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# Woods Hole Oceanographic Institution



# Tidal Observations at Ria Formosa, Algarve, Portugal

by

Paulo Salles Stephen P. O'Malley George Voulgaris David G. Aubrey

May 2000

## **Technical Report**

Funding was provided by WHOI Sea Grant, EU MAST III Program, UNAM, Mellon Foundation and Rinehart Coastal Research Center.

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## 1. INTRODUCTION

This project is part of the field campaign of the MAST3 Project InDIA (Inlet Dynamics Initiative: Algarve) conducted in the lagoon of Ria Formosa in Algarve, Portugal.

Whereas the InDIA fieldwork partners focused on the New Ancão Inlet in the Ancão Peninsula, with intensive field measurement in its vicinity (2.5 km<sup>2</sup>), the work presented here covers the entire lagoon and its six inlets. The field campaign was meant to provide detailed data for the calibration and validation of a hydrodynamic numerical model. The model will ultimately simulate the hydrodynamics of the Ria Formosa lagoon and will serve as a tool to analyze the persistence of multiple tidal inlets in the system and identify the processes responsible for such persistence.

For the model setup, the field measurements are needed to provide (i) updated bathymetry of the estuary, and (ii) detailed surveys of each inlet. In situ measurements of (iii) water level fluctuations within the estuary and (iv) current velocities are required for calibration purposes, as well as for validation (in instances where more than a single data set is available). Items (ii), (iii) and (iv) are covered by this report.

The survey of the inlets, item (ii), was conducted from a survey vessel using Differential Global Positioning (DGPS) and a high precision Fathometer.

The water level fluctuations within the estuary, item (iii), was obtained using tide recorders. Internally recording pressure/temperature loggers (PTL) were deployed at different locations in the lagoon in order to document the tidal characteristics throughout the system. The approximate location of the deployments was determined from maps trying to cover the entire lagoon and the actual location was eventually determined *in situ* to ensure an optimal location in terms of navigability, security and data quality. In addition an Acoustic Doppler Velocimeter was deployed offshore, in the vicinity of the Cacela Inlet, in order to record the offshore tide.

Finally, the current velocities at the inlets and other selected locations, item (iv), was obtained using a broadband high frequency Acoustic Doppler Current Profiler (ADCP).

This report gives first a brief description of the instrumentation used in the field (section 2), then describes the methods used to deploy the instruments, perform the surveys and gather the data (section 3), and explains the procedures for data reduction and shows some results (section 4 and Annex). All the raw and processed data is stored in electronic format.

## 2. INSTRUMENTATION

## 2.1 Tide Gauges

Tidal data were acquired using internally recording pressure/temperature loggers. For this program Brancker TG205 gauges were used. The Brancker instruments were chosen because of their proven reliability, ease in use and they provide measurement accuracies appropriate for this project. Each instrument was calibrated at the Woods Hole Oceanographic Institution prior to deployment. The accuracy and nominal operating range for each instrument is provided in Table 2.1.

Instruments use a Druck strain gauge to measure total pressure ( $P_{atm} + P_{H2O}$ ). Within each sampling period, a user-defined number of "burst" samples were taken and then averaged to provide a single value for that period. Although the number of bursts is programmable, the interval between each measurement is fixed at 0.5 seconds. Battery and data storage limitations over the length of deployment defined the maximum amount of data that can be acquired. The typical sample interval is six minutes which when deployed over a full lunar cycle provide adequate data to derive the harmonic constituents of the local tides.

Instrument	Accuracy (cm)	Resolution (cm)
TG 1	0.5	+ 1.0
TG 2	0.7	<u>+</u> 1.5
TG 3	1.1	+ 2.2
TG 4	1.2	+ 2.5
TG 5	1.2	<u>+</u> 2.5
TG 6	1.2	<u>+</u> 2.5
TG 7	1.2	<u>+</u> 2.5
TG 8	1.2	<u>+</u> 2.5
TG 9	1.1	<u>+</u> 2.2

## Table 2-1 Tide Gauge Specifications.

## 2.2 ADCP

An acoustic doppler current profiler (ADCP), manufactured by RD Instruments was used to measure and record current velocity profiles at each inlet in the Ria Formosa system. The ADCP transmits an acoustic pulse of known frequency (1200kHz) into the water and calculates the current velocity based on the change in frequency (Doppler shift) of the returning echoes. The unit provides high-resolution vertical profiles of the current by reporting the speed and direction of flow at discrete layers (or bins or depth cells) below the survey vessel. Each vertical strip containing depth cells is called an ensemble.

In shallow coastal systems, bin sizes are usually chosen to have a length of 1 meter or less. The data will provide a single averaged velocity and direction from

the multiple samples taken within each bin. Near surface data are not provided due to the displacement of the instrument and a "blanking period" during which time the ADCP does not listen for returns immediately after transmit. Data at the bottom layer are usually not valid due to interference from return signals from the side lobes of the transmit pulse. This invalid data zone at the bottom is usually about 6% of the water depth.

The ADCP does recognise the higher intensity backscatter from the water / sea bottom interface. These "bottom-track" data may be valuable in deriving information about other characteristics of the survey area. For example, bottom track data from cross-channel transects will provide a profile of channel depth from which the total area may be found. When multiplied by the water column velocities the total flow through the channel is provided. In addition, the speed at which the survey boat is travelling over the bottom may also determined by the return frequency shift. This velocity data combined with the ADCP's internal compass can provide recorded data of vessel speed and direction.

Navigational control was provided by differential GPS. The data are passed to a computer program which displays time display to the boat operator. When passed to the "Hypack" computer software, a plan view of the adjacent coastline, trackline to be run and an icon representing the boat are shown on the screen and updated each second. Matching data at the common time base combines the ADCP and navigation data files.

## 2.3 ADV

An internally recording Acoustic Doppler Velocimeter (ADV) was used to measure the current velocity and surface wave conditions at a site located seaward of the easternmost inlet. The ADV, manufactured by Sontek, measures current by transmitting a 5 MHz acoustic pulse and determining the Doppler shift of the return signal. The ADV senses three components of flow velocities of up to 5 m/s. The combination of small sampling volume and sampling rates of up to 25 Hz make turbulence measurements also possible. The instrument was chosen for this application because of it's excellent low flow performance and the ADV internal power and recording systems allow long term remote deployments.

## Table 2-2 ADV Specifications.

Acoustic frequency	5 MHz
Velocity range	1 mm/s to 5 mm/s 0.1 mm/s
Sampling rate	Programmable from 0.1 to 25 Hz

This instrument was chosen because of its capability of giving pressure and directional wave data. The sampling strategy was designed accordingly. For the pressure alone, the sampling rate for each burst was 0.2 Hz, twenty four samples

were averaged to record a data point every six minutes. This burst type is consistent to the sampling design adopted for the tide gauges. For wave measurement, the instrument sampled at a frequency of 2Hz for a period of 5 minutes (i.e. 600 samples), repeating the sampling every hour. Details of the ADV deployment set-up are given in Annex B-1.

#### 2.4 Navigational Control

Positioning of all fixed instrumentation and survey vessel tracking was accomplished using differential global positioning system technology (DGPS). A Trimble AgGPS 132 receiver was installed on the survey vessel. A single deep cycle battery (car battery) provided 12-volt DC power. Positions were referenced to the WGS-84 ellipsoid and later transformed to the local Universal Transverse Mercator projection, zone 29.

The largest source of stand-alone GPS data is due to Selective Availability (S/A). S/A is introduced by the U.S. government for the purpose of restricting full GPS accuracy to all but authorised users. The magnitude of S/A combined with other error sources (variable atmospheric conditions) results in horizontal errors of up to 100 meters. In order to remove the selective availability error, a differential correction signal was a received and applied to the raw GPS positions. This differential data is created by determining the difference between known position and that provided by GPS at precisely the same location. The resulting horizontal accuracy of the DGPS data used in this program is less than one meter, as shown in Figure 2.1.





Figure 2.1 provides results of a position repeatability test performed prior to start of fieldwork with the Trimble AgGPS 132. 3600 measurements were recorded over one hour at a fixed position. The distance from the mean position for each of the position values is less than 1 meter. This high repeatability is particularly valuable when recovering bottom mounted instruments, whose positions have not been marked at the surface, in low visibility water.

## 2.5 Fathometer

Bathymetric data were collected with an Odom Echotrac, dual frequency fathometer. Echo sounder transmit frequencies are manually selected (200 and 24 kHz) to provide the best resolution over variable bottom compositions. Instrument accuracy is  $\pm$  0.25 cm. This Odom depth sounder provides a paper chart record and digital depth data that are output via RS-232 serial line to the recording computer. One sounding per second is the typical update frequency when working in shallow coastal areas, which provides a depth value every 2 meters at survey speed.

The Odom fathometer is calibrated at the start of each survey day or whenever operations are moved to an area where the water properties differ from those at the last calibration site. Calibration is performed by adjusting the speed of sound value the Odom uses to calculate depths. Shallow water survey areas allow the operators to measure the true water depth with a surveyor's stadia rod and then adjust the speed of sound value accordingly until the measured and calculated values agree.

## 2.6 Land Survey Instrumentation

Transfer of vertical control from provided benchmarks to the installed tide gauges was performed using a Topcon model GTS 3-B total station. System components consist of the measuring unit, tripod, triple prism reflector and stadia rod. The distance measurement capability under worse case conditions (haze with visibility of 7km, sunlight and ordinary heat shimmer) is  $\pm$  5mm. Vertical accuracy under similar conditions is  $\pm$  00° 00' 3".

## 3. FIELD METHODS AND PROCEDURES

The deployment locations of the tide gauges and the ADVs (including an approximate location of the ADV deployed by POL near the New Ancão Inlet) and the ADCP survey locations are show in Annex C.1.

