Report No. CG-D-16-98

## Investigation of Grade E Cargo Flammability

Engineering Computer Optecnomics, Inc. 1356 Cape St. Claire Road Annapolis, MD 21401-5216

and

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16. Abstract This research indicates that certain Grade E cargoes can ignite at temperatures below their flash point if they are first heated above their flash point, allowed to cool and then reheated. Ignition and chromatographic studies were performed on two No. 6 oils meeting Grade E cargo requirements to determine if they exhibit below flash point ignition behavior. Their flash points were obtained by the Pensky-Martens Closed Cup Method (ASTM Method D93). This was followed by tests to determine whether these oils could ignite at temperatures below their flash point. In addition, chromatographic analyses were performed on the bulk oils and their vapors to determine whether significant fractionation of light components was occurring. Chromatographic analyses comparing the bulk oils and their vapors(after heating, cooling, heating cycle) showed no evidence of preferential fractionation of the lighter components of the oil, a potential cause of the below flash point behavior. However, these analyses did indicate significant differences in the chemical composition of the two oils, which may affect differing ignition behavior. Significant mist formation in the vapor space was observed to occur just before ignition.					
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#### **EXECUTIVE SUMMARY**

Instances where Grade E cargo have ignited at temperatures apparently below their flash points have been documented by the U.S. Coast Guard. Most of the cases can be attributed to local heating to temperatures above the flash point. But, several instances have not been attributable to other causes.

The current study builds on earlier research indicating that certain Grade E cargos, e.g. some No. 6 oils, can ignite at temperatures below their flash point if they are first heated to temperatures above their flash point, allowed to cool and then reheated below their flash points. Ignition and chromatographic studies were performed on two No. 6 oils meeting Grade E cargo requirements to determine if they exhibit below flash point ignition behavior.

One of the test oils did ignite consistently below its measured flash point after a heating, cooling, heating progression. However, the difference between the ignition temperature and the measured flash point was within the reproducibility of the ASTM closed cup flash point procedure. The other test oil did not ignite below its flash point.

Chromatographic analyses comparing the bulk oils and their vapors (after a heating, cooling, heating cycle) showed no evidence of preferential fractionation of the lighter components of the oil, one possible cause of below flash point behavior. However, these analyses did show significant compositional differences between the two test oils, which may be related to their differing ignition behavior.

Significant mist formation in the vapor space was observed to occur just before ignition. This may also be related to the below flash point ignition behavior.

Refinements to the experimental equipment are recommended to better isolate and discriminate among potential causes of below flash point ignition behavior. Tests with a wider range of Grade E cargos are also needed to determine the extent of this behavior as well as its mechanism.

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#### **1.0 BACKGROUND**

Grade E cargo is defined in the Code of Federal Regulations (CFR) as a combustible liquid having an open cup flash point of 150°F (65.5°C) or higher.<sup>1</sup> Common Grade E cargoes include No. 6 fuel oil, asphalt, lubricating oil, animal and vegetable oils, and oily waste water.

Inerting the atmosphere over Grade E cargos carried in bulk on vessels is not required by the Code of Federal Regulations. This is apparently based on the belief that the heating of these cargos (which is necessary for handling) will not raise the temperature of the cargos above their flash point.

Reference 2 searched the U.S. Coast Guard (USCG) CASMAIN database for fires resulting from ignition of Grade E cargo at temperatures below the cargo's flash point. A total of eight incidents from November 1977 to March 1990 were found. The USCG and National Transportation Safety Board (NTSB) reports of these incidents were reviewed. Four of these incidents involved residual fuel oils, two involved oily wastewater, and one each involved asphalt and sewage sludge. Most of these fires could be explained by either (a) small quantities of low flash point contaminants mixed in with the Grade E cargo, or (b) localized heating above the flash point by open flames. Contamination with low flash point materials could result in a mixture of low flash point vapors that could ignite at temperatures below the flash point of the bulk cargo. Heating with an open flame, e.g., welding, could result in localized regions where the flash point of the cargo is exceeded. However, several of the incidents investigated do not have a clear explanation and may be the result of below flash point ignition.

The U.S. Coast Guard conducted earlier research<sup>2-4</sup> in an effort to quantify the problem and to identify potential monitoring devices that could be useful in alerting vessel crews of a potentially hazardous situation. This research identified that the Grade E cargos that possess the most potential for explosive atmospheres are petroleum derivatives such as residual fuel oils and asphalts.<sup>3</sup> Research to date indicated that standard combustible gas indicators were unsatisfactory in detecting the hazards posed by Grade E cargo.

However, research with a 2.25 cubic foot rectangular test tank did show evidence of below flash point Grade E oil ignition.<sup>3</sup> The oil studied did not ignite as it was heated to its flash point even though a spark ignition source was periodically applied. The oil did explode above its flash point, as expected. But, a spark applied after the oil had cooled to well below its flash point resulted in a second explosion. Normally, combustible materials do not ignite or explode below their flash point.

