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Prediction of Radar Pulse Envelope Distortion due to Tropospheric Propagation

Marina Ozerova

DSTO-TN-0125

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## Prediction of Radar Pulse Envelope Distortion due to Tropospheric Propagation

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Electronic Warfare Division Electronics and Surveillance Research Laboratory

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#### ABSTRACT

This project is a part of research into the detection of radar signals at ranges well beyond the horizon by exploiting the effect of tropospheric scattering. A result of this work is a program written in C language which enables the distortion of the envelope of a given radar pulse, which occurs as a result of propagating over any path by tropospheric scattering, to be predicted.

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## Prediction of Radar Pulse Envelope Distortion due to Tropospheric Propagation

#### **EXECUTIVE SUMMARY**

The objective of the work described in this report is to investigate the possibilities of detecting radar transmissions from very long range by means of tropospheric scatttering.

The propagation of radio waves via the troposphere occurs as a result of a scattering mechanism which takes place in the volume of the tropospheric medium where the beams of the transmitting and receiving antennas overlap.

Radar signals which propagate via the troposphere will have a distorted pulse envelope shape due to the difference in the transit time between the shortest and longest paths from the transmitter to the receiver via the extremities of the scattering volume. The extent of the distortion will depend on the pulse duration compared to the time difference between propagation via the longest and shortest paths.

The main objective of the work described in this report was to predict the distortion of the pulse envelope shape of radar signals after propagation via the troposphere. In order to optimise the detection of tropospheric scattered radar signals it is desirable to be able to predict this distortion to enable a better matched filter to be designed.

The procedure adopted is to assume that the variations to the pulse shape result from the spatial distribution of the scattering and the scattering mechanism is equivalent to the reflection of the signal from a large number of point reflectors randomly distributed within the scattering volume.

#### Author

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Marina Ozerova recently joined DSTO as a Professional Officer Class 1 in Wide Area Surveillance Division although the work described in this report was done in Electronic Warfare Division prior to her appointment. Marina was born in Russia and graduated from the Physics Faculty of Nizhny Novgorod State University in 1987. She defended her project on low temperature deposition of  $A_2B_6$ semiconductors using high frequency plasma thermodecomposition of  $Cd(CH_3)_2$  and  $Te(CH_3)_2$  metal organic compounds widely used in infra-red detectors. Marina emigrated to Australia in 1993 and has since become an Australian Citizen. After arriving in Australia she undertook a number of work experience jobs to help adapt to the Australian work environment and to improve her command of English. Work experience included working as a Physicist for the Department of Mines and Energy, the Radiation Protection Branch of the S.A. Health Commission and, finally, with Electronic Warfare Division of the DSTO.

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## 1. Introduction

The problem of scattering of electromagnetic waves in the troposphere attracts considerable attention from scientists and engineers. The phenomenon related to long-range atmospheric propagation of short waves beyond the limits of the "radio horizon" is known to be one of the least developed subjects of this kind.

Thus, the propagation of radio waves via the troposphere occurs as a result of the poorly understood mechanism of scattering which takes place in the volume of space where the beams of the transmitting and receiving antennas overlap.

The goal of this project was not to dwell on all the numerous problems associated with the use of radio scattering for the purpose of long range communication. Instead, the main objective of the current project were to predict the distortion of the pulse envelope shape of radar signals after propagation via the troposphere. The ability to predict the pulse envelope will enable a better matched filter to be designed for detecting the signals.

Radar signals which propagate via the troposphere will have a distorted pulse envelope shape if the difference in the transit time between the shortest and longest paths from the transmitter to the receiver, via the extremities of the scattering volume, is comparable with the pulse duration and in most instances this will be the case. In order to optimise the detection of tropospheric scattered radar signals it is desirable to be able to predict the pulse envelope distortion that will occur.

The area of our interest is in estimating the variations to the pulse shape and since this envelope shape distortion will not result from the scattering mechanism itself but from the spatial distribution of the scattering, it should be possible to calculate the likely effect by assuming the scattering mechanism is equivalent to the reflection of the signal from a large number of point reflectors distributed within the scattering volume.

As can be seen from Figure 1, if the elevation and azimuth beam shapes of the transmitting and receiving antennas are known, then we could calculate the signal strength and relative phase at the receiver for some nominal transmitter power and a nominal cross section reflector situated at any given point within the scattering volume. It is also possible to calculate the transit time between transmission and reception of this reflected signal.



Figure 1: Scattering volume.

It is reasonable to assume that the envelope shape of the signal reflected from a point reflector will be identical to the envelope shape of the transmitted signal. Applying this condition to a large number of identical point reflectors distributed throughout the scattering volume and summing all the individual signals, taking into account the transit time delay of the amplitude envelope and the phase of each signal, then it should be possible to construct the probable amplitude profile of a troposcattered signal for any given transmitted signal envelope shape.

In this project we will not take into account the scattering phenomenon itself, i.e. attenuation, depolarisation and volume scattering effects leading to troposcatter losses. Only a brief theoretical introduction of these effects will be given. Results of computations of troposcatter losses employing known empirical approaches, i.e. NBS, Yeh, Rider etc. were presented in [5].

However, it is believed that the results of the current project which considers the change in the envelope shape due to spatial distribution of the reflectors inside the scattering volume, could be coupled with the results of earlier work [5] in future tasks in order to estimate the combined effect.

## 2. Radio scattering in the troposphere

This section is a brief introduction and overview of the theory of propagation of radio waves via the troposphere.

#### 2.1 Interaction processes in the troposphere

There are a number of possible mechanisms whereby radiowaves can interact with the lower atmosphere to produce scattering, these include:

- absorption and dispersion in atmospheric gases (oxygen, water vapour and minor constituents);
- scattering from atmospheric turbulence and scintillation;
- scattering and absorption in populations of hydrometeors (including anisotropic effects, forward scatter, back scatter, and scattering at arbitrary angles);
- scattering and absorption in sand and dust particle populations;
- refraction and reflection in stable atmospheric layers;
- thermal emission from hydrometeors and atmospheric gases.[1]

#### 2.2 Theory of scattering and absorption

Attenuation, depolarization and volume scattering of radiowaves due to atmospheric particles are phenomena, which severely limit the performance of telecommunication systems.

Currently, mainly frequencies below 20 GHz are used by communication systems although the use of some millimetre wave frequencies where high absorption occurs has been advocated in the literature for short range secure links.

The basic theory describing different models for attenuation, depolarization and volume scattering is the theory for single-particle scattering. Particle scattering effects become more severe with higher frequencies. This is aggravated by the increasing effect of small particles, such as liquid droplets, which are present in great numbers in the atmosphere.

The problem of single and multiple scattering has been discussed by many authors. Some approaches have different interpretations of formulae and different ways to derive them.

Let us introduce just one model - single scattering approximation, which was described in Reference [3]. Here, the author considered a random medium illuminated by a transmitter. A part of the transmitted wave was scattered by the randomness of the medium and this scattered wave was detected by a receiver (Figure 2).

There was considered a volume  $\delta V$  in the random medium. It was assumed that the randomness of the medium was so slight that the wave incident on  $\delta V$  was almost equal to the incident wave in the absence of the random medium.



Figure 2: Geometry showing transmitter, receiver and random medium.

It was described by the amount of scattered power due to the random medium in  $\delta V$  in terms of the equivalent scattering cross section per unit volume  $\sigma(0, I)$ , then the received power P<sub>r</sub> is given by the radar equation

$$P_{\rm r} / P_{\rm t} = \lambda^2 G_{\rm t}(i) G_{\rm r}(0) \ \sigma(0,i) \delta V / \ (4\pi)^2 R_1^2 R_2^2 \quad , \tag{1}$$

where Pt - transmitted power

 $G_t$ ,  $G_r$  - gain functions of the transmitter and receiver antennas in the directions of i and -0.

The basic scattering theory must be reviewed in order to find the limitations of its applicability to electromagnetic wave problems.

The theory of single and multiple scattering has been discussed in References [1, 2, 3, 4]. At this time, no references could be found that treat the basic scattering theory, as applied to communication systems, in a completely consistent way. This makes it difficult to understand the scattering theory [1].

## **2.3** Application of the theory of radio scattering in the troposphere to beam communication

Booker and Gordon [4] describe in their work the experiments made in the Caribbean Sea in 1945. The goal of these experiments was to explore the radio consequences of the evaporation-duct that exists at the ocean surface. As a result of this project it was discovered that, at any rate under some circumstances, field strength well beyond the horizon decreases with distance more slowly than could be expected on any existing theory. The wavelength used was 9 cm in this experiment. They found that the unexpectedly high field strengths obtained at long range on 9 cm were not due to duct propagation, and, accounting for the rather violent fading associated with them, it was suggested that a scattering mechanism was involved.



Figure 3: Antennas beams.