## 3.1 Tidal Measurements

The tide gauges were deployed at nine different locations throughout the system as shown in Figure C.1.1. These sites were chosen to maximise spatial coverage and to record data in areas that are of significance to future numerical modelling

efforts. The gauges were set at depths that insured the pressure transducers would remain submerged at low water events and that they would not cause a hazard to local boating or fishing activity. Sixteen sample bursts were taken at a rate of 2 Hz and then averaged to provide a single point for each six-minute sampling interval. This rate provided 240 samples/day. The instruments were mounted to sub-surface pipes that had been water jetted into the sea bottom. Instrument positions were obtained using the differential global positioning system (DGPS) referenced to the WGS-84 ellipsoid. Positions were recorded for use during recovery and later tidal analysis. In order to minimise the possibility of the instrument being tampered with during the deployment, the positions were not marked at the surface. Elevations of the pressure recorders were established with the land survey equipment and referenced to the Portuguese Vertical Datum (hydrographic zero =– 2.00 m with respect to the mean sea level in the port of Cascais, near Lisbon).

In addition to the data provided by the Brancker tide gauges, sea surface elevations were also recorded by the acoustic doppler velocimeter/wave gauge (ADV) deployed offshore, south of Cacela. Because of the difficulty in obtaining vertical position of the pressure transducer at such a distance offshore, the data are not directly referenced to any datum. It was assumed that the MWL offshore of Faro is the same as that at Cascais and therefore the data were considered valid for inclusion in analysis of local tidal characteristics.

## 3.2 Bathymetry

Bathymetric survey data were acquired using an integrated hydrographic surveying system (Hypack). Positioning of the vessel was accomplished using differential global positioning system while soundings were taken with an Odom fathometer. Electrical power for system operation was provided by a 100 watt 110 AC generator.

A 6-meter outboard motor powered vessel was configured to serve as the survey platform. The computer, fathometer electronics and DGPS unit were installed inside the vessel cabin. The fathometer transducer was mounted to the hull via an aluminium gimbal mount, which could be rotated 90° to bring the transducer out of the water during transit to and from survey sites. Since it is required that the transducer face is submerged for proper operation, it was necessary to measure this "draft" below the water surface an add the value to all raw depths. This correction function was performed by the Odom fathometer before transmittal of data to the PC.

Guidance to the vessel helmsman was provided by the survey software. The computer monitor display program shows a digitised coastline, dashed lines representing pre-defined survey tracks and an icon representing the survey boat. Digital values of the distance off line, water depth and several other parameters are also shown.

## 3.3 ADCP Surveys

The ADCP was configured to record and average 20 current velocity values at 0.25 m depth increments (bins) each throughout the water column. The uniformly shallow depths of the Cacela inlet allowed for improved measurement resolution by reducing the bin size to 0.10 m. A data file for each transect pair (one direction and then the opposite) was named by it's starting time and then recorded on the integrated PC via a RS-232 serial connection. Raw data were provided in hexadecimal format that was converted to ASCII during post processing. Each line file consists of a bin number, bin depth, velocity north, velocity east, resultant velocity, resultant direction, raw compass value, pitch, roll and then several columns of data quality indicators.

Cross-channel ADCP surveys were performed at six inlets of the Ria Formosa system. The ADCP transducer unit was mounted to the boat in the same manner as the bathymetry unit, where the over-the-side equipment was mounted to a gimbaled device and the DGPS antenna located directly above. During each survey, the vessel was run between two buoys that were placed at recorded positions on each side of the channel. DGPS guidance was again provided to the helmsman through the real-time display. Given the different characteristics of each location (size, depth, wave condition during the survey), the instrument was configured before each survey to optimise the data quality. For instance the sample rate, the size of the depth cells, the speed of the boat and the depth of the transducer faces below the water surface were determined before the start of the each survey, and the instrument configured accordingly. The specific instrument configuration for the New Ancão Inlet survey is shown in Annex C.1. The other configurations are available in electronic format. Each particular transect (or survey line) was chosen so that the flow and total volume of water through the inlet could be determined. The line was repeated approximately every 30 minutes over the course of a full tidal cycle (12-13 hours). At the end of each line, the vessel was brought as close to the shoreline as possible in order to maximise the area over which measurements were taken. The actual lengths of each transect varied over the course of the day as the sea surface elevation changed with tide. This variation was minimised by designing the vessel course, and saving it in the navigation computer, in a preliminary visit to the site during low tide. Plots of the designed lines (plotted over orthophotomaps from a 1991 aerial coverage) are provided in Annex C.2.

## 4. DATA REDUCTION AND RESULTS

## 4.1 Tide Data

The tidal data were collected by the 9 PTL deployed inside the lagoon and by the ADV deployed offshore. The field campaign was designed to collect tidal data for

at least a lunar cycle. The ADV was deployed offshore as planned. Due to problems with the analog board, the instrument had to be replaced and the deployment was delayed. In addition, since the deployment sites of the last two tide gauges and the ADV were close together in the easternmost part of the system, it was decided to wait for the new ADV and deploy the 3 instruments the same day. Furthermore, the ADV stopped recording nine days after being damaged by a trawling net.

Table 4.1 shows the deployment duration and the percentage of data recovered from each instrument.

Instrument	Location	Deployment dates	Deployment duration (days)	Data return
TG 1 (#8096)	Faro Beach (near bridge)	1/21 to 2/28	38	100%
TG 2 (#5078)	New Ancão Inlet	1/21 to 2/29	39	100%
TG 3 (#3853)	Main Channel	1/21 to 2/28	38	100%
TG 4 (#8711)	Main (Farol) Inlet	1/22 to 2/28	37	62%
TG 5 (#8712)	Armona Inlet	1/22 to 2/28	37	100%
TG 6 (#8710)	Olhão	1/22 to 2/28	37	68%
TG 7 (#8709)	Fuzeta	1/25 to 2/28	34	100%
TG 8 (#8713)	Tavira (Santa Luzia)	2/4 to 2/28	24	100%
TG 9 (#5081)	Cacela	2/4 to 2/28	24	100%
ADV (#9001)	Cacela (offshore)	2/4 to 2/13	9	100%

Table 4-1 Tide	Gauges and A	<b>OV Deployment</b>	t Duration and	Data Return.
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TG 4 and TG 6 failed 23 and 25 days after deployment, respectively. The pressure readings were translated to water surface elevation using the elevation of the pressure transducers (see section III), removing the atmospheric pressure and assuming a constant water density of approximately 1,024.5 kg.m<sup>-3</sup>. The hourly values of atmospheric pressure are shown in the Annex E.

Figure 4.1 shows the records of Sea Surface Elevation. In that figure, the data from the offshore instrument #1000 was provided by the Proudman Oceanographic Laboratory. For both offshore instruments (#1000 and #9001) the mean sea surface elevation was assumed to be 2.00 m above datum, as the Mean Water Level in Cascais.

The water surface elevation records shown in Figure 4.1 were analyzed in order to derive the amplitude and phases of the tidal constituents. The results of this analysis will be used (i) to study the tidal distortion inside the estuary and thus contribute in the understanding of the hydrodynamics of this multiple tidal inlet system, and (ii) as a tool for the calibration of the numerical model.

The harmonic analysis of the tides from the data of each instrument was performed using the software package developed by the Institute of Ocean Sciences (Foreman, 1977).



#### Figure 4.1 Tidal Records for Each Instrument.

The program analyzes hourly height tide gauge data for a given period of time. Amplitudes and Greenwich phase lags are calculated via a least squares fit

method coupled with nodal modulation for only those constituents that can be resolved over the length of the record. For short records with which certain important constituents cannot be resolved from the data, provision is made for the inference of the amplitude and phase of these constituents from others.

Prior to tidal analysis, the data were decimated to hourly observations and the time base corrected to GMT. Then the data were reformatted in the format needed for the program's input file, as show in Figure IV.2 for the New Ancão Inlet data.

2	1.00		0.	0				1			-				
8	1721 19919	8 :	L 399	919											
	5078New	In	let	(Port	ugal	L) (	SMT 3	3659	-758	3					
1	5078	21	1999	99999	99999	99999	99999	99999	99999	99999	99999	99999	99999	99999	9999
2	5078	21	1999	99999	99999	99999	9999	321	321	287	237	177	124	101	119
1	5078	22	199	154	205	257	293	333	348	320	272	215	158	111	102
2	5078	22	199	128	166	216	256	292	312	303	266	213	159	115	104
-															
1	5078	26	299	276	237	190	150	123	119	140	172	215	254	282	302
2	5078	26	299	288	258	215	169	138	126	139	167	212	253	290	315
1	5078	27	299	318	293	248	195	147	114	110	132	171	220	265	295
2	5078	27	299	319	302	267	214	161	122	109	126	163	213	263	301
1	5078	28	299	325	331	294	244	182	129	98	97	125	170	226	269
2	5078	28	299	302	319	301	255	197	142	107	96	125	172	227	278
1	5078	1	399	312	343	326	284	227	165	109	839	99999	99999	99999	9999
2	5078	1	3999	99999	99999	99999	99999	99999	99999	99999	9999	99999	99999	99999	9999

# Figure 4.2 Sample input file for the Harmonic Analysis software (New Ancão inlet, partial).

The record lengths used for the analysis and the number of constituents for which amplitudes and phases were derived are listed in Table 4.2.

Instrument	Hours analysed	Constituents Derived
TG 1 (#8096)	914	36
TG 2 (#5078)	928	36
TG 3 (#3853)	912	36
TG 4 (#8711)	544	18
TG 5 (#8712)	888	36
TG 6 (#8710)	600	18
TG 7 (#8709)	819	36
TG 8 (#8713)	574	18
TG 9 (#5081)	572	18
ADV (#9001)	213	10

In addition, filtering tests were performed to the data for all instruments in order to detect possible spikes and noise in the data. For that, Godin's filter was used, as suggested by Foreman (1977). This filter is a triple moving average filter, which performs three consecutive convolutions to the original data with a 10, 10 and 11 points averaging impulse response, respectively. The program applies suitable amplitude corrections to compensate for the smoothing effect of these filters.

After performing the harmonic analysis to the original and the filtered data it was found that the differences in amplitude and phase between both data sets were minimal. The results also show that the standard deviations of the amplitude, A, and phase,  $\varphi$ , for each tidal constituent are much larger for the filtered data than for the original data (2 to 3 times and 3 to 4 times for the short and long data sets, respectively), suggesting a higher confidence in the unfiltered data results. Furthermore, the unfiltered data results show values of A and  $\varphi$  which fall within the confidence intervals of the corresponding values from the filtered data results with a 68.3% confidence level (+/- one standard deviation). Therefore, it was concluded that the data did not need filtering prior to the harmonic analysis computations.

