50511					30.68	131.0E	47969
231	291900	27.9N 130.7E	LAND			21661	50400					78.4N	129.5E	47409
232	241900	30.0N 130.7E	LAMD	g ว บบ	20				MOVE		TAKAHATA			
233	292000	30.1N 130.8E	CI-AJ	<b>ცე</b> მს	20			EYE	MOVE	0420	TAKAHATA			
234	292000	30.16 13n.8E	CMAJ				50216						129.5E	47909
235	292000	30.2N 13n.9E				21571	50314					30.6N	131.0E	47869
236	202100	30.3N 130.9E	LAND				50108						131.0E	47869
237	292100	30.3N 131.0E	LAND			65///	50511					58.4M	129.5E	47909
539	202100	30.3N 130.9E		6-100	20			EAE	MOVG	0420	TAKAHATA	20	ina er	. 7000
239	595500	30.34 131.1E					50506						129.5E	47909
240	202200	30.4N 131.1E				21571	50614					30.00	131.0E	47869 47909
241	292300	30.59 131.2E	LAND				50313					20.4N	129.5E	47869
242	202300	30.4N 131.4E	LAND			10401	50419	ee	****	0530	STHOKOSIKI	30.04	131.00	41003
243	292300	30.6N 131.4E		610D	50				HOVE		S140<051K1			
244	300000	30.9N 131.5E		Gn0D	50	~	50414	EVE	Move	0550	3140707111	30 6N	131.05	47869
245	300000	30.8N 131.6E		a - (10)	20	7///1	20414		MOVE	0524	STHOKASIKI	.10 . 0.1	131100	4,5
245	300100	31.04 131.78	LA*ID	GOUD	~"	20271	50316	2,5	1117917	0324	.,, 10., 10.1	30 6N	131.0E	47869
247	300500	31.3N 131.9E	LAND			45/12	5////					33.4N	130.3E	47906
248 249	340500	31.4M 131.8E	LAMD LAMD	6100	20	17.712	3,	FVF	MOVE	0530	STMOKOSIKI			-
250	3n0200	31.4N 131.9E	LAND	0.100	- 11	6////	11111					33,3₩	134.2E	47999
251		31.5N 131.9E	LAND				50411					33.4N	130.38	47806
252	300300											32.1N	131.5E	47854
253	3n0300 3n0300	31.5N 132.2E 31.5N 132.2E		6n0D	10			EVE	MOVE	0530	STMOKOSIKI			
254	300300	31.5N 132.2E		0.745		5///1	50419					30.6N	131.0E	47869
255	300400	31.7N 132.3E			30			EYE	MOVG	0645	KUSHTHOTO			
256	300400	31.9N 132.4E	LAND			5///1	50419	-				30.6N	131.0E	47869
251	300400	31.8N 132.5E		<b>ცე</b> 00	20			EYE	MOVE	0550	SEBURI			
258	300400	31.9N 132.2E		•		55/72	64019						130.3E	<b>▲7</b> 8∩6
259	300400	31.7N 132.36	LAND			5////	50424					33,3∾	134.2E	47899
260	300500	32.0N 132.76				5////	50522					30,6N	131.0E	47869
261	300500	32.1N 132.78		ცე0ე	20			EYE	MOVG	0540	SEBURI			
595	300500	32.0N 132.7E				10501	50524					33,3N	134.2E	47899
263	300500	31.9N 132.78			75			EYE	HOVE	0440	KJSHIMOTO			
264	300500	32.2N 132.8E	LAND			64745	50430					33.4N	130.3E	47806
265	300520	32.2N 132.HE	LAND	6500			_					32.IN	131.5E	47954
266	300600	32.3M 132.9E	LAND				50522						134.2E	47899
267	300600	32.2N 133.1E	LAND			5///1	50519					30.0N	131.0E	47869 47954
268	300500	32.2N 132.9E	LAND	<b>ცი</b> მმ								35.1M	131.5E	47792
269	300500	32.2N 133.0E	LAND		_	746/3	50322			0540	SEBURI	34.34	1.35.6E1	41176
270	300600	32.3N 137.0E	LAND	GnOD	25					0540 0155	KUSHTMOTO			
271	3n0600	32.2N 132.76	LAND		45					0540	SEBURI			
272	3n0700	32.4N 137.38	LAND	GnOD	20	10511	50522	E A E	Miser	0340	3-00K2	33.3N	134.2E	47899
273	300700	32.5N 137.2E	LAND		4.0	10551	30322	EVE	Move	0150	KJSHIMOTO	55.5.	, , , , , ,	4.0.2
214	300/00	32.6N 132.6	LAND		411	244/7	50419	E VE	Hitely	0130	403.11.010	34.3N	132.6E	47792
275	300700	32.5N 133.28					5052/						132.66:	47792
276	300800	37.9N 133.76					50524						134.26	47899
278	300800	32.89 133.66 33.00 133.76	LAND	ცესნ	20	20,100	10321	EYE	Hove	0540	SEBURI			• • •
274	300900	31.1N 174.06		0.702	45					0345	KJSHIMOTO			
280	300900	33.1× 137.96				20541	50522					33.3N	134.2E	47899
281	300900	33.14 133.96		คาบหิ	20		- '	EYE	MOVE	0540	SEBURI			
282	300900	33.IN 134.0		. ,		65//2	50524					34.3N	132.6E	47792
283	301000	33.4N 134.36				2054]	50522					33.3N	134.2E	47999
284	301000	33.3N 137.21	LAND		4.5			EYE	MOVE	0540	K NÉ41WOTO			
285	301000	37.4N 134.4	LAND			65//2	50527					34.3N	135.6E	<b>47792</b>
286	301000	33.2N 133.9				65///	50716					35.3N	138.7E	47639
287	3n1100	37.5N 134.50	LAND		40			EYE	MOVG	0645	KU54TH0T0			
288	3n1100	33.9N 134.8	LAND				50427						132.6E	47792
289	301100	33.5N 134.6	LAND				50524						134.25	47899
290	3,1100	33.4N 134.5					50032					35.38	138.7E	47639
291	301100	33.9N 134.7				105//	11111		Me	0135	KASATORI	34.41	135.7E	47773
595	301200	33.7N 134.7			45			EYE	MUAG	0435	KASAIDRI	25 24	120 TE	47639
293	3n1200	31.5N 135+1					70724						138.7E	47849
294	301500	34.0N 134.8				30541	54024						135.7E	47773
295	301500	34.1N 135.0	LAND			45.44	70522					35 3N	138.7E	47639
296	3n1300	33.9N 135.0				3054)						26.24	127.BE	47937
297	301300	34.24 135.2	LAND		30	7074	•	FUF	Move	0345	KASATORI		. E. OL	41771
298	301300	34.1H 135.0	LAND		117	3272	11111	CAE		5375	14.2-1-UNI	34.6N	135.7E	47773
299 300	3n1300 3n1400	34.24 135.01 34.34 135.71	E LAND			31864	illill					34.6N	135.7E	47773
301	301400	34.4N 135.6					70424						138.7E	47639
302	301400	34.6N 135.5	LAND		20	,		EVE	MOVE	0445	KASATORI	. •		
303	301500	35.0N 136.2				30860	5////					34.6N	135.7E	47773
304	301500	35.0N 136.11	LAHD		45			EYE	MOVE	0445	KASATORI			
305	301500	34.9N 136.0	LAND			35///	70330					35,3N	139.7E	47639
306	301600	35.0N 136.6			75			EYE	MOVE	3635		37.4N	136.9€	47600
307	301500	35.4H 136.7					1 50532					34.6N	135.7E	47773
308	301700	35.8N 137.2				3496	50535						135.7EI	47773
309					75			FVF	MOVE	0455		37.4N	136.9E	47500
	301700	35.54 137.3	LAND		1.79									
310	301700	35.6N 137.2I	LAND			35///	70432					35,3N	135.78	47639
	3n1700 3n2300	35.5N 137.3I 35.6N 137.2I 39.1N 141.3I 40.5N 141.8I	E LAND	GOUD POUR	20	35///	70432	EYE	MOVE	0595 3110	AGAMAY AGAMAY	35,3N	139.78	47639

SYMDOTIC FIXES

FIX NO.	TTHE	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)	COMMENIS
1	190000	15.04 149.0E	10	200	
2	191200	13.54 147.5E	10	200	
3	200000	13.0N 146.0E	10	150	
4	201200	12.04 143.0E	10	200	
5	210000	11.5N 140.5E	15	200	
6	511500	11.0M 138.0E	15	150	
7	211800	12.9N 130.BE	15	150	
à	220000	12 0u 130-0F	20	150	

# TROPICAL STORM PAMELA

### CATELLITE FIXES

F1x	[TME (7)	FTX POSTTION	4CC8Y	3000 MASCYO	SATFLI ITE	COMMENTS	SITE	
1 4 5 6 7 8 9		14.5% 144.3E 14.0% 143.4F 10.0% 141.4F 10.0% 142.3E 20.5% 130.6E 21.0% 130.6E 21.0% 136.4E 23.2% 137.9F 24.3% 137.6E	PCN 3 PCN 6 PCN 6 PCN 6 PCN 3 PCN 3 PCN 3	T0.0/0.0 T2.0/2.0 /((2.0/24HRC T1.5/2.0 /W0.5/27HRC T1.0/1.0	DMSP37 DMSP35 DMSP37	INII JAS EXPUSEN (FCC	PGTW PGTW PGTW PGTW PGTW RPMK PGTW PGTW	
				Δ.	TRCHAFT F	xES		
		ETX FTX	FLT L <b>VL</b>			ET-LYL+4ND ACCRY	EYË FYE ORIEN- SHAPE DYAW/TATION	OUTY IAN DENSEL AU.
• 1 2 3 4 5	250827 252222 252258 260307 260504	14.6N 142.1E 20.5N 140.1E 20.5N 140.1E 21.2N 138.5E 21.9N 137.9E	700MB 1500F1 700MB 1500F1 1500F1	3151 1004 50 100 1004 25 050 3129 20 360 1003 25 060 1003 15 150	30 130 50 120 50 150	54 100 35 3 3 16 050 30 5 5 20 350 60 17 100 60 5 10 21 110 40 10 5		+16 + 7 1 +24 +22 +21 2 +11 + 7 2 +28 +25 + 8 30 3

# TROPICAL STORM ROGER

### CATELLITE FEXES

FIX	TIME	FTX						
NO.	(7)	DOS111(m)	ACCRY	DAUSAK	CODE	SATFILITE	COMMENTS	SITE
<b>-</b> 1	0>1233	13.5× 135.7E	PCN 5			DMSP39		PGTW
2	031513	18.1x 138.6E	PCN 5			DMSP36		PGTW
3	032036	20.84 134.9E	PCY 5			D45P37		PGTW
4	032313	20.5N 136.4E	PCN 5	T1.0/1.0	/50.0/24HR	DMSPAA		PGTW
Ś	040055	20.9N 335.7E	PCN 5			DMSP39		PGTW
6	040055	20.9N 135.6E	PCN 5	T1.5/1.5	3	DMSP39	INIT DOS	RPMK
7	040917	21.9N 135.2E	PCN 5			DMSP37		PGTW
용	041154	21.7N 133.4E	PCN 5			DMSP39		RODN
y	041155	21.5N 133.5E	PCN 5			DMSP36		PGTW
10	042157	20.9H 133.1E	PCN 6	T2+0/2-0	/D1.0/22HR9	DMSP37		PGTW
11	042158	20.3N 133.6E	PCN S	13.5/3.5		DMSP37	INI Jes	RODN
12	050036	20.0M 133.8E	PCN 6			DMCB34	· · ·	PGTW
13	050217	20.24 133.3E	PCN 6			DMSP39	EDGE OF DATA	PGTW
14	050217	20.0N 133.5E	PCN 5			DMSP39		RPMK
15	050217	20.3N 137.3E	PCN 5			DMSP39		RODN
16	051317	21.74 135.6E	PCN 3			DMSP39	EXPOSED   LCC	PGTW
17	051317	21.70 135.6E	PCN 3			DMSP39		RODN
18	051317	21.4N 135.7E	PCN 5			Duspag		RKSO
19	051319	21.9N 135.4E	PCN 5			DMSP36		RPMK
20	051319	21.8N 135.7E	PCN 3			DMSP36		PGTW
21	052137	23.4N 134.9E	PCN 5	T1.0/2.0	/W1.0/24HR4	DMSP37		PGTW
22	060019	23.9N 135.0E	PCN 5			DMSP36		PGTW
23	060158	24.4N 135.0E	PCN 5	13.0/3.0	)	DMSP39	INII Jės	RPMK
24	060158	24.1N 135.1E	PCN 5		•	DMSPRG		PGTW
Ž5	060158	24. PN 135.0E	PON 5	T3+0/3+0	1	DMSP39	INII Das	RKSD
26	061017	26.64 134.6E	PCV 5			DMSP37		RKSD
27	061018	26.9N 134.2E	PCN 5			DMSP37		RPMK
28	041016	25.0N 135.6E	PCN 5			DMSP37		PGTW
54	061257	27.3N 135.4E	PCN 5			DMSP39		RKSD
30	061301	27.1N 135.1E	PCN 5			DMSP34		PGTW
31	061301	26.9N 135.4E	PCN 5			DMSP36		RPMK
32	062117	29.0N 136.3E	PCN 6			DMSP37		PGTW
								10.2