Booker and Gordon considered transmission from point T to point R at distance d round the curved surface of the earth by means of beamed antennas pointed more or less at each other as indicated in Figure 3. It was assumed that there were no ducts and that as far as ordinary reflection is concerned propagation was orthodox. It was supposed that both antennas were pointed horizontally at their respective locations, and that their axes lay in the vertical plane through T and R. For simplicity it was considered that the T and R antennas were identical. It was found that if the transmitter and receiver are omnidirectional, scattering is in general important from nearly the whole of the atmosphere above the horizons of both transmitter and receiver. However, in practice, both transmitter and receiver antennas usually have some directivity, and scattering is then important only in the region of atmosphere where the transmitting and receiving beams overlap.

As a result of the Caribbean experiments the following conclusions were made:

- 1. The modified scale of turbulence is expected to decrease with height above the earth's surface.
- 2. The theory of atmospheric scattering seems to predict a decrease of scattered field strength with distance that is too low to agree with the observation, in fact the scattering almost certainly decreases with height in most practical cases.
- 3. The height of the important scattering volume increases with the increase of distance between transmitter and receiver. An associated decrease of the modified scale of atmospheric turbulence would cause the scattering signal received to decrease more rapidly with the increase of range than for a uniformly turbulent atmosphere.
- 4. The same theory which is used for calculating the scattering signal at long distances may also be used in most cases for calculating the fading range at shorter distances.

## 3. Practical Procedure

First of all, it is necessary to emphasise that, because of the diverse nature of the problem, various approximations should be employed to obtain useful results. Therefore, some useful approximation techniques applicable to a variety of different situations will be presented in this project.

- 1. We will assume that the transmitter and receiver beam shapes are effectively rectangular.
- 2. We assign the transmitter to be at the origin (x = 1, y = 0) of a two dimensional coordinate system and the receiver to be on the x axis at a point that can be calculated from the great circle distance between the transmitter and receiver sites on the earth surface.
- 3. We assume both transmitter and receiver beam width to be the same.
- 4. Then we need to calculate the inclination of the transmitter and receiver antenna beams from the x axis, so that it is possible to calculate the x, y coordinates of the intersecting volume.
- 5. Next, it is necessary to calculate the coordinates of an array of point reflectors which were initially assumed to be regularly spaced within the intersecting volume although this was later extended to include a uniform density random distribution.

- 6. For each of the points in the array we then calculate the path length between transmitter and receiver via each point and hence determine the transmit time for each point reflected signal. Because we are interested only in the differences, we subtract the mean transit time from the actual transit time to obtain the delta transit time.
- 7. Since the signal which is assumed to be reflected from the reflector at each point starts from the transmitter with the same phase, we must now calculate the relative RF phase of each reflected signal by dividing the path length via each point reflector by the free space wavelength of the RF signal and discarding the integer part.
- 8. Since we have initially chosen to assume a rectangular beam shape and that the path difference from each point reflector will only differ by a small percentage we now assume that all the signals reflected from the point reflectors have the same (unity) amplitude profile.



Figure 4: Pulse shape.

- 9. Now we define a suitable transmitter amplitude profile (pulse shape) by introducing three character-parameters, namely rise time  $t_r$ , fall time  $t_f$ , and duration  $t_d$ .
- 10. Finally, we produce a temporal plot of the resulting troposcattered waveform shape by doing a vector sum of all the point reflector outputs at each of a large number of time increments encompassing the pulse width and the range of delta transit time. The above is illustrated in Figure 4, and expressed more formally in the following equations:

$$\mathbf{A} = \sum (\mathbf{a}_i \cos \varphi_i + \mathbf{j} \ \mathbf{a}_i \sin \varphi_i), \tag{2}$$

where A - complex amplitude of the resulting envelope signal,

a<sub>i</sub> - amplitude of initial envelope signal

j = √-1

 $\varphi_i = (vl_i/c - Integer[vl_i/c]) 2\pi$ 

 $\phi_i$  - the phase of a signal reflected by point "i" from scattering volume,

v - RF frequency in MHz,

c - the light speed in vacuum in [km/s]'

 $l_i$  - the length of the path from the transmitter to receiver via point "i" in [km].



Figure 5: Geometry of beam intersection region.

	$y = tan(\theta - \beta) x$	(equation for line 1)	(3)
	$y = tan(\theta + \beta) x$	(equation for line 2)	(4)
Assumpti	on $\theta_1 = \theta_2 = \theta$		
	$\beta_1 = \beta_2 = \beta$		
y = - tan[θ	$[-\beta] x + b$		
$0 = - \tan[\theta]$	-β]d+b		
d tan[θ - β	b] = b		
	$y = dtan[\theta - \beta] - ta$	$n[\theta - \beta] \mathbf{x}$ , (equation for line 3)	(5)
	$y = dtan[\theta + \beta] - t$	<b>an[<math>\theta</math> + <math>\beta</math>] x , (equation for line 4)</b>	(6)
	$\tan[\theta - \beta] x = d\tan \theta$	$n[\theta - \beta] - tan[\theta - \beta] x$ ,	(7)
	$2\tan[\theta - \beta] = dta$	ın[θ - β] ,	(8)
	x = d/2 ,		(9)

where

R - effective radius of Earth (4/3 physical radius)

 $\boldsymbol{\beta}$  - the half beam width angle

l - the distance between the transmitter and the receiver

 $\boldsymbol{\phi}$  - the elevation angle of transmitter

n - number of points

 $1 = R\alpha$ 

 $d^{2} = 2R^{2} - 2R^{2}\cos\alpha = 2R(R - R\cos\alpha) , \qquad (10)$ 

 $\mathbf{d} = \sqrt{2\mathbf{R}(\mathbf{R} - \mathbf{R}\cos\alpha)} \quad , \tag{11}$ 

$$\gamma = (\pi - \alpha)/2 \quad , \tag{12}$$

$$\delta = \pi/2 - \gamma = \pi/2 - \pi/2 + \alpha/2 = \alpha/2 \quad , \tag{13}$$

$$\theta = \phi + \delta \quad , \tag{14}$$



Figure 6: Scattering region.

We have equations for lines 1, 2, 3 and 4.

The ordinate of point N ( y coordinate of N) is the maximum y value of the point to be distributed to the area.

The y coordinate of M is the minimum of y coordinate.

In the program the user specifies the numbers of rows, **r** and the spacing between the rows is  $\Delta$ .

$$\Delta = \text{distance NM/r} \quad , \tag{15}$$

We know coordinates for the point N. N is specified by  $(x_N, y_N)$ . Take the y coordinate and decrease it's value by  $\Delta$ , i.e.  $y_N - \Delta$ .

From Equation 2 substitute  $y_N - \Delta$  for y and solve for x. This gives us the first point of the first row - point N.

To get the next point, the coordinate will be  $(x_N + \Delta, y_N - \Delta)$ . To find the maximum value of x put  $y_N - \Delta$  into the equation 4 and solve x

While all this is being done, i.e. when each point is determined, we can at this time calculate the distance from transmitter to the receiver via the point. If the coordinates of the point are  $(x_P, y_P)$  then the distance from the transmitter to the receiver is

$$\mathbf{D} = \sqrt{((\mathbf{x}_{\rm P} - \mathbf{x}_{\rm T})^2 + (\mathbf{y}_{\rm P} - \mathbf{y}_{\rm T})^2) + \sqrt{((\mathbf{x}_{\rm P} - \mathbf{x}_{\rm R})^2 + (\mathbf{y}_{\rm P} - \mathbf{y}_{\rm R})^2)} , \qquad (16)$$

where  $x_T, y_T$  - coordinates of the transmitter,

 $x_R$ ,  $y_R$  - coordinates of the receiver,

which are  $(x_T, y_T) = (0, 0)$ 

$$(x_R, y_R) = (d, 0)$$

## 4. Operation

The software was developed and runs on an IBM PC and is written in Borland, Turbo C++, version 1.00. The plotting macros require the use of Excel, version 5.0. This section describes how the software can be operated.

#### 4.1 Installation

- pulse\_d.exe, pulse\_e.exe and pulse\_r.exe files should be installed in c:\tc\bin directory
- pulse\_d.xls, pulse\_e.xls and pulse\_r.xls files in any directory

#### 4.2 Execution

To obtain a plot of the reflection point distribution:

- run pulse\_d.exe in DOS;
- save output to a file called result\_d.txt;
- when finished computations, open **pulse\_d.xls** in Excel;
- run the program in "Execute" Sheet of pulse\_d.xls workbook.

To obtain a table of data and a plot of the pulse after reflection from a uniform array of points:

- run pulse\_e.exe in DOS;
- save output to a file called result\_e.txt;
- when finished computations, open pulse\_e.xls in Excel;
- run the program in "Execute" Sheet of pulse\_e.xls workbook

To obtain a table of data and a plot of the pulse after reflection from a random array of points:

- run pulse\_r.exe in DOS;
- save output to a file named result\_r.txt;
- when finished computations, open pulse\_r.xls in Excel;
- run the program in "Execute" Sheet of pulse\_r.xls workbook.