The results of the harmonic analysis for the full data sets of each instrument are listed in the Annex D.

## 4.2 Bathymetry Data Processing

Bathymetry data were collected at the Ria Formosa during 29-30 January, 1999. Seven files were provided for processing. Due to what was most likely operator error, data collected at the Cacela site did not contain depth values and were therefore not of use. Valid data were acquired at the following locations:

Main Inlet (Farol) 4.1 km Tavira 2.3 km	New Ancão Inlet	5.3 km	Armona	15.9 km
	Main Channel	17.5 km	Fuzeta	7.3 km
	Main Inlet (Farol)	4.1 km	Tavira	2.3 km

Plots of the bathymetric survey coverage are provided in Annex A. Upon initial inspection, it was determined that the real time conversion of navigational data from the WGS-84 geographic coordinates to UTM zone 29 (XY) was done incorrectly. It appears that while in the field, the transformation parameters were incorrectly set resulting in erroneous positional data. Fortunately the geographic coordinates provided by the DGPS were logged in the field. These have allowed for datum transformation to occur during post processing.

## Example of \*.RAW data file

FTP NEW INF "PAULO" "SHETLAND" "INDIA" "ALGARVE" 0.000000 0.000000 1500.0 FIL "DAT" "" "" ELL WGS-84 6378137.000 298.257223563 PRO UTM North 5.387639 0.9996000 0.000000 0.000000 0.000000 500000.0000 TND 12:40:48 01/29/99 DEV 0 228 "GPS" DEV 1 16 "ODOM" PRI 0 EOH FIX 1 EC1 1 45648.679 11.40 (time, depth) RAW 0 45648.982 4 370043.450 -74855.930 5.31 124049.00(X,Y,Lat, Long, ...) POS 0 45648.982 605933.95 4096338.31 EC1 1 45649.341 11.50 GYR 0 45649.025 124.40 (time, heading) RAW 0 45649.002 4 370046.450 -74856.930 5.31 124049.00

Data were processed using the Hypack® hydrographic software package. Processing consisted of editing and sorting the data. A brief description of each process follows:

## Editing

Editing consists of three processes, tide correction, elimination of "bad" points and conversion of the data format.

## Tide Correction

Raw bathymetry and tide correction data are read into the editing program where they are aligned according to time stamp in each file. Tide correction values (provided in feet above the datum) are subtracted from the raw depth data giving water surface elevations referenced to the datum.

## Elimination of "Bad " Data

Each survey profile was plotted on screen at a large scale to provide visual evaluation of the data. Spikes in the bathymetry and other data, which were obviously in error, were deleted from the file. Data were then re-plotted using a linear interpolation to replaced deleted data.

## <u>Format</u>

The data format was changed from the raw field version, which provides extensive header information, to a more processing oriented style (\*.ALL). The ALL format is required for input into the SORTING routine.

N	ORMAL	A	LL	UTM			12:40	):48	01/2	9/99	WF	IOI	SHET	LAND
IN	IDIA	ALG	ARVE											
G	PS	C	DOM				GP	S		WGS-84				
1	605934.	16 4	096338.	25 1	1.50	0.00	-12.11	456	49.34	0.00	0.00	0.000		
1	605934.	36 40	096338.	19 1	1.50	0.00	-12.11	456	49.67	0.00	0.00	0.000		
1	605934.	55 40	096338.	12 1	1.60	0.00	-12.11	456	50.00	0.00	0.00	0.000		
1	605934.	70 40	096338.	00 1	1.50	0.00	-12.11	456	50.33	0.00	0.00	0.000		

#### Example of \*.ALL data file

#### Sorting

The Hypack SORT program performs two functions:

- 1) The data format is changed from the \*.ALL format created by the edit routine to \*.xyz where
  - X = the UTM X coordinate
  - Y = the UTM Y coordinate
  - Z = the corrected water depth in feet
- 2) The number of data points within a user input radius is reduced to one. This allows plotting of data without overwriting of characters. An indication of the amount of data eliminated in this process is indicated by the "% saved" value.

	Number of points	_		
<u>File Name</u>	after processing	<u>% Saved</u>	<u>Max Depth (ft)</u>	Min Depth (ft)
Armona.xyz	9168	54.5	36.21	-8.66
Fuzeta.xyz	4289	47.5	18.19	-2.09
Main Inlet.xyz	2524	46.9	99.80	-2.61
New Inlet.xyz	3277	50.2	18.68	-5.54

The final output consists of the files shown in the previous table. These \*.XYZ data files are ASCII files with one column for each field as shown below.

Exam	ple	of	*.XYZ	data file

000605934.99	004096337.77	-0.91	
000605936.25	004096336.99	-1.01	
000605937.92	004096336.51	-0.91	
000605938.81	004096337.14	-0.61	
000605939.87	004096336.46	-1.21	
000605941.25	004096335.62	-1.12	
000605942.05	004096334.99	-0.72	
000605943.78	004096333.85	-1.32	
000605944.85	004096333.08	-0.92	

## 4.3 ADCP Data

The ADCP delivered real time data to a computer screen and to a storage device during the length of the surveys. While these data was gathered in one computer, another computer was used to store geographic position data from the DGPS, as explained in section 2.4. These two sets of data form the bulk of the ADCP data. As mentioned in section 3.3, each survey had its own instrument configuration. The details of each configuration, as well as the survey locations, are shown in Annex C-1 and available in electronic format.

Following is the procedure for the ADCP data reduction:

- 1. Transformation from raw (binary) to text (ASCII) files. The data output from the instrument comes in binary format. These files were converted to text files for further post-processing.
- 2. Matlab® routines were created to reduce the data and plot the velocity profiles for each line. Selected velocity profiles for each survey are plotted in Annex C-2 and available in electronic format. These plots show the magnetic North and East velocities throughout the measured region. They also show the bottom of the channel to have an idea of the size of the measured portion of the water column. It can be noticed that there are two layers in the water column (near the surface and close to the bottom) in which there are no measurements.

The size of the upper unmeasured layer is the sum of (1) the "blank after transmit" due to the ringing effect in the pulse transmitted by the instrument, which for the 1,200 kHz instrument used is approximately 0.5 m, and (2) the depth of the transducer faces below the water surface.

The size of the lower unmeasured layer is equal to the portion of the water column below the maximum range of the instrument, which in turn corresponds to the location where the signal strength drops to levels comparable to the noise level. The maximum range of the instrument is approximately 94% of the water column, minus one depth cell.

3. Due to problems with the DGPS signal reception during the ADCP surveys, not all the lines have an accurate geographic position. This problem was solved by obtaining the average position of the start point of the lines with good DGPS information and by assuming that the rest of the lines started in the same point. This assumption is valid since (1) the start point was always marked with a buoy, as explained in section 3.3, and (2) the precise location of each line with respect to the other was unnecessary given that the objective of the ACP surveys was to obtain the overall velocity profile and total discharge through the inlet and channel cross-sections.

#### 4. Discharge computations.

The total discharge through the inlet and channel cross-sections was computed by integrating the velocity profiles along the area covered by each line. More specifically, the procedure to compute the discharges consisted of:

- a) When appropriate, the cross-sections surveyed were subdivided into subsections as shown by the vertical dashed lines in the velocity profiles (see Annex C-2). This was done to differentiate discharges from the channels to discharges from the banks.
- b) The vertically averaged North and East velocities for each ensemble (see section 2.2) of each subsection were projected in the direction perpendicular to the ensemble orientation.
- c) The resulting velocity for a given ensemble was multiplied by the total area corresponding to this ensemble (= length of the ensemble X total depth) to account for the unmeasured layers.
- d) The total discharge was computed as the sum of all the ensemble discharges for a given line at a given time. In instances where the velocity profile for a given line had bad ensembles such that the average velocity was visibly wrong, an estimate was computed by interpolating the adjacent velocities.

The results of the discharge computations are shown in the Annex C-3 and available in electronic format.

## 5. ACKNOWLEDGMENTS

We thank Wayne D. Spencer, William Robertson V and Zoe Hughes for their cooperation in the field data acquisition. In addition we would like to thank all the people from the other InDIA partnership institutions and from Portugal who helped us during the field campaign.

The work was undertaken as part of the MAST3 Project INDIA and is a result of research sponsored jointly by NOAA National Sea Grant College Program Office, Department of Commerce, under Grant No. NA86RG0075, Woods Hole Oceanographic Institution Sea Grant Project No. R/G-27, by the Commission of the European Communities, Directorate-General for Science, Research and Development under MAST Contract No. MAS3-CT97-0106, by the National Autonomous University of Mexico through a fellowship to Paulo Salles; by the Mellon Foundation through a grant to Dr. David G. Aubrey, and by the Rinehart Coastal Research Center who provided the publication costs. The views expressed herein are those of the authors and do not necessarily reflect the views of NOAA or any of its subagencies. The U.S. Government is authorized to produce and distribute reprints for governmental purposes notwithstanding any copyright notation that may appear hereon.

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## ANNEX A: Bathymetric Survey Coverage



Figure A.1 Bathymetric Survey Coverage in the New Ancão Inlet.



Figure A.2 Bathymetric Survey Coverage in the Main Channel.



Figure A.3 Bathymetric Survey Coverage in the Main (Farol) Inlet.



Figure A.4 Bathymetric Survey Coverage in the Armona Inlet.



Figure A.5 Bathymetric Survey Coverage in the Fuzeta Inlet.



Figure A.6 Bathymetric Survey Coverage in the Tavira Inlet.



Figure A.7 Bathymetric Survey Coverage in the Cacela Inlet.