This behavior indicates an ignition mechanism different than occurs with an open or closed cup flash point tester. In flash point measurements, ignition theoretically occurs when the concentration of combustibles in the vapor, in equilibrium with the heated liquid, reaches a critical level. Below this temperature, combustion is not supported. However, the experiment described above does not appear to conform to this expected behavior.

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Below flash point ignition behavior may be due to a variety of reasons, including:

- Not attaining equilibrium conditions during the open/closed cup flash point measurements
- Separation of the fuel into components with higher and lower flash points
- Preferential vaporization of organic components with different flash points
- Some other mechanism for ignition

This behavior is not a concern with cargos other than Grade E materials because the atmosphere over lighter cargos is inerted. But Grade E cargos are not considered sufficiently ignitable to warrant this safety protection at this time.

#### 2.0 APPROACH

The current study was designed to extend the research conducted earlier.<sup>3</sup> Three Grade E oils were obtained from industrial sources for this study. Their flash points were obtained by the Pensky-Martens Closed Cup Method (ASTM Method D93).<sup>5</sup> This was followed by tests in the 2.25 cubic foot test chamber, mentioned earlier, to determine whether these oils would ignite at temperatures below their flash point. In addition, chromatographic analyses were performed on the bulk oils and their vapors to determine whether significant fractionation of light components was occurring.

#### 3.0 RESULTS AND DISCUSSION

#### 3.1 Test Oils

Three No. 6 oils, all meeting Grade E cargo requirements, were obtained for this project from the following sources:

Sample 1 -	Amerada Hess Corporation		
Sample 2 -	The Somerset Refinery, Inc.		
Sample 3 -	Colonial Oil Industries, Inc.		

The Material Safety Data Sheets (MSDS) for these oils are provided in Appendix A.

#### 3.2 Flash Point Measurements

The closed cup flash points of these oils were obtained in accordance with the Pensky-Martens method. For this project, the flash point for each oil was determined twice in accordance with ASTM Method D93. The two flash points were then averaged.

The closed cup flash point of Sample 1 could not be determined due to its high water content. As an alternative, a Cleveland Open Cup Flash and Fire Point (ASTM Method D92) was conducted on this oil. The open cup flash point was  $163 \degree C (315 \degree F)$ . ASTM reports the reproducibility of this method to be  $\pm 17 \degree C (30 \degree F)$ . The fire point was  $202 \degree C (396 \degree F)$  with a reproducibility, reported by ASTM, of  $\pm 14 \degree C (25 \degree F)$ . The high water content in this No. 6 oil (not an unusual occurrence) and the resultant inability to obtain a closed cup flash point made this oil unsuitable for the ensuing experiments.

The closed cup flash points for Samples 2 and 3 were as follows:

Sample 2 - 81.1°C (178°F) Sample 3 - 99.4°C (211°F)

ASTM reports the reproducibility of the closed cup method to be  $\pm 10^{\circ}$ C (18°F).

#### 3.3 Ignition Tests

Samples 2 and 3 were then subjected to experimentation in the ignition test chamber utilized in the earlier studies and described in detail in Reference 3. Electrical resistance heaters controlled by a single thermostat were attached to the outside of the test chamber to heat the oil. Two thermocouples were placed in the bulk oil and two thermocouples were placed in the vapor space above the bulk oil. A temperature read-out was used to monitor the temperatures in the test chamber. Ignition sparks were provided by a spark plug inserted through the top of the chamber into the vapor space.

A general protocol was developed for these experiments. For each test, the chamber would be filled with the test oil to either 25% or 75% of capacity. When the test chamber was filled to 25% of capacity (about 3 inches deep), the two thermocouples in the bulk oil were placed approximately 1-1/2 inches from the bottom. The two vapor space thermocouples were placed approximately 6 inches from the top of the chamber. The spark plug was also placed at this level. When the test chamber was filled to 75% of capacity (9 inches depth) the bulk oil thermocouples were placed approximately 3 inches from the bottom. The vapor space thermocouples and the spark plug were placed approximately 2 inches from the top of the chamber.

The oil was heated by the electrical resistance heaters to approximately  $11^{\circ}C$  ( $20^{\circ}F$ ) above its measured flash point. The heaters were then shut off and the oil allowed to cool to approximately  $11^{\circ}C$  ( $20^{\circ}F$ ) below its measured flash point. At this point, the spark plug was discharged to see if ignition would result. If not, the temperature would be raised  $3^{\circ}C$  ( $5^{\circ}F$ ) and ignition was attempted (using the spark plug as the ignition source) again. The temperature was elevated in  $3^{\circ}C$  ( $5^{\circ}F$ ) increments until ignition did occur. Efforts were made to have the vapor space be at about the same temperature as the pool of oil in the bottom of the test chamber.

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However, the very different heat capacities of the vapor compared to the liquid oil made this goal very difficult. During heating and cooling cycles, the vapor changed temperature much more rapidly than the liquid oil. The heaters were turned on periodically during the heating and cooling cycles in an attempt to keep temperatures as uniform as possible. This technique worked fairly well, especially after the operators became experienced at it.

The temperatures at which oil Sample 2 (flash point 81.1°C, 178°F) ignited are summarized in Table 1. The bulk oil and head space ignition temperatures are the average of the two thermocouple readings in the bulk oil and the two thermocouple readings in the vapor space. The results are listed in the order in which the experiments were conducted.