# ATROMAFT FIXES

FIX NU.	TTME (7)	F1X P0S1T1UN	FLT L <b>V</b> L		DB5 MSLP									EYE SHAPE	-PSIRO SYS	TPP/96 VMI VENO	45N 40.
2 3 4 5	040308 040305 041820 042125	14.1N 140.2E 21.1N 135.7E 21.2N 135.1E 20.9M 133.5E 20.4N 133.7E 24.1N 134.5E	1500F  1500F  700MH 700MH	7007 3015	998 982 987 992	35 40	n80 n30 180	10 25	35 40 32 36	350 010 010 080	10 25 60 45	7 7 5	3 5 5			+25 +24 +24 28 +26 +23 +24 +26 +25 +26 26 +16 +11 +13 +14 + 6 +12 +12 +10	2 3 4 5 5

### SYMPOTTE FIXES

FIA NO.	TTME (7)	FTY POSTTION	INTENSITY ESTIMATE	VEAREST DATA (NM)	COMMENTS
• 1	010000	13.0v 141.1F	20	120	
a ž		13.1× 13#.0E	20	240	
Ē		12.04 142.0F	50	210	
•	060000	24.0N 134.5E	40	10	
5	061200	27.0N 135.5E	45	70	
6	070000	31.5N 137.0E	35	190	

### TYPHOON SARAH

### SATELL ITE FIXES

F1X	T M E   (7)	FIX POSITION	ACCRY	1140244 0005	G. 7-1. 1-21		
		O T T T T T	FC(,41	DAUSTK COUE	SATELL 176	E COMMENTS	SITE
* 5	012259 020131	16.24 121.0E	PCN 5		DMSP37	INIT J#S	RODN
+ 3	021139	17.5% 122.BE 16.4% 120.4E	Pon 5		Drashd	INII DOS	RPMK
* 4	021415	15.9N 120.0E	PCN 5		BMSP36		RPMK RPMK
<b>9</b> 5	021414	16.0v 120.1E 15.5v 121.7E	Pov 5	*0 a.a a .aa3	DMSP39		RODN
7	611vF0	14.5M 119.8E	PCN 5				RPMK
* b	030255	14.44 11A.9E	PCN 5		Duspay		RODN RPMK
* 10	031355 031355	14.24 120.4E	Pon 5		DHZP34		ROUN
* 11	032218	15.8N 119.2E 15.3N 119.0E	PON 5	T0.0/0.0 /S0.0/24HRs	DUSPRA DUSPRA		RPMK
12	040055	14.3N 110.1E	PCN 5				RPMK RODN
* 13 14	04U236 041058	15.1N 11R.8E	PCN 5		DESPRO		RPMK
15	041336	13.9% 119.0E	PC4 5		DMSP39		RODN
* 16	041337	15.0W 110.8E	PC4 5		DMSD3A		PGT₩ RPMK
18	042157 050036	13.5N 11A.3E 12.8N 119.1E	PCN 5		DMSP34		PGTW
19	050036	12.4N 119.1E	PCN 5		Duspak		PGTW
50	050217	12.5N 118.8E	PON 5	T2-0/2.0	DMCD34	INII Jds	PGT# PGT#
21	050217 050217	13.1N 11R.2E	PCN 5	11.5/1.5 /D1.5/28HRs			RPMK
23	051038	12.1N 119.2E	PCN 6	12.5/2.5 /00.5/25HR9	045P37		RODN
24	051317	12.3M 119.0E	PCN 6		DMSP39		PGT# PGT#
26 25	051317 051319	12.1N 114.7E	PCN 5		DMCD30		RODN
27	051319	12.3N 119.2E	PCN 5		DMSP36 DMSP36		PGTW
28	052319	12.3N 118.9E	PCN 5		DMSP37		RPMK RODN
29 30	052319 060016	12.3N 118.7E	Prn 5		DMSP37		RPMK
31	060158	12.4N 119.7E	PCN 5	TZ-0/2.0 /50.0/24HRs	DMSP36 PFSPMG		PGTW
32 33	060158	12.3N 110.5E	PON 5	T1.0/1.5 /WU.5/24HRC			PGTW RPMK
34	061018 061018	12.2N 110.3E	PCN 5		DMSP37		RPHK
35	061301	12.2N 119.1E	PCN 5		TEGPHO AFGPHO		PGTW
36 37	061301	12.4N 119.6E	PCN 5		DMSP36		RPMK PGTW
38	051439 051439	12.1N 149.4E	PCN 5 PCN 5		DMSP19		RODN
39	062259	12.2N 119.2E	PCN 3	T2.0/2.0 /D1.0/21HRs	DMSP34 DMSP36		RPNK
40 41	062259 070138	12.0N 120.0E	PON 5	T2.5/2.5	DMSP37	INII Des	RPMK Rodn
42	070139	12.2N 119.3E	PCN 3 PCN 3	12.5/2.5 /D0.5/24HRs	045P39 045P34		PGTM
43	070143	15°54 110°3£	PC4 5		Duspak		RODN RPMK
45	070240 071139	11.4M 118.1E 12.1M 119.3E	PCN 5		DMCP39		RPMK
46	071139	11.7M 119.2E	PCN 5		DMSP37 DMSP37		RPMK
47	071242	11.5N 11A.4E	PCN 5		DMSP36		RODN RPMK
48 49	071243 071420	11.9N 119.3E	PCN 5 PCN 5		DMSP36		PGTW
50	072238	11.2M 119.3E	PCN 5	T3.0/3.5+/D0.5/24HRs	DMSP39 DMSP37		RODN
51	072238	11.1N 119.2E	PC4 >	0, 3, 5, 7, 0, 0, 3, 24, 111, 1	DMSP37		RPMK RODN
52 53	0e0124 0e0301	11.2N 119.3E 11.2N 119.5E	PCN 5	T3 0 10 0 100 0 100 100 100 100 100 100 1	DMSP36		RPMK
54	0s1118	11.3N 119.0E	PCN 5	T3.0/3.0 /D0.5/28HRS	DMSP39 DMSP37	PSN CYTR OF COO	RODN
55 56	081118	10.9N 119.3E	PCN 5		DMSP37	NO EYE/PON BASED ON 2 CH RANDS	RPMK RODN
57	091406 091406	10.9N 119.2E 10.9N 119.3E	PCN 5 PCN 5		DMSP36	CI UP/QUTFLOW THEREASED	RPMK
58	8152B0	10.5N 11A.2E	PCN 5	F4+0/4+0 /01+5/21HRs	DHSP36 DHSP37	•	RODN PGT#
59 50	092218 090107	11.0N 11R.1E	PCN 5	T4.0/4.0 /01.0/24HRs	DMSP37		RPMK
ьì	040545	11.2N 11R.0E	PCN 1 PCN 3	T4.5/4.5 /01.5/22HRs	DMSP36 DMSP39		RODN
62	091058	11.6N 117.5E	PCN 1		DMSP37		RPMK RPMK
63 64	091059 091342	11.6N 117.4E 11.6N 117.1E	PCN 1 PCN 1		0MSP37		ROON
65	091342	11.5N 117.4E	PON I		044636 044636		PGTW
66 67		11.9N 117.3E	PCN 1		DMSP36		RODN RPMK
68	092158 1n0049	11.4N 116.5E 11.4N 116.2E	PCN I	T5+0/5+0 /D1+0/26HRS	DMSP37 DMSP36		RPMK
69	100049	11.3N 116.4E	PCN I	T5.0/5.0 /D1.0/26HRS	DMSP3K		RPMK
70 71		11.4M 116.4E	PCN 1	15.5/5.5 /D1.0/25HRS	DMSP39		PGTW RODN
		11.7N 116.1E 11.6N 116.0E	PCN 1 PCN 1		DMSP37		RPMK
73	101038	11.9N 116.1E	PCN I		DMSP39 DMSP37		RODN
		11.9N 115.9E	PCN I		DMSP36		PGTW RPMK
76		11.5N 115.9E 11.9N 116.0E	PCN 2		DHSP36 DHSP39	PSTIMATE CAPE OF THE	RODN
77	102319	12.1M 115.7E	PCN 3	15.0/5.0 /S0.0/22HRs	DMSP37	ESTIMATE CHTH OFF EDGE OF DATA	RPMK RPMK
		11.9N 115.6E 12.0N 115.5E	PCN 3	T4.5/5.5 /W1.0/21HRs	045937		RODN
ម១		12.0N 115.2E	PCN 3	T4.5/5.0 /W0.5/25HRs	DMSP36 DMSP39		RPMK
81	111018	12.34 114.8E	PCN 5		D45937		PGTW PGTW
		12.9N 115.ZE 12.4N 114.7E	PCN 6 PCN 3		DMSP37		RPHK
84	111445	12.4N 114.3E	PON 3		DMSP36 DMSP39		PGTW
85	111445	12.5N 114.3E	PCN 5		DMCD30		RPMK RODN
		12.2N 114.4E 13.0N 114.0E	PCN 3	T4.5/5.0 /W0.5/26HRS	DMSP37		RODN
88	120154	12.9N 114.3E	PCN 5	T3.5/4.5 /W1.0/26HRS	DMSP36		RPMK
89		13.0M 113.9E	PC4 5		DMCD34		RODN RPMK

90 91 93 94 95 96 97 98 99 100 103 105 107 108 109 111 111	121139 121426 121426 12238 120336 130307 131119 131119 131119 131119 131119 131119 131105 140248 140248 140248 14058 141359 142339 142339 142329 140229	13.3N 113.0E 13.4N 112.4E 13.4N 112.4E 13.0N 112.3E 13.2N 112.3E 13.2N 112.3E 13.3N 112.4E 13.3N 112.4E 13.6N 111.7E 13.6N 111.7E 13.6N 111.7E 13.6N 111.7E 13.5N 110.7E 13.3N 100.2E 13.3N 100.2E 13.3N 100.2E 13.1N 100.2E 13.3N 100.2E 13.3N 100.2E 13.3N 100.2E 13.3N 100.2E 13.3N 100.2E	3.4N 112.4E PCN 3 3.4N 112.4E PCN 5 3.4N 112.3E PCN 5 3.2N 112.3E PCN 5 3.2N 112.4E PCN 5 3.2N 112.4E PCN 5 3.2N 112.4E PCN 1 3.6N 111.4E PCN 1 3.6N 111.7E PCN 3 3.7N 111.1E PCN 3 3.8N 12.4N PCN 3 3.8N 10.4N PCN 3 3.N							RPMK RODN RPMK RODN RPMK RODN RPMK RODN RPMK RODN RODN RODN RODN RODN RODN RODN RODN		
					2146	CMAP; FIXES						
FIX NO.	TIME (7)	FIX POSITION							EYE Shape	EYE ORIEN DIAW/TATIO	ONAL IAN DE	(C) 45N PVSST NO.
1 2 3 4 5 6 7 8 9 10 11 12 13	051001 060342 070203 070431 080210 080512 090405 160142 160143 160343 120700 120923	12.6N 119.3E 12.4N 119.7E 12.2N 119.4E 12.2N 119.3E 11.3N 119.2E 11.3N 117.9E 11.3N 117.9E 11.5N 116.5E 11.7N 116.5E 12.0N 115.4E 12.0N 115.4E 12.0N 115.4E 12.0N 113.4E	700MB 301 700MB 305 700MB 397 700MB 397 700MB 397 700MB 377 700MB 387 700MB 387 700MB 377 700MB 377 700MB 377 700MB 377	996 10 985 20 982 22 980 21 960 26 929 37 959	45 360 50 40 010 50 50 030 11 75 330 10 75 300 20 45 080 70 50 060 5 50 070 60 65 130 20 65 080 20 45 180 36	1 130 32 010 1 140 50 360 1 340 73 270 1 170 78 360 5 370 40 220 5 100 101 040 5 150 93 060 7 070 115 020 0 120 73 060 5 140 74 320 5 240 70 140	30 30 15 10 30 10 10 15 15 20	4454545212254	CIRCILAR CIRCILAR CIRCILAR CIRCILAR CIRCILAR CIRCILAR CIRCILAR CIRCILAR CIRCILAR CIRCILAR	20 20 10 8 20 15	+14 +17 + 5 +13 +13 + 3 +15 +15 +16 +16 + 5 +11 +12 + 6 +13 +14 + 9 +11 +19 + 6 +25 +14 +11 +25 + 4 +14 +15 +11	3 4 4 5 5 5 6 6 7 7 8 8 8 9
FIX NO.	T1ME: (7)	FTX POSTTION	RADAR ACCRY	EYE SHAPE	EYF DI AM	RADOB-CODE ASWAR TODEF		c	OMMENTS		RADAR Position	SITE
1 2 3 4 5	041208 041300 041308 041800 060000	14.1N 119.7E 13.8N 119.8E 14.0N 119.5E 13.4N 119.2E 13.6N 119.0E	LÂND LÂND LÂND LÂND LÂND	CIRCUL	Áq:						16.3M 120.6E 16.3M 120.6E 16.3M 120.6E 16.3M 120.6E 13.7M 100.6E	98321 98321 98321 98321 48455
					SYNOPI	ITC FIXES						
FIX NO.	TTME (7)	FTX POSTTIUN	INTENSITY ESTIMATE	NEAREST DATA (NM)		COMMENTS						
1 2 3 4	011200 020000 030000 041200	14.5N 120.5E 15.0N 121.0E 15.0N 121.0E 14.0N 119.8E	10 10 10 15	60 90 60 90								