ANNEX B: ADV Deployment Characteristics and Data Output

## **B.1: ADV Deployment Setup Specifications**

File -----> c:\sontek\data\india004.ADR FileSize (bytes) ----> 3909463 Number of Bursts in File --> 1426 Time of first Burst -----> 1999/02/03 14:00:01 Time of last Burst -----> 1999/02/13 11:24:01 ADV Hardware Configuration SoftwareVerNum -----> 6.7 Dsp SoftwareVerNum -----> 4.0 Electr. Board Rev. -----> SerialNumber -----> B126H Probe type -----> OCEAN PROBE Probe Orientation -----> UP CompassInstalled -----> YES RecorderInstalled -----> YES TempInstalled -----> YES PressInstalled ----> YES Pressure Scale -----> 0.000675 dbar/count Pressure Offset -----> -1.392810 dbar ExtSensorInstalled -----> NO ParosSensorInstalled -----> NO Transformation Matrix -----> 2.716 -1.355 -1.360 ----> 0.008 2.369 -2.375 ----> 0.344 0.345 0.345 **ADV Deployment Setup** DefaultTemp ----- (deg C) -> 15.00 DefaultSal ----- (ppt) ---> 35.00 DefaultSoundSpeed (m/s) ---> 1506.70 TempMode -----> MEASURED VelRange Index -----> 4 CoordSystem -----> ENU OutFormat -----> BINARY -----Sampling 1-----Sampling 2-----Sampling 3 Number of Bursts -> 1188 238 0 SampRate - (Hz) --> 0.20 2.00 0.00 BurstInterval (s)-> 720 3600 0 SamplesPerBurst --> 600 24 0 RecordAmpCorr ----> YES YES YES RecordCompass ----> YES YES YES RecordSensor ----> YES YES YES RecordStat -----> YES YES YES RecordExtSensor --> NO NO NO RecordParos -----> NO NO NO Bytes per Burst --> 626 13298 0 DeploymentName -----> INDIA Comments: None Figure B.1.1 ADV Deployment Setup Specifications.

## B.2: Raw Data



Figure B.2.1 ADV Pressure Data.

The previous figure shows the ADV-East (Cacela, offshore) pressure data. The line corresponds to "Sampling 1" (see table in Annex B.1) and the crosses correspond to "Sampling 2".











## ANNEX C: ADCP Survey Characteristics and Sample Data Output



Figure C.1.1 Deployment and Survey Locations.
## C.2 ADCP Instrument Configuration, Survey Lines and Selected ADCP Velocity Profiles

Figure C.2.1 ADCP Configuration File for the New Ancão Inlet Survey.

```
BEGIN RDI CONFIGURATION FILE
COMMUNICATIONS
ADCP
             ( ON COM1 9600 N 8 1 ) [ Port Baud Parity Databits Stopbits ]
             ( OFF COM2 9600 N 8 1 ) [ Port Baud Parity Databits Stopbits ]
ENSOUT
NAV
             ( ON
                   COM2 9600 N 8 1 ) [ Port Baud Parity Databits Stopbits ]
             ( OFF COM4 9600 N 8 1 ) [ Port Baud Parity Databits Stopbits ]
REFOUT
EXTERNAL
             ( OFF COM4 9600 N 8 1 ) [ Port Baud Parity Databits Stopbits ] }
ENSEMBLE OUT
ENS CHOICE (NNNNNNN) [Vel Corr Int %Gd Status Leader BTrack Nav]
ENS OPTIONS (NONE 1 3 1 3) [Ref First Last Start End]
ENS TYPE
             ( RAW ) [ RAW (default) or AVERAGED data transmitted ] }
ADCP HARDWARE
Firmware
               (8.25)
Angle
               (
                      20 )
Frequency
                    1200 )
               (
System
                   EARTH )
               (
Mode
                       1)
               (
                    DOWN )
Orientation
               (
Pattern
                  CONVEX ) }
               (
DIRECT COMMANDS
WS25
WF44
BX100
WN032
WD111100000
WP00010
BP008
WM4
TP000010
WV352
EX11111 }
RECORDING
Deployment ( NEWI )
           ( C )
Drive 1
Drive 2
           (
               C )
           (YES)
ADCP
Average
           (YES)
Navigation (YES ) }
CALIBRATION
ADCP depth
                                0.40 m
                            (
                                            )
Heading / Magnetic offset
                               0.00
                                        -5.50 deg )
                           (
                               0.00 deg
Transducer misalignment
                           (
                                           )
Intensity scale
                                0.43 dB/cts
Absorption
                               0.470 dB/m
                            (
Salinity
                                35.0 ppt
Speed of sound correction (
                                 YES
Pitch & roll compensation
                                 YES
                           (
Tilt Misalignment
                                0.00 deg
                            (
                                             )
Pitch_Offset
                                0.000 deg
                            (
                                              )
Roll Offset
                                0.000 deg
                            (
                                              )
Top discharge estimate
                                CONSTANT
                            (
                                             )
Bottom discharge estimate (
                                  POWER
                                             )
Power curve exponent
                            (
                                  0.1667
                                            )
Edge_slope coefficient
                              -1.00000 ) [-1=Trianglar(0.3535):-2=Square(0.91):User] }
```

## ADCP Configuration File for the New Ancão Inlet Survey (Cont.).

```
PROCESSING
Average every ( 0.00 s )
Depth sounder ( NO )
MaxFileSize ( 1200 )
Refout_info ( 1 8 30.00 1.000 0
                                           1) [bins:1st last, limit, weight, format,
delaysec]
External_formats (NNNNN) [HDT HDG RDID RDIE ]
External_decode (NNNN) [heading pitch roll temp ]
Start_Shore_distance ( 1500 ) [ cm ]
End_Shore_distance
                      (1000) [ cm ]
Edge_distance_prompt ( YES )
}
GRAPHICS
{
            ( SI )
Units
Velocity Reference (
                       BOTTOM
                               )
East Velocity
                   ( -300.0 300.0
                                    cm/s )
North_Velocity
                   ( -300.0 300.0
                                    cm/s )
Vert_Velocity
                     -30.0
                             30.0
                                    cm/s )
                   (
Error_Velocity
                   (
                     -10.0
                              10.0
                                    cm/s )
Depth
                         1
                               28
                                    bin )
Intensity
                          0
                               200
                                       dB)
Discharge
                     -1000
                              1000
                                   m3/s )
                   (
East_Track
                     -1523
                              1464
                                       m )
                   (
North Track
                     -1536
                             1451
                   (
                                       m)
Ship track
                   ( 1 bin 100.0
                                    cm/s )
Proj_Velocity
Proj_Angle
                   (-100.0 100.0 cm/s)
                       0.0 deg from N )
                   (
Bad_Below_Bottom
                      NO )
Linel
                   {
                                                                     )
Line2
                                                                     )
                   (
}
HISTORY
SOFTWARE
               ( BB-TRANSECT )
Version
               (2.80)
}
END RDI CONFIGURATION FILE
```



Figure C.2.2 New Ancão Inlet ADCP Survey Transects.



Figure C.2.3 Selected Velocity Profile, Transect A, New Ancão Inlet.



Figure C.2.4 Selected Velocity Profile, Transect B, New Ancão Inlet.



Figure C.2.5 Main Inlet ADCP Survey Transects.



Figure C.2.6 Selected Velocity Profile, Transect A, Main Inlet.



Figure C.2.7 Selected Velocity Profile, Transect B, Main Inlet.



Figure C.2.8 Selected Velocity Profile, Transect C, Main Inlet.



Figure C.2.9 Armona Inlet ADCP Survey Transects.



Figure C.2.10 Selected Velocity Profile, Transect A, Armona Inlet.



Figure C.2.11 Selected Velocity Profile, Transect B, Armona Inlet.



Figure C.2.12 Fuzeta Inlet ADCP Survey Transects.



Figure C.2.13 Selected Velocity Profile, Transect A, Fuzeta Inlet.



Figure C.2.14 Selected Velocity Profile, Transect B, Fuzeta Inlet.



Figure C.2.15 Tavira Inlet ADCP Survey Transects.



Figure C.2.16 Selected Velocity Profile, Transect A, Tavira Inlet.



Figure C.2.17 Selected Velocity Profile, Transect B, Tavira Inlet.

C-20

Note: Given the lack of recent bathymetry and the mobility of the inlet (as shown in Figure A.6), the production of a figure with the actual location of the transect superimposed to a image of the site was not possible.



Figure C.2.18 Selected Velocity Profile, Transect A, Cacela Inlet.

## C.3: ADCP Discharge Computations



Figure C.3.1 Transect A (1/1) Velocity and Discharge, New Ancão Inlet.



NEW INLET: Mean Cross-sectional Velocities for Transects B, (subsection 1 of 3).

Figure C.3.2 Transect B (1/3) Velocity and Discharge, New Ancão Inlet.



Figure C.3.3 Transect B (2/3) Velocity and Discharge, New Ancão Inlet.



Figure C.3.4 Transect B (3/3) Velocity and Discharge, New Ancão Inlet.



Figure C.3.5 Transect A (1/2) Velocity and Discharge, Main Inlet.



MAIN INLET: Mean Cross-sectional Velocities for Transects A, (subsection 2 of 2).

Figure C.3.6 Transect A (2/2) Velocity and Discharge, Main Inlet.



MAIN INLET: Mean Cross-sectional Velocities for Transects B, (subsection 1 of 3).

Figure C.3.7 Transect B (1/3) Velocity and Discharge, Main Inlet.





Figure C.3.8 Transect B (2/3) Velocity and Discharge, Main Inlet.



Figure C.3.9 Transect B (3/3) Velocity and Discharge, Main Inlet.



Figure C.3.10 Transect C (1/2) Velocity and Discharge, Main Inlet.



Figure C.3.11 Transect C (2/2) Velocity and Discharge, Main Inlet.



ARMONA INLET: Mean Cross-sectional Velocities for Transects A, (subsection 1 of 2).

Figure C.3.12 Transect A (1/2) Velocity and Discharge, Armona Inlet.



ARMONA INLET: Mean Cross-sectional Velocities for Transects A, (subsection 2 of 2).

Figure C.3.13 Transect A (2/2) Velocity and Discharge, Armona Inlet.



Figure C.3.14 Transect B (1/2) Velocity and Discharge, Armona Inlet.



ARMONA INLET: Mean Cross-sectional Velocities for Transects B, (subsection 2 of 2).





FUZETA INLET: Mean Cross-sectional Velocities for Transects A, (subsection 1 of 1).

Figure C.3.16 Transect A (1/1) Velocity and Discharge, Fuzeta Inlet.



FUZETA INLET: Mean Cross-sectional Velocities for Transects B, (subsection 1 of 1).

.



Figure C.3.17 Transect B (1/1) Velocity and Discharge, Fuzeta Inlet.


TAVIRA INLET: Mean Cross-sectional Velocities for Transects A, (subsection 1 of 6).