## Table 1Ignition Tests with No. 6 Oil - Sample 2

Amt. Of Oil, % of <u>Chamber Capacity</u>	Ignition Tem Bulk Oil	perature, °C (°F) Vapor Space	Comments
25%	75.2°C (167°F)	75.6°C (168°F)	Orange-blue flame
25%	75.6°C (168°F)	77.0°C (171°F)	Blue-orange flame
25%	75.9°C (169°F)	74.7°C (166°F)	Orange-blue flame (less intense than earlier)
75%	75.2°C (167°F)	75.6°C (168°F)	Orange-blue flame

The ignition measurements on Oil Sample 2 were remarkably consistent. In all four experiments, ignition occurred below the flash point by about  $5.6^{\circ}C$  (10°F). This tends to support the contention that this oil can ignite below its flash point after being heated above the flash point, allowed to cool, and then reheated slowly. However, the reproducibility of the closed flash point method, as stated by ASTM, is  $\pm 10^{\circ}C$  (18°F). The test oil ignition temperature deviated from the closed cup flash point by less than the method's stated reproducibility. But, these data are certainly indicative of below flash point ignition.

A visual inspection of the vapor space was performed during the last two experiments before ignition (using the results of the first two experiments as a guide). The test chamber cover was lifted slightly in an attempt to observe whether significant mist formation was occurring. At temperatures below the point where ignition occurred, there was little or no mist formation in the vapor space. At the temperature where ignition occurred, mist formation was significant, essentially filling the vapor space with a smoky mist. This mist formation just prior to ignition

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was observed in the two experiments where it was checked. Mist formation may be an important factor in below flash point ignition by increasing the fuel-air interfacial surface area. This large surface area may allow for combustion with lower energy input, i.e. at lower temperatures.

Table 2

The temperatures at which oil Sample 3 (flash point 99.4°C, 211°F) ignited are summarized in Table 2. The results are listed in the order in which the experiments were conducted.

Amt. Of Oil, % of <u>Chamber Capacity</u>	<u>Ignition Tem</u> <u>Bulk Oil</u>	<u>Comments</u>	
75%	104°C (220°F)	111°C (232°F)	Heavy smoke before ignition; orange flame
75%	110°C (231°F)	116°C (240°F)	Blue-orange flame
25%	102°C (216°F)	96.4°C (206°F)	Blue-orange flame; some surface burning
25%	98.3°C (209°F)	113°C (235°F)	Orange-blue flame

As with oil Sample 2, the results are rather consistent among the four experiments. But, with oil Sample 3, the ignitions occurred above the measured flash point in all cases. Thus, this oil did not exhibit any below flash point ignition behavior. Mist formation was not checked during these experiments, which were performed before the tests with Sample 2.

#### 3.4 Chromatographic Analyses

Chromatographic analyses were performed to provide data on whether enhanced vaporization of the light ends of the test oils was occurring. If so, this could help explain the observed below flash point ignition of oil Sample 2. Chromatograms were obtained on both liquid test oils. Then the two oils were subjected to the same thermal progression as performed during the ignition experiments discussed above. The thermal treatment for the chromatographic analyses were performed in a small test chamber with a septum for withdrawal of a headspace sample. The test chamber was filled to 25% capacity with each test oil. Chromatograms of the headspace samples were obtained and compared with the chromatograms of the bulk oils to see if the lighter ends, especially for oil Sample 2, were vaporized preferentially.

The bulk oil samples were analyzed chromatographically by direct injection using a flame ionization detector. The chromatographic conditions were based on ASTM D2887 procedures. Standards of a reference No. 6 fuel oil and a calibration solution mixture were analyzed along with the samples. These standards provided a reference for the sample oils' peak patterns and provided some hydrocarbon peaks for comparison.

Figures 1 and 2 are the chromatograms of the bulk oil and vapor space for oil Sample 2. This is the oil that ignited below its measured flash point. These chromatograms are remarkably consistent in terms of both peak pattern and intensity. Thus, these chromatograms show no evidence of preferential vaporization of the lighter fractions of the oil.

Figures 3 and 4 are the chromatograms of the bulk oil and vapor space for oil Sample 3. This is the oil that did not ignite below its measured flash point. The peak pattern of the vapor space is quite similar to that of the bulk oil. However, the intensity of the peaks in the vapor space chromatogram changed significantly compared to the bulk oil chromatogram. The peak pattern and intensity of the two chromatograms were very similar up to the range of undecane (C11). Following this, the concentrations of the peaks in the vapor space sample chromatogram were increasingly intense through the eicosane (C20) range. If anything, the concentration of heavier ends increased in the vapor space sample, compared to the bulk oil.

The peak pattern and peak areas for oil Sample 3 corresponded with the peak pattern of the No. 6 fuel oil reference standard. However, the peak pattern and peak areas for oil Sample 2 did not correspond with the reference. This sample had a consistent peak "spiking" pattern of hydrocarbons, but was lacking the peak components in the main region of the No. 6 reference fuel oil pattern. Sample 2's peak pattern was similar to the reference up to the tetradecane (C14) range and after octacosane (C28). Between C24 and C28, the reference oil's pattern was not evident.

