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# REFLECTION OF A SHORT NARROW LIGHT PULSE FROM A SCATTERING AND ABSORBING OCEAN\*

Vladimir I. Haltrin

Naval Research Laboratory, Ocean Sciences Branch, Code 7331, Stennis Space Center, MS 39529-5004, USA  
Phone: 601-688-4528, fax: 601-688-5379, e-mail: <haltrin@nrlssc.navy.mil>

## ABSTRACT

A very simple analytical expression for the shape of a pulse reflected from scattering and absorbing seawater is obtained. The resulting equation can be used for algorithms connected with the rapid assessment of optical water properties from remote platforms.

## 1.0 INTRODUCTION

Even though there is a multitude of publications devoted to the propagation of a light pulse through a scattering and absorbing medium like seawater (see Refs. in Dolin and Levin, 1991), very few of them are practical enough to be used in real-time detection algorithms, mainly because of the complexity of the resulting equations. Instead, inadequate and oversimplified expressions are coded in many real detection programs. In this article an attempt is made to derive a very simple analytical expression for the spacial-temporal shape of a light pulse propagating in seawater. The resulting equation has a very simple form and depends parametrically on the characteristics of the emitter and detector, as well as the inherent optical properties of water.

### 1.1 Emitter and Detector Parameters

First, let us specify the parameters of an emitter and detector. For simplicity, a Lambert-Gaussian detector is assumed. Such a detector adequately emulates the majority of real detectors. The sensitivity of this detector is regarded as Lambertian, *i.e.*, it is independent of the angle of incidence of light. The sensitivity of the detector surface declines with the distance  $\rho$  from the center of the detector according to the Gaussian law:

$$T_D(\rho) = \frac{k_D}{4\rho^2} \exp\left(-\frac{\pi\rho^2}{4\rho_D^2}\right), \quad (1)$$

where  $\rho_D$  is the sensitivity radius which is defined by

$$\rho_D = \frac{2\pi}{k_D} \int_0^{\infty} T_D(\rho) \rho^2 d\rho, \quad (2)$$

and  $k_D$  is the detection efficiency of the receiver

$$k_D = 2\pi \int_0^{\infty} T_D(\rho) \rho d\rho. \quad (3)$$

We assume an emitter that is Gaussian both over the angle and over the distance from the center. It emits an infinitely short pulse represented by a temporal delta function. Such an assumption is mathematically convenient because the response from any arbitrary-shaped pulse can be calculated by mere convolution of the delta-shaped pulse response with the shape function of the real pulse (Morse and Feshbach, 1953). The energy density of the light pulse

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$$\Delta_1(\mathbf{r}, \mathbf{n}) = \frac{bf}{4\pi} \int_{\Omega_-} L_{p_1}(\mathbf{r}, \mathbf{n}) p_-(-\mathbf{nn}') d\mathbf{n}' + \frac{b(1-f)}{4\pi} \int_{\Omega_+} L_{p_2}(\mathbf{r}, \mathbf{n}) p_+(-\mathbf{nn}') d\mathbf{n}', \quad (21)$$

$$\Delta_2(\mathbf{r}, \mathbf{n}) = \frac{bf}{4\pi} \int_{\Omega_+} L_{p_2}(\mathbf{r}, \mathbf{n}) p_+(-\mathbf{nn}') d\mathbf{n}' + \frac{b(1-f)}{4\pi} \int_{\Omega_-} L_{p_1}(\mathbf{r}, \mathbf{n}) p_-(-\mathbf{nn}') d\mathbf{n}'. \quad (22)$$

## 2.2 Small-Angle Approximation

Let us choose the phase function components  $p_+$  and  $p_-$  in such a manner that their *tails* in the backward hemisphere are exponentially small, so that

$$|\Delta_1| \ll |Q_1| \quad \text{and} \quad |\Delta_2| \ll |Q_2|. \quad (23)$$

The resulting phase function from Eqn.(10) with its parts satisfying the inequalities above still gives us a very satisfactory approximation for a realistic ocean phase function (Haltrin, 1984).