#### SUPER TYPHOON TIP

#### SATELL ITF FIRES

X 1 1	T T M E (7)	F1X P0511100	ACCBY	Dua- u - cor			
				DAUSAR CODE	SATELLITE	CO-HIFNTS	SITE
5	041154				りたほうその		PGTW
3	042015				0M9477	INII DOS	PGTW
4	050957				AFGPMG		PGTW
5	051137			•	DMSP37		PGTW
6	051955				DMSP37		PGTW
ž	052237			_	DMSP37		PGTW
	050016						PGTW
9	060836		PCN 6		Dwcban		PGTW
lú	041116		PCN 6		Dwsb37 Dwsb34		PGT#
11	061119						KGWC
12	062219				DMSP36	LOW CONFIDENCE	-PG <u>T</u> ₩
13	070916	6.9N 152.1E	PCN 6		045P37	COM COMPADENCE	PGTW
] 4	071101	7.3∾ 152.4€	PCN 5		Duspak		PGTW
15	072338		PCN 5	T3.0/3.0 /01.0/24HRs			PGTW
16	072343	7.4M 152.1E	PCN 5		DMSP36		PGTW PGTW
17	040755	9.14 151.28	PCN 6		DMSP37		PGTW
ls	0A1043	9.4M 151.0F	PCN 4		DMSP36		PGTW
19	092037		PCN 3		DMSP37		PGTW
20	092325	11.7N 14R.3E	PCN 3	13.5/3.5 /00.5/24HRS	PERSHU		PGTW
21	000101	11.9N 14R.LE	PCN 3		DMCDAG		PGTW
22	002016		PCN 4	_	DMSP37		PGTW
23	100042		PCN 3	T5.0/5.0	DMSP34	Spc Jini	RODN
24 25	100042		PCN 3	14.5/4.5	DMCD30	INI) Jas	RPMK
26	100042		PCN 3	T4.5/4.5 /N1.0/25HRs	Duspag		PGTW
* 21	100857	13.7N ]41.4E	PCN 6		DMSP37		PGTW
29	100957	14.24 141.68	PCN 6		DMSP77		RODN
27	]nl]+;	13.9N 141.1E	PCN 2		DMSPRA		PGTW
30	1,1149	13.9N 141.3E	PCN 2		DHSP36		RPMK
31	101149	13.1h 141.0E 14.14 130.7E	PCA S	<b>74</b> *	DMSP36		RODN
32	111016	14.9N 130.6E	PCN 1	76+0/6+0 /D]+5/24HR<	DMSP36		RPMK
33	111018	14.8v 139.3E	Pon 1 Pon 1		DMSD36		PGTW
34	111131	15.0N   13R.1E	Priv 4		DMSP37		RODN
35	111304	14.9N 139.2E	PCN 1		DMCD34		PGTW
36	112117	15.14 138.6E	PCN 1	17.5/7.5		TAITY Odo	RPMK
37	112117	15.1% 13A.5E	PCN I	17.0/7.0	DMSP37 DMSP37	INII OOS	RODN
38	120012	15.2N 130.2E	PCN I	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	DMSP36	1411 305	PGTW
39	120144	16.4W 13R.3E	PCN 1	T7.0/7.0 /D1.0/25HRS	DMSB34		PGTW
40	120145	16.5M 13R.0E	PON L		DMZB30		RPMK
41	120957	14.9N 137.3E	PCN I		DMSP37		PGTW
42	121254	17.0N 137.2E	PCN 1		DMSP36		PGTW
43	121254	16.8N 137.2E	PCN 1		DMSP36		PGTW
44	122057	16.9N 136.3E	PCN 1		DMSP37		RODN PGTW
45	122354	16.5N 136.1E	PCN 1	T0.5/7.0 /W0.5/27HRc	DMSP36		PGTW
46	130156	16.5N 136.0E	PCN 1		DMSP74		PGTW
47	130159	16.5v 136.1E	PCN 1	T7.0/7.5 /W0.5/28HRC	DMSP39		RODN
48	130937	14.54 135.4E	PCN 1		DMSP37		PGTW
49	131550	15.7N 135.4F	PCN 1		DMSP39		RODN
50	131536	16.7N 135.4E	PCN 3		DMSP36		PGTW
51	132036	16.9N 134.6E	PCN 5		DMSP37		PGTW
52	132336	16.9N 137.9E	PCN 1	T5+0/6+0 /W1+5/24HR<	DMSP36		PGTW
53	140106	17.1M 133.7E	PCN 1		Duspay		PGTW
54	140107	38.FEE MG.71	PCN 1	T6.0/7.0 /W1.0/24HRS	DMSP34		RODN
55	140917	17.1N 132.5E	PCN 1		DMSP37		PGTW
56 57	141206	17.3N 132.2E	PCN 1		DMSP39		PGTW
58	141206	17.1N 132.2E	PCN 1		PFGPMO		RODN
	141348	17.44 132.1E 17.94 131.2E	PCN I	#5 A /F A /GA = -3=	0MSP39		PGTW
	150047	18.1N 130.6E	PCN 1	T5.0/5.0 /S0.0/22HRs	DMSP37		PGTW
	150048	18-14 130-7E	PON 1	75.E46 0 400 503005	DMSP79		PGTW
	150059	18.0N 130.7E	PCN 2	T5.5/6.0 /W0.5/24HRS	DMSP39		RODN
	150229	18.2N 130.6E	PCN 1		DMSP36		PGTW
	151038	18.2N 129.5E	PCN D		DMSP39 DMSP37		RODN
	151200	13.44 129.3E	PCN 5		DMSP36		PGTW
	151329	14.5N 129.2E	PCN 5		DMCD30		PGTW
	151329	14.5v 129.2E	PCN 5		045939		PGTW
	152137	19.3N 129.2E	PCN 1	T5.0/5.0 /S0.0/24HRs	DMSP37		RODN
	160041	19.44 129.1E	PCN 3		DMSP36		PGTW
	160209	19.34 129.2E	PCN 3		DMSPRG		PGTW
	140510	19.4N 120.1E	PCN 3	T5+0/5+5-/W0+5/25HRS	DMSP39		PGTW
	161018	20.2N 12R.7E	PCN 3		DMSP37		RODN
	161324	20.3N 12R.6E	PCN 3		DMSP36		PGTW PGTW
	162117	20.9N 12R.2E	PCN 3		DMSP37		PGTW
	170024	31.8M 128.1E	PCN 3	T5+0/5+0-/S0+0/27HRS	DHSP36		PGTW PGTW
	170151	21.4N 12R.DE	PCN 3	. =	DHSP39		PGTW
	170151	21.6N 128.0E	PC4 3	T5.0/5.0	DHSP39	INIT Des	RPMK
	170151	21.5N 127.9E	PCN 1	T5.0/5.0 /50.0/24HRS	DMSP39		RODN
	170957	22.7N 127.8E	PCN 3		DMSP37		PGTW
	171251	23.0N 127.8E	PCN 3		DMSP39		RODN
	171306	22.94 127.8E	PCN 3		DMSP36		PGTW
	172056	24.1N 128.0E	PCN 3		DMSP37		PGTW
	172057	24.44 127.7E	PCN 6		DMSP37		RODN
	10006	25.0N 12R.3E	PCN 3	T4.5/5.0 /W0.5/24HR9	DMSP36		PGTW
	180131	52.5N 158.5E	PCN 3	T4.5/5.0 /W0.5/24HR4	DMSP39		RPMK
	140132	25.2N 12R.0E	PCN 3		DMSPRG		PGTW
	140132	25.4v 12R.0E	PCN 3	T3.5/4.5 /W1.5/24HRS	DMSP39		RODN
	190937	27.2N 129.4E	PCN 3		DHSP37		PGTW
	190937	27.5N 120.4E	PCN 4		DMSP37		RODN
90	141118	28.5" 159.6E	PCN 3		DMSP37		RODN

91 92 93 94 95 96 97 98	181231 181248 182036 182348 190112 190112 19112 191212 191212 192016	28.6N 130.5E 28.7N 130.5E 30.6N 131.8E 32.7N 134.8E 33.4N 134.6E 33.3N 135.2E 41.1N 145.6E 41.1N 145.6E 41.1N 145.6E 41.7N 146.4E	PCN 3 PCN 3 PCN 3 PCN 3 PCN 3 PCN 5 PCN 5 PCN 5	13.0/ 14.0/	4+0 /½ 4+0	1.5/6	24HR<	D*	45P39 45P36 45P37 45P36 45P39 45P39 45P39	EXPSD EXPSD	LLCC	:			; ; ; ; ;	PMK PGTH PGTH PGTH RKSO PGTH RODY RKSO RKSO			
							A	1 20	PAFT I	IXES									
FIX NO.	TTME (7)	FTX POSTTION	FLT 1.VL		085 MSLP					-FLT-LVL /VEL/BRG				EYE Shape		RIEN-	PYF TEM		
	040614 050030 050800 050800 051943 052222 0607713 070307 071858 0	6.2N 153.0E 5.4N 156.3E 5.9N 156.3E 5.7N 156.4E 7.1N 157.4E 7.1N 157.4E 7.5N 157.5E 7.4N 157.5E 7.9N 157.5E 7.9N 157.5E 6.9N 157.2E 10.3N 150.1E 10.8N 144.6E 12.7N 147.5E 12.9N 137.3E 12.9N 137.5E 16.7N 137.5E	1500FI 700MB 1500FI 700MB		1004 1003 1003 1003 1000 998 1005 997 995 991 985 981 974 959 949 900 870 884 903 905 922 919 924 931 935 939	25 25 35 30 40 35 30 30 30 50 50 50 50 50 50 50 50 50 50 50 50 50	310 300 180 230 050 320 150 330 080 070 360 050 090 310 130 240 030 240	20 10 10 10 45 48 10 10 57 6 25 55 135 7 7 130 15	240 180 210 210 250 060 070 080 140 270 110 270 140 140 140 140 140 140 270 270	78 360 106 10 125 050 120 160 125 180 125 180 110 103 110 110 110 110 130 110 130 115 270 116 130 105 130 105 130 110 104 86 340 110 110 87 360 87 180 67 18 67 18 67 18 67 18 67 18 67 18 67 18 68 190 87 180 69 200 72 210 89 900 60 010	15500000000000000000000000000000000000	??R45?4545055485555???????!!??44444645??444??\$45555444455844	252235345554533333	CIRCIILAR	40 55 15 10 12	130 100 150	+1n +11 +  +2i +15 +  +12 +15 +  +13 +15 +  +14 +10 +  +14 +10 +  +14 +10 +  +14 +10 +  +14 +10 +  +15 +15 +  +16 +15 +  +17 +13 +18 +  +18 +17 +  +18 +18 +  +19 +17 +  +19 +19 +  +17 +19	23778 1080 110 2 101123 4 1515 4 16 16 16 16 16 16 16 16 16 16 16 16 16	1 2 3 3 3 4 4 4 5 6 7 7 7 7 7 8 8 8 8 9 9 9 9 10 11 11 12 13 3 13 14 14 15 15 15 15 15 15 15 15 15 15 15 15 15
		<u> </u>							P F [X								HADAD		e115
	TTME (7)	FTX POSTTTON	RADAR A	CCRY	SHAP		DIA			H-CODE R TDDFF			•	COMMENTS.			HADAR Posttion		GITF
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	090410 090435 090500 090510 090635 090735 090735 090835 090910 090935 090910	12.40 146.5E 12.80 146.3E 12.90 146.8E 12.90 146.8E 12.90 146.8E 12.90 146.8E 12.90 146.6E 12.90 146.5E 12.90 146.5E 12.70 146.2E 12.90 146.1E 12.40 146.0E 12.50 144.8E 12.70 144.8E	LAND LAND LAND LAND LAND LAND LAND LAND	FAIR FAIR GNUD GNUD GNUD GNUD GNUD GNUD GNUD GNUD	CIRCU CIRCU CIRCU CIRCU CIRCU CIRCU CIRCU CIRCU CIRCU CIRCU CIRCU	ILAR ILAR ILAR ILAR ILAR ILAR ILAR	2 1 1 1 2 2 2	0005555000056			wat	_L ೧۱	PEN :	SE-S#-N#-N			13.6N 144.1 13.6N 145.1 13.6N 145.1 13.6N 145.1 13.6N 145.1 13.6N 144.1	96 96 97 97 97 97 97 97 97 97 97 97	91218 91218 91218 91218 91218 91218 91218 91218 91218 91218 91218 91218 91218