The chromatography results indicate significant compositional differences between oil Samples 2 and 3. These compositional differences may be relevant in the differing ignition of the two oil samples.

#### 3.5 Discussion

The ignition tests provide strong, but not conclusive, evidence of below flash point ignition behavior with oil Sample 2. Such behavior was not observed with oil Sample 3. Clearly, Sample 2 consistently ignited about 5.6°C (10°F) below its measured flash point after being heated above its flash point, allowed to cool, and then reheated with periodic ignition attempts. However, ASTM reports the reproducibility of its closed cup flash point method to be  $\pm 10^{\circ}$ C (18°F). Thus, the ignition behavior of Sample 2 is within its ASTM reproducibility.

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The comparative chromatographic analyses of the oil samples and their vapors showed no indication of preferential fractionation of the light ends of either of the oils. But, the chromatographic analyses did indicate significant compositional differences between the two test oils which may be relevant to their differing ignition behavior.

Significant mist formation was observed in the vapor of Sample 2 just before ignition. This may be related to the observed below flash point ignition but more investigation is required.

The test apparatus worked well but a number of improvements are needed to provide data to better determine whether below flash point ignition is a real phenomenon under certain conditions and, if so, its mechanism. Recommended improvements include:

- Separate heating controls for the vapor space and the bulk oil heaters to provide more consistent temperature control in the two regions
- Controllers capable of finer temperature control in both the vapor space and the bulk oil
- Quantitative mist detector in the vapor space
- Oxygen concentration monitor in the vapor space
- Additional thermocouples to better characterize thermal gradients in the vapor space and the bulk oil
- Chromatographic analyses be expanded to include Hydrogen Sulfide  $(H_2S)$

Finally, it must be recognized that the behavior of two oil samples can not be extrapolated reliably to characterize the behavior of the many Grade E oil cargos carried in commercial ships. Ignition tests and chromatographic analyses are needed on a much wider range of Grade E products to characterize the extent of below flash point ignition and the conditions under which it may occur.



#### UNDERWRITERS LABORATORIES



Figure 1 Chromatogram of Bulk Oil Sample 2



#### UNDERWRITERS LABORATORIES



Figure 2 Chromatogram of Oil Sample 2 Vapor Source

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REPORT FUELCIL

Date Processed 02/03/98 05:01:43 PM

Millenium Results Report:

SampleName Fuel Oil #3 Headspace

Figure 3 Chromatogram of Bulk Oil Sample 3

-10-

 Millenium Results Report:
 REPORT\_FUELDIL

 SampleName #3 Headspace w/heat&cool
 Date Processed 02/03/98 05:01:57 PM

 Channel Descr. FID
 Vial 1 Inj 1 Channel SATIN Channel ID 5764

#### UNDERWRITERS LABORATORIES



Figure 4 Chromatogram of Oil Sample 3 Vapor Source

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## 4.0 CONCLUSIONS AND RECOMMENDATIONS

Ignition and chromatographic studies were performed on two No. 6 Oils meeting Grade E cargo requirements to determine if they exhibit below flash point ignition behavior. One oil did ignite consistently below its measured flash point, but the difference was within the reproducibility of the ASTM closed cup flash point procedure. The other test oil did not ignite below its flash point.

Chromatographic analyses did not indicate preferential fractionation of the lighter components of the oil, a potential cause of the below flash point behavior. However, these analyses did indicate significant differences in the chemical composition of the two oils, which may affect their differing ignition behavior.

Significant mist formation in the vapor space was observed to occur just before ignition. This may also be related to the below flash point ignition behavior.

Refinements to the experimental equipment are recommended to better isolate and discriminate among potential causes of below flash point ignition behavior. Tests with a wider range of Grade E cargos are also needed to determine the extent of this behavior as well as its mechanism.

#### 5.0 REFERENCES

1. 46 CFR Part 30 SubChapter D, Para. 30.10-15, and 46 CFR Part 30 Subchapter D, Para. 32.53-1.

2. Zalosh, R. and Subbarao, L., "Fire and Explosion Hazards of Grade E Cargo - Phase 2: Vapor Flammability Tests," Contract No. DTCG39-94-F-E0041, August 1996.

3. Zalosh, R. and Finnegan, D., "Fire and Explosion Hazards of Grade E Cargo," USCG Report CG-D-39-95, Contract No. DTCG39-93-F-E00571, October 1995.

4. Finnegan, D., "Study of Flash Point of Multicomponent Flammable Liquid Solutions," Master's Thesis, Worcester Polytechnic Institute, December 1994.

5. ASTM D 93-90," Test Method for Flash Point by Pensky-Martens Closed Tester, American Society for Testing and Materials, Philadelphia, PA.