Note that the programs pulse\_e.xls and pulse\_r.xls are identical except for the result file accessed and the labels on the resulting curves.

## 5. Conclusions

1. Software for computing the modulation envelope after propagation of a given radar signal via the troposphere accounting for the effect of spatial distribution of point reflectors in the scattering volume has been designed and tested.

At this stage, the propagation model is based on point reflectors in a single plane having vertical and horizontal directions with two types of distribution, namely, equidistantly spaced and randomly spaced with uniform density. Elevation angles of both transmitter and receiver were chosen to be equal, as well as their beamwidth angles.

2. The Turbo C++ executable file allows one to plot resulting graphs on the screen and save the data in text format.

A special program was designed in Visual Basic for Excel, which can automatically read the data from the text file generated in Turbo C++ and then plot the graph of envelope amplitude versus time.

[Note that, with hindsight, it would have been much easier for users if the whole program had been designed in Visual Basic. In this case, a computation could be realised by striking one key either on keyboard or on the mouse.]

3. Analysis of the results of computations of radar pulse envelope distortion due to tropospheric propagation have shown (Appendix 1, 2):

- pulse shape envelope does change significantly with beamwidth and elevation angle as might be expected since these parameters determine the distance between the shortest and longest paths via the reflection points;
- with uniform distribution there is some evidence of an interference pattern, which is smoothed out to a large degree with a random distribution.

4. The next steps in developing the current model describing radar pulse envelope distortion are envisaged to be:

- extending the analysis to a three dimensional case;
- introducing a vertical variation in the density of the random distribution of reflecting points to reflect the likely variation resulting from the change in density of the troposphere with height;
- introducing some randomness and vertical variation in the amplitude of the reflection from each reflecting point;
- since real radars that we might wish to detect frequently employ a vertical fan shaped (cosec<sup>2</sup>) beam, which is unlikely to be the best beam shape to use on the receiver, a new model is needed to take into account different values of beam width for the transmitting and receiving antennas.

### 6. Acknowledgments

This work was done in Electronic Warfare Division under a Technical Support Services contract and the author is grateful for the access to the DSTO library and other facilities that were made available.

The author would like to gratefully acknowledge the contribution from Dr A.Kulessa for the help and advice, he gave me while I was doing this project. Also the author wishes to express her thanks to Mr R. Lindop for help received on the same topic.

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## Appendix A: Computations of Radar Pulse Envelope Distortion for Uniform Distribution



Grid with uniform distribution of knots



Resulting Envelope Amplitude vesus Time (uniform grid)

Beamwidth angle beta (degrees):	1.2
Great circle distance I (km):	300
Elevation angle phi (degrees):	0.7
Number of knots inside the scattering volume n:	1000
Operating frequency (MHz):	2830
Pulse rise time (µs):	0.1
Pulse width (µs):	0.5
Pulse fall time (µs):	0.15

.

1	Time(i)	An	nplitude	1	Time[i]	Ап	nplitud <del>a</del>	i	Time[i]	An	nplitude	1	Time[I]	Ап	nplitude		Time[i]	Am	plitude
	1	(arbit	rary units)			(arbit	rary units)			(arbit	rary units)			(arbit	rary units)			(arbit	rary units)
		Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting
1	0.03	0.3	0.733	43	1.29	0	0	85	2.55	0	0	127	3.81	0	0	169	5.07	0	0
2	0.06	0.6	1.645	44	1.32	0	0	86	2.58	0	0	128	3.84	0	0	170	5.1	o	o
з	0.09	0.9	7.693	45	1.35	0	0	87	2.61	O	0	129	3.87	0	0	171	5.13	0	0
4	0.12	1	17.318	46	1.38	0	0	88	2.64	0	0	130	3.9	0	0	172	5.16	0	0
5	0.15	1	24.379	47	1.41	0	0	89	2.67	0	0	131	3.93	0	0	173	5.19	0	0
6	0.18	1	27.143	48	1.44	0	0	90	2.7	0	0	132	3.96	0	0	174	5.22	0	0
7	0.21	1	25.031	49	1.47	0	0	91	2.73	0	0	133	3.99	0	0	175	5.25	0	0
8	0.24	1	23.353	50	1.5	0	0	92	2.76	0	0	134	4.02	0	0	176	5.28	0	0
9	0.27	1	22.825	51	1.53	0	0	93	2.79	0	0	135	4.05	0	0	177	5.31	0	0
10	0.3	1	22.686	52	1.58	0	0	94	2.82	0	0	136	4.08	0	O	178	5.34	0	0
11	0.33	1	22.686	53	1.59	0	0	95	2.85	0	0	137	4.11	0	0	179	5.37	0	O
12	0.36	1	22.686	54	1.62	0	0	96	2.88	0	0	138	4.14	0	0	180	5.4	0	0
13	0.39	1	22.686	55	1.65	0	0	97	2.91	0	0	139	4.17	0	0	181	5.43	0	0
14	0.42	1	22.686	58	1.68	0	0	98	2.94	0	0	140	4.2	0	0	182	5.46	0	0
15	0.45	1	22.686	57	1.71	0	0	99	2.97	0	0	141	4.23	0	0	183	5.49	0	0
16	0.48	1	22.686	58	1.74	0	0	100	3	0	0	142	4.26	0	0	184	5.52	0	0
17	0.51	1	22.686	59	1.77	0	0	101	3.03	0	0	143	4.29	0	0	185	5.55	0	0
18	0.54	1	22.686	60	1.8	0	0	102	3.06	0	0	144	4.32	0	0	186	5.58	0	0
19	0.57	1	22.686	61	1.83	0	0	103	3.09	0	0	145	4.35	0	0	187	5.61	0	0
20	0.6	1	22.686	62	1.86	0	0	104	3.12	0	0	146	4.38	0	0	188	5.64	0	0
21	0.63	0.8	22.525	63	1.89	0	0	105	3.15	0	0	147	4.41	0	0	189	5.67	0	0
22	0.66	0.6	21.595	64	1.92	0	0	106	3.18	0	0	148	4.44	0	0	190	5.7	0	0
23	0.69	0.4	17.787	65	1.95	0	0	107	3.21	0	0	149	4.47	0	0	191	5.73	°	0
24	0.72	0.2	12.583	66	1.98	0	0	108	3.24	°	0	150	4.5	0	0	192	5.76	0	0
25	0.75	0	8.163	67	2.01	0	°	109	3.27	0	°	151	4.53	0	0	193	5.79	0	0
26	0.78	0	4.978	68	2.04	0	°	110	3.3	1 °	0	152	4.56	0	0	194	5.82	0	0
27	0.81	0	5.264	65	2.07	0	0	111	3.33		0	153	4,59	0	0	195	5.85	0	0
28	0.84		4.45	70	2.1		0	112	3.36	0		154	4.62	0	0	196	5.88	0	0
24	0.87		1.643		2.13		0	112	3.39	1		150	4.65			197	5.91		0
3	0.9		0.232	1	2,18				3.42			150	4.00			198	5.94		0
31	0.93		0.032		2.19				3.45			15	4./1			199	5.97		0
3	2 0.90			1.	2.22				3.40			150	4.74			200	′  °	ľ	
	0.99			12	2.25	1.			3.51				4.11						
3	1.02			12	2.28				3.54			10	4.0	l .				1	
	1,05			12	2.31			1.70	3.57				4.03						
3	7 1 1 14			12	2.34		1	12	3.0			10	3 4 80						
				1.	2.3/			12	3.03				4.09	1 %					
1.	1 1 4 7			1				1	3 3 80		1		5 4 05			1			1
				l,	2.43			12	4 3.72			16	6 4 98						
Ľ	1 1 2				2 2 40			12	3.75			10	7 5.01						
4	2 1.25	0	ő	8	4 2.52	0	l ő	12	8 3.78	0	ő	16	8 5.04	0	l ő				1



Time, µs

Normalised Amplitude (dimensionless units)