10	091110	12.74	144.7E	LAND	ციმს	CTRCHLAR	15									
1	001135	12.30	144.5E	CPAJ	GOUD	CIRCHLAR	15							13.6N		91218 91218
1.			144.5E		600D	CTRCHLAR	15 15							13.6N	144.9E	91218
20		12.84	144.35	LAND	FAIR	CTRCHLAR	15							13.6№ :	144.9E	91518 91518
23	2 001410		144.2E		6 <b>20</b> 0	CIRCULAR CIRCULAR	15 15							13.6N		91?18 91218
5.		12.84	147.ME	LAND	6100 6100	CIRCULAR	15							13,6N	144.9E	91518
2:	091535	12.70	143.HE	CMAJ	6200	CIRCULAR	15 15							13.6N 1		91218 91218
. 51			147.6E		<b>ცი</b> 0ს	CIRCULAR	1 N 1 N							13.60	144.9E	41218
21	8 001710	12.74	143.6E	LAND	იე0D	CIRCHLAR	10							13.6N 1		91218
2: 3:		12.94	143.5E 143.5E	LAND	გი <b>ს</b> ს	CTRCHLAR	10							13.6N 1	144.98	91218
3. 3.		12.94	147.3E	LA-JO	650D	CIRCULAR	7							13.6N 1	144.9E	01518 01518
3:	001935	12.AN	143.3E	[ AND	GnOU	CIRCULAR	10			HVY	ATTE	NALIAN		13.6N 1 13.6N 1		91218 91518
31 3:		12.34i	143.1E 127.8E	しんいり	FAIR Grod	CIRCULAR	10 45			FuE	Mana	3410		13.6N 1	144.9E	91218
30	171400	27.74	127.7E	LAND	ผาบบ		4.5			EYE	MOVE	3210		24.8N	25.3E	47927 47927
3; 3t		23.74	127.7E	LAND LAND	<b>ცი</b> 00 ცი <b>0</b> D		45 45					3420 3420		24.8N	25.3E	47927
39		23.44	127.6E	LAND	GNUD		45	*****	53416			3420		24.8N	125.3E	47927 47927
41	171900		127.6E		POOR			1///3	53/16	E۷E	MOVE	3205		26.2N	27.8E	47937 47927
4,			127.5E 127.8E		PODR			41113	70311			3615		26,3N 1	25.BE	47929
4	172000	24.24	127.6E	LAND	POOR					EYE	MOVE	0115		26,2N 1	127.BE	47937 47929
4!			127.7E 127.5E		FAIR			6///3	70211					26.2N 1 26.4N 1	27.8E	47937
4		24.34	127.5E	LAND	PhOH				~^11"	EYE	Mone	3415		26.3N 1	25.8E	47931 47929
41	172200	24.5%	127.4E	LAND	<b>G</b> n00				70110	EYE	Move	3520		26.2N 1	27.8E	47937 47929
5:			127.8E		POUR			6///3	73608					26.2M	27.8E!	47937
5.	006511	24.92	127.9F	I AND				5///1	70209					26.4N 1	27.8E	47991 4 <u>799</u> 7
5. 54			127.7E	LAND	PoDR Podr					FvE	Move	3520		26.4N 1 24.8N 1	21.8E	47931 47927
5: 5:		24.9N	127.BE	LAND	PODR GOUU		4.0					0220		26.4N T	27.8EI	47931
5	140000	25.1N	127.9E	LAND			40	3//19	70111	645	MOVE	0220		26.2N	25.8E	47929 47937
56 56			127.8E	LAND LAND	POOR POOR									26.4N Î 26.4N Î	27.8E	47931
60	190100	25.24	128.0E	LAND				3//15	70308					26.2N j	27.8E:	47931 47937
68	180135		12A.1E 127.9E	LAND LAND	GnOD PnOR		4.0			EAF	MOVE	0420		26,3N 1	26.8E	47929 47931
6.			12A.0E	LAND LAND	<b>ცე</b> 00		45	3//12	70111	FME	Maya	3430		26,2N i	27.8E	47937
65	140510	25.9N	158.0E	LAND	PoOR		4.7			£7L	1911919	3430		26.3M 1 26.4N 1	27.BE	47929 47931
66			124.1E	LAND LAND	POUR			3//42	70514					26.4N 1 26.2N 1	27.8E	47931 47937
66 * 69			12A.3E	LAND	GOOD POOR		55			EYE	MOVE	0320		26.3N i	25.8E	47929
70	180335	26.1N	128.5E	LAND	POOR									26.4N 1 26.4N 1	27.8EI	47931 47931
71 72			34.4E	LAND					70218 5////					26.2N i 28.4N 1		47997 47909
73 74	190600	24.0N	128.4E	LAND	GnDD PnDR		55	.,	3	EYE	MOVE	0335		26.3N 1	26.8E	47999
75	190435	26.4N	128.7E	LAND	PnOR									26,4N 1	27.8E	47931 47931
76 77			128+4E	L AND	6n0D 6n0D					EVE	MOVE	NNE		26.2N 1	27.7E	47930
78	140500	26.4N	128.4E	LAND	5.745				50327	E * L	HITT	MAL		26.2N 1	27.5E	47930 47909
79 80			128.5E	LAND	GOOD		60	3///4	70222	EVE	Move	0235		26.2N 1	27.8E	47937 47929
81 82		26.7N	128.6E	LAND	POÜR Poür									26.4N î	27.8E	47931
83	140545	24.6N	128.6E	LAND	PoOR									26.4N 1 26.2N T		47931 47930
84 85		26.6N	124.6E	LAND LAND	POOR Fair		55				MOVE			26.2N	27.7EI	47930
86	180600	26.6N	128•7E	LAND			7.5	6///4		E7E	MOVE	0330		26.2N 1	27.8E	47999 47937
87 88	190610	26.4N 26.9N	12A.7E	LAND LAND	POOR			45///	50509					28.4N 1 26.4N 1	29.5E	47909 47931
89 90		27.0N 24.9N		LÁND LÁND	POOR			6///2	70320	FUE	Mayo	0230		26.2M 1	27.8E	47937
91	180700	24.8N	12A.9E	LAND				65///	50430					26.3H 1 28.4H 1:	24.5E	47929 47 <del>9</del> 09
92 93		27.1N 27.1N		LAND	POOR			6///3		E¥€	MAVA	0435		26.3N 1	26.8E	47929 47937
94 95	190800	27.2N	30.0E	LAND	0000			65///						28.4N 1	29.58	47909
96	190900	27.5N 27.2N	120.5E	LAND	POOR			11113		EYE	MOVA	U445		27.44 11 26.2N 11	27.BE	47942 47937
97 98		27.5N 27.7N	129.3E 129.5E	LAND LAND				65///	50519					28.4N 1	29:5E	47909 47909
99	191000	27.7N	120.4E	LAND	PnOR			,,,,,	50010		MOVG			27.4N 1	2B.7E	47942
100 101	181100	27.8N 28.0N	129.8E 129.7E	LAND LAND	PnDR			65///	50324	EYE	MOVG	U640		27.4N 1	28.7EI 29.5EI	47942 47989
105	191200 191300	28.3N	129.8E 13n.0E	LAND				55///	50316					28.4N 1	29.5E	47909
104	181400	28. AN	13n•4E	LAND				55///	50527					28.4N 1	29.5E	<del>47909</del> 479 <b>09</b>
106	1a1500 1a1500	29.2N	130.9€	LAND LAND				6///2						30.6N 1	31.0E	47869 47909
107	191600	29.4N	131.3E	LAND				6///1	50627					30,6N 1	31.0E	47969
	182330	35°5N 50°6N	134.2E	LAND LAND	PoOR			6///1	20255				KUSHIMOTO	30,6N 1	31.0E	47869

#### SUPER TYPHOON VERA

#### SATELL TIF FIXES

FIX NO.	T1M5: (7)	FTX POSTTION	4CCRY	BYDRAK CODE	SATFILITE	CJ4MFNTS	5		SITE		
1	372316	6.2N 149.DE	PCN 5	T1.0/1.0	DMSP36	INII Ods			PGÍW		
2	010026	6.2N 14R.9E	PcN 5		Dadbdo				PGTW		
3	010814 011126	6.0H 14R.3E 6.3H 147.9E	PCN 5		045077 045079	CI UP			PGTW PGTW		
5	011158	6.3N 147.2E	PCN 5		045036				PGTW		
6	012055	6.94 146.7E	PCN 5		DUSPRI				PGTW		
7	012258	6.9N 146.0E	PCN 5	12.0/2.0 /D1.0/24HR	c Dušpak				PGTW		
8	020007	6.6N 145.7E	PCN 5		DNSP34				PGTW		
10	0>0935	7.2N 143.9E	PCN 5		045P37				PGT#		
11	021140 021248	7.2N 143.6E 7.1N 143.4E	PCN 5		DMSP39				PGTW		
12	0>12+B	6.9N 143.2E	PCN 6		DMSP34				RPMK		
13	0>2034	7.54 141.5E	PCN 3		DMSP37				PGTW		
14	030021	9.3N 141.0E	PCN 3	T3.5/3.5	7545mG 7545mG	INII 092			RODN PGT#		
15 16	030021 030129	7.9N 141.1E 8.2N 140.7E	PCN 3 PCN 3	T3.0/3.0 /01.0/25HR	045644 045644				PGTW		
17	030914	9.0N 137.8E	PCN 6		DMSP17				PGTM		
18	8551F0	9.2N 137.1E	PCN 6		045939				PGTW		
19	622120	9.4N 137.2E	PCM 5		DMSP39				RODN		
20	031302	9.2N 136.9E	PC4 6		D45936 D45937				PGTW PGTW		
55 51	032155 040003	10.5% 133.8E	PCN 1 PCN 1	T5+0/5+0+/02+0/24HR					PGTW		
23	040110	10.5% 132.7E	PCN I	124(1/3404/11241)/141111	DHSP39				PGIW		
24	040110	10.54 132.6E	PCN L	r5.n/5.0	DMSP39	SAC LINI			RPHK		
25	041035	11.44 129.7E	₽ÇN S		DMSP37				PGTW		
26 27	041244	30.051 NP-11	PĆN 1		045P36				PGTW RODN		
28	041245 041351	11.7N 12A.8E	PCN 2		045P39				PGTW		
29	042135	12.4H 126.6E	PCN 1	15.5/6.5 /D0.5/22HR					PGTW		
30	042135	12.50 124.5E	PCN 1		DMSP37				RPMK		
31	050126	12.9N 125.9E	PCN 1	T6.0/6.0-/D1.0/24HR	AFGSMU S	26G TINI			RPMK RODN		
32	050232	13.1N 125.9E	PCN 1	10.5/6.5	DMZD3A	INTI 002			RPHK		
33 34	050232 051015	13.1N 125.8E	PCN 3		DMSP37				PGT₩	,	
35	05 226	14.4N 123.9E	PCN 1		DMSP36				PGTW		
36	05) 332	14.6N 123.6E	PCN 1		DMSP39				ROOM		
37-	051332	14.54 123.7E	PCN 1		Dwabae				PGTW		
38 39	051408	14.54 124.1E	PCN 1		DMSP36 DMSP39				RPMK ROON		
40	052256 060108	15.4N 122.9E	PCN 3	T4.5/5.5 /W1.0/27HR					PGTW		
41.	060109	15.64 122.9E	PCN 3	T5.5/6.5-/W1.0/23HR	c Dwcb34				RODN		
42	060213	15.7M 122.3E	PCN 1		DMSP39				RODN		
43	040213	15.8N 122.5E	PCN 1	T6.0/6.0-/S0.0/24HR	C DMSP39				RPMK PGTW		
45	060954 061312	16.7N 122.2E	PCN 3 PCN 5		DMSP39				PGTW		
46	061350	17.2N 122.3E	PCN 5		DMSP36				RPMK		
47	061351	17.2N 122.3E	PCN 3		DHSP36				RODN		
48	045536	18.3N 121.5E	PCN 3		DMSP37 DMSP36				RODN PGTW		
49 50	070050 070153	18.5N 121.7E	PCN 5 PCN 5	T4.0/5.0 /WZ.0/Z4HR					RPMK		
51	070154	14.64 121.7E	PCN 5	T3.0/4.0 /W1.5/25HR					PSTM		
52	071116	18.7H 127.1E	PCN 1		DMSP37				RPMK		
53	071332	16.8N 117.8E	PCN 5		DMSP36	ADDUT LD			PGTW		
54	080032	16.1N 114.5E	PCN 5		DMSP36	APRNT LLCC			PGTW		
					ATRCRAFT F	XES					
FIX	TIME	FTX	FLT	70043 OBS MAX-SEC		LT-LVL-4ND			YE DRIEN-	EYR TEMPL (C)	MSN
NO.	(7)	POSITION	LVL	HGT MSLP VEL/ARG	PAR DIE	/EL/BHG/HNG N	AV/MET	SHAPE DI	MOITATION	TPPV9G VMJ VŤUO	ND.
1	020525	7.4% 144.5E	1500FT	994 50 130	7 160	65 060 20	5 2			-21 +2+ +22	2
Š	030500	8.6N 139.3E	700MH	297 <sub>1</sub> 70 090	5 350	46 240 30	5 2	0100		+1+ +10	*
3	030753	8.84 13A.4E	700HB	2946 982		73 020 A	5 5	CIRCULAR 17		+11 +15 + 8	5
5	031933 032049	10.10 134.7E	700MB 700MB	272n 2643 945 130 270		120 080 13 125 270 10	5 5	CIRCULAR 20 CIRCULAR 8		+14 +11 +1m +19 + B	5
6	040507	10.2M 134.3E	700MB	2399 130 110		170 110 5	6 1	CIRCULAR F		+12 +25 +13	6
ž	041300	12.24 127.46	700Mb	2349 915	124	1 <del>00 000</del> 10	4 2	GIRCHLAR		+19 +14	7
8	042125	12.5N 126.5E	700MH	2372 919 120 330		111 180 15	4 2	CONCENTRIC SE	70	+14 +18 +14	7 8
9	050418	13.24 125.1E	700MH 700MH	2413 130 050 2410 130 340	7 (20 ) 4 340 )	116 050 12 100 2/0 1n	Я 5 4 2	CIRCULAR 7		+16 +12 +10 +15 +15	8
10 11	050702 052017	13.6N 124.8E	700MB 700MB	2557 130 340	7 .759	103 110 30	4 2	CIRCULAR 10		+15' +15	ÿ
12	052232	15.1N 122.7E	700MH	2587 941 55 060	40 1A0	85 070 25	5 1	CIRCULAR 30		+15 +15 +15	9
13	060620	16.3N 127.3E	700MB	2647 100 450	35		10	CIRCULAR			10
14	100540	17.84 121.6E	700MB		130	52 020 6n	5			+15 + 4	11