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MATERIAL SAFETY DATA SHEETS FOR THE TEST OILS

## THE SOMERSET REFINERY, INC

600 MONTICELLO ST. P.O. BOX 1547 SOMERSET, KY 42502

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## MATERIAL SAFETY DATA SHEET

MSDS NO. 11

EMERGENCY PHONE NUMBER	606-678	-8194	CH	EMTREC	800-424-9300
I. PI	RODUCT IDE	NTIFICATIO	N		
PRCDUCT: #6 Fuel Oil	<u> </u>	CHEMIC	CAL NAME:	Petroleum	Residual
CHEMICAL FAMILY: Petroleu	m	FORMU	LA: C20-C80	-C80   CAS NO. : MIXTURE	
NA ONAL FIRE PROTECT ON A LEAST (0),SLIGHT (1),MODERAT EXTREME (4)			FIR		2
И. Н	AZARDOUS	COMPONEN	TS		
INGREDIENT		%	CSHA L	IMIT	TLV
Mixture-Petroleum Hydrocarbons		100	NA		5MG/M3 (8 Hr. TWA)
	HYSICAL AN		L PROPERT	IES	
BOILING POINT VAPOR PRESS. 300-760 F <a href="https://www.science.com">VAPOR PRESS.</a>		EVAPOR		JTYL ACETATE=1	
VOLATILE BY VOLUME % NA	MOLECULAR WT			APPEARANCE Black Liquid	
iV. F	INT PRUVE	TIDIN INFOR	MAT-01		tut, c
	AUTOIGNITI NA	ON TEMP	FLAMMA LOV 3.9		S % VOL IN AIR UPPER 20.1
EXT NGUISHING MEDIA					

water spray only to cool containers exposed to fire. If leak or spill has not ignited, use water spray to disperse the vapors.

Carbon dioxide, dry chemical, or foam. Water stream may spread fire, use

HAZARDOUS DECMPOSITION PRODUCTS
Incomplete combustion can vield corbon menoxide and various hydrocarbons
etc.
FIRE AND EXPLOSION HAZARDS
Never weld or use torch on containers, even empty.Can ignite explosively.
Explosion hazard in fire situation. Vapor heavier than air and may travel
considerable distance to a source of ignition and flash back.
HAZARDOUS POLYMERIZATION STABILITY
X WILL NOT OCCUR WILL OCCUR STABLE
V. HEALTH INFORMATION
INHALATION
Inhalation of vapors can cause nasal and respiratory irritation,
dizziness, weakness, fatigue, stupor.
EYE CONTACT Acute: Irritation
SKIN CONTACT
Chronic: Irritation, dermatitis,
ING::STION
Can cause gastrointestinal initiation, sause a vomiting at C diambea 1997
Aspiration of materials into the lungs can cause chemical pheumonitis which can be fatal.
REPORTED AS POTENTIAL CARCINOGEN         OR CARCINOGEN         X         NOT APPLICABLE         INTER. AGENCY FOR RESEARCH ON CANCER         NATIONAL TOXICOLOGY PROGRAM         OSHA
VI. FIRST AID PROCEDURES
INHALATION Move exposed person to fresh air. If breathing has stopped, porform
artificial respiration. Get medical attention as soon as possible.
EYE CONTACT
Immediately flush eyes with water for a minimum of 15 minutes,
occasionally lifting the lower and upper lids.
Get medical attention promptly.
SKINCONTACT
If clothing suaked immedial in a fill reaction and wash skin with soap in and water. Launder clothing before wearing: Get medical attention promptly.
INGESTION
Do NOT induce vomiting. Get medical attention as soon as possible. Aspiration of materials into lungs do to vomiting can cause chemical pneumonitis which can be fatal.

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		VII. EMPL	OYEE PROTEC	TION	
REGPIR	ATORY PROTEC Approved orga		above the TLVs		
PROTEC	TIVE CLOTHING				
		EYES-	Chuinn an	Clair, Suce surgerd	
		SKIN-	Gloven: Nitril resistant to o	e, neopra≓e drioth <b>e⊨matatia</b> ! I.	
VENTILA	TION				
Us co	e in well ventilated mpliance. Respor	l area. In con Isible individua	fined spaces me als should evalua	chanical ventilation may be re te air concentrations of specified of the s	quired for TLV ic regulated
		VIII. TRAN	SPORTATION	AND STORAGE INFORMATI	ON
DOT HA	ZARDOUS MATE	RIAL		DOT HAZARD CLASS	
		XY	ES NO	Combustible Liquid	
DOT SH	IPPING NAME AN		IN 1993		
STCRAC	Do not handle			rks, or strong oxidants. as NFPA Class III Liquid.	
		IX. ENVIR	ONMENTAL PR	OTECTION	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
SPILLS	sources. Build	like to contain	flow. Remove i	ate mea and remove ignition ree liquit to not flush to serve lace in clused container for	ər or
EPA Haz	zardous Waste	Yes	XNo	Waste Characteristic :	NA
WASTE	DISPOSAL:		······································	· · · · · · · · · · · · · · · · · · ·	
			erial is hazardous al state and fede	waste . Disposal should eral laws.	
DISCLA	IMER:				