DSTO-TN-0125

Beamwidth angle beta (degrees):	2
Great circle distance I (km):	300
Elevation angle phi (degrees):	5
Number of knots inside the scattering volume n:	1000
Operating frequency (MHz):	2800
Pulse rise time (µs):	0.1
Pulse width (µs):	0.5
Pulse fall time (µs):	0.15

i	Time[i]	Am	nplitude	i	Time[i]	Am	plitude	i	Time[i]	An	nplitude	i	Time[i]	Am	plitude	i	Time[i]	An	plitude
		(arbit	rary units)			(arbitr	ary units)			(arbit	rary units)	1		(arbit	rary units)			(arbit	rary units)
		Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting
1	0.03	0.3	1.092	43	1.29	0	10.602	85	2.55	0	0	127	3.81	0	0	169	5.07	0	0
2	0.06	0.6	2.227	44	1.32	0	10.161	86	2.58	0	0	128	3.84	0	0	170	5.1	0	0
3	0.09	0.9	2.725	45	1.35	0	9.798	87	2.61	0	0	129	3.87	0	0	171	5.13	0	0
4	0.12	1	3.266	46	1.38	0	7.356	88	2.64	0	o	130	3.9	0	0	172	5.16	0	0
5	0.15	1	5.524	47	1.41	0	5.425	89	2.67	0	o	131	3.93	0	0	173	5.19	0	0
6	0.18	1	9.197	48	1.44	0	4.941	90	2.7	0	0	132	3.96	0	0	174	5.22	0	0
7	0.21	1	13.159	49	1.47	0	5.154	91	2.73	0	0	133	3.99	0	0	175	5.25	0	0
8	0.24	1	16.307	50	1.5	0	4.411	92	2.76	0	0	134	4.02	0	0	176	5.28	0	0
9	0.27	1	16.142	51	1.53	0	4.223	93	2.79	0	0	135	4.05	0	0	177	5.31	0	0
10	0.3	1	20.073	52	1.56	0	4.565	94	2.82	0	0	136	4.08	0	0	178	5.34	0	0
11	0.33	1	23.898	53	1.59	0	4.54	95	2.85	0	0	137	4.11	0	0	179	5.37	0	0
12	0.36	1	30.251	54	1.62	0	4.576	96	2.88	0	0	138	4.14	0	0	180	5.4	0	0
13	0.39	1	36.069	55	1.65	0	3.43	97	2.91	0	0	139	4.17	0	0	181	5.43	0	0
14	0.42	1	39.101	56	1.68	0	2.202	98	2.94	0	0	140	4.2	0	0	182	5.46	0	0
15	0.45	1	41.745	57	1.71	0	0.875	99	2.97	0	0	141	4.23	0	0	183	5.49	0	.0
16	0.48	1	39.632	58	1.74	0	0.511	100	3	0	0	142	4.26	0	0	184	5.52	0	0
17	0.51	1	37.914	59	1.77	0	0.311	101	3.03	0	0	143	4.29	0	0	185	5.55	0	0
18	0.54	1	35.567	60	1.8	0	0.111	102	3.06	0	0	144	4.32	0	0	186	5.58	0	0
19	0.57	1	34.7	61	1.83	0	0	103	3.09	0	0	14	5 4.35	0	0	187	5.61	0	0
20	0.6	1	35.275	62	2 1.86	. 0	0	104	3.12	0	0	14	3 4.38	0	0	188	5.64	0	0
21	0.63	0.8	37.663	63	1.89	0	0	105	3.15	0	0	14	4.41	0	0	189	5.67	0	0
2	2 0.66	0.6	41.095	64	1.92	0	0	106	3.18	0	0	14	3 4.44	0	0	190	5.7	0	0
23	3 0.69	0.4	43.956	65	5 1.95	0	0	107	3.21	0	0	14	9 4.47	0		191	5.73	0	0
2	4 0.72	0.2	44.555	66	3 1.98	0	0	108	3.24	0	0	15	0 4.5	0	0	192	2 5.76	0	0
2	5 0.75	0	43.177	6	7 2.01	0	0	109	3.27	0	0	15	1 4.53	0	0	193	5.79	0	0
2	6 0.78	0	41.212	6	3 2.04	0	0	110	3.3	0	0	15	2 4.56	0	0	194	5.82	0	0
2	7 0.81	0	38.653	6	9 2.07	0	0	111	3.33	0	0	15	3 4.59	0	l °	195	5 5.85		0
2	8 0.84	0	36.077	7	D 2.1	0	0	112	2 3.36	0	0	15	4 4.62	0	0	196	5 5.88		
2	9 0.87	0	33.739	7	1 2.13	0	0	11:	3 3.39	0	0	15	5 4.65	0	0	19	5.91	l °	0
3	0.9	0	30.5	7	2 2.16	0	0	11	4 3.42	1°	0	15	6 4.68			19	5.94		
3	1 0.93	0	27.016	7	3 2.19	0	0	118	3.45	0		15	4.71			19	5.9/		
3	2 0.96	0	22.756	7	4 2.22	0	0	11	3.48			15	4.74		0	20	6	l °	l u
3	3 0.99	0	16.268	7	5 2.25	0	0	11	7 3.51	1 °	0	11	9 4.77				1		
3	4 1.02	0	10.254	17	6 2.28	0	0	11	8 3.54			10	0 4.8			Į	1		
3	5 1.05	0	6.895	7	/ 2.31	1 0			9 357			10	4.83				1		
3	6 1.08	0	6.736		8 2.34			12	3.6				4.85				1		
13	1.11		7.36	1	9 2.37				3.63				4.88						
	8 1.14		/.985		2.4		0		∡ <u>3.66</u>				4.92				1		
	1.17		8.08	1	2.43			12	3 3.69				4.95			1			
ľ	1.2	.   °	8.666		2 2.46				- 3.72 - 3.72				27 5.04			ľ			
Ľ	1 1.23	:   ^	8.585		2.49			12	5 3./5 6 3.78				58 5 04						
- 1 -	12 1.20	, , , ,	1 10.117	ា	~ 2.02		1	11 '*				1		, v					





Beamwidth angle beta (degrees):	4
Great circle distance I (km):	300
Elevation angle phi (degrees):	2.1
Number of knots inside the scattering volume n:	1000
Operating frequency (MHz):	2830
Pulse rise time (us):	0.1
Pulse width (us):	0.5
Pulse fall time (µs):	0.15

ı	Tim	ie[i]	Am	plitude	i	Time[i]	Am	plitude	1	Time[i]	An	plitude	i	Tir	me(i)	Am	plitude	1	Time[i]	An	plitude
	l		(arbitr	ary units)			(arbitr	ary units)			(arbit	rary units)	1			(arbitr	ary units)			(arbit	rary units)
		T T	Initial	Resulting			Initial	Resulting			Initial	Resulting				Initial	Resulting			Initial	Resulting
1	0	.03	0.3	8.325	43	1.29	0	8.341	85	2.55	0	2.813	12	27	3.81	0	1	169	5.07	0	1
2	0	0.06	0.6	20.664	44	1.32	0	8.607	86	2.58	٥	2.813	12	28	3.84	0	1	170	5.1	0	1
3	0	0.09	0.9	28.265	45	1.35	0	8.636	87	2.61	0	2.813	12	29	3.87	0	1	171	5.13	0	1
4		).12	1	32.298	46	1.38	0	7.286	88	2.64	0	2.813	1:	30	3.9	•	0.924	172	5.16	0	
5	0	0.15	1	28.21	47	1.41	0	5.836	89	2.67	0	2.785	1	31	3.93	0	0.724	173	5.19	0	1
6	1	0.18	1	28.058	48	1.44	0	4.864	90	2.7	0	2.613	1	32	3.96	0	0.524	174	5.22		
7	1	0.21	1	29.739	49	1.47	0	4.535	91	2.73	0	2.444	1	33	3.99	0	0.324	175	5.25		
8	1	0.24	1	31.349	50	1.5	0	5.002	92	2.76	0	2.282		34	4.02	0	0.124	1/6	5.20		
9	1	0.27	1	33.626	51	1.53	0	5.114	93	2.79	0	2.125	1	35	4.05	0	0	177	5.51		
10	1	0.3	1	36.175	52	1.56	0	4.929	94	2.82	0	2		36	4.08	0		170	5.34	۱.	
1	1	0.33	1	38.007	53	1.59	0	4.348	95	2.85		2		37	4.11			180	5.57		
1	2   '	0.36	1	40.448	54	1.62	0	3.415	96	2.88		1.749		138	4.14			181	5.43		
1	3	0.39	1	40.695	55	1.65	l °	2.604	97	2.91		1.349		139	4.17		0.319	182	5.48		1
1	4	0.42	1	40.907	56	1.68	0	2.063	88	2.94		0,949			4.23		0.919	183	5.49		1
1	5	0.45	1	43.106	57	1.71	l °	1.641	99	2.97		0.549			4.25		1 519	184	5 52	0	
1	6	0.48	1	44.858	58	1.74	0	1.285	100	1		0.149		143	4 29		2	185	5.55	0	1
1	7	0,51	1	46.885	58	1.77		1.285	101	3.03				144	4.32	ő	2	186	5.58	0	0.816
1	8	0,54	1	47.681	60	1.8		1.265	102	3.00			1	145	4.35	0	2	187	5.61	0	0.616
	9	0.57		46.215	ຼີ	1.83	1	1 381	104	3.12	۱.			146	4.38	0	2	186	5.64	0	0.418
		0.6		43.815		1.00	۱.	1.001	105	3 15	0	0		147	4.41	0	2	189	5.67	0	0.216
		0.03	0.0	28.30		4 1 1 92		1 597	106	3.18	0	0		148	4.44	0	2	190	5.7	0	0.016
	2	0.00	0.0	20.38		1 1 05		1 731	107	3.21	0			149	4.47	0	2	19	1 5.73	0	0
1	24	0.03	0.7	19 463	6	8 1 98		1.864	108	3 3.24	0	0		150	4.5	0	2	19	2 5.76	0	0
	25	0.75	0.1	14 717	l e	7 201		1,893	109	3.27	0	0	ŀ	151	4.53	0	2	19	3 5.79	0	0
	28	0.78	l õ	13.98	6	8 2.04	0	1,922	110	3.3	0	0.114	:	152	4.56	0	2	19	4 5.82	0	0
	27	0.81	0	14.974	6	9 2.07	0	1.934	11	3.33	0	0.41	•	153	4.59	0	2	19	5 5.85	0	0
	28	0.84	0	12.969	17	0 2.1	0	1.73	11:	2 3.36	0	0.71	4	154	4.62	0	2	19	6 5.88	0	0
	29	0.87	0	11.699	7	1 2.13	0	1.524	11	3 3.39	0	1	- 1	155	4.65	0	2	19	7 5.91	0	0
	30	0.9	0	8.735	17	2 2.16	0	1.354	11	4 3.42	0	1	- 11	156	4.68	0	2	19	8 5.94	*   °	0
	31	0.93	0	6.322	17	3 2.19	0	1.322	11	5 3.45	5 <b>0</b>	1	- 11	157	4.71	0	2	19	9 5.9	7   0	0
1	32	0.96	0	5.021	17	4 2.22	2 0	0.98	11	6 3.48	3 0	1	1	158	4.74	0	2	20	6 0	°	°
	33	0.99	0	4.079	17	5 2.2	5 0	0.703	11	7 3.51	0	1		159	4.77	0	2				
	34	1.02	0	4.917		76 2.2	3 0	0.963	11	8 3.54	4   O	1		160	4.8	0	1.788				1
	35	1.05	0	6.483		77 2.3	1 0	1.66	11	9 3.5	7 0	1 1		161	4.83	0	1.388		1		1
	36	1.08	0	8.225	:    :	78 2.3	4 0	2.405	12	3.6			ľ	162	4.86	0	0.988				1
	37	1.11	0	8.815	•   ·	79 2.3	7 0	2.813	12	3.6	3 0	1		163	4.89		0.588				
	38	1.14	0	9.456		80 2.4	۰ I ۱	2.813	12	22 3.6	6 0	1		164	4.92		0.188				
	39	1.17	0	9.176	3	81 2.4	3 0	2.813	12	23 3.6	9 0			165	4.95		0074				
	40	1.2	0	7.649	•	82 2.4	6 0	2.813	1	24 3.7	2 (	!!!		166	4,98		0.270				
	41	1.23	0	7.41	2	83 2.4	9 0	2.813		25 3.7	5 0			167	5.0		0.876				1
	42	1.26	0	7.62	5	84 2.5	2 0	2.813	111	20 3.7	°   '	·   ·		11.106	1 3.0		0.010				