Figure C.3.18 Transect A (1/6) Velocity and Discharge, Tavira Inlet.



TAVIRA INLET: Mean Cross-sectional Velocities for Transects A, (subsection 2 of 6).

Figure C.3.19 Transect A (2/6) Velocity and Discharge, Tavira Inlet.



TAVIRA INLET: Mean Cross-sectional Velocities for Transects A, (subsection 3 of 6).

Figure C.3.20 Transect A (3/6) Velocity and Discharge, Tavira Inlet.



TAVIRA INLET: Mean Cross-sectional Velocities for Transects A, (subsection 4 of 6).

Figure C.3.21 Transect A (4/6) Velocity and Discharge, Tavira Inlet.



Figure C.3.22 Transect A (5/6) Velocity and Discharge, Tavira Inlet.



TAVIRA INLET: Mean Cross-sectional Velocities for Transects A, (subsection 6 of 6).

Figure C.3.23 Transect A (6/6) Velocity and Discharge, Tavira Inlet.

Time (h)



Figure C.3.24 Transect B (1/1) Velocity and Discharge, Tavira Inlet.



CACELA INLET: Mean Cross-sectional Velocities for Transects A, (subsection 1 of 1).



Time (h)

-60 L 

ANNEX D: Tidal Harmonic Analysis Results



Figure D.1 Harmonic Analysis and Admittance Technique Results.

The program outputs, for each tidal constituent, the amplitude (meters) and phases (degrees), AL and GL respectively and the same amplitudes and phases after nodal modulation and astronomical argument adjustments, A and G.

NUM	BER O	F VALID DATA =	913	AVERAGE	2 = 1.68	STANDARI	DEVIATION	N = .77	7
THE	ORETI	CAL RMS = .0	7 MAT	RIX CONDI	TION =	.33			
Brid	ige (1	Portugal)	GMT						
ANAJ	LYSIS	OF HOURLY TID	AL HEI	GHTS STN	8096 5H	21/ 1/99	) TO 16H 28	3/ 2/99	
NO.C	DBS.=	914 NO.PTS	.ANAL.	= 914 M	IIDPT=15H	9/ 2/99	SEPARATION	N =1.00	
NO	NAME	FREQUENCY	STN	M-Y/ M-Y	A	G	AL	$\operatorname{GL}$	
1	$\mathbf{Z0}$	.00000000	8096	199/ 299	1.6812	360.00	1.6812	360.00	
2	MM	.00151215	8096	199/ 299	.0093	164.59	.0093	327.18	
3	MSF	.00282193	8096	199/ 299	.0575	19.25	.0575	168.87	
4	ALP1	.03439657	8096	199/ 299	.0030	157.00	.0026	230.95	
5	2Q1	.03570635	8096	199/ 299	.0031	155.08	.0027	215.25	
6	Q1	.03721850	8096	199/ 299	.0140	299.17	.0122	162.74	
7	01	.03873065	8096	199/ 299	.0632	330.59	.0541	357.42	
8	NO1	.04026859	8096	199/ 299	.0020	207.07	.0019	164.77	
9	K1	.04178075	8096	199/ 299	.0678	93.24	.0619	185.14	
10	J1	.04329290	8096	199/ 299	.0072	188.98	.0065	88.79	
11	001	.04483084	8096	199/ 299	.0114	132.02	.0073	127.85	
12	UPS1	.04634299	8096	199/ 299	.0030	228.56	.0018	20.60	
13	EPS2	.07617731	8096	199/ 299	.0199	129.55	.0212	296.70	
14	MU2	.07768947	8096	199/ 299	.0529	145.75	.0550	117.18	
15	N2	.07899925	8096	199/ 299	.1669	72.69	.1724	31.76	
16	M2	.08051140	8096	199/ 299	.9710	79.73	1.0006	201.46	
17	L2	.08202355	8096	199/ 299	.0207	80.66	.0209	194.92	
18	S2	.08333334	8096	199/ 299	.3499	127.68	.3494	37.60	
19	ETA2	.08507364	8096	199/ 299	.0312	144.70	.0240	322.16	
20	MO3	.11924210	8096	199/ 299	.0112	220.61	.0098	9.18	
21	M3	.12076710	8096	199/ 299	.0046	329.41	.0048	331.87	
22	MK3	.12229210	8096	199/ 299	.0159	340.75	.0149	194.39	
23	SK3	.12511410	8096	199/ 299	.0077	52.65	.0070	54.48	
24	MN4	.15951060	8096	199/ 299	.0170	296.66	.0181	17.47	
25	M4	.16102280	8096	199/ 299	.0554	291.30	.0588	174.77	
26	SN4	.16233260	8096	199/ 299	.0058	346.30	.0060	215.30	
27	MS4	.16384470	8096	199/ 299	.0488	359.78	.0502	31.44	
28	S4	.16666670	8096	199/ 299	.0148	112.65	.0147	292.50	
29	2MK5	.20280360	8096	199/ 299	.0108	225.29	.0104	200.66	
30	2SK5	.20844740	8096	199/ 299	.0033	51.08	.0030	322.83	
31	2MN6	.24002200	8096	199/ 299	.0158	213.99	.0173	56.54	
32	M6	.24153420	8096	199/ 299	.0334	212.90	.0366	218.10	
33	2MS6	.24435610	8096	199/ 299	.0453	264.67	.0480	58.06	
34	2SM6	.24717810	8096	199/ 299	.0157	346.61	.0161	288.19	
35	3MK7	.28331490	8096	199/ 299	.0022	95.76	.0022	192.86	
36	M8	.32204560	8096	199/ 299	.0054	29.69	.0061	156.62	

#### Table D-1 Results for TG1

#### Table D-2 Results for TG2

NUM	BER OF	VALID DATA =	927	AVE	RAGE	= 2.07	STANDARI	DEVIATIO	V = .	74
THE	ORETICA	L RMS = .0	7 MAT	RIX CO	LIDNC	ION =	.33			
New	Inlet	(Portugal)	GMT	i -						
ANA	LYSIS O	F HOURLY TID	AL HEI	GHTS	STN	5078 1	7H 21/ 1/9	9 ТО 8Н 3	1/ 3/99	
NO.	OBS.=	928 NO.PTS	.ANAL.	= 92	28 MI	DPT= OH	10/ 2/99	SEPARATIO	N = 1.00	
							,			
NO	NAME	FREQUENCY	STN	M-Y/	M-Y	А	G	AL	GL	
1	Z0	.00000000	5078	199/	399	2.0774	.00	2.0774	.00	
2	MM	.00151215	5078	199/	399	.0193	186.15	.0193	343.84	
3	MSF	.00282193	5078	199/	399	.0367	2.72	.0367	143.20	
4	ALP1	.03439657	5078	199/	399	.0018	157.97	.0016	120.48	
5	201	.03570635	5078	199/	399	.0028	123.93	.0025	68.41	
6	Q1	.03721850	5078	199/	399	.0141	281.27	.0122	24.25	
7	01	.03873065	5078	199/	399	.0640	321.77	.0548	223.12	
8	NO1	.04026859	5078	199/	399	.0030	148.30	.0029	335.52	
9	K1	.04178075	5078	199/	399	.0669	83.14	.0611	39.67	
10	J1	.04329290	5078	199/	399	.0055	147.34	.0050	266.88	
11	001	.04483084	5078	199/	399	.0072	100.82	.0046	311.41	
12	UPS1	.04634299	5078	199/	399	.0027	227.92	.0017	229.83	
13	EPS2	.07617731	5078	199/	399	.0165	126.84	.0176	47.18	
14	MU2	.07768947	5078	199/	399	.0258	135.52	.0268	215.24	
15	N2	.07899925	5078	199/	399	.1616	57.37	.1670	120.49	
16	M2	.08051140	5078	199/	399	.9389	67.99	.9675	288.86	
17	L2	.08202355	5078	199/	399	.0156	89.66	.0157	298.16	
18	S2	.08333334	5078	199/	399	.3456	111.77	.3450	111.70	
19	ETA2	.08507364	5078	199/	399	.0251	130.18	.0193	32.00	
20	MO3	.11924210	5078	199/	399	.0078	205.09	.0069	327.32	
21	M3	.12076710	5078	199/	399	.0033	297.91	.0035	269.08	
22	МКЗ	.12229210	5078	199/	399	.0118	323.57	.0111	140.98	
23	SK3	.12511410	5078	199/	399	.0088	28.86	.0080	345.32	
24	MIN4	<b>.1</b> 5951060	5078	199/	399	.0072	255.90	.0076	179.90	
25	M4	.16102280	5078	199/	399	.0310	258.41	.0329	340.16	
26	SN4	.16233260	5078	199/	399	.0024	323.31	.0024	26.35	
27	MS4	.16384470	5078	199/	399	.0311	325.00	.0320	185.80	
28	S4	.16666670	5078	199/	399	.0094	72.22	.0093	72.06	
29	2MK5	.20280360	5078	199/	399	.0039	234.52	.0037	272.81	
30	2SK5	.20844740	5078	199/	399	.0013	324.46	.0012	280.85	
31	2MN6	.24002200	5078	199/	399	.0069	229.80	.0076	14.68	
32	M6	.24153420	5078	199/	399	.0096	239.08	.0105	181.71	
33	2MS6	.24435610	5078	199/	399	.0167	270.37	.0177	352.05	
34	2SM6	.24717810	5078	199/	399	.0086	318.94	.0088	179.66	
35	3MK7	.28331490	5078	199/	399	.0023	352.58	.0023	251.74	
36	<b>M</b> 8	.32204560	5078	199/	399	.0028	342.34	.0032	145.85	

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#### Table D-3 Results for TG3