The information and recommendations contained in this publication have been complied from sources believed reliable and to represent the best current opinion on the subject at the time of publication. Since we cannot anticipate or control the may different conditions under which this information or our produce may be used, we make no guarantee that the recommendations will be adequate for all individuals or situations. Eacli user of the product described herein should determine the suitability of the described product for his or

her particular purpose and should comply with all federal and state rules and regulations concerning the



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MATERIAL SAFETY DATA SHEET



ther or

$\bigcirc$		,			APEX	•
	:*		••.	MSDS /	NUMBER	
SECTION I MATERIAL	IDENTIFIC	ATION	· 24 HC	UR EMERGE	NCY INFOR	MATION
PRODUCT/			CLARKI	APEX . 314 - 8		
HEMICAL NAME No. 6 fuel ail					24-9300	
CHEMICAL SYNONYMS Bunker fuel, coker charge				os:	FIRE	E
THEMICAL FAMILY					,入	
FORMULA Aromatic	petroleu	n ail :	J = HIG	- / / /	2 > AEACI	<b>FIVITY</b>
OTHER IDENTIFICATION .				ERATE Y	Y	
MATERIAL USE OR .			1 = SLIC		OTH	ER
	tal fuel o	11	0 = LEA	HEALTH		
SECTION II		INGREDIENT				
COMPONENT	%	Units)	COMP	DNENT	*	TLV
						(Units)
Perroloum						
Heavy fraction consisting		Not establis				
of a complex mixture of high molecular weight		(recommanded				
hydrocarbons.		concentration as benzene s				
May contain polynuclear		as venzene s	0100163.)			
aromatic hydrocarbons.						
			!			
	{	÷	•			
	1			· · ·		
			ν.			
	1					
SECTION III	·	PHYSICAL DA				
	MELTING		A			
· · ·	c l	Varies	'c	VAPOR PRESSUR	in Hg, @	
SPECIFIC GRAVITY .	VOLATILE	BY VOLUME		VAPOR DENSITY		
040-1 0.9402-1.000	Not e	established	%		N/A	
SOLUBILITY HIL		Noti -	tablished			<b></b>
APPEANATE E AND COONS		· T}·····	·			
	brouze ec	olor, heavy ar	omatic od	0r.		
SECTION IV		AND EXPLOSIC				
FLASH POINT AND METHOD	and the second se	TEMPERATURE		MABLE LIMITS (%)		
▶ 150° 100		$nition = 765^{\circ}$		t establishe		L UEL
EXTRUSTIGHTS MEDIA					<u> </u>	
Jeam, carbon dioxide, dr	y chemical	1.				
SECUAL FILLEFIGHTING PHOCEDURES AN				· · · · · · · · · · · · · · · · · · ·		
Do not use Feam at storage	: temperati	ures above 200	<sup>o</sup> F. Fire	men flghting	fuel oil #	fires
should use necessary proce be used when fighting first	CTIVE equ	ipment and bre	athing ap	paratus as w	ould normal	lly
be used when fighting fire	u wnete ti	nere may be da	nger of b	reathing.haz	ardous prog	jucts
UNGSUAL FINE AND EXPLUSION INFORM	ATION					
	Nor	ne.	• •	۰ <b>.</b>		
)RMA M56: 100				سينى منيني متيطروسين		

	· · · · · · · · · · · · · · · · · · ·			
USHA PELD	ACGIH ILV F	ACTION LEVEL		
ا <u>طلا</u>	HEALTH EFFECT	shod Not established		
	ACUTE	CHRONIC		
INHALATION	Tration of respiratory tract moreus membranes, musea, CNS depression, pulmonary edema	Irration of respiratory tract much membranes, possible mild chemical pnoumonitis with high concentration		
INGESTION	Large quantities can result in nausea, CNS depression.	Na known effects.		
SKIN CONTACT	Irritaion, particulary of mucous membranes.	Repeated and prolonged skin contact result in skin disorders and potenti. sensitization.		
EVE CONTACT	······································	- Schwage and Cashe		
	Irritation of the cornea and/or conjunctiva.	Irritation of the cornea and/or conjunctiva.		
FIRST AID PROCED	DURES			

INHALATION-remove from vapor to fresh air, if unconscious seek medical aid. INCESTION-DO NOT INDUCE VOMITING, seek medical aid.SKIN CONTACT-promptly remove oil soaked clothing, wash skin with soap and water, if irritation develops, seek medical ald.EVE CONTACT-flush with copious amounts of water, if tritation develops, seek medical aid.

SECTION VI		REACTIVITY		
STAHILITY .	LIUNSTABLE	.SSIARLE	AZARDOUS PULYMERIZATION P	E WILL NOT DECU
CONDITIONS TO	Source of ign	ltion, heat, etc.		

Strong oxidants, e.g., chlorine and concentrated oxygen. TYPICAL DECUMPOSITION PRODUCTS

Incomplete combustion will produce carbon monoxide, organic acids, aldehydes.

#### SECTION VIL

#### SPILL OR LEAK PROCEDURES

Avoid excepsive inhalation or skin contact. Absorb, scrape up, or incinerate under proper conditions or secure in a chemical land fill. Observe Federal, state and local governmental spill and water quality regulations. Contain spills by diking or impoundir to prevent entrance into water courses and ground water.