#### RAJAD FIXES

Flx NU.	[1#E (7)	#1X WU]	RADAR	#CC4Y	EYE SHAPE	EYF Diam	AGMAK Reugh		COMMENTS	HADAR Postiton	SITE
1	0,0716	11.2m 130.7E	∆CF T								54445
2	050500	13.2N 124.6E	LAND				204/1			10.3N 124.08	98546
3	050505 050500	13.5% 125.5E 13.7% 125.3E	(AND				11755			14.1N 123.08	
5	050500	13.5v 125.0E	LAND				70111			14.1M 123.0E	
6	050500	15.5M 122.7E	LAZID				10543			14.0% 124.3E 14.1% 123.0E	
7	050530	13.7N 124.7E	CAND				206//			14.UN 124.3E	
5	050700	17.8N 124.5E	LAND				257/0			10.3M 124.0E	
9	050700	13.8N 125.1E	LAND				2021]			14.1N 123.0E	
10	050800 050800	13.84.124.9E	[AND				20211			14,1M 123.08	
15	050900	14.0v 124.5E	(AVD				2065/ 2061/			14.0N 124.3E	
13	050700	17.9v 124.6E	LAND				20211			14.0N 124.3E 14.1N 123.0E	
14	0 < 0 9 0 0	13.9N 124.6E	(A+ID				20211	52921		14.UN 124.3E	98447
15	051000	14.1N 124.5E	(L6AJ				202//			14.0N 124.3E	
16	051100	13.54 125.5E	LAND				301//	11111		14.1m 123.0E	
17 18	951300 951400	14.3N 124.0E	LA-ID LA-ID				20231 20211			30.ESt w1.41	
19	051500	14.7N 123.7E	LAND				10332			14.1% 123.0E	
20	051300	15.14 123.3E	AND				10412			14.1N 123.0E	
21	051540	14.9v 123.6E	LAND	POOR			•			15.2N 120.6E	
5.5	051 <del>9</del> 00	15.0N 127.6E	LAND	POUR						15.2N 120.6E	
23		15.0N 123.5E	LAND	PA0R						15.24 120.6E	98327
24 25	052005 052035	15.1N 123.2E	LAND LAND	POUR POUR						15.2N 120.6E	
26	052110	15.2N 123.1E	LAND	POUR						15.2N 120.6E	
27	052135	15.2v 123.0E	LAND	POOR						15.24 120.6E	
28	615520	15.34 177.9E	LAND	POUR						15.2N 120.6E	
29	052235	15.3N 122.9E	LAND	PYÜK						15.2N 120.6E	
* 30 * 31	052300	15.2m 123.4E	LAND				1////			16.3N 120.6E	
35	052300 052300	15.4N 122.HE	LAND	POUR			18543	53204		14.1N 123.0E	
33	040000	15.64 123.UE	LAND	P-10K			1022/	5////		15.2N 120.6E 16.3N 120.6E	
34	060100	15.1N 122.6E	LAND				10543			14.1N 123.0E	
35	060100	15.7N 127.9E	LAND				202//	5////		16.3N 120.6E	98321
36	060500	15.9N 127.5E	LAHO				10543			14.1M 123.0E	98440
37 38	060500	15.9N 122.9E	LAND				1021/			16.3N 120.6E	98321
39	060300 060300	15.3N 127.4E	LAND				10543			14.1N 123.0E	98440
40	060400	14.5M 155.3E	LAND				10543			16.3M 120.6E 16.3M 120.6E	98321
41	060400	16.24 122.3E	LAND				10543			14.1N 123.0E	
42	060430	16.34 122.85	LAND				1083/			16.3N 120.6E	
4.3	040500	16.3N 122.2E	LAND				10543			14.1N 123.0E	
44 45	060500 060500	16.5N 127.0E	LAND LAND				1074/	43408		16.3N 120.6E	
46	060700	16.54 122.5E	LAND				1083/			14.1N 123.0E	
47	040930	16.5N 122.3E	LAND				21253			16.3N 120.6E	
+8	001200	16.7N 127.1E	LAND				15000			16.3N 120.6E	
49	061500	17.3N 122.1E	LAND				45///			16.3M 120.6E	98321
50	061500	17.4N 122.0E	LAND				45///			16.3W 120.6E	
51 52	061900 061900	17.4N 121.9E	LÁND LÁND				45///			16.3N 120.6E	
53	070100	16.74 127.4E 17.94 121.1E	LAND				1021/			16.3N 120.6E	
54	070200	18.0N 120.7E	LAND				20351			16.3M 120.6E 16.3M 120.6E	98321
55	070300	39.021 MI.PI	LAND				20341	52913		16.3N 120.6E	
56	070300	18.1N 120.8E	LAND				45///	11111		16,3M 120.6E	98321
57	070500	18.2N 120.4E	LAND				45///			16.3N 120.6E	98321
58 59	070500	18.3v 120.1E	GMAJ				53///			16,3N 120.6E	
60	070700	18.4N 120.2E	LAND				35242			16.3N 120.6E	
	.,.,.,	*4 1-4 11 441E	Child				-11777	124//		16.3M 120.6E	98371
						SYMOPT	TC FIXE	:5			
FIX	TruF	F**	TMTEN	STTU 1154	nceT.						

FIX NO.	TTME (7)	POSITION	INTENSITY ESTIMATE	MEAREST DATA (NM)	COMMENIS
1	290000	6.0N 158.5E	n5	60	
2	291500	6.0N 156.5E	05	120	
3	300000	5. DN 155.0E	10	225	
4	301200	6. DN 157.0E	Ó5	320	
Ś	310000	5.0N 151.0E	10	90	
6	311200	6.0N 149.0E	15	75	
7	071200	17.0M 118.0E	30	30	
8	090000	15.5M 117.5E	20	90	
9	005160	15-0N 117-0F	15	120	

# TROPICAL STORM WAYNE

FIX NO.	TTME (7)	FTX POSTTION	ACCRY	DADJAWK CODE	RATFII FTE	COMMENTS	SITE		
1234456789011123445678901123145671890122344567890132334556788901323345667889401	070012 070032 070032 070254 072034 080914 080914 081234 091235 091215 090115 090115 091215 091215 091215 091215 1010056 101015 1010337 101337 101337 101337 101337 101337 101318 110218 110218 110318 10318	12.7N 140.7E 13.0N 137.5E 14.5N 130.8E 14.7N 134.8E 16.4N 132.5E 16.2N 132.5E 16.6N 131.5E 16.6N 131.5E 16.6N 131.5E 16.6N 120.7E 16.5N 120.6E 15.7N 120.6E 15.7N 120.6E 15.7N 120.7E 16.4N 120.3E 17.5N 120.3E	5 6 5 6 6 5 7 7 8 6 6 6 7 8 7 8 8 8 8 8 8 8 8 8 8 8	TU-0/0-0  T1-5/1-5 /01-5/24HRS  T2-5/2-5=/D1-0/24HRS T2-0/7-0  T2-0/7-5 /WN-5/21HRS	DMSP 34  DMSP 37  DMS	INII JAS/2ND CNTR AT PSN BSJ ON UI FLOW DSN HELCTD ECTHRUD  ULC 153N 1294F  INII JAS  EAPSD LLCC INII JAS  INII JAS  INII JAS  INII JAS			
42	131054	15.9N 127.0E	PCN 4 PCN 5		045037 045036		PGT# PGTW		
43 44	131326	15.6N 122.4E 15.6N 122.3E	PCN 3		DHSP76		RODN		
				<b>a</b>	TRUPAFT FI	XES			
FIX NO.	T1ME- (7)	FTX POSTTION	FLT LVL	70043 OBS MAX-SFC+ HGT MSLP VEL/ARG/	WVD MAX-F RVG DIR/V	ET-FAF-4ND WWANWEL	EYE FYE ORIEN- SHAPE DIAW/TATION	EYF TEMP (F) TREVENT VEHIO	45N NO.
1 2 3 4 5 6 7 8 9	0x2027 0x2153 0x0528 0x1947 0x2140 1x1906 1x2213 1x0540 1x0525 1x0615 1x0558	15.8% 13n.1E 15.8% 13n.1E 15.8% 13n.1E 17.3% 120.2E 17.3% 120.2E 18.3% 120.2E 18.5% 120.2E 18.5% 120.2E 18.5% 120.2E 18.5% 120.2E	700MB 700MB 700MB 700MB 700MB 700MB 700MB 700MB 700MB 700MB	3004 3010 50 n60 3035	15 100 10 160 170 20 160 210 75 230 30 060 30 150	32 080 15 10 3 37 360 15 5 3 51 070 12 5 5 5 38 060 30 5 5 38 060 30 5 5 27 230 15 6 2 30 140 90 4 5 30 320 90 5 10 17 010 30 5 5 48 010 180 4 5		*13 *12 *12 *14 *11 *13 *15 *11 *10 *15 *11 *11 *16 *11 *11 *16 *11 *19 *10 *15 *11 *12 *15 *11 *23 *25 *26	5 6 7 7 9 9 10 10
				SYN	OPTIC FIXE	s			
F1X NO.	TTME- (7)	FTX POSTTION	INTENS ESTIMA		C	DMMENTS			

1 070000 9.9v 141.5E 15 180

# TROPICAL DEPRESSION 26

#### SATELLITE FIXES

F1x NO.	TTME- (7)	F1X P051110%	<b>ACCRY</b>	DVn>≜K COD	E	SATELL TTE	COMMENTS		SITE					
1 2 3 4 5 6 7 8 9	292255 301137 302238 019056 019056 019307 011119 011156 012048 012219 012219 02037	13.2N 154.6F 16.1N 154.5E 18.7N 157.5E 18.7N 157.0E 20.3V 157.2E 20.6W 151.1E 20.6W 151.1E 20.5W 151.0E 22.5N 150.0E 23.9W 140.4E 24.3W 140.7E	9 5 3 3 6 6 6 7 6 7 6 7 7 7 7 7 7 7 7 7 7 7	T2+0/2.0	1 • 0 / 2 4 HR S	DMSP3h DMSP3h DMSP3h DMSP3y DMSP37 DMSP39 DMSP37 DMSP3h DMSP3h DMSP3h	LL EXP ULCC INII DOS RELUCATEN LLCC		PGTW PGTW PGTW PGTW PGTW PGTW PGTW PGTW					
	ATRCHAFT FIXES													
FIX ND.	T1ME (7)	FIX POSITION	FLT L <b>VL</b>	70043 OBS HGT MSLP	MAX-SFC- VEL/ARG/	WYD MAX- RYG NTR/	FLT+LVL+4ND ACC VEL/8NG/AND NAV/	TRY EYE MET SHAPE	EYE ORIEN- DIAM/TATION	ONAL TAN DONAGE ERE LEMB (C)	45N 40•			
S I	011913 012149	23.0N 149.8E 23.8N 149.8E		1001 S018	40 090	270 5° 260	27 200 4n 4 35 200 2n 4	6 3		+15 +11 +14 + 6	3 3			
	SYNDOTIC FIXES													
	TTME (7)	FTX POSTTION	INTENST!			C	DMMENTS							
1	051500	28.20 152.1F	15	120										