<b>NTT TR (1</b>			011							
NUM	BER OF	VALID DATA =	911	AVE	RAGE	= 1.97	STAND	ARD DEVIATIO	ON = .79	1
THE	JRETICAL	L RMS = .0	6 MA'I	RIX CO	JND1.	$\Gamma ION =$	.33			
M. (	Channel	. (Portuga	GMT							
ANA	LYSIS O	F HOURLY TID.	AL HEI	GHTS	STN	3853 :	18H 21/	1/99 TO 171	H 28/ 2/99	l .
NO.	OBS.=	912 NO.PT	S.ANAL	.= 9	912	MIDPT=1	7H 9/	2/99 SEPARA	rion = 1.00	I.
NO	NAME	FREQUENCY	STN	M-Y/	M - Y	А	G	AL	$\operatorname{GL}$	
1	$\mathbf{Z}0$	.00000000	3853	199/	299	1.9739	360.00	1.9739	360.00	
2	MM	.00151215	3853	199/	299	.0298	183.76	.0298	345.27	
3	MSF	.00282193	3853	199/	299	.0256	325.04	.0256	112.62	
4	ALP1	.03439657	3853	199/	299	.0037	178.18	.0032	227.37	
5	201	.03570635	3853	199/	299	.0033	93.49	.0029	127.95	
6	01	.03721850	3853	199/	299	.0154	281.07	.0133	117.85	
7	01	.03873065	3853	199/	299	.0644	318.39	.0551	317.34	
8	NO1	.04026859	3853	199/	299	0013	197 68	0013	126 37	
9	К1	.04178075	3853	199/	299	0694	80 18	0633	142 00	
10	J1	04329290	3853	199/	299	0053	158 95	.0035	27 59	
11	001	04483084	3853	199/	299	0048	112 96	0031	76 51	
12	UPS1	04634299	3853	199/	200	.0040	2/9 20	.0031	6 00	
13	EDG5	07617731	3853	100/	200	.0033	104 02	.0020	0.00	
14	MIIOZ	07769947	2022	100/	299	.0114	110 44	.0122	217.13	
15	NO2	07900025	2022	100/	299	1764	E0 CC	.0230	34.94	
16	M2 M2	.07099925	2022	100/	299	1 0000	70.00	1 0207	320.86	
17	112	.00031140	2022	100/	233	1.0090	70.02	1.0397	133.79	
10	02 02	.00202355	2023	199/	299	.0221	92.80	.0222	148.00	
10	04 1700 10	.005333334	2023	199/	299	.3805	113.34	.3/99	323.27	
19	EIAZ MOD	.08507364	3853	199/	299	.0213	126.74	.0163	242.95	
20	MOS	.11924210	3853	199/	299	.0078	169.57	.0069	232.29	
21	M3	.120/6/10	3853	199/	299	.0053	290.91	.0055	206.42	
22	MK.3	.12229210	3853	199/	299	.0122	292.50	.0115	58.09	
23	SK3	.12511410	3853	199/	299	.0059	356.73	.0054	268.47	
24	MN4	.15951060	3853	199/	299	.0205	233.24	.0219	199.20	
25	M4	.16102280	3853	199/	299	.0687	241.49	.0729	9.02	
26	SN4	.16233260	3853	199/	299	.0102	278.07	.0106	30.19	
27	MS4	.16384470	3853	199/	299	.0548	302.31	.0563	216.00	
28	S4	.16666670	3853	199/	299	.0100	27.34	.0100	87.19	
29	2MK5	.20280360	3853	199/	299	.0059	171.51	.0057	.86	
30	2SK5	.20844740	3853	199/	299	.0014	28.00	.0013	149.67	
31	2MN6	.24002200	3853	199/	299	.0078	159.61	.0085	189.34	
32	M6	.24153420	3853	199/	299	.0189	167.02	.0207	358.32	
33	2MS6	.24435610	3853	199/	299	.0261	214.00	.0277	191.45	
34	2SM6	.24717810	3853	199/	299	.0071	267.98	.0072	31.59	
35	3 <b>M</b> K7	.28331490	3853	199/	299	.0028	292.40	.0028	185.52	
36	M8	.32204560	3853	199/	299	.0077	290.39	.0086	185.45	

#### Table D-4 Results for TG4

NUM	BER OF	VALID DATA	= 543	AVERAGE	= 1.36	STANDAR	D DEVIATION	J = .73	
THE	ORETIC	AL RMS = .:	15 MATI	RIX CONDI	TION =	.72			
Μ.	Inlet	(Portugal)	GMT						
ANA	LYSIS	OF HOURLY TI	DAL HEIG	GHTS STN	8711 12	2H 22/ 1/	99 TO 3H 14	1/ 2/99	
NO.	OBS.=	544 NO.PT	S.ANAL.:	= 544 M	IDPT=19H	2/ 2/99	SEPARATIO	J =1.00	
						, ,			
NO	NAME	FREQUENCY	STN	M-Y/ M-Y	A	G	AL	$\operatorname{GL}$	
1	ZO	.00000000	8711	199/ 299	1.3599	360.00	1.3599	360.00	
2	MSF	.00282193	8711	199/ 299	.0196	329.13	.0196	285.35	
3	01	.03873065	8711	199/ 299	.0679	319.11	.0580	112.66	
4	K1	.04178075	8711	199/ 299	.0738	74.87	.0673	113.46	
5	M2	.08051140	8711	199/ 299	.9902	67.14	1.0205	262.25	
6	S2	.08333334	8711	199/ 299	.3614	113.14	.3608	263.07	
7	<b>M</b> 3	.12076710	8711	199/ 299	.0057	268.59	.0059	201.12	
8	SK3	.12511410	8711	199/ 299	.0028	351.76	.0026	180.27	
9	M4	.16102280	8711	199/ 299	.0365	238.75	.0387	268.98	
10	MS4	.16384470	8711	199/ 299	.0333	309.82	.0342	294.86	
11	S4	.16666670	8711	199/ 299	.0085	17.71	.0085	317.56	
12	2MK5	.20280360	8711	199/ 299	.0036	176.56	.0034	245.39	
13	2SK5	.20844740	8711	199/ 299	.0019	73.31	.0017	51.75	
14	<b>M</b> 6	.24153420	8711	199/ 299	.0177	157.12	.0193	22.47	
15	2MS6	.24435610	8711	199/ 299	.0195	206.78	.0207	26.93	
16	2SM6	.24717810	8711	199/ 299	.0059	288.57	.0060	63.53	
17	3MK7	.28331490	8711	199/ 299	.0015	313.75	.0015	217.69	
18	M8	.32204560	8711	199/ 299	.0037	283.46	.0042	343.92	

#### Table D-5 Results for TG5

NUM	BER OF	VALID	DATA	= 887	AVE	RAGE	= 2.58	ST	ANDARD	DEVIATION	v = .	77
THE	DRETICA	AL RMS	= .	06 MAT	RIX CO	ONDI	CION =	.34				
Arma	ona (Po	ortugal	.)	GMT								
ANAI	LYSIS (	OF HOUF	LY TI	DAL HEI	GHTS S	STN	8712 14	н 22,	/ 1/99	TO 13H 28	3/ 2/99	
NO.C	DBS.=	888	NO.PT	S.ANAL.	= 88	38 M	IDPT= 1H	10/	2/99	SEPARATION	V = 1.00	
								,	_,			
NO	NAME	FREQ	UENCY	STN	M-Y/	M-Y	A		G	AL	$\operatorname{GL}$	
1	Z0	.000	00000	8712	199/	299	2.5845		.00	2.5845	.00	
2	MM	.001	51215	8712	199/	299	.0362	177	.21	.0362	334.36	
3	MSF	.002	282193	8712	199/	299	.0285	299	.61	.0285	79.07	
4	ALP1	.034	39657	8712	199/	299	.0021	111	.17	.0018	61.29	
5	2Q1	.035	570635	8712	199/	299	.0038	131	.29	.0033	62.91	
6	Q1	.037	21850	8712	199/	299	.0146	271	.48	.0127	1.06	
7	01	.038	373065	8712	199/	299	.0650	316	.50	.0556	203.90	
8	NO1	.040	26859	8712	199/	299	.0019	190	.11	.0018	2.86	
9	Kl	.041	78075	8712	199/	299	.0684	74	.96	.0625	16.45	
10	J1	.043	29290	8712	199/	299	.0061	139	.19	.0055	243.15	
11	001	.044	83084	8712	199/	299	.0027	112	.41	.0017	306.87	
12	UPS1	.046	34299	8712	199/	299	.0007	345	.99	.0005	331.21	
13	EPS2	.076	517731	8712	199/	299	.0077	98	.12	.0081	351.03	
14	MU2	.077	768947	8712	199/	299	.0149	115	.14	.0155	166.89	
15	N2	.078	399925	8712	199/	299	.1718	53	.19	.1775	87.87	
16	M2	.080	)51140	8712	199/	299	.9844	65	.34	1.0144	257.23	
17	L2	.082	202355	8712	199/	299	.0207	96	.02	.0208	274.99	
18	S2	.083	33334	8712	199/	299	.3687	107	. 92	.3681	77.85	
19	ETA2	.085	507364	8712	199/	299	.0129	125	.66	.0099	356.86	
20	MO3	.119	24210	8712	199/	299	.0052	231	.32	.0046	310.62	
21	M3	.120	76710	8712	199/	299	.0049	287	.45	.0051	215.15	
22	MK3	.122	29210	8712	199/	299	.0092	337	.87	.0087	111.25	
23	SK3	.125	511410	8712	199/	299	.0065	22	.35	.0059	293.76	
24	MN4	.159	951060	8712	199/	299	.0078		.97	.0083	227.55	
25	M4	.161	02280	8712	199/	299	.0128	319	.38	.0136	343.16	
26	SN4	.162	233260	8712	199/	299	.0035	41	.03	.0037	45.64	
27	MS4	.163	84470	8712	199/	299	.0239	18	.16	.0246	179.98	
28	S4	.166	566670	8712	199/	299	.0112	99	.51	.0112	39.36	
29	2MK5	.202	280360	8712	199/	299	.0045	204	.46	.0044	169.74	
30	2SK5	.208	344740	8712	199/	299	.0017	354	.75	.0015	236.09	
31	2MN6	.240	02200	8712	199/	299	.0095	173	.19	.0104	231.66	
32	Mб	.241	53420	8712	199/	299	.0208	172	.13	.0228	27.81	
33	2MS6	.244	135610	8712	199/	299	.0282	226	.36	.0299	220.06	
34	2SM6	.247	717810	8712	199/	299	.0086	308	.87	.0088	80.61	
35	3 <b>M</b> K7	.283	331490	8712	199/	299	.0009	107	.54	.0009	264.71	
36	M8	.322	204560	8712	199/	299	.0018	341	.77	.0020	29.34	