SECTION IX	OTHER INFORMATION
VENTILATION	LUCALEXHAUST Recommended where airborne concentrations exceed 0.2 mg/m <sup>3</sup>
050000000000000000000000000000000000000	GENERAL EXHAUSTE Recommended for use in enclosed or semi-enclosed
PERSONAL	Respiratory projection) Combination particulate and vapor air putifying or Self-contained breathing upparatus recommended at an above 0 2-2/2020 bee
EQUIPMENT	GLOVES Butyl rubber, L'E PROTECTION Splash poggle OTHER) zene soluble neoprene, polyethylene of shields with safety Full body pyc glasses.

#### SECTION VIII

#### SPECIAL PROTECTION AND CONTROL INFORMATION

The information contained herein is based on data available at this time and is believed to be accurate. However, no warranty is expressed or implied recarding the accuracy of these data or the results to be obtained form the use therof. Since information contained herein may be applied under conditions beyond our control and with shich we may be unfamiliar, no responsibility is assumed for the results of its use. The person receiving this information shall make his own determination of the suitability of the material for his particular purpose.

MATERIAL			Health Adminis			
Distribution and a USDI	Safe	inv and He		r Ship Repairing,		
		SECTI				
ANUFACTURER'S NAME		02011		EMERGENCY TELEPHON		
Colonial Oil Industries. Inc. DORESS (Number, Street, City, State, and ZIP Con North Lathrop Avenue. P. O. Bo HEMICAL NAME AND SYNONYMS Petroleum Heavy Fuel Oil HEMICAL FAMILY Petroleum Hydrocarbon			FORMULA Complex mixtu	re of petroleum hy		
SECTION	11 -		DOUS INGRED	•		TLV
PAINTS, PRESERVATIVES, & SOLVENTS	*	TLV (Units)	ALLOYS AND	METALLIC COATINGS	×	(Units)
IGMENTS		n.a.	BASE METAL		_	n.a.
ATALYST	Τ	n.a.	ALLOYS			n.a.
EHICLE	1	n.a.	METALLIC COATH	NGS		n.a.
OLVENTS	$\uparrow$	n.a.	FILLER METAL	R CORE FLUX		n.a.
DDITIVES	1	n.a.	OTHERS			n.a.
THERS	+	n.a.				
HAZARDOUS MIXTURE	S OF	OTHER LI	QUIDS, SOLIDS, OR	GASES	×	TLV (Units)
						<b></b>
	<u>_</u>					
SE	CTIC	ON III - I	PHYSICAL DAT			
BOILING POINT ("F-) IBP-90%	4	50-1100	SPECIFIC GRAVIT	A DESCRIPTION OF A DESC		.969
		<0.01mm	PERCENT, VOLAT		Neg]	ligible
APOR PRESSURE (MM Hg.) & 2000						
		76	EVAPORATION A	esate = 1)		0.01
VAPOR PRESSURE (MM Hg.) @ 2000 VAPOR DENSITY (AIR=1)		<del>76</del> gligibl	EVAPORATION A	ATE = 1)		0.01
VAPOR DENSITY (AIR=1)	Ne	gligibl	EVAPORATION A			).01
VAPOR DENSITY (AIR=1) SOLUBILITY IN WATER APPEARANCE AND ODOR Dark liqu	Ne id.	scrong	EVAPORATION A ( <u>II-BUTYI AC</u> e asphalt-like	odor.		).01
VAPOR DENSITY (AIR=1) SOLUBILITY IN WATER APPEARANCE AND ODOR DATE LIQU SECTION IV	Ne id.	scrong	e asphalt-like	ZARD DATA		Uet
VAPOR DENSITY (AIR=1) SOLUBILITY IN WATER APPEARANCE AND ODOR Dark liqu SECTION IV FLASH POINT (Method used) PM Closed Cup 180°F.	Ne id.	scrong	EVAPORATION A ( <u>II-BUTYI AC</u> e asphalt-like	azard DATA		
VAPOR DENSITY (AIR=1) SOLUBILITY IN WATER APPEARANCE AND ODOR Dark liqu: SECTION IV FLASH POINT (Method used) PM Closed Cup 180°F. EXTINGUISHING MEDIA FORm. dry chemical, CO2.	Ne id. - Fli wat	gligibl Strong RE AND	EVAPORATION R ( <u>ID-BUTY) AC</u> e asphalt-like EXPLOSION HA FLAMMAGLE ay, or fog.	AZARD DATA		Uet
VAPOR DENSITY (AIR=1) SOLUBILITY IN WATER APPEARANCE AND ODOR Dark liqu: SECTION IV FLASH POINT (Method used) PM Closed Cup 180°F. EXTINGUISHING MEDIA Form, dry chemical, CO2.	Ne id. - Fli wat	gligibl Strong RE AND	EVAPORATION R ( <u>ID-BUTY) AC</u> e asphalt-like EXPLOSION HA FLAMMAGLE ay, or fog.	AZARD DATA		Uet
VAPOR DENSITY (AIR=1) SOLUBILITY IN WATER APPEARANCE AND ODOR Dark liqu: SECTION IV FLASH POINT (Method used) PM Closed Cup 180°F. EXTINGUISHING MEDIA FOAM, dry chemical, CO2, SPECIAL FIRE FIGHTING PROCEDURES Use air-supplied rescue Cool exposed containers	Ne id. - Fli wat	gligibl Strong RE AND ter spra	EVAPORATION R ( <u>n-Butyl Ac</u> e asphalt-like EXPLOSION HA FLAMMABLE ay, or fog. for enclosed a	AZARD DATA		Uet
VAPOR DENSITY (AIR=1) SOLUBILITY IN WATER APPEARANCE AND ODOR Dark liqu: SECTION IV FLASH POINT (Method used) PM Closed Cup 180°F. EXTINGUISHING MEDIA FORm. dry chemical, CO2.	Ne id. - Fli wat equi	gligibl Strong RE AND ter spra ipment	EVAPORATION A ( <u>ID-BUTYI AC</u> asphalt-like EXPLOSION HA FLAMMABLE ay, or fog. for enclosed a	AZARD DATA		Uet
VAPOR DENSITY (AIR=1) SOLUBILITY IN WATER APPEARANCE AND ODOR Dark liqu: SECTION IV FLASH POINT (Method used) PM Closed Cup 180°F. EXTINGUISHING MEDIA FORM. dry chemical: CO2. SPECIAL FIRE FIGHTING PROCEDURES Use air-supplied rescue Cool exposed containers	Ne id. - Fli wat equ: wit	gligibl Scrong RE AND ter spra ipment : h_water rong_ox	EVAPORATION A ( <u>ID-BUTYI AC</u> asphalt-like EXPLOSION HA FLAMMABLE ay, or fog. for enclosed a	AZARD DATA	Forr	Uet
VAPOR DENSITY (AIR=1) SOLUBILITY IN WATER APPEARANCE AND ODOR Dark liqu: SECTION IV FLASH POINT (Method used) PM Closed Cup 180°F. EXTINGUISHING MEDIA FORM. dry chemical: CO2. SPECIAL FIRE FIGHTING PROCEDURES USE air-supplied rescue Cool exposed containers UNUSUAL FIRE AND EXPLOSION HAZARDS DO. DOT. STORE OF MIX with D. B NOT APPLICADIE	Ne id. - Fli wat equ: wit	gligibl Scrong RE AND ter spra ipment : h_water rong_ox	EVAPORATION R ( <u>n-Butyl Ac</u> e asphalt-like EXPLOSION HA FLAMMABLE ay, or fog. for enclosed a idants.	AZARD DATA	Forr	Uet 6.02
APOR DENSITY (AIR=1) OLUGILITY IN WATER APPEARANCE AND ODOR Dark liqu: SECTION IV SECTION IV SECT	Ne id. - Fli wat equ: wit	gligibl Scrong RE AND ter spra ipment : h_water rong_ox	EVAPORATION R ( <u>n-Butyl Ac</u> e asphalt-like EXPLOSION HA FLAMMABLE ay, or fog. for enclosed a idants.	AZARD DATA	Forr	Uet 6.02