#### TYPHOON ABBY

### SATELL TIF FIXES

FIX	TTME (7)	F1X	ACCRY	DAUSAK CODE	ATFILTIE	CJMMFNTS	SITE		
1	304238	6.50 162.05	PON 5	rl.5/1.5	DHENSK	Spc 11NI	PGT# PGT#		
2	010907 011119	6.0% 161.2E 5.7% 161.9E	PCN 6		DMCD37		PGTH		
4	011155	7.60 162.88	PCN 5		Dwcbsa		PGTW		
5	012219	5.74 Jon. 2E	PCN 5	T3.0/7.0 /111.5/24HRS	0MSP36		PGTW PGTW		
6 7	020746	5.94 150.45	PCN 6		DHSP36		PGIW		
4	021135	A.OM 150.56	PCV n		Dachido		PGTW PGTW		
10	020018 020018	5.96 150.0E	Prv 5 Prv 5	T3.5/3.5 /DD.5/26HRS	Drebad Vrash0		PGTW		
11	031042	6.70 150.2E	PCN 6	13047303 71.0037 40.00	DHERSH		PGTW		
15	031117	6.7% 159.4E	PCN 6		Littlen Dresie		PGTW KGWC		
13	031619 032324	5.94 152.8E 3.04 152.4E	PCN B		042534		PGTW		
15	032358	3.0v 158.5E	PCN 3	T4.074.0 /D0.5/24HRS	Dwdb34		PGTW		
16	041024	4.3N 156.1E	PCN 6		DMZRJA		PGTW PGTW		
17 18	041058 042306	9.24 156.0E 4.44 159.9E	PCV 6 PCV 5		DMSP36		PGTW		
19	042339	4.54 157.9E	PCN 5	T4.0/4.0 /S0.0/24HRs	DMZD30		PGTW PGTW		
50	051147 051220	7.74 152.HE	PCN 5		0m2634 0m2634	APRNT LLC INDICATED TO N	PGTW		
55 51	051739	7.54 152.5E	PCN b		TTHOSM		KGWC		
23	052248	8.4N 151.1E	PcN >		DMSP36	2ND CIRC AT ORAN 1504E	PGTW PGTW		
24 25	021159	4.9N 151.2E	PCN 5	T4.0/4.0 /S0.0/24HRS	044634 044634	UL CNIH AT 105N 1479E	PGTW		
5.9	041501	1.5v ]50.5E	PCN 5		Buchsa		PGTW		
27	061728	10.24 140.0E	PON 6	-3	PERPAR AFGEND		KG#C PGT#		
29 29	070011 070042	10.00 145.7E	PCN 5	T3.5/4.0 /W0.3/25HRS	Dridnin		PGTW		
30	071111	144.34 144.3E	PCN 5		Ducase		PGTW		
31	071141	10.34 146.25	PCN 5	T2.5/3.5 /W1.0/24HRs	DNZDJA		PGTW PGTW		
32	072352 040022	11.44 144.5E	PON 5	15.4/5.2	DMZb3A	ZÞC IINI	RODN		
34	0 R U D Z Z	11.5% 144.3E	PON 5		Deca30		PGTW PGTW		
35	0e1234 0e1303	12.3H 141.HE	PCN 5		DHERZA DHERZH	UPR LVL	RODN		
36 37	081303	12.14 130.6E	PCN 5		DMED3A		PGT₩		
35	042334	11.50 130.4E	PCN 5	T3.n/3.0 /D0.5/24HR<	DMSP36		PGTW PGTW		
39 40	090144	11.4% [38.BE	PCN 5		DNZDJA		PGTW		
41	001244	9.8N 134.4E	PCN 5		Ducada		RODN		
42	445141	30.0N 135.PE	PCN 5		PERPMO		PGT# KGWC		
43 44	041337 1nu058	11.5N 135.2E 11.3N 137.5E	PCN 4		DWSP34		PGTW		
45	100125	11.3M 137.4E	PCN 5	T4.0/4.0 /01.0/25HRs	ONSPRA		PGTW		
46	101157	12.2N 132.6E	PCN 5		0MSP14 DMSP34		PGT# RDDN		
47 48	101157	12.24 132.5E	Pon 5		DMSP34		PGTW		
49	191926	13.84 131.3E	PCN 4		TTROSM		KG#C		
50	110039	30.0E NP.FE	PCN 5	T4.5/4.5	AF92MG PF42MG	INI ( )ds	PGTW RPMK		
52 52	110105	14.0M 130.4E	PCN 3	15.0/5.0-/D1.0/24HRS	DHCD30	• • •	PGTW		
53	111320	15.2N 130.4E	PCN J		045634 046634		PGTW PGTW		
54 55	111346 111346	15.1N 130.4E 15.2N 130.3E	PCN P PCN 1	T5+0/5+0	Dwdbda	INII JOS	RODY		
56	120051	15.4N 130.7E	PCN 1		AFGPMO		PGTW		
57	120046	15.5N 130.6E	PCN I PCN I	T5.0/5.0 /50.0/23HRS			PGT# RPMK		
58 59	120046 120227	15.5M 130.4E	PON I	13007920 7.7023724	Ducoau		RPMK		
ÞÚ	120700	17.3m 130.2E	PCN 2		MPHATT AFAPMO		KGWC PGTW		
65 61	121302	14.20 132.4E 19.40 132.1E	PCN 3 PCN 3		DWZD34		RPMK		
63	121327	14.3N 132.4E	PON 3		Dw2h3A		PGTW		
64	130003	19.9N 134.7E	PCN 3	T4.5/5.0 /W0.5/23HRS	AFRAMO PFRAMO		PGTW PGTw		
65 66	130508	20.04 135.3E 20.14 135.2E	PCN 3 PCN 1	T9.0/5.0 /W1.0/26HRS	DMCD30		ROĐN		
6/	131244	21.4N 134.5E	PCN 5		75 45 40 PE 45 40		PGTW PGTW		
69	131309	21.4N 139.5E 21.8N 139.2E	PCN 5		045634		RODN		
70	131753	21.9N 139.8E			TTHOSN		KGWC		
71	172345	22.0M 142.5E	PCN 1	T4+0/4+0 /S0+0/22HRS	)		RODN PGT⊯		
		22.14 142.1E 22.14 142.5E		T4.0/4.5 /W0.5/24HRG			PGTW		
	140001	K. 41 147.00C		7					
				,	TRCPAFT F	IXES			
FIX	TIME	FTX	FLT	70043 385 MAX-SFC-	-M40 M4X-	FLT-LYL-MND ACCRY EYE		EYE TEMP (C)	WSN NO+
NO.	(7)	P051110n	I,VL	HGT MSLP VEL/ARG	1846 UIH	VEL/BRG/ANG NAV/MET SHAP	E DINANTALION	OUT IN DPUSST	40+
			_			76 040 50 5 5		+25 +26 +23	ı
1	912210	5.8N 160.4E			15 090 05 090	36 020 5n 3 5 89 360 12 2 5		+ 9 +11	2
2 1	02010 030920	6.3N 150.1E			130	39 360 25 3 5		+ 4 +10 + 9	3
4	20E1E0	6.5N 159.0E	700MB	3049 995	150	38 110 2n 2 2		+10 +14 + 9 +14 +10	3
5	032130	7.9x 158.8E			15 150 25 050	40 070 60 5 5 41 340 90 5 5		+11 +14 +10	4
6 7	040108 040718	8.24 158.2E 8.14 156.9E		7019 989 50 740	10 360	50 270 56 A 5		+ H +14 +10	5
В	050159	9.2N 154.4E	70046	986 80 270		53 330 20 2 5 53 330 60 3 9		+14 +18 +10 +12 +13 +12	6 7
10	05094D 051300	7.5N 153.4E 7.7N 153.4E			120	59 050 15 6 3		+13 + 9	7
11	0<1421	7.7N 152.5E	7n0#H	3070 1001	120	50 350 60 7 4		+12 +12 +12	7 8
12		8.3N 151.9E		3136 1000 50 ngn	30 070	45 310 5n 2 4		+10 +14 + 6	•

13	060051	8.8N 151.9E	7n04H	3135		35	170	35	กรถ	41	360	90	,	3						
14	040515	9.0M 151.7E	700MH	3123	1002		550	30	120		360	90	Ś							성
15	040835	9.4N [51.9E	700MB	3094	1000		290	30	050			150						* +14 +		8
16	061502	4.3N ]49.7E	7aam8	3099			, , ,	,,	1311				10	4			+11	n +13 +1	2	y
* 17	061402	9.4N 148.4E	70048	3099	1002						2+0	30						+13 +1	0	ý
* 18	062030	4.4N 146.1E	700MB	408n	1002		250		260		160		5	20			+14	• +11 +1		ý
19	062127	10.0N 146.BE	700MB	100()	205		350	25	900		350		4	5						10
e 20	071503	10.2N 144.7E	700MB	3059	995	20	050	25	140		ひっぴ	22	4	20			•2	+25 +2	2 37	10
21	071907	10.2N 146.8E	700MB		996				230		150	50	5	5				+13 +1		15
55	072128	11.1M 144.8E	7nomb	3053					147	33	040	90	5	5				+15 +		12
23	080553			3065	996		020	50	150	43	040	80	4	5			. 1 .	+15 +1		
24	080858	12.34 143.6E	7nome	1084		30	020	30	110	34	020	35	5	5			+1.	, +13, +1	1	15
25	081938	11.9N 147.4E	710MB	30,45					190	27	100	11n	10	5			. 14			13
56		11.3N 139.7E	700MB	3045					150	23	070	5	15	10			+ 1+	• +13 +1		13
27	045156	11.6N 139.4E	700MB	3084		25	230	15	140		070	60	10	- 5				+13 +1		14
	090617	11.2N 137.6E	7nomh	3066		35	300	30	100		300	40		5				+15 +		] 4
28	090812	10.5v 136.3E	7 n D M B	2992	988		360	5	110		360	10		ś	CIRCULAR			+15 +		15
29	091934	14.9N 134.4E	700MB	2925					080		330	30		-	CIRCILLAR	15		+15 +		15
30	092207	11.1N 134.2E	700MH	7935		6.0	190	25	150		040	30	5	5				+ 15 +	•	16
31	102247	13.5N 130.9E	7nomb	2797	964		120	35	170		150	-	7	.,						16
35	110554	14.3N 130.2E	700MB	2792	,,,		300	10	310			35	•	•			+10	+ 15+	•	18
33	110827	14.4N 130.1E	700MH	2776	963		030	13			530	60	5	5				+15 +1	)	19
34	112149	15.9N 13n.3E	700MB	2682	954				250		140	76	5	5			+15	+15 +1		19
35	1>2105	19.4N 133.8E	700MH	2001	754	100	110	30		105		36	5	5				+19 +1		Žΰ
36	122214	19.5N 134.0E	700MB	2664					320	84		15	4	3					•	22
37	130906	20.7N 136.BE			951		310	30				30	5	3				+1		25
38	131938		700MH	2762	962	110	180	50		118		25	5	7	CIRCULAR	30	.14	+19 +		
39	132220	22.1N 141.4E	700MH	2934					180	75		30	5	5	.,		*1.5	+17 +		23
40		22.5N 145.0E	TOOME	300S			350	50	230	45	080	30	5	10						24
40	140737	22.7N 145.5E	1500F7		1001	40	270	15	530	39	070	45		2			+ n	+17 +	,	24
													_	_						75

# SYNDPTIC FIXES

FIX	TTHE-	F1X	INTENSITY	NEAREST	COMMENTS
NO.	(7)	POSITION	ESTIMATE	DATA (NM)	
3 5	290000 3n0000 141200	7.0% 169.0E 7.0% 164.5E 23.0% 148.0E	15 15 20	100 120 200	

#### TROPICAL STORM HEN

#### SATELLITE FIXES

FIX NO.	T+ME (7)	FTX POSITION	ACCRY	DVna	AK COD	ε	!	SATFE	1 TE		С	D#MFF	115			SITE			
1 2 3 9 5 6 7 8 9 10 11 12 13 14 15 17 18	221336 230023 230204 230217	11.74 132.0E 11.74 137.9E 11.54 127.0E 11.55 126.7E 11.55 126.7E 11.56 123.8E 11.66 123.8E 11.66 123.8E 12.64 123.8E 12.64 123.8E 12.64 123.8E 13.65 123.8E 13.65 123.8E 13.65 123.8E 13.65 123.8E 13.65 123.8E 13.65 123.8E 13.65 123.8E 13.65 123.8E 13.67 110.2E 13.69 110.2E 15.74 110.2E 15.74 110.2E 16.74 110.2E	PCN 5 PCN 3 PCN 3 PCN 5 PCN 5	T2.5/	3.5-/N 3.5 3.0 /0	1.0/2	SHRC	DMSI DMSI TTRI DMSI DMSI DMSI DMSI DMSI	936 936 936 936 936 936 936 936 936 936	In	IT	045 045 045				PGTW PGTW PGTW PGTW ROTW ROTW ROTW RODN RODN RODN ROUN ROTW ROTW ROUN ROUN ROTW ROTW ROTW ROTW ROTW			
51 50 19	230217 230640 231304	14.5N 119.3E 14.0N 121.3E 20.0N 123.9E	PCN 5 PCN 6 PCN 5	14.57	3.0 /W	0.5/4	4HKC	TIRE	ns»							KGWC PGTW			
55	231317	20.0N 124.1E	PCN 5					DWS	<b>P</b> 79							PGTW			
							٨	TRCPA	FT F	IXES	i								
FIX NO.	TTME (7)	FTX POSTTION	FLT LVL	70043 HGT	OBS		SFC- SRG/	₩VD I				∉ND ∕NNG			EYE T SHAPE	EYE ORIEN- DIAM/TATION			45N ND•
1 2 3 4	210620 212225 220813 22239	11.5N 125.BE 12.5N 127.3E 13.4N 119.BE 15.5N 119.4E	700MB 700MB 700MB	3047 3013 3052	992 996 995	50 70	030 360 320 020	10	100 210 120 170	46 38 72 56	090 150	6n	1	3	CIRCILLAR	25	+11 +1 +13 + +14 +	8	1 2 4 6
							۵	A JAH I	FŢ¥E	s									
FIA NO.	T1ME (7)	FTX POSITION	RADAR #	CCSY	EYF		EYF DI a			-co0					COMMENTS		RADAR Position	AILE AND M	
2 3 4 5 6	2;0710 2;0940 2;1108 2;1200 2;1300 2;0700 2;1900	12.0N 125.2E 12.0N 125.2E 12.0N 124.2E 11.9N 123.4E 11.9N 123.4E 13.5N 110.9E 15.2N 110.4E	LAND LAND LAND LAND LAND LAND LAND	FAIR	CIRCU		2	10 12 20	0510 2013 0330	5// 527 526 526	14						10.3N 124.0E 10.3N 124.0E 10.3N 124.0E 10.3N 124.0E 10.3N 124.0E 15.2N 120.6E 15.2N 120.6E	98546 98546 98546 98546	6 6 6 7