### Table D-6 Results for TG6

NUM	BER OF	VALID DATA	= 599	AVE	RAGE	= 2.18	STANDAR	D DEVIATION	N = .7	5
THE	ORETICA	L RMS =	.15 MAT	RIX CO	ONDIT	TION =	.81			
Olha	ao (Por	tugal)	GMT							
ANA	LYSIS O	F HOURLY T	IDAL HEI	GHTS	STN	8710 15H	4 22/ 1/9	9 TO 14H 16	5/ 2/99	
NO.0	OBS.=	600 NO.P	IS.ANAL.	= 60	00 M	DPT= 2H	4/2/99	SEPARATIO	N =1.00	
NO	NAME	FREQUENCY	Y STN	M-Y/	M-Y	А	G	AL	$\operatorname{GL}$	
1	Z0	.0000000	8710	199/	299	2.1848	.00	2.1848	.00	
2	MSF	.00282193	3 8710	199/	299	.0270	6.49	.0270	291.23	
3	01	.03873065	5 8710	199/	299	.0614	319.33	.0525	40.63	
4	K1	.04178075	5 8710	199/	299	.0698	77.86	.0637	10.19	
5	M2	.08051140	8710	199/	299	.9995	70.29	1.0301	86.90	
6	S2	.08333334	4 8710	199/	299	.3441	116.67	.3436	56.59	
7	M3	.12076710	8710	199/	299	.0079	296.44	.0082	321.21	
8	SK3	.12511410	8710	199/	299	.0045	23.62	.0041	255.88	
9	M4	.16102280	8710	199/	299	.0244	300.81	.0260	334.03	
10	MS4	.16384470	8710	199/	299	.0295	5.67	.0303	322.20	
11	S4	.16666670	8710	199/	299	.0092	88.75	.0092	328.60	
12	2MK5	.20280360	8710	199/	299	.0060	182.08	.0058	147.63	
13	2SK5	.20844740	8710	199/	299	.0009	29.91	.0008	202.08	
14	MG	.24153420	8710	199/	299	.0310	168.61	.0339	218.44	
15	2MS6	.24435610	8710	199/	299	.0326	222.16	.0345	195.30	
16	2SM6	.24717810	8710	199/	299	.0095	317.17	.0098	213.63	
17	3MK7	.28331490	8710	199/	299	.0015	88.73	.0015	70.89	
18	M8	.32204560	8710	199/	299	.0026	1.94	.0029	68.39	

#### Table D-7 Results for TG7

NUM	BER OF	VALID DA	TA =	819 AV	ERAGE	= .37	STAN	NDARD DEVIATI	ON = .6	6
THE	ORETIC	AL RMS =	.06	MATRIX	CONDI	TION =	.42			
Fuze	eta (P	ortugal)		GMT						
ANAI	LYSIS	OF HOURLY	TIDAL	HEIGHTS	STN	8709 11	H 25/	1/99 TO 13H	28/ 2/99	
NO.C	OBS.=	819 NO	.PTS.AN	NAL.=	819 M	IDPT=12H	11/2	2/99 SEPARATI	DN = 1.00	
								-,	2100	
NO	NAME	FREQUE	NCY S	STN M-Y	/ м-ч	A		G AL	$\operatorname{GL}$	
1	$\mathbf{Z}0$	.00000	000 87	709 199	/ 299	.3807	360.0	.380	7 360.00	
2	MM	.00151	215 87	709 199	/ 299	.0110	114.2	.011	252.35	
3	MSF	.00282	193 87	709 199	/ 299	.1077	24.8	32 .107	7 128.72	
4	ALP1	.03439	657 87	709 199	/ 299	.0018	120.0	.001	5 356.76	
5	2Q1	.03570	635 87	709 199	/ 299	.0045	151.4	44 .003	353.15	
6	Q1	.03721	850 87	709 199	/ 299	.0105	299.7	75 .009	L 280.37	
7	01	.03873	065 87	709 199	/ 299	.0641	335.2	.054	3 94.62	
. 8	NO1	.04026	859 87	709 199	/ 299	.0038	165.2	26 .003	7 190.72	
9	K1	.04178	075 87	709 199	/ 299	.0634	94.5	.057	9 229.61	
10	J1	.04329	290 87	709 · 199	/ 299	.0082	181.5	53 .007	3 100.02	
11	001	.04483	084 87	709 199	/ 299	.0112	123.3	.007	L 113.00	
12	UPS1	.04634	299 87	709 199	/ 299	.0046	211.3	35 .002	3 332.71	
13	EPS2	.07617	731 87	709 199	/ 299	.0172	174.0	.018	3 187.10	
14	MU2	.07768	947 87	709 199	/ 299	.0643	172.5	56 .066	7 325.42	
15	N2	.07899	925 87	709 199	/ 299	.1311	63.9	93 .135	1 183.23	
16	M2	.08051	140 87	709 199	/ 299	.8298	73.5	58 .855	L 331.03	
17	L2	.08202	355 87	709 199	/ 299	.0217	70.0	.021	295.56	
18	S2	.08333	334 87	709 199	/ 299	.2674	120.3	30 .267	120.22	
19	ETA2	.08507	364 87	709 199	/ 299	.0256	169.4	43 .019	7 48.72	
20	MO3	.11924	210 87	709 199	/ 299	.0118	305.4	48 .010-	1 322.32	
21	M3	.12076	710 87	709 199	/ 299	.0011	251.3	.001	L 97.36	
22	МКЗ	.12229	210 87	709 199	/ 299	.0144	54.7	73 .013	5 87.25	
23	SK3	.12511	410 87	709 199	/ 299	.0056	85.2	27 .005	L 220.26	
24	MN4	.15951	060 87	709 199	/ 299	.0335	67.5	.035	5 84.27	
25	M4	.16102	280 87	709 199	/ 299	.0660	77.2	.070	l 232.19	
26	SN4	.16233	260 87	709 199	/ 299	.0132	131.3	.013	7 250.58	
27	MS4	.16384	470 87	709 199	/ 299	.0588	121.8	.060	5 19.26	
28	S4	.16666	670 87	709 199	/ 299	.0152	194.0	.015	L 193.88	
29	2MK5	.20280	360 87	709 199	/ 299	.0082	318.6	58 .007	9 248.66	
30	2SK5	.20844	740 87	709 199	/ 299	.0009	133.1	.000	3 268.08	
31	2 <b>M</b> N6	.24002	200 87	709 199	/ 299	.0125	292.1	.013	7 206.34	
32	MG	.24153	420 87	709 199	/ 299	.0228	284.1	.024	336.52	
33	2MS6	.24435	610 87	709 199	/ 299	.0281	339.0	.029	3 133.90	
34	2SM6	.24717	810 87	709 199	/ 299	.0092	58.2	.009	5 315.58	
35	3MK7	.28331	490 87	709 199	/ 299	.0042	263.6	55 .0043	2 91.07	
36	<b>M</b> 8	.32204	560 87	709 199	/ 299	.0055	279.8	.006	2 229.69	

### Table D-8 Results for TG8

NT IM	BED OF 1	- גידעם מדדעי	572	AVEDA	CE - 1 /	C CTRANDAL		I_ 7C	
NUMBER OF VALUE DATA - 575 AVERAGE = 1.46 STANDARD DEVIATION = .76									
THEORETICAL RMS = .14 MATRIX CONDITION = .76									
Tav	ira (Po	rtugal)	GMT						
ANA	LYSIS O	F HOURLY TIDA	AL HEIG	GHTS S	STN 8713	12H 4/ 2/9	9 TO 9H 28	3/ 2/99	
NO.	OBS.=	574 NO.PTS	ANAL.=	= 574	MIDPT=10	H 16/ 2/99	SEPARATIO	J =1.00	
NO	NAME	FREQUENCY	STN	M-Y/ M	1-Y	A G	AL	$\operatorname{GL}$	
1	<b>Z</b> 0	.00000000	8713	299/ 2	99 1.452	5.00	1.4525	.00	
2	MSF	.00282193	8713	299/ 2	.057	9 266.05	.0579	250.07	
3	01	.03873065	8713	299/ 2	.99 .067	6 311.16	.0579	225.23	
4	K1	.04178075	8713	299/ 2	.066	1 71.88	.0604	232.13	
5	M2	.08051140	8713	299/ 2	99 1.021	9 62.14	1.0528	139.47	
6	S2	.08333334	8713	299/ 2	99 .391	0 100.29	.3904	160.21	
7	M3	.12076710	8713	299/ 2	.002	5 283.76	.0026	39.62	
8	SK3	.12511410	8713	299/ 2	.001	2 224.92	.0011	85.10	
9	M4	.16102280	8713	299/ 2	.024	9 206.48	.0265	1.15	
10	MS4	.16384470	8713	299/ 2	.021	2 283.20	.0218	60.45	
11	S4	.16666670	8713	299/ 2	.002	2 28.43	.0022	148.27	
12	2MK5	.20280360	8713	299/ 2	.000	2 154.27	.0002	109.20	
13	2SK5	.20844740	8713	299/ 2	.99 .001	0 21.03	.0009	301.13	
14	M6	.24153420	8713	299/ 2	99 .007	8 150.41	.0086	22.41	
15	2MS6	.24435610	8713	299/ 2	.011	1 204.61	.0117	59.20	
16	2SM6	.24717810	8713	299/ 2	.000	9 335.89	.0010	173.07	
17	3MK7	.28331490	8713	299/ 2	99 .000	3 151.32	.0003	183.58	
18	M8	.32204560	8713	299/ 2	99 .002	6 259.29	.0029	208.63	