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## SECTION V + HEALTH HAZARD DATA

THRESHOLD LIMIT VALUE 5 mg/m for oil mist. EFFECTS OF OVEREXPOSURE

OF OVEREXPOSURE Prolonged or repeated skin contact may cause mild skin irritation.

EMERGENCY AND FIRST AID PROCEDURES In case of skin contact, wash with soap and water. If splashed into eyes,

## flush with clear water until irritation subsides.

## SECTION VI - FEACTIVITY DATA

			CONDITIO	NS TO AVOID	
STABILITY	UNSTABLE				·····
ĺ	STABLE	x			
INCOMPATABILIT	Alerials to avoid	1)			<u>مر</u>
HAZARDOUS DEC	OMPOSITION PRO		•		
				CONDITIONS TO AVOID	
HAZARDOUS	MAY OC				
POLYMERIZATION	WILL NO	WILL NOT OCCUR			

## SECTION VII - SPILL OR LEAK PROCEDURES

STEPS TO BE TAKEN IN CASE MATERIAL IS RELEASED OR SPILLED Recover free liquid. Add absorbent to spill area.

Keep petroleum products out of streams and waterways.

WASTE DISPOSAL METHOD Incinerate absorbed material.

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	SECTION VIII - SPECIA	L PROTECTION	INFORMATION	
RESPIRATORY PRO	TECTION (Specify type) Ly not needed.		SPECIAL	
VENTILATION	Needed only to capture	hot fumes.	•	
	MECHANICAL (General)		OTHER	
PROTECTIVE GLOVES Normally not needed		EYE PROTECT Normaily	not needed.	
OTHER PROTECTIN	DE EQUIPMENT DERVIOUS APRON if needed.			

## SECTION IX - SPECIAL PRECAUTIONS

PRECAUTIONS TO BE TAKEN IN HANOLING AND STORING Keep containers closed. Keep away from heat and open flame.

OTHER PRECAUTIONS Avoid breathing of oil mist. Remove oil-impregnated clothing. Wash

thoroughly after exposure.

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