# 2. NORTH INDIAN OCEAN CYCLONE FIX DATA

#### TC 17-79

#### SATELLITE FEXES

	TIME	F	тx					
NO.	(7)	P0513	1100	ACCRY	SAUSAK CODE	SATELLITE	COMMENTS	SITE
1	052354	6.5N	80.7E	PCV 6	T1.0/1.0	045937	CNTH PACED ON UPD LINE OF THE	
2	841548	7.7N	87.6E	PCN 6	F1.0/1.0	DMSP37	CNTH BASED ON HER LYL OHTELOW	KGWC
3	061705	8.54	88.5E	PCN 6	71.0/1.0	DMSP35	POSIT DARED HOR LVL ANTICYCLONE:	KGMC
4	121670	7.5%	₽9•4E	PCN b	T1.0/1.0	DHSP37	1.111 345	KGWC
5	U7U549	4.8N	H7.HE	PrN 6	T2.5/2.5 /01.5/30HRS			KGWC
5	071220	A. 9N	HK.HE	PCN 6		DMSP37	EDGE OF NATA POSIT BASED CURV	KGWC
7	071547	7 . ON	46.7E	PON 6		DMSP35	TOOL OF HATA MUSTI BASED CORN	KGWC
8	090100	5.9N	BK. 1E	PCN 4	T3.0/3.0 /D0.5/19HRS		APPHNT LOW LVI CIRC	KGWC
9	080528	5.74	HA.3E	PCN 1	T4.0/4.0 /01.5/24HRS		ALLENT THE EAST CIRC	Kewc
10	0A1341	6.14	86.4E	PCN 1		DMSP37	STORM UN EAST FORE OF PICTURE	KGWC
11	081810	7.24	86.7E	PCN 2		DMSP	STORM ON EAST FIRE OF PICTURE	KGWC
12	040040	7.2N	84.3E	PCN 2		DHSP37	EYE COVERED BY THIN CI CANDRY	KGWC
13	090840	7.8N	87.5E			FTROSN	EVE DISTORTED	KGWC
14	091321	9.7N	HA. OE	PCN 4	T3.5/4.0-/W0.5/24HRS		CTR BANED ON CH BANDS	FJDG
15	091751	10.2N	45.5E	PCN 1		DMSP	EYE HAVIGED	KGWC
16	100021	10.7N	84.6E	PC4 1		DMSP37	ETZ MAGED	KGWC
17	100451	11.6N	84.5E	PCN I	T5.0/5.0 /01.0/24HRs		EYE EMMENDED	KGWC
18	101305	12.14	43.6E	PON 2	, , , , , , , , , , , , , , , , , , , ,	DMSP	GOOD EYE GOOD OI DUTFLOW	KGWC
19	101734	12.50	47.4E	PCN 1		DASP	EYE WELL DEFINED	KGWC
* 20	102115	13.00	47.2E			TIROSN	EYE WELL DEFINED EST. DIG	KGMC
* 21	102124	9.44	M4.3E			TTROSM	EYE NOT USBL	FJDG
22	110001	12.5N	82.5E	SCN 5	T5.0/5.0 /D1.5/24HRS	DMSP37	EYE ON ENGE OF DATA	FJDG
53	110142	12.7N	83.3E	PCN 2		DMSP37	EYE WELL DEFINED	KGWC
24	110615	13.3N	62.7E	PCN 2	T6.0/6.0 /D1.0/26HRS	005035	EYE WELL DEFINED AND EMBEDDED	KGWC
25	111001	14.3M	80.5E			TIROSN	EYE WELL DEFINED	KBMC
26	111241	14.1N	82.0E	PCN 2	T6.0/6.0 /D1.0/24HRS	DMSP37	EYE NOT VSBL MIE TO CI CANOPY	FJDG
27	111715	13.9N	81.2E	PCN 1		DMSP	W EDGE OF DATA CI CAP OVER EVE	KGWC
28	150155	14.3N	81.0E	PCN 4		DMSP37	CDO MONE DANG TO CALL OFFI	KGWC
29	120556	14.7N	8n.8E	PCN 4		DMSP35	EYE NO! VSBL ANOD CI OUTFLOW	KGWC
* 3U	121135	15.5N	78.9E			TIROSN	EYE DEFINABLE EST. DIG	KGWC
31	121405	14.5N	79.1E	PCN 4		DMSP37	EYE NOT USBL	FJD6
32	130102	16.9N	78.0E	PCN 6		DMSP37	UPR LAP ANTICACTONE	KGWC
33	130538	16.0N	77.4E	PON 6	T3.0/4.0-/W2.0/24HRS	DMSP35		KGWC

#### TC 18-79

#### SATELLITE FEXES

	FIX NO.	TTME: (7)	FIX POSITI		ACCRY	DVDRAK	CODE	SATFLLITE	COMMENTS	SITE
•	1 2 3	170645 171349 171927	18.7N 17.6N	69.2E 71.1E 66.0E	PCN 6 PCN 6 PCN 6	T1.0/1.0		DMSP35 DMSP37 DMSP35	INIT ONS/ANTICYCLONE ALOFT	KGWC
•	5 6 7	180230 180627 181100 181511	17.7N (	65.0E 64.2E 60.0E 62.9E	PCN 6 PCN 4	12.0/2.0	/01.0/24HRS	DMSP37 DMSP35 TTROSN	UPR LVL ANTICYCLONE GI OUTFLOW	KGWC KGWC KNSS
	9 10	181909 190000 190210	18.5N 6	62.6E 59.9E 50.7E	PCN 6 PCN 6 PCN 6			DMSP37 DMSP35 TTROSN	POSIT MARED ON EXTRAP	KGMC KGMC KNSS
	11	190608 190750 191139	18.2N 6 18.3N 5	50.1E 59.3E 57.0E	PCN 5	T2.5/2.5	/D0+5/24HRS	DMSP37 DMSP35 TERSM TERSM	ON EDGE OF DATA	KGWC KGWC
	14 15 16 17	191450 191950 192300	19.1N 5	9.5E 9.7E 9.0E	PCN 5 PCN 6		/00.5/24HRS	DMSP37 DMSP35 T1ROSN	BASED ON EXPOSED LLC POSIT MASED ON EXTRAP	KNSS KGWC KGWC KNSS
	18 19 20	2n0150 2n0731 2n1430 210419	19.3N 5	7.6E 4.9E 7.1E	PCN 5 PCN 5 PCN 6		/W0.5/24HRs	DMSP37 DMSP35 DMSP37	POSIT WASED ON EXTRAP	KGMC KGMC
		-,-717	17444 3	7.46	PCN 5	11.0/2.0	/W1.0/27HRs	DMSP37		KBWC

#### SYNDPTIC FIXES

FIX NO.	TIME FIX (7) POSTTION		INTENSITY ESTIMATE	NEMREST DATA (NM)	COMMENTS	
1	171200	17.5N	67.0E	30	40	
2	171800	18.0N	65.5E	30	20	
* 3	190600	19.0N	59.0E	45	60	
4	191200	19.0N	60.0E	35	80	
* 5	211900	21.0N	56.5E	15	200	

#### TC 22-79

#### SATER TIF FIXES

	IX O.	TTME: (7)	FT POSTT		4CCRY	DVORAK CODE	SATFE I TTE	COMMENTS	SITE
	ı	211200	8.5N	84.0E			TTROSN		KNSS
-	•	211340	11.5N	85.4E	PCN 6		DMSP37	INI Jus	KG₩C
	٠				PCN 6		DMSP39	INII JOS	KGWC
	3	211502	12.0N	85.2E				*****	KGWC
•	4	220039	14.6N	A7.2E	PCN 6	T1.5/1.5	045037		KNSS
	5	220100	13.5N	P3.lE			TTROSN		
	6	220443	14.3N	84.0E	PCN 6		DMSP39		KG₩C
	-					-1	DMSP37	INI 1 Dds	KG₩C
	- 7	221320	15.DN	82.8E	PCN 6	T1.5/1.5	DMSP39	INI) 045	KGWC
	В	221543	15.2N	87.4E	PCN 6				KGWC
	9	230413	16.84	81.2E	PCN 6	T1+5/1+5	DMSP16	INIT DASYESH HASED ON CONV	
	10	230424	16.9N		PCN 6	T1-0/1-5 /W0-5/24HRS	DMSP39	PSN BADEN ON CENTER UF CONV	KGWC

#### SYMPOTIC FIXES

FIX NO.	TTHE (7)	FTX POSTTION	INTENSITY	NEAREST DATA (NM)	COMMENIS
ī	200000	9.0N BR.0E		250 200	

#### TC 23-79

#### SATELLITE FEXES

FIX	TIME	FI	X					SITE
NO.	(7)	POSTT	IOM	ACCRY	DAOSAK CODE	SATFLITTE	COMMENTS	3115
i	180559	12.44	71.8E	PCN 5	T1.0/1.0	PFGPMQ	INIT DAS/CENTER BASED ON LLCC	KGWC
· ž	191441	12.6N	70.1E	PCN 6		DMSP37		KGWC
3	190140	14.4N	7n.4E	PCN 5	T2.0/2.0 /D1.0/24H	e DMSP37		KGWC
4	190443	14.1N	71.3E	PCN 5		DMSP34		KGWC
* 5	190541	14.1N	71.9E	PCN 5		DMSP39		KGWC KGWC
* 6	191421	14.0N	69.0E	PCN 6		DMSP37		
* 7	191640	13.5N	68.7E	PCN 6		DMSP39		KGWC
8	200120	14.4N	70.3E	PCN 6	TU-5/1.5 /W1-5/24H	RC DMSP37	PSN BSU ON COTR OF CONV/NO LLC	KGWC
9	200512	15.6N	7n•4E	PCN 6		DM263A		KGWC KNSS
* 10	201015	15.0N	69.DE			TIROSN		KGWC
11	201400	15.9N	69.8E	PCN 6		DMSP37		
12	201606	16.2N	69.4E	PCN 6		DMSPRA	PSN BSU ON APPRNT LLCC	KGWC
13	210059	16.7N	69.0E	PCN 6		DMSP37	PSN 854 ON APPRNT LLCC	KGWC KGWC
14	210321	16.9N	69.5E	PCN 4		DMCD34		KNSS
15	211100	18.0N	68.0E	PCN 4		TTROSN		KG#Ĉ
16	211340	17.9N	69•4E	PCN 6	T1.0/1.0 /D0.5/24H	Rs DMSP37		FJDJ
• 17	211447	16.4N	67.0E			TIROSN		KGWC
18	220039	18.5N	64.2E	PCN 3	T3.0/3.0 /02.0/24H	Rs DMSP37		KNSS
* 19	220100	17.7N	65.4E			TTROSN		KGWC
20	220221	18.5N	66.SE	PCN 3		DMSP37		KGWC
21	220625	18.8N	65.7E	PCN 3		DMSP39		KNSS
22	221130	19.0N	64.2E			TTROSN		KGWC
23	.2>1501	19.4N	64.3E	PCN 6		DMSP37	UPR LYL OUTFLOW GOOD	KGWC
24	551115	50.5H	63.3E	PCN 6		DMSP36	PSN BASED ON CENTROID OF CDO	KG#C
25	221724	19.3M	63.5E	PCN 6	T3.0/3.0 /D2.0/24H		SAM BESEL ON CHAINOID OF COD	KGWC
26	230200	19.7N	62.4E	PCN 4	12.0/3.0 /W1.0/24H			KGWC
27	230413	19.6N	62.3E	PCN 3		DMSP36	DE DASES DE ENGRESS LLO	KGWC
28	270606	19.7N	63.2E	PCN 3		DMSP39	PSN BASEN ON FXPOSED LLC	KNSS
29	231100	19.14	61.0E			TIROSN		KGWC
30	231441	20.04	61 • 0E	PCN 6	T2.0/3.0 /W1.0/24H	Rs DMSP37	POSIT USD ON FATHAP	KGWC
31	231705	20.3N	60.8E	PCN 6		PF92MG	PUSIT 450 UN FAIREF	KGWC
32	240140	20.44	60.1E	PCN 3	T1.0/2.0 /W1.0/24H			KGWC
33	240354	20.3N	60.0E	PCN 3		DMSP36	GOOD LE CED I THE/NO CDO	KGWC
34	240547	19.9N	59•4E	PCN 3		Dwcb30		KG#C
35	241421	19. AN	58.8E	PCN 6		045P37	PSN-DS BSD ON LL CU LINE CONV NIL/POSIT HSD ON LLC	KGWC
* 36	241646	19.60	58.1E	PCN 6		PF97mQ	COME APPARATE HOD ON PER	AGMC

#### SYNDSTIC FIXES

FIX NO.	TTME (7)	FIX POSTTION	ESTIMATE		COMMENIS
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1 241800 20.0N 57.0E 10 200