Let us solve Eqns. (18) in the small-angle approximation (Wells, 1982; Walker, 1987; Arnush, 1972; Dolin and Levin, 1991) with the phase functions described above. We should also make the following simplifications that are typical for the small-angle approximation:

$$\left. \begin{aligned} \mathbf{n} = n_z + \mathbf{s}, \quad n_z \equiv (0, 0, 1 - s^2/2), \quad \mathbf{n} \nabla_r \equiv \left(1 - \frac{1}{2}s^2\right) \frac{\partial}{\partial z} + \mathbf{s} \nabla_\rho, \quad p_\pm(\mathbf{nn}') \rightarrow p_\pm(|\mathbf{s}'|), \\ \mathbf{nn}' = 1 - (\mathbf{n} - \mathbf{n}')^2/2, \quad \mathbf{n} - \mathbf{n}' = \mathbf{s}', \quad \mathbf{n}' = \mathbf{n} + (\mathbf{n}' - \mathbf{n}) = 1 + (\mathbf{s} - \mathbf{s}'), \\ L_{p_i}(\mathbf{r}, \mathbf{n}) \rightarrow L_{p_i}(z, \rho, \mathbf{s}), \quad L_{p_i}(\mathbf{r}, \mathbf{n}') \rightarrow L_{p_i}(z, \rho, \mathbf{s} - \mathbf{s}'). \end{aligned} \right\} \quad (24)$$

Now we have the approximate system of equations for the Laplace transforms of radiances:

$$\left[ \begin{aligned} \left(1 - \frac{1}{2}s^2\right) \frac{\partial}{\partial z} + \mathbf{s} \nabla_\rho + \varepsilon \right] L_{p_1}(z, \rho, \mathbf{s}) &= Q_1(z, \rho, \mathbf{s}), \\ -\left(1 - \frac{1}{2}s^2\right) \frac{\partial}{\partial z} - \mathbf{s} \nabla_\rho + \varepsilon \right] L_{p_2}(z, \rho, \mathbf{s}) &= Q_2(z, \rho, \mathbf{s}). \end{aligned} \right] \quad (25)$$

The Fourier transform of radiance in the plane that is orthogonal to the direction of the pulse propagation is:

$$L_{p_i}(z, \rho, \mathbf{s}) = \iint d\mathbf{k} d\mathbf{q} F_{p_i}(z, \mathbf{k}, \mathbf{q}) e^{-i\mathbf{k}\rho - i\mathbf{q}\mathbf{s}}, \quad (26)$$

$$F_{p_i}(z, \mathbf{k}, \mathbf{q}) = \frac{1}{(2\pi)^4} \iint d\rho ds L_{p_i}(z, \rho, \mathbf{s}) e^{i\mathbf{k}\rho + i\mathbf{q}\mathbf{s}}. \quad (27)$$

Now we have the following system of equations for the Laplace-Fourier transforms of the forward and backward radiances:

$$\left[ \begin{aligned} \left(1 - \frac{1}{2}s^2\right) \frac{\partial}{\partial z} - \mathbf{k} \frac{\partial}{\partial \mathbf{q}} + \varepsilon \right] F_{p_1}(z, \mathbf{k}, \mathbf{q}) &= V_+(\mathbf{q}) F_{p_1}(z, \mathbf{k}, \mathbf{q}) + V_-(\mathbf{q}) F_{p_2}(z, \mathbf{k}, \mathbf{q}), \\ -\left(1 - \frac{1}{2}s^2\right) \frac{\partial}{\partial z} + \mathbf{k} \frac{\partial}{\partial \mathbf{q}} + \varepsilon \right] F_{p_2}(z, \mathbf{k}, \mathbf{q}) &= V_+(\mathbf{q}) F_{p_2}(z, \mathbf{k}, \mathbf{q}) + V_-(\mathbf{q}) F_{p_1}(z, \mathbf{k}, \mathbf{q}), \end{aligned} \right] \quad (28)$$

where

$$V_\pm(\mathbf{q}) = \frac{b(1-f)}{4\pi} \int p_\pm(|\mathbf{s}|) e^{i\mathbf{q}\mathbf{s}} ds = \frac{b(1-f)}{2} \int_0^{\theta_{\max}} J_0(q\theta) p_\pm(\theta) d\theta, \quad (29)$$

and  $J_0$  is the zero-order Bessel function. Retaining only terms proportional to  $q^2$ , we get:

$$\left. \begin{aligned} V_+(q) &\equiv b(1-f) - b\langle\theta^2\rangle q^2/4, \\ V_-(q) &\equiv bf - b\langle(\pi-\theta)^2\rangle q^2/4, \end{aligned} \right\} \quad (30)$$

where the angular brackets  $\langle \dots \rangle$  denote averaging over the phase function given by Eqn. (10) according to the rule:

$$\langle x(\mu) \rangle = \frac{1}{2} \int_{-1}^1 p(\mu) x(\mu) d\mu. \quad (31)$$

Equations (28) for the light pulse components should satisfy the following boundary condition:

$$F_{p1}(z, \mathbf{k}, \mathbf{q}) \Big|_{z=0} = F_{p0}(\mathbf{k}, \mathbf{q}) = P_0 \exp\left(-\frac{\rho_E^2 \mathbf{k}^2}{\pi} - \frac{D_\theta \mathbf{q}^2}{4}\right). \quad (32)$$