(etim sesinoisnamib) abutilqmA basilomison

Beamwidth angle beta (degrees):	8
Great circle distance I (km):	300
Elevation angle phi (degrees):	4.1
Number of knots inside the scattering volume n:	1000
Operating frequency (MHz):	2830
Pulse rise time (µs):	0.1
Pulse width (µs):	0.5
Pulse fall time (µs):	0.15

i	Time[i]	An	plitude	i	Time[i]	Am	nplitude	i	Time[i]	Am	plitude	i	Time[i]	Am	plitude	i	Time[i]	Am	plitude
		(arbit	rary units)			(arbiti	rary units)			(arbit	rary units)			(arbit	rary units)			(arbit	rary units)
		Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting
1	0.03	0.3	4.2	43	1.29	0	13.484	85	2.55	0	5.451	127	3.81	0	1.793	169	5.07	0	2.836
2	0.06	0.6	9.2	44	1.32	0	15	86	2.58	0	5.115	128	3.84	0	1.981	170	5.1	0	2.836
3	0.09	0.9	14.26	45	1.35	0	14.854	87	2.61	0	4.66	129	3.87	0	1.981	171	5.13	0	2.836
4	0.12	1	17.176	46	1.38	0	13.859	88	2.64	0	4.168	130	3.9	0	1.981	172	5.16	0	2.836
5	0.15	1	16.486	47	1.41	0	12.773	89	2.67	0	3.634	131	3.93	0	2.186	173	5.19	0	2.836
6	0.18	1	16.243	48	1.44	0	11.524	90	2.7	0	3.373	132	3.96	0	2.555	174	5.22	0	2.836
7	0.21	1	16.386	49	1.47	0	10.928	91	2.73	0	3.22	133	3.99	0	3.061	175	5.25	0	2.836
8	0.24	1	15.854	50	1.5	0	11.034	92	2.76	0	2.017	134	4.02	0	2.968	176	5.28	0	2.836
9	0.27	1	14.569	51	1.53	0	9.837	93	2.79	0	1.989	135	4.05	0	2.538	177	5.31	0	2.836
10	0.3	1	13.437	52	1.56	0	7.151	94	2.82	0	1.685	136	4.08	0	2.041	178	5.34	0	2.635
11	0.33	1	13.681	53	1.59	0	6.056	95	2.85	0	2.208	137	4.11	0	1.336	179	5.37	0	2.249
12	0.36	1	13.045	54	1.62	0	5.826	96	2.88	0	1.81	138	4.14	0	0.77	180	5.4	0	1.98
13	0.39	1	11.505	55	1.65	0	7.212	97	2.91	0	1.938	139	4.17	0	0.612	181	5.43	0	2.017
14	0.42	1	11.937	56	1.68	0	7.585	98	2.94	0	1.316	140	4.2	0	1.077	182	5.46	0	2.064
15	0.45	1	14.357	57	1.71	0	7.246	99	2.97	0	1.122	141	4.23	0	1.803	183	5.49	0	2.1
16	0.48	1	18.554	58	1.74	0	6.036	100	3	0	1.761	142	4.26	0	2.102	184	5.52	0	1.45
17	0.51	1	21.987	59	1.77	0	5.97	101	3.03	0	2.265	143	4.29	0	2.176	185	5.55	0	1.144
18	0.54	1	22.489	60	1.8	0	7.327	102	3.06	0	2.339	144	4.32	0	1.903	186	5.58	0	1.233
18	0.57	1	21.963	61	1.83	0	8.785	103	3.09	0	2.446	145	4.35	0	1.478	187	5.61	0	1.424
20	0.6	1	18.666	62	1.86	0	10.634	104	3.12	0	2.603	146	4.38	0	1.22	188	5.64	0	1.638
2	0.63	0.8	13.431	63	1.89	0	13.298	105	3.15	0	2.713	147	4.41	0	1.039	189	5.67	0	1.638
2	2 0.66	0.6	8.402	64	1.92	0	16.002	106	3.18	0	2.791	148	4.44	0	0.902	190	5.7	0	1.638
2	0.69	0.4	5.118	65	5 1.95	0	18.004	107	3.21	0	2.539	149	4.47	0	0.788	191	5.73	1 °	1.638
24	0.72	0.2	2.062	66	3 1.98	0	19.544	108	3.24	0	2.427	150	4.5	0	0.727	192	5.78	0	1.638
2	5 0.75	0	3.752	67	2.01	0	20.59	109	3.27	0	2.491	151	4.53	۰ I	0.478	193	5.79	<b>°</b>	1.638
2	3 0.78	0	6,346	68	3 2.04	0	20.262	110	3.3	0	2.463	152	4.56	0	0.274	194	5.82	0	1.638
2	0.81	0	9.377	69	2.07	0	19.236	111	3.33	0	1.987	153	4.59	0	0.491	195	5.85	0	1.494
2	3 0.84	0	11.257	70	2.1	0	18.03	112	3.36	0	0.858	154	4.62	0	0.55	196	5.88	0	1,185
2	9 0.87	0	13.937	71	1 2.13	0	16.221	113	3.39	0	0.643	155	4.65	0	0.537	197	5.91	0	1.139
3	0.9	0	15.914	72	2 2.16	0	13.427	114	3.42	0	1.614	156	4.68	0	0.28	198	5.94	0	1.379
3	1 0.93	0	17.166	73	3 2.19	0	11.844	115	3.45	0	2.226	157	4.71	0	0.236	199	5.97	0	1.379
3	2 0.96	0	19,168	74	4 2.22	0	11.283	116	3.48	0	2.219	158	4.74	l °	0.582	200	6	0	1.289
3	3 0.99	0	19.947	7	5 2.25	0	11.751	117	3.51	0	1.153	159	4.77	0	0.935	1			
3	4 1.02	0	18.085	7	6 2.28	0	12.079	118	3 3.54	0	1.538	160	4.8	1°	1.556	1			1
3	5 1.05	0	15.624	7	7 2.31	0	11.653	118	3.57	0	2.346	161	4.83	0	2.096				
13	6 1.08	0	12.471	7	8 2.34	0	10.515	120	3.6	0	2.156	162	4,86	0	2.189				
3	7 1.11	0	9.01	7	9 2.37	0	9.894	12	3.63	°.	2.068	163	4.89	l °	2.427				
3	8 1.14	0	8.165	8	0 2.4	0	8.612	12	3.66	l °	2.07	164	4.92	1 °	2.426	1			1
3	8 1.17	۰ I	8.997	8	1 2.43	l °	7.762	123	3 3.69	0	1.996	16	4.95	l °	2.436	l.		1	1
14	0 1.2	0	9.42	8	2 2.48	0	7.415	12	4 3.72	0	1.679	160	4.98	0	2.629			1	
14	1 1.23	0	9.895	8	3 2.49	0	6.776	12	5 3.75	0	1.385	16	5.01		2.824		1		1
- 14	21 1.26	1 0	1 12.134	11 8	4 2.52	1 0	6.125	11 12	51 3.78	1 0	1 1.481	11 16	5 5.04	1 0	2.836	11		1	1