Table D-9 Results for TG9

NUM	BER OF	VALID DATA =	571	AVERAGE	= 2.02	STANDARI	D DEVIATION	N = .5	2
THE	ORETICA	L RMS = .1	0 MATH	RIX CONDIT	ION =	.76			
Cac	ela (Po	rtugal)	GMT						
ANA	LYSIS O	F HOURLY TID.	AL HEIC	GHTS STN	5081 16H	4/ 2/9	9 TO 11H 28	3/ 2/99	
NO.	OBS.=	572 NO.PTS	.ANAL.=	= 572 MI	DPT=13H	16/ 2/99	SEPARATION	V =1.00	
NO	NAME	FREQUENCY	STN	M-Y/ M-Y	A	G	AL	$\operatorname{GL}$	
1	ZO	.00000000	5081	299/ 299	2.0407	.00	2.0407	.00	
2	MSF	.00282193	5081	299/ 299	.1147	34.05	.1147	15.03	
3	01	.03873065	5081	299/ 299	.0540	335.86	.0463	208.10	
4	K1	.04178075	5081	299/ 299	.0537	90.34	.0491	205.47	
5	M2	.08051140	5081	299/ 299	.6654	80.11	.6856	70.49	
6	S2	.08333334	5081	299/ 299	.2000	112.57	.1997	82.49	
7	MЗ	.12076710	5081	299/ 299	.0086	222.77	.0090	208.20	
8	SK3	.12511410	5081	299/ 299	.0050	276.57	.0046	1.63	
9	M4	.16102280	5081	299/ 299	.1771	112.85	.1880	93.61	
10	MS4	.16384470	5081	299/ 299	.1086	151.12	.1117	111.43	
11	S4	.16666670	5081	299/ 299	.0084	115.27	.0084	55.12	
12	2MK5	.20280360	5081	299/ 299	.0082	84.36	.0079	180.26	
13	2SK5	.20844740	5081	299/ 299	.0024	2.40	.0022	57.38	
14	M6	.24153420	5081	299/ 299	.0383	114.60	.0419	85.75	
15	2MS6	.24435610	5081	299/ 299	.0332	155.74	.0352	106.42	
16	2SM6	.24717810	5081	299/ 299	.0054	177.84	.0056	108.07	
17	3MK7	.28331490	5081	299/ 299	.0042	94.35	.0042	180.63	
18	M8	.32204560	5081	299/ 299	.0093	98.30	.0105	59.82	

Table D-10 Results for ADV

NUMB	ER OF	F VALID DATA =	213	AVERAGE	= -5.04	STANDAR	D DEVIATION	1 = .5	5
THEO	RETIC	CAL RMS = .2	1 MAT	RIX CONDIT	ION =	.97			
Offs	hore	(East, B.1)	GMT	ı					
ANAL	YSIS	OF HOURLY TIDE	AL HEI	GHTS STN	9001 15	H 4/ 2/9	9 TO 11H 13	/ 2/99	
NO.C	BS.=	213 NO.PTS	.ANAL.	= 213 MI	DPT= 1H	9/ 2/99	SEPARATION	I =1.00	
NO	NAME	FREQUENCY	STN	M-Y/ M-Y	А	G	AL	GL	
1	$\mathbf{Z}0$	.00000000	9001	299/ 299	5.0450	180.00	5.0450	180.00	
2	K1	.04178075	9001	299/ 299	.0386	77.48	.0352	19.95	
З	M2	.08051140	9001	299/ 299	.6971	53.49	.7183	221.00	
4	M3	.12076710	9001	299/ 299	.0075	336.90	.0078	228.02	
5	M4	.16102280	9001	299/ 299	.0173	147.22	.0184	122.24	
6	2MK5	.20280360	9001	299/ 299	.0013	314.65	.0013	232.14	
7	2SK5	.20844740	9001	299/ 299	.0037	169.93	.0034	52.26	
8	M6	.24153420	9001	299/ 299	.0040	72.40	.0044	214.93	
9	3MK7	.28331490	9001	299/ 299	.0022	276.90	.0022	1.91	
10	M8	.32204560	9001	299/ 299	.0020	78.54	.0022	28.58	

## ANNEX E: Atmospheric Pressure Data



Figure E.1 Atmospheric Pressure Data.

## ANNEX F: Electronic Data Format

The electronic data corresponds to the pressure data (tide gauges, ADV and atmospheric), bathymetric data and ADCP data collected in Portugal. Following is a description of the data format and structure. Each type of data is located in its own directory and in subdirectories when appropriate. Following details of the directory structure and file format for each data type.

### PRESSURE DATA

Main Directory: "PressureData"

The Pressure data is organised in subdirectories corresponding to each tide gauge and the ADV pressure sensor (see Table 4.1 and Figure C.1.1 for name and location of tide gauges). Each subdirectory contains two text files: one with the raw data (\*raw.dat) and the other with the pressure translated to water surface elevation and the atmospheric pressure removed. The water surface elevation is referred to the Hydrographic Datum (Z.H., 2 m below the Mean Sea Level). The water density used was 1,024.5 kg.m<sup>-3</sup>.

The format of the files is in columns as [year; month; day; hour; minute; second; pressure or water surface elevation (in meters of water)].

In addition, the atmospheric hourly data is contained in the subdirectory "Atmospheric". The format of this file is [year; month; day; hour; pressure (mbar); pressure (in equivalent meters of water)].

Note:

The water surface elevation appears not to be correct for some instruments. This is attributed to the poor quality and level of maintenance of some benchmarks used to survey the elevation of the pressure transducers.

### **BATHYMETRIC DATA**

Main directory: "Bathymetry".

The bathymetric data is in XYZ format and is separated in files corresponding to each survey.

Note:

The horizontal position of the survey in Cacela is included to provide information about the actual position of the inlet.

## ADV DATA

Main directory: "ADV".

The raw data is located in the "Raw" subdirectory and consists of two files for each sampling type. The sampling types (1 and 2) are described in Figure B.1.1.

The \*.HDR files contain the burst header information. Note that this file includes data when the instrument was out of the water. The format is the following:

Column #	Data Type and Units
1	Burst Number
2	Year – Time for start of first sample of burst
3	Month – Time for start of first sample of burst
4	Day – Time for start of first sample of burst
5	Hour – Time for start of first sample of burst
6	Minute – Time for start of first sample of burst
7	Second – Time for start of first sample of burst
8	Sampling rate (Hz)
9	Samples per burst
10	Recorder data byte
11	Sound speed (m/s)
12	Boundary range from probe tip (cm) (-0.01 if not detected)
13	Boundary range from center of sampling volume (cm; -0.01 if not detected)
14	Battery voltage
15	Mean signal strength, receiver 1 (counts)
16	Mean signal strength, receiver 2 (counts)
17	Mean signal strength, receiver 3 (counts)
18	Mean correlation, receiver 1 (percent)
19	Mean correlation, receiver 2 (percent)
20	Mean correlation, receiver 3 (percent)
21	Mean heading (°)
22	Mean pitch (°)
23	Mean rol (°)
24	Mean temperature (°C)
25	Mean pressure (dbar)
26	Standard deviation signal strength, receiver 1 (counts)
27	Standard deviation signal strength, receiver 2 (counts)
28	Standard deviation signal strength, receiver 3 (counts)
29	Standard deviation correlation, receiver 1 (percent)
30	Standard deviation correlation, receiver 2 (percent)
31	Standard deviation correlation, receiver 3 (percent)
32	Standard deviation heading (°)
33	Standard deviation pitch (°)
34	Standard deviation rol (°)
35	Standard deviation temperature (°C)
36	Standard deviation pressure (dbar)

#### Table F.6-11 \*.HDR File Type Format

The formatted data is contained in the subdirectory "Formatted" and has the time and mean velocity and pressure for each burst. The bursts for which the instrument was out of the water were removed.

The \*.TS files contain the velocity data corresponding to each sample of all the bursts recorded. The format is the following:

Column #	Data Type and Units
1	Burst Number
2	Sample number
3	Velocity East (cm.s <sup>-1</sup> )
4	Velocity North (cm.s <sup>-1</sup> )
5	Velocity Up (cm.s <sup>-1</sup> )
6	Amplitude, receiver 1 (counts)
7	Amplitude, receiver 2 (counts)
8	Amplitude, receiver 3 (counts)
9	Correlation, receiver 1 (percent)
10	Correlation, receiver 2 (percent)
11	Correlation, receiver 3 (percent)
12	Heading (°)
13	Pitch (°)
14	Rol (°)
15	Temperature (°C)
16	Pressure (dbar)

 Table F.6-12 \*.TS File Type Format

The water density used was 1,024.5 kg.m<sup>-3</sup>.

The format for the pressure files is:

[year; month; day; hour; minute; pressure (m of water)]

The format for the velocity files is:

[year; month; day; hour; minute; velocity east (cm.s<sup>-1</sup>); velocity north (cm.s<sup>-1</sup>); velocity up (cm.s<sup>-1</sup>)].

## ADCP DATA

Main directory: "ADCP".

The ADCP data is contained in 6 subdirectories, one for each inlet. The data relevant for each subsection is in turn divided in 6 files, with a common prefix and a common suffix, and is organised as follows:

- \* **bd\_** \*.dat files: depth (m) of the center of each bin with respect to the water surface.
- \* **bt\_**\*.**dat** files: depth of the seafloor for each ensemble.
- \* **ve\_** \*.**dat** files: east velocity (cm.s<sup>-1</sup>) for each bin (one ensemble per column).
- \* vn\_ \*.dat files: north velocity (cm.s<sup>-1</sup>) for each bin(one ensemble per column).
- \* x\_\*.dat files: x-position (UTM with WGS-84 datum) of each ensemble.
- \* **y\_**\*.dat files: y-position (UTM with WGS-84 datum) of each ensemble.

The prefix has the time of the beginning of the survey in HHMMSS.

The suffix has the name of the inlet and the subsection (e.g. A1, B3,...).

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REPORT DOCUMENTATION 1. REPORT NO. PAGE WHOI-2000-04	2.	3. Recipient's Accession No.
4. Title and Subtitle Tidal Observations at Ria Formosa Algarve Portugal		5. Report Date May 2000
Indal Observations at the Formosa, Algarve, Fortugar		6.
7. Author(s) Paulo Salles, Stephen P. O'Malley, George Voulgaris, Da	vid G. Aubrev	8. Performing Organization Rept. No.
A. Parterming Organization Name and Addrose		WHOI-2000-04
Woods Hole, Massachusetts 02543		11. Contract(C) or Grant(G) No. (C)
		(G)
12. Sponsoring Organization Name and Address		13. Type of Report & Period Covered
WHOI Sea Grant		Technical Report
Mast III Program UNAM		14.
15. Supplementary Notes This report should be cited as: Woods Hole Oceanog. Inst. Tech.	Rept., WHOI-2000-04.	
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18. Availability Statement	19. Security Class (This Re	port) 21. No. of Pages
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