Now we can estimate the terms in the left part of Eqn. (30) which are proportional to  $s^2$ :

$$\frac{1}{2} s^2 \frac{\partial}{\partial z} L_i \sim \langle\theta^2\rangle c L_i. \quad (33)$$

At the same time our corrections due to the phase function in Eqn (27) have the following order of magnitude:

$$\frac{b}{4} \langle\theta_\pm^2\rangle q^2 L_i \sim b \langle\theta^2\rangle \frac{1}{\langle\theta^2\rangle} L_i \sim b L_i. \quad (34)$$

So, if the condition  $\langle\theta^2\rangle \ll \omega_0$  holds, all terms which are proportional to  $s^2$  in the left part of Eqn. (28) may be neglected. With this in mind, Eqns. (24) acquire the following form:

$$\left. \begin{aligned} \left( \frac{\partial}{\partial z} - \mathbf{k} \frac{\partial}{\partial \mathbf{q}} + \alpha + \beta_1 q^2 \right) F_{p1}(z, \mathbf{k}, \mathbf{q}) - (bf - \beta_2 q^2) F_{p2}(z, \mathbf{k}, \mathbf{q}) &= 0, \\ -(bf - \beta_2 q^2) F_{p1}(z, \mathbf{k}, \mathbf{q}) + \left( -\frac{\partial}{\partial z} + \mathbf{k} \frac{\partial}{\partial \mathbf{q}} + \alpha + \beta_1 q^2 \right) F_{p2}(z, \mathbf{k}, \mathbf{q}) &= 0, \end{aligned} \right\} \quad (35)$$

where  $\alpha = a + bf + p/v$ ,  $\beta_1 = b \langle\theta^2\rangle / 4$  and  $\beta_2 = b \langle(\pi - \theta)^2\rangle / 4$ , and the boundary condition for Eqns. (35) is given by Eqn. (32).

Next, let us represent the downward pulse radiance as a sum of the unscattered part  $F_{p1}^Q$  (the source) and the scattered part  $F_{p1}^S$ :

$$F_{p1}(z, \mathbf{k}, \mathbf{q}) = F_{p1}^Q(z, \mathbf{k}, \mathbf{q}) + F_{p1}^S(z, \mathbf{k}, \mathbf{q}). \quad (36)$$

The backward pulse radiance consists only of scattered radiation  $F_{p2}(z, \mathbf{k}, \mathbf{q}) = F_{p2}^S(z, \mathbf{k}, \mathbf{q})$ . The unscattered forward pulse radiance  $F_{p1}^Q$  satisfies the following propagation equation:

$$\left( \frac{\partial}{\partial z} - \mathbf{k} \frac{\partial}{\partial \mathbf{q}} + \alpha + \beta_1 q^2 \right) F_{p1}^Q(z, \mathbf{k}, \mathbf{q}) = 0, \quad (37)$$

with the same condition on the boundary given by Eqn. (29). The solution to Eqn. (37) is given by the expression:

$$F_{p1}^Q(z, \mathbf{k}, \mathbf{q}) = F_p^0(\mathbf{k}, \mathbf{q} + \mathbf{k}z) \exp \left[ -\alpha z - \beta_1 \int_0^z (\mathbf{q} + \mathbf{k}\eta)^2 d\eta \right]. \quad (38)$$

This expression can also be represented by the following analytical formula:

$$F_{p1}^Q(z, \mathbf{k}, \mathbf{q}) = P_0 \exp \left[ -\frac{\rho_E^2 \mathbf{k}^2}{\pi} - \frac{D_\theta \mathbf{q}^2}{4} - \left( \alpha + \frac{D_\theta}{2} \mathbf{k}\mathbf{q} + \beta_1 \mathbf{q}^2 \right) z - \left( \frac{D_\theta}{4} \mathbf{k}^2 + \beta_1 \mathbf{k}\mathbf{q} \right) z^2 - \beta_1 \frac{\mathbf{k}^2}{3} z^3 \right]. \quad (39)$$