## Appendix B: Computations of Radar Pulse Envelope Distortion for Random Distribution



Grid with random distribution of knots



Beamwidth angle beta (degrees):	1.2
Great circle distance I (km):	300
Elevation angle phi (degrees):	0.7
Number of knots inside the scattering volume n:	1000
Operating frequency (MHz):	2830
Pulse rise time (µs):	0.1
Pulse width (µs):	0.5
Pulse fall time (μs):	0.15

i	Time[i]	Ал	nplitude	1	Time[i]	Am	nplitude	i	Time[i]	Ап	plitude	i	Time[i]	Am	plitude	1	Time[i]	An	plitude	
		(arbit	rary units)		1	(arbit	rary units)			(arbit	rary units)			(arbitr	ary units)			(arbit	rary units)	
		Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting	
1	0.03	0.3	4.012	43	1.29	0	0	85	2.55	0	0	127	3.81	0	0	169	5.07	0	0	
2	0,06	0.8	7.129	44	1.32	0	0	86	2.58	0	o	128	3.84	0	٥	170	5.1	0	0	
3	0.09	0.9	12.174	45	1.35	0	0	87	2.61	0	0	129	3.87	· 0	0	171	5.13	0	0	
4	0.12	1	17.2	46	1.38	0	0	88	2.64	0	0	130	3.9	0	0	172	5.16	0	0	
5	0.15	1	25.452	47	1.41	0	0	89	2.67	0	0	131	3.93	0	0	173	5.19	0	0	
6	0.18	1	33.082	48	1.44	0	D	. 90	2.7	0	0	132	3.96	0	0	174	5.22	0	0	
7	0.21	1	38.284	49	1.47	0	0	91	2.73	0	0	133	3.99	0	0	175	5.25	0	0	
8	0.24	1	40.247	50	1.5	0	0	92	2.76	0	0	134	4.02	0	0	176	5.28	0	0	
9	0.27	1	40.471	51	1.53	0	0	93	2.79	0	0	135	4.05	0	0	177	5.31	0	0	
10	0.3	1	40.558	52	1.56	0	0	94	2.82	0	0	136	4.08	0	0	178	5.34	0	0	
11	0.33	1	40.558	53	1.59	0	0	95	2.85	0	0	137	4.11	0	0	179	5.37	0	0	
12	0.36	· 1	40.558	54	1.62	0	0	96	2.88	0	0	138	4.14	0	0	180	5.4	0	0	
13	0.39	1	40.558	55	1.65	0	0	97	2.91	0	0	139	4.17	0	0	181	5.43	0	0	
14	0.42	1	40,558	56	1.68	0	0	98	2.94	0	0	140	4.2	0	0	182	5.46	0	0	
15	0.45	1	40.558	57	1.71	0	0	99	2.97	0	0	141	4.23	0	0	183	5.49	0	0	
18	0.48	1 1	40.558	58	1.74	0	0	100	3	0	0	142	4.26	0	0	184	5.52	0	0	
17	0.51	1	40.558	59	1.77	0	0	101	3.03	0	0	143	4.29	0	0	185	5.55	0	0	
18	0.54	1	40.558	60	1.8	0	0	102	3.06	0	0	144	4.32	0	0	186	5.58	0	0	
19	0.57	1	40.558	61	1.83	0	0	103	3,09	0	0	145	4.35	0	0	187	5.61	0	0	
20	0.6	1	40.558	62	1.86	0	0	104	3.12	0	0	146	4.38	0	0	188	5.64	0	•	
21	0,63	0.8	40.731	63	1.89	0	0	105	3.15	0	0.	147	4.41	0	0	189	5.67	0	0	
22	0.66	0.6	38.705	64	1.92	0	0	106	3.18	0	0	148	4.44	٥	0	190	5.7	0	0	
23	0.69	0.4	35.273	65	5 1.95	0	0	107	3.21	0	0	149	4.47	0	. 0	191	5.73	0	•	
24	0.72	0.2	30.394	66	3 1.98	0	0	108	3.24	0	0	150	4.5	0	0	192	5.78	0	0	1
25	0.75	0	22.659	67	7 2.01	0	0	109	3.27	0	0	151	4.53	0	0	193	5,79	0	0	1
26	6 0.78	0	14.311	68	3 2.04	0	0	110	3.3	0	0	152	4.56	0	0	194	5.82	0	0	i
27	0.81	0	8.296	69	2.07	0	0	111	3.33	0	0	153	4,59	0	0	195	5.85	0	0	
28	3 0.84	0	4.151	70	2.1	0	0	112	3.36	0	٥	154	4.62	0	0	196	5.88	0	0	
29	0.87	0	1.484	7	1 2.13	0	0	113	3.39	0	0	155	4.65	0	0	197	5.91	0	0	1
30	0.9	0	0.2	7:	2 2.16	0	0	114	3.42	0	0	156	4.68	0	0	198	5.94	0	0	
3'	1 0.93	0	0	7:	3 2.19	0	0	115	5 3.45	0	0	157	4.71	0	0	199	5.97	0	0	
33	2 0.96	0	0	74	4 2.22	0	0	118	3.48	0	0	158	4.74	0	0	200	6	0	0	
3	3 0,99	0	0	7	5 2.25	0	0	117	3.51	0	0	159	4.77	0	•					
3	4 1.02	0	•	7	6 2.28	0	0	118	3 3.54	0	0	160	4.8	0	0					
3	5 1.05	0	0	17	7 2.31	0	0	118	3.57	0	0	16	4.83	0	۰ I		1			
3	8 1.08	0	•	7	8 2.34	0	0	120	3.6	0	•	16	4.86	0	0			1		
3	7 1.11	0	0	7	9 2.37	0	•	12	3.63	0	0	16:	3 4.89	0	0	1		1		
3	8 1.14	0	•	8	0 2.4	0	0	12	2 3.66	0	•	16	4 4.92	0	0	1			1	
3	9 1.17	0	0	8	1 2.43	0	0	12	3 3.69	0	0	16	5 4.95	0	0			1		ľ
4	0 1.2	0	0	8	2 2.46	0	0	12	4 3.72	0	0	16	6 4.98	°	0					l
4	1 1.23	0	0	8	3 2.49	0	0	12	5 3.75	0	0	16	7 5.01	0			1			L
14	21 1.26	1 0	0	18	4 2.52	1 0	1 0	11 12	6 ( 3.78	1 0	1 0	1 16	8 5.04	0	1 0	1	1		1	

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Beamwidth angle beta (degrees):	2
Great circle distance I (km):	300
Elevation angle phi (degrees):	4
Number of knots inside the scattering volume n:	1000
Operating frequency (MHz):	2800
Pulse rise time (us):	0.1
Pulse width (µs):	0.5
Pulse fall time (µs):	0.15