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#### SATELLITE FEXES

FIX NO.	TYME: 17)	FTX POSTTION	ACCRY	DYDRAK CODE	SATELLITE	COMMENTS	SITE
1234 5678 10112134 115167 118170 2212	2x1424 2x2358 2x01445 2x1333 2x14546 3x130 3x130 3x1315 3x1215 3x1223 3x1257 3x	10.24 92.5 10.58 91.5 11.28 90.7 11.58 90.3 12.58 90.3 12.18 60.3 12.18 60.3 12.18 60.3 12.18 60.3 12.18 60.3 12.18 60.3 12.58 86.7 13.68 86.7 13.68 86.7 13.68 86.7 13.68 86.7 13.68 86.7 13.68 86.7 13.68 86.7 13.68 86.7 13.68 86.7 13.68 86.7 13.68 86.7 13.68 86.7 13.68 86.7 13.68 86.7 13.68 86.7 13.68 86.6	PO 0000 DE 00 DE 7 1 1 DE PO CON NO NE POCO NO NE POCO	T0.5/0.5 T1.5/1.5 T1.5/1.5 T1.5/1.5 /S0.0/27HRS	DMSP37 DMSP39 DMSP37 DMSP37 DMSP30 OMSP30 OMSP30 OMSP30 TTPOSN DMSP37	Sec iivi	KGWC KGHC FJDJ KGMC KGWC KGWC KGWC KGWC KGWC KGWC KGWC KGW

#### TC 25-79

#### SATELLITE PRAES

FIX NO.	TTHE (7) .	FTX POSTTION	ACCRY	DAUS#K CODE	SATFII TTE	COMMENTS	SITE
* 1 2 3 4 5 5 6 7 7 8 9 10 11 12 12 13 14 15 16 17	17U502 171417 171648 14U161 14U524 14U524 15U356 15U305 15U705 16U216 14U557 14U646 17U527 17U527 17U526	11-3N 72-01 14-5N 70-11 13-6N 60-91 12-6N 69-51 12-3N 69-71 15-0N 69-71 14-5N 69-71 14-5N 69-71 14-70 70-91 17-2N 70-91 17-2N 70-91 17-8N 70-11 18-5N 69-81	PCN 6 5 5 PCN 6 3 9 PCN 5 3 PCN 5 5 PCN 5 5 PCN 5	T0.5 T0.5/0.5 /S0.0/26HR4 T0.5/0.5 /S0.0/24HR4 T1.5/1.5 /D1.0/24HR4 T1.0/1.5 /W0.5/24HR4	DMSP 17 C DMSP 19 DMSP 17 DMSP 19 DMSP 17 DMSP 17 DMSP 17 DMSP 19 DMSP 17 DMSP 17	EXPSD LLCC	KGMC KGMC KGMC KGMC KGMC KGMC KGMC KGMC

### TC 26-79

## SATELL LIF FEXES

FIX NO.	TIME	FIX Position	ACCRY	DADSWK CODE	SATFLI TTE	COMMENTS	SITE
12 34 56 77 89 10 111 123 * 15 15 16 17 * 18 19 20	2n1528 210033 210009 211314 211509 211510 220013 221253 221253 222353 27235 2723	8.0N 94.0E 9.0N 92.5E 10.5N 92.6E 10.5N 91.8E 10.5N 91.6E 10.9N 91.6E 10.3N 88.7E 10.3N 88.7E 10.3N 80.2E 10.3N 80.2E 10.3N 80.2E 10.3N 80.2E 10.3N 80.2E 10.3N 80.2E 10.3N 80.2E 10.3N 80.3E 10.3N 80.5E 10.3N 80.5E 10.3N 80.5E 10.3N 80.5E		T0-5/0.5 †0-5/0.5 /S0-5/24HRS †0-0/0.0 †2-5/2-5 /02-0/25HRS †1-5/2-5 /W1-0/24HRS	DMSP39 DMSP39 DMSP37 DMSP39 DMSP37 DMSP39 DMSP37 DMSP37 DMSP37 DMSP37 DMSP37 DMSP37 DMSP37 DMSP37 DMSP39 DMSP37 DMSP39 DMSP37 DMSP37 DMSP39 DMSP37 DMSP39 DMSP37 DMSP39 DMSP37	UPR LVL CNTR UPR LVL CNTR INIT 04S ULAC ULAC ULAC ULAC ULAC ULAC ULAC ULAC	KGWC KGWC KGWC KGWC RPMK KGWC KGWC RPMK KGWC KGWC KGWC KGWC KGWC KGWC KGWC KGW

# **APPENDIX**

1. CONTR	ACTIONS	ICAO	International Civil Aviation Organization
AC&W	Aircraft Control and Warning System	IR	Infrared
ACCRY	Accuracy	KM	Kilometer(s)
ACFT	Aircraft	КT	Knot(s)
AIREP	Aircraft Weather Report(s)	LLCC	Low Level Circulation Center
	(Commerical and Military)	LVL	Level
ANT	Antenna	M	Meter(s)
APT	Automatic Picture Transmission	M/SEC	Meters per Second
ARWO	Aerial Reconnaissance Weather Officer	MAX	Maximum
ATT	Attenuation	MB	Millibar(s)
AVG	Average	MET	Meteorological
AWN	Automated Weather Network	MIN	Minimum
BRG	Bearing	TTAHOM	Modified Hatrack
CDO	Central Dense Overcast	MSN	Mission
CI	Current Intensity	NAV	Navigational
CLD	Cloud	NAVPGSCOL	Naval Postgraduate School
CLSD	Closed	NEDN	Naval Environmental Data Network
CNTR	Center	NEDS	Naval Environmental Display Station
CONF	Confidence (number)	NEPRF	Naval Environmental Prediction
CPA	Closest Point of Approach	1421 141	Research Facility
DEG	Degree(s)	NESS	National Environmental Satellite Service
DIAM	Diameter	NET .	Near Equatorial Trough
DIR	Direction	NM	Nautical Mile(s)
DMSP	Defense Meteorological Satellite Program	NOAA	National Oceanic and Atmospheric
EASTPAC	Eastern Pacific	NRL	Naval Research Laboratory
ELEV	Elevation	NTCC	Naval Telecommunications Center
FLT	Flight	OBS	Observation(s)
GOES	Geostationary Operational Environmental Satellite	PCN	Position Code Number
HATRACK	Hurricane and Typhoon Tracking (numerical forecast)	PE	Primitive Equation
am		PSBL	Possible
HGT	Height	PTLY	Partly
HPAC	Mean of XTRP and Climatology	QUAD	Quadrant
HU	Hurricane	RADOB	Radar Observation
HR	Hour(s)	RECON	Reconnaissance
HVY	Heavy		

RNG Range Rapid RPD

SAT Satellite

SFC Surface

SLP (MSLP) Sea Level Pressure (Minimum Sea Level Pressure)

Synchronous Meteorological SMS

Satellite

Spiral Overlay SPOL

SRP Selective Reconnaissance Program

STNRY Stationary

Sea Surface Temperature SST

ST Super Typhoon

Tropical Cyclone ጥሮ

Tropical Cyclone Aircraft Reconnaissance Coordinator TCARC

TCM Tropical Cyclone Model

ΨD Tropical Depression

Television Infrared Observation TIROS

Satellite

тs Tropical Storm

TYTyphoon

Tropical Upper Tropospheric Trough (Sadler, 1976) ጥፒያጥጥ

Velocity VEL. VIS Visual VSBL Visible

WESTPAC Western Pacific

World Meteorological Organization WMO

WND

Weather Reconnaissance Squadron WRS

XTRP Extrapolation

Zulu Time (Greenwich mean time)

#### 2. DEFINITIONS

BEST TRACK - A subjectively smoothed path, versus a precise and very erratic fixto-fix path, used to represent tropical cyclone movement.

CENTER - The axis or pivot of a tropical cyclone. Usually determined by wind, temperature or pressure distribution.

CYCLONE - A closed atmospheric circulation rotating about an area of low pressure (counterclockwise in the northern hemisphere)

EPHEMERIS - Position of a body (satellite) in space as a function of time. When no geographical reference is available for When gridding satellite imagery, then only ephemeris gridding is possible which is solely based on the theoretical satellite position and is susceptible to errors from satellite pitch, orbit eccentricity and the nonspherical earth.

EXPLOSIVE DEEPENING - A decrease in the minimum sea level pressure of a tropical cyclone of 2.5 mb/hr for 12 hrs or 5.0 mb/hr for 6 hrs (ATR 1971).

EXTRATROPICAL - A term used in warnings and tropical summaries to indicate that a cyclone has lost its "tropical" characteristics. The term implies both poleward displacement from the tropics and the conversion of the cyclone's primary energy sources from release of latent heat of condensation to baroclinic processes. The term carries no implications as to strength or size.

EYE - "EYE" is used to describe the central area of a tropical cyclone when it is more than half surrounded by wall cloud.

FUJIWHARA EFFECT - An interaction in which tropical cyclones within about 700 nm of each other begin to rotate cyclonically about one another. When intense tropical cyclones are within about 400 nm of each other, they may also begin to move closer to each other.

MAXIMUM SUSTAINED WIND - Maximum surface wind speed averaged over a 1-minute period of time. Peak gusts over water average 20 to 25 percent higher than sustained wind.

RAPID DEEPENING - A decrease in the minimum sea level pressure of a tropical cyclone of 1.25 mb/hr for 24 hrs (ATR 1971).

RECURVATURE - The turning of a tropical cyclone from an initial path toward the west of northwest to the north then northeast.

SIGNIFICANT TROPICAL CYCLONE - A tropical cyclone becomes "significant" with the issuance of the first numbered warning by the responsible warning agency.

SUPER TYPHOON/HURRICANE - A typhoon/ hurricane in which the maximum sustained surface wind (1-minute mean) is 130 kt or greater.

TROPICAL CYCLONE - A nonfrontal low pressure system of synoptic scale developing over tropical or subtropical waters and having a definite organized circulation.

TROPICAL CYCLONE AIRCRAFT RECONNAISSANCE COORDINATOR - A CINCPACAF representative designated to levy tropical cyclone aircraft weather reconnaissance requirements on reconnaissance units within a designated area of the PACOM and to function as coordinator between CINCPACAF, aircraft weather reconnaissance units, and the appropriate typhoon/ hurricane warning center.

TROPICAL DEPRESSION - A tropical cyclone in which the maximum sustained surface wind (1-minute mean) is 33 kt or less.

TROPICAL DISTURBANCE - A discrete system of apparently organized convection--generally 100 to 300 miles in diameter--originating in the tropics or subtropics, having a non-frontal migratory character, and having maintained its identity for 24 hours or more. It may or may not be associated with a detectable perturbation of the wind field. As such, it is the basic generic designation which, in successive stages of intensification, may be classified as a tropical depression, tropical storm or typhoon (hurricane).

TROPICAL STORM - A tropical cyclone with maximum sustained surface winds (1-minute mean) in the range of 34 to 63 kt, inclusive.

TROPICAL UPPER TROPOSPHERIC TROUGH (TUTT)
- "A dominant climatological system, and a
daily synoptic feature, of the summer season
over the tropical North Atlantic, North
Pacific and South Pacific Oceans," from
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TYPHOON/HURRICANE - A tropical cyclone in which the maximum sustained surface wind (1-minute mean) is 64 kt or greater. West of 180 degrees longitude they are called typhoons and east of 180 degrees they are called hurricanes. Foreign governments use these or other terms for tropical cyclones and may apply different intensity criteria.

WALL CLOUD - An organized band of cumuliform clouds immediately surrounding the central area of a tropical cyclone. The wall cloud may entirely enclose the eye or only partially surround the center.

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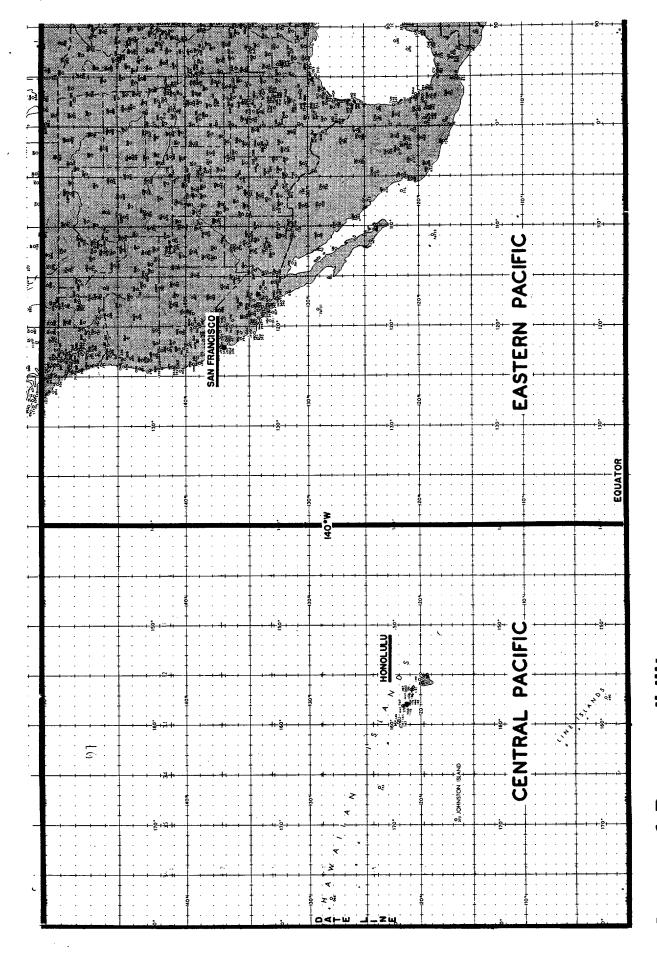
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