The scattered parts of the forward and backward radiances of the pulse are satisfied by the following equations:

$$\left. \begin{aligned} \left( -\frac{\partial}{\partial z} + \mathbf{k} \frac{\partial}{\partial \mathbf{q}} + \alpha + \beta_1 \mathbf{q}^2 \right) F_{p2}^s(z, \mathbf{k}, \mathbf{q}) &= (bf - \beta_2 \mathbf{q}^2) F_{p1}^Q(z, \mathbf{k}, \mathbf{q}), \\ \left( \frac{\partial}{\partial z} - \mathbf{k} \frac{\partial}{\partial \mathbf{q}} + \alpha + \beta_1 \mathbf{q}^2 \right) F_{p1}^s(z, \mathbf{k}, \mathbf{q}) &= (bf - \beta_2 \mathbf{q}^2) F_{p2}^s(z, \mathbf{k}, \mathbf{q}), \end{aligned} \right\} \quad (40)$$

with the boundary conditions

$$F_{p1}^s(z, \mathbf{k}, \mathbf{q}) \Big|_{z=0} = 0, \quad \lim_{z \rightarrow \infty} F_{pi}^s(z, \mathbf{k}, \mathbf{q}) = 0, \quad i = 1, 2. \quad (41)$$

The next step, according to the method given by Both (1929), Snyder (1949) and Romanova (1968), involves the following substitutions:

$$\mathbf{q} = \mathbf{g} - \mathbf{k}z, \quad F_{pi}^s(z, \mathbf{k}, \mathbf{q}) = F_{pi}^s(z, \mathbf{k}, \mathbf{g} - \mathbf{k}z) \equiv \Phi_{pi}^s(z, \mathbf{k}, \mathbf{g}), \quad (42)$$

which convert Eqns. (40) into the following one-dimensional system of two equations:

$$\left. \begin{aligned} \left[ -\frac{d}{dz} + \alpha + \beta_1 (\mathbf{g} - \mathbf{k}z)^2 \right] \Phi_{p2}^s(z, \mathbf{k}, \mathbf{g}) &= [bf - \beta_2 (\mathbf{g} - \mathbf{k}z)^2] F_{p1}^Q(z, \mathbf{k}, \mathbf{g} - \mathbf{k}z), \\ \left[ \frac{d}{dz} + \alpha + \beta_1 (\mathbf{g} - \mathbf{k}z)^2 \right] \Phi_{p1}^s(z, \mathbf{k}, \mathbf{g}) &= [bf - \beta_2 (\mathbf{g} - \mathbf{k}z)^2] \Phi_{p2}^s(z, \mathbf{k}, \mathbf{g}). \end{aligned} \right\} \quad (43)$$

The solutions to Eqns. (43) can be found with the help of the following two (forward,  $G_+$ , and backward,  $G_-$ ) Green functions (Vladimirov, 1971):

$$G_{\pm}(z, \mathbf{k}, \mathbf{g}) = H(\pm z) \exp \left[ \mp \alpha z \mp \beta_1 \int_0^z (\mathbf{g} - \mathbf{k}\eta)^2 d\eta \right], \quad (44)$$

which are solutions to the equations:

$$\left[ \pm \frac{d}{dz} + \alpha + \beta_1 (\mathbf{g} - \mathbf{k}z)^2 \right] G_{\pm}(z, \mathbf{k}, \mathbf{g}) = \delta(z), \quad (45)$$

where  $H(z)$  ( $H = 1$ , for  $z > 0$ ,  $H = 0$ , for  $z \leq 0$ ) is a Heavyside or step function (Morse and Feshbach, 1953).

The final solutions to Eqns. (43) are:

$$\Phi_{p2}^s(z, \mathbf{k}, \mathbf{g}) = \int G_-(z - \xi, \mathbf{k}, \mathbf{g}) [bf - \beta_2 (\mathbf{g} - \mathbf{k}\xi)^2] F_{p1}^Q(\xi, \mathbf{k}, \mathbf{g} - \mathbf{k}\xi) d\xi, \quad (46)$$

$$\Phi_{p1}^s(z, \mathbf{k}, \mathbf{g}) = \int G_+(z - \xi, \mathbf{k}, \mathbf{g}) [bf - \beta_2(\mathbf{g} - \mathbf{k}\xi)^2] \Phi_{p2}^s(\xi, \mathbf{k}, \mathbf{g}) d\xi + C_1(\mathbf{k}, \mathbf{g}) \exp\left[-\alpha z - \beta_1 \int_0^z (\mathbf{g} - \mathbf{k}\eta)^2 d\eta\right], \quad (47)$$

where  $C_1(\mathbf{k}, \mathbf{g})$  is an arbitrary function that is determined by the boundary condition.