i	Time[i]	Amplitude		i	Time[i]	Arr	plitude	i	Time[i]	Amplitude		1	i Time[i] Amplitude		1	Time[i]	An	plitude		
		arbit	rary units)	'		(arbit	rary units)			(arbitrary units)				(arbite	ary units)			(arbit	rary units)	
	ł	Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting	
1	0.03	0.3	1,055	43	1.29	0	12.628	85	2.55	0	0	127	3.81	0	0	169	5.07	0	0	İ.
2	0.06	0.6	2.412	44	1.32	0	10.248	86	2.58	0	0	128	3.84	0	0	170	5.1	0	0	l.
3	0.09	0.9	4.094	45	1.35	0	7.891	87	2.61	0	0	129	3.87	0	0	171	5.13	0	0	Ĺ
4	0.12	1	8.946	46	1.38	0	6.667	88	2.64	0	0	130	3,9	0	0	172	5.16	0	0	Í.
5	0.15	1	13.161	47	1.41	0	5.317	89	2.67	0	0	131	3.93	0	0	173	5.19	0	0	
6	0.18	1	17.091	48	1.44	0	3.978	90	2.7	0	0	132	3.96	0	0	174	5.22	0	0	L
7	0.21	1	16.751	49	1.47	0	2.668	91	2.73	0	0	133	3.99	0	0	175	5.25	0	0	1
8	0.24	1	12.496	50	1.5	0	1.374	92	2.76	0	0	134	4.02	0	0	176	5.28		0	
9	0.27	1	10.864	51	1.53	0	0.693	93	2.79	0	0	135	4.05	0	0	177	5.31	0	0	L
10	0.3	1	11.494	52	1.56	0	0.493	94	2.82	0	0	136	4.08	<u>Р</u> .	0	178	5.34			1
11	0.33	1	13.042	53	1.59	0	0.293	95	2.85	0	0	137	4.11		• 0	179	5.37			
12	0.36	1	13.158	54	1.62	0	0.093	96	2.88	0	0	138	4.14	0	0	180	5.4			
1:	0.39	1	13.967	55	1.65	0	0	97	2.91	0	0	139	4.17	0	0	181	5.43			1
11	0.42	1	17.627	56	1.68	0	0	98	2.94	0		140	4.2			182	5.40			Ł
1	6 0.45	1	24.203	57	1.71	0	0	99	2.97			141	4.23	0		103	5.49			
1	3 0.48	1	30.908	58	1.74	0	0	100	3	0		142	4.26			185	5.55			
1	7 0.51	1	36.937	59	1.77	0		101	3.03			140	4.29			186	5.58			
1	B 0.54	1	39.337	60	1.8			10.	2 3.06			144	4.32			187	5.61			
1	9 0.57	11	40.692	61	1.83		0	10.	3 3.09			14	4.55			188	5.64	0	0	L
2	0 0.6		41.491	62	2 1.86			104	3.12			14				189	5.67	0	0	1
	1 0.63	0.8	39.367		1.09			10	8 3 18			14	3 4.44	l õ	0	190	5.7	0	0	ł
	2 0.66	0.6	30.109		1.92			10	7 321			14	9 4.47	0	0	19	1 5.73	0	0	
1	3 0.09	0.4	30.528		8 1 1 98			10	8 3.24	0	0	15	0 4.5	0	· 0	19	2 5.76	0	0	L
	6 0.72	0.2	42 72	Ĩ	7 201			10	9 3.27	0	0	15	1 4.53	0	0	19	3 5.79	0	0	1
	6 0.79		45 483	l e	8 204	0		11	0 3.3	0	0	15	2 4.56	0	0	19	4 5.82	0	0	
	7 0.81		47.33	6	9 2.07		0	11	1 3.33	0	0	15	3 4.59	0	0	19	5 5.85	0	0	L
	8 0.84		46,909	7	0 21	0	0	11	2 3.36	0	0	15	4 4.62	0	0	19	6 5.88	0	0	1
	9 0.87		44.501	7	1 2.13	0	0	11	3 3.39	0	0	15	5 4.65	0	0	19	7 5.91	0	0	
	0.9	0	41.046	17	2 2.16	0	0	11	4 3.42	0	0	15	6 4.68	0	0	19	8 5.94	0	0	1
	31 0.93	3 0	37.939	7	3 2.19	0	0	11	5 3.45	0	0	15	7 4.71	0	0	19	9 5.97	0	0	
	32 0.96	5 O	35.688	7	4 2.22	0	0	11	6 3.48	0	0	15	8 4.74	0	0	20	0 6	0	0	
	33 0.99	0	35.073	7	5 2.25	0	0	11	7 3.51	0	0	15	9 4.77	0	0	1				
	34 1.03	2 0	31.582	:    7	6 2.28	0	0	11	8 3.54	0	0	16	0 4.8	0	0	ĥ			1	
1	35 1.0	5 0	26.922	:    7	7 2.31	0	0	11	9 3.57	0	0	16	61 4.83	0	0					
	36 1.04	3 0	22.673	17	8 2.34	0	0	12	20 3.6	0	0	16	52 4.86	0	0		1			
	37 1.1	1 0	19.573	17	9 2.37	/   o	0	12	21 3.63	0	0	16	33 4.89	0	0					
	38 1.1	4 0	18.176	3    8	30 2.4	0	0	1	22 3.66	0	0	16	34 4.92	2 0	0	l.		1		
	39 1.1	7 0	18.173	3    8	31 2.43	3 0	0	1	23 3.69	0	0	1	35 4.95	5 0	0		1			
1	40 1.2	2 0	18.72	7    ł	32 2.46	3   0	0	1	24 3.72	2 0	0	10	56 4.98	3 0	0					1
	41 1.2	3 0	17.54	5    4	33 2.4	9 0	0	1	25 3.75	5 0	0	1	87 5.0						1	
	42 1.2	6 0	15.01	2	84 2.5	2 0	0	1	26 3.78	3 0	0	1	68 5.0	<u>ه ا</u> د	0					_

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Reamwidth angle beta (degrees):	4
Great circle distance I (km):	300
Elevation angle phi (degrees):	2.1
Number of knots inside the scattering volume n:	1000
Operating frequency (MHz):	2830
Pulse rise time (us):	0.1
Pulse width (us):	0.5
Pulse fall time (us):	0.15

	Time		Amplitude		Amplitude		1 Amplitude		;	Timelil	Am	plitude	i	Time	An	nplitude	i	Time[]]	Алт	plitude	11	Time[i]	An	plitude	
'	1	-113			l .		(arbit	arv units)			(arbit	rary units)			(arbiti	rary units)	1		(arbit	rary units)					
		H	(arbit	ary units)			Initial	Reculting			Initial	Resulting	1		Initial	Resulting		1	Initial	Resulting					
			nital	Resulting	-	1 20	0	4.73	85	2.55	0	0.349	127	3,81	0	1.573	169	5.07	0	0.832	Ĺ				
1	0.	.03	0.3	1,190	43	1.23		4 598	86	2.58	0	0.347	128	3.84	0	1.573	170	5.1	0	0.632					
2	0.	.06	0.0	10.012	44	1.32		4 287	87	2.61	0	0.347	129	3.87	0	1.573	171	5.13	0	0.432	L				
Ľ		42	1.9	20.132	48	1.38	l o	3.913	88	2.64	0	0.347	130	3.9	0	1.573	172	5,16	0	0.232					
	١	12		31.009	40	1.41	0	3.91	89	2.67	0	0.347	131	3.93	0	1.573	173	5.19	0	0.032	L				
ι.	۱.	40		35 371	48	1.44	0	3,998	90	2.7	0	0.347	132	3.96	0	1.573	174	5.22	0	0	1				
ľ,	1	21		44 845	49	1.47	0	3,998	91	2.73	0	0.343	133	3.99	0	1.573	175	5.25	0	0	1				
Ľ	1	24		53.907	50	1.5	0	3.998	92	2.76	0	0.414	134	4.02	0	1.547	176	5.28	0	0					
l .		27		61,915	51	1.53	0	3.998	93	2.79	0	0.552	135	4.05	0	1.477	177	5.31	0	0	Į.				
10		0.3	1	64,519	52	1.56	0	3.998	94	2.82	0	0.72	136	4.08	0	1.432	178	5.34	0	0	L				
	1.	1.33	1	64.268	53	1.59	0	3.998	95	2.85	0	0.901	137	4.11	0	1,337	175	5.37	0	0					
1		1.36	1	63.382	54	1.62	0	3.998	96	2.88	0	1	138	4.14	0	1.21	180	5.4	0	0					
1	3 0	0.39	1	63.526	55	1.65	0	3.998	97	2.91	0	1	13	4.17	0	1.144	18	5.43	0	0					
1	4 0	0.42	1	63.575	56	1.68	0	3.998	98	2.94	0	1 1	14	4.2	0	0,954	18	2 5.46	0	0	Ł				
	5 6	0.45	1	63.529	5	1.71	0	3.828	99	2.97	0	1	14	1 4.23	0	0.701	18	3 5.49			Ł				
1	6	0.48	1	63.522	5	3 1.74	0	3.619	100	3	0	1	14	2 4.26	0	0.487	18	4 5.52							
1	7	0,51	1	65.248	5	9 1.77	0	3.449	10'	3.03	0	1	14	3 4.29	0	0.287	18	5 5.55			ł				
1	8	0.54	1	68.462	6	0 1.8	0	3.491	10:	2 3.06	0	1	14	4 4.32	0	0.087	18	5.58			L				
1	9	0.57	1	73.087	6	1 1.83	0	3.374	10:	3 3.09	0	0,891	14	5 4.35			18	0 5.01	1	l ő					
2	:0	0.6	1	77.048	6	2 1.86	0	3.279	10	4 3.12	0	0.691	14	6 4.38				0 5.04							
12	1	0.63	0.8	75.013	6	3 1.89	0	3.062	10	5 3.15	0	0.491	14	7 4.41				5 5.07	1						
	22	0,66	0,6	70.84	6	4 1.92	. 0	2.574	10	6 3.18	0	0.291	11	8 4.44		0.052		5 75	.   .	0.254					
12	23	0.69	0.4	66.171	6	5 1.95	. 0	2.047	10	7 3.21	0	0.091		9 4.4/		0.200		576		0.554					
	24	0.72	0.2	61.137	6	6 1.98	0	1.855	10	8 3.24	0			4.5		0.000		3 570		0.854					
1:	25	0.75	0	54.312	:    e	2.0	0	1.855	10	9 3.27				4.54		1 1		5.8		1					
1	26	0.78	0	49.432	: [[•	38 2.0	4 O	1.855		0 3.3				53 4 50				95 5.8	5 0	1					
1	27	0.81	0	43.191		39 2.0		1.855		1 3.3				54 4.6				96 5.8	8 0	1 1					
	28	0.84	0	35.877		70 2.1		1.855		2 3.3				55 4.6	5 0			97 5.9	1 0	1					
	29	0.87	0	28.604		71 2.1	3 0	1./40		13 3.3		0.094		56 4.6	8 0	1	1	98 5.9	4 0	1					
	30	0.9	0	23.31	<u> </u>	72 21		1 388		15 34		0.394		57 4.7	1 0	1	1	99 5.9	7 0	1					
- 1	31	0.93		19.95		73 21		1 254		16 34	8 0	0.694		58 4.7	4 0	1	2	00 6	1	1					
	32	0.96		19.32	21	75 00	2   °	1 254		17 3.5		1.07		59 4.7	7 0	1	1								
- 1	33	0.99		19.44		78 22		1 254		18 3.5		1.281	ı    †	60 4.1	3 0	1									
1	34	1.02		19,60	ĭ	77 24		1,254		19 3.5	7	1.51	,    .	61 4.8	3 0	1				1					
	30	1.05		10.42		78 25		1.254		20 3.	6   1	0 1.674	4	162 4.8	6 0	1	1			1					
	30	1.08		18.19	Ĭ	79 2		1.254		21 3.6	33	0 1.58	9	163 4.8	39 (	1									
	31	1.11		18 19	, I	80 2	4 0	1,089		22 3.0	56	0 1.55	8	164 4.9	2 0	1 1			1	l					
	30	1.14		13.00		81 2	43 0	0.81		23 3.6	39	0 1.57	3	165 4.9	95 1	1 1									
	40	12		9,80	5	82 2	46 0	0.59	,    ·	124 3.	72	0 1.57	3	166 4.9	98	0 1									
	41	1 23		6,96	18	83 2	49 1	0.42	2	125 3.	75	0 1.57	3	167 5.	01	0 1	1								
	42	1 26		5.49		84 2	52	0.32	s    ·	126 3.	78	0 1.57	3	168 5.	04	0 1	1								