After simplification, we obtain the following expressions for  $F_{pi}$ :

$$F_{p1}(z, \mathbf{k}, \mathbf{q}) = F_p^0(\mathbf{k}, \mathbf{q} + \mathbf{k}z) \exp[-\alpha z - \beta_1 \int_0^z (\mathbf{q} + \mathbf{k}\eta)^2 d\eta] \left\{ 1 + \int_0^z d\xi [bf - \beta_2(\mathbf{q} - \mathbf{k}\xi)^2] \times \right. \\ \left. \times \exp[-\beta_1 \int_{\xi-z}^z (\mathbf{q} + \mathbf{k}\eta)^2 d\eta] \int_{-\infty}^0 d\zeta [bf - \beta_2(\mathbf{q} - \mathbf{k}\xi + \mathbf{k}\zeta)^2] \exp[2\alpha\zeta - \beta_1 \int_{\zeta}^{\xi-\zeta} (\mathbf{q} - \mathbf{k}\eta)^2 d\eta] \right\}, \quad (48)$$

$$F_{p2}(z, \mathbf{k}, \mathbf{q}) = F_p^0(\mathbf{k}, \mathbf{q} + \mathbf{k}z) e^{-\alpha z} \int_{-\infty}^0 d\xi [bf - \beta_2(\mathbf{q} - \mathbf{k}z + \mathbf{k}\xi)^2] \exp[2\alpha\xi - \beta_1 \int_{\xi}^{z-\xi} (\mathbf{q} - \mathbf{k}\eta)^2 d\eta]. \quad (49)$$

### 2.3 Detector Response to the Infinitely Short Laser Pulse Reflected from Water

After the integration of the received radiances over the sensitive area of the detector, the relative (normalized by the pulse power  $P_0$ ) response of the detector placed at the depth  $z$  will be

$$\eta_1(z, w) = \frac{\delta(w) v e^{-\alpha(w+z)}}{1 + \left(\frac{\rho_0}{\rho_A}\right)^2 \left[1 + \frac{4D_1\sigma_0}{3s_0^2}\right] \frac{s_0 z}{\rho_A}} + \int_0^z \frac{\theta(w) (\beta \rho_A)^2 v e^{-\alpha(w+z)} d\xi}{2a_1 + 2D_2(2\xi^2 - w\xi) + D_1\sigma_0 \left(\frac{4\xi^3}{3} + 2w\xi^2 - w^2\xi\right)}, \quad (50)$$

where

$$a_1 = \rho_A^2 + \rho_0^2 + s_0^2 z^2 + D_2 w^2 + \frac{D_1 \sigma_0}{3} (4z^3 + w^3), \quad w = vt - z, \quad (51)$$

$$\left. \begin{aligned} \eta_2(z, w) &= \frac{\beta v}{2D_w} \theta(w) \exp[-\alpha(w+z)], \\ D_w &= 1 + \left(\frac{\rho_0}{\rho_A}\right)^2 + D_2 \left(1 + \frac{D_1 \sigma_0 w}{3D_2}\right) \left(\frac{w}{\rho_A}\right)^2 + \left(1 + \frac{4D_1 \sigma_0}{3s_0^2} z\right) \left(\frac{s_0 z}{\rho_A}\right). \end{aligned} \right\} \quad (52)$$

At  $z = 0$ , the detector response to the reflected pulse will be:

$$\eta_2(\tau) = \frac{a_0 \theta(\tau) e^{-\tau}}{1 + a_2 \tau^2 + a_3 \tau^3}, \quad (53)$$

where

$$\tau = t/t_0, \quad t_0 = (\alpha v)^{-1}, \quad a_0 = \frac{8\pi^7 \omega_0 f}{[1 - \omega_0(1-f)] [1 + (\rho_E / \rho_D)^2]}, \quad (54)$$

$$a_2 = \frac{\pi D_2}{8c^2 (\rho_E^2 + \rho_D^2) [1 - \omega_0(1-f)]^2}, \quad a_3 = \frac{\pi \omega_0 (1-f) D_1}{24c^2 (\rho_E^2 + \rho_D^2) [1 - \omega_0(1-f)]^3}, \quad (55)$$

where  $f$  is the weight coefficient in Eqn. (10).

The values of  $\eta_2$  calculated according to Eqns. (53)-(55) were compared with the results computed with the Monte Carlo code by Kattawar (1992). The discrepancies between the natural logarithms of the  $\eta_2$  computed by both these methods for inherent optical properties and phase functions by Petzold (1972) do not exceed 15%.

### 3.0 CONCLUSIONS

Relatively simple analytical equations derived in a small-angle scattering approximation have been obtained for the infinitely short light pulse reflected by seawater. These equations depend on the inherent optical properties of seawater, as well as the parameters of the pulse and receiver. They can be transformed into equations for an arbitrarily-shaped pulse by a simple convolution procedure. The logarithmic precision of these equations is estimated to be in the range of 15%. The results of this paper can be used for algorithms connected with the rapid assessment of water properties from remote airborne and shipborne platforms.

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