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Beamwidth angle beta (degrees):	8
Great circle distance I (km):	300
Elevation angle phi (degrees):	4.1
Number of knots inside the scattering volume n:	1000
Operating frequency (MHz):	2830
Pulse rise time (us):	0.1
Pulse width (us):	0.5
Pulse fall time (µs):	0.15

i	Tim	e(I)	Am	plitude	1	Time[i]	Am	plitude	i Time[i] Amplitude		1	Tim	e[i]	Amplitude		i	Time[i]	An	nplitude			
Ĺ	1	"	(arbitr	ary units)			(arbitr	ary units)			(arbit	rary units)	1			(arbitr	ary units)			(arbi	rary units)	
	1	h	nitial	Resulting			Initial	Resulting			Initial	Resulting		1		Initial	Resulting			Initial	Resulting	
1	0	.03	0.3	5.753	43	1.29	0	15.318	85	2.55	0	2.051	127	3.	.81	0	1.984	169	5.07	0	0.746	
2	0	.06	0.6	11.226	44	1.32	0	14.151	86	2.58	0	1.001	128	3.	.84	0	2.516	170	5.1	0	0.546	
3	0	.09	0.9	15.123	45	1.35	0	12.421	87	2.61	0	0.398	129	3	.87	0	2.722	171	5.13	0	0.346	
4	0	.12	1	13.946	46	1.38	0	10.485	88	2.64	0	0.923	130		3.9	0	2.815	172	5.16		0.146	
5	0	.15	1	12.391	47	1.41	0	9.325	89	2.67	0	1.181	13	3	.93	0	2.864	173	5.19	0		
6	0	).18	1	11.029	48	1.44	0	9.272	90	2.7	0	1.302	13:	2 3	.96	0	2.921	174	5.22		0.017	l
7	0	0.21	1	11.398	49	1.47	0	9.231	91	2.73	0	0.736	13	3 3	1.99	0	2.634	175	5.25		0.317	l
8	1	0.24	1	12.685	50	1.5	0	9.074	92	2.76	0	0.347	13		1.02	Š	2.597	177	5.31	ő	0.617	ł
9	1	).27	1	15.375	51	1.53	0	9.073	93	2.79	0	0.361	13		1.05	0	3.031	178	5.34	ŏ	0.921	l
10		0.3	1	18.887	52	1.56	l °	7.829	94	2.82		0.837	13	, ,	4.00	0	3.059	179	5.37		1,289	ł
1	1 (	0.33	1	20.709	53	1.59		5.798	95	2.85		1.59	13		4 1 4		3.059	180	5.4	0	1.58	ł
1	2	0.36	1	23.251	54	1.62		3.9	90	2.00		1.655	13		4 17	ů ů	3.059	181	5.43	0	1.873	1
1	3	0.39	1	25.258	55	1.65		3.514	37	2.01		1 677	14		4.2	0	3.02	182	5.46	0	1.968	۱
1	4	0.42	1	27.503	50	1.68		A 101		2.04		1.65	14		4.23	0	2.529	183	5.49	0	1.968	۱
Ľ	2	0.45	1	27.470	5	1.7		5 134	100	3	0	1.598	14	12	4.26	0	1.988	184	5.52	0	1.968	ł
Ľ	]	0.40		27.000	5	1 1 77		7.474	101	3.03	0	2.072	14	13	4.29	0	1.402	18	5.55	0	1.968	Į
Ľ	2	0.51		25.054	6	1 1.8		10.685	102	3.06	0	2.509	1	14	4.32	0	0.874	180	5.58	0	1.968	l
1.		0.57		24.458	6	1 1.83	0	12.503	103	3.09	0	2.19	1	45	4.35	0	0.487	18	7 5.61	0	1.968	1
	20	0.6		24.397	6	2 1.86	0	13.74	104	3.12	0	1.57	1	46	4.38	٥	0.581	18	8 5.64	0	1.968	l
	21	0.63	0.8	21.68	6	3 1.89	0	14.767	105	3.15	0	1.06	1	47	4.41	0	0.666	18	9 5.67	0	1.968	ł
	22	0.66	0.6	18.845	6	4 1.92	0	15.838	10	3.18	0	1.11	1	48	4.44	0	0.674	19	0 5.7	0	1,968	
	23	0.69	0.4	16.793	8	5 1.95	0	15.858	10	3.21	0	1.507	1	49	4.47	0	0.522	19	1 5.73	0	1.968	
	24	0.72	0.2	15.34	6	6 1.98	0	16.076	10	8 3.24	0	1.657	1	50	4.5	0	0.256	19	2 5.76	0	1,968	
	25	0.75	0	13.446	e	17 2.01	0	15.494	10	9 3.27	0	1.624	1	51	4.53	0	0.088	19	3 5.79	0	1.908	
	26	0.78	0	16.38	•	8 2.04	1 0	15.031	11	0 3.3	0	1.816	1	52	4.56	0	0.101	19	5.82		1.900	
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	29	0.87	0	17.026	°    '	2.1	3 0	13.225	11	3 3.39		2./89		58	4.00		0.802	19	8 5.94		1.368	
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1	34	1.02		10.59		77 22		6.407		9 3.5		1.93	,	161	4.83	0	1.385					
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	39	1.17	6	19.67	5	81 2.4	3 0	6.868	1	23 3.6	9	0 1.12	4	165	4.95	5 O	1.218	3				
	40	1.2	0	20.05	99	82 2.4	18 0	6.6	1	24 3.7	2	0 1.2	5	166	4.98	3 0	1.14	4				
	41	1.23	0	18.8	7	83 2.4	49 (	5.273	1	25 3.7	5	0 1.11	4	167	5.01		1.07				1	
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Prediction of Radar Pulse Envelope Distortion due to Tropospheric Propagation

#### Marina Oszerova

#### (DSTO-TN-0125)

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19. ABSTRACT This project is a part of research into the detection of radar signals at ranges well beyond the horizon by exploiting the effect of tropospheric scattering. A result of this work is a program written in C language which enables the distortion of the envelope of a given radar pulse, which occurs as a result of propagating over any path by tropospheric scattering, to be predicted